



Feasibility Research

EIA, Flood Risk & Transport Assessment:

Urban Planning and Design

Integrated Transport Solutions Infrastructure Development

Structural Design

Eco and MMC Focused Flood Risk Assessment and Drainage Strategy Report Issue 3 2-4 Shoot-Up Hill, London 14065 For Notting Hill Genesis

Engineering at its Best



Report For

Notting Hill Genesis

Scheme No: 14065

2-4 Shoot-Up Hill, London

Flood Risk Assessment and Drainage Strategy Report Issue 3

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Flood Risk Assessment and Drainage Strategy Report - Issue 3

1.0 Introduction

Tully De'Ath have been commissioned by Notting Hill Genesis to provide a Flood Risk Assessment and Drainage Strategy Report to accompany a planning application for the proposed residential development at 2-4 Shoot-Up Hill, London NW2 3QN.

The purpose of the report is to demonstrate to the Planners and the Lead Local Flood Authority representatives within the London Borough of Camden, that the proposed development is subject to an acceptable risk of flooding and can be drained both safely and sustainably for the lifetime of the development.

The present report has been produced in accordance with the technical guidance set out within the following documents:

- London Borough of Camden Local Plan Policy CC3
- London Plan Policy 5.13 and Draft New London Plan Policy SI.13
- National Planning Policy Framework (NPPF) (updated version February 2019)
- Ciria SuDS Manual (2015)
- London Borough of Camden Surface Water Management Plan
- London Borough of Camden Strategic Flood Risk Assessment (SFRA)

London Borough of Camden Water and Flooding Planning Guidance (March 2019)

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2.0 Site Location and Setting

The site is located to the eastern end of No's 2-4 Shoot-Up Hill, London, within the administrative boundary of the London Borough of Camden.

The site is bounded by Maygrove Road to the south, and residential properties to the north, east and west. The approximate central postcode is NW2 3QN. The National Grid Reference is TQ246846.

Refer to Appendix A for a Site Location plan.



3.0 Existing Conditions

3.1 Land Use

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The site covers an approximate area of 290m², and is currently occupied by a number of outbuildings, which include a timber shed and a small brick-built single-storey building, as well as part of the rear garden of No. 4 Shoot up Hill. These structures are surrounded by a mixture of rough ground and concrete hard standing.

3.2 Local Topography

The topographical survey undertaken in August 2018 (Appendix B) indicates that the majority of the site is relatively flat, with an average ground level of approximately 45.8m AOD.

In terms of the surrounding adopted highway network, Maygrove Road appears to fall gradually southwestwards towards Shoot-Up Hill, with levels ranging from 45.62m AOD to 45.52mAOD along the road section adjacent to the site.

3.3 Drainage

With reference to the Thames Water sewer records (included in Appendix C), the local adopted sewer network appears to comprise a single 1016 x 686mm combined asset, which runs in an east-west direction along Maygrove Road towards Shoot-Up Hill.

Based upon this record information, it is understood that the invert level of this asset at its closest point to the site is 41.15m, approximately 4.5m below road level.

A drainage survey has not been undertaken on the site however, it is noted that a rainwater pipe and a yard gully is noted on the survey, and due to the age of the buildings it is considered likely that these drains connect to the adjacent combined sewerage system.

3.4 <u>Geology</u>

The British Geological Survey records contain a borehole scan on property No.4/6 Shoot-Up Hill, immediately adjacent to the north of the site, which indicates Made Ground, over Alluvium, over London Clay Formation.

No ground water was encountered in the borehole, which was dug to a depth of 19.2m.

An intrusive onsite ground investigation established that below a layer of made ground (up to 1.2m thick) the natural geology is silty clay, over London Clay.

Based upon the presence of the impermeable clay layers described above, infiltration techniques are not considered to be suitable as a means of surface water disposal.

3.5 Local Water Courses and Water Features

The site is approximately 3km to the north of the Regents Canal and 7km north of the River Thames. No other water courses are present within the vicinity of the site.

4.0 Development Proposals

4.1 The proposed development will provide 6 residential flats within a four-storey block, which includes external hard and soft landscaping to the front and rear of the block.

A set of architectural drawings can be found in Appendix F.



5.0 Fluvial and Tidal Flood Risk Assessment

5.1 With reference to the flood maps obtained from the Gov.uk website (Appendix E), the site lies entirely within a Flood Zone 1, which means that the probability of flooding from tidal and fluvial sources is less than 1 in 1000 (0.1%) in any one year.

It is therefore considered that the proposed development will be subject to a very low risk of flooding from Fluvial and Tidal sources.

In terms of flood risk, the development is classed as More Vulnerable within the NPPF, which is considered appropriate development for a Flood Zone 1 area.

1 6.0 Other Sources of Flooding

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6.1 Ground Water Flooding

With reference to map 4 in Appendix D of Camden's Flood Risk Management Strategy, the site is not classed as being at risk from groundwater flooding.

In addition to this, and as mentioned in Section 3.4 above, it is worth noting that the record information for the 19.2m deep borehole dug in the vicinity of the site does not highlight the presence of groundwater.

The risk from this type of flooding is therefore considered to be low.

6.2 Surface Water Flooding

With reference to the Gov.uk (Appendix E) and Camden SFRA's (Appendix D), the site is not located within an area which is subject to surface water flooding, although it is noted that the adjacent property to the west does have a high surface water flood risk, which appears to relate to a local low spot.

It is also noted that opposite the site, Maygrove Road is highlighted as having a Low to Medium risk of surface water flooding.

To mitigate any potential risk associated to this source of flooding, it is proposed that the existing vehicular crossover (which currently acts as the site entrance) is removed and replaced with a full-height section of footway, laid with a gradient away from the development and towards the adjacent Maygrove Road carriageway.

In addition, the ground floor units will be set at a minimum level of 45.840m AOD, which is slightly higher than the existing average ground level on site (45.800m AOD), and approximately 240mm higher than the highest point within the adjacent adopted carriageway in Maygrove Road.

6.3 Sewer Flooding

Based upon Figure 5a 'DG5 Internal Sewer Flooding' of Camden's Strategic Flood Risk Assessment (Appendix E), no internal sewer flooding events have been recorded in the postcode area where the site is located. With regard to exterior sewer flooding, the records show that only two properties have been affected by this type of flooding over the past 10 years, although the exact location of such properties is not specified.

With reference to Figure 6 of Camden's Strategic Flood Risk Assessment (Appendix D), the site is located on the boundary of a critical drainage strategy (group 3_010), but not within a Local Flood Risk Zone.

With reference to Chapter 8, a new surface water system is to be provided which will restrict flows to the minimum practical value and attenuation provided to accommodate 1 in 1 in 100 return period including a 40% allowance for climate change.

See Appendix G for the indicative Drainage Strategy plan

Based on the above, it is considered that the proposed development will be subject to an acceptable risk of flooding from sewer sources.



6.4 <u>Reservoirs</u>

With reference to the Gov.uk maps (Appendix E), the site is not considered to be at risk of flooding from reservoir sources.

N 7.0 Surface Water Drainage Proposals

7.1 SuDS General

Appropriately designed, constructed and maintained, SuDS are more sustainable than conventional drainage systems and can help to:

- Reduce run-off rates.
- Reduce the risk of flooding.
- Encourage natural groundwater re-charge.
- Reduce pollutant concentrations in storm water.
- Reduce volume of surface water run-off,
- Provide habitats for wildlife.

7.2 <u>SuDS Appraisal</u>

There are many site-specific factors which will influence the choice of any SuDS devices used within a development. The primary factors are:

- How the land is to be used- whether domestic, commercial or industrial.
- Soil contamination.
- Existing soil conditions i.e. ground permeability, water table levels.
- Site topography e.g. steeply sloping.
- Space availability urban or non-urban.

In considering the above and taking into account that infiltration is very unlikely to work, the following SuDS are proposed to be introduced for this development:

- Biodiverse/Green roofs.
- Off-site flow control and above/below ground attenuation.

7.3 <u>Biodiverse Roofs</u>

Biodiverse/green roofs involve various types of soil and vegetation cover of roof areas, which are generally underlain by a drainage blanket linked to the rainwater down-pipe system. The provision of these systems can improve the water quality of the run-off generated at roof level while also contributing towards the removal of air pollutants and dust. Additionally, they can also provide an ecosystem that can replace natural habitats that have been lost due to urbanization.

In dry climatic conditions, they can significantly reduce the volume of run-off from roof areas due to the water demand of the vegetation and/or evaporation from the granular surfaces.

It is understood that the proposed development will incorporate a biodiverse roof system across the majority of the roof area.



7.4 Off-site Flow Control and Above/Below Ground Attenuation

The use of off-site flow controls in conjunction with attenuation tanks have proven to be beneficial with reducing flood risk both within and beyond the site, as they significantly reduce the peak discharge rate into the sewer network downstream of the site.

As discussed in Section 8.5, the current proposals allow for the installation of both above and below ground attenuation storage structures, so that off-site discharge rates for all storm events up to and including the 1 in 100 + 40% CC can be restricted as far as practically possible.

Refer to Appendices G and H for the indicative Drainage Strategy plan and associated MicroDrainage Calculations.

7.5 Other SuDS Devices Considered Not Suitable for the Development – Drainage Hierarchy

In developing the surface water drainage strategy and selecting appropriate SuDS features for the development, the drainage hierarchy contained within the new London Plan Draft Policy SI.13 has been considered. This recommends the following methods for surface water disposal (in order of preference):

- 1. Rainwater harvesting (including a combination of green and blue roofs).
- 2. Infiltration techniques and green roofs.
- 3. Rainwater harvesting (including a combination of green and blue roofs).
- 4. Infiltration techniques and green roofs.
- 5. Rainwater harvesting (including a combination of green and blue roofs).
- 6. Infiltration techniques and green roofs.
- 7. Rainwater attenuation in open water features for gradual release.
- 8. Rainwater discharge direct to a watercourse (unless not appropriate).
- 9. Rainwater attenuation above ground (including blue roofs).
- 10. Rainwater attenuation below ground.
- 11. Rainwater discharge to a surface water sewer or drain
- 12. Rainwater discharge to a combined sewer.

As described in Section 8.5, the drainage strategy generally follows the above hierarchy in that, where feasible, it incorporates the preferred drainage features. This includes the provision of green and blue roofs as well as a below ground attenuation tank (Items 1, 2, 5 and 6).

With that said, it is worth noting that there are certain items of the hierarchy that could not be incorporated due to the below reasons:

Rainwater Harvesting (Item 1)

Rainwater harvesting systems currently available do not cater for the catchment of surface water from non-roof external surfaces such as roads, car parks and pedestrian areas due to the increased levels of treatment required. The inclusion of rainwater harvesting can therefore increase the complexity of the required surface water drainage network and thus the environmental impact involved in its construction.

In addition to this, it is anticipated that the proposed development will incorporate green roofs which would have a detrimental effect on the potential rainwater harvesting system. From a hydraulic/hydrological point of view, green roofs provide certain degree of runoff retention, which would therefore reduce the volume of water reaching the harvesting tank, resulting in a reduced available volume of rainwater for the resident's use and therefore, making the system less cost efficient.



Also, from a water quality perspective, rainwater from green roofs usually contain high levels of dissolved organic carbon as well as pesticides and fertilizers that may be used for its maintenance and therefore, the combination of both green roofs and rainwater harvesting systems is questionable.

Given the above, rainwater harvesting is not considered to be appropriate in this instance and will therefore not be provided for this development.

Infiltration Techniques (Item 2)

As described in section 3.4, the anticipated sub-soil conditions would prevent the use of infiltration techniques as a suitable means of surface water disposal.

Attenuation in Ponds or Open Water Features (Item 3)

In the right circumstances these facilities can also provide aesthetic and amenity value.

As with many developments in an urban area it is difficult to accommodate SuDS such as this in view of the limited space available for landscaping.

Accordingly, this form of SuDS will not be incorporated into the development.

Discharge Direct to a Watercourse (Item 4), or to a Surface Water Sewer (Item 7)

As noted in Chapter 3, there are no watercourses or surface water sewers in the vicinity of the area and therefore, the discharge of surface water flows via these will not be possible.

8.0 Sustainable Drainage Options

8.1 Existing and Proposed Impermeable Areas

With reference to the plans included in Appendices B and F, the existing and proposed impermeable areas have been estimated as:

- Existing Impermeable Area: 140m²
- Proposed Impermeable Area: 275m²

These figures indicate a net increase of 135m² in impermeable areas as a result of the proposed development.

8.2 Existing Surface Water Discharges

Whilst no drainage survey has been undertaken it can be seen from the survey that a rain water pipe and a gully currently existing on the site, which suggests that there is a connection into the adjacent sewerage system.

Considering the existing impermeable area of 140m², and based upon the standard rainfall rates from TRRL 595, the existing peak surface water discharge rates from the site can be estimated as follows:

- 1 in 1 Year Storm Event: 50mm/hr x 140m² = 2 l/s
- 1 in 30 Year Storm Event: 113mm/hr x 140m² = 4.4 l/s
- 1 in 100 Year Storm Event: 144mm/hr x 140m² = 5.6 l/s



8.3 Ground Infiltration

The most favorable form of surface water discharge involves the retention of surface water within the development, where it is allowed to soak into the underlying ground. This requires suitable permeable and un-contaminated ground conditions beneath the site. In order to avoid any potential detrimental effects upon building foundations, soakage facilities generally need to be located at a minimum off- set of 5m from any building structure.

With reference to Section 3.4, the presence of clay sub-soils implies that the site has very poor infiltration capacity. Additionally, the proposed site layout would prevent the installation of any soakage feature at least 5m away from the building foundations.

Due to the above, surface water flows will need to be drained off-site.

8.4 <u>Proposed Surface Water Off-site Connection</u>

Having discounted ground infiltration and given the absence of watercourses and surface water sewers in the vicinity of the site, it became apparent that the only feasible means of surface water disposal will involve a new connection into the 1016 x 686mm adopted combined sewer that runs along Maygrove Road.

In particular, the proposed drainage strategy allows for the surface water flows from the site (restricted as per Section 8.5) to be discharged into the adopted combined sewer in Maygrove Road via a new 150mm dia. combined gravity connection.

Refer to Appendix G for an indicative Drainage Strategy Plan.

8.5 Flow Control and Attenuation

As stated with Camden's Local Policy CC3, new developments should aim to restrict off site surface water flows to values that are as close as practically possible to greenfield rates. Such criteria should apply for all storm events up to and including the 1 in 100-year storm with an additional 40% allowance for climate change.

Based upon the total site area of 290m², the greenfield runoff rates have been calculated using Micro Drainage Software's Source Control programme 'ICP SuDS'. A summary of the results can be found below:

Return Period	Greenfield Runoff Rate (I/s)	Proposed Discharge Rate (I/s)
1 in 1 year	<0.1	2.5
1 in 30 year	0.1	2.5
1 in 100 year	0.1	2.5

From an initial feasibility assessment, it became apparent that achieving such low rates would have a series of future maintenance implications, which would be mainly related to the very small size of the aperture that would need to be incorporated within the flow control device.

Flow control will be provided via a vortex flow control (VFC) – e.g. Hydrobrake or similar- and therefore, it is worth taking into account the VFC manufacturer's recommendations when it comes to minimum orifice sizes. In particular, the proposed off-site discharge rates (also shown within the table above) are based on restricting the orifice size within the VFC to a minimum size of 75mm, which is widely considered as the minimum aperture that still provides an acceptable level of protection against potential blockages.

