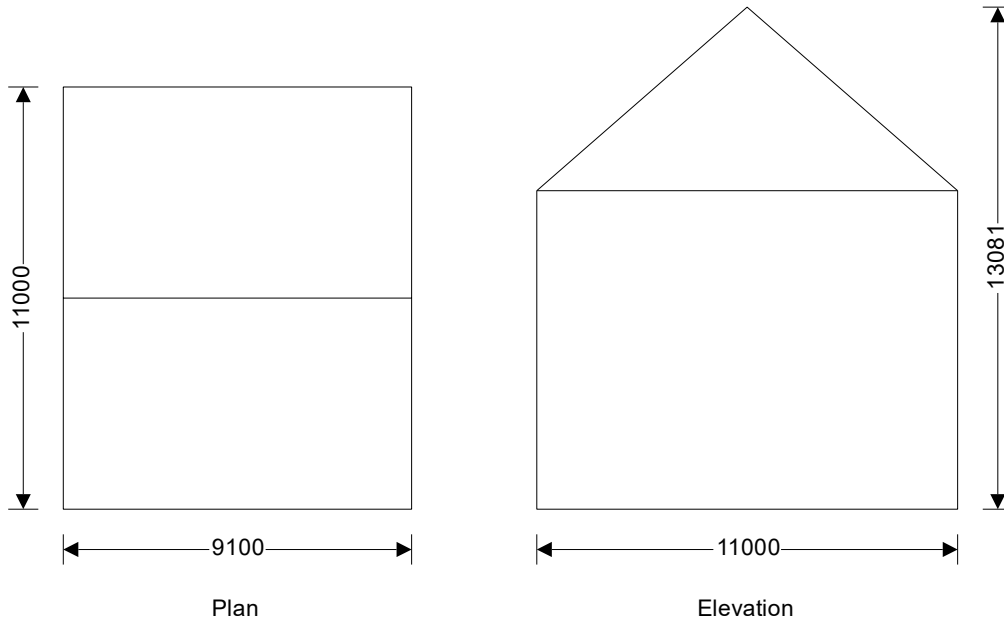
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WIND LOADING (EN1991-1-4)

TEDDS calculation version 3.0.15



Building data


Type of roof	Duopitch
Length of building	L = 9100 mm
Width of building	W = 11000 mm
Height to eaves	H = 8300 mm
Pitch of roof	$\alpha_0 = 41.0$ deg
Total height	h = 13081 mm

Basic values

Location	London
Wind speed velocity (FigureNA.1)	$V_{b,map} = 21.4$ m/s
Distance to shore	$L_{shore} = 66.00$ km
Altitude above sea level	$A_{alt} = 20.0$ m
Altitude factor	$C_{alt} = A_{alt} \times 0.001m^{-1} + 1 = 1.020$
Fundamental basic wind velocity	$V_{b,0} = V_{b,map} \times C_{alt} = 21.8$ m/s
Direction factor	$C_{dir} = 1.00$
Season factor	$C_{season} = 1.00$
Shape parameter K	$K = 0.2$
Exponent n	$n = 0.5$
Probability factor	$C_{prob} = [(1 - K \times \ln(-\ln(1-p)))/(1 - K \times \ln(-\ln(0.98)))]^n = 1.00$
Basic wind velocity (Exp. 4.1)	$V_b = C_{dir} \times C_{season} \times V_{b,0} \times C_{prob} = 21.8$ m/s
Reference mean velocity pressure	$q_b = 0.5 \times \rho \times v_b^2 = 0.292$ kN/m ²

Orography

Orography factor not significant	$c_o = 1.0$
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Terrain category	Town
Average height of surrounding buildings	$h_{ave} = 11000$ mm
Distance to nearest building	$X_{dis} = 5000$ mm
Distance upwind to shoreline	$L_{shore} = 66.0$ km
Distance inside town terrain	$L_{town} = 1.0$ km
Average height of surrounding buildings	$h_{ave} = 11000$ mm
Distance to nearest building	$X_{dis} = 5000$ mm

