

Appendix 10

Flood Risk Assessment and SuDS Strategy

Transformation of the Ugly Brown Building

GD Partnership LTD Flood Risk Assessment and SUDS Strategy

August 2017



TRANSFORMATION OF THE UGLY BROWN BUILDING, CAMDEN FLOOD RISK ASSESSMENT AND SUDS STRATEGY

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CONTENTS

Exe	cutive Summaryv
1.	Introduction1Application History1General Information1Scope of Study2
2.	Site Description3Location3Existing Development3Topographic Survey and Site History4Proposed Development5
3.	National and Local Planning Policy7National Planning Policy Framework7The London Plan7Local Planning Policy7Camden Local Plan (2017)8Camden Strategic Flood Risk Assessment9Sequential Test9
4.	Potential Flooding On Site10Flooding from Rivers and the Sea10Flooding from Surface Water10Flooding from Sewers11Flooding from Groundwater12Flooding from Artificial Sources13Flood Warning and Emergency Access/Egress14Climate Change14
5.	Surface Water Management15Existing Site Runoff15Greenfield Runoff16Existing Site Drainage16Proposed Surface Water Drainage System16Sustainable Drainage Systems (SuDS)19SuDS Management and Maintenance21



Flood Risk Assessment and SuDS Strategy

6.	Summary of Flood Risk Assessment	22
7.	Conclusions	26
Appe	ndix A - Drawings	27
Арре	ndix B - Thames Water Asset Search	28
Арре	ndix C - Calculation Sheets	29
Арре	ndix D - Camden SuDS Pro-Forma	30

LIST OF FIGURES

Figure 1 - Location of proposed development site	3
Figure 2 - Aerial photograph of site	4
Figure 3 - Environment Agency online surface water flood map	11
Figure 4 - Environment Agency Reservoir Inundation Map	13
Figure 5 - SuDS Hierarch	20

LIST OF TABLES

Table 1: Proposed discharge rates for the 100-year event + 40% climate change	. 18
Table 2: Proposed attenuation storage volumes	. 19



GLOSSARY OF TERMS

AOD	Above Ordnance Datum
CDA	Critical Drainage Area
FFL	Finished Floor Level
FRA	Flood Risk Assessment
LBC	London Borough of Camden
LLFA	Lead Local Flood Authority
LPA	Local Planning Authority
NPPF	National Planning Policy Framework
PPG	Planning Practise Guidance
SFRA	Strategic Flood Risk Assessment
SuDS	Sustainable Drainage Systems
TWUL	Thames Water Utilities Limited



EXECUTIVE SUMMARY

The proposed development is located on the site named the 'The Ugly Brown Building' north of St Pancras International rail station in the London Borough of Camden (LBC). Proposals for the site are the erection of 6 new buildings, ranging in height from 2 storeys to 12 storeys above ground, and 2 basement levels comprising a mixed-use business, residential, hotel, retail and storage development with associated landscaping work. The site lies in Flood Zone 1 and is therefore considered to be at 'very low' risk of flooding from rivers or the sea. A full flood risk assessment (FRA) is required for developments in Flood Zone 1 which are more than 1 hectare or in an area with critical drainage problems, both of which apply to the site.

Potential flooding from rivers and the sea, surface water, sewers, groundwater and artificial sources have been assessed within the report. The development is considered to be at low risk from all sources of flooding, with the greatest risk from surface water/sewer flooding due to pressure on the Thames Water sewer network within the local area.

A surface water management plan has been designed to contain the 1% annual probability +40% climate change event, therefore reducing the risk of surface water flooding on the site and elsewhere.

The drainage strategy includes Sustainable Drainage System (SuDS) elements in order to reduce the rate of runoff by 50% from the pre-development rates in line with London Plan Policy 5.13. Part of the site will drain by gravity to the adjacent Regent's Canal and the remaining areas will drain to the combined sewer. This combination is deemed necessary to avoid including a pumped system as the water level of the canal is relatively high compared to site levels.

Attenuation storage is provided in the form of blue roofs and combination biodiverse/blue roofs on all buildings wherever possible and drained at controlled rates directly to the canal. Some roof areas are reserved for plant and will therefore drain to below ground storage on each plot. The remaining external areas will also drain to the underground storage before discharging at a controlled rate via a flow control device to the Thames Water combined sewer on St Pancras Way.



