# **Agar Grove Block B (Phase 2a)**

# **Energy and Sustainability Update**

# **Rev P02**

27<sup>th</sup> May 2022

# $\mathbf{E}\mathbf{B}$  Camden



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# **1.0 EXECUTIVE SUMMARY**

<span id="page-3-0"></span>Planning permission was granted in August 2014 (and amended in 2020) for the comprehensive redevelopment of the Agar Grove Estate comprising mixed-tenure new homes along with retail, business and community spaces.

To date, Blocks A, F, G and H have been completed and construction works on Blocks I and JKL are underway.

This Report is submitted in support of an application to amend Block B of the approved scheme. The need for these changes arises due to the current housing needs of the returning Agar Grove estate residents; responding to current and emerging building regulations; and to take into account lessons learnt during the first phases of development, particularly in relation to Passivhaus.

Block B includes 2No. residential towers with 94No. dwellings, with a Community Centre and Flexible Workspace and Landlord's ancillary areas at Ground and first floor levels.

As described in the original planning application the Passivhaus standard will be used to deliver an enhanced GLA 'Be Lean' performance, denoting a low operational energy and high thermal comfort building. To maximise energy/carbon savings individual exhaust air heat pumps are now proposed for Block B dwellings and Air Source Heat Pump systems are proposed for the non- residential areas. This in line with the government's plan to phase out gas boilers. Photovoltaic panels will be located on the uppermost roofs of each building.

Block by block air source heat pump heating systems are still proposed for Block B in line with the draft new London plan and the government's plan to phase out gas boilers. However, Block B contains dwellings with very low thermal demands due to the Passivhaus approach, allowing decentralised exhaust air heat pumps (ExAHP) to provide heating. Photovoltaic panels will be located on the uppermost roofs of each building.

As a result of these measures a total carbon reduction of 69 % is achieved across the residential areas of the development and a 35% for the non-residential areas, resulting in a total site wide saving of 65% against Part L 2013.

A 25% saving will be made at the 'Be Lean' stage for residential areas and a 25% saving for the Non-residential areas.

# <span id="page-3-1"></span>**1.1 Carbon Dioxide Reduction Targets**

The carbon reduction target at the time of the original application was 40% reduction over 2010 Part L requirements. This 40% overall reduction was to include a 20% reduction in carbon dioxide emissions from onsite renewables.

As the carbon intensity of the grid continues to reduce new emission factors have been released and are proposed for use by the draft London Plan. To reflect this, the carbon reduction has been calculated using SAP 10 carbon emission factors in line with the draft new London Plan and to reflect the decarbonisation of the grid. According to the Greater London Authority document 'Energy Assessment Guidance' a 35% reduction against Part L 2013 is equivalent to a 40% reduction against Part L 2010

# <span id="page-3-2"></span>**1.2 Emissions Factors**

Unless otherwise stated SAP 10 current carbon emissions have been used throughout this report.

Carbon dioxide emissions factors for the original planning application based on SAP 2012 and current SAP 10 are provided in the table below.





**SAP 2012 and SAP 10 carbon factors**

The SAP 10 carbon factors better reflect the decarbonisation of grid electricity. This results in electrically powered heat pumps being favoured for heating and means CHP engines are less beneficial in carbon terms. It also results in the perceived benefit of PVs being reduced

The SAP 10.2 adopted as part of the June 2022 changes to the building regulations in England and Wales set out a carbon factor for grid electricity at 0.136 kg CO2/kWh will mean an all-electric based development will reduce its carbon emissions by a further 41% compared to the SAP 10 (current) figures above.

# <span id="page-4-0"></span>**1.3 Key Strategies**

The key energy strategies are described below:

# **Be Lean**- Demand Reduction

- High fabric performance- Passivhaus standards
- Mechanical Ventilation with Heat Recovery (MVHR) throughout

**Be Clean**- Efficient Energy Supply

• High efficiency MVHR

**Be Green**- Renewable Energy

- Air Source Heat Pumps used to provide heating and generate hot water
- PV array



# **1.4 Summary of Results**

<span id="page-5-0"></span>The proposed development has been remodelled in SAP incorporating the fabric and servicing strategy changes described above and in sections 3, 4 and 5.

# **Domestic**







**6**

#### Figure 1 - Domestic SAP 10 Carbon Emissions Summary



Table 1: Carbon Dioxide Emissions after each stage of the Energy Hierarchy for domestic buildings

Table 2: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for domestic buildings



\*carbon price is based on GLA recommended price of £95 per tonne of carbon dioxide unless Local Planning Authority price is inputted in the 'Development Information' tab



Table 3: Carbon Dioxide Emissions after each stage of the Energy Hierarchy for non-domestic buildings



Table 4: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for non-domestic buildings



\*carbon price is based on GLA recommended price of £95 per tonne of carbon dioxide unless Local Planning Authority price is inputted in the 'Development Information' tab

#### **Non Domestic**



**Figure 1 - Non-Domestic SAP 10 Carbon Emissions Summary**



Table 3: Carbon Dioxide Emissions after each stage of the Energy Hierarchy for non-domestic buildings



Table 4: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for non-domestic buildings



\*carbon price is based on GLA recommended price of £95 per tonne of carbon dioxide unless Local Planning Authority price is inputted in the 'Development Information' tab



# **Total site wide carbon savings**



**Table 1 - SAP 10 Total site-wide carbon savings**



# <span id="page-11-0"></span>**2.0 CO<sup>2</sup> MODELLING METHODOLOGY**

# **2.1 Dwellings**

<span id="page-11-1"></span>The carbon footprints as shown in the tables above have been calculated using the following methods:

# **Dwellings:**

A Dwelling Emissions Rate (DER) has been calculated in line with the Building Regulations Part L 2013 methodology SAP 2012 using accredited software Stroma FSAP 2012. The results were then converted using the GLA SAP 10 conversion spreadsheet with the carbon factors listed in Section [1.2.](#page-3-2)

SAP calculations have been carried out for all of the 35No. unique SAP dwelling Energy types identified via different flat sizes, orientations, locations within each block i.e. bottom/middle/top floors. Full SAP flat type markups are provided in appendix 1, examples in the figure below. SAP work sheet and GLA SAP 10 spreadsheet can be found in appendix 2.