The velocity pressure for the windward face of the building with a 0 degree wind is to be considered as 1 part as the height h is less than b (cl.7.2.2)

The velocity pressure for the windward face of the building with a 90 degree wind is to be considered as 2 parts as the height h is greater than b but less than 2b (cl.7.2.2)

Peak velocity pressure - windward wall - Wind 0 deg and roof

Reference height (at which q is sought)	$z = 8300$ mm
Displacement height (Annex A.2)	$h_{dis} = \min(0.8 \times h_{ave}, 0.6 \times z) = 4980$ mm
Exposure factor (Figure NA.7)	$C_e = 1.69$
Exposure correction factor (Figure NA.8)	$C_{e,T} = 0.78$
Peak velocity pressure	$q_p = C_e \times C_{e,T} \times q_b = 0.38$ kN/m ²

Structural factor

Structural damping	$\delta_s = 0.100$
Height of element	$h_{part} = 8300$ mm
Size factor (Table NA.3)	$C_s = 0.85$
Dynamic factor (Figure NA.9)	$C_d = 1.04$
Structural factor	$C_s C_d = C_s \times C_d = 0.882$

Peak velocity pressure - windward wall (lower part) - Wind 90 deg

Reference height (at which q is sought)	$z = 11000$ mm
Displacement height (Annex A.2)	$h_{dis} = \min(0.8 \times h_{ave}, 0.6 \times z) = 6600$ mm
Exposure factor (Figure NA.7)	$C_e = 1.85$
Exposure correction factor (Figure NA.8)	$C_{e,T} = 0.82$
Peak velocity pressure	$q_p = C_e \times C_{e,T} \times q_b = 0.44$ kN/m ²

Structural factor

Structural damping	$\delta_s = 0.100$
Height of element	$h_{part} = 11000$ mm
Size factor (Table NA.3)	$C_s = 0.83$
Dynamic factor (Figure NA.9)	$C_d = 1.03$
Structural factor	$C_s C_d = C_s \times C_d = 0.862$

Peak velocity pressure - windward wall (upper part) - Wind 90 deg and roof

Reference height (at which q is sought)	$z = 13081$ mm
Displacement height (Annex A.2)	$h_{dis} = \min(0.8 \times h_{ave}, 0.6 \times z) = 7849$ mm
Exposure factor (Figure NA.7)	$C_e = 1.95$
Exposure correction factor (Figure NA.8)	$C_{e,T} = 0.84$
Peak velocity pressure	$q_p = C_e \times C_{e,T} \times q_b = 0.48$ kN/m ²

Structural factor

Structural damping	$\delta_s = 0.100$
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Height of element $h_{part} = 2081$ mm
 Size factor (Table NA.3) $C_s = 0.87$
 Dynamic factor (Figure NA.9) $C_d = 1.03$
 Structural factor $C_s C_d = C_s \times C_d = 0.897$

Structural factor

Structural damping $\delta_s = 0.100$
 Height of element $h_{part} = 13081$ mm
 Size factor (Table NA.3) $C_s = 0.83$
 Dynamic factor (Figure NA.9) $C_d = 1.03$
 Structural factor $C_s C_d = C_s \times C_d = 0.855$

Structural factor - roof 0 deg

Structural damping $\delta_s = 0.100$
 Height of element $h_{part} = 13081$ mm
 Size factor (Table NA.3) $C_s = 0.83$
 Dynamic factor (Figure NA.9) $C_d = 1.04$
 Structural factor $C_s C_d = C_s \times C_d = 0.865$