With this in mind and based upon the available gravity head over the VFC, it is proposed that off-site discharge rates are restricted to a maximum of 2.5 l/s for all storm events up to and including the 1 in 100 + 40% CC storm event.



To achieve the above, and given the constraints imposed by the proposed site layout (i.e. limited external space available for below ground attenuation storage), the current proposals allow for surface water flows from the roof to be restricted 'at source' to the minimum rate practically possible, via the provision of an 85mm deep blue roof system with bespoke flow control outlets designed to limit roof outflows to a maximum of 1.0 l/s. The detailed design of the blue roof system will need to be undertaken by the supplier of the installed system based upon the parameters mentioned above.

This restricted flow from the blue roof system, along with any additional runoff generated within the rest of the proposed impermeable areas on site, will be in turn conveyed into a below ground attenuation tank located at the rear of the ground floor terrace, and designed to accommodate a minimum of 7.6m³ of attenuation storage.

It has been calculated that this volume will be sufficient to restrict the surface water discharge rate to a maximum of 2.5 l/s for all storm events up to the 1 in 100 + 40% CC event.

Refer to Appendix H for Micro-Drainage calculations and Appendix I for the Camden SuDS Proforma.

8.6 Surface water attenuation has been provided to accommodate a 1 in 100-year event with an additional 40% allowance for climate change. However, to mitigate the potential impact of an exceedance storm event, external ground levels will be designed to fall away from the building.

9.0 Foul Drainage Strategy

Based on the peak daily flow of 4000 litres per dwelling specified in Sewers for Adoption 7th Edition, the introduction of 6 No. residential units within the proposed development will produce a peak foul design flow of approximately 0.28 l/s.

The existing site does not appear to have a foul drainage system; however, the new foul flows are very low and are unlikely to have a negative impact on the capacity of the adopted sewerage system.

Due to recent changes in legislation the sewerage undertakers are not able to object to a planning application due to a lack of foul water capacity.

Should it be established that the existing onsite drainage is connected to the combined sewers, the new reduction in surface water flows for the larger return periods will more than offset the small increase in foul flows.

With reference to the indicative Drainage Strategy drawing included in Appendix G, the new foul drainage system will connect to the combined sewer within Maygrove Road via a new 150mm dia. gravity connection, which will be subject to a S106 Agreement with Thames Water.



10.0 Maintenance

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Maintenance of any drainage scheme is essential to ensure that it continues to perform as designed.

Maintenance of the drainage for this development will be the responsibility of the developer. Within the site's 'Health & Safety File' details of routine maintenance inspections should be included together with guidance on how and when these should be undertaken.

Generally, the drainage system requires regular inspection/clearing to prevent blockages due to the accumulation of silt. It also needs to be maintained on a regular basis. It is recommended that the system is initially inspected and cleared by a suitably trained person every six months for at least the first two years of operation to establish the long-term inspection/clearing interval appropriate for this site. Inspection/clearing should also be carried out after every major storm event.

In addition to any specific requirements from relevant manufacturers, regular maintenance of the drainage system should include the following:

- Checking all inspection chambers and clearing of silt, debris and other blockages as required.
- Rainwater downpipes and gullies to be cleaned-out at roof and ground levels.
- Trapped gullies and drainage channels within the drainage network should be inspected and cleared of silt.
- Green roof areas to be kept clear of weeds, debris and dead leaves. The outlet gullies on the green roofs must be inspected and cleared on a regular basis.

All maintenance must be carried out by suitably trained individuals. Refer to Appendix J for detailed maintenance schedule.



11.0 Conclusions

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11.1 Flood Risk

The information contained within the Gov.uk flood maps indicates that the site lies within a Flood Zone 1 area. This represents a low risk of flooding from both tidal and fluvial sources (less than a 1 in 1000 probability in any given year).

The Camden's Strategic Flood Risk Assessment maps show that the site is entirely within an area not at risk from groundwater flooding.

The site is not located within an area which is subject to surface water flooding, although it is noted that the adjacent site to the west is located within a high flood risk area, which appears to be related to a localised low spot.

With reference to Figure 5a 'DG5 Internal Sewer Flooding' of Camden's Strategic Flood Risk Assessment, no internal sewer flooding events have been recorded in the postcode area where the site is located. With regards to exterior sewer flooding, the records show that only two properties have been affected by this type of flooding over the past 10 years, although the exact location of such properties is not specified.

As indicated within the Gov.uk maps, the site and nearby areas are not at risk of flooding from reservoir sources.

Based on the above, it is considered that the proposed development will be subject to a low risk of flooding and will not increase the flood risk beyond the site.

11.2 Drainage

In view of the anticipated geological formations beneath the site, surface water drainage via infiltration devices is not considered to be feasible. Instead, surface water flows will be discharged off-site via a new 150mm dia. combined gravity connection into the 1016 x 686mm combined adopted sewer in Maygrove Road.

The proposed drainage strategy includes the provision of surface water attenuation, both above and below ground, to reduce the off-site surface water discharge rates to the minimum practically possible (2.5l/s) for all storm events up to and including the 1 in 100 year + 40%CC event. A variety of SuDS such as green and blue roofs will be incorporated to control and treat surface water run-off from the site.

In terms of foul drainage, flows will also be discharged into the 1016 x 686mm combined adopted sewer in Maygrove Rd via the new 150mm dia. gravity connection.

The anticipated foul peak flow of 0.28 l/s is likely to have no detrimental impact on the hydraulic capacity of the adopted sewer network.

Approval to connect to the existing adopted combined sewer in Maygrove Rd will be subject to an Agreement with Thames Water under the terms of a Section 106 in accordance with the Water Industry Act 1991.

The on-site drainage system will be maintained by a Notting Hill Genesis for the lifetime of the development. Maintenance will be in accordance with a site-specific maintenance strategy.



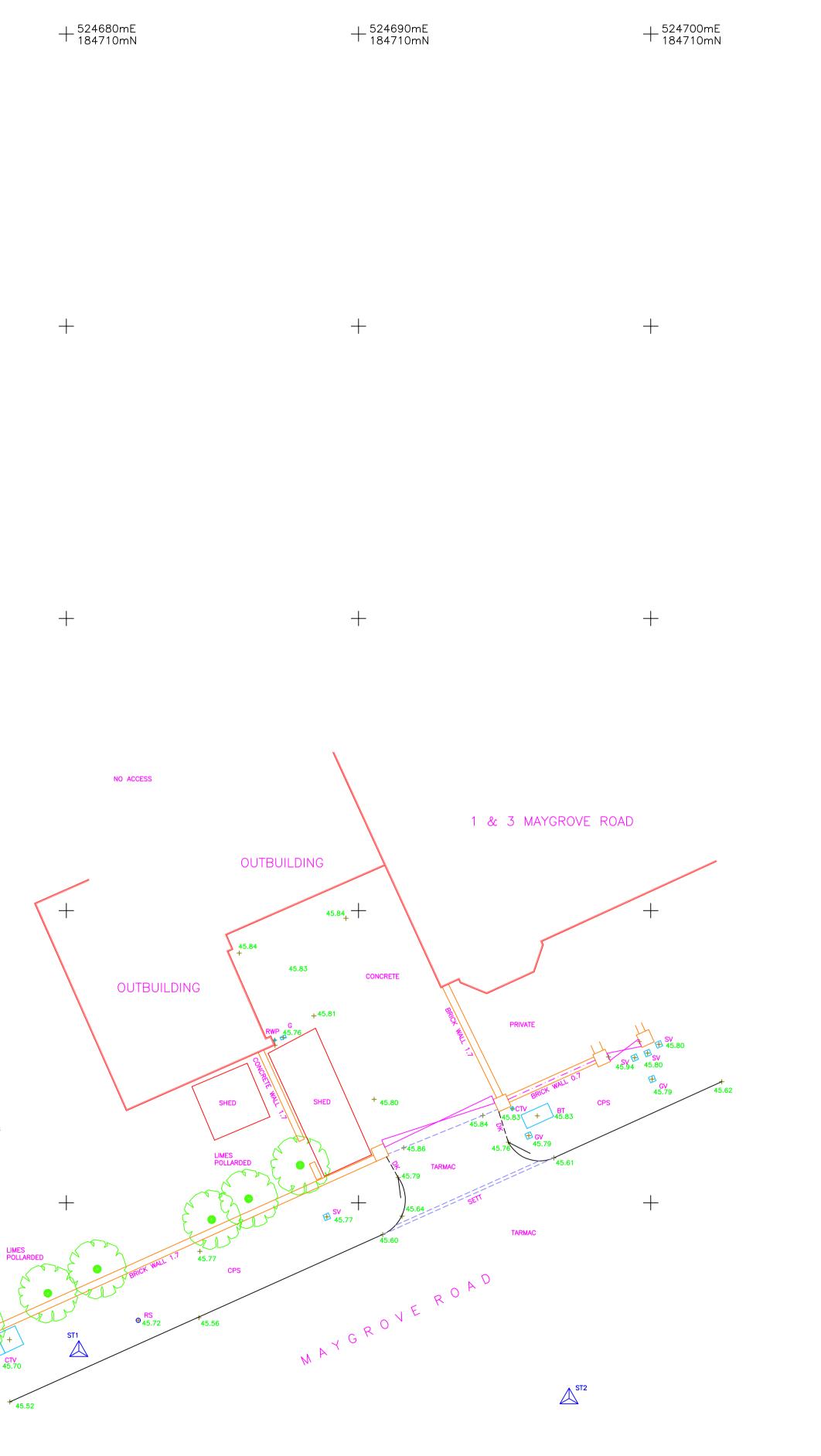
Appendix A – Site Location Plan





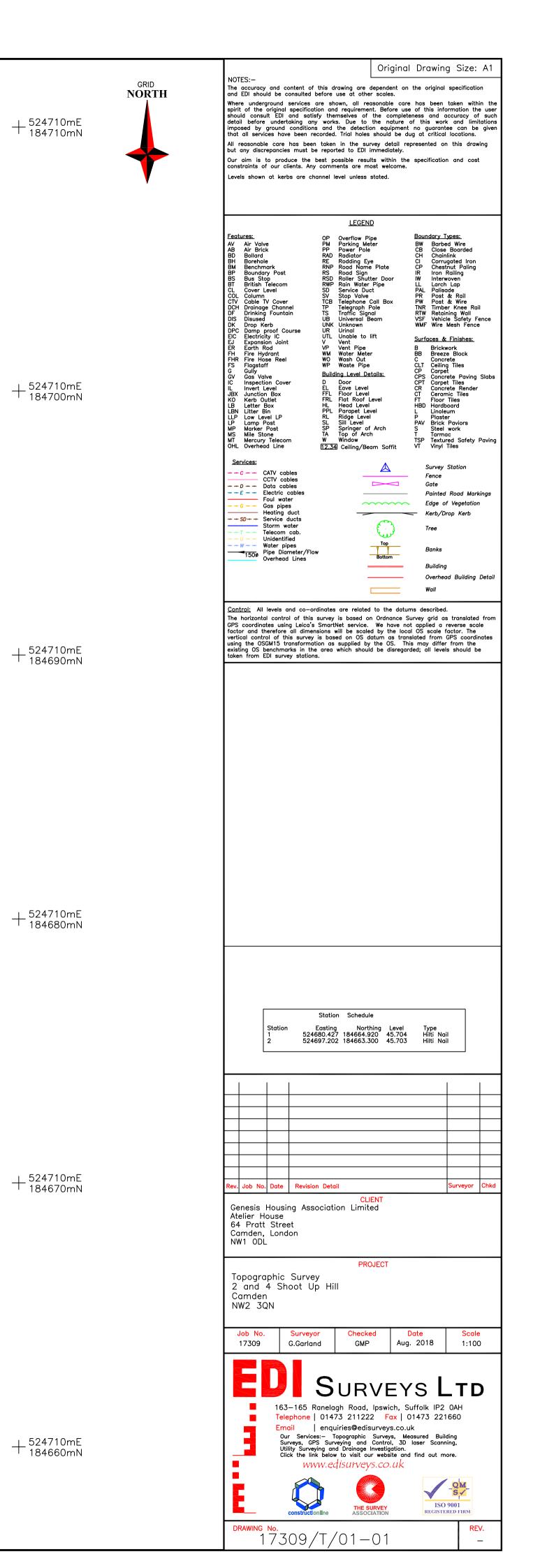
Appendix B – Topographical Survey and Existing Impermeable Areas

+ 524650mE + 184710mN	+ ^{524660mE} 184710mN	+ 524670mE 184710mN
+ 524650mE 184700mN	+	+ CLAUDIUS COURT
+ ^{524650mE} 184690mN	+	+
+ 524650mE 184680mN	6 & 8 SHOOT UP HILL	Contrologine Graduation +
		PRIVATE GARDENS
+ 524650mE 184670mN	+ 2 & 4 SHOO	LIMES POLLARDED
+ 524650mE 184660mN	+ ^{524660mE} 184660mN	+ ^{524670mE} 184660mN

