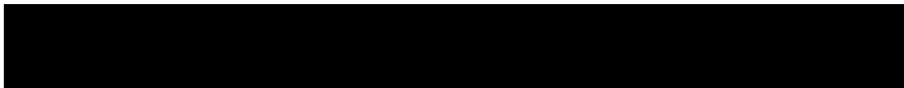


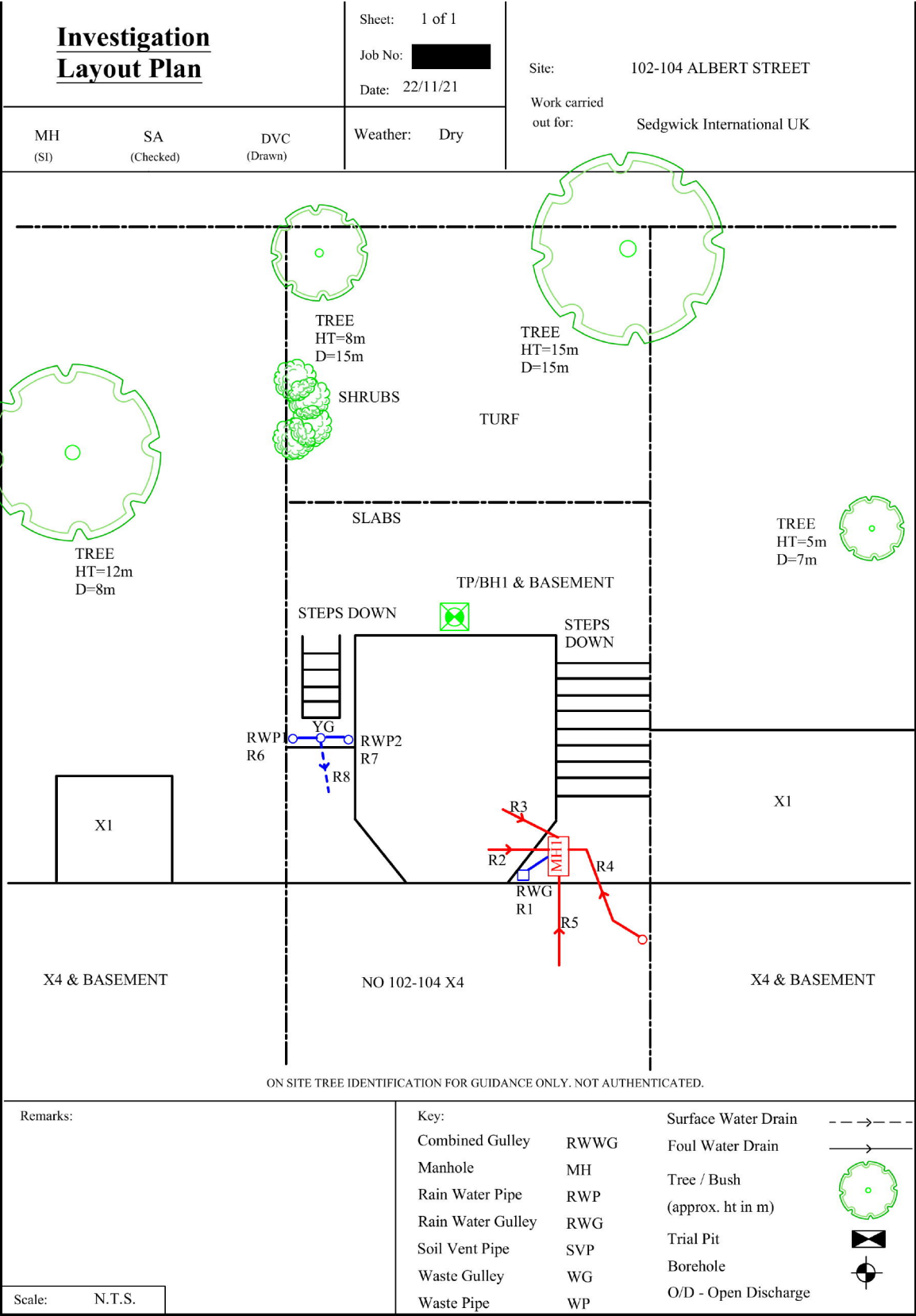
## SITE INVESTIGATION FACTUAL REPORT

Report No: [REDACTED]  
Client: Sedgwick International UK - Maidstone  
Site: 102-104, Albert Street  
Camden  
Client Ref: [REDACTED]  
Date of Visit: 22/11/2021



Home Emergency Response - Subsidence Investigation - Drainage Services – Crack & Level Monitoring – Property Video Surveys





TEST REPORT: Trial Pit

REPORT NUMBER: [REDACTED]

