

ENERGY & SUSTAINABILITY ASSESSMENT

ST JOHN'S STUDIO

PROPERTY ADDRESS

Harley Road, London, NW3 3BY,

> **DATE** April 2022

PREPARED BY EAL Consult









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1. EXECUTIVE SUMMARY

This Sustainability statement has been prepared to support the planning application for the extension and alterations to St John's Studio in Harley Road, NW3 3BY. The strategy highlights how the proposed development will promote sustainability throught both design and operation and summarises the relevant regulatory and planning policies applicable and how the relevant policy targets will be addressed and achieved.

The strategy reponds to the UK Planning and regulatory framework, the National Planning Policy Framework 2021, the New London Plan 2021 and Camden Local Plan 2017.

In accordance with the Energy Hierarchy detailed within The New London Plan 2021, this statement outlines an overall commitment to reducing energy consumption under occupancy through the adoption of a 'Fabric First' principle, which will seek enhanced insulation standards and improved heating and lighting efficiencies in comparison to the standard requirements of Approved Document Part L1A 2013. Further carbon emission reduction can be achieved by using renewables (Air Source Heat Pumps).

Energy Effcicency & Carbon Reduction:

- Passive design principles including a high level of insulation and reduced air permeabilty to deliver Part L1A 2013 compliant Building in absence of renewable technologies. It will achieve 2.3% reduction in carbon emissions over Part L1A baseline.
- Air Source Heat Pumps have been proposed for the specific scheme and will deliver a
 further 46.2% reduction in regulated carbon emissions over Part L1A baseline when
 utilising the proposed carbon factor changes to building Regulations Part L.

Material and waste management:

- Minimising the use of virgin materials during construction by recycling and reusing where feasible
- Low waste benchmark levels will be targeted during construction with requirements identifying that the diversion of waste from landfill is to be achieved by the contractor.

Recommendation and Results:

This report demonstrates that the proposed development by incorporating the measures above can achieve an average carbon emission reduction of **48.5% with the use of:**

• Air Source Heat Pumps.

The following tables demonstrate the carbon emissions and savings.

Table 1. Carbon Dioxide emissions after each stage of the Energy Hierarchy

| | Regulated Carbon dioxide emissions (Tonnes CO2 per annum) | |
|---------------------------------------|---|-------|
| | Regulated | Total |
| Building Regs Notional Development | 6.19 | 7.42 |
| After Energy demand Reduction | 6.04 | 7.25 |
| After Renewables | 3.19 | 3.82 |

Table 2. Carbon Dioxide Savings from each stage of the Energy Hierarchy

| | Regulated Carbon dioxide savings (Tonnes CO ₂) | % Reduction |
|---|--|----------------|
| Savings from energy efficiency measures | 0.14 | 2.3% |
| Savings from Renewables | 2.86 | 46.2% |
| Total savings | 3 | 48.5% |

2. INTRODUCTION

Site description

Built in the late 1990's, the house has had various additions over the years, including a rear extension, porch, balconettes, and cornicing to the windows, that in addition to the choice of brickwork laid in stretcher bond, has resulted in a discordant pastiche of the surrounding context. The existing building is in need of retrofitting to meet modern building standards and become a positive contributor to the Conservation area. In addition to re-ordering the interior, the project aims to provide a new, contemporary reading of the context retaining carbon extensive parts of the existing structure but re-forming the facade openings, adding a floor to part of the structure, extending to the rear, and refacing the house with an angled terracotta rainscreen cladding.

Methodology

This energy assessment outlines the energy demand from the development together with the associated CO₂ emissions, using the present Building Regulations Part L as a baseline. It demonstrates how the emissions from energy use in the development will be reduced through energy efficiency measures.

The proposed scheme is required to achieve carbon emission reduction principles in accordance with the UK Planning and regulatory framework,

The methodology employed to determine the potential CO₂ savings is in accordance with the three-step Energy Hierarchy.

- **Be Lean** Improve the energy efficiency of the scheme;
- **Be Clean** Supply as much of the remaining energy requirement with low carbon; technologies such as district heating if available or combined heat and power (CHP); and
- **Be Green** Offset a proportion of the remaining carbon dioxide emissions by using renewable technologies.
- Be Seen monitor, verify and report on post-construction energy performance

The government approved Standard Assessment Procedure (SAP) methodology software (2013) has been used to determine the CO₂ emissions and energy requirements. It compares CO₂ emissions from regulated energy use (DER) with those of an equivalent dwelling built to Part L1A 2013 (TER), a notional dwelling of the same size and shape. These calculations do not include emissions from cooking or appliances.

Opportunities for incorporating features into the development that contribute to the objectives of sustainable development were explored during the design process, to ensure that where possible, the proposals achieve best practice.

3. PLANNING POLICY CONTEXT

National Planning Policy Framework 2021 – emphasised the concept of sustainable development by encouraging local authorities to adopt proactive strategies to mitigate and adapt to climate change. It recommends the move to a low carbon future by:

- Avoiding increased vulnerability to the range of impacts arising from climate change.
 When new development is brought forward in areas which are vulnerable, care should be taken to ensure that risks can be managed through suitable adaptation measures, including through the planning of green infrastructure; and
- Contributing to reduce greenhouse gas emissions, such as through its location, orientation
 and design. Any local requirements for the sustainability of buildings should reflect the
 Government's policy for national technical standards.
- To help increase the use and supply of renewable and low carbon energy and heat, plans should:
 - provide a positive strategy for energy from these sources, that maximises the potential for suitable development, while ensuring that adverse impacts are addressed satisfactorily (including cumulative landscape and visual impacts);
 - consider identifying suitable areas for renewable and low carbon energy sources, and supporting infrastructure, where this would help secure their development;
 and
 - o identify opportunities for development to draw its energy supply from decentralised, renewable or low carbon energy supply systems and for colocating potential heat customers and suppliers.

The London Plan 2021 provides the strategic framework for an integrated socio-economic, transportation and environmental development plan across the capital to 2050. The Plan seeks to ensure new developments are designed to enable the efficient use of energy and support the development of sustainable energy infrastructure to produce energy more efficiently. It sets out a range of policies that apply to new developments.

Policy SI 2 Minimising Greenhouse Gas Emissions:

- A. Development proposals should make the fullest contribution to minimising carbon dioxide emissions in accordance with the following energy hierarchy: a) Be lean: use less energy and manage demand during operation, b) Be clean: exploit local energy resources (such as secondary heat) and supply energy efficiently and cleanly, c) Be green: maximise opportunities for renewable energy by producing, storing and using renewable energy on-site
- B. Major development proposals should include a detailed energy strategy to demonstrate how the zero-carbon target will be met within the framework of the energy hierarchy.
- C. A minimum on-site reduction of at least 35 per cent beyond Building Regulations is required for major development. Residential development should achieve 10 per cent, and non-residential development should achieve 15 per cent through energy efficiency measures. Where it is clearly demonstrated that the zero-carbon target cannot be fully achieved on-site, any shortfall should be provided, in agreement with the borough, either: 1) through a cash in lieu contribution to the borough's carbon offset fund, or 2) off-site provided that an alternative proposal is identified, and delivery is certain.
- D. Boroughs must establish and administer a carbon offset fund. Offset fund payments must be ring-fenced to implement projects that deliver carbon reductions. The operation of offset funds should be monitored and reported on annually.

- E. Major development proposals should calculate and minimise carbon emissions from any other part of the development, including plant or equipment, that are not covered by Building Regulations, i.e. unregulated emissions.
- F. Development proposals referable to the Mayor should calculate whole lifecycle carbon emissions through a nationally recognised Whole Life-Cycle Carbon Assessment and demonstrate actions taken to reduce life-cycle carbon emissions.
- 9.2.1 The Mayor is committed to London becoming a zero-carbon city. This will require reduction of all greenhouse gases, of which carbon dioxide is the most prominent. London's homes and workplaces are responsible for producing approximately 78 per cent of its greenhouse gas emissions. If London is to achieve its objective of becoming a zero-carbon city by 2050, new development needs to meet the requirements of this policy. Development involving major refurbishment should also aim to meet this policy.
- 9.2.2 The energy hierarchy should inform the design, construction, and operation of new buildings. The priority is to minimise energy demand, and then address how energy will be supplied and renewable technologies incorporated. An important aspect of managing demand will be to reduce peak energy loadings.

Camden Local Plan 2017

Policy CC1 Climate change mitigation

The Council will require all development to minimise the effects of climate change and encourage all developments to meet the highest feasible environmental standards that are financially viable during construction and occupation.

We will:

- a. promote zero carbon development and require all development to reduce carbon dioxide emissions through following the steps in the energy hierarchy;
- b. require all major development to demonstrate how London Plan targets for carbon dioxide emissions have been met;
- c. ensure that the location of development and mix of land uses minimise the need to travel by car and help to support decentralised energy networks;
- d. support and encourage sensitive energy efficiency improvements to existing buildings;
- e. require all proposals that involve substantial demolition to demonstrate that it is not possible to retain and improve the existing building; and
- f. expect all developments to optimise resource efficiency.

For decentralised energy networks, we will promote decentralised energy by:

- g. working with local organisations and developers to implement decentralised energy networks in the parts of Camden most likely to support them;
- h. protecting existing decentralised energy networks (e.g. at Gower Street, Bloomsbury, King's Cross, Gospel Oak and Somers Town) and safeguarding potential network routes; and
- requiring all major developments to assess the feasibility of connecting to an existing decentralised energy network, or where this is not possible establishing a new network.

To ensure that the Council can monitor the effectiveness of renewable and low carbon technologies, major developments will be required to install appropriate monitoring equipment.

4. ENERGY STRATEGY

The Energy strategy for the proposed housing is based on the Building Regulations Part L1A; it adopts a set of principles to guide design and decisions regarding energy, balanced with the need to optimise environmental and economic benefits. It seeks to incorporate energy efficiency through the approach detailed below.

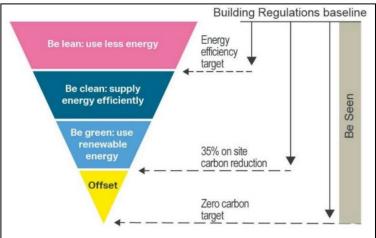


Figure 1. Energy Hierarchy

Be 'Lean' - Demand Reduction

The building fabric performance and engineering systems have been optimised in order to use less energy prior to the inclusion or consideration of Low and Zero Carbon (LZC) Technology.

Through passive design measures, efficient building fabric and engineering systems the building is estimated to achieve 2.3% reduction in annual regulated CO₂ emissions over Part L1A benchmark, therefore demonstrating compliance with Building Regulations Through passive means alone without the utilisation of renewable technologies.

Passive Design Measures:

Fabric Performance - The fabric performance values aim to reduce unwanted heat loss and heat gains, whilst maintaining a comfortable internal environment.

Table 3. Fabric energy Efficiency Standard

| The word alone and | Part L1A Minimum |
|--------------------|-------------------------|
| Thermal element | Standard |
| Wall | 0.30W/m ² k |
| Roof | 0.20 W/m ² k |
| Floor | 0.25 W/m ² k |
| Glazing | 1.2 W/m ² k |
| Doors | 1.2 W/m ² k |

The heat loss of different building elements is dependent upon their U –value. A building with low U values provides better levels of insulation and reduced heating demand.