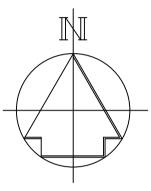


+ 524680mE 184660mN

+ 524690mE 184660mN + 524700mE 184660mN







<u>LEGEND</u>

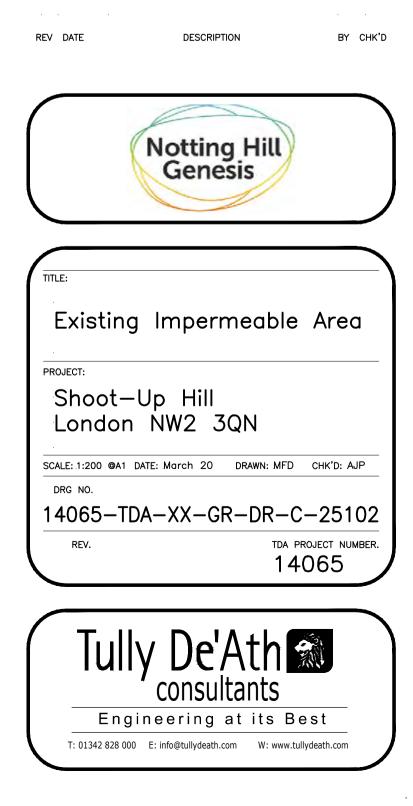
Site Boundary



Total Impermeable Area = 140m²

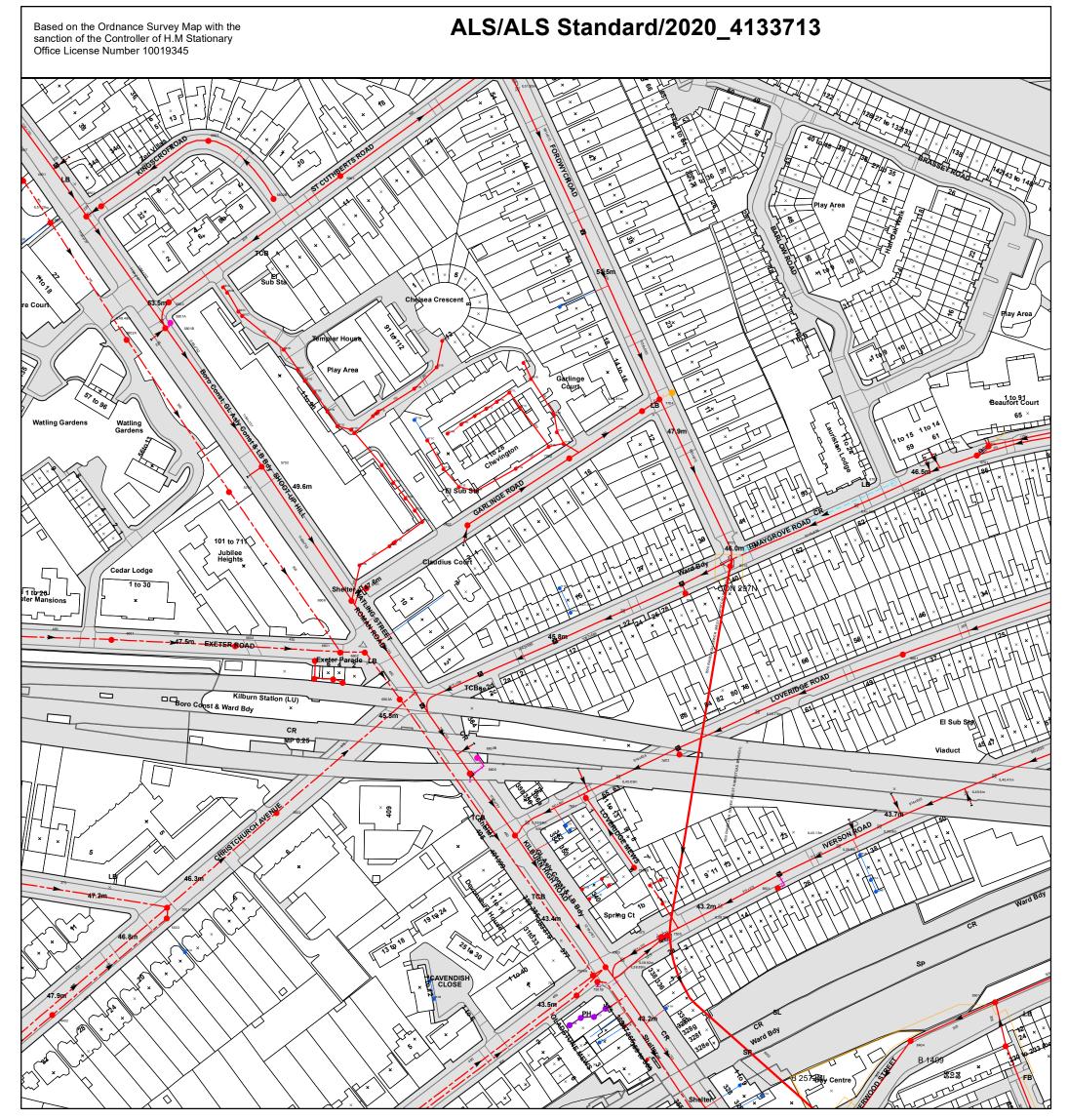
Impermeable Area

PRELIMINARY -FOR PLANNING





Appendix C – Thames Water Sewer Records





The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified before any works are undertaken. Crown copyright Reserved

Scale:	1:1792	Comments:
Width:	500m	
Printed By:	G1KANAGA	
Print Date:	08/01/2020	
Map Centre:	524708,184699	
Grid Reference:	TQ2484NE	

ALS/ALS Standard/2020_4133713

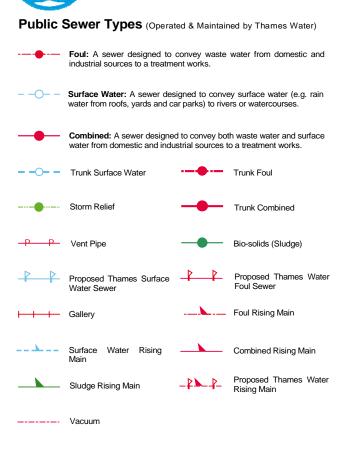
NB: Level quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates no Survey information is available.

REFERENCE	COVER LEVEL	INVERT LEVEL
741G		
7511		
781C		
7703	48.64	44.7
5701	49.86	47.35
6702 603B	47.77	45.43
5903	57.39	54.39
501B	43.17	40.43
8404		
4801	55.09	41.46
56AD		
501B	43.83	39.58
6606	47.5	40.61
5803		
9401		
8501		
7603		
7527		
7503	43.13	38.83
504A	43.24	40.39
603A	45.57	42.57
8702	46.36	43.61
6701	47.45	44.83
4802	55.56	52.5
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671G		
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7704	48.7	44.7
671X	40.7	44.7
671Z		
672B		
781B		
751A		
581B		
581D		
581F		
751B		
581G		
671N		
671P		
681A		
671R		
671T		
671V		
481A		
741B		
741D		
751E		
751G	46.47	42.55
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671A 671E		
771B		
6711		
671K		
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771F		
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651B		

751H	REFERENCE	COVER LEVEL	INVERT LEVEL
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7505 43.09 31.6 5602 47.27 44.35 504B 43.37 7 504B 43.37 7 5001 7 7 9501 702 50.06 40.96 9501 50.82 7 8 9501 50.82 50.82 7 9504 52.88 50.82 7 801B 52.81 41.29 7 9601 46.81 43.86 7 9601 46.81 43.86 7 9601 46.61 43.41 3 9701 46.05 40.1 7 9602 46.61 43.41 3 9716 45.93 43.06 7 771A 7 7 7 7 9715 43.11 8 7 9716 7 7 7 9716 7 7 7 9717 7 <td>851C</td> <td></td> <td></td>	851C		
7505 43.09 31.6 5602 47.27 44.35 504B 43.37 7 504B 43.37 7 5001 7 7 9501 702 50.06 40.96 9501 50.82 7 8 9501 50.82 50.82 7 9504 52.88 50.82 7 801B 52.81 41.29 7 9601 46.81 43.86 7 9601 46.81 43.86 7 9601 46.61 43.41 3 9701 46.05 40.1 7 9602 46.61 43.41 3 9716 45.93 43.06 7 771A 7 7 7 7 9715 43.11 8 7 9716 7 7 7 9716 7 7 7 9717 7 <td></td> <td>56.93</td> <td>54.31</td>		56.93	54.31
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801B52.8141.29801A-8061144.8366BC-660146.81802B57.454.53870146.0548.0945.09660246.6143.41550245.8443.05771A-671C-851A-752543.11841C-671Y-774A-774A-75531.8466BD-841C-671Y-771A-771A-775-774-671Y-775-771D-771D-771D-771D-771D-771D-771D-771D-771A-771D-771D-771D-771D-771D-771D-771D-771C-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q-771Q- <td></td> <td>52.88</td> <td>50.82</td>		52.88	50.82
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8601 44.83 41.34 666C	801B	52.81	41.29
668C	801A		
6601 46.81 43.86 7601	8601	44.83	41.34
7601 F7.4 54.53 8701 46.05 40.1 5601 46.09 45.09 6602 46.61 43.41 5502 45.84 43.05 771A 0 0 671C 1 1 871A 0 0 671C 1 1 851A 0 1 851A 1 1 7525 43.11 1 8715 31.84 66BD 841C 1 1 671Y 1 1 671A 1 1 771D 1 1 841C 1 1 671A 1 1 781A 1 1 <td< td=""><td>66BC</td><td></td><td></td></td<>	66BC		
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5502 45.84 43.05 771A - - 671C - - 671C - - 851A - - 7525 43.11 - 8715 31.84 - 66BD - - 841C - - 672A - - 771D - - 581A - - 581A - - 581E - - 581E - - 671M - - 6710 - - 6710 - - 6710 - - 6711 - - 6712 - - 6714 - - 6715 - - 6710 - - 6714 - - 7415 -			
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672A Image: Constraint of the second sec			
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771D			
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581C			
581E Instant 751D Instant 751C Instant 671M Instant 6710 Instant 6710 Instant 6710 Instant 6710 Instant 6710 Instant 67110 Instant 6718 Instant 6710 Instant 6711 Instant 7412 Instant 7414 Instant 7415 Instant 9701 46.43 42.265 741F Instant 671D Instant 6711 Instant 6714 Instant 6715 Instant 6716 Instant 7716 Instant 761A <t< td=""><td></td><td></td><td></td></t<>			
751D			
751C			
671M			
6710	751C		
671Q	671M		
681B Instance Instance 671S Instance Instance 671U Instance Instance 671W Instance Instance 671W Instance Instance 741A Instance Instance 741C Instance Instance 741E Instance Instance 751F Instance Instance 9701 46.43 42.265 741F Instance Instance 671D Instance Instance 671F Instance Instance 671F Instance Instance 671H Instance Instance 671L Instance Instance 671L Instance Instance 761A Instance Instance 741H Instance Instance 4402 Instance Instance	6710		
681B Instance Instance 671S Instance Instance 671U Instance Instance 671W Instance Instance 671W Instance Instance 741A Instance Instance 741C Instance Instance 741E Instance Instance 751F Instance Instance 9701 46.43 42.265 741F Instance Instance 671D Instance Instance 671F Instance Instance 671F Instance Instance 671H Instance Instance 671L Instance Instance 671L Instance Instance 761A Instance Instance 741H Instance Instance 4402 Instance Instance	671Q		
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9701 46.43 42.265 741F 671D 671F 671H 671J 671L 771E 761A 4402			
741F 671D 671F 671H 671J 671L 771E 761A 741H 4402			
671D 671F 671F 671F 671H 671F 671J 671C 671L 671C 771E 671C 761A 671C 741H 671C 4402 671C		46.43	42.265
671F 671H 671H 671L 671L 671L 771E 671L 761A 761A 741H 671L 4402 671L			
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771E			
761A			
741H 4402			
4402			
651A			

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified before any works are undertaken. Crown copyright Reserved

ALS Sewer Map Key



Sewer Fittings

A feature in a sewer that does not affect the flow in the pipe. Example: a vent is a fitting as the function of a vent is to release excess gas.

- Air Valve Dam Chase Fitting
- ≥ Meter

Π

0 Vent Column

Operational Controls

A feature in a sewer that changes or diverts the flow in the sewer. Example: A hydrobrake limits the flow passing downstream.

X Control Valve Ф Drop Pipe Ξ Ancillary Weir

Outfall

Inlet

Undefined End

End Items

いし

End symbols appear at the start or end of a sewer pipe. Examples: an Undefined End at the start of a sewer indicates that Thames Water has no knowledge of the position of the sewer upstream of that symbol, Outfall on a surface water sewer indicates that the pipe discharges into a stream or river.

- ****/ Public/Private Pumping Station
 - * Ø
 - Invert Level

Other Symbols

< Summit

Areas

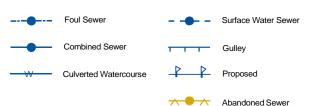
Lines denoting areas of underground surveys, etc.

Symbols used on maps which do not fall under other general categories

Change of characteristic indicator (C.O.C.I.)

Agreement **Operational Site** :::::: Chamber Tunnel Conduit Bridge

Other Sewer Types (Not Operated or Maintained by Thames Water)



Notes:

hames

Water

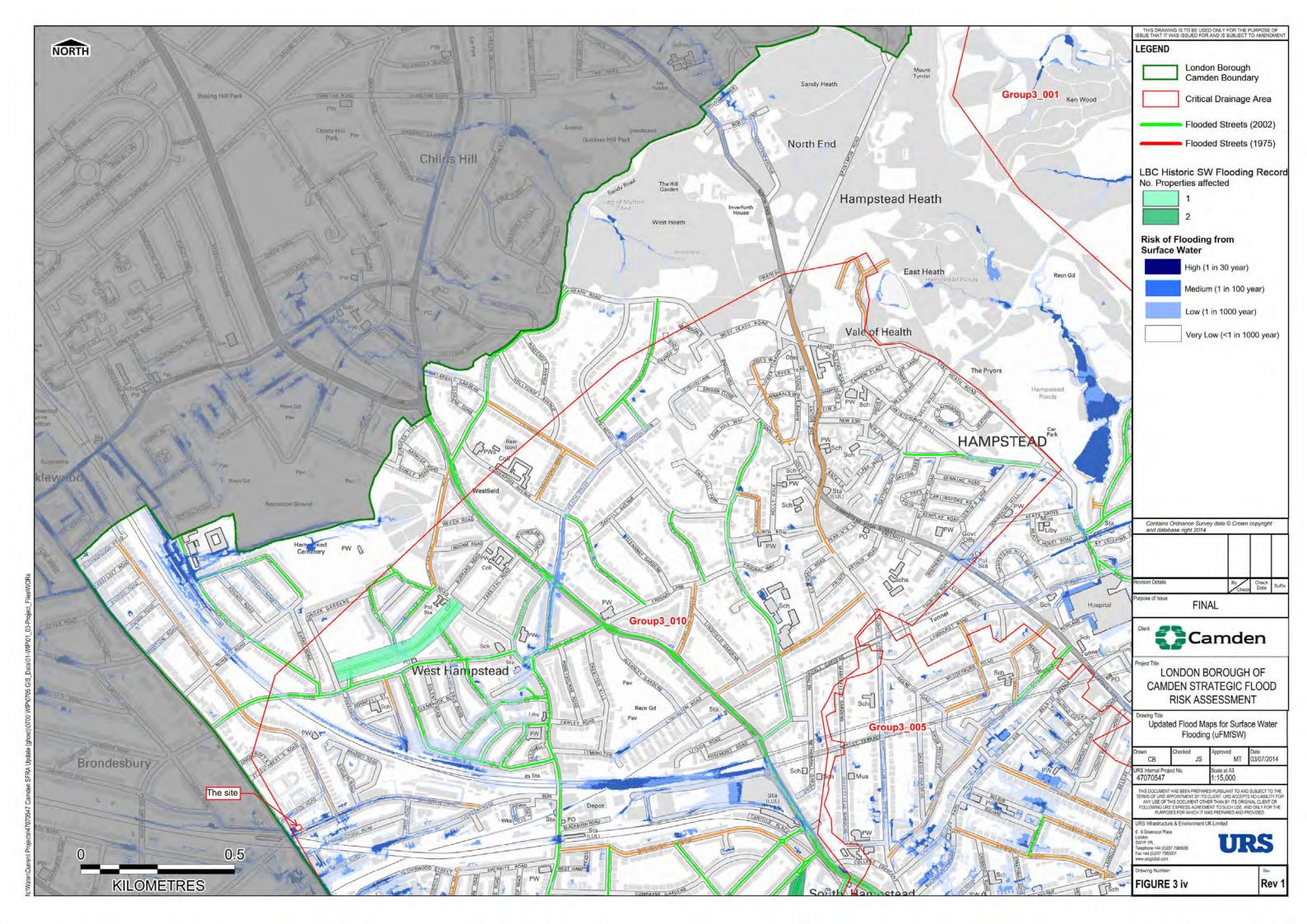
- 1) All levels associated with the plans are to Ordnance Datum Newlyn.
- 2) All measurements on the plans are metric.
- 3) Arrows (on gravity fed sewers) or flecks (on rising mains) indicate direction of flow.
- 4) Most private pipes are not shown on our plans, as in the past, this information has not been recorded.
- 5) 'na' or '0' on a manhole level indicates that data is unavailable.