TRIAL PIT REF: TP1

CLIENT: Sedgwick International UK

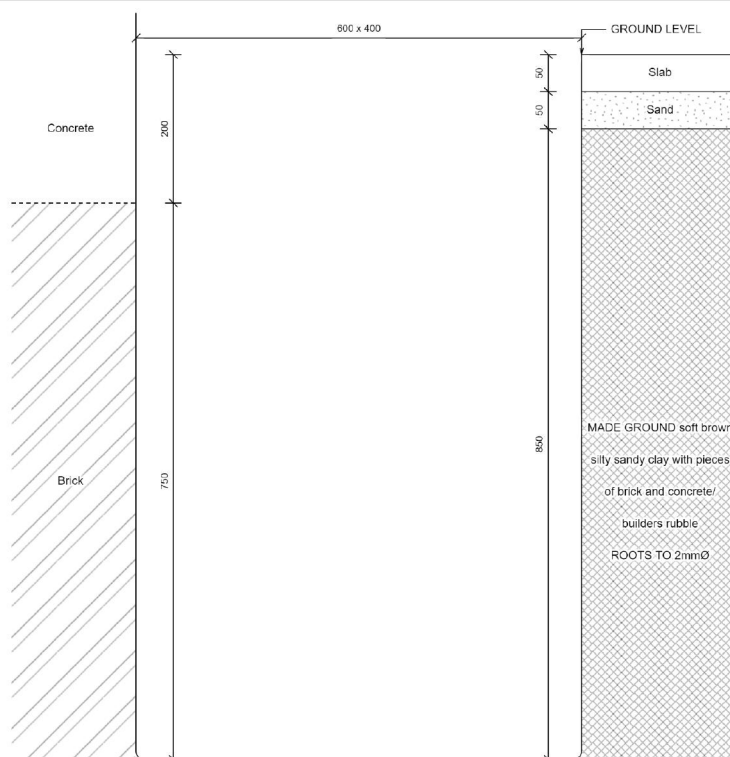
JOB NO: [REDACTED]

EXCAVATION METHOD: Hand tools

DATE: 22/11/2021

SITE: 102-104 ALBERT STREET

WEATHER: Dry



For Strata below 950mm see Bore Hole log

U/S not found No samples taken tp abandoned at 950mm due to collapsing made ground. BH done to rear of tp to avoid made ground.

Key:

D Small disturbed sample J Jar sample  
B Bulk disturbed sample V Pilcon vane (kPa)  
W Water sample M Mackintosh probe  
TDTD Too dense to drive

Remarks:

Test results reported relate only to the items tested.  
This report shall not be reproduced except in full without approval of the Laboratory.

For and on behalf of CTS

Adam Mason - Quality Control

Approved Signatory  
23-Nov-21

Construction Testing Solutions Ltd.  
Registered in England No. 05998333

Report version 1

Page 1 of 1

<b>Borehole</b>		<b>1</b>		Sheet: 1 of 1	Site: 102-104 ALBERT STREET
				Job No:	
				Date: 22/11/2021	
Boring Method: Hand Auger		Weather: dry		Ground Level:	Client: Sedgwick International UK
Diameter (mm): 75					
Depth	Soil Description			Thickness	Legend
(m)					
0.00	See Trial Pit			1.00	
1.00	Stiff brown-grey veined CLAY			1.50	
2.50	Very stiff brown-grey veined silty CLAY with claystone nodules			2.40	
5.00	End of BH				
Remarks: BH ends at 5.0m. BH dry and open on completion, No roots observed below 2.7m. Datum installed at 5.0m.				Key: D - Disturbed Sample B - Bulk Sample W - Water Sample      Roots J - Jar Sample      Roots V - Pilcon Shear Vane (kPa) Roots M - Mackintosh Probe      Depth to Water (m) TDTD - Too Dense To Drive	
To Max				Depth Dia	
				(m) (mm)	
				1.50 2	
				1.70 1	
Logged: IC AM Checked: Approved: Version V1.0 28/01/16				N.T.S.	



**Construction Testing  
Solutions**

## **SITE INVESTIGATION LABORATORY TEST REPORT**

**SI REPORT NUMBER:** [REDACTED]

**CLIENT :** CET Property Assurance (Sedgwick International UK)

**SITE:**  
102-104 Albert Street  
London  
NW1 7NE

**DATE OF SITE VISIT:**  
22/11/2021

**DATE RECEIVED BY LABORATORY:**  
23/11/2021

Compiled by [REDACTED]  
L. Kirby - Laboratory Technician (B)

Approved by [REDACTED]  
J. Garrett - Laboratory Manager (B)

**DATE REPORTED:** 30-Nov-2021

## Laboratory Summary Results

Our Ref: [REDACTED]

Location: 102-104 Albert Street, London, NW1 7NE  
 Client: CET Property Assurance (Sedwick International UK)  
 Address: [REDACTED]