The development will incorporate high levels of insulation and efficient glazing; thereby reduce demand for space heating. The table below shows the U values for the development and the associated improvements over Building Regulations.

Table 4. Energy Efficient design Specification

| Element | Standard | Specification |
|---------------------------|-------------------------|------------------------|
| Wall New Wall Existing | 0.30 W/m²k | 0.15W/m²k 0.25W/m²k |
| Floor | 0.25W/ m ² k | 0.2W/m²k |
| Roof | 0.2 W/ m²k | 0.11 W/ m²k |
| Glazing | 1.4 W/ m²k | 1.1W/ m²k |

Space Heating & Cooling - Space heating could be provided by underfloor heating for the dwelling;

Efficient Lighting and Controls - Throughout the development natural lighting will be optimised. The development will also incorporate low energy light fittings throughout. All light fittings will be specified as low energy lighting and will accommodate compact fluorescent (CFLs) or fluorescent luminaries only.

Ventilation - The use of natural ventilation is proposed for the dwelling;

Domestic hot water (DHW) system – domestic hot water is supplied for the dwelling; via the air source heat pump and cylinder.

Be 'Clean' - Supply Energy Efficiently

The Be Clean step of the energy hierarchy refers to the use of 'Clean energy supply'. This includes, but is not limited to, the use of Combined Heat and Power (CHP) and District Heat Networks. Policy TP1 seeks for new development to promote the use of CHP and district heating.

In light of the small scale nature of the proposed development, it is apparent that the use of CHP is also technically and financially unviable in this instance.

Be 'Green' - Renewable Energy

Once energy demand reduction measures have been applied, methods for generating low and zero carbon energy can be assessed. The following renewable technologies can be considered for the project: Biomass, Water source heat pump, air source heat pump, Wind energy and solar photovoltaic panels.

Table 5. Renewable Technologies Feasibility Table

| Technology | Pros | Cons | |
|--|--|---|--|
| Biomass Heating A biomass system designed for wood pellets, which have a high-energy content, would fuel this development. | Less volume of storage Less maintenance and produce considerably less ash residue | Nox Emissions which may impacts High Costs Not suitable for the project | |
| Ground Source Heat Pump It circulates a mixture of water and antifreeze around a loop of pipe, called a ground loop, which is buried in the garden. Heat from the ground is absorbed into the fluid and passes through a heat exchanger into the heat pump | Use all through the year | High Costs Not suitable for this project | |
| Air Source Heat Pump They are an efficient and environmentally- friendly way of heating using air drawn freely from the atmosphere. They operate rather like a refrigerator in reverse, absorbing heat from the air into a working fluid which is passed into a compressor where its temperature is increased before it is transferred into the heating and hot water circuits of the building | Can generate less CO₂ than conventional heating systems. Cheaper Provides heating and hot water Less maintenance Can be used as airconditioning in the summer | Needs electricityCan be noisy | |
| Wind Turbines Wind turbines are available in various sizes from large rotors able to supply whole communities to small roof or wall-mounted units for individual dwellings. | CheaperLess CO₂ | Local wind speeds in the area is likely to be below the level generally required for investment in large wind turbines. Noise and signal interference. Detrimental aesthetic impact | |

Solar Photovoltaic Panels (PV)

Photovoltaic panels extract the energy of the sun to generate electricity. They operate most efficiently when oriented to the south and are inclined to about 35 degrees.



- Cheaper
- Less CO₂
- No input power in order to generate electricity.

Not enough space

Renewable Technologies Feasibility Review Conclusion

The renewable energy sources that have been reviewed for this project are Biomass Heating, Ground Source Heat Pump, Air Source Heat Pump, Domestic Wind Turbine and Solar Photovoltaic Panels (PV).

On review of the above technologies, it has been concluded that the use of an air source heat pump is to be incorporated in the design because it achieves a CO2 percentage reduction of **46.2%** contributing to an overall reduction of 48.5% in carbon emissions.

Be Seen: Post-Construction Monitoring

To truly achieve net zero-carbon buildings we need to have a better understanding of their actual operational energy performance. To reduce the 'performance gap' the fourth stage, 'be seen', is a critical element in minimising greenhouse gas emissions and keeping running costs low.

Quality assurance mechanisms and commitments that will be considered as part of the energy strategy are:

- Gaining quality assurance accreditation (e.g. Heat Trust)
- Following quality standards (e.g. CIBSE Code of Practice)
- Transparent billing, including separation of the ongoing maintenance and capital replacement aspects of the standing charge
- Aftercare support (e.g. BREEAM Man 05 Aftercare)
- Heat tariffs options given to occupants
- Consumer choice for metering arrangements at no extra cost (e.g. Prepayment Meters (PPM)
- Thermal storage linked to pricing signals and renewable generation

5. SUSTAINABLE DESIGN

The proposed project incorporates sustainable design and construction measures capable of mitigating and adapting to climate change to meet future needs. This section details site-specific initiatives which demonstrate how the conversion helps to meet the sustainability objectives set out in the National Planning Framework 2021.

Energy Use and Pollution

The design of the development has taken into consideration day lighting to habitable spaces to improve the wellbeing of occupants. Good levels of daylight will offer occupants a pleasant and highly valued connection to the outdoors and plenty of natural light. It will also reduce the use of artificial lighting and therefore energy use. All light fittings will be specified as low energy lighting.

No external lighting is required. The location and orientation of windows help to create a design that avoids overheating in the summer.

Pollution: Air, Noise and Light

The layout of the development can provide good internal air quality for habitable areas but not too much so as to waste heat. The use of openable windows will create horizontal airflow. By achieving a good naturally ventilated building the energy demand for air conditioning and mechanical ventilation will thereby be eliminated within the development.

The development will not increase the air pollution of the area by reducing as a start, its energy consumption, which in turn will reduce emissions that lead to air pollution.

Other measures will include:

- a. Use of eco-friendly building materials
- b. Non-toxic paints
- c. Installation of energy efficient appliances and devices
- d. Use of renewable technologies

Light pollution can best be described as artificial light that is allowed to illuminate or intrude upon areas not intended to be lit. Light in the wrong place at the wrong time can be intrusive.

Intrusive light is over bright or poorly directed lights shining onto neighbouring property which affect the neighbours' right to enjoy their property. Therefore, the proposal will incorporate lighting measures in order to avoid causing a nuisance.

Water: Water Efficiency

In domestic and non-domestic buildings, the demand for water can be reduced as much as 50% using a variety of simple and innovative strategies that are integrated into the plumbing and mechanical systems. In order to reduce water consumption the proposed development will include efficient fixtures with low flow rates. Total internal water consumption will not exceed 105 litres/person/day.

Table 7. Water Fittings Standards

| Schedule Appliance Water Consumption | | | |
|--------------------------------------|---------------------------------|--------|--|
| Appliance | Appliance Flow rate or Capacity | | |
| WC | Dual flush WC 4/2.6 litre | 14.72 | |
| Basin | nsin 1.7 litres/min | | |
| Shower 8 litres/minute flow | | 24.00 | |
| Bath | 160 litres | 25.60 | |
| Sink | 4 litres/min | 14.13 | |
| W/machine | Default used | 16.66 | |
| Dish Washer | Default used | 3.90 | |
| | | 104.99 | |

Pollution

All contractors would be required to sign up to the nationally recognised Considerate Constructors Scheme which requires, amongst other things that dust emissions, potential noise pollution, impacts on water quality and the potential for ground contamination are minimised during demolition and construction. The Contractor would also be obliged to adhere to a site specific Code of Construction Practice to reduce potential nuisance effects.

Waste

A space for reuse and recycling has been included at the ground floor unit for the residents exclusive use.

Flood Risk

The development site is located in a Low Flood Risk Area on the Environment Agency Flood Risk Map.

Biodiversity

The proposed development will incorporate measures to support and enhance the environment through consideration of the existing site, including measures to mitigate the impact of the development and enhance site biodiversity.

6. Reuse and optimising resource efficiency

The proposed development aims to optimise resource efficiency and use circular economy principles and section 9 of Energy efficiency CPG Jan 2021.

Reusing existing building

The proposed development seeks to retain existing elements of substantial embodied carbon such as the structural concrete floors, foundations and flank walls. This will minimise the need to construct new extensive structural elements of high embodied carbon. To achieve this a lightweight structure will be used in the additional floor and new front/rear facades to remain within the weight capacity of the existing structure.

The material demolished in the front and rear facades will be reused. More details are provided on table 8.

Development options

Table 8 presents the potential options explored to assess the condition of the existing building. The options were outlined in the Section 9.5 of Energy efficiency CPG Jan 2021. These are: i) Refit, ii) Refurbish, iii) Substantial refurbishment and extension, and iv) Reclaim and recycle.

Table 8. Development options

| Option | Comment |
|---|---|
| Refit | The proposal looks to significantly improve the insulative capacity of the existing elements to be retained. This includes internally lining existing walls with insulation and upgrading windows. |
| | It will couple the improved insulation with a MVHR system to provide ventilation and reduce heat waste. It will also introduce an ASHP to provide a clean and efficient heat source. |
| | However, the proposal does not retain the existing structure as is and instead seeks to retain elements of high embodied carbon such as the concrete foundations, flank walls, and concrete beam and block floors. |
| Refurbish | The proposal looks to introduce an efficient and clean heat source whilst improving insulative qualities of the existing building. Doing so would significantly extend the life of the existing building. |
| | Adaptation measures include an adjustable solar shading sunscreen with the terracotta baguette façade and permeable paving throughout the exterior. |
| Substantial refurbishment and extension | The proposal seeks to demolish and reconstruct the front and rear facades to effectively accommodate an additional floor. In doing so the proposal will have the capacity to accommodate a growing extended family. |
| | However, whilst doing the above works existing elements of substantial embodied carbon will be retained such as the structural |

| | concrete floors, foundations, and flank walls. This minimises the need to construct new extensive structural elements of high embodied carbon. To achieve this a lightweight structure will be used in the additional floor and new front/rear facades to remain within the weight capacity of the existing structure. |
|---------------------|--|
| | The material demolished in the front and rear facades will be reused in the existing building. This mainly consists of concrete blockwork and bricks. The bricks will be reused to extend the flank walls to accommodate the new front/rear façade. Concrete blockwork will be used to repair existing concrete beam and block floors. |
| Reclaim and recycle | The partial demolition of the building includes front/rear facades, windows, and the pitched roof timber structure and tile finish. The construction will seek to re-use the materials on site where possible. |
| | On site opportunities for re-use include the extension of flank brick walls, repairing existing beam and block floors, infill elements to the garden and permeable paving to exterior hard surfaces. |
| | When not possible to reuse on site material will be suitably recycled off site. |

Resource efficiency and Circular economy principles

The proposed development seeks to incorporate measures to improve resource efficiency and reduce the waste through the various stages of the development process. These are summarised in the table below.