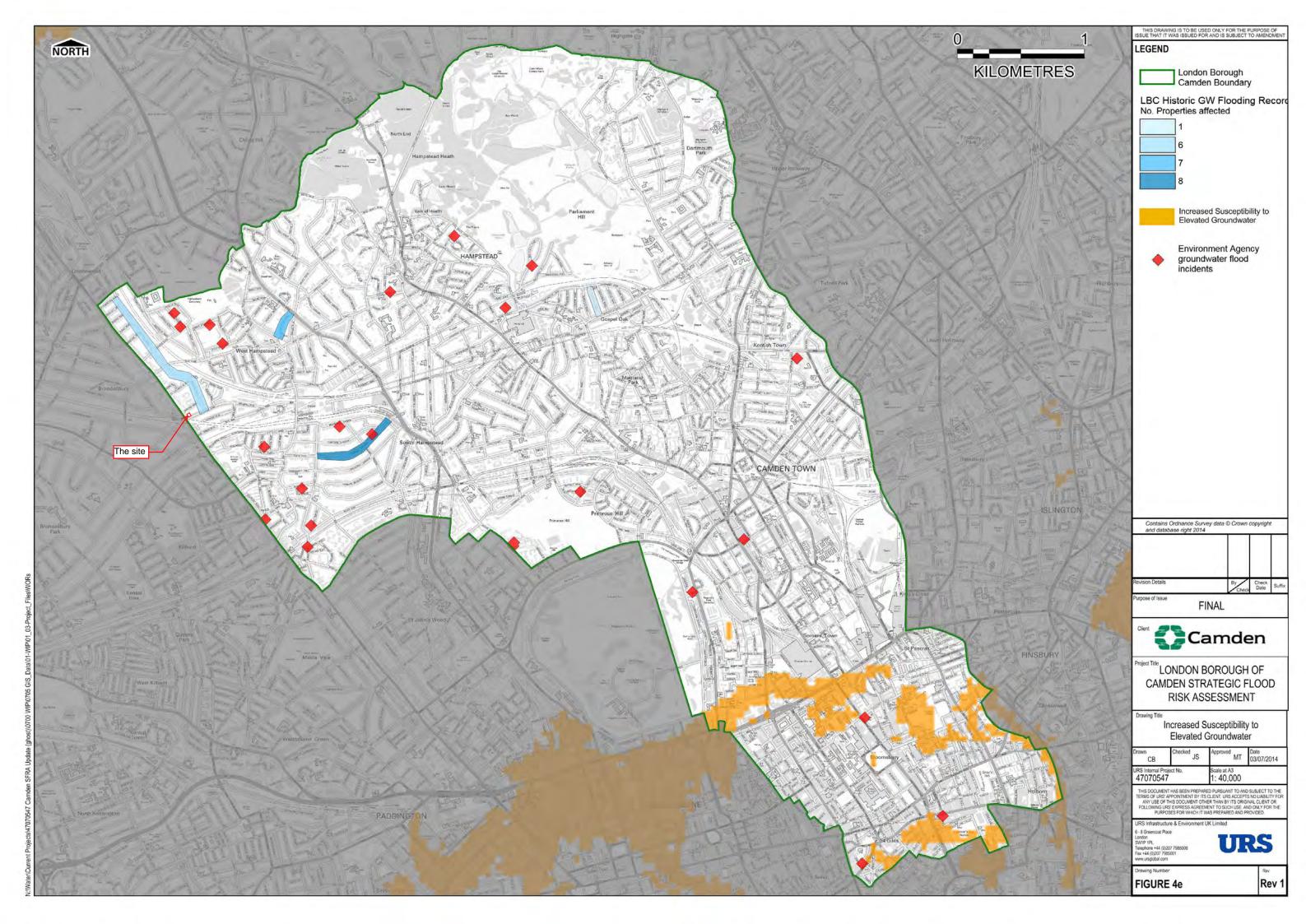
6) The text appearing alongside a sewer line indicates the internal diameter of the pipe in milimetres. Text next to a manhole indicates the manhole reference number and should not be taken as a measurement. If you are unsure about any text or symbology present on the plan, please contact a member of Property Insight on 0845 070 9148.

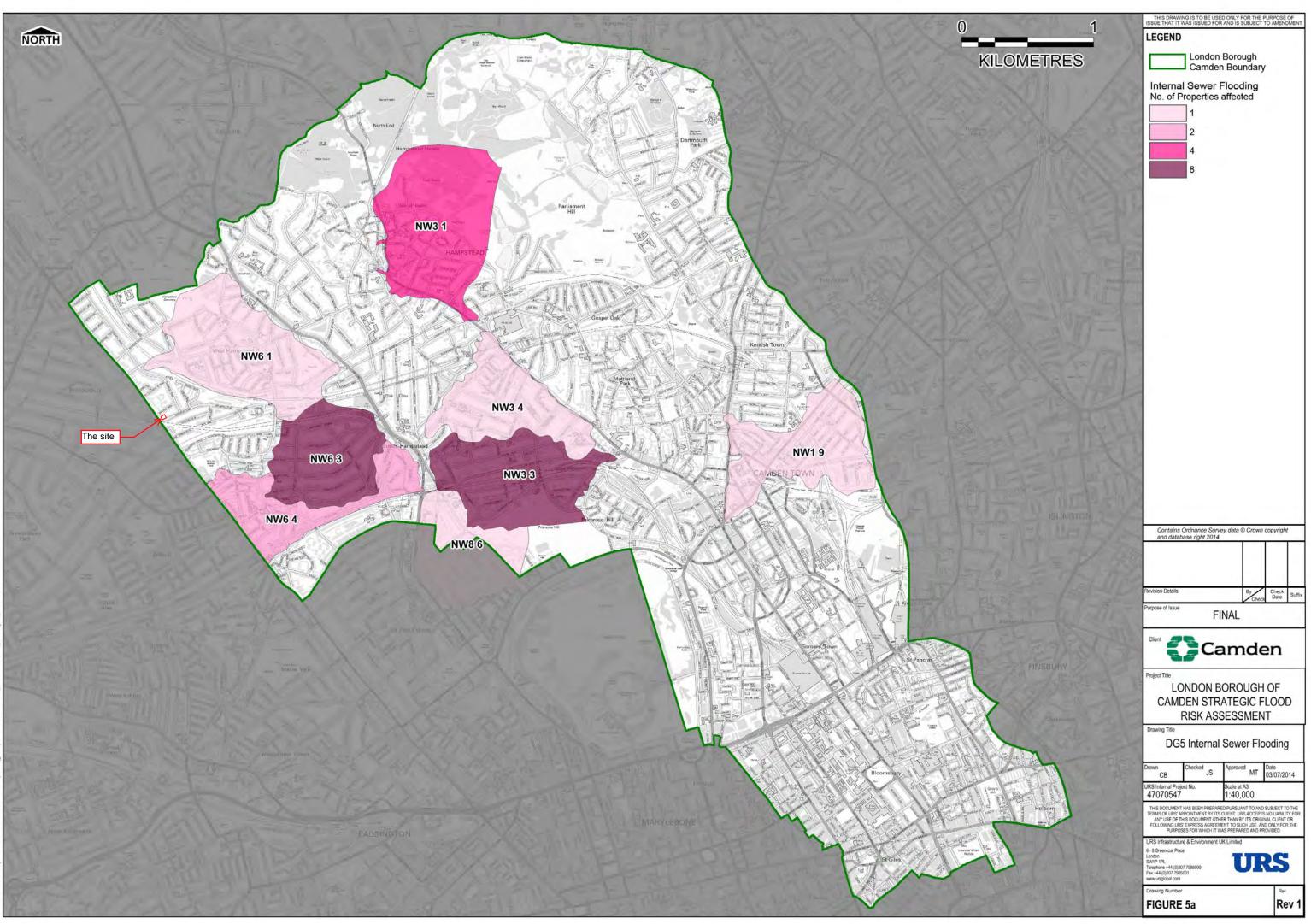
Thames Water Utilities Ltd, Property Searches, PO Box 3189, Slough SL1 4W, DX 151280 Slough 13 T 0845 070 9148 E searches@thameswater.co.uk I www.thameswater-propertysearches.co.uk



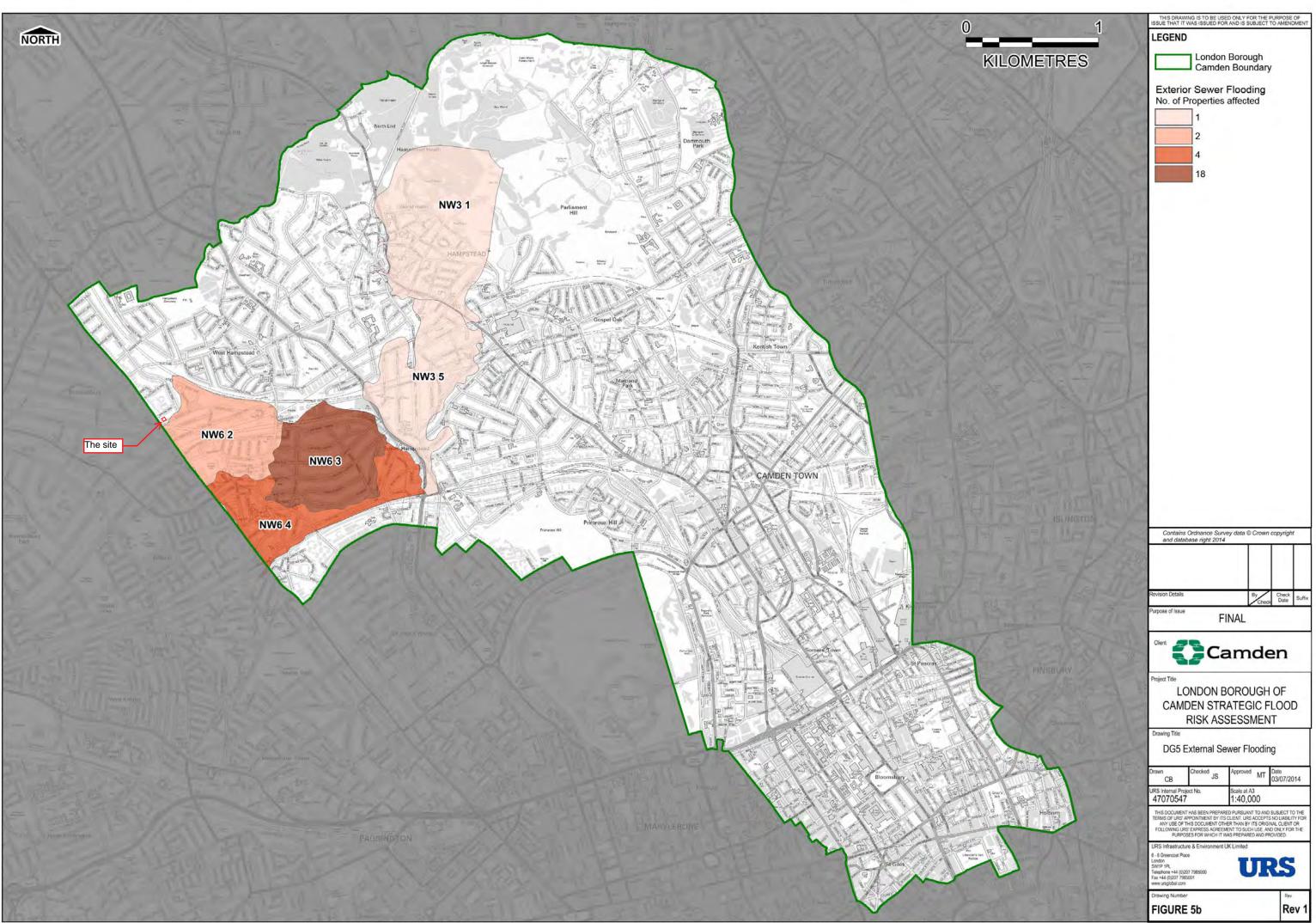
Appendix D – SFRA Flood Maps



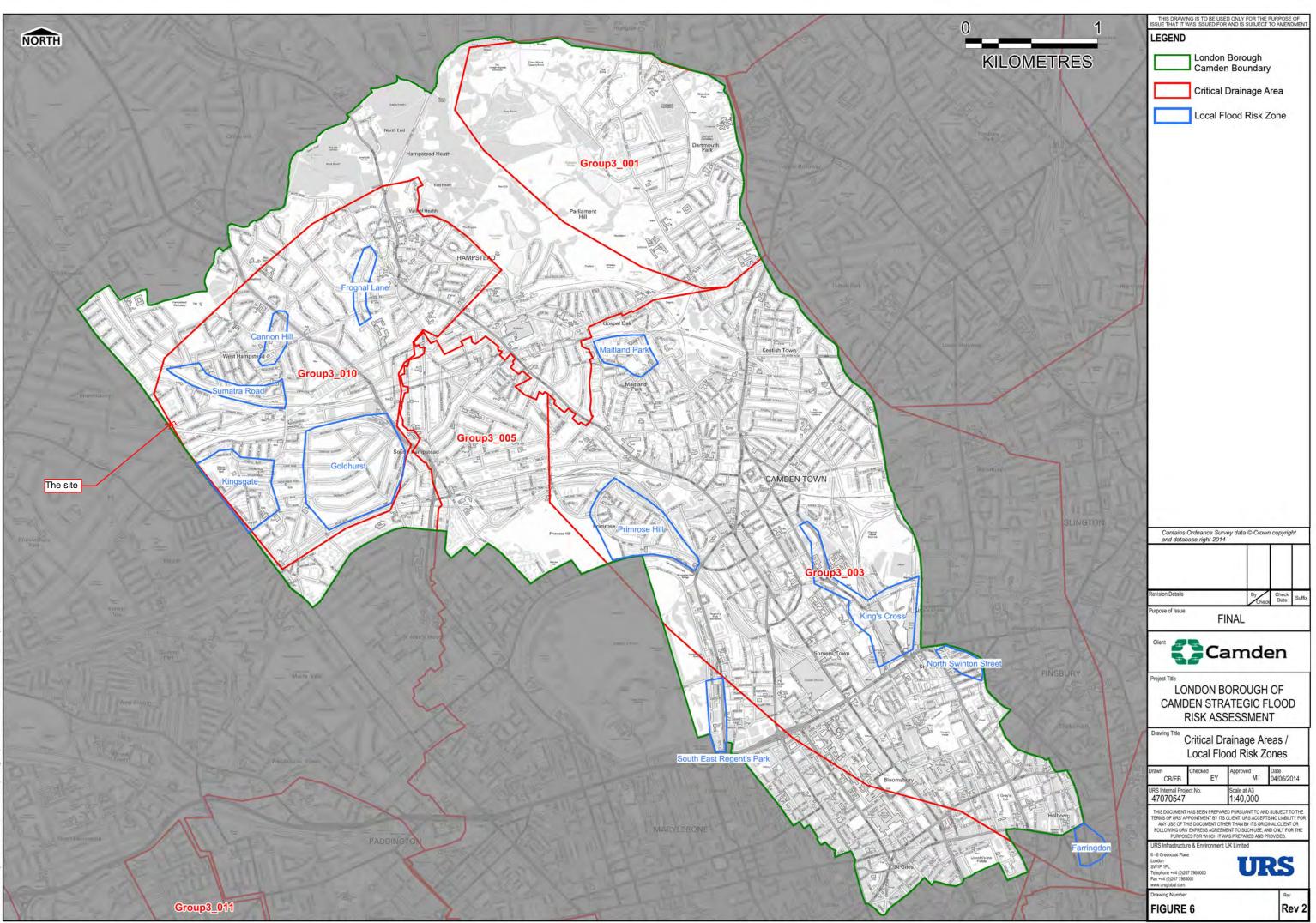




Water/Current Projects/47070547 Camden SFRA Update (ghost)/0700 WIP/0705 GIS_Data(01-WIP/01_03-Project_Files/WOF