1. INTRODUCTION

Application History

A planning application, for the redevelopment of the Ugly Brown Building, was submitted to the London Borough of Camden in September 2017. The application is currently pending (ref: 2017/5497/P).

During the course of determination, a number of further design sessions have been held with London Borough of Camden Planning, Design and Conservation Officers. During these sessions officers have made a number of suggestions as to how the scheme might be
 refined. Furthermore, comments from a range of third parties have also been received during the determination process.

In order to address the aforementioned comments, revisions have been made to the scheme accordingly. This flood risk assessment and drainage strategy provides an assessment of the revised scheme, submitted to the London Borough of Camden in March 2018, and supersedes the original report submitted in September 2017.

General Information

 1.4. The proposed development is located on the site named the 'Ugly Brown Building' north of St Pancras International rail station in the London Borough of Camden. The site boundary encloses an area of approximately 1.14 ha.

The application is for demolition of the existing building and erection of 6 new buildings, ranging in height from 2 storeys to 12 storeys above ground, and 2 basement levels comprising a mixed-use business floorspace (B1), residential (C3), hotel (C1), gym (D2), flexible retail (A1-A4) and storage space (B8) development with associated landscaping work.

The latest online Environment Agency Flood Zone maps indicate that the site lies in Flood Zone 1 and is therefore considered to be at 'very low' risk of flooding from rivers or the sea. A full flood risk assessment (FRA) is required for developments in Flood Zone 1 of more than 1 hectare in size or which are located in an area with critical drainage problems as notified by the Environment Agency. A flood risk assessment has therefore been prepared to accompany the planning application. As well as considering the risk of flooding to the site, the impact the development may have on flooding elsewhere has been assessed, with particular reference to surface water run-off.

1.6.



This assessment has been compiled to meet the requirements of the National Planning Policy Framework (NPPF)¹.

Scope of Study

The main objectives of this study are to:

1.7.

1.8.

- assess the risk and implications of flooding on the site from all possible flood sources, including the future risk as a result of projected climate change over the lifetime of the development;
- assess the impact of the proposed development on flood risk elsewhere, with particular consideration of surface water management on the site;
- provide a flood risk assessment of the site, compliant with the guidelines set out in the NPPF and associated Planning Practice Guidance (PPG)², to accompany any application for planning permission;
- outline a drainage strategy for the new development by incorporating SUDS; and,
- provide advice on the site layout and design that will ensure safe operation of the site in an extreme flood or rainfall event, and avoid causing an unacceptable impact on the risk of flooding elsewhere.

¹ Department for Communities and Local Government (2012), National Planning Policy Framework.

² Department for Communities and Local Government (2014), *Planning Practice Guidance: Flood risk and coastal change*. <u>www.gov.uk/guidance/flood-risk-and-coastal-change</u>. Accessed 22/03/2017.



2. SITE DESCRIPTION

Location

The site address is 2-6 St Pancras Way, London, NW1 0TB and is located on land between St Pancras Way and Regent's Canal, approximately 500 m north of St Pancras International train station within the London Borough of Camden. Regent's Canal runs along the north eastern boundary of the site but this is not designated an Environment Agency 'Main River'.

2.1. The site location is shown in Figure 1.



2.2.

2.3.

Figure 1 - Location of proposed development site

The site is bounded by Regent's Canal to the north east, by St Pancras Hospital to the south, by St Pancras Way to the west and by residential developments to the north.

Existing Development

The site covers a total area of approximately 1.14 ha and comprises a large four-storey building divided into three plots - A, B and C - each independently occupied. Plots A and B are currently office space, the latter occupied by Ted Baker Headquarters, and plot C is a data centre. The area along St Pancras Way is mostly hard-paved with a small grassy bed with shrubs and small trees to the south. The canal-side area is made up of a gravel fill.



Topographic Survey and Site History

A topographic survey of the site was carried out in February 2016 by Clugston Construction Limited, and is presented in Drawing 1 in Appendix A. The survey has been orientated to the Ordnance Survey National Grid and survey levels have also been GPS verified.

The ground levels range between 20.4 m AOD at the southernmost corner of the site and 2.4. 23.6 m AOD along the edge of the canal at the north eastern boundary. The ground level increases north along St Pancras Way ranging from 20.4 m to 21.9 m AOD, and more steeply east along Granary Street from 20.4 m to 23.6 m AOD along the southern site boundary.