<span id="page-11-2"></span>**Figure 2 - SAP Energy Type Markup**

# **2.2 Non-residential areas**

The non-residential areas are located on the ground and first floor with a double height community hall situated on the west wall of the western block. The rest of the western block's ground floor area consists of a residential lobby, concierge office and space that has not yet been allocated. Meanwhile the ground floor of the eastern block contains plant space, bike storage and bin storage.  $83m^2$  of general flexible workspace is also situated on the ground floor and is connected to the first-floor flexible workspace that covers all the first floor, with no specific areas being marked out. Similarly, the western block's first floor consists entirely of community area and meeting rooms, demanding similar needs to the flexible workspace. In total, the commercial space covers 1850m<sup>2</sup> of floor space that has been assessed for Part L energy usage using IES modelling software (IES VE 2021.4.0.0). MEP systems in place to ensure user comfort is delivered efficiently are detailed below.

- VRF heat pump system
- Mechanical ventilation with heat recovery (MVHR)
- Efficient LED with daylighting control
- Local point of view hot water heating for restrooms and kitchens





**Figure 3 - No-Domestic Part L IES model**





# <span id="page-13-0"></span>**3.0 BUILDING FABRIC PERFORMANCE (BE LEAN)**

# **3.1 Fabric Performance summary**

<span id="page-13-1"></span>As described in the previous planning report carbon emissions will be reduced primarily implementing 'passive' energy efficiency measures. Block B has been designed based on the Passivhaus approach.

It is recognised that Passivhaus is better at delivering lower energy in use than the SAP methodology. Achieving Passivhaus certification helps close the performance gap between what is designed and what is built. This is because Passivhaus follows a rigorous process, adopts stringent quality control measures during design and construction and uses tried and tested energy modelling tools (Passivhaus Planning Package or PPP)

Fabric performance targets are shown below.

# **Be Lean / Fabric Performance**

- Wall U-value  $-0.18$  W/m2K
- Window U-value 0.85 W/m2K
- Roof U-Value 0.15 W/m2K
- Glazing g-value  $-0.4$
- Whole building airtightness 0.6 Air changes per hour@50Pa
- Thermal bridging calculated in line with SAP methodology
- Use of Passivhaus Certified High Efficiency Mechanical Ventilation with Heat Recovery units for both residential and non-residential areas (MVHR)

# **4.0 HEATING INFRASTRUCTURE (BE CLEAN)**

<span id="page-13-2"></span>At the original planning application stage, high efficiency gas condensing boilers were selected. As discussed in sectio[n1.2](#page-3-2) the carbon factor for grid electricity is dropping over time and therefor electrification of heat has been investigated and energy strategy revised accordingly.



#### **Connection to existing networks**

As described in the original planning application connection to the existing King's Cross Argent network would not be feasible as the route would require crossing a major railway line and the existing boiler house has no



spare capacity.

#### **Figure 4 - London heat map**

No new heat networks have been developed in the area since the previous application.

#### **Site wide district heating network**

Latest GLA policy suggest that that CHP is no longer appropriate for a development such as Agar Grove Phase 2a CHP: A site wide heat network across the entire masterplan site, was earlier deemed inappropriate due to the phased delivery of the development and objections raised by residents during consultation.

An on-site heat network for Agar grove Phase 2a was investigated and compared against alternative strategies described in Sectio[n 0.](#page-17-2) On balance was found that decentralised systems would provide lower overall costs to residents than systems with an on-site heat network, reducing the risk of fuel poverty. Decentralised systems provide large carbon savings and allow a clear route to Passivhaus certification.

Benefits of decentralised system vs on-site heat network summarised below, see Section [0](#page-17-2) for a more detailed description.

- No heat network distribution losses or pumping energy
- Lower annual servicing costs to residents
- Lower overall fuel costs
- No heat metering and billing/administration costs
- Lower plant replacement/sinking fund costs
- Lower overall annual costs to residents

#### **Decarbonisation of the Grid**

When looking at energy efficiency it is also useful to consider fuel sources and their carbon efficiency. Heating and hot water provided by natural gas boilers was previously proposed for the site. This is becoming a now becoming a comparatively carbon intense fuel source compared to mains electricity.

The current carbon intensity of the UK electricity grid is considerably lower than the factors written into the 2013 Part L of the Building Regulations. SAP 10.0 carbon emissions factors have been used in the calculations throughout this report - in line with GLA guidance on preparing energy assessment.



The latest proposed SAP 10.2 carbon factor for grid electricity at 0.136 kg CO2/kWh will mean an all-electric based development (such Agar Grove Phase 2a) will reduce its carbon emissions by a further 41% compared to the SAP 10. This is more representative of the real-world situation.

As more renewable technologies are used to supply the electricity grid it is expected that this figure will continue to reduce. In terms of carbon reduction, efficient all electric systems are preferable. This is shown in the Department of Energy and Climate Change Energy and Emissions Predictions.