Table 9. Resource efficiency measures

| Stage | Measures | Comment |
|--------|--------------------------------------|---|
| Design | Energy efficiency building design | The proposal aims to design highly energy efficient building by incorporation passive design measures and renewables (Air source heatpump) Refer to section 4 and 6 of this report |
| | Material efficiency | The reuse of existing materials from the demolition of existing buildings (Brick walls, brickwork,) Existing concrete floors repaired and retained At least 20% of the total value of materials used should derive from recycled and reused content in the products and materials selected; Steel will have a high recycled content; |

| Construction | Minimise the use of resources (energy, water, land) Resource efficiency | Monitor the water and energy consumption and report the equivalent carbon emissions. Pre-demolition audit to be carried out and target benchmark of ≤ 11.1 tonnes of construction waste per 100m2; |
|----------------------------|---|--|
| | Minimise waste generation | Reusable packing solutions with key product manufacturers will be explored at the earliest opportunity. Solutions may include flat pallets, bulk bags, steel stillages and returnable cable drums; Pre-fabrication of materials/elements such as bathroom pods, pipework and |
| | Diversion of waste from landfill | riser materials will be considered; Construction waste – minimum 80% diversion from landfill rate; Demolition waste – minimum 90% diversion from landfill rate; |
| | Sustainable sourcing | All timber used in the development will come from a legal Source (FSC Scheme). At least 80% of the building materials will be responsibly sourced and will use suppliers who can provide an EMS certificate or equivalent. Materials rated with an A or B in the BRE Green Guide to Specification will be preferred. |
| Operation | Maintenance | Implement a good maintenance/ repair strategy to maximise life of materials Consider repair before replacement When replacements required select high durability materials with low maintenance requirements |
| Deconstruction/end of life | Deconstruction | Design for deconstruction and reuse of materials Divert waste from landfill (via reuse, recycling or recovery) Demolition and construction waste - 95% to reuse, recycling, recovery |

7. CONCLUSION

The development has been designed to exceed Part L1A building regulations requirements. In line with the national and local policies, regulated CO₂ emissions from the development will be reduced by **48.5%** from the notional emissions once energy efficiency measures and lean measures are taken into account.

In order to achieve the required carbon emissions reduction, the report concludes and proposes the use of energy efficient measures outlined in the section 4 of this report.

An appraisal of the proposed development has been undertaken against key sustainability objectives identified from relevant policy guidance. The framework for the appraisal was guided by the National Plan. This process has ensured that the development responds to the sustainable development objectives that are relevant to the area. Key sustainability initiatives in ecology, waste management, water, health and wellbeing, materials, pollution and Surface water management have been incorporated in the design of the proposed Development.

8.APPENDIX

I. SAP Calculations

Project Information

Building type Semi-detached house

Reference

Date 22 April 2022

Email: none Project The Studio

St. Johns Lodge Harley Road LONDON NW3 3BY

SAP 2012 worksheet for New dwelling as designed - calculation of energy ratings

1. Overall dwelling dimensions

| | Area | Av. Storey | Volume | |
|------------------|--------|------------|---------|------------------|
| | (m²) | height (m) | (m³) | |
| Ground floor (1) | 146.83 | 3.31 | 486.01 | (3a) |
| First floor | 118.87 | 3.20 | 380.38 | (3b) |
| Secondfloor | 111.86 | 3.00 | 335.58 | (3c) |
| Thirdfloor | 56.04 | 2.10 | 117.68 | (3d) |
| | 433.60 | | | (4) |
| | | | 1319.66 | (5) |

2. Ventilation rate

| | | | | | | | | | | | m³ per ho | our |
|-------------|-------------|------------|-------------|-------------|-----------|----------|-----------|--------|----------------|------|-----------|--------------|
| | | | | | | | main + s | eondar | y + othe | r | | |
| | | | | | | | heating | | | | | 4- > |
| | er of chim | • | | | | | 0 + 0 + 0 | | < 40 | | 0.00 | (6a) |
| | er of oper | | | | | | 0 + 0 + 0 |) | <i><</i> 20 | | 0.00 | (6b) |
| Numbe | er of inter | mittent fa | ans | | | | 7 |) | < 10 | | 70.00 | (7a) |
| Numbe | er of pass | ive vents | ; | | | | 0 |) | < 10 | | 0.00 | (7b) |
| | | ess gas f | | | | | 0 |) | < 40 | | 0.00 | (7c) |
| | | | | | | | | | | | Air chand | ges per hour |
| | | | | | | | | | | | 0.05 | (8) |
| Pressu | re test. r | esult q50 |) | | | | | | 3.50 | | | (17) |
| | meability | | | | | | | | 0.00 | | 0.23 | (18) |
| 7 tii poi i | noability | | | | | | | | | | 2.00 | (19) |
| | | | | | | | | | | | 0.85 | (20) |
| Infiltrat | ion rata i | acarnara | tina chal | ter factor | | | | | | | 0.19 | (20) |
| | | • | _ | hly wind s | | | | | | | 0.19 | (21) |
| | | | | | peeu | 1 | | | | | | |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
| 5.10 | 5.00 | 4.90 | 4.40 | 4.30 | 3.80 | 3.80 | 3.70 | 4.00 | 4.30 | 4.50 | 4.70 | |
| | | | | | | | | | | | 52.50 | (22) |
| Wind F | actor | | | | | | | | | | | |
| 1.27 | 1.25 | 1.23 | 1.10 | 1.07 | 0.95 | 0.95 | 0.93 | 1.00 | 1.07 | 1.13 | 1.18 | |
| | | | | | | | | | | | 13.13 | (22a) |
| Adjuste | ed infiltra | tion rate | (allowing | g for shelt | ter and w | ind spee | ed) | | | | | |
| 0.25 | 0.24 | 0.24 | 0.21 | 0.21 | 0.18 | 0.18 | 0.18 | 0.19 | 0.21 | 0.22 | 0.23 | |
| | | | | | | | | | | | 2.54 | (22b) |
| Ventila | tion : nat | ural vent | ilation, ii | ntermitte | nt extrac | t fans | | | | | | , , |
| | | inge rate | , | | | | | | | | | |
| 0.53 | 0.53 | 0.53 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.53 | (25) |
| 0.53 | 0.53 | 0.53 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.53 | (23) |

| 3. Heat losse | s and heat lo | ss paramete | r | | | | |
|---------------------------------|---------------|-------------|----------|-------------|-------|-------------------|------|
| Element | Gross | Openings | Net area | U-value | AxU | kappa-value A x k | (|
| | area, m² | m² | A, m² | W/m²K | W/K | kJ/m²K kJ/K | |
| Window - Doul | ble-glazed, | | 6.190 | 1.05 (1.10) | 6.52 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | ` , | | | , , |
| soft coat (Sou | th) | | | | | | |
| FRONT-SID | EENTRANCE | DOOR | | | | | |
| Window - Doul | ble-glazed, | | 17.245 | 1.05 (1.10) | 18.17 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Sou | thWest) | | | | | | |
| FRONTGF | | | | | | | |
| Window - Doul | ble-glazed, | | 5.824 | 1.05 (1.10) | 6.14 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Sou | th) | | | | | | |
| FRONT-SID | EFF | | | | | | |
| Window - Doul | ble-glazed, | | 15.584 | 1.05 (1.10) | 16.42 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Nort | h) | | | | | | |
| REAR-SIDE | FF | | | | | | |
| Window - Doul | ble-glazed, | | 5.460 | 1.05 (1.10) | 5.75 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Sou | | | | | | | |
| FRONT-SID | ESF | | | | | | |
| Window - Doul | ble-glazed, | | 14.610 | 1.05 (1.10) | 15.39 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Nort | | | | | | | |
| REAR-SIDE | | | | | | | |
| Window - Doul | - | | 11.123 | 1.05 (1.10) | 11.72 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Nort | hEast) | | | | | | |
| REAR SF | | | | | | | |
| Window - Doul | - | | 12.620 | 1.05 (1.10) | 13.30 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Nort | hEast) | | | | | | |
| REAR FF | | | | | | | |
| Window - Doul | - | | 14.160 | 1.05 (1.10) | 14.92 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Sou | thWest) | | | | | | |
| FRONTFF | | | | | 40.4- | | (o=) |
| Window - Doul | | | 12.480 | 1.05 (1.10) | 13.15 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Sou | tnvvest) | | | | | | |
| FRONTSF | | | 44.540 | 4.40 | 45.00 | | (00) |
| Full glazed do | | | 14.510 | 1.10 | 15.96 | | (26) |
| Double-glazed | | | | | | | |
| low-E, En=0.1 | , son coar | | | | | | |
| (SouthWest) FRONT3F | | | | | | | |
| | or - | | 19.496 | 1.10 | 21.45 | | (26) |
| Full glazed do Double-glazed | | | 13.430 | 1.10 | Z1.40 | | (26) |
| low-E, En=0.1 | - | | | | | | |
| (North) | , son coal | | | | | | |
| REAR-SIDE | | | | | | | |
| INLAIN SIDE | | | | | | | |

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| Assume | e r heatin g ed occupa | ancy, N | _ | | | | | | | | kWh/yea 3.31 | (42 |
|----------|----------------------------------|-------------|-------------|-------------|-----------|----------|--------|--------|--------|--------|------------------------|------------|
| Annual | average l | hot water | usage ir | n litres pe | er day Vd | ,average |) | | | | 112.71 | (43) |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
| Hot wat | er usage | in litres p | oer day f | or each r | nonth | | | | | | | |
| 123.98 | 119.47 | 114.96 | 110.45 | 105.95 | 101.44 | 101.44 | 105.95 | 110.45 | 114.96 | 119.47 | 123.98 | (44) |
| Energy | content c | of hot wat | er used | | , | J | | | | J | | |
| 183.86 | 160.80 | 165.93 | 144.67 | 138.81 | 119.78 | 111.00 | 127.37 | 128.89 | 150.21 | 163.97 | 178.06 | |
| | content (a | annual) | | | | JC | | | | | 1773.34 | (45 |
| 27.58 | 24.12 | 24.89 | 21.70 | 20.82 | 17.97 | 16.65 | 19.11 | 19.33 | 22.53 | 24.59 | 26.71 | (46 |
| , | r volume, | | | | | | 300.00 | | | | | (47 |
| | cturer's d | | cylinder I | oss facto | or (kWh/c | day) | 2.14 | | | | | (48 |
| • | ature Factorial lost from | | r ovlinde | r (le\\/b/e | lov () | | 0.5400 | | | | 1.16 | (49 (55 |
| | orage los | | er Cyllride | i (KVVII/C | iay) | | | | | | 1.10 | (33) |
| 35.82 | 32.36 | 35.82 | 34.67 | 35.82 | 34.67 | 35.82 | 35.82 | 34.67 | 35.82 | 34.67 | 35.82 | (56 |
| Net stor | age loss | | JL | | | J | JL | | JI. | JL | | |
| 35.82 | 32.36 | 35.82 | 34.67 | 35.82 | 34.67 | 35.82 | 35.82 | 34.67 | 35.82 | 34.67 | 35.82 | (57 |
| Primary | loss | | Л | | | J | Л | , | JI. | Л | | |
| 23.26 | 21.01 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 | (59 |
| Total he | at require | ed for wa | ter heati | ng calcul | ated for | each mo | nth | | 1 | , | | |
| 242.94 | 214.17 | 225.02 | 201.85 | 197.90 | 176.96 | 170.08 | 186.46 | 186.07 | 209.30 | 221.15 | 237.14 | (62 |
| Output f | from wate | er heater | for each | month, l | kWh/mor | nth | | | | | | |
| 242.94 | 214.17 | 225.02 | 201.85 | 197.90 | 176.96 | 170.08 | 186.46 | 186.07 | 209.30 | 221.15 | 237.14 | (64 |
| | | | | | | - | | | | | 2469.03 | (64 |
| Heat ga | ins from | water he | ating, kV | /h/month | 1 | | | | | | | |
| 108.40 | 96.16 | 102.44 | 93.85 | 93.42 | 85.57 | 84.17 | 89.62 | 88.60 | 97.21 | 100.26 | 106.47 | (65 |