Date Sampled: 22/11/2021

Date Received: 23/11/2021

Date Tested: 23/11/2021

Date of Report: 30/11/2021

TP/BH No	Sample Ref Depth (m)	Type	Moisture Content (%) [1]	Soil Fraction > 0.425mm (%) [2]	Liquid Limit (%) [3]	Plastic Limit (%) [4]	Plasticity Index (%) [5]	Liquidity Index [6]	Modified Plasticity Index (%) [10]	Soil * Class [7]	Filter Paper Contact Time (d)	Soil Sample Suction (kPa) [8]	Oedometer Strain [9]	Estimated * Heave Potential (Dd) (mm) [16]	In situ * Shear Vane Strength (kPa) [11]	Organic * Content (%) [12]	pH * Value [13]	Sulphate Content * (g/l)		* Class [16]
																		SO <sub>3</sub> [14]	SO <sub>4</sub> [15]	
BH1	1.0	D	34	<5	78	25	53	0.17	53	CV	7	74.7			76					
	1.5	D	32	<5	78	24	54	0.14	54	CV	7	224			87					
	2.0	D	27	<5											119					
	2.5	D	26	<5	79	24	55	0.04	55	CV	7	934			> 150					
	3.0	D	29	<5											> 150					
	3.5	D	31	<5	80	29	51	0.03	51	CV	7	573			> 150					
	4.0	D	29	<5											> 150					
	4.5	D	28	<5							7	628			> 150					
	5.0	D	28	<5							7	544			> 150					