The solid blue line in the following graph shows how the carbon intensity of the UK grid is predicted to drop based on 2019 predictions, and the dashed blue line is the same measure based on 2018 predictions.



**Figure 5 - Department of Energy and Climate Change (DECC) Energy and Emissions Predictions (EEP) 2018 and 2019.**

#### **Heat Source Selection**

As previously described above SAP 10 carbon emission rates more accurately reflect the carbon intensity of the electricity grid. In line with latest GLA policy, electrification of heat has been prioritised, with heat pumps specified to maximise carbon savings.



# <span id="page-16-0"></span>**5.0 RENEWABLE ENERGY (BE GREEN)**

Heat pumps have been identified in the previous section as a more suitable heat source than gas boilers due to decarbonisation of the grid. This change in heat source will impact the selection of supplementary renewable technologies chosen. PV has also been maximised to all available/suitable roof area.

# <span id="page-16-1"></span>**5.1 Air Source Heat Pumps**

A heat pump is akin to a domestic fridge: it uses electricity to move heat from one material to another. An air source heat pump (ASHP) moves heat from the outside air to a fluid (water). It uses a refrigerant to achieve this, and generally uses electricity as a power source. [Figure 6](#page-16-3) illustrates in simple terms how a typical ASHP works.



<span id="page-16-3"></span>**Figure 6 - How an air source heat pump works**

As the ASHP is moving heat from one location to another, it is possible to transfer more heat than the energy put in. This is generally defined by the Coefficient of Performance (COP):

$$
COP = \frac{Useful\ heat\ transferred}{Energy\ Input}
$$

<span id="page-16-2"></span>So a heat pump that moved 3kW of heat for 1kW of electrical power input would have a COP of 3. The COP is generally higher the closer the air and water temperatures are to each other.

# **5.2 Climate Change**

Recent years have seen particularly warm summers, which are anticipated to continue with ongoing climate change. Carbon emissions contribute to climate change, so there is a responsibility to choose low-carbon solutions where possible.



The increasing temperatures also mean that summer comfort is increasingly becoming a concern. This means designs should allow for future climate change, and ideally ensure comfortable conditions can be achieved, including the provision of comfort cooling where passive measures will be inadequate.

# <span id="page-17-0"></span>**5.3 Passivhaus Primary Energy Assessment**

<span id="page-17-2"></span>For the Passivhaus standard, the predicted total energy demand of the building is modelled. Passivhaus modelling results give a more reliable estimate of the in-use energy consumption, than those associated with Building Regulations compliance.

# <span id="page-17-1"></span>**5.4 Proposed System and Rationale**

# **Domestic**

The proposed system uses individual compact Exhaust Air Heat Pumps (ExAHP) within each flat to locally generate heating and hot water. These units combine the functions of a traditional MVHR unit with a heat pump and hot water cylinder.



- 1. Warm exhaust air is blown across the heat exchanger and the heat is transferred into the refrigerant circuit. The cold exhaust air passes to the outside of the house.
- 2. The compressor raises the pressure of the refrigerant, resulting in an increase in temperature in the heat pump
- 3. Energy extracted from the exhaust air is transferred into a water-based heating system to heat your home and hot water.
- 4. In the condenser, the refrigerant reverts to liquid form, ready to turn into gas once more and to collect new heat energy.

**Figure 7 - Exhaust air heat pump system**

Compact exhaust air heat pumps are only suitable dwellings with very low thermal demands. The rigorous Passivhaus approach used on Agar Grove Phase 2a will ensure the actual 'in use' heating demand is low enough to allow this technology to be used successfully.

ExAHP units recover energy from extracted air using a highly efficient counter flow heat exchanger in the same way as an MVHR unt. The remaining energy that is not utilised by the counter flow heat exchanger is used by the heat pump to charge a hot water, and to further heat the supply air.

The heat pump within an EXAHP unit is typically capable of running in reverse in summer to provide a small amount of cooling allowing the unit to temper the incoming supply air by up to around to 10 °C however it does not function as an air conditioning system. When 'cooling' mode is activated, the supply air is dehumidified; this helps provide a more pleasant indoor climate than is possible with standard MVHR system.



Heat energy extracted from the air is recovered where possible and used to produce hot water, offsetting associated energy demand.

The principal benefits of this system are:

- Efficiency: Generating heat locally with heat pumps, maximises efficiency avoiding heat losses and pumping energy associated with centralised systems.
- Fuel Poverty: Lowest overall costs to residents.
- Environmental impact: the use of electricity is consistent with a decarbonising electricity grid, and a design that is aligned with limiting environmental impact
- Compliance: the use of electricity is in line with the new London Plan
- Air quality: the use of electricity means there is no combustion on the site, and so no omission of particulates, or incomplete products of combustion  $(NO<sub>x</sub> etc.)$
- Futureproofing: the ExAHP units can provide both heating and small amount of cooling. Cooling also allows residents to shut their windows at night, and still be thermally comfortable, if there are external noise issues.
- Passivhaus : Compact units have low energy consumption and leaner pipework distribution that could help reduce heat losses, total energy demand and therefore achieve Passivhaus targets.

# **Non-domestic**

It is proposed that the non-domestic areas, including community Centre and Flexible Workspace are serviced with VRF style heat pumps systems to provide heating and cooling supplies.

We note that the Flexible Workspace is likely to be handed over as shell and core space only, however for the purposes of the energy / carbon modelling carried out under this energy assessment, we have assumed VRF systems will be installed as this is a likely fit out strategy.

# **Supplementary renewable technologies**

The original planning application identified solar thermal collectors and photovoltaic (PV) panels as the most appropriate renewable technologies for the site. As the heat source for Block B is being changed the suitability of these technologies has been reviewed.