5. Internal gains

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
|------------|------------|------------|----------|---------|---------|---------|---------|---------|---------|---------|---------|--|
| Metabol | ic gains, | Watts | | | | | | | | | | |
| 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | |
| Lighting | gains | | | | • | | | | | | | |
| 124.63 | 110.70 | 90.03 | 68.16 | 50.95 | 43.01 | 46.48 | 60.41 | 81.08 | 102.95 | 120.16 | 128.10 | |
| Applianc | es gains | • | | | | | | | | | | |
| 834.64 | 843.30 | 821.48 | 775.01 | 716.36 | 661.24 | 624.41 | 615.75 | 637.57 | 684.04 | 742.69 | 797.81 | |
| Cooking | gains | | | | | | | | | | | |
| 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | |
| Pumps a | and fans | gains | | | | | | | | | | |
| 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 | |
| Lossese | e.g. evap | oration (r | negative | values) | | | | | | | | |
| -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | |
| Water he | eating ga | ins | | | | | | | | | | |
| 145.70 | 143.10 | 137.69 | 130.34 | 125.57 | 118.85 | 113.14 | 120.46 | 123.06 | 130.66 | 139.25 | 143.11 | |
| Total inte | ernal gair | าร | | | | | | | | | | |
| 1232.23 | 1224.35 | 1176.45 | 1100.76 | 1020.13 | 950.35 | 911.28 | 923.87 | 968.97 | 1044.91 | 1129.36 | 1196.27 | |

6. Solar gains (calculation for January)

| | Area & Flux | g & FF | Shading | Gains |
|--|----------------------|-------------|---------|----------|
| Window - Double-glazed, argon filled, low-E, | 0.9 x 6.190 46.75 | 0.63 x 0.80 | 0.77 | 101.0728 |
| En=0.1, soft coat (South) | | | | |
| FRONT-SIDE ENTRANCE DOOR | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 17.245 36.79 | 0.63 x 0.80 | 0.77 | 221.6165 |
| En=0.1, soft coat (SouthWest) | | | | |
| FRONTGF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 5.824 46.75 | 0.63 x 0.80 | 0.77 | 95.1012 |
| En=0.1, soft coat (South) | | | | |
| FRONT-SIDE FF | 0.045 504.40.00 | 0.00 0.00 | 0.77 | F7 0704 |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 15.584 10.63 | 0.63 X 0.80 | 0.77 | 57.8781 |
| En=0.1, soft coat (North) REAR-SIDE FF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 5.460 46.75 | 0.63 x 0.80 | 0.77 | 89.1574 |
| En=0.1, soft coat (South) | 0.9 X 3.400 40.73 | 0.03 X 0.00 | 0.77 | 09.1374 |
| FRONT-SIDE SF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 14.610 10.63 | 0.63 x 0.80 | 0.77 | 54.2608 |
| En=0.1, soft coat (North) | 0.0 % 1 1.0 10 10.00 | 0.00 X 0.00 | 0 | 0 112000 |
| REAR-SIDE SF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 11.123 11.28 | 0.63 x 0.80 | 0.77 | 43.8337 |
| En=0.1, soft coat (NorthEast) | | | | |
| REAR SF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 12.620 11.28 | 0.63 x 0.80 | 0.77 | 49.7331 |
| En=0.1, soft coat (NorthEast) | | | | |
| REAR FF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 14.160 36.79 | 0.63 x 0.80 | 0.77 | 181.9709 |
| En=0.1, soft coat (SouthWest) | | | | |
| FRONTFF | | | | |

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| 6. Solar gains (calculation for January) | Area & Flux | ~ 0 ГГ | Chadina | Caina | |
|---|---|--------------------------------------|---|---|--------|
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONTSF | 0.9 x 12.480 36.79 | g & FF 0.63 x 0.80 | Shading 0.77 | Gains 160.3812 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT3F | 0.9 x 14.510 36.79 | 0.63 x 0.80 | 0.77 | 186.4688 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE | 0.9 x 19.496 10.63 | 0.63 x 0.80 | 0.77 | 72.4067 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (NorthEast) REAR GF | 0.9 x 23.766 11.28 | 0.63 x 0.80 | 0.77 | 93.6574 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (NorthEast) REAR 3F | 0.9 x 14.580 11.28 | 0.63 x 0.80 | 0.77 | 57.4571 | |
| Rooflight at 70° or less - Double-glazed, argon filled, low-E, En=0.1, soft coat (n/a) ROOF | 0.9 x 10.130 26.00 | 0.63 x 0.80 | 1.00 | 119.4692 | |
| Total solar gains, January | | | | 1584.46 | (83-1) |
| Solargains | | | | | |
| | 503.5 7122.6 6093 | .9 4858.0 324 | 8.5 1924.23 | 1338.93 | (83) |
| Total gains | | | | | (0.1) |
| 2816.7 4068.8 5458.4 7066.1 8308.4 8 | 453.8 8033.8 7017 | .8 5826.9 429 | 3.4 3053.6 | 2535.2 | (84) |
| | | | | | |
| Lighting calculations | | | | | |
| | Area | g 0.80 | FF x Shad | | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | Area 0.9 x 6.19 | g 0.80 | FF x Shad 1.00 x 0.8 | - | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR | | | | 3 3.70 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | 0.9 x 6.19 | 0.80 | 1.00 x 0.83 | 3 3.70 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | 0.9 x 6.19 | 0.80 | 1.00 x 0.83 | 3 3.70 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) | 0.9 x 6.19 0.9 x 17.25 | 0.80 | 1.00 x 0.83 | 3 3.70 3 10.31 3 3.48 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | 0.9 x 6.19 0.9 x 17.25 0.9 x 5.82 | 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 3 3.70 3 10.31 3 3.48 3 9.31 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, | 0.9 x 6.19 0.9 x 17.25 0.9 x 5.82 0.9 x 15.58 | 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 3 3.70 3 10.31 3 3.48 3 9.31 3 3.26 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF | 0.9 x 6.19 0.9 x 17.25 0.9 x 5.82 0.9 x 15.58 0.9 x 5.46 | 0.80 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 3 3.70 3 10.31 3 3.48 3 9.31 3 3.26 3 8.73 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE ENTRANCE DOOR Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF | 0.9 x 6.19 0.9 x 17.25 0.9 x 5.82 0.9 x 15.58 0.9 x 5.46 0.9 x 14.61 | 0.80 0.80 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 3 3.70 3 10.31 3 3.48 3 9.31 3 3.26 3 8.73 3 6.65 | |

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Lighting calculations

| | Area | g | FF x Shading | |
|--|-------------|------|--------------|------|
| Window - Double-glazed, argon filled, low-E, | 0.9 x 14.16 | 0.80 | 1.00 x 0.83 | 8.46 |
| En=0.1, soft coat (SouthWest) FRONTFF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 12.48 | 0.80 | 1.00 x 0.83 | 7.46 |
| En=0.1, soft coat (SouthWest) FRONTSF | | | | |
| Rooflight at 70° or less - Double-glazed, | 0.9 x 10.13 | 0.80 | 0.80 x 1.00 | 5.83 |
| argon filled, low-E, En=0.1, soft coat (n/a) | | | | |
| 01 7474/40000 0470 | | | | |

GL = 74.74 / 433.60 = 0.172

C1 = 0.500 C2 = 0.960EI = 880

7. Mean internal temperature

Temperature during heating periods in the living area, Th1 (°C)

| Heating | ı system ı | esponsiv | veness | | | | | | | | 0.75 | |
|-------------|------------|-----------|-------------|------------|-----------|--------|-------|-------|-------|-------|-------|------|
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
| tau | | · | | | , | | · | | • | | | |
| 29.51 | 29.54 | 29.56 | 29.68 | 29.70 | 29.80 | 29.80 | 29.82 | 29.76 | 29.70 | 29.65 | 29.61 | |
| alpha | | | | | | | - | | | | | |
| 2.97 | 2.97 | 2.97 | 2.98 | 2.98 | 2.99 | 2.99 | 2.99 | 2.98 | 2.98 | 2.98 | 2.97 | |
| Utilisation | on factor | for gains | for living | area | | | - | | | | | |
| 0.98 | 0.96 | 0.90 | 0.77 | 0.60 | 0.44 | 0.33 | 0.39 | 0.62 | 0.88 | 0.97 | 0.99 | (86) |
| Mean in | ternal te | mperatur | e in living | area T1 | | | - | | | | | |
| 19.24 | 19.57 | 20.01 | 20.46 | 20.74 | 20.86 | 20.89 | 20.88 | 20.77 | 20.32 | 19.67 | 19.18 | (87) |
| Temper | ature du | ring heat | ing perio | ds in rest | of dwelli | ng Th2 | | | | | | |
| 19.73 | 19.73 | 19.73 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | (88) |
| Utilisation | on factor | for gains | for rest | of dwellir | ng | • | | | | | | |

21.00

(85)

(93)

| 0.98 | 0.95 | 0.88 | 0.73 | 0.54 | 0.36 | 0.24 | 0.29 | 0.54 | 0.84 | 0.96 | 0.99 | (89) |
|---------|------------|----------|------------|-----------|-----------|-------|-------|-------|-------|-------|-------|------|
| Mean in | ternal ter | nperatur | e in the r | est of dw | elling T2 | | | | | | | |
| 17.41 | 17.88 | 18.49 | 19.10 | 19.45 | 19.57 | 19.60 | 19.60 | 19.50 | 18.95 | 18.03 | 17.31 | (90) |

| | | | | | | | | | | |
|-----------|------------|-----------|------------|----------|----------|--|------|------|----|------|
| Living ar | ea fractio | on (146.8 | 33/433.6 | (0) | | | | 0.3 | 34 | (91) |
| Mean int | ernalten | nneratur | e (for the | whole dv | vellina) | | | | | |

| Wicarrin | ciriai toi | nperatar | c (ioi tiic | WIIOIC G | weiling) | | | | | | | |
|----------|------------|------------|-------------|-----------|-----------|-----------|----------|-------|-------|-------|-------|------|
| 18.03 | 18.45 | 19.01 | 19.56 | 19.88 | 20.01 | 20.04 | 20.03 | 19.93 | 19.41 | 18.59 | 17.94 | (92) |
| Apply ac | diustmen | t to the m | ean inte | rnal temi | oerature. | . where a | ppropria | te | , | | | |

| | | | | | | | | | | • | |
|--|-------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 18.03 18.45 19.01 19.56 19.88 20.01 20.04 20.03 19.93 19.4 | 18.59 17.94 | 19.41 | 19.93 | 20.03 | 20.04 | 20.01 | 19.88 | 19.56 | 19.01 | 18.45 | 18.03 |