2.5.

2.6.

The retaining wall along the edge of the canal has a ground level along the top of 23.6 m AOD with the level in the canal measured at 23.13 m AOD (as at 22/01/2016). A drained walkway runs along the canal-facing side of the building at a level of 21.6 m AOD, with steps and a ramp leading up to the top of the retaining wall.







Proposed Development

The proposed development comprises of demolition of the existing building and erection of 6 new buildings, ranging in height from 2 storeys to 12 storeys above ground, and 2 basement levels comprising a mixed-use business floorspace, residential, hotel, gym, flexible retail and storage space development with associated landscaping work. The site is divided into three plots; A, B and C, and architect's drawings of the proposed development are included in Appendix A.

The proposals are for the demolition of the existing building and redevelopment to provide accommodation arranged around publicly accessible spaces. The proposed development comprises:

2.8.

2.7.

- an extended HQ for Ted Baker and boutique own brand hotel;
- business floorspace;
- residential dwellings;
- public open space along the canal edge and St Pancras Way, and within a central courtyard;
- retail units at ground floor creating a central public place;
- basements on each plot to provide centralised servicing and further commercial lettings.

2.9.

2.10.

2.11.

The vulnerability classification of the development, as set out in Table 2 of the PPG, is 'more vulnerable' for the residential units and hotels and 'less vulnerable' for the commercial elements of the development.

Plot A and B have one basement level and Plot C has two basement levels proposed. The basement (Level -1) on Plot A has floor levels ranging between 17.5 m and 18.0 m AOD and comprises cycle storage, commercial units and plant. On Plot B, the split-level basement includes car parking for 30 cars with a Finished Floor Level (FFL) of 19.1 m AOD, and plant and multi-purpose space at 16.3 m AOD. Plot C upper basement includes retail space, gym facilities and cycle storage with a FFL from 16.1 m to 17.5m AOD. The lower basement (Level -2) is located solely within Plot C, and is to be used as storage with a FFL of 13.4 m AOD.

Vehicular access to the site is via an entrance from St Pancras Way to Plot B car park approximately halfway along the western boundary.



The ground floor level is 21.7 m AOD in Plot A, varies between 21.4 m and 23.6 m AOD in Plot B, and between 20.2 m and 23.6 m AOD on Plot C.

2.12.



3. NATIONAL AND LOCAL PLANNING POLICY

National Planning Policy Framework

The National Planning Policy Framework (NPPF) was published in March 2012 and sets out the Governments' planning policies for England and how these are expected to be applied. The NPPF states that:

"Inappropriate development in areas at risk of flooding should be avoided by directing
 ^{3.1.} development away from areas at highest risk, but where development is necessary, making it safe without increasing flood risk elsewhere."

In addition to the NPPF, the Planning Practice Guidance was released to clarify planning aspects of flood risk management. The Planning Practice Guidance clarifies which development types are considered appropriate within each Flood Zone.

The London Plan

3.2.

- The London Plan³ is the overarching spatial strategy for the Greater London Area, and ^{3.3.} provides the basic foundation for planning policy in London. Flood risk and drainage are considered in the London Plan under Chapter 5 "London's response to Climate Change", within the Climate change adaptation section, Policies 5.11 through to 5.15.
- ^{3.4.} Policy 5.12 sets out detailed policy regarding flood risk management, and requires compliance with the NPPF and associated Planning Practice Guidance. The policy includes additional emergency provision for any development required to pass the Exception Test, and a requirement for protection of flood defences and watercourses. Policy 5.13 covers Sustainable Drainage, and requires implementation of the 7-stage drainage hierarchy, as well as a consideration of "water use efficiency, water quality, biodiversity, amenity and recreation".

Local Planning Policy

The site lies within the London Borough of Camden, which also acts as the Lead Local Flood Authority (LLFA). Below are a list of the policies relevant to flood risk within the recently adopted Camden Local Plan.

³ Mayor of London, Further Alterations to the London Plan 2015, March 2016



Camden Local Plan (2017)

Camden has recently adopted the new Local Plan, and below are the relevant policies regarding flooding and SuDS.