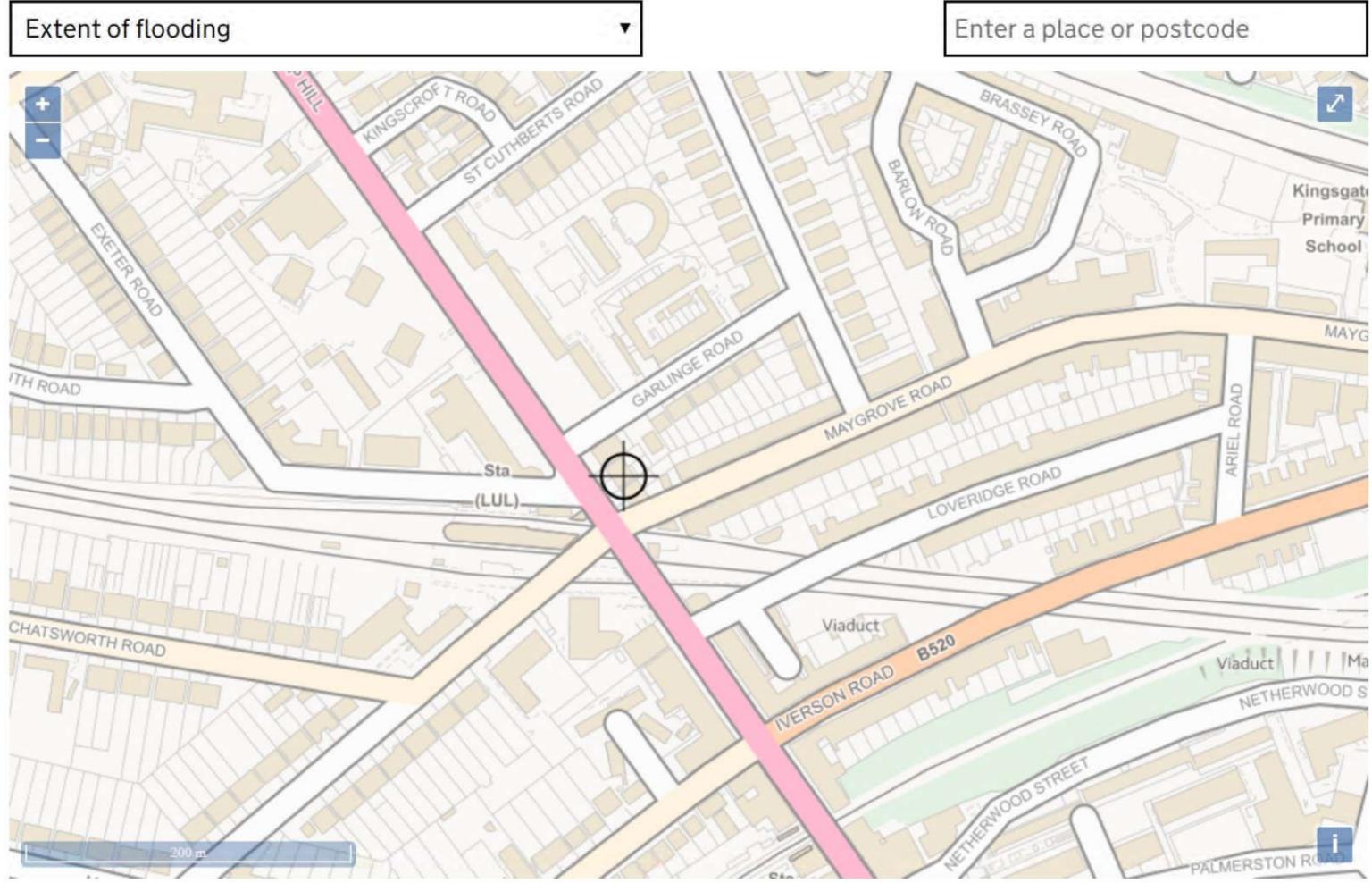
ater/Current Projects/47070547 Camden SFRA Update (ghost)/0700 WIP/0705 GIS_Data/01-WIP/01_03-Project_Files/W



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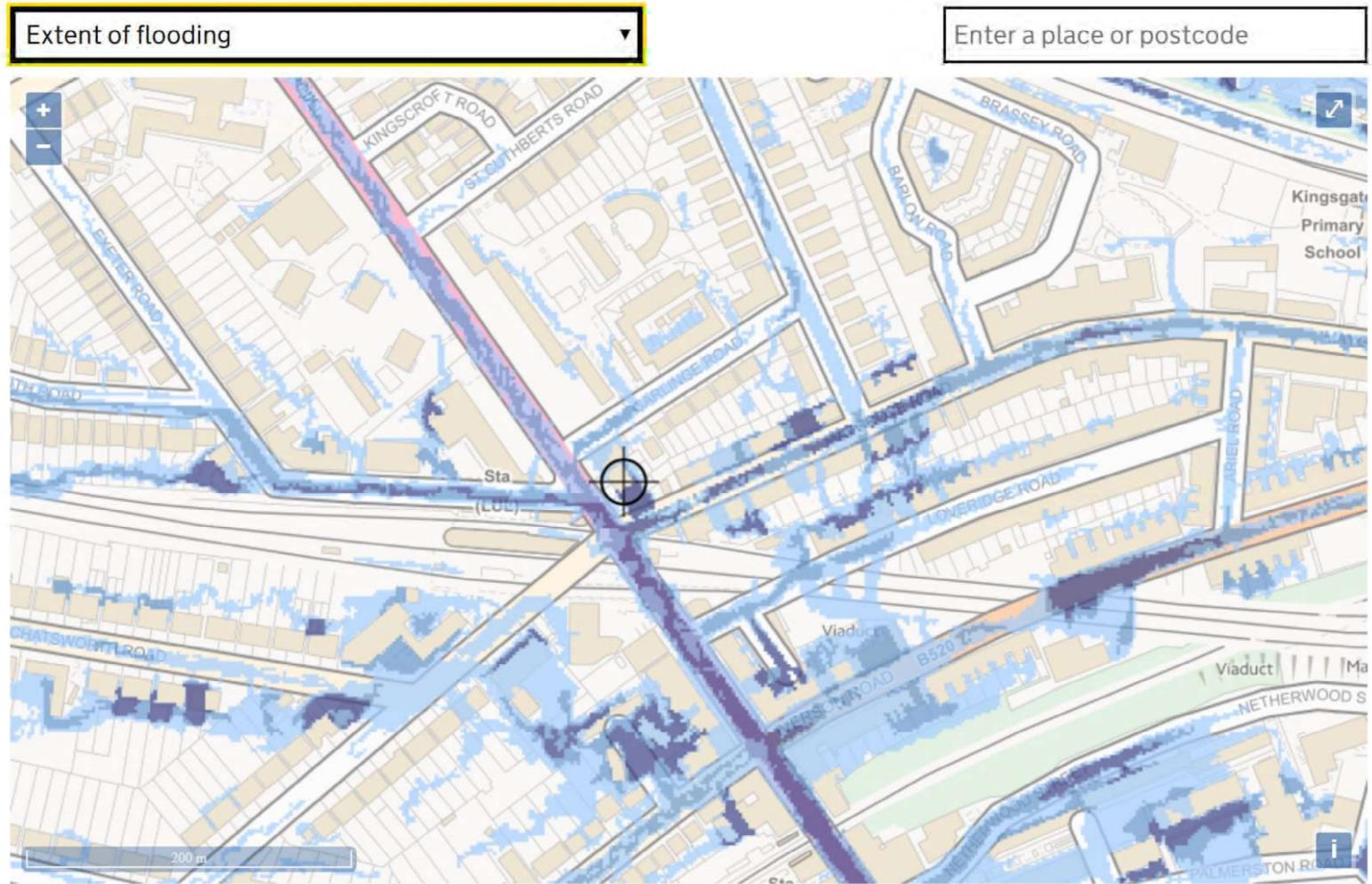