Incorporating solar thermal collectors into the proposed system would be difficult, a separate system would be required to provide the hot water from the solar thermal collectors to dwellings.

It is instead proposed that PV panels only are installed on the highest roofs, these have been maximised to all available roof area.





# **Figure 8 - Roof plant layout**

The photovoltaic (PV) array is shown in figure 8. The PV array generates 23,803 kWh/year of electricity towards the energy compliance calculations.



# <span id="page-20-0"></span>**6.0 WATER, OTHER RESOURCES AND SUSTAINABLE CONSTRUCTION**

The sustainability approach beyond energy and carbon dioxide remains unchanged from the original planning application.

# <span id="page-20-1"></span>**6.1 Water**

Domestic water consumption is designed to achieve 105 litres/person/day.

The landscaping strategy also includes the provision of SUDS to the Mayor's preferred standard through green roofs, permeable paving and rain gardens.

# <span id="page-20-2"></span>**6.2 Materials and Sustainable Construction**

Wherever possible preference will be given to environmentally low impact materials: cement replacements will be specified in order to reduce the impact of concrete elements; the insulation used will not contain substances known to contribute to ozone depletion or have the potential to contribute to global warming



# <span id="page-21-0"></span>**7.0 SUMMER COMFORT AND CLIMATE CHANGE ADAPTATION**

# **7.1 Original planning application requirements versus latest guidance**

<span id="page-21-1"></span>The UK government and Camden council have both introduced legislation to ensure new developments address the emerging issues of the climate emergency and climate change:

- 1. Reduce carbon emissions to limit the severity of climate change- **minimise energy use**.
- 2. **Ensure developments are resilient** to increased overheating risks from future climate scenarios.

The Camden Local Plan 2017 calls for following the London Plan Cooling Hierarchy which aims to reduce overheating risk whilst also reducing reliance on air conditioning systems.

As described in the original application, the design team has been aware from an early stage of the need to mitigate the risk of overheating; and to create thermally comfortable spaces that will continue to operate successfully in future climates. It is a requirement for Passivhaus certification that the risk of overheating is mitigated. Passivhaus defines this risk as the percentage of time where the internal temperature exceeds 25°C. This should not exceed 10% for the year, however, considering future climate scenarios this should ideally be below 5%.

To reduce energy demand from cooling, the design follows the London Plan Cooling Hierarchy by adopting a passive design - opening windows for natural ventilation. However, there is a greater risk of overheating, both with the current and predicted future climate with a natural ventilation strategy. An overheating analysis was completed with the aims of showing compliance with legislation whilst also driving the design.

# **Methodology**

The design standards for residential summer comfort have advanced since the original application. In line with the draft New London Plan, CIBSE's TM59 was used as the framework to assess overheating risk and to guide design to militate against this in the homes and TM52 was the approach used in the commercial spaces. TM59 has two criteria to pass – daytime comfort for all rooms, and night-time comfort for bedrooms. Various flats were reviewed including flats with higher solar gains due to being south facing and/or limited shading, single aspect glazing which doesn't allow cross flow and ground floor apartments where security issues mean limited opening of windows.

#### **Conclusion**

Following the London Plan Energy Hierarchy 'Be Lean, be clean, be green', the first option should 'be lean' adopting more passive design measures which will bring down energy demand. Measures that could be adopted now include adding blinds/shades/louvres to limit solar gains and the removal of fixed low-level glazing which adds to solar gains but does not aid natural ventilation. Retrofit options in the future include providing solar control film, fitting more external shading/louvres and adding ceiling fans.

Overheating modelling results can be found in Appendix 1, Overheating Risk Assesment.

The domestic apartments passed TM59 (except for one top floor living room which would require external shading to pass) with natural ventilation only.

Window opening areas have been optimised for overheating mitigation, however the non-domestic on ground floor and first floor do not pass TM52 with natural ventilation only. This is due to the solar irradiance and occupancy gains which are significant. These spaces will require active cooling during the warmest parts of the year. The aspiration is that natural ventilation will be used for as much of the year as possible and cooling only used as a last resort.

As also required by the Energy Assessment guidance, the overheating assessment has also tested the development against future weather scenario datasets. Results for these weather scenarios are also included in the report in Appendix 1.



# **7.2 London Plan cooling hierarchy**

<span id="page-22-0"></span>The most up to date London Plan cooling hierarchy is shown below in bold with the project response in blue.

# **1. Reduce the amount of heat entering the building through orientation, shading, high albedo materials, fenestration, insulation and the provision of green infrastructure**

Compared to the original planning application, the amount of glazing has been significantly reduced whilst balancing competing demmands for good internal daylight levels. Low G-value glass has beeen specified to reduce internal solar gain. Deep window reveals have been incorportated to help shade agains high angle summer sun. Where possible balconies have been are used to shade windows on the levels below.

# **2. Minimise internal heat generation through energy efficient design**

Proposed decentralised energy strategy means that there is no heating network pipes running through communal areas, reducing the the risk of these areas overheating. Hot water pipework within flats to be as short as possible in line with Passivahus guidance.

#### **3. Manage the heat within the building through exposed internal thermal mass and high ceilings**.

Floor to floor heights in resi areas optimised to reduce embodied carbon emissions,

There is a double height space in community centre area which will mitigate against overheating.

# **4. Provide passive ventilation`**

Dual aspect flats provided wherever possible. All dwellings capable of being cooled passively via opening windows in line with new Part O guidance p- see separate Overheating risk assessmen in the aappendices. Large openings also provided for non donestic areas to allow natural ventialtion, double height space in communit centre used for stack effect.