### Test Methods / Notes

[1] BS 1377: Part 2: 1990, Test No 3.2

[2] Fatness of < 5%, otherwise measured

[3] BS 1377: Part 2: 1990, Test No 4.4

[4] BS 1377: Part 2: 1990, Test No 5.3

[5] BS 1377: Part 2: 1990, Test No 5.4

[6] BS 1377: Part 2: 1990, Test No 5.4

[7] BS 1377: Part 2: 1990, Test No 5.4

[8] BS 1377: Part 2: 1990, Test No 5.4

[9] BS 1377: Part 2: 1990, Test No 5.4

[10] BS 1377: Part 2: 1990, Test No 5.4

[11] BS 1377: Part 2: 1990, Test No 5.4

[12] BS 1377: Part 2: 1990, Test No 5.4

[13] BS 1377: Part 2: 1990, Test No 5.4

[14] BS 1377: Part 2: 1990, Test No 5.4

[15] BS 1377: Part 2: 1990, Test No 5.4

[16] BS 1377: Part 2: 1990, Test No 5.4

[17] BS 1377: Part 2: 1990, Test No 5.4

[18] BS 1377: Part 2: 1990, Test No 5.4

[19] BS 1377: Part 2: 1990, Test No 5.4

[20] BS 1377: Part 2: 1990, Test No 5.4

[21] BS 1377: Part 2: 1990, Test No 5.4

[22] BS 1377: Part 2: 1990, Test No 5.4

[23] BS 1377: Part 2: 1990, Test No 5.4

[24] BS 1377: Part 2: 1990, Test No 5.4

[25] BS 1377: Part 2: 1990, Test No 5.4

[26] BS 1377: Part 2: 1990, Test No 5.4

[27] BS 1377: Part 2: 1990, Test No 5.4

[28] BS 1377: Part 2: 1990, Test No 5.4

[29] BS 1377: Part 2: 1990, Test No 5.4

[30] BS 1377: Part 2: 1990, Test No 5.4

[31] BS 1377: Part 2: 1990, Test No 5.4

[32] BS 1377: Part 2: 1990, Test No 5.4

[33] BS 1377: Part 2: 1990, Test No 5.4

[34] BS 1377: Part 2: 1990, Test No 5.4

[35] BS 1377: Part 2: 1990, Test No 5.4

[36] BS 1377: Part 2: 1990, Test No 5.4

[37] BS 1377: Part 2: 1990, Test No 5.4

[38] BS 1377: Part 2: 1990, Test No 5.4

[39] BS 1377: Part 2: 1990, Test No 5.4

[40] BS 1377: Part 2: 1990, Test No 5.4

[41] BS 1377: Part 2: 1990, Test No 5.4

[42] BS 1377: Part 2: 1990, Test No 5.4

[43] BS 1377: Part 2: 1990, Test No 5.4

[44] BS 1377: Part 2: 1990, Test No 5.4

[45] BS 1377: Part 2: 1990, Test No 5.4

[46] BS 1377: Part 2: 1990, Test No 5.4

[47] BS 1377: Part 2: 1990, Test No 5.4

[48] BS 1377: Part 2: 1990, Test No 5.4

[49] BS 1377: Part 2: 1990, Test No 5.4

[50] BS 1377: Part 2: 1990, Test No 5.4

[51] BS 1377: Part 2: 1990, Test No 5.4

[52] BS 1377: Part 2: 1990, Test No 5.4

[53] BS 1377: Part 2: 1990, Test No 5.4

[54] BS 1377: Part 2: 1990, Test No 5.4

[55] BS 1377: Part 2: 1990, Test No 5.4

[56] BS 1377: Part 2: 1990, Test No 5.4

[57] BS 1377: Part 2: 1990, Test No 5.4

[58] BS 1377: Part 2: 1990, Test No 5.4

[59] BS 1377: Part 2: 1990, Test No 5.4

[60] BS 1377: Part 2: 1990, Test No 5.4

[61] BS 1377: Part 2: 1990, Test No 5.4

[62] BS 1377: Part 2: 1990, Test No 5.4

[63] BS 1377: Part 2: 1990, Test No 5.4

[64] BS 1377: Part 2: 1990, Test No 5.4

[65] BS 1377: Part 2: 1990, Test No 5.4

[66] BS 1377: Part 2: 1990, Test No 5.4

[67] BS 1377: Part 2: 1990, Test No 5.4

[68] BS 1377: Part 2: 1990, Test No 5.4

[69] BS 1377: Part 2: 1990, Test No 5.4

[70] BS 1377: Part 2: 1990, Test No 5.4

[71] BS 1377: Part 2: 1990, Test No 5.4

[72] BS 1377: Part 2: 1990, Test No 5.4

[73] BS 1377: Part 2: 1990, Test No 5.4

[74] BS 1377: Part 2: 1990, Test No 5.4

[75] BS 1377: Part 2: 1990, Test No 5.4

[76] BS 1377: Part 2: 1990, Test No 5.4

[77] BS 1377: Part 2: 1990, Test No 5.4

[78] BS 1377: Part 2: 1990, Test No 5.4

[79] BS 1377: Part 2: 1990, Test No 5.4

[80] BS 1377: Part 2: 1990, Test No 5.4

[81] BS 1377: Part 2: 1990, Test No 5.4

[82] BS 1377: Part 2: 1990, Test No 5.4

[83] BS 1377: Part 2: 1990, Test No 5.4

[84] BS 1377: Part 2: 1990, Test No 5.4

[85] BS 1377: Part 2: 1990, Test No 5.4

[86] BS 1377: Part 2: 1990, Test No 5.4

[87] BS 1377: Part 2: 1990, Test No 5.4

[88] BS 1377: Part 2: 1990, Test No 5.4

[89] BS 1377: Part 2: 1990, Test No 5.4

[90] BS 1377: Part 2: 1990, Test No 5.4

[91] BS 1377: Part 2: 1990, Test No 5.4