Appendix E – Gov.uk Flood Maps



Extent of flooding from rivers or the sea



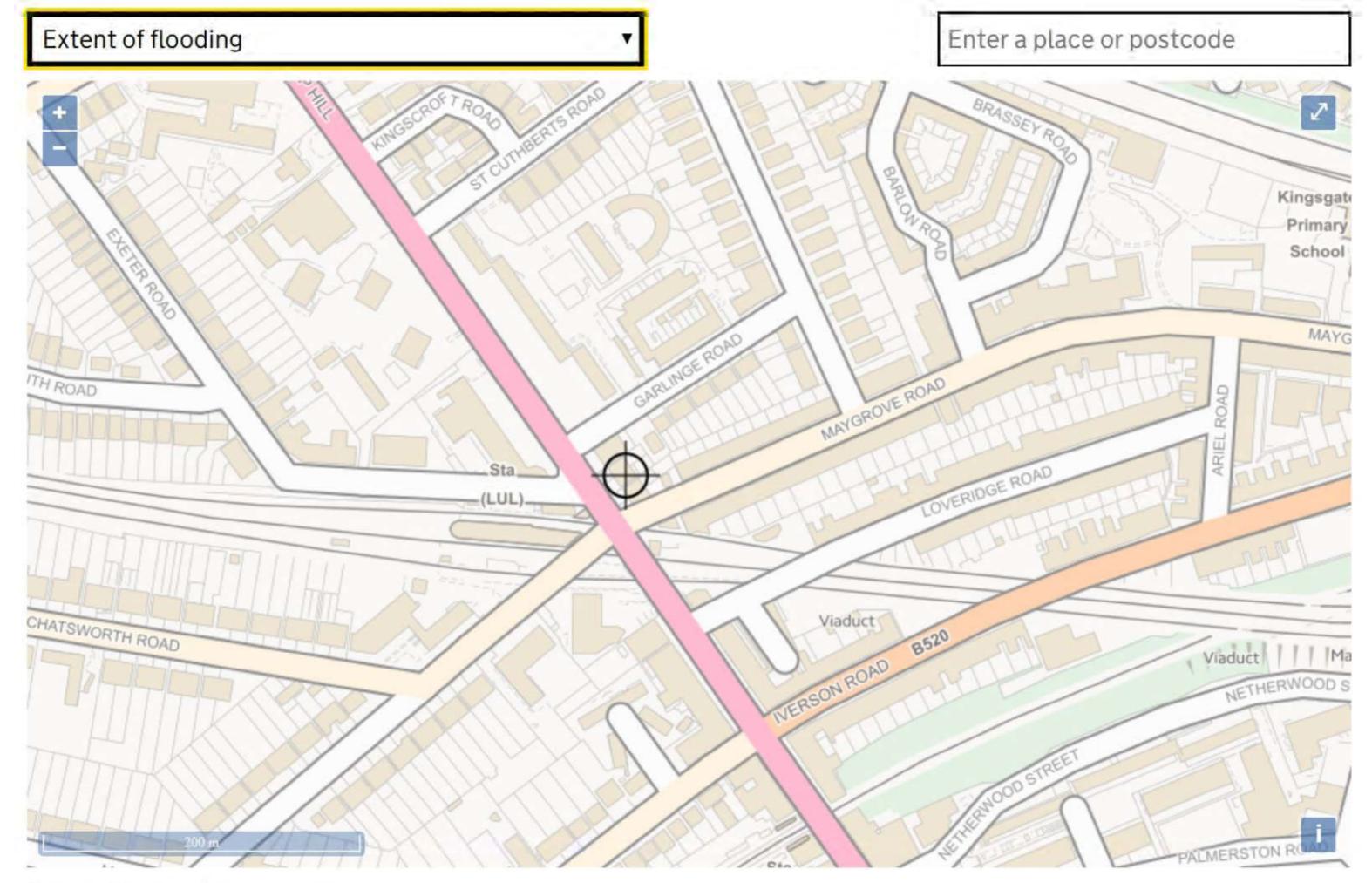


Extent of flooding from surface water



Very low

 \oplus Location you selected



Extent of flooding from reservoirs

Maximum extent of flooding \oplus Location you selected



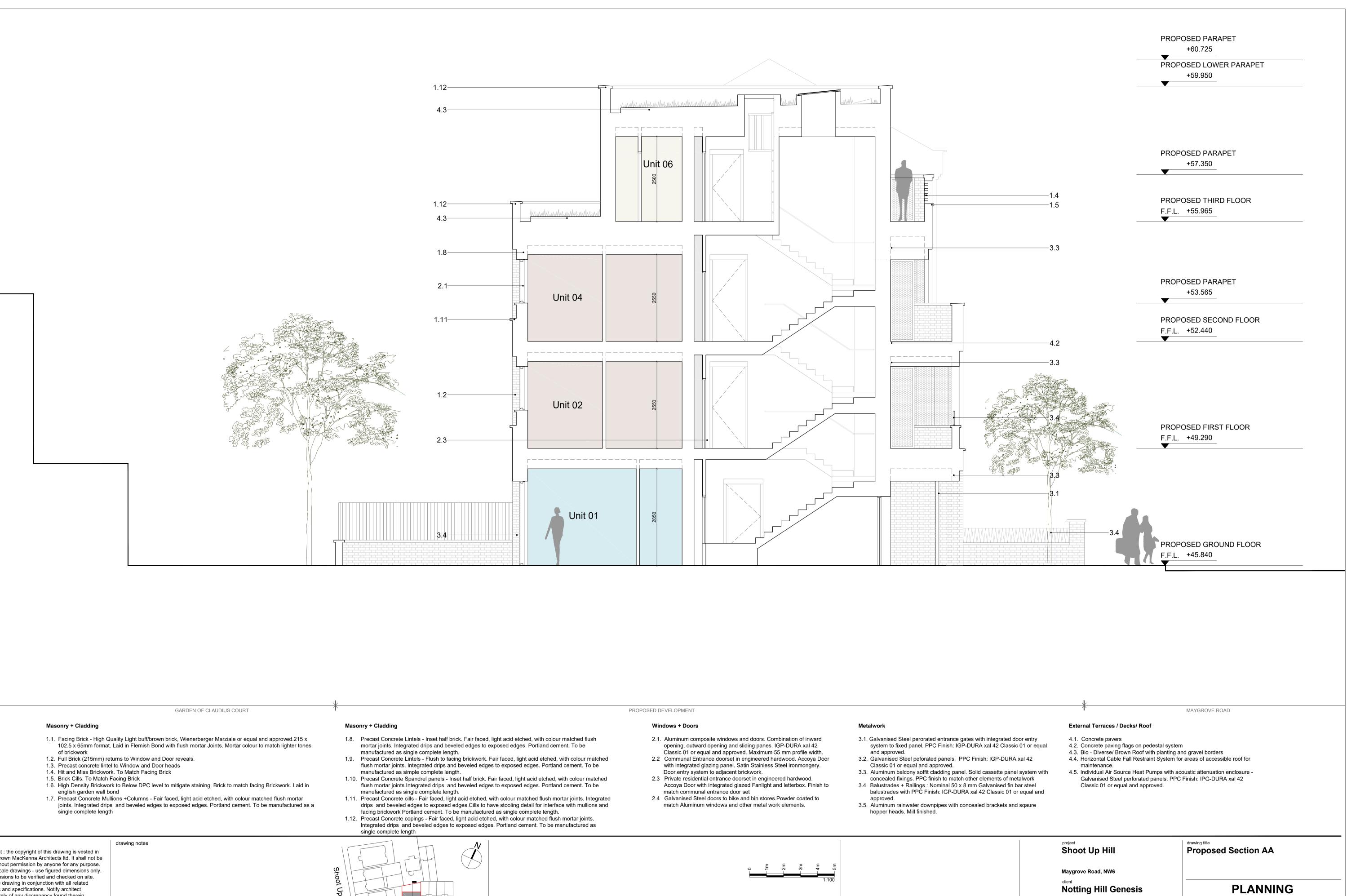
Appendix F – Development Proposals

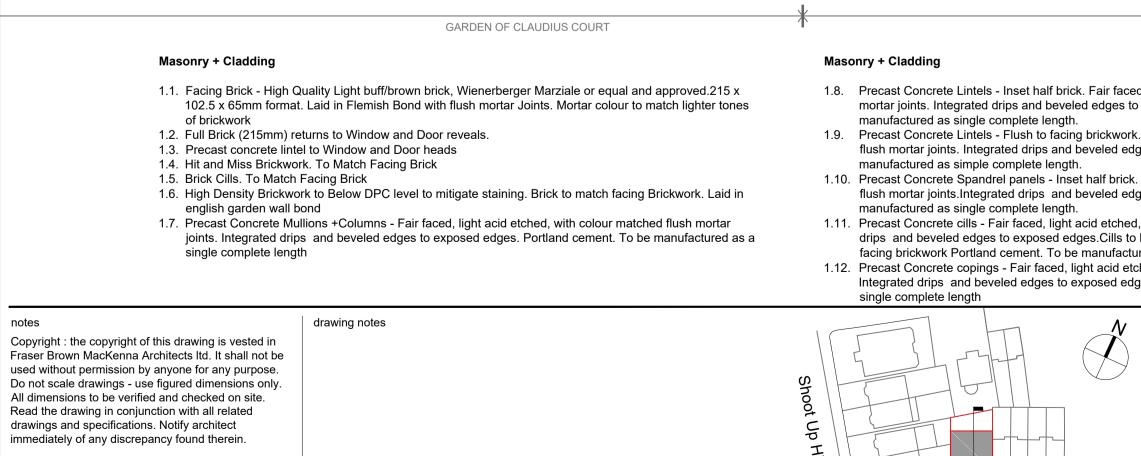


B FBM FBM 18.05.2021 Landscape layout updated A RDA SR 07.12.2020 Basement removed and layout modified	
REV BY CHKD DATE AMENDMENT DETAILS	REV BY CHKD DATE AMENDMENT DETAILS

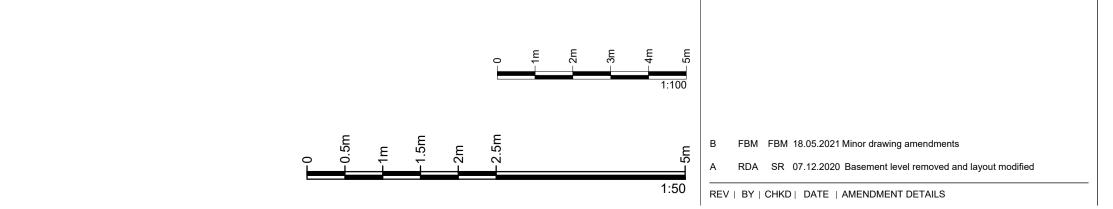


B FBM FBM 18.05.2021 Landscape Layout Updated	
A RDA SR 07.12.2020 Basement level removed and layout modified	
REV BY CHKD DATE AMENDMENT DETAILS	REV BY CHKD DATE AMENDMENT DETAILS





Maygrove Road



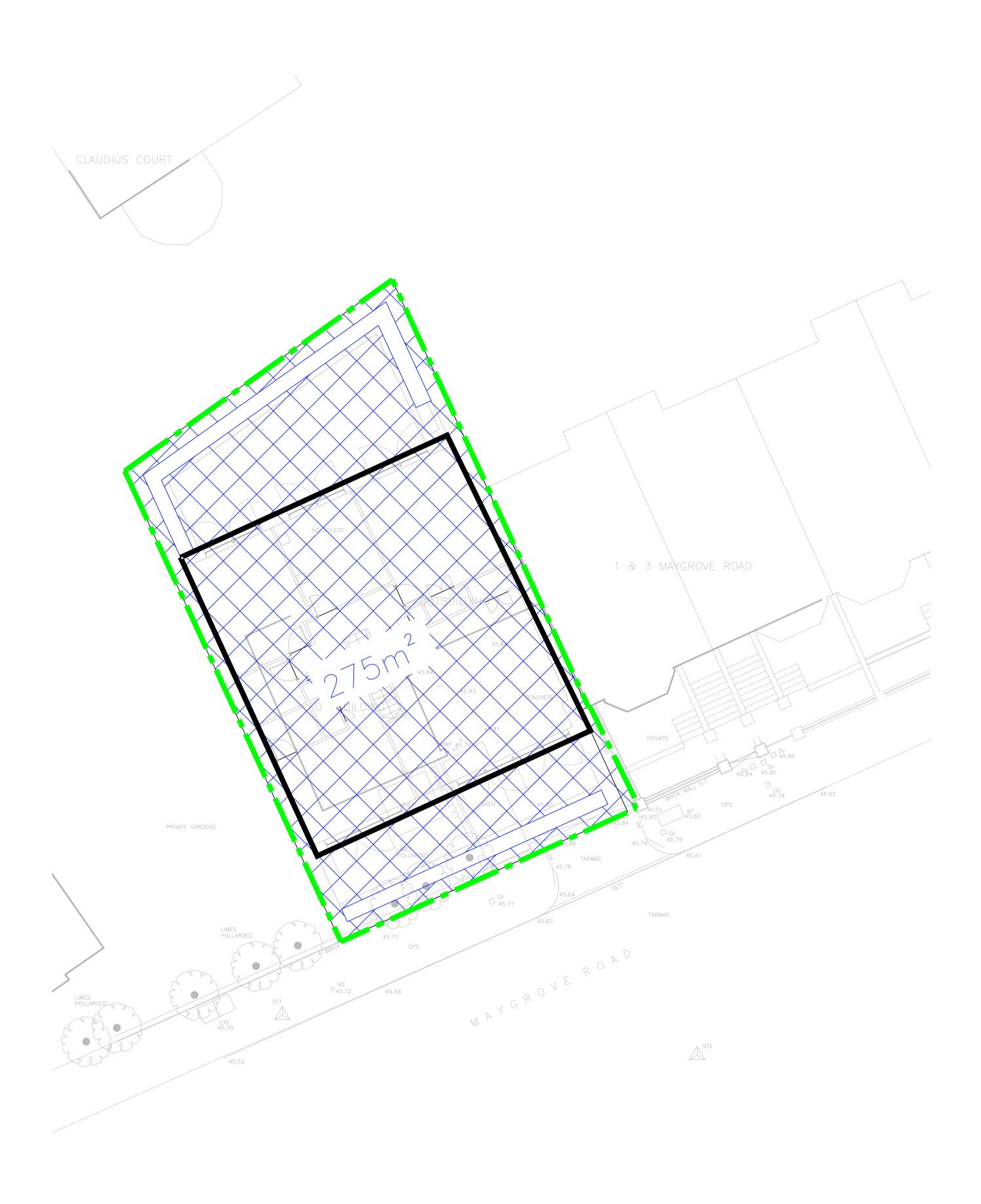
FraserBrownMacKennaArchitects 15-18 Featherstone St. London EC1Y 8SL www.fbmarchitects.com T:020 7251 0543

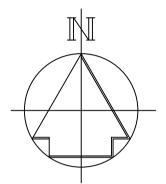
London Borough of Camden

scale drawn by 1:50@A1/1:100@A3 MW

DRAWING NUMBER

checked by FBM date ©04/02/2020 status 956 3101 B P





<u>LEGEND</u>

Site Boundary



Total Impermeable Area = 275m²

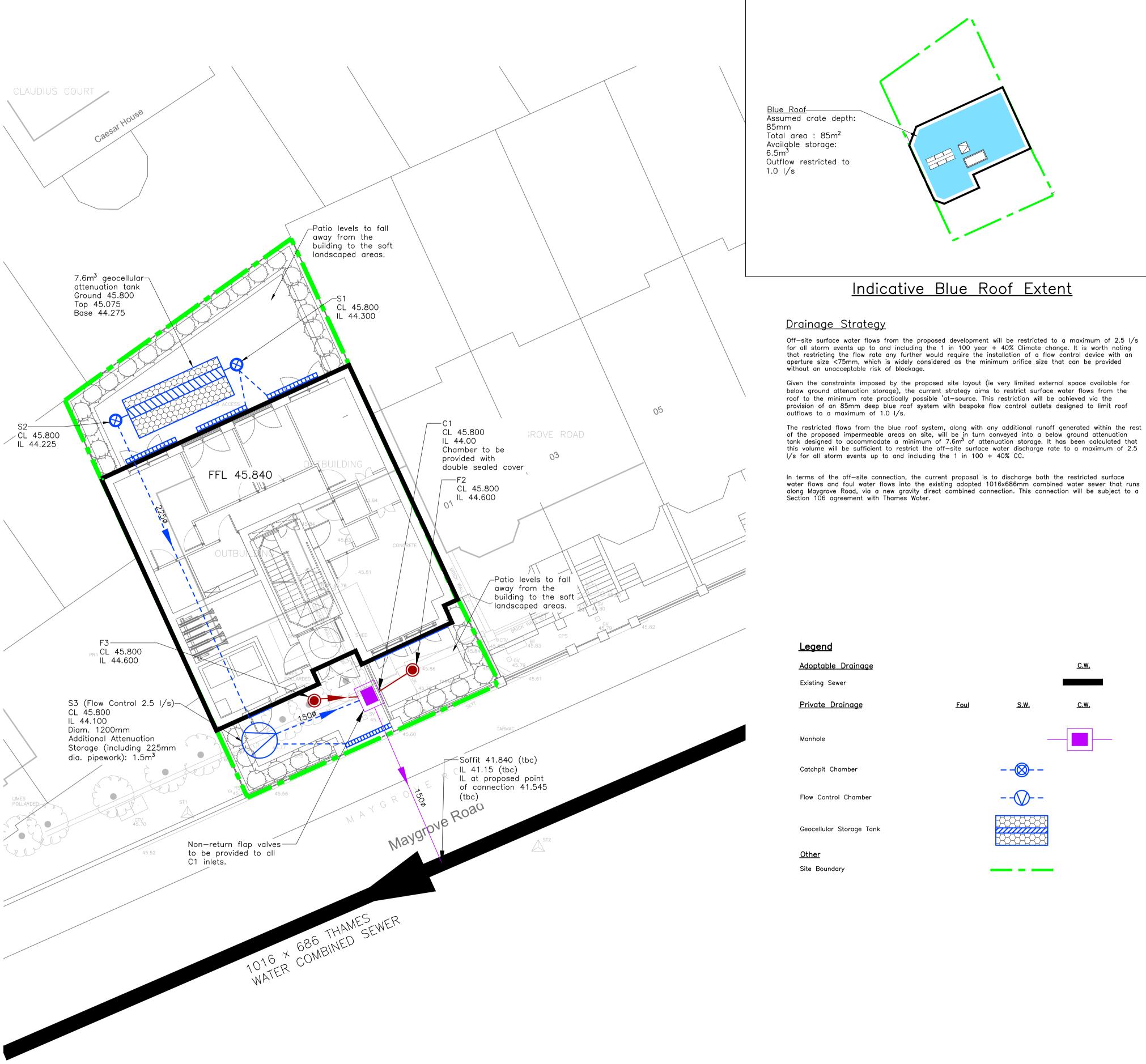
Impermeable Area

PRELIMINARY -FOR PLANNING





Appendix G – Indicative Drainage Strategy

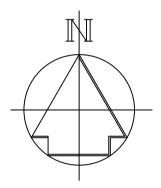


.

Off—site surface water flows from the proposed development will be restricted to a maximum of 2.5 I/s for all storm events up to and including the 1 in 100 year + 40% Climate change. It is worth noting that restricting the flow rate any further would require the installation of a flow control device with an aperture size <75mm, which is widely considered as the minimum orifice size that can be provided without an unacceptable risk of blockage.

Given the constraints imposed by the proposed site layout (ie very limited external space available for below ground attenuation storage), the current strategy aims to restrict surface water flows from the roof to the minimum rate practically possible 'at-source. This restriction will be achieved via the provision of an 85mm deep blue roof system with bespoke flow control outlets designed to limit roof outflows to a maximum of 1.0 I/s.

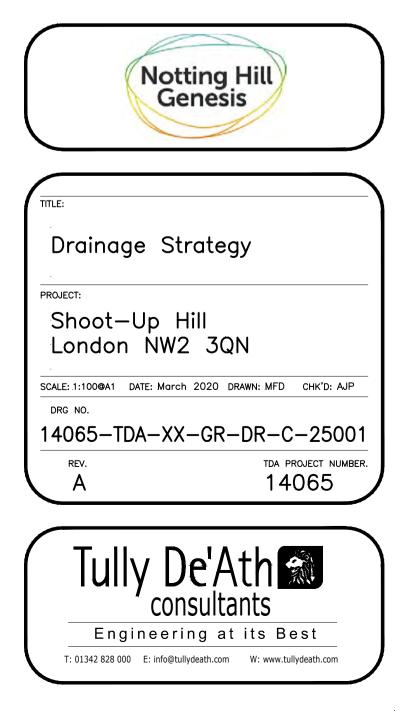
The restricted flows from the blue roof system, along with any additional runoff generated within the rest of the proposed impermeable areas on site, will be in turn conveyed into a below ground attenuation tank designed to accommodate a minimum of 7.6m³ of attenuation storage. It has been calculated that this volume will be sufficient to restrict the off—site surface water discharge rate to a maximum of 2.5 I/s for all storm events up to and including the 1 in 100 + 40% CC.