# **5. Provide mechanical ventilation**

All dwellings and commercial areas to be provided with high efficiency Passivhaus certified MVHR units with controls capable of using 'free cooling' when the outside air temperature is below internal, they will also have a bypass for summer operation

# **5. Provide acticve cooling**

As descibed in sectio[n 0,](#page-17-2) the EXAHP units is capable of running in reverse in summer to provide a small amount of cooling allowing the unit to temper the incoming supply air by up to around to 10 °C however it **does not function as an air conditioning system**. When 'cooling' mode is activated, the supply air is dehumidified; this helps provide a more pleasant indoor climate than is possible with standard MVHR system. Heat energy extracted from the air is recovered where possible and used to produce hot water, offsetting associated energy demand .



# <span id="page-23-0"></span>**APPENDIX 1 – OVERHEATING RISK ASSESSMENT**

# <span id="page-23-1"></span>**1.0INTRODUCTION**

This report describes the overheating assessment of the Planning Application for the Regeneration of the Agar Grove Estate.



#### **Description of Proposal**

The construction of this development is phased to ensure existing residents only move once. The phasing has allowed the design for Phase 2a to be revisited.

This report is included as an overheating assessment as part of the planning amendment for Block B. Block B includes 2No. residential towers with 94No. dwellings, with a Community Centre and Flexible Workspace and Landlord's ancillary areas at Ground and first floor levels.

In recent years, with increased awareness of the warming climate and the 'urban heat island' effect, consideration of the overheating of buildings has justifiably drawn greater focus.

New overheating standards have consequently been introduced and adopted as planning requirements in many areas. In this report, we will first look at the planning requirements for the Agar Grove Estate; before describing the overheating risk, analysis carried out, presenting the results against the requisite standard and discussing the implications of this for building occupants.

The results of the overheating assessment shows that all spaces could fulfil the criteria for mitigation of overheating in accordance with CIBSE TM49 / TM59 criteria, using weather data DSY1 (Design Summer Year) for the 2020s, high emissions, 50% percentile scenario.

Overheating analysis for more extreme weather data sets are also included, as per the requirements of the current and London Plan guidance, see Section 1.1. There is no requirement, under the 2021 London Plan guidance, for the spaces to comply with the overheating criteria using these more extreme weather files, nonetheless the results have been provided within the report.

# <span id="page-23-2"></span>**1.1 London Plan**

In accordance with policy SI 4 of the London Plan, new developments must show that they follow the cooling hierarchy to reduce potential overheating and reduce reliance on air conditioning systems.



# **Policy SI 4 Managing heat risk**

- Development proposals should minimise adverse impacts on the urban heat  $\overline{A}$ island through design, layout, orientation, materials and the incorporation of green infrastructure.
- Major development proposals should demonstrate through an energy <sub>B</sub> strategy how they will reduce the potential for internal overheating and reliance on air conditioning systems in accordance with the following cooling hierarchy:
	- 1) reduce the amount of heat entering a building through orientation, shading, high albedo materials, fenestration, insulation and the provision of green infrastructure
	- 2) minimise internal heat generation through energy efficient design
	- 3) manage the heat within the building through exposed internal thermal mass and high ceilings
	- 4) provide passive ventilation
	- 5) provide mechanical ventilation
	- 6) provide active cooling systems.

The London Plan energy assessment guidance requires analyses of the risk of overheating to be undertaken, and compliance must be demonstrated with the following standards:

- Building Regulations Part L, Criterion 3 relating to solar gain. For all new buildings
- CIBSE TM59, using TM49 weather files, for new domestic buildings
- CIBSE TM52, using TM49 weather files, for new non-domestic buildings

# <span id="page-24-0"></span>**1.2 CIBSE Technical Memorandum 52**

CIBSE TM52 describes an 'adaptive' model of human comfort. Adaptive comfort models have been developed based on scientific research into human adaptation to temperature variation. Instead of fixed or absolute limits on temperature, the comfort parameters vary according to the prevailing weather conditions – so, for example, the maximum adaptive temperature will be higher during a period of hot weather.

The overheating risk criteria in TM52 are based on a 'maximum adaptive temperature', Tmax, a function of the running mean of the external air temperature. ΔT is then defined as the difference between the internal operative temperature, Top, and Tmax (ΔT=Top-Tmax). The operative temperature is simply a measure of internal temperature that considers radiant temperature as well as air temperature.

ΔT is calculated on an hourly basis and rounded to the nearest whole number. It is used to define three criteria, with a building failing to meet two out of three deemed at risk of overheating:

# - **Criterion 1 - Hours of Exceedance:**

The percentage of occupied hours for which ΔT > 1 must be less than 3%.

I.e. the operative temperature can only exceed the maximum adaptive temperature by more than 1°C for a maximum of 3% of occupied hours.

#### - **Criterion 2 - Weighted Exceedance:**

The sum of ΔT for each hour the building exceeds T<sub>max</sub> must not exceed 6 in any one day.



So, for example, a building which exceeds  $T_{\text{max}}$  by 1°C for two hours and by 2°C for one hour in a day would meet the criterion (weighted exceedance = 4); while a building exceeding  $T_{max}$  by 1°C for three hours and by 2°C for two hours would not meet the criterion (weighted exceedance = 7).

# - **Criterion 3 - Threshold/Upper Limit Temperature:**

ΔT must never exceed 4°C.

That is, the operative temperature can never exceed the maximum adaptive temperature by 4.5°C or more.

These criteria apply to all occupied rooms in a non-domestic building.

# <span id="page-25-0"></span>**1.3 CIBSE Technical Memorandum 59**

CIBSE TM59 builds on the work undertaken in TM52 and adapts it to specifically address the issue of overheating in dwellings.