Peak velocity pressure for internal pressure

Peak velocity pressure – internal (as roof press.) $q_{p,i} = 0.48$ kN/m²

Pressures and forces

Net pressure $p = C_s C_d \times q_p \times C_{pe} - q_{p,i} \times C_{pi}$

Net force $F_w = p_w \times A_{ref}$

Roof load case 1 - Wind 0, $C_{pi} 0.20$, $-C_{pe}$

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
F (-ve)	-0.13	0.48	-0.15	5.49	-0.83
G (-ve)	-0.13	0.48	-0.15	5.49	-0.83
H (-ve)	-0.05	0.48	-0.12	55.34	-6.53
I (-ve)	-0.50	0.48	-0.30	55.34	-16.77
J (-ve)	-0.83	0.48	-0.44	10.97	-4.81

Total vertical net force $F_{w,v} = -22.47$ kN

Total horizontal net force $F_{w,h} = 8.78$ kN

Walls load case 1 - Wind 0, $C_{pi} 0.20$, $-C_{pe}$

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
A	-1.20	0.48	-0.60	16.55	-9.98
B	-0.80	0.48	-0.43	83.71	-36.34
C	-0.50	0.48	-0.31	17.34	-5.33
D	0.80	0.38	0.18	75.53	13.26
E	-0.51	0.38	-0.27	75.53	-20.29



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Overall loading

Equiv leeward net force for overall section $F_l = F_{w,WE} = -20.3$ kN
 Net windward force for overall section $F_w = F_{w,wD} = 13.3$ kN
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.86$ as h/W is 1.189
 Overall loading overall section $F_{w,D} = f_{corr} \times (F_w - F_l + F_{w,h}) = 36.3$ kN

Roof load case 2 - Wind 0, $c_{pi} -0.3$, $+c_{pe}$

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
F (+ve)	0.80	0.48	0.48	5.49	2.61
G (+ve)	0.57	0.48	0.38	5.49	2.09
H (+ve)	0.62	0.48	0.40	55.34	22.18
I (+ve)	-0.50	0.48	-0.06	55.34	-3.51
J (+ve)	-0.83	0.48	-0.20	10.97	-2.18

Total vertical net force $F_{w,v} = 15.99$ kN

Total horizontal net force $F_{w,h} = 21.37$ kN

Walls load case 2 - Wind 0, $c_{pi} -0.3$, $+c_{pe}$

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
A	-1.20	0.48	-0.36	16.55	-6.02
B	-0.80	0.48	-0.19	83.71	-16.28
C	-0.50	0.48	-0.07	17.34	-1.17
D	0.80	0.38	0.42	75.53	31.36
E	-0.51	0.38	-0.03	75.53	-2.20

Overall loading

Equiv leeward net force for overall section $F_l = F_{w,WE} = -2.2$ kN
 Net windward force for overall section $F_w = F_{w,wD} = 31.4$ kN
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.86$ as h/W is 1.189
 Overall loading overall section $F_{w,D} = f_{corr} \times (F_w - F_l + F_{w,h}) = 47.1$ kN

Roof load case 3 - Wind 90, $c_{pi} 0.20$, $-c_{pe}$

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
F (-ve)	-1.20	0.48	-0.59	8.02	-4.71
G (-ve)	-1.17	0.48	-0.58	8.02	-4.62
H (-ve)	-0.60	0.48	-0.34	64.13	-21.92
I (-ve)	-0.43	0.48	-0.27	52.47	-14.21

Total vertical net force $F_{w,v} = -34.31$ kN

Total horizontal net force $F_{w,h} = 0.00$ kN



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Walls load case 3 - Wind 90, c_{pi} 0.20, -C_{pe}

Zone	Ext pressure coefficient C _{pe}	Peak velocity pressure q _p , (kN/m ²)	Net pressure p (kN/m ²)	Area A _{ref} (m ²)	Net force F _w (kN)
A	-1.20	0.38	-0.49	18.26	-8.96
B	-0.80	0.38	-0.36	57.27	-20.56
D _b	0.80	0.44	0.21	112.61	23.52
D _u	0.80	0.48	0.25	4.98	1.24
E	-0.52	0.48	-0.31	117.60	-36.43