Policy CC2 Adapting to climate change

The Council will require development to be resilient to climate change. All development 3.6. should adopt appropriate climate change adaptation measures such as:

• a. the protection of existing green spaces and promoting new appropriate green infrastructure;

3.7.

- b. not increasing, and wherever possible reducing, surface water runoff through increasing permeable surfaces and use of Sustainable Drainage Systems;
- c. incorporating bio-diverse roofs, combination green and blue roofs and green walls where appropriate; and
- d. measures to reduce the impact of urban and dwelling overheating, including application of the cooling hierarchy.

Policy CC3 Water and flooding

- ^{3.8.} The Council will seek to ensure that development does not increase flood risk and reduces the risk of flooding where possible. We will require development to:
 - a. incorporate water efficiency measures;
 - b. avoid harm to the water environment and improve water quality;
 - c. consider the impact of development in areas at risk of flooding (including drainage);
 - d. incorporate flood resilient measures in areas prone to flooding;
 - e. utilise Sustainable Drainage Systems (SuDS) in line with the drainage hierarchy, unless inappropriate, to achieve a greenfield run-off rate where feasible; and
 - f. not locate vulnerable development (such as basement dwellings) in floodprone areas.



Camden Strategic Flood Risk Assessment

URS prepared a Strategic Flood Risk Assessment⁴ (SFRA) for the London Borough of Camden in July 2014. The SFRA is used to inform this site-specific flood risk assessment.

Sequential Test

- 3.9. The site lies entirely within Flood Zone 1 and the vulnerability classification for the development is *Less Vulnerable* for the retail and business use, and *More Vulnerable* for the residential units and hotel.
- The sequential test is not normally required for development within Flood Zone 1 unless "the Strategic Flood Risk Assessment for the area, or other more recent information, indicates there may be flooding issues now or in the future" (PPG). The dominant risk of flooding in the borough is from surface water as a result of sewer overloading, however the risk is shown to be low for the application site, and therefore the sequential test is not required for this development.

Additionally, Table 3 of the PPG for Flood Risk and Coastal Change deems all development 3.12. to be appropriate within Flood Zone 1.

⁴ London Borough of Camden (July 2014) Strategic Flood Risk Assessment



4. POTENTIAL FLOODING ON SITE

Flooding from Rivers and the Sea

As stated in the Camden SFRA, all Main Rivers historically located within the Borough are now culverted and incorporated into the Thames Water Utilities Limited (TWUL) sewer network and therefore there is no fluvial flood risk to the site. The site is also shown to be in Flood Zone 1 according to the Environment Agency flood map for planning, which is defined as land having a less than 0.1% annual probability of river or sea flooding. Therefore the risk of flooding from rivers or the sea is very low.

The site is located approximately 20 m above sea level and consequently there is considered to be no risk of flooding from the sea.

4.2. Flooding from Surface Water

- Flooding can occur during periods of intense rainfall from runoff flowing overland before entering a watercourse or sewer. In an urban environment, the risk of flooding from surface water and from overloaded sewers is closely related, and both are included in the relevant surface water flooding datasets. Flooding events are typically of short duration (unless there is a drainage system blockage), but can be severe.
- ^{4.4.} The Environment Agency has published a surface water flood map available online, as shown in Figure 3. The information on this map is suitable for identifying approximate areas which would flood and the likely depth of this flooding. It is unlikely to be reliable for
 ^{4.5.} identifying individual properties at risk.

4.6.

4.1.

Appendix B Figure 6 of the SFRA shows the majority of Camden has been identified as being within a Critical Drainage Area (CDA) - "A discrete geographic area (usually a hydrological catchment) where multiple and interlinked sources of flood risk (surface water, groundwater, sewer, main river and/or tidal) cause flooding in one or more Local Flood Risk Zones during severe weather thereby affecting people, property or local infrastructure."

The site is predominantly shown to have a *very low* risk of surface water flooding as shown as 'clear' on the flood map, equivalent to less than 0.1% annual probability of flooding. The northern part of the site is shown to be at *low* risk (between 0.1% and 1% annual probability). The thin strips of *medium* risk areas along the canal are due to the existing walkway along that side of the building, currently set 2 m below the top of bank. This walkway will no longer exist in the proposed development.