[92] BS 1377: Part 2: 1990, Test No 5.4

[93] BS 1377: Part 2: 1990, Test No 5.4

[94] BS 1377: Part 2: 1990, Test No 5.4

[95] BS 1377: Part 2: 1990, Test No 5.4

[96] BS 1377: Part 2: 1990, Test No 5.4

[97] BS 1377: Part 2: 1990, Test No 5.4

[98] BS 1377: Part 2: 1990, Test No 5.4

[99] BS 1377: Part 2: 1990, Test No 5.4

[100] BS 1377: Part 2: 1990, Test No 5.4

[101] BS 1377: Part 2: 1990, Test No 5.4

[102] BS 1377: Part 2: 1990, Test No 5.4

[103] BS 1377: Part 2: 1990, Test No 5.4

[104] BS 1377: Part 2: 1990, Test No 5.4

[105] BS 1377: Part 2: 1990, Test No 5.4

[106] BS 1377: Part 2: 1990, Test No 5.4

[107] BS 1377: Part 2: 1990, Test No 5.4

[108] BS 1377: Part 2: 1990, Test No 5.4

[109] BS 1377: Part 2: 1990, Test No 5.4

[110] BS 1377: Part 2: 1990, Test No 5.4

[111] BS 1377: Part 2: 1990, Test No 5.4

[112] BS 1377: Part 2: 1990, Test No 5.4

[113] BS 1377: Part 2: 1990, Test No 5.4

[114] BS 1377: Part 2: 1990, Test No 5.4

[115] BS 1377: Part 2: 1990, Test No 5.4

[116] BS 1377: Part 2: 1990, Test No 5.4

[117] BS 1377: Part 2: 1990, Test No 5.4

[118] BS 1377: Part 2: 1990, Test No 5.4

[119] BS 1377: Part 2: 1990, Test No 5.4

[120] BS 1377: Part 2: 1990, Test No 5.4

[121] BS 1377: Part 2: 1990, Test No 5.4

[122] BS 1377: Part 2: 1990, Test No 5.4

[123] BS 1377: Part 2: 1990, Test No 5.4

[124] BS 1377: Part 2: 1990, Test No 5.4

[125] BS 1377: Part 2: 1990, Test No 5.4

[126] BS 1377: Part 2: 1990, Test No 5.4

[127] BS 1377: Part 2: 1990, Test No 5.4

[128] BS 1377: Part 2: 1990, Test No 5.4

[129] BS 1377: Part 2: 1990, Test No 5.4

[130] BS 1377: Part 2: 1990, Test No 5.4

[131] BS 1377: Part 2: 1990, Test No 5.4

[132] BS 1377: Part 2: 1990, Test No 5.4

[133] BS 1377: Part 2: 1990, Test No 5.4

[134] BS 1377: Part 2: 1990, Test No 5.4

[135] BS 1377: Part 2: 1990, Test No 5.4

[136] BS 1377: Part 2: 1990, Test No 5.4

[137] BS 1377: Part 2: 1990, Test No 5.4

[138] BS 1377: Part 2: 1990, Test No 5.4

[139] BS 1377: Part 2: 1990, Test No 5.4

[140] BS 1377: Part 2: 1990, Test No 5.4

[141] BS 1377: Part 2: 1990, Test No 5.4

[142] BS 1377: Part 2: 1990, Test No 5.4

[143] BS 1377: Part 2: 1990, Test No 5.4

[144] BS 1377: Part 2: 1990, Test No 5.4

[145] BS 1377: Part 2: 1990, Test No 5.4

[146] BS 1377: Part 2: 1990, Test No 5.4

[147] BS 1377: Part 2: 1990, Test No 5.4

[148] BS 1377: Part 2: 1990, Test No 5.4

[149] BS 1377: Part 2: 1990, Test No 5.4

[150] BS 1377: Part 2: 1990, Test No 5.4

[151] BS 1377: Part 2: 1990, Test No 5.4

[152] BS 1377: Part 2: 1990, Test No 5.4

[153] BS 1377: Part 2: 1990, Test No 5.4

[154] BS 1377: Part 2: 1990, Test No 5.4

[155] BS 1377: Part 2: 1990, Test No 5.4

[156] BS 1377: Part 2: 1990, Test No 5.4

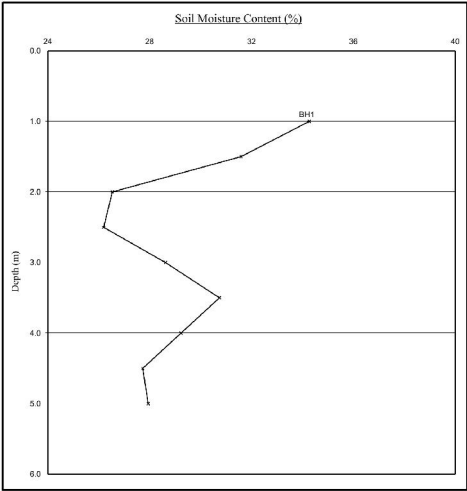
[157] BS 1377: Part 2: 1990, Test No 5.4

[158] BS 1377: Part 2: 1990, Test No 5.4

[159] BS 1377: Part 2:

Moisture Content Profiles

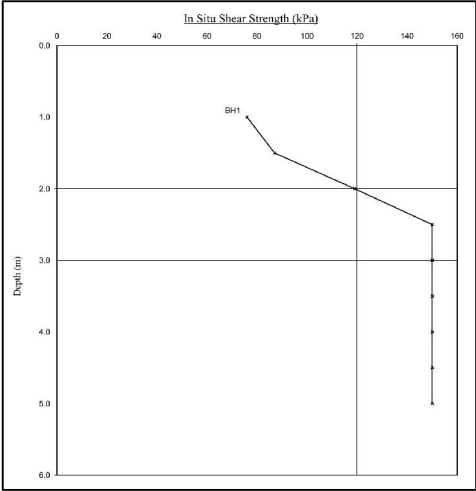
Our Ref: [redacted]  
Location: 102-104 Albert Street, London, NW1 7NE  
Work carried out for: CET Property Assurance (Sedgwick International UK)



Notes:  
1. If plotted, 0.4 LL and PL-2 (after Driscoll, 1983) should only be applied to London Clay (and similarly overconsolidated clay) at shallow depths.  
2. Unless specifically noted the profiles have not been related to a site datum.

Shear Strength Profiles

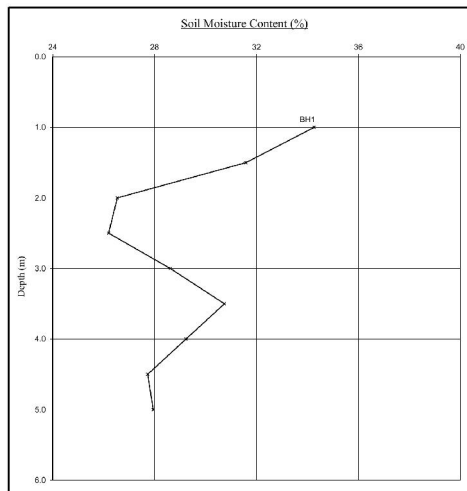
Date Sampled: 22/11/2021  
Date Received: 23/11/2021  
Date Tested: 23/11/2021  
Date of Report: 30/11/2021



Note:  
1. Unless otherwise stated, values of Shear Strength were determined in situ by CTS using a Pileon Hand Vane the calibration of which is limited to a maximum reading of 150 kPa.  
2. Unless specifically noted the profiles have not been related to a site datum.