8. Space heating requirement

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
|------------|------------|------------|------------|-----------|---------|-----------|-----------|--------|---------|--------|----------|---|
| Utilisatio | on factor | for gains | , | | | , | | | , | , | | |
| 0.98 | 0.94 | 0.86 | 0.72 | 0.55 | 0.38 | 0.26 | 0.31 | 0.55 | 0.83 | 0.95 | 0.98 | |
| Useful g | ains | , | , | | | , | | | , | , | | |
| 2746.5 | 3814.9 | 4710.5 | 5117.5 | 4552.3 | 3219.2 | 2100.4 | 2197.2 | 3225.7 | 3569.2 | 2909.6 | 2487.0 | |
| Monthly | average | external | tempera | ture | | , | , | ^ | , | | | |
| 4.30 | 4.90 | 6.50 | 8.90 | 11.70 | 14.60 | 16.60 | 16.40 | 14.10 | 10.60 | 7.10 | 4.20 | |
| Heat los | s rate for | mean in | ternal te | mperatu | re | | | | , | | | |
| 8581.8 | 8464.2 | 7805.3 | 6628.5 | 5084.3 | 3349.9 | 2130.2 | 2248.7 | 3613.3 | 5475.3 | 7147.6 | 8564.0 | |
| Fraction | of month | n for heat | ing | | | | | | , | | | |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 1.00 | |
| Space h | eating re | quireme | nt for eac | ch month | , kWh/m | onth | | | , | | | |
| 4341.5 | 3124.4 | 2302.6 | 1087.90 | 395.78 | - | - | - | - | 1418.09 | 3051.4 | 4521.3 | |
| Total sp | ace heat | ing requi | rement p | er year (| kWh/yea | ar) (Octo | ber to Ma | ay) | , | | 20242.86 | ; |
| Space h | eating re | quireme | nt per m² | kWh/m | ²/year) | | | | | | 46.69 |) |

8c. Space cooling requirement - not applicable

| 9a. Ene | ergy requ | uiremen | ts | | | | | | | | | |
|---|--------------------------|-----------|-----------|------------|----------|--|--------|--------|-----------------|--------|----------|----------------|
| | ondary he | | | | | | | | | | kWh/year | |
| | n of space cy of mai | | | • , | s) | | | | 1.0000 3.90% | | | (202) (206) |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | (|
| Spaceh | eating re | quireme | nt | | JI | | | | JL | | | |
| 4341.5 | 3124.4 | 2302.6 | 1087.90 | 395.78 | - | - | - | - | 1418.09 | 3051.4 | 4521.3 | (98) |
| Append | lix Q - mo | nthly en | ergy sav | ed (main | heating | system 1 | 1) | | JI. | JL | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (210) |
| Space h | neating fu | iel (main | heating | system 1 | ĺ) | JL . | | , | Л | JI. | | |
| 4623.5 | 3327.3 | 2452.2 | 1158.57 | 421.49 | - | - | - |]- | 1510.21 | 3249.6 | 4815.0 | (211) |
| Append | lix Q - mo | nthly en | ergy sav | ed (main | heating | system 2 | 2) | , | Л | JI. | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (212) |
| Space h | neating fu | iel (main | heating | system 2 | 2) | | | | , | | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (213) |
| Append | lix Q - mo | nthly en | ergy save | ed (seco | ndary he | ating sys | stem) | | , | | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (214) |
| Space h | eating fu | el (secor | ndary) | | , | <u>, </u> | ., | | , | | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (215) |
| Waterh | | , | | | , | | | | , | | | |
| | eating re | | | | | | | | | | | |
| | 214.17 | JL | 201.85 | 197.90 | 176.96 | 170.08 | 186.46 | 186.07 | 209.30 | 221.15 | 237.14 | (64) |
| | cy of wate | | | | | | | | | | 80.20 | (216) |
| 90.26 | 90.13 | 89.83 | 89.04 | 87.03 | 80.20 | 80.20 | 80.20 | 80.20 | 89.37 | 90.09 | 90.30 | (217) |
| _ | eating fu | | 06 | | | | | | | | | |
| 269.15 | 237.63 | 250.49 | 226.69 | 227.39 | 220.65 | 212.07 | 232.49 | 232.01 | 234.20 | 245.48 | 262.62 | (219) |
| Annual | totals | | | | | | | | | | kWh/year | |
| Space h | neating fu | ıel used, | main sy | stem 1 | | | | | | | 21557.89 | (211) |
| | neating fu | | ndary) | | | | | | | | 0.00 | (215) |
| | eating fu | | | | | | | | | | 2850.86 | (219) |
| | ity for pui I heating | • | s and ele | ectric kee | ep-not | | | | | | 30.00 | (230c) |
| | with a far | | d flue | | | | | | | | 45.00 | (230c) |
| | ectricity f | | | n/vear | | | | | | | 75.00 | (231) |
| | ity for ligh | | | | | | | | | | 880.44 | (232) |
| • | saving/ge | eneration | technolo | ogies | | | | | | | | |
| Append | | | | | | | | | | | 0.000 | (000) |
| • | y saved (| • | ated (): | | | | | | | | 0.000 | (236a) |
| Energ | y used () | ١. | | | | | | | | | 0.000 | (237a) |
| Total de | livered e | nergy for | all uses | | | | | | | | 25364.18 | (238) |

| 10a | Fuel | costs | เมรากต | Table | 12 | prices |
|------|-------|-------|--------|-------|----|--------|
| ıva. | ı ucı | CUSIS | usiiiu | Iabic | 12 | มเเษยง |

| , | kWh/year | Fuel price p/kWh | £/year | |
|-------------------------------|-----------|---------------------|---------|-------|
| Space heating - main system 1 | 21557.886 | 3.480 | 750.21 | (240) |
| Space heating - main system 2 | 0.000 | 0.000 | 0.00 | (241) |
| Water heating cost | 2850.86 | 3.480 | 99.21 | (247) |
| Mech vent fans cost | 0.000 | 13.190 | 0.00 | (249) |
| Pump/fan energy cost | 75.000 | 13.190 | 9.89 | (249) |
| Energy for lighting | 880.436 | 13.190 | 116.13 | (250) |
| Additional standing charges | | | 120.00 | (251) |
| Electricity generated - PVs | 0.000 | 0.000 | 0.00 | (252) |
| Appendix Q - | | | | |
| Energy saved or generated (): | 0.000 | 0.000 | 0.00 | (253) |
| Energy used (): | 0.000 | 0.000 | 0.00 | (254) |
| Total energy cost | | | 1095.45 | (255) |
| 11a. SAP rating | | | 0.42 | (256) |
| 0.5 | | | 0.96 | (257) |
| SAPvalue | | | 86.59 | (050) |
| | | | 87 | (258) |
| SAP band | | | В | |

12a. Carbon dioxide emissions

| | Energy kWh/year | Emission factor kg CO2/kWh | Emission kg CO2/y | _ |
|----------------------------------|--------------------|-------------------------------|-------------------|--------|
| Space heating, main system 1 | 21557.89 | 0.216 | 4656.50 | (261) |
| Space heating, main system 2 | 0.00 | 0.000 | 0.00 | (262) |
| Space heating, secondary | 0.00 | 0.519 | 0.00 | (263) |
| Waterheating | 2850.86 | 0.216 | 615.79 | (264) |
| Space and water heating | | | 5272.29 | (265) |
| Electricity for pumps and fans | 75.00 | 0.519 | 38.93 | (267) |
| Electricity for lighting | 880.44 | 0.519 | 456.95 | (268) |
| Electricity generated - PVs | 0.00 | 0.519 | 0.00 | (269) |
| Electricity generated - µCHP | 0.00 | 0.000 | 0.00 | (269) |
| Appendix Q - | | | | |
| Energy saved (): | 0.00 | 0.000 | 0.00 | (270) |
| Energy used (): | 0.00 | 0.000 | 0.00 | (271) |
| Total CO2, kg/year | | | 5768.16 | (272) |
| | | | kg/m²/yea | ar |
| CO2 emissions per m ² | | | 13.30 | (273) |
| Elvalue | | | 83.85 | (273a) |
| El rating | | | 84 | (274) |
| El band | | | В | |

Calculation of stars for heating and DHW

Main heating energy efficiency
Main heating environmental impact
Water heating energy efficiency
Water heating environmental impact

 $(3.48 / 0.9090) \times (1 + (0.29 \times 0.25)) = 4.1059$, stars = 4 $(0.2160 / 0.9090) \times (1 + (0.29 \times 0.25)) = 0.2549$, stars = 4 3.48 / 0.8640 = 4.0276, stars = 4 0.2160 / 0.8640 = 0.2500, stars = 4

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Project Information

Building type Semi-detached house

Reference

Date 22 April 2022

Email: none Project The Studio

St. Johns Lodge Harley Road LONDON NW3 3BY

REGULATION COMPLIANCE REPORT - Approved Document L1A, 2012 Edition, England

assessed by program JPA Designer version 6.05.054, printed on 02/05/2022 at 10:05:19

New dwelling as designed

1 TER and DER

Fuel for main heating system: Gas (mains) (fuel factor = 1.00)

Target Carbon Dioxide Emission Rate TER = 14.27

Dwelling Carbon Dioxide Emission Rate DER = 13.94

OK

1b TFEE and DFEE

Target Fabric Energy Efficiency (TFEE)

Dwelling Fabric Energy Efficiency (DFEE)

TFEE = 62.9

DFEE = 55.8

DFEE = 55.8 OK

2a Thermal bridging

Thermal bridging calculated using default y-value of 0.15

2b Fabric U-values

Element **Highest** <u>Average</u> Wall 0.25 (max. 0.30) 0.25 (max. 0.70) OK **Curtain Wall** 0.15 (max. 2.20) 0.15 (max. 2.20) OK Floor 0.12 (max. 0.25) 0.12 (max. 0.70) OK Roof 0.11 (max. 0.20) 0.11 (max. 0.35) OK **Openings** 1.10 (max. 2.00) 1.10 (max. 3.30) OK

3 Air permeability

Air permeability at 50 pascals: 3.50
Maximum: 10.00

OK

OK

4 Heating efficiency

Main heating system:

Boiler and underfloor heating, mains gas

Vaillant ecoFIT pure 630

Source of efficiency: from boiler database

Vaillant ecoFIT pure 630 VU 306/6-3 (H-GB)

Efficiency: 89.9% SEDBUK2009

Minimum: 88.0%

Secondary heating system:

None -

Page 11 of 12

5 Cylinder insulation Hot water storage Manufacturer's declared cylinder loss factor (kWh/day) 2.14 Permitted by DBSCG 2.86 OK Primary pipework insulated Yes OK **6 Controls** (Also refer to "Domestic Building Services Compliance Guide" by the DCLG) Time and temperature zone control OK Space heating controls Cylinderstat - Yes OK Independent timer for DHW - Yes OK **Boiler Interlock** Yes OK 7 Low energy lights Percentage of fixed lights with low-energy fittings: 100.0% Minimum: 75.0% OK 8 Mechanical ventilation Not applicable 9 Summertime temperature Overheating risk (Thames Valley): OK Slight OK Based on: Thermal mass parameter: 153.18 Overshading: Average or unknown (20-60 % sky blocked) Orientation: SouthWest Ventilation rate: 8.00 Blinds/curtains: None with blinds/shutters closed 0.00% of daylight hours 10 Key features

Double-glazed, argon filled, low-E, En=0.1, soft coat U-value 1.10 W/m²K

Flat roofs U-value 0.11 W/m²K Ground floors U-value 0.12 W/m²K

Pitched roofs insulated between rafters U-value 0.11 W/m²K

Design air permeability 3.5 m³/h.m²

Project Information

Building type Semi-detached house

Reference

Date 22 April 2022

Email: none Project The Studio

St. Johns Lodge Harley Road LONDON NW3 3BY

SAP 2012 worksheet for New dwelling as designed - calculation of energy ratings

1. Overall dwelling dimensions

| | Area | Av. Storey | Volume | |
|-----------------|--------|------------|---------|------------------|
| | (m²) | height (m) | (m³) | |
| Groundfloor (1) | 146.83 | 3.31 | 486.01 | (3a) |
| First floor | 118.87 | 3.20 | 380.38 | (3b) |
| Secondfloor | 111.86 | 3.00 | 335.58 | (3c) |
| Thirdfloor | 56.04 | 2.10 | 117.68 | (3d) |
| | 433.60 | | | (4) |
| | | | 1319.66 | (5) |

2. Ventilation rate

| | | | | | | | | | | | m³ per ho | our |
|-------------|-------------|------------|-------------|-------------|-----------|----------|-----------|--------|----------------|------|-----------|--------------|
| | | | | | | | main + s | eondar | y + othe | r | | |
| | | | | | | | heating | | | | | 4- > |
| | er of chim | • | | | | | 0 + 0 + 0 | | < 40 | | 0.00 | (6a) |
| | er of oper | | | | | | 0 + 0 + 0 |) | <i><</i> 20 | | 0.00 | (6b) |
| Numbe | er of inter | mittent fa | ans | | | | 7 |) | < 10 | | 70.00 | (7a) |
| Numbe | er of pass | ive vents | ; | | | | 0 |) | < 10 | | 0.00 | (7b) |
| | | ess gas f | | | | | 0 |) | < 40 | | 0.00 | (7c) |
| | | | | | | | | | | | Air chand | ges per hour |
| | | | | | | | | | | | 0.05 | (8) |
| Pressu | re test. r | esult q50 |) | | | | | | 3.50 | | | (17) |
| | meability | | | | | | | | 0.00 | | 0.23 | (18) |
| 7 tii poi i | noability | | | | | | | | | | 2.00 | (19) |
| | | | | | | | | | | | 0.85 | (20) |
| Infiltrat | ion rata i | acarnara | tina chal | ter factor | | | | | | | 0.19 | (20) |
| | | • | _ | hly wind s | | | | | | | 0.19 | (21) |
| | | | | | peeu | 1 | | | | | | |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
| 5.10 | 5.00 | 4.90 | 4.40 | 4.30 | 3.80 | 3.80 | 3.70 | 4.00 | 4.30 | 4.50 | 4.70 | |
| | | | | | | | | | | | 52.50 | (22) |
| Wind F | actor | | | | | | | | | | | |
| 1.27 | 1.25 | 1.23 | 1.10 | 1.07 | 0.95 | 0.95 | 0.93 | 1.00 | 1.07 | 1.13 | 1.18 | |
| | | | | | | | | | | | 13.13 | (22a) |
| Adjuste | ed infiltra | tion rate | (allowing | g for shelt | ter and w | ind spee | ed) | | | | | |
| 0.25 | 0.24 | 0.24 | 0.21 | 0.21 | 0.18 | 0.18 | 0.18 | 0.19 | 0.21 | 0.22 | 0.23 | |
| | | | | | | | | | | | 2.54 | (22b) |
| Ventila | tion : nat | ural vent | ilation, ii | ntermitte | nt extrac | t fans | | | | | | , , |
| | | inge rate | , | | | | | | | | | |
| 0.53 | 0.53 | 0.53 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.53 | (25) |
| 0.53 | 0.53 | 0.53 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.52 | 0.53 | (23) |

| 3 Heat losse | s and heat lo | ss naramete | r | | | | |
|---------------------------|---------------|-------------|-------------------|-------------|-------|-------------------|-------|
| Element | Gross | Openings | Net area | U-value | AxU | kappa-value A x K | |
| | area, m² | m² | A, m ² | W/m²K | W/K | kJ/m²K kJ/K | |
| Window - Doul | • | | 14.610 | 1.05 (1.10) | 15.39 | | (27) |
| argon filled, lo | • | | | ` , | | | ` ' |
| soft coat (Nort | h) | | | | | | |
| REAR-SIDE | SF | | | | | | |
| Window - Doul | ole-glazed, | | 5.460 | 1.05 (1.10) | 5.75 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Sou | | | | | | | |
| FRONT-SID | | | | | | | |
| Window - Doul | • | | 15.584 | 1.05 (1.10) | 16.42 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Nort | • | | | | | | |
| REAR-SIDE | | | | | | | (O-) |
| Window - Doul | • | | 5.824 | 1.05 (1.10) | 6.14 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Sou | • | | | | | | |
| FRONT-SID | | | 47.045 | 4.05 (4.40) | 40.47 | | (07) |
| Window - Doul | • | | 17.245 | 1.05 (1.10) | 18.17 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Sou FRONT GF | uivvesi) | | | | | | |
| Window - Doul | nle-alazed | | 6.190 | 1.05 (1.10) | 6.52 | | (27) |
| argon filled, lo | • | | 0.130 | 1.03 (1.10) | 0.52 | | (21) |
| soft coat (Sou | | | | | | | |
| , | E ENTRANCE | DOOR | | | | | |
| Window - Doul | | Doon | 12.480 | 1.05 (1.10) | 13.15 | | (27) |
| argon filled, lo | • | | | , | 10.10 | | (=,) |
| soft coat (Sou | | | | | | | |
| FRONTSF | , | | | | | | |
| Window - Doul | ole-glazed, | | 14.160 | 1.05 (1.10) | 14.92 | | (27) |
| argon filled, lo | | | | ` , | | | , , |
| soft coat (Sou | thWest) | | | | | | |
| FRONTFF | | | | | | | |
| Window - Doul | ole-glazed, | | 12.620 | 1.05 (1.10) | 13.30 | | (27) |
| argon filled, lo | w-E, En=0.1, | | | | | | |
| soft coat (Nort | hEast) | | | | | | |
| REAR FF | | | | | | | |
| Window - Doul | • | | 11.123 | 1.05 (1.10) | 11.72 | | (27) |
| argon filled, lo | | | | | | | |
| soft coat (Nort | hEast) | | | | | | |
| REAR SF | | | 44.500 | 4.40 | 40.04 | | (00) |
| Full glazed do | | | 14.580 | 1.10 | 16.04 | | (26) |
| Double-glazed | | | | | | | |
| low-E, En=0.1 (NorthEast) | , soit coat | | | | | | |
| REAR 3F | | | | | | | |
| Full glazed do | or - | | 23.766 | 1.10 | 26.14 | | (26) |
| Double-glazed | | | 23.700 | 1.10 | 20.17 | | (20) |
| low-E, En=0.1 | | | | | | | |
| (NorthEast) | , | | | | | | |
| REAR GF | | | | | | | |
| | | | | | | | |

| | e r heatin ged occupa | | y require | ements | | | | | | | kWh/yea 3.31 |
|----------|------------------------------|-------------|------------|-------------|-----------|----------|--------|--------|--------|--------|------------------------|
| Annual | average l | hot water | usage ir | n litres pe | er day Vd | ,average |) | | | | 112.71 |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| Hot wat | er usage | in litres p | oer day f | or each r | nonth | , | | | , | | |
| 123.98 | 119.47 | 114.96 | 110.45 | 105.95 | 101.44 | 101.44 | 105.95 | 110.45 | 114.96 | 119.47 | 123.98 |
| Energy | content c | of hot wat | ter used | | | | | | , | | |
| 183.86 | 160.80 | 165.93 | 144.67 | 138.81 | 119.78 | 111.00 | 127.37 | 128.89 | 150.21 | 163.97 | 178.06 |
| | content (a tion loss | annual) | | | | | | | | | 1773.34 |
| 27.58 | 24.12 | 24.89 | 21.70 | 20.82 | 17.97 | 16.65 | 19.11 | 19.33 | 22.53 | 24.59 | 26.71 |
| , | r volume, | | | _ | | | 150.00 | | | | |
| | cturer's d | | cylinder l | oss facto | or (kWh/c | day) | 2.00 | | | | |
| • | ature Factorial lost from | | er cylinde | r (kWh/c | lav) | | 0.5400 | | | | 1.08 |
| | orage los | | ,, oyac | . (| ω,, | | | | | | 1.00 |
| 33.48 | 30.24 | 33.48 | 32.40 | 33.48 | 32.40 | 33.48 | 33.48 | 32.40 | 33.48 | 32.40 | 33.48 |
| Net stor | age loss | | JL | | | J | JL | | JI. | J | |
| 33.48 | 30.24 | 33.48 | 32.40 | 33.48 | 32.40 | 33.48 | 33.48 | 32.40 | 33.48 | 32.40 | 33.48 |
| Primary | loss | , | Л | | , | , | Л | | JI. | , | |
| 23.26 | 21.01 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 | 23.26 | 22.51 | 23.26 | 22.51 | 23.26 |
| Total he | at requir | ed for wa | ter heati | ng calcul | ated for | each mo | nth | | JL. | Д | |
| 240.60 | 212.05 | 222.68 | 199.58 | 195.55 | 174.69 | 167.74 | 184.11 | 183.80 | 206.95 | 218.88 | 234.80 |
| Output 1 | from water | er heater | for each | month, k | «Wh/mor | nth | | | | | |
| 240.60 | 212.05 | 222.68 | 199.58 | 195.55 | 174.69 | 167.74 | 184.11 | 183.80 | 206.95 | 218.88 | 234.80 |
| | -8- | * | | | | | | | | | 2441.44 |
| Heat ga | ins from | water he | ating, kV | /h/month | 1 | | | | | | |
| 106.53 | 94.47 | 100.57 | 92.03 | 91.55 | 83.76 | 82.30 | 87.74 | 86.79 | 95.34 | 98.45 | 104.60 |