<u>General Notes</u>

PRELIMINARY -FOR PLANNING

A 10.03.21 Architect layout updated and drainage CH AJP strategy amended to suit. REV DATE DESCRIPTION BY CHK'D





Appendix H – Micro-Drainage Calculations

Tully De'Ath Ltd		Page 1
Sheridan House Hartfield Road		
Forest Row		The second
East Sussex RH18 5EA		Micro
Date 30/03/2020 17:17	Designed by chloh	Drainage
File Tank.SRCX	Checked by	Diamaye
XP Solutions	Source Control 2019.1	
XP Solutions	Source Control 2019.1	

ICP SUDS Mean Annual Flood

Input

Return Period (years) 100 SAAR (mm) 600 Urban 0.000 Area (ha) 0.029 Soil 0.300 Region Number Region 6

Results 1/s

QBAR Rural 0.0 QBAR Urban 0.0

Q100 years 0.1

Q1 year 0.0 Q30 years 0.1 Q100 years 0.1

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Tully De'Ath Ltd							Page 1
Sheridan House Hart	field Ro	ad Blue	e Roof				
Forest Row		Atte	enuatio	n			1
East Sussex RH18 5E	A						Mission
Date 10/03/2021 10:1		Des	igned b	V MED			— Micro
			-	-			Drainago
File Cascade - Rev A	CASX		cked by				
XP Solutions		Sou	rce Con	trol 2019	9.1		
Casaada	Gummaru	of Result	ta for	Plue Poot	F - Bou	A CDC	v
	<u>Summary</u>	OI Nesui	05 101	DIUE NOOI	L Kev	A. DIC	<u></u>
	Upstre Structu		flow To	Overflo	оw То		
	(Nc	one) Tank -	Rev A.SI	RCX (1	None)		
	Н	alf Drain T	'ime : 53	minutes.			
Storm	Max	Max N	lax	Max	Max	Max	Status
Event	Level I	Depth Infil		Control S	Outflow	Volume	
	(m)	(m) (]	l/s)	(1/s)	(l/s)	(m³)	
15 min Summe	r 49.552 (0.052	0.0	1.0	1.0	4.2	0 K
30 min Summe			0.0	1.0	1.0		
60 min Summe			0.0	1.0	1.0		
120 min Summe			0.0	1.0	1.0		
180 min Summe			0.0	1.0			
240 min Summe			0.0	1.0	1.0		
360 min Summe			0.0	1.0	1.0		
480 min Summe			0.0	1.0	1.0		
600 min Summe			0.0	1.0	1.0		
720 min Summe			0.0	1.0	1.0		
960 min Summe			0.0	1.0			
1440 min Summe			0.0	0.7	0.7		
2160 min Summe			0.0	0.5	0.5	0.8	0 K
2880 min Summe			0.0	0.4	0.4		
4320 min Summe				0.3			
	Storm	Rain	Flooded	Discharge	• Time-Pe	ak	
	Event	(mm/hr)	Volume	Volume	(mins)	
			(m³)	(m³)			
1	.5 min Sumr	mer 181.656	0.0	4.9)	17	
		mer 116.908				31	
	50 min Sumr					50	
	0 min Sumr					84	
	30 min Sumr					20	
	0 min Sumr					54	
	50 min Sumr					218	
	30 min Sumr					280	
	0 min Sumr					338	
	20 min Sumr					392	
	50 min Sumr					500	
	0 min Sumr					36	
	50 min Sumr					00	
	30 min Sumr					168	
288	80 min Sumr	mer 3.406	0.0	17.6	14	168	

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4320 min Summer 2.365 0.0 18.3 2184

Fully De'Ath Ltd							Page 2
Sheridan House Hartf	field Ro	ad	Blue Roof				
Forest Row			Attenuatio	n			1000
Last Sussex RH18 5EA	A						Mirror
Date 10/03/2021 10:18	2		Designed b	V MFD			- Micro
			-	-			Drain
File Cascade - Rev A.	CASX		Checked by				
KP Solutions			Source Con	trol 201	.9.1		
Cascade	Summary	of R	<u>esults for</u>	Blue Roc	of - Rev	A.SRC	X
Storm	Max	Max	Мах	Max	Max	Max	Status
Event	Level		Infiltration				Status
	(m)	(m)	(1/s)	(1/s)	(1/s)	(m ³)	
5760 min Summe	r 49.504	0.004	0.0	0.2	0.2	0.3	ОК
7200 min Summe	r 49.504	0.004	0.0	0.2	0.2	0.3	ОК
8640 min Summe	r 49.503	0.003	0.0	0.2	0.2	0.2	ΟK
10080 min Summe	r 49.503	0.003	0.0	0.1	0.1	0.2	O K
15 min Winte	r 49.552	0.052	0.0	1.0	1.0	4.2	ΟK
30 min Winte	r 49.562	0.062	0.0	1.0	1.0	5.0	ΟK
60 min Winte			0.0	1.0	1.0		
120 min Winte			0.0	1.0	1.0	5.4	
180 min Winte			0.0	1.0	1.0		
240 min Winte			0.0	1.0	1.0		
360 min Winte			0.0	1.0	1.0		
480 min Winte			0.0	1.0	1.0		
600 min Winte			0.0	1.0	1.0		
720 min Winte			0.0	0.9	0.9		
960 min Winte			0.0	0.7	0.7		
			0.0	0.5	0.5	0.8	
1440 min Winte							
1440 min Winte 2160 min Winte	r 49.507	0.007	0.0	0.3	0.3		
1440 min Winte	r 49.507 r 49.505	0.007 0.005	0.0		0.3 0.3 0.2	0.4	ОК

	Stor Even		Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)
5760	min	Summer	1.836	0.0	19.0	2936
7200	min	Summer	1.519	0.0	19.7	3592
8640	min	Summer	1.307	0.0	20.3	4408
10080	min	Summer	1.156	0.0	21.0	5120
15	min	Winter	181.656	0.0	4.9	17
30	min	Winter	116.908	0.0	6.3	30
60	min	Winter	71.589	0.0	7.7	52
120	min	Winter	46.272	0.0	10.0	90
180	min	Winter	35.217	0.0	11.4	128
240	min	Winter	28.709	0.0	12.4	162
360	min	Winter	21.137	0.0	13.7	228
480	min	Winter	16.763	0.0	14.4	282
600	min	Winter	13.911	0.0	15.0	326
720	min	Winter	11.902	0.0	15.4	384
960	min	Winter	9.254	0.0	15.9	500
1440	min	Winter	6.417	0.0	16.6	726
2160	min	Winter	4.428	0.0	17.2	1092
2880	min	Winter	3.406	0.0	17.6	1468
4320	min	Winter	2.365	0.0	18.4	2196
		C	1982-20	19 Inno	vyze	

Tully De'Ath Ltd		Page 3
Sheridan House Hartfield Road	Blue Roof	
Forest Row	Attenuation	Sec. and
East Sussex RH18 5EA		Micro
Date 10/03/2021 10:18	Designed by MFD	Drainage
File Cascade - Rev A.CASX	Checked by AJP	Diamage
XP Solutions	Source Control 2019.1	

Cascade Summary of Results for Blue Roof - Rev A.SRCX

Storm Event	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)			Max Volume (m³)	Status
5760 min Winter	49.503	0.003	0.0	0.1	0.1	0.2	ΟK
7200 min Winter	49.502	0.002	0.0	0.1	0.1	0.2	ОК
8640 min Winter	49.502	0.002	0.0	0.1	0.1	0.2	ОК
10080 min Winter	49.502	0.002	0.0	0.1	0.1	0.1	ОК

	torm vent	Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)
5760 r	min Winter	1.836	0.0	19.0	2952
7200 r	min Winter	1.519	0.0	19.7	3752
8640 r	min Winter	1.307	0.0	20.3	4720
10080 r	min Winter	1.156	0.0	21.0	5136

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Forest Row Attenuation Micro Cast Sussex RH18 5EA Designed by MFD File Cascade - Rev A.CASX Checked by AJP	Tully De'Ath Ltd			Page 4
Bast Sussex RH18 5EA Designed by MFD Checked by AJP Checked by AJP Cile Cascade - Rev A.CASX Checked by AJP CP Solutions Source Control 2019.1 Cascade Rainfall Details for Blue Roof - Rev A.SRCX Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version 2013 Site Location GB 524679 184670 TQ 24679 84670 Data Type Data Type Point Summer Storms Yes Winter Storms Yes Cv (Summer) 0.900 Cv (Winter) 0.900 Climate Change % +40 Time Area Diagram Total Area (ha) 0.012 Time (mins) Area From: To: (ha)	Sheridan House Hartfield Road	Blue Roof		
Date 10/03/2021 10:18 Pile Cascade - Rev A.CASX Checked by AJP Source Control 2019.1 Cascade Rainfall Details for Blue Roof - Rev A.SRCX Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version 2013 Site Location GB 524679 184670 TQ 24679 84670 Data Type Point Summer Storms Yes Cv (Summer) 0.900 Cv (Winter) 0.900 Shortest Storm (mins) 10080 Climate Change % +40 Time Area Diagram Total Area (ha) 0.012 Time (mins) Area From: To: (ha)	Forest Row	Attenuation		Section and
Date 10/03/2021 10:18 Pile Cascade - Rev A.CASX Checked by AJP Source Control 2019.1 Cascade Rainfall Details for Blue Roof - Rev A.SRCX Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version 2013 Site Location GB 524679 184670 TQ 24679 84670 Data Type Point Summer Storms Yes Cv (Summer) 0.900 Cv (Winter) 0.900 Shortest Storm (mins) 10080 Climate Change % +40 Time Area Diagram Total Area (ha) 0.012 Time (mins) Area From: To: (ha)	East Sussex RH18 5EA			Mirco
Prile Cascade - Rev A.CASX Checked by AJP Source Control 2019.1 Cascade Rainfall Details for Blue Roof - Rev A.SRCX Rainfall Model Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version 2013 Site Location GB 524679 184670 TQ 24679 84670 Data Type Data Type Point Summer Storms Yes Winter Storms Yes Cv (Summer) 0.900 CV (Winter) 0.900 Shortest Storm (mins) 15 Longest Storm (mins) 10080 Climate Change % +40 Time Area Diagram Total Area (ha) 0.012 Time (mins) Area From: To: To: Time (mins) Area		Designed by MFD		
If the Calcolate Dynamic Difference Dynamic Difference Dynamic Difference Dynamic RP Solutions Source Control 2019.1 Cascade Rainfall Details for Blue Roof - Rev A.SRCX Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version 2013 Site Location GB 524679 184670 TQ 24679 84670 Data Type Data Type Point Summer Storms Yes Winter Storms Yes Winter Storms Yes Cv (Winter) 0.900 Cv (Winter) 0.900 Shortest Storm (mins) 15 Longest Storm (mins) 10080 Climate Change % +40 Time Area Diagram Total Area (ha) 0.012 Time (mins) Area From: To: (ha)				Drainage
Cascade Rainfall Details for Blue Roof - Rev A.SRCX Rainfall Model FEH Return Period (years) 100 FEH Rainfall Version Summer Storm GB 524679 184670 TQ 24679 84670 Data Type Doint Summer Storms Yes Winter Storms CV (Summer) O.900 CV (Summer) O.900 CV (Winter) O.900 Climate Change % Hotal Area Diagram Total Area (ha) 0.012 Time (mins) Area From: To: (ha)				
Rainfall ModelFEHReturn Period (years)100FEH Rainfall Version2013Site Location GB 524679 184670 TQ 24679 84670Data TypeData TypePointSummer StormsYesWinter StormsYesCv (Summer)0.900Cv (Winter)0.900Shortest Storm (mins)15Longest Storm (mins)10080Climate Change %+40Time Area DiagramTotal Area (ha) 0.012Time (mins) AreaFrom: To:(ha)	XP Solutions	Source Control 2019.1		
	Rainfall Mo Return Period (yea FEH Rainfall Vers Site Locat Data T Summer Sto Winter Sto Cv (Summ Cv (Wint Shortest Storm (mi Longest Storm (mi Climate Chang Ti	etails for Blue Roof - Ro del rs) ion ion GB 524679 184670 TQ 24679 ype rms rms er) er) ns) re % ime Area Diagram etal Area (ha) 0.012 Time (mins) Area From: To: (ha)	FEH 100 2013 Ø 84670 Point Yes Yes 0.900 0.900 15 10080	
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Tully De'Ath Ltd		Page 5
Sheridan House Hartfield Road	Blue Roof	
Forest Row	Attenuation	100 A
East Sussex RH18 5EA		Mirco
Date 10/03/2021 10:18	Designed by MFD	
File Cascade - Rev A.CASX	Checked by AJP	Drainage
XP Solutions	Source Control 2019.1	
Storage is (cails for Blue Roof - Rev A. Online Cover Level (m) 50.000 Lar Storage Structure	SRCX
Infiltration Coefficien Infiltration Coefficien	t Side (m/hr) 0.00000	ity 0.95
Depth (m) Area (m²) Inf. A	area (m²) Depth (m) Area (m²) Inf	. Area (m²)
0.000 85.0 0.085 85.0	85.0 0.086 0.0 88.1	88.2
Deptn/Flow R	<u>elationship Outflow Control</u>	
Inv	vert Level (m) 49.500	
Depth (m) Flow (1/s) Depth	epth (m) Flow (1/s) Depth (m) Fl	ow (1/s)
0.010 0.5000	0.020 1.0000 0.800	1 0000
0.010 0.0000	0.020 1.0000 0.000	1.0000
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Tully De'Ath Ltd		Page 1
Sheridan House Hartfield Road	Below Ground	
Forest Row	Attenuation Tank	Sec. Sec.
East Sussex RH18 5EA		Mirco
Date 10/03/2021 10:17	Designed by MFD	Desinado
File Cascade - Rev A.CASX	Checked by AJP	Diamaye
XP Solutions	Source Control 2019.1	

Cascade Summary of Results for Tank - Rev A.SRCX

Upstream Outflow To Overflow To Structures

Blue Roof - Rev A.SRCX (None) (None)

Half Drain Time : 24 minutes.

	Storr Event		Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control (1/s)	Max Σ Outflow (1/s)	Max Volume (m³)	Status
15	min S	Summer	44.842	0.567	0.0	2.5	2.5	5.4	ОК
30	min S	Summer	44.921	0.646	0.0	2.5	2.5	6.1	ОК
60	min S	Summer	44.925	0.650	0.0	2.5	2.5	6.2	ОК
120	min S	Summer	44.952	0.677	0.0	2.5	2.5	6.4	ОК
180	min S	Summer	44.929	0.654	0.0	2.5	2.5	6.2	ОК
240	min S	Summer	44.883	0.608	0.0	2.5	2.5	5.8	ОК
360	min S	Summer	44.758	0.483	0.0	2.5	2.5	4.6	ОК
480	min S	Summer	44.568	0.293	0.0	2.5	2.5	2.8	ОК
600	min S	Summer	44.447	0.172	0.0	2.5	2.5	1.6	ОК
720	min S	Summer	44.367	0.092	0.0	2.5	2.5	0.9	ОК
960	min S	Summer	44.281	0.006	0.0	2.4	2.4	0.1	ОК
1440	min S	Summer	44.275	0.000	0.0	1.8	1.8	0.0	ОК
2160	min S	Summer	44.275	0.000	0.0	1.3	1.3	0.0	ОК
2880	min S	Summer	44.275	0.000	0.0	1.0	1.0	0.0	ОК
4320	min S	Summer	44.275	0.000	0.0	0.7	0.7	0.0	O K

	Storm Event		Rain (mm/hr)		Discharge Volume (m³)		
15	min	Summer	181.656	0.0	11.8	17	
30	min	Summer	116.908	0.0	15.2	31	
60	min	Summer	71.589	0.0	18.7	52	
120	min	Summer	46.272	0.0	24.1	86	
180	min	Summer	35.217	0.0	27.6	120	
240	min	Summer	28.709	0.0	29.8	156	
360	min	Summer	21.137	0.0	33.0	228	
480	min	Summer	16.763	0.0	34.9	280	
600	min	Summer	13.911	0.0	36.3	334	
720	min	Summer	11.902	0.0	37.3	390	
960	min	Summer	9.254	0.0	38.6	492	
1440	min	Summer	6.417	0.0	40.2	0	
2160	min	Summer	4.428	0.0	41.6	0	
2880	min	Summer	3.406	0.0	42.6	0	
4320	min	Summer	2.365	0.0	44.4	0	
			1000 00	10 -			
		C	1982-20	19 Inno	ovyze		

Tully De'Ath Ltd		Page 2
Sheridan House Hartfield Road	Below Ground	
Forest Row	Attenuation Tank	The second
East Sussex RH18 5EA		Mirco
Date 10/03/2021 10:17	Designed by MFD	Drainage
File Cascade - Rev A.CASX	Checked by AJP	Diamaye
XP Solutions	Source Control 2019.1	