## Moisture Content Profiles

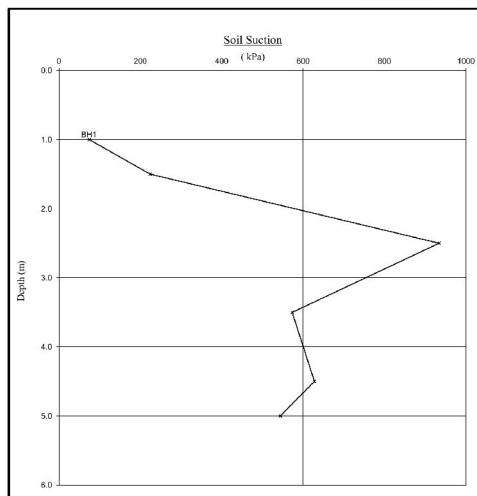
Our Ref: [REDACTED]  
Location: 102-104 Albert Street, London, NW1 7NE  
Work carried out for: CET Property Assurance (Sedgwick International UK)



Notes:  
1. If plotted, 0.4 LL and PL-2 (after Driscoll, 1983) should only be applied to London Clay (and similarly overconsolidated clay) at shallow depths.  
2. Unless specifically noted the profiles have not been related to a site datum.

## Soil Suction Profiles

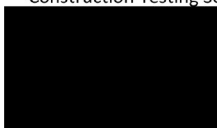
Date Sampled: 22/11/2021  
Date Received: 23/11/2021  
Date Tested: 23/11/2021  
Date of Report: 30/11/2021



Note:  
When shown, the theoretical equilibrium suction profiles are based on conventional assumptions associated with London Clay (and similarly overconsolidated clays) at shallow depths. Note that the sample disturbance component is dependent on the method of sampling and any subsequent recompaction. The above plots show this to be 100kPa which is the value suggested by the BEEF on the back of their limited number of tests on recompacted samples. This may or may not be appropriate in this instance and judgement should be exercised.



Construction Testing Solutions



Intec



## ROOT IDENTIFICATION

102-104 Albert Street

Client Reference: [Redacted]  
Report Date: 24 November 2021  
Our Ref: R43948

Sub Sample	Species Identified		Root Diameter	Starch
<b>BH1:</b>				
to 2.7m	<i>Fraxinus</i> spp.	1	2 mm	Moderate
to 2.7m	<i>Acer</i> spp.	2	2 mm	Moderate

**Comments:**

- 1 - Plus 1 other also identified as *Fraxinus* spp.
- 2 - Plus 2 decayed roots, probably the same.

*Fraxinus* spp. include common ash.

*Acer* spp. are maples, including sycamore, Norway maple, and Japanese maples.

**Signed:** R J Shaw

Unless we are otherwise instructed in writing, the above sample material will normally be disposed of 6 years after the date of this report.

<b>Coding Sheet</b>		Sheet:		Site:	102-104 ALBERT STREET		
		Job No.:					
		Date:	22/11/2021	Client:	SEDGWICK INTERNATIONAL UK		

<b>Run:</b>	<b>1</b>							
From:	MH1	Invert Level:		Direction:	U/S			
To:	rwg1	Invert Level:	400	Function:	S/W			
Pipe Material:	Cast Iron	Pipe Dia:	100					
Water/Pressure Test:		Drain Break-In:	No	Gully Condition:	As Built			
Distance (m)	Code	Clock Ref at to	Dia mm	Intrusion % mm	Shared Run:	Yes		
					If Shared How:	With flats		
0.00	ST				Remarks	Surface Material	Length (m)	
0.40	MC				cast to pvc			
0.90	FH				reached rwg1			
Comments:								

<b>Run:</b>	<b>2</b>							
From:	MH1	Invert Level:		Direction:	U/S			
To:	U/S	Invert Level:	400	Function:				
Pipe Material:	Cast Iron	Pipe Dia:						
Water/Pressure Test:		Drain Break-In:	No	Gully Condition:				
Distance (m)	Code	Clock Ref at to	Dia mm	Intrusion % mm	Shared Run:	No		
					If Shared How:			
0.00	ST				Remarks	Surface Material	Length (m)	
5.00	GO				run capped off			
5.00	SA				Survey abandoned			
Comments:								

<b>Run:</b>	<b>3</b>							
From:	MH1	Invert Level:		Direction:	U/S			
To:	U/S	Invert Level:	400	Function:	F/W			
Pipe Material:	Cast Iron	Pipe Dia:	100					
Water/Pressure Test:		Drain Break-In:	No	Gully Condition:				
Distance (m)	Code	Clock Ref at to	Dia mm	Intrusion % mm	Shared Run:	Yes		
					If Shared How:	With flats		
0.00	ST				Remarks	Surface Material	Length (m)	
0.50	DEG			30	Debris grease	concrete	0.5	
1.70	FH				reached 1.7m	inside not seen		
Comments:								
possible internal gully								