5. Internal gains

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|------------|------------|------------|----------|---------|---------|---------|---------|---------|---------|---------|---------|
| Metabol | ic gains, | Watts | , | | , | , | | | , | , | |
| 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 | 198.34 |
| Lighting | gains | | | | • | | | | • | | - |
| 124.63 | 110.70 | 90.03 | 68.16 | 50.95 | 43.01 | 46.48 | 60.41 | 81.08 | 102.95 | 120.16 | 128.10 |
| Appliand | ces gains | 3 | | | | | | | | | |
| 834.64 | 843.30 | 821.48 | 775.01 | 716.36 | 661.24 | 624.41 | 615.75 | 637.57 | 684.04 | 742.69 | 797.81 |
| Cooking | gains | • | | | | | • | | | | |
| 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 | 58.14 |
| Pumps a | and fans | gains | | | | | | | | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Losses | e.g. evap | oration (r | negative | values) | | | | | | | |
| -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 | -132.22 |
| Water he | eating ga | ins | | | | | | | | | |
| 143.18 | 140.58 | 135.17 | 127.82 | 123.05 | 116.33 | 110.62 | 117.94 | 120.54 | 128.14 | 136.73 | 140.59 |
| Total inte | ernal gaiı | ns | | | | | | | | | |
| 1226.71 | 1218.83 | 1170.93 | 1095.24 | 1014.61 | 944.83 | 905.76 | 918.35 | 963.45 | 1039.39 | 1123.84 | 1190.75 |

6. Solar gains (calculation for January)

| | Area & Flux | g & FF | Shading | Gains |
|--|--------------------|-------------|---------|----------|
| Window - Double-glazed, argon filled, low-E, | 0.9 x 14.610 10.63 | 0.63 x 0.80 | 0.77 | 54.2608 |
| En=0.1, soft coat (North) | | | | |
| REAR-SIDE SF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 5.460 46.75 | 0.63 x 0.80 | 0.77 | 89.1574 |
| En=0.1, soft coat (South) | | | | |
| FRONT-SIDE SF | 0.045 50440.00 | 0.000.00 | 0.77 | FZ 0704 |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 15.584 10.63 | 0.63 X 0.80 | 0.77 | 57.8781 |
| En=0.1, soft coat (North) REAR-SIDE FF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 5.824 46.75 | 0.63 x 0.80 | 0.77 | 95.1012 |
| En=0.1, soft coat (South) FRONT-SIDE FF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 17.245 36.79 | 0.63 x 0.80 | 0.77 | 221.6165 |
| En=0.1, soft coat (SouthWest) | | | | |
| FRONTGF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 6.190 46.75 | 0.63 x 0.80 | 0.77 | 101.0728 |
| En=0.1, soft coat (South) | | | | |
| FRONT-SIDE ENTRANCE DOOR | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 12.480 36.79 | 0.63 x 0.80 | 0.77 | 160.3812 |
| En=0.1, soft coat (SouthWest) FRONTSF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 14.160 36.79 | 0.63 x 0.80 | 0.77 | 181.9709 |
| En=0.1, soft coat (SouthWest) FRONTFF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 12.620 11.28 | 0.63 x 0.80 | 0.77 | 49.7331 |
| En=0.1, soft coat (NorthEast) | | | | |
| REAR FF | | | | |

Page 5 of 14

| 6. Solar gains (calculation for January) | | . == | O | | |
|--|---|------------------------------|--|------------------------------|--------|
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (NorthEast) REAR SF | Area & Flux 0.9 x 11.123 11.28 | g & FF 0.63 x 0.80 | Shading 0.77 | Gains 43.8337 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (NorthEast) REAR 3F | 0.9 x 14.580 11.28 | 0.63 x 0.80 | 0.77 | 57.4571 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (NorthEast) REAR GF | 0.9 x 23.766 11.28 | 0.63 x 0.80 | 0.77 | 93.6574 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE | 0.9 x 19.496 10.63 | 0.63 x 0.80 | 0.77 | 72.4067 | |
| Full glazed door - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT3F | 0.9 x 14.510 36.79 | 0.63 x 0.80 | 0.77 | 186.4688 | |
| Rooflight at 70° or less - Double-glazed, argon filled, low-E, En=0.1, soft coat (n/a) ROOF | 0.9 x 10.130 26.00 | 0.63 x 0.80 | 1.00 | 119.4692 | |
| Total solar gains, January | | | | 1584.46 | (83-1) |
| Solar gains | | | | | |
| | 03.5 7122.6 6093. | 9 4858.0 3248 | 3.5 1924.23 <i>1</i> | 1338.93 | (83) |
| Total gains | 10.0 0000 0 7010 | 0 5004 4 4007 | 0 00404 | 2502.7 | (0.4) |
| 2811.2 4063.3 5452.9 7060.6 8302.9 84 | 48.3 8028.3 7012. | 3 5821.4 4287 | 7.9 3048.1 2 | 2529.7 | (84) |
| | | | | | |
| Lighting calculations | | | | | |
| | Area | g 0.80 | FF x Shadir | - | |
| Lighting calculations Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF | Area 0.9 x 14.61 | g 0.80 | FF x Shadir 1.00 x 0.83 | ng 8.73 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | | | | - | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) | 0.9 x 14.61 | 0.80 | 1.00 x 0.83 | 8.73 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | 0.9 x 14.61 0.9 x 5.46 | 0.80 | 1.00 x 0.83 1.00 x 0.83 | 8.73 3.26 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) | 0.9 x 14.61 0.9 x 5.46 0.9 x 15.58 | 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 8.73 3.26 9.31 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, | 0.9 x 14.61 0.9 x 5.46 0.9 x 15.58 0.9 x 5.82 | 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 8.73 3.26 9.31 3.48 | |
| Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE SF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (North) REAR-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (South) FRONT-SIDE FF Window - Double-glazed, argon filled, low-E, En=0.1, soft coat (SouthWest) FRONT GF Window - Double-glazed, argon filled, low-E, | 0.9 x 14.61 0.9 x 5.46 0.9 x 15.58 0.9 x 5.82 0.9 x 17.25 | 0.80 0.80 0.80 0.80 | 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 1.00 x 0.83 | 8.73 3.26 9.31 3.48 | |

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Lighting calculations

| | Area | g | FF x Shading | |
|--|-------------|------|--------------|------|
| Window - Double-glazed, argon filled, low-E, | 0.9 x 12.62 | 0.80 | 1.00 x 0.83 | 7.54 |
| En=0.1, soft coat (NorthEast) | | | | |
| REAR FF | | | | |
| Window - Double-glazed, argon filled, low-E, | 0.9 x 11.12 | 0.80 | 1.00 x 0.83 | 6.65 |
| En=0.1, soft coat (NorthEast) | | | | |
| REAR SF | | | | |
| Rooflight at 70° or less - Double-glazed, | 0.9 x 10.13 | 0.80 | 0.80 x 1.00 | 5.83 |
| argon filled, low-E, En=0.1, soft coat (n/a) | | | | |
| ROOF | | | | |
| GL = 74.74 / 433.60 = 0.172 | | | | |
| C1 = 0.500 | | | | |

C2 = 0.960

EI = 880

| Temper | n interna rature du | ring heat | ing perio | ds in the | living are | ea, Th1 (° | °C) | | | | 21.00 |
|-----------|-------------------------------|-------------|-------------|------------|------------|------------|-------|--------|-------|-----------|-------|
| | system | | - N | 1 | | | | T - | | | 0.75 |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
| tau | | | 70 | | | | | | 1 | | |
| 29.51 | 29.54 | 29.56 | 29.68 | 29.70 | 29.80 | 29.80 | 29.82 | 29.76 | 29.70 | 29.65 | 29.61 |
| alpha | | | | | | | | | | | |
| 2.97 | 2.97 | 2.97 | 2.98 | 2.98 | 2.99 | 2.99 | 2.99 | 2.98 | 2.98 | 2.98 | 2.97 |
| Utilisati | on factor | for gains | for living | area | | _ | | | | | |
| 0.99 | 0.96 | 0.90 | 0.77 | 0.60 | 0.44 | 0.33 | 0.39 | 0.62 | 0.88 | 0.97 | 0.99 |
| Tweekd | lay | | | | | | | | | | |
| 18.99 | 19.37 | 19.87 | 20.38 | 20.70 | 20.84 | 20.88 | 20.87 | 20.74 | 20.22 | 19.48 | 18.92 |
| Tweeke | nd | | | | | | | | | | |
| 19.86 | 20.07 | 20.36 | 20.65 | 20.83 | 20.91 | 20.93 | 20.93 | 20.85 | 20.56 | 20.14 | 19.82 |
| 24 inste | ad of 16 | • | | | • | | | | · | | |
| 8.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 24 inste | ad of 9 | | | | | | | | | | |
| 21.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 16 inste | ad of 9 | | | | 1 | | | | | | |
| 1.00 | 20.00 | 7.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 22.00 |
| Mean in | ternal te | mperatu | re in livin | garea T1 | | | _* | | | | |
| 20.93 | 20.07 | 20.12 | 20.45 | 20.74 | 20.86 | 20.89 | 20.88 | 20.77 | 20.32 | 19.66 | 19.82 |
| Temper | rature du | ring heat | ing perio | ds in res | t of dwell | ing Th2 | | | | | |
| 19.73 | 19.73 | 19.73 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 | 19.74 |
| Utilisati | on factor | for gains | for rest | of dwelli | ng | | | | | IL | |
| 0.98 | 0.95 | 0.88 | 0.73 | 0.54 | 0.36 | 0.24 | 0.29 | 0.54 | 0.84 | 0.96 | 0.99 |
| Tweekd | lay | | _ | | | _ | | | | | |
| 17.41 | 17.88 | 18.49 | 19.10 | 19.45 | 19.57 | 19.60 | 19.60 | 19.50 | 18.95 | 18.03 | 17.31 |
| Tweeke | nd | | _ | | | _ | | | | | |
| 17.41 | 17.88 | 18.49 | 19.10 | 19.45 | 19.57 | 19.60 | 19.60 | 19.50 | 18.95 | 18.03 | 17.31 |
| | nternal te | | | rest of dv | | | | | | | |
| 19.58 | 17.88 | 18.49 | 19.10 | 19.45 | 19.57 | 19.60 | 19.60 | 19.50 | 18.95 | 18.03 | 17.31 |
| | rea fracti | _ | | | | 1 | | 1.0.00 | 1 | 1 2 2 2 2 | 0.34 |
| _ | iternal te | ` | | , | welling) | | | | | | |
| 20.04 | 18.62 | 19.04 | 19.56 | 19.88 | 20.01 | 20.04 | 20.03 | 19.93 | 19.41 | 18.58 | 18.16 |
| Apply a | djustmer | nt to the r | nean inte | rnal tem | perature | _ | _ L | ate | | | |
| 20.04 | 18.62 | 19.04 | 19.56 | 19.88 | 20.01 | 20.04 | 20.03 | 19.93 | 19.41 | 18.58 | 18.16 |