Overall loading

Equiv leeward net force for upper section $F_l = F_{w,WE} / A_{ref,WE} \times A_{ref,wu} = -1.5$ kN
 Net windward force for upper section $F_w = F_{w,wu} = 1.2$ kN
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.87$ as h/L is 1.437
 Overall loading upper section $F_{w,u} = f_{corr} \times (F_w - F_l + F_{w,h}) = 2.4$ kN
 Equiv leeward net force for bottom section $F_l = F_{w,WE} / A_{ref,WE} \times A_{ref,wb} = -34.9$ kN
 Net windward force for bottom section $F_w = F_{w,wb} = 23.5$ kN
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.87$ as h/L is 1.437
 Overall loading bottom section $F_{w,b} = f_{corr} \times (F_w - F_l) = 50.6$ kN

Roof load case 4 - Wind 90, c_{pi} -0.3, +c_{pe}

Zone	Ext pressure coefficient C _{pe}	Peak velocity pressure q _p , (kN/m ²)	Net pressure p (kN/m ²)	Area A _{ref} (m ²)	Net force F _w (kN)
F (+ve)	0.57	0.48	0.38	8.02	3.04
G (+ve)	0.47	0.48	0.34	8.02	2.71
H (+ve)	0.37	0.48	0.30	64.13	19.03
I (+ve)	0.27	0.48	0.26	52.47	13.42

Total vertical net force $F_{w,v} = 28.83$ kN
 Total horizontal net force $F_{w,h} = 0.00$ kN

Walls load case 4 - Wind 90, c_{pi} -0.3, +C_{pe}

Zone	Ext pressure coefficient C _{pe}	Peak velocity pressure q _p , (kN/m ²)	Net pressure p (kN/m ²)	Area A _{ref} (m ²)	Net force F _w (kN)
A	-1.20	0.38	-0.25	18.26	-4.58
B	-0.80	0.38	-0.12	57.27	-6.84
D _b	0.80	0.44	0.45	112.61	50.50
D _u	0.80	0.48	0.49	4.98	2.43
E	-0.52	0.48	-0.07	117.60	-8.25

Overall loading

Equiv leeward net force for upper section $F_l = F_{w,WE} / A_{ref,WE} \times A_{ref,wu} = -0.3$ kN
 Net windward force for upper section $F_w = F_{w,wu} = 2.4$ kN
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.87$ as h/L is 1.437



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Overall loading upper section $F_{w,u} = f_{corr} \times (F_w - F_l + F_{w,h}) = 2.4 \text{ kN}$
 Equiv leeward net force for bottom section $F_l = F_{w,we} / A_{ref,we} \times A_{ref,wb} = -7.9 \text{ kN}$
 Net windward force for bottom section $F_w = F_{w,wb} = 50.5 \text{ kN}$
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.87$ as h/L is 1.437
 Overall loading bottom section $F_{w,b} = f_{corr} \times (F_w - F_l) = 50.6 \text{ kN}$

Roof load case 5 - Wind 90, $C_{pi} -0.30$, + C_{pe}

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
F (+ve)	0.57	0.48	0.38	8.02	3.04
G (+ve)	0.47	0.48	0.34	8.02	2.71
H (+ve)	0.37	0.48	0.30	64.13	19.03
I (+ve)	0.27	0.48	0.26	52.47	13.42

Total vertical net force $F_{w,v} = 28.83 \text{ kN}$

Total horizontal net force $F_{w,h} = 0.00 \text{ kN}$

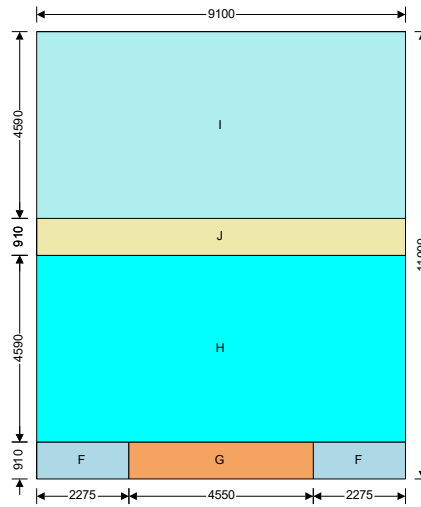
Walls load case 5 - Wind 90, $C_{pi} -0.30$, + C_{pe}