<b>Run:</b>	<b>4</b>										
From:			MH1	Invert Level:			Direction:	U/S			
To:			U/S	Invert Level:	400		Function:	F/W			
Pipe Material:			Cast Iron	Pipe Dia:	100						
Water/Pressure Test:				Drain Break-In:	No		Gully Condition:				
Distance (m)	Code	Clock Ref at	to	Dia mm	Intrusion %	mm	Shared Run:	Yes			
							If Shared How:	With flats			
0.00	ST						Remarks	Surface Material	Length (m)		
0.20	MC						cast to pvc				
0.50	LR						Line deviates right	concrete	0.5		
1.50	LL						Line deviates left	inside vinyl floor			
2.00	LU						Line deviates up				
2.10	FH						reached possible int. SVP				
Comments:											
<b>Run:</b>	<b>5</b>										
From:			MH1	Invert Level:			Direction:	D/S			
To:			D/S	Invert Level:	400		Function:	Comb			
Pipe Material:			Cast Iron	Pipe Dia:	100						
Water/Pressure Test:				Drain Break-In:	No		Gully Condition:				
Distance (m)	Code	Clock Ref at	to	Dia mm	Intrusion %	mm	Shared Run:	Yes			
							If Shared How:	With flats			
0.00	ST						Remarks	Surface Material	Length (m)		
2.00	FH						reached 2.0m	concrete	1		
Comments:											
<b>Run:</b>	<b>6</b>										
From:			yg	Invert Level:			Direction:	U/S			
To:			rwp1	Invert Level:			Function:	S/W			
Pipe Material:			PVC	Pipe Dia:	100						
Water/Pressure Test:				Drain Break-In:	No		Gully Condition:	As Built			
Distance (m)	Code	Clock Ref at	to	Dia mm	Intrusion %	mm	Shared Run:	Yes			
							If Shared How:	With flats			
0.00	ST						Remarks	Surface Material	Length (m)		
0.20	DES				100		Debris silt	concrete			
0.20	SA						unable to push				
Comments:											
<b>Run:</b>	<b>7</b>										
From:			yg	Invert Level:			Direction:	U/S			
To:			rwp2	Invert Level:			Function:	S/W			
Pipe Material:			PVC	Pipe Dia:	100						
Water/Pressure Test:				Drain Break-In:	No		Gully Condition:				
Distance (m)	Code	Clock Ref at	to	Dia mm	Intrusion %	mm	Shared Run:	Yes			
							If Shared How:	With flats			
0.00	ST						Remarks	Surface Material	Length (m)		
0.10	DES				100		Debris silt	concrete			
0.10	SA						unable to push				
Comments:											

Run:	8											
From:			yg		Invert Level:				Direction:		D/S	
To:			D/S		Invert Level:				Function:		S/W	
Pipe Material:			PVC		Pipe Dia:		100					
Water/Pressure Test:					Drain Break-In:		No		Gully Condition:			
Distance (m)	Code	Clock Ref at to		Dia mm	Intrusion % mm		Shared Run:				Yes	
							If Shared How:				With flats	
0.00	ST							Remarks		Surface Material	Length (m)	
0.20	DES				100			Debris silt		concrete		
0.20	SA							unable to push				
Comments:												

To: Sedgwick International



Date: 22-Nov-21

Flao: 0

## ESTIMATE

Site - 102-164 Albert Street

Item	No recommendations required to the private drainage surveyed.	Amount
	Runs 6/7 and 8 are PVC and look in good condition but have a lot of silt in them, if survey is required then a return with a jetter would be required to survey these runs.	

### Notes

Repairs to shared runs and off boundary pipe-work may be the responsibility of the water authority.

### Condition Grade

- A - Structurally sound with no leakage evident.
- B - Cracks and fractures observed.
- C - Structurally unsound

Quotation is binding only if accepted within 28 days from date of issue and is subject to our Standard Terms and Conditions  
The price qualification notes, stated on the drainage solutions schedule of rates, apply to this quotation.  
CET Structures Ltd undertakes to return to site free of charge to carry out remedial work to the drainage repairs set out above for a period of 2 months from the date of this invoice. The company standard charge rates will apply to the visit should the work requested be unrelated to the said repairs.

## **CET STRUCTURES LTD TERMS AND CONDITIONS**

**Site:-** 102-104 Albert Street

**Client :-** Sedgwick International  
**Attention of:-**

**Client Ref:-**

**Job Number:-**

**Insurer:-**

**Date:-** 22-Nov-21

### **General Terms and Conditions**

- 1 On site parking is a prerequisite of any drain repair contract. This quotation is to the addressee only and should not be forwarded unless prior agreement is obtained from CET Structures Ltd. Every effort will be made to match existing surfaces however, there will be evidence of excavation works in certain circumstances.
- 2 The rates do not include for excavation of surfaces other than soft ground or concrete < 100mm thick; reinstatement other than concrete <100mm thick; internal excavations; reinstatement >750mm in width; excavation of depths greater than 1.2m; reinforced concrete.
- 3 CET's standard soakaway that is priced on the agreed alliance schedule of drainage rates is constructed to dimensions specified in the NHBC Guidelines for small soakaways. The soakaway is generally located 5m from any foundations (should site constraints permit) and is constructed to provide adequate short term surface water storage and percolation into surrounding ground. This small 1m<sup>3</sup> soakaway is usually of sufficient capacity to accommodate average rainfall from an average surface area of roof space, however in extreme weather conditions and /or larger than average roof surface area feeding the soakaway, surcharging may occur. Alternative designs and prices are available at a cost along with percolation testing. Certain ground conditions may not be suitable for soakaway design due to low permeability and this information is not always readily available.