	Stor: Even		Max Level	Max Depth	Max Infiltration	Max Control	Max Σ Outflow	Max Volume	Status
			(m)	(m)	(1/s)	(1/s)	(1/s)	(m³)	
5760	min	Summer	44.275	0.000	0.0	0.5	0.5	0.0	ОК
7200	min	Summer	44.275	0.000	0.0	0.4	0.4	0.0	ΟK
8640	min	Summer	44.275	0.000	0.0	0.4	0.4	0.0	ΟK
10080	min	Summer	44.275	0.000	0.0	0.3	0.3	0.0	ΟK
15	min	Winter	44.845	0.570	0.0	2.5	2.5	5.4	ΟK
30	min	Winter	44.928	0.653	0.0	2.5	2.5	6.2	ΟK
60	min	Winter	44.927	0.652	0.0	2.5	2.5	6.2	ΟK
120	min	Winter	44.931	0.656	0.0	2.5	2.5	6.2	ΟK
180	min	Winter	44.875	0.600	0.0	2.5	2.5	5.7	ΟK
240	min	Winter	44.789	0.514	0.0	2.5	2.5	4.9	ΟK
360	min	Winter	44.524	0.249	0.0	2.5	2.5	2.4	ΟK
480	min	Winter	44.363	0.088	0.0	2.5	2.5	0.8	ΟK
600	min	Winter	44.282	0.007	0.0	2.4	2.4	0.1	ΟK
			44.275		0.0		2.1	0.0	ΟK
			44.275		0.0		1.7		
			44.275		0.0				
			44.275		0.0	0.8	0.8		
			44.275		0.0		0.6		
4320	min	Winter	44.275	0.000	0.0	0.4	0.4	0.0	ΟK

	Storm Event	Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)	
5760	min Summer	1.836	0.0	46.0	0	
7200	min Summer	1.519	0.0	47.6	0	
8640	min Summer	1.307	0.0	49.1	0	
10080	min Summer	1.156	0.0	50.7	0	
15	min Winter	181.656	0.0	11.8	17	
30	min Winter	116.908	0.0	15.2	31	
60	min Winter	71.589	0.0	18.7	56	
120	min Winter	46.272	0.0	24.0	90	
180	min Winter	35.217	0.0	27.5	130	
240	min Winter	28.709	0.0	30.0	170	
360	min Winter	21.137	0.0	33.0	226	
480	min Winter	16.763	0.0	35.0	276	
600	min Winter	13.911	0.0	36.3	322	
720	min Winter	11.902	0.0	37.2	0	
960	min Winter	9.254	0.0	38.6	0	
1440	min Winter	6.417	0.0	40.2	0	
2160	min Winter	4.428	0.0	41.6	0	
2880	min Winter	3.406	0.0	42.6	0	
4320	min Winter	2.365	0.0	44.4	0	
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Tully De'Ath Ltd		Page 3
Sheridan House Hartfield Road	Below Ground	
Forest Row	Attenuation Tank	Sec. 1
East Sussex RH18 5EA		Mirco
Date 10/03/2021 10:17	Designed by MFD	Drainage
File Cascade - Rev A.CASX	Checked by AJP	Diamaye
XP Solutions	Source Control 2019.1	

Cascade Summary of Results for Tank - Rev A.SRCX

Storm Event	Max Level (m)	Max Depth (m)	Max Infiltration (l/s)	Max Control Σ (l/s)	Max Outflow (l/s)		Status
5760 min Winter	44.275	0.000	0.0	0.3	0.3	0.0	ОК
7200 min Winter	44.275	0.000	0.0	0.3	0.3	0.0	ОК
8640 min Winter	44.275	0.000	0.0	0.3	0.3	0.0	ОК
10080 min Winter	44.275	0.000	0.0	0.2	0.2	0.0	ОК

Stor Even		Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)
5760 min	Winter	1.836	0.0	46.0	0
7200 min	Winter	1.519	0.0	47.6	0
8640 min	Winter	1.307	0.0	49.1	0
10080 min	Winter	1.156	0.0	50.7	0

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Tully De'Ath Ltd			Page 4
Sheridan House Hartfield Road	Below Ground		
Forest Row	Attenuation Tank		1
East Sussex RH18 5EA			
			Micro
Date 10/03/2021 10:17	Designed by MFD		Drainage
File Cascade - Rev A.CASX	Checked by AJP		Brainage
XP Solutions	Source Control 201	9.1	
<u>Cascade Rainfall</u>	Details for Tank -	<u>Rev A.SRCX</u>	
Rainfall Mo	dol	FEH	
Return Period (yea		100	
FEH Rainfall Vers		2013	
	ion GB 524679 184670 TQ		
Data T		240/9 840/0 Point	
Summer Sto		Yes	
Winter Sto		Yes	
Cv (Summ		0.900	
Cv (Summ Cv (Wint		0.900	
CV (Wint Shortest Storm (mi		15	
Longest Storm (mi		10080	
Climate Chang		+40	
		+40	
<u>T:</u>	ime Area Diagram		
То	tal Area (ha) 0.017		
	Time (mins) Area From: To: (ha)		
	0 4 0.017		
<u></u>	292 - 2010 Transmission		
©19	982-2019 Innovyze		

Tully De'Ath Ltd						Page 5
Sheridan House Hartf	ield Road	d Below	Ground			
Forest Row		Atten	uation Tan	k		Sec. 1
East Sussex RH18 5EA						Micro
Date 10/03/2021 10:17		Desig	ned by MFD			
File Cascade - Rev A.	CASX	Check	ed by AJP			Drainage
XP Solutions		Sourc	e Control	2019.1		
Infiltrati	Storage : <u>Cel</u> on Coeffic	is Online Co <u>lular Stor</u> Invert Level Sient Base (r	for Tank over Level (r age Struct (m) 44.27 n/hr) 0.0000 n/hr) 0.0000	n) 45.875 <u>cure</u> 5 Safety F 0 Por		
Depth (m) Are	a (m²) Inf	. Area (m²)	Depth (m) A	Area (m²)]	Inf. Area	(m²)
0.000 0.800	10.0 10.0	10.0 20.1	0.801	0.0	2	20.1
	<u>Hydro-Br</u>	<u>ake® Optim</u>	um Outflow	<u>v Control</u>		
	De. I: Dutlet Pip	Design Head sign Flow (1 Flush-F Object Applicat Sump Availa Diameter (nvert Level e Diameter (e Diameter (/s) lo™ ive Minimis ion ble mm) (m) mm)		0.975 2.5 alculated n storage Surface Yes 76 44.100 100 1200	
Control Points	Head (m)	Flow (l/s)	Contro	ol Points	Head	(m) Flow (l/s)
Design Point (Calculated) Flush-Flo ¹			Mean Flow o		Flo® 0. ange	.610 2.0 - 2.2
The hydrological calcul Hydro-Brake® Optimum as Hydro-Brake Optimum® be	specified utilised	l. Should an then these a	nother type storage rout.	of control ing calcul	device ot ations wil	her than a l be invalidated
Depth (m) Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m) F	[low (l/s)	Depth (m)	Flow (l/s)
0.100 2.1	1.200		3.000	4.2	7.000	6.2
0.200 2.4 0.300 2.5	1.400		3.500 4.000	4.5 4.8	7.500 8.000	6.5 6.7
0.300 2.5				4.8 5.1	8.000	6.8
0.400 2.5				5.3	9.000	7.0
0.500 2.3				5.6	9.000	7.0
0.800 2.3				5.8	5.000	1.2
1.000 2.5				6.0		
		©1982-201	9 Innovyze			



Appendix I – London Borough of Camden SuDS Pro-Forma



GREATER LONDON AUTHORITY



	Project / Site Name (including sub- catchment / stage / phase where appropriate)	- 2a Shoot-Up Hill		
	Address & post code	2a Shoot-Up Hill, London NW2 3QN		
	OC Cridnet (Festing Northing)	E 524663		
	OS Grid ref. (Easting, Northing)	N 184685		
tails	LPA reference (if applicable)			
1. Project & Site Details	Brief description of proposed work	The proposed development will provide 6 flats within a four-storey block, which includes a lower ground floor level covering the whole site. Terrace areas are proposed at this lower ground floor level to the front and back of the		
• •	Total site Area	290 m ²		
	Total existing impervious area	140 m ²		
	Total proposed impervious area	275 m ²		
	Is the site in a surface water flood risk catchment (ref. local Surface Water Management Plan)?	Yes		
	Existing drainage connection type and location	RWP and gulies are noted on the site but no drainage survey undertaken		
	Designer Name	Martin Deus		
	Designer Position	Civil Engineer		
	Designer Company	Tully De'Ath		

	2a. Infiltration Feasibility				
	Superficial geology classification	n/a			
	Bedrock geology classification		London Clay		
	Site infiltration rate	N/A	m/s		
	Depth to groundwater level	>19	m belo	w ground level	
	Is infiltration feasible?		No		
	2b. Drainage Hierarchy				
ements		Feasible (Y/N)	Proposed (Y/N)		
ang	1 store rainwater for later use	Ν	Ν		
ırge Arr	2 use infiltration techniques, such surfaces in non-clay areas	as porous	Ν	Ν	
2. Proposed Discharge Arrangements	3 attenuate rainwater in ponds or features for gradual release	open water	Ν	Ν	
ropose	4 attenuate rainwater by storing ir sealed water features for gradual results.		Y	Y	
2. P	5 discharge rainwater direct to a w	atercourse	Ν	Ν	
	6 discharge rainwater to a surface sewer/drain	water	Ν	Ν	
	7 discharge rainwater to the comb	Y	Y		
	2c. Proposed Discharge Details				
	Proposed discharge location	Adopted com	bined sewer in	Maygrove Rd.	
	Has the owner/regulator of the discharge location been consulted?	To be consul	sulted at detailed design stage		



GREATER LONDON AUTHORITY



	3a. Discharge Rat	tes & Required Ste	orage			
		Greenfield (GF) runoff rate (l/s)	Existing discharge rate (I/s)	Required storage for GF rate (m ³)	Proposed discharge rate (l/s)	
	Qbar	<0.1	\ge	\geq	\geq	
	1 in 1	<0.1	2	n/a	2.5	
	1 in 30	0.1	4.4	n/a	2.5	
	1 in 100	0.1	5.6	n/a	2.5	
	1 in 100 + CC	\searrow	\geq	13.2	2.5	
	Climate change a	llowance used	40%			
3. Drainage Strategy	3b. Principal Met Control	hod of Flow	Vortex Flow Control Device			
e St	3c. Proposed Sul	S Measures				
inag			Catchment	Plan area	Storage	
Dra			area (m²)	(m ²)	vol. (m ³)	
ы.	Rainwater harves	ting	0	\geq	0	
	Infiltration systen	ns	0	\geq	0	
	Green roofs		119	119	0	
	Blue roofs		115	85	6.5	
	Filter strips		0	0	0	
	Filter drains		0	0	0	
	Bioretention / tre		0	0	0	
	Pervious paveme	nts	0	0	0	
	Swales		0	0	0	
	Basins/ponds		0	0	0	
	Attenuation tanks	S	275	204	7.6	
	Total		509	204	14.1	

	A. Dischause & Dusing as Church	During (a setting of sharing and		
	4a. Discharge & Drainage Strategy	Page/section of drainage report		
	Infiltration feasibility (2a) – geotechnical factual and interpretive reports, including infiltration results	Section 3.4		
	Drainage hierarchy (2b)	Chapter 7		
u	Proposed discharge details (2c) – utility plans, correspondence / approval from owner/regulator of discharge location	Section 8.4 and Appendix C		
4. Supporting Information	Discharge rates & storage (3a) – detailed hydrologic and hydraulic calculations	Section 8.5 and Appendix H		
ting Inf	Proposed SuDS measures & specifications (3b)	Chapter 7		
bol	4b. Other Supporting Details	Page/section of drainage report		
Sup	Detailed Development Layout	Appendix F		
4.	Detailed drainage design drawings, including exceedance flow routes	Appendix G		
	Detailed landscaping plans	Appendix F		
	Maintenance strategy	Chapter 10 & Appendix J		
	Demonstration of how the proposed SuDS measures improve:			
	a) water quality of the runoff?	Section 7.3		
	b) biodiversity?	Section 7.3		
	c) amenity?	Section 7.3		



Appendix J – Detailed Maintenance Schedules

SuDS Maintenance Schedule

Item	Task	Frequency	Location	Access	Comments		
Main Drainage N	Main Drainage Network						
Rainwater downpipes	Clean out at roof level and ground level	Twice yearly for the first 2 years of operation then annually	Roof level, around building perimeter and internal system suspended beneath first floor slab and ground floor slab	High level access required to roof outlets. Communal hard and soft landscaping	Works undertaken by appropriately qualified person(s).		
Chambers, silt- traps & catchpits	Clean out chamber/sump				For RWP outlets at roof level follow health &		
Pipe network & drainage channels	Pipes to be inspected and condition assessed. Pipes/channels to be cleaned (jetted) as necessary		Outside building	Communal hard and soft landscaping	safety regulations dealing with working at height		

Flow Control Devices						
Hydrobrake chambers	Clean out chamber/sump	Monthly for first 3 months then twice yearly	Front garden	Communal hard landscaped area.	Works undertaken by appropriately qualified person(s)	
	Inspect flow control unit and remove debris					

Geocellular Attenuation Tanks					
Upstream & downstream catchpit chambers	Clean out chamber/sump	Twice yearly for the first 2 years of operation then annually	Rear communal	Rear Communal	Works undertaken by appropriately
Inlets, outlets, vents and overflows	Inspect/check to ensure in good condition and correct operation	Annually and after large storms			
Geocellular units	CCTV inspection. Clean (jet) if required	5 Years or if excessive silt/debris observed in upstream & downstream catchpit chambers	garden	garden	qualified person(s)

Item	Task	Frequency	Location	Access	Comments		
Biodiverse & Blu	Biodiverse & Blue Roofs						
Generally	Inspect all components including soil substrate, inlet/outlets, fire breaks, underside of roof for structural integrity & signs of leakage. Remove litter/debris.	Monthly for first 12 months then annually or after severe storms	Biodiverse roof: All roof areas	High level	Works undertaken by appropriately qualified person(s)		
Biodiverse areas/planting/shr ubs/trees	Pruning, remove cuttings/debris/fall en leaves, weeding, remove invasive species, replace dead plants	Monthly for first 12 months every 6 months or as required					
Grassed areas	Mowing, remove debris/cuttings	Fortnightly or monthly as appropriate during growing season.	Blue roof: Higher level roof	access to roof	following health & safety regulations dealing with working at height		
Hard landscaped areas (Resin bound gravel e.g. Addaset, Addabound or Terrabound by Addagrip)	Remove organic matter from surface (with brush and suction cleaner)	Monthly for first 3 months then twice yearly (in spring and autumn)			noight		
Roof outlets	Clean out, inspect, remove plant growth	Monthly for first 12 months every 6 months or as required and always after severe storms					

Feasibility Research

EIA, Flood Risk & **Transportation** Assessment

Urban Planning and **Design**

Integrated Transport Solutions

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Structural Design

Eco and MMC **Focused**

Tully De'Ath offers a range of excellent design services to a wide client base. If you want to find out more about the services we offer, please contact your nearest office on the details below.



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