CIBSE TM59 requires all dwellings to meet the following criteria:

# - **Criterion 1 - for living rooms, kitchens and bedrooms:**

The percentage of occupied hours for which ΔT > 1 must be less than 3%.

I.e. the operative temperature can only exceed the maximum adaptive temperature by more than 1°C for a maximum of 3% of occupied hours.

# **I.e. Top - Tmax < 1°C, for 97% of occupied hours.**

#### - **Criterion 2 - for bedrooms only:**

To guarantee comfort during the sleeping hours (from 10pm to 7am) the operative temperature in bedrooms shall not exceed 26°C for more than 1% of annual hours (corresponding to 32 hours).

# **I.e. Top<26°C for 99% of hours between 22:00 and 07:00**

TM59 defines profiles for internal gains for different residential space types, allowing different buildings' performance to be compared fairly.

# <span id="page-25-1"></span>**1.4 Weather Data**

Alongside the development of improved overheating standards, weather data that are more representative of the current climate and the projected future climate have also been developed. CIBSE have now produced a huge range of weather data sets, covering a variety of weather and climate scenarios up to the year 2100.

Three new probabilistically generated 'Design Summer Years' (DSY) were released in 2016 specifically for the assessment of overheating:

- DSY1 representing an above average, warm summer (approximate return period for London weather files: 7 years)
- DSY2 containing a short but extreme period of heat (approximate return period for London weather files: 16 years)
- DSY3 a longer period of intense, but less extreme, heat (approximate return period for London weather files: 24 years)

Each of these DSY have been projected forward using probabilistic climate models to give future weather data sets covering the periods 2011-2040 (DSY#2020s); 2041-2070 (DSY#2050s); and 2071-2100 (DSY#2080s). Each



of these is then available for a 'high', 'medium' and 'low' emissions scenario; and each of these as a 10th, 50th and 90th percentile - i.e. respectively that with a 90%, 50% or 10% chance of being exceeded.

DSY following this methodology have been produced for 14 locations across the UK. To capture the effects of the Urban Heat Island, DSY are available for three separate sites in London, each applicable to developments in a different zone of the city:

- London Weather Centre used for development in the high-density urban areas of the 'central activity zone'
- London Heathrow used in the lower density urban and suburban areas
- London Gatwick for the low-density peri-urban and rural areas around the city

The Agar Grove Estate site sits within the lower density urban area of London, and as such, in line with the GLA guidance on preparation of energy statements, the weather data for London Heathrow will be used.

As can be seen from the expected return periods of the Design Summer Years, they all represent unusual weather occurrences. However, DSY1 represents what might be called a more frequently experienced 'hot' summer, while DSY2 and DSY3 do represent much less frequent 'extreme' weather events.

This is acknowledged in the London Plan 2021, which requires only compliance against the 2020s DSY1 weather file, in the high emissions scenario at the 50th percentile: i.e. DSY1\_2020\_High\_50. While accepting that it is extremely difficult to achieve a pass, the London Plan also asks that buildings be tested against the more extreme 2020s weather years – DSY2 and DSY3 – and the DSY1 projected forward to the 2050s and 2080s. However, it should be noted that there is no requirement to meet the TM52 or TM59 criteria for these weather years, but the results will be reported, and potential future mitigation measures discussed where necessary.





# <span id="page-27-0"></span>**2.0 METHODOLOGY**

# <span id="page-27-1"></span>**2.1 Dynamic Thermal Simulation**

The IES 2021 software package has been used to model the building. This software dynamically simulates the performance of a building over time, using hourly weather data to calculate internal conditions based on the user inputs: the 3D geometry and the thermal parameters of each building element.

# <span id="page-27-2"></span>**2.2 TM52: Community Hall, Community Rooms and Flexible Storage**

Figures 1-3 shows the IES model from all elevations. The geometry and fenestration have been based on the Architectural information issued on the 11<sup>th</sup> May 2022. All spaces have been modelled in detail with associated gains and thermal properties – refer to section **Error! Reference source not found.** for further details.



**Figure 1: IES Model showing the south elevation of the non-domestic spaces**



**Figure 2: IES Model showing the north elevation of the non-domestic spaces**





**Figure 3: IES Model showing the west elevation (left) and the east elevation (right) of the non-domestic spaces**

However, the overheating risk assessed by TM52 only applies to permanently occupied spaces – i.e. those with continuous occupation during the operational day. The rooms considered here are highlighted in the architectural plan extract below and labelled with the reference used in this document.



**Figure 4: Internal layout of the ground floor of Block B**



**Figure 5: Internal layout of the first floor of Block B**



# <span id="page-29-0"></span>**2.3 TM59: Dwellings Model**

For residential developments containing multiple dwellings TM59 requires that a sample of the 'worst case' dwellings are analysed. In this case a selection of 16No. dwellings has been made, representing a sample of the dwelling types in the building most at risk of overheating. These are generally located on the upper floors – where shading from balconies and adjacent buildings is at a minimum – and includes those dwellings with glazed facades orientated to the west or south where the highest solar gains will occur. The flats selected and the reason for their selection is summarised in the following table.







Figures 4-5 below shows the 16 selected flats in the context of the overall building. The internal layouts of these flats can be seen in Figures 6-8.



**Figure 4: South Elevation of IES Model of Block B with modelled flats shown in blue**

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**Figure 5: North Elevation of IES Model of Block B with modelled flats shown in blue**



**Figure 6: Internal layouts of Floor G Block B flats**





**Figure 7: Internal layouts of Floor 8 Block B2 Flats**



**Figure 8: Internal Layouts of Upper Floor Block B2 Flats**

#### **Communal Corridors**

TM59 recommends that where heating pipework is present in communal corridors and there is a risk of overheating, these should be modelled. There is window openings and no hot water pipework in the corridors, so it is not considered that the corridors are at particular risk of overheating.