### **Notes**

For excavation and reinstatement of any steps, will be done on day work rate.

With a minimum of 4 hours. Materials at cost plus 25%.

Any obstacles, shrubs & plants that are located in the working area will need to be removed by others to allow for these works

## Water Authority Sewer Condition Codes

<b>B</b>	Broken pipe at... (or from... to...) o'clock	<b>JN</b>	Junction at... o'clock, diameter... mm
<b>BR</b>	Branch Major	<b>JX</b>	Junction defective at.. o'clock, diameter.. mm
<b>CC</b>	Crack circumferential from... to... o'clock	<b>LC</b>	Lining of sewer changes/starts/finishes at this
<b>CL</b>	Crack longitudinal @... o'clock	<b>LD</b>	Line of sewer deviates down
<b>CM</b>	Cracks multiple from... to... o'clock	<b>LL</b>	Line of sewer deviates left
<b>CN</b>	Connection at... o'clock, diameter... mm	<b>LN</b>	Line defect at (or from.. to.. ) o'clock
<b>CNI</b>	Connection at... o'clock, diameter... mm, intrusion... mm	<b>LR</b>	Line of sewer deviates right
<b>CU</b>	Camera under water	<b>LU</b>	Line of sewer deviates up
<b>CX</b>	Connection defective at... o'clock	<b>MB</b>	Missing bricks at.. (or from.. to..) o'clock
<b>CXI</b>	Connection defective at... o'clock, diameter... mm, intrusion... mm	<b>MC</b>	Material of sewer changes at this point
<b>D</b>	Deformed sewer... %	<b>MH</b>	Manhole/node
<b>DB</b>	Displaced bricks at (or from.. to..) o'clock	<b>MM</b>	Mortar missing medium at.. (or from.. to..) o'clock
<b>DC</b>	Dimension of sewer changes at this point	<b>MS</b>	Mortar missing surface at.. (or from.. to..) o'clock
<b>DE</b>	Debris (non silt/grease)... % cross-sectional loss	<b>MT</b>	Mortar missing total at.. (or from.. to..) o'clock
<b>DEG</b>	Debris grease... % cross-sectional area loss	<b>OB</b>	Obstruction... % height/diameter loss
<b>DES</b>	Debris silt... % cross-sectional area loss	<b>OJL</b>	Open joint large
<b>DI</b>	Dropped invert, gap... mm	<b>OJM</b>	Open joint medium
<b>EHJ</b>	Encrustation heavy from.. to.. o'clock % cross-sectional area loss (at joint)	<b>PC</b>	Length of pipe forming sewer changes at this new length... mm
<b>ELJ</b>	Encrustation light from.. to.. o'clock %	<b>RFJ</b>	Roots fine (at joint)
<b>EMJ</b>	Encrustation medium from.. to.. o'clock %, cross-sectional area loss (at joint)	<b>RMJ</b>	Roots mass... % cross-sectional area loss (at joint)
<b>ESH</b>	Scale heavy... % cross-sectional area loss from... to... o'clock	<b>RTJ</b>	Roots tap (at joint)
<b>ESL</b>	Scale light from... to... o'clock	<b>SA</b>	Survey abandoned
<b>ESM</b>	Scale medium... % cross-sectional area loss from... to... o'clock	<b>SC</b>	Shape of sewer changes at this point
<b>FC</b>	Fracture circumferential from... to... o'clock	<b>SSL</b>	Surface damage, spalling large at (or from.. to.. o'clock
<b>FL</b>	Fracture longitudinal at... o'clock	<b>SSM</b>	Surface damage, spalling medium at (or from.. to.. o'clock
<b>FM</b>	Fractures multiple from... to... o'clock	<b>SSS</b>	Surface damage, spalling slight at (or from.. to.. o'clock
<b>GO</b>	General observation at this point	<b>SWL</b>	Surface damage, wear large at... (or from.. to.. o'clock
<b>GP</b>	General photograph number... taken at this point	<b>SWM</b>	Surface damage, wear medium at... (or from.. to.. o'clock
<b>H</b>	Hole in sewer at... o'clock	<b>SWS</b>	Surface damage, wear slight at.. (or from.. to.. o'clock
<b>IDJ</b>	Infiltration dripper at (or from... to...) o'clock (at joint)	<b>V</b>	Vermin (rats and mice)
<b>IGJ</b>	Infiltration gusher at (or from... to...) o'clock (at joint)	<b>WL</b>	Water level... % height/diameter
<b>IRJ</b>	Infiltration runner at (or from... to...) o'clock (at joint)	<b>X</b>	Sewer collapsed... % cross-sectional area loss
<b>ISJ</b>	Infiltration seep at (or from... to...) o'clock (at joint)	<b>FH</b>	End of survey
<b>JDM</b>	Joint displaced medium		
<b>JDL</b>	Joint displaced large		