8. Space heating requirement

| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec |
|--------------------------------------|------------|------------|-----------|----------|---------|-----------|-----------|--------|---------|--------|---------|
| Utilisatio | n factor | for gains | | , | | , | | | , | , | |
| 0.98 | 0.94 | 0.86 | 0.72 | 0.55 | 0.38 | 0.26 | 0.31 | 0.55 | 0.83 | 0.95 | 0.98 |
| Usefulgains | | | | | | | | | | | |
| 2762.0 | 3817.6 | 4711.4 | 5115.1 | 4551.6 | 3218.9 | 2100.3 | 2197.1 | 3224.8 | 3566.3 | 2904.8 | 2483.8 |
| Monthly average external temperature | | | | | | | | | | | |
| 4.30 | 4.90 | 6.50 | 8.90 | 11.70 | 14.60 | 16.60 | 16.40 | 14.10 | 10.60 | 7.10 | 4.20 |
| Heat los | s rate for | mean in | ternal te | mperatu | re | | | | | | |
| 9837.4 | 8570.4 | 7828.7 | 6627.1 | 5084.3 | 3349.8 | 2130.2 | 2248.7 | 3613.1 | 5475.0 | 7144.1 | 8699.2 |
| Fraction | of month | n for heat | ting | | | | | | | | |
| 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | - | - | - | - | 1.00 | 1.00 | 1.00 |
| Space h | eating re | quireme | nt for ea | ch month | , kWh/m | onth | | | | | |
| 5264.1 | 3193.9 | 2319.2 | 1088.63 | 396.32 | - | - | - | - | 1420.13 | 3052.3 | 4624.3 |
| | ace heat | • | | • | | ar) (Octo | ber to Ma | ay) | , | , | 21358.9 |
| Space h | eating re | quireme | nt per m² | kWh/m | ²/year) | | | | | | 49.2 |

8c. Space cooling requirement - not applicable

| 9a. Energy requirements | |
|-------------------------|--|
|-------------------------|--|

| | | uiremen | | | | | | | | | kWh/year | |
|--|---------------------------------------|--|-----------------------|--------------------|----------|--|--------|--------|------------------|--------|---------------------------------------|-------------------------|
| Fraction | of spac | eating sy e heat fro in heating | om main | system(| s) | | | 5 | 1.0000 04.98% | | | (202) (206) |
| Jan | Feb | Mar | Apr | May | Jun | Jul | Aug | Sep | Oct | Nov | Dec | |
| Spaceh | eating re | quireme | nt | | | | | | , | | | |
| 5264.1 | 3193.9 | 2319.2 | 1088.63 | 396.32 | - | - | - | - | 1420.13 | 3052.3 | 4624.3 | (98) |
| Append | ix Q - mo | onthly en | ergy sav | ed (main | heating | system 1 | 1) | | Л | J. | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (210) |
| Space heating fuel (main heating system 1) | | | | | | | | | | | | |
| 1042.43 | 632.48 | 459.27 | 215.58 | 78.48 | - | - | - |]- | 281.23 | 604.44 | 915.74 | (211) |
| Append | ix Q - mo | onthly en | ergy sav | ed (main | heating | system 2 | 2) | | Л | J(| | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (212) |
| Space h | neating fu | uel (main | heating | system 2 | 2) | | | | , | | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |]- | - | - |]- | 0.00 | 0.00 | 0.00 | (213) |
| Append | ix Q - mo | nthly en | ergy sav | ed (seco | ndary he | ating sys | stem) | | , | | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (214) |
| Space h | eating fu | iel (secor | ndary) | ж | | <u>, </u> | ., | | JI. | -J. | | |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | - | - | - | - | 0.00 | 0.00 | 0.00 | (215) |
| Waterh | | | J. | | | | | | , | | | |
| Waterh | eating re | quiremer | nt | | | | | | | | | |
| 240.60 | 212.05 | 222.68 | 199.58 | 195.55 | 174.69 | 167.74 | 184.11 | 183.80 | 206.95 | 218.88 | 234.80 | (64) |
| Efficiend | cy of wat | er heater | | | | | | | | | 313.50 | (216) |
| 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | 313.50 | (217) |
| Waterh | eating fu | el | _ | | | | | | | | | |
| 76.75 | 67.64 | 71.03 | 63.66 | 62.38 | 55.72 | 53.51 | 58.73 | 58.63 | 66.01 | 69.82 | 74.90 | (219) |
| Space h Water h | neating fu neating fu eating fu | uel used, iel (secor el mps, fan: | ndary) | | on hot | | | | | | kWh/year 4229.65 0.00 778.77 | (211) (215) (219) |
| Total ele Electrici | ectricity fity for ligh | or the ab nting (100 eneration | ove, kWl 0.00% fix | h/year ked LEL) | ;р-поt | | | | | | 0.00 880.44 | (231) (232) |
| • | ity gener | ated - µC | | - | | | | | | | 0.00 | (235) |
| | | or genera | ated (): | | | | | | | | 0.000 | (236a) |
| | y used () | | | | | | | | | | 0.000 | (237a) |
| Total de | livered e | nergy for | all uses | | | | | | | | 5888.86 | (238) |

10a. Fuel costs using Table 12 prices

| | kWh/year | Fuel price p/kWh | £/year | |
|-------------------------------|----------|---------------------|--------------|----------------|
| Space heating - main system 1 | 4229.654 | 13.190 | 557.89 | (240) |
| Space heating - main system 2 | 0.000 | 0.000 | 0.00 | (241) |
| High-rate percentage | 100.000% | | | (243) |
| Low-rate percentage | 0.000% | | | (244) |
| High-rate cost | 778.77 | 13.190 | 102.72 | (245) |
| Low-rate | 0.00 | 13.190 | 0.00 | (246) |
| Mech vent fans cost | 0.000 | 13.190 | 0.00 | (249) |
| Pump/fan energy cost | 0.000 | 13.190 | 0.00 | (249) |
| Energy for lighting | 880.436 | 13.190 | 116.13 | (250) |
| Additional standing charges | | | 0.00 | (251) |
| Electricity generated - PVs | 0.000 | 0.000 | 0.00 | (252) |
| Appendix Q - | | | | |
| Energy saved or generated (): | 0.000 | 0.000 | 0.00 | (253) |
| Energy used (): | 0.000 | 0.000 | 0.00 | (254) |
| Total energy cost | | | 776.74 | (255) |
| 11a. SAP rating | | | | |
| · · | | | 0.42 0.68 | (256) (257) |
| SAPvalue | | | 90.49 | (050) |
| SAP band | | | 90 B | (258) |

12a. Carbon dioxide emissions

| | Energy | Emission factor | Emission | S | |
|----------------------------------|----------|------------------------|-----------------|--------|--|
| | kWh/year | kg CO2/kWh | kg CO2/y | ear | |
| Space heating, main system 1 | 4229.65 | 0.519 | 2195.19 | (261) | |
| Space heating, main system 2 | 0.00 | 0.000 | 0.00 | (262) | |
| Space heating, secondary | 0.00 | 0.519 | 0.00 | (263) | |
| Waterheating | 778.77 | 0.519 | 404.18 | (264) | |
| Space and water heating | | | 2599.37 | (265) | |
| Electricity for pumps and fans | 0.00 | 0.519 | 0.00 | (267) | |
| Electricity for lighting | 880.44 | 0.519 | 456.95 | (268) | |
| Electricity generated - PVs | 0.00 | 0.519 | 0.00 | (269) | |
| Electricity generated - µCHP | 0.00 | 0.519 | 0.00 | (269) | |
| Appendix Q - | | | | | |
| Energy saved (): | 0.00 | 0.000 | 0.00 | (270) | |
| Energy used (): | 0.00 | 0.000 | 0.00 | (271) | |
| Total CO2, kg/year | | | 3056.32 | (272) | |
| | | | kg/m²/year | | |
| CO2 emissions per m ² | | | 7.05 | (273) | |
| Elvalue | | | 91.44 | (273a) | |
| El rating | | | 91 | (274) | |
| El band | | | В | | |

Calculation of stars for heating and DHW

Main heating energy efficiency Main heating environmental impact Water heating energy efficiency Water heating environmental impact $(13.19 / 5.0498) \times (1 + (0.29 \times 0.25)) = 2.8014$, stars = 5 $(0.5190 / 5.0498) \times (1 + (0.29 \times 0.25)) = 0.1102$, stars = 5 13.19 / 3.1350 = 4.2073, stars = 4 $0.52 / + (0.00 \times 0.52) = 0.1656$, stars = 5

Project Information

Building type Semi-detached house

Reference

22 April 2022 Date

Email: none Project The Studio

> St. Johns Lodge Harley Road LONDON NW3 3BY

REGULATION COMPLIANCE REPORT - Approved Document L1A, 2012 Edition, England

assessed by program JPA Designer version 6.05.054, printed on 02/05/2022 at 10:05:19

New dwelling as designed

1 TER and DER

Fuel for main heating system: Standard tariff (fuel factor = 1.55)

Target Carbon Dioxide Emission Rate TER = 21.46**Dwelling Carbon Dioxide Emission Rate** DER = 7.35

OK

OK

1b TFEE and DFEE

Target Fabric Energy Efficiency (TFEE) TFEE = 62.9Dwelling Fabric Energy Efficiency (DFEE)

DFEE = 55.8OK

2a Thermal bridging

Thermal bridging calculated using default y-value of 0.15

2b Fabric U-values

Element Highest <u>Average</u> Wall 0.25 (max. 0.30) 0.25 (max. 0.70) OK **Curtain Wall** 0.15 (max. 2.20) 0.15 (max. 2.20) OK Floor 0.12 (max. 0.25) 0.12 (max. 0.70) OK Roof 0.11 (max. 0.20) 0.11 (max. 0.35) OK **Openings** 1.10 (max. 2.00) 1.10 (max. 3.30) OK

3 Air permeability

Air permeability at 50 pascals: 3.50 Maximum: 10.00

4 Heating efficiency

Main heating system:

Air source heat pump, underfloor, electric

Grant AERONA3

Source of efficiency: from boiler database

Secondary heating system:

None -

5 Cylinder insulation

Hot water storage No cylinder

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6 Controls

(Also refer to "Domestic Building Services Compliance Guide" by the DCLG)

Space heating controls 2207 Time and temperature zone control

Hot water controls No cylinder

Boiler Interlock No OK

7 Low energy lights

Percentage of fixed lights with low-energy fittings: 100.0%

Minimum: 75.0% OK

8 Mechanical ventilation

Not applicable

9 Summertime temperature

Overheating risk (Thames Valley):

Slight OK

OK

Based on:

Thermal mass parameter: 153.18

Overshading: Average or unknown (20-60 % sky blocked)

Orientation: SouthWest

Ventilation rate: 8.00

Blinds/curtains:

None with blinds/shutters closed 0.00% of daylight hours

10 Key features

Double-glazed, argon filled, low-E, En=0.1, soft coat U-value 1.10 W/m²K

Flat roofs U-value 0.11 W/m²K Ground floors U-value 0.12 W/m²K

Pitched roofs insulated between rafters U-value 0.11 W/m²K

Design air permeability 3.5 m³/h.m²