# <span id="page-34-0"></span>**2.4 Cooling/Ventilation Strategy**

Window recesses (200mm) have been implemented across all the glazing to shade the windows from high angle summer sun providing a passive design solution to limit solar gain.

Window opening profiles, detailed in the approved Part O document, shown below have been incorporated into the TM59 model.

2.6 All of the following limits on CIBSE's TM59, section 3.3, apply.

- a. When a room is occupied during the day (8am to 11pm), openings should be modelled to do all of the following.
	- i. Start to open when the internal temperature exceeds 22°C.
	- ii. Be fully open when the internal temperature exceeds 26°C.
	- iii. Start to close when the internal temperature falls below 26°C.
	- iv. Be fully closed when the internal temperature falls below 22°C.

b. At night (11pm to 8am), openings should be modelled as fully open if both of the following apply.

- i. The opening is on the first floor or above and not easily accessible.
- ii. The internal temperature exceeds 23°C at 11pm.
- c. When a ground floor or easily accessible room is unoccupied, both of the following apply.
	- i. In the day, windows, patio doors and balcony doors should be modelled as open, if this can be done securely, following the guidance in paragraph 3.7 below.
	- ii. At night, windows, patio doors and balcony doors should be modelled as closed.

It is assumed that as all the dwellings are on the  $2^{nd}$  to the  $17<sup>th</sup>$  floor the windows can be modelled as fully open at night from 11pm to 8am when the internal temperature exceeds 23°C. The use of unrestricted windows through the night is key to the mitigation of overheating risk and it must be ensured that this is possible from the perspective of safety and security of occupants.

All flats are to be provided with MVHR units to optimise the energy efficiency of winter ventilation. These will operate in summer-bypass mode when conditions are appropriate. The effect of increased mechanical ventilation rates are also considered.

All flats are assessed without the need for mechanical cooling in line with the London Plan Cooling Hierarchy.



# <span id="page-35-0"></span>**2.5 Input Parameters**












## **3.0 RESULTS**

The report confirms that the residential apartments and the non-residential elements could comply with the London Plan Policy SI 4, for the required weather year - DSY1 (Design Summer Year) for the 2020s, high emissions, 50% percentile scenario).

As also required by the Energy Assessment guidance, the overheating assessment has also tested the development against future weather scenario datasets. Results for these weather scenarios are also included in the report.

### **3.1 DSY1 2020s High 50**

#### **TM52: Non-domestic**

The results of the TM52 overheating risk assessment using the GLA mandatory weather file, DSY1 2020s High 50, for the non-domestic spaces are shown in the table below. The numbers below each criterion indicate the value corresponding to that criterion – so criterion 1 indicates the percentage of hours where ΔT exceeds 1K (max. 3%); criterion 2 the peak weighted exceedance (max. 6), and criterion 3 the peak value of ΔT (max. 4K). Any criteria being failed are then indicated, and the overall pass/fail result (if two or more criteria are failed).

The model was initially run with the windows being allowed to open during the day as per the conditions described in Section 2.5 and during the night the windows were modelled as fully closed. The g value implemented in the model was 0.4. The results of these conditions are shown in the table below:



As shown from the results, all spaces fail the TM52 overheating analysis. This is due to several factors including the significant amount of solar gain due to the high proportion of glazing. Another reason is the high occupancy, and resulting high internal gains, in some of the spaces including the flexible workspaces, meeting rooms and community halls.

The window opening strategy is shown in Figures 9-11 below. A red box with the letter F indicates a fixed pane of glazing, a blue box with the letter O indicates an openable window which is closed at night for security reasons and an orange box with the letters SD indicates a security door which is closed all the time.

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**Figure 9: North elevation and window opening strategy indicated by the coloured boxes**



**Figure 10: South elevation and window opening strategy indicated by the coloured boxes**



**Figure 11: East elevation (left) and west elevation (right) and window opening strategy indicated by the coloured boxes**

The high proportion of fixed glazing shown in the figures above has a significant effect on the overheating.

To improve the performance of these spaces it is recommended that the solar gain be reduced and night ventilation introduced. Solar gain could be reduced via increased shading, reduced glazing area or reduced glazing g value – here we have looked only at glazing g value, however it may be possible to achieve the same performance using an alternative method. Night ventilation allows a building to purge heat built up during the day when there is typically cooler outside air available. It can be extremely effective at reducing daytime temperatures; however, it is dependent on the provision of secure openings and management /control of these to ensure they are opened at appropriate times.

To determine whether the spaces will pass with night-time natural ventilation the windows were allowed to open with a 100mm restriction at night. At night the windows were modelled to open when the external temperature exceeds 18°C and when the internal temperature is greater than the external temperature. Furthermore, half of the area of the ground floor windows were also allowed to open with a 100mm restriction at night and the g-value for all glazing was reduced to 0.3. The results of this are shown in the table below.







Despite these measures, the results show that most spaces still fail and therefore it is evident that the high occupancy in combination with the current facade design will impose an overheating risk. Therefore, it is likely that the commercial spaces will require some element of mechanical cooling to achieve comfortable internal summertime conditions. The input data provided above should be reviewed to ensure this is a realistic representation of how the spaces will be used. Even if a mechanically cooled solution is pursued, effort should still be concentrated on passive design measures and optimisation of the façade to minimise the cooling energy required.