Zone	Ext pressure coefficient C_{pe}	Peak velocity pressure q_p , (kN/m ²)	Net pressure p (kN/m ²)	Area A_{ref} (m ²)	Net force F_w (kN)
A	-1.20	0.38	-0.25	18.26	-4.58
B	-0.80	0.38	-0.12	57.27	-6.84
D _b	0.80	0.44	0.45	112.61	50.50
D _u	0.80	0.48	0.49	4.98	2.43
E	-0.52	0.48	-0.07	117.60	-8.25

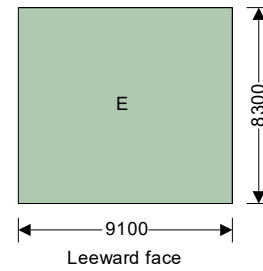
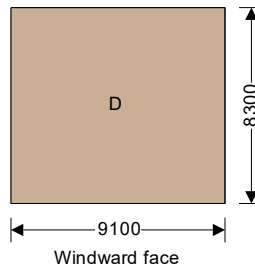
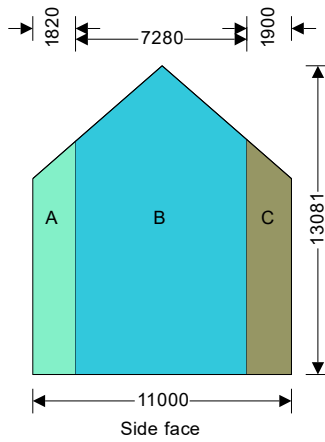
Overall loading

Equiv leeward net force for upper section $F_l = F_{w,we} / A_{ref,we} \times A_{ref,wu} = -0.3 \text{ kN}$
 Net windward force for upper section $F_w = F_{w,wu} = 2.4 \text{ kN}$
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.87$ as h/L is 1.437
 Overall loading upper section $F_{w,u} = f_{corr} \times (F_w - F_l + F_{w,h}) = 2.4 \text{ kN}$
 Equiv leeward net force for bottom section $F_l = F_{w,we} / A_{ref,we} \times A_{ref,wb} = -7.9 \text{ kN}$
 Net windward force for bottom section $F_w = F_{w,wb} = 50.5 \text{ kN}$
 Lack of correlation (cl.7.2.2(3) – Note) $f_{corr} = 0.87$ as h/L is 1.437
 Overall loading bottom section $F_{w,b} = f_{corr} \times (F_w - F_l) = 50.6 \text{ kN}$

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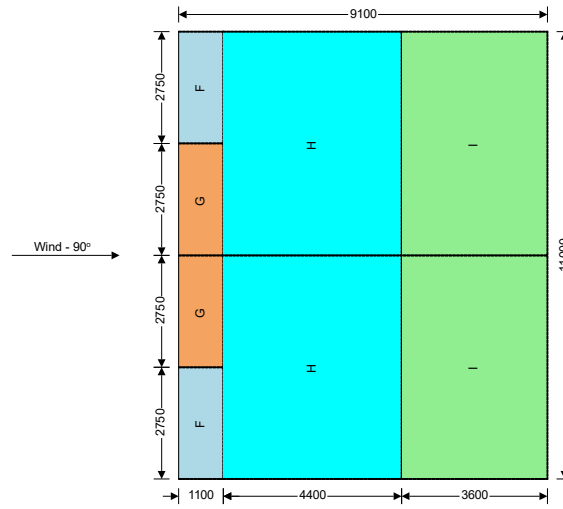
↑ Wind - 0°
 Plan view - Duopitch roof





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Plan view - Duopitch roof