#### **TM59: Residential**

The report presents cases where the residential apartments comply with the London Plan Policy SI 4, for the required weather year - DSY1 (Design Summer Year) for the 2020s, high emissions, 50% percentile scenario).

#### **Option 1:**

For Option 1, the windows are unrestricted during the day and at night as per the conditions highlighted in 'Windows and Natural Ventilation Opening' in Input Parameters above. As we can see from the results below, all of the rooms, except one living room pass the TM59 overheating analysis.







As shown above, there is one space failing: B\_06\_XX\_B1\_F4\_3B5P\_Living Room. This is likely due to its north-west position which gets high solar gains in the afternoon. A solution to this would be to introduce some external shading to reduce the effect of the solar gain.

### **Option 2:**

For Option 2, the windows are unrestricted during the day, however, during the night they are now modelled as closed. As shown below, having no night-time ventilation has a significant effect on the results and the analysed rooms are now failing the TM59 overheating analysis. This highlights the importance of having nighttime ventilation to pass TM59, so it is critical to ensure that openings are designed to facilitate this safely and securely.











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### **3.2 Extreme and Future Weather Files**

This section presents results from the overheating assessments for the extreme weather years tested – DSY2 and DSY3 for the 2020s high emission scenario at the 50<sup>th</sup> percentile. These years represent weather events with a return period of 16 and 24 years respectively. DSY2 contains a short but extremely intense period of heat, while DSY3 contains a slightly less intense, but much longer hot spell.

London Plan Policy SI 4 does not require the designs to comply with these extreme weather datasets.

#### **Commercial Spaces**

#### **DSY2 2020s High 50**



#### **DSY3 2020s High 50**



**DSY1 2050s High 50**







#### **DSY1 2080s High 50**



The commercial spaces fail to meet the TM52 criteria for both the DSY2 and DSY3 weather years. DSY2 comprises a short, very intense spell of heat – meaning the maximum adaptive temperature stays relatively low through it, which is manifested in the severe failures seen in the upper limit temperature criterion 3. DSY3 contains a slightly less intense, but much longer period of hot weather – again a feature manifested in the buildings failing to meet the hours of exceedance criterion 1.

Thus, different approaches may be required to ameliorate performance in each of these scenarios. For DSY2, it is thought that additional shading – either internal or external – and more active window control – for example closing them during very hot weather – could be effective mitigation measures. For DSY3 increased thermal mass would be beneficial, allowing the building to more effectively cool through the night during an extended hot spell and thus reduce the daily temperature peaks.

For the future weather scenarios, the commercial spaces again fail to meet the TM52 criteria – though for the 2050s scenario this is less severe (covering 2041-2070). The 2080s (covering 2071 – 2100), demonstrates a more dramatic failure for the teaching spaces. The performance in both these scenarios would be improved by the measures mentioned above – the addition of exposed thermal mass along with more shading and active window control – but also more flexible measures will have a positive effect – such as the use of local or ceiling mounted fans to produce a perceived cooling effect.



#### **Residential**

#### **Option 1 – Future and Extreme Files**

#### **DSY2 2020s High 50s**







#### **DSY3 2020s High 50s**







#### **DSY1 2050s High 50s**









#### **DSY1 2080s High 50**





As can be seen, the dwellings also perform less well during extreme weather events – the bedrooms fail to meet the night-time temperature limit of criterion 2. However, it should be noted that this is a non-adaptive criterion – instead it is an absolute temperature limit that will inevitably become more difficult to achieve as the weather becomes hotter. The kitchen and living areas fail the overheating analysis.

Many of the failures in DSY2 are quite marginal. This suggests that relatively straightforward measures could improve conditions for these relatively infrequent very hot days – for example the use of desk or ceiling fans, which can provide a perceived cooling effect of 2-3°C; or other shading devices across the building could be implemented.



#### **Further Information**

#### **TM52 Commercial Spaces Internal Gains:**









## **APPENDIX 2 – SAP MODELLING OUTPUT GLA CONVERSION SPREADSHEET**





**Contract** 

Table 2: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for domestic buildings **Table 2: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for domestic buildings** 











Table 4: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for non-domestic buildings Table 4: Regulated Carbon Dioxide savings from each stage of the Energy Hierarchy for non-domestic buildings





# **SAP 2012 Performance SAP 10.0 Performance**

# **Domestic**

Table 1: Carbon Dioxide Emissions after each stage of the Energy Hierarchy for domestic buildings **Table 1:** Carbon Dioxide Emissions after each stage of the Energy Hierarchy for domestic buildings



**Non-domestic** unless Local Planning Authority price is inputted in the 'Development Information' tab

Table 3: Carbon Dioxide Emissions after each stage of the Energy Hierarchy for non-domestic buildings **Table 3:** Carbon Dioxide Emissions after each stage of the Energy Hierarchy for non-domestic buildings

\*carbon price is based on GLA recommended price of £95 per tonne of carbon dioxide

\*carbon price is based on GLA recommended price of £95 per tonne of carbon dioxide unless Local Planning Authority price is inputted in the 'Development Information' tab

\*carbon price is based on GLA recommended price of £95 per tonne of carbon dioxide unless Local Planning Authority price is inputted in the 'Development Information' tab

unless Local Planning Authority price is inputted in the 'Development Information' tab







# **SITE-WIDE**











**Non-domestic SAP 10.0 Carbon Emissions**













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 $\mathsf{O}_2$ **(kgCO<sup>2</sup> p.a.) (kgCO<sup>2</sup> / m<sup>2</sup> )Calculated BER SAP 10.0**





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## **APPENDIX 3 – SAP ENERGY TYPE MARKUPS**



