GDP



Figure 3 - Environment Agency online surface water flood map

4.7. The surface water drainage strategy for the development (refer to Section 5 of this report) will ensure that overland flow is appropriately managed on the site, by use of green/blue roofs and underground attenuation storage. The surface water management system will ensure no flooding for the 1% annual probability plus climate change event will occur on the

4.8. site.

4.9.

If an extreme rainfall event occurred causing surface water flooding in the wider area, it is expected that flood water would be contained within St Pancras Way since ground levels within the road are lower than on site. The risk of surface water flooding to the site is therefore considered to be low, on the condition that an adequate maintenance programme is adopted for the onsite surface water system.

Flooding from Sewers

Thames Water asset location plans have been acquired for the site and surrounding area, included in Appendix B. These show a 2134 mm diameter trunk combined sewer passing beneath the site with an invert level of 13.6 m AOD, approximately 2 m below the proposed (17.5 m basement on plot А AOD). In addition, there is а 1093 x 762 mm combined sewer along St Pancras Way flowing in a north-south direction, with a contributing 152 mm diameter sewer along Granary Street.

4.10.

4.14.



A Thames Water sewer flooding history enquiry at 6a St Pancras Way indicates that there have been no incidents of flooding in the requested area as a result of surcharging public sewers. It is therefore unlikely that the sewers in the vicinity will surcharge onto the site unless linked to a surface water flood event. In the unlikely event of sewer flooding from the sewer in St Pancras Way, flood water is likely to be contained within the road flowing south past the site.

Figure 5a in Appendix B of the SFRA displays information from the DG5 internal sewer flooding register and the site is shown to be in a postcode district that has no recorded incidents of flooding.

- A drainage CCTV survey of the existing site was carried out by Drainage Technical Services Ltd on 2nd April 2017. This confirmed that all surface water drainage, including from the canal-side, discharges to the combined sewer network on St Pancras Way.
- The proposed scheme will include entirely new sewer infrastructure, only retaining the existing connection to the public sewer network. The surface water network onsite will be designed and sized based on expected discharges for the 1% annual probability event including an allowance for climate change for the lifetime of the development. On the basis of this information, the risk of flooding from sewers is considered to be low.

Flooding from Groundwater

- The bedrock geology underlying the site shown on the British Geological Survey online map consists of London Clay Formation (clay, silt and sand). No superficial deposits are shown in the area. The geology is confirmed by two boreholes (TQ28SE314 and TQ28SE1564) adjacent to the site. London Clay forms an impermeable layer lowering the risk of groundwater
 4.15. emergence at the surface, and at the site's location, the absence of a superficial aquifer results in a low risk of perched groundwater.
- Figure 4e in Appendix B of the SFRA displays areas at increased susceptibility to elevated groundwater along with historic records of groundwater flooding held by LBC and the Environment Agency. The site is not shown to be at increased susceptibility to elevated groundwater and there are no records of groundwater flooding incidents within a 500 m radius of the site.

The SFRA refers to the Camden Geological, Hydrogeological and Hydrological Study, stating that, within Camden, groundwater can be encountered within river terrace deposits, isolated perched water bodies within sandy layers of the London Clay and a more significant water table within the Bagshot Beds. Based on available below-ground information, there is



no indication of any substantial sandy layers underlying the site or presence of shallow groundwater. Therefore the risk of groundwater flooding to the site is considered to be low.

Despite the expected low risk, groundwater levels can fluctuate throughout the year and therefore, it is recommended that consideration should be given to flood resistant design for the basement units as a preventative measure against future ingress of groundwater or damp.

4.17.

4.18.

Flooding from Artificial Sources

Flooding can occur as a result of the failure of infrastructure that impounds water, such as reservoirs, lakes and canals. The site is not shown to be within the maximum extent of possible flooding from reservoirs on the Environment Agency Reservoir Inundation Map (as shown in Figure 4).



4.19.

Figure 4 - Environment Agency Reservoir Inundation Map

The Reservoirs Act 1975⁵ (as amended by the Flood and Water Management Act 2010⁶) requires asset owners to maintain their reservoirs such that the annual probability of a breach of the reservoir is less than 1 in 50,000. It is therefore considered that the risk of flooding from reservoirs is extremely low.

⁵ Reservoirs Act 1975 (c.23). London, Her Majesty's Stationery Office.

⁶ Flood and Water Management Act 2010 (c.29). London, Her Majesty's Stationery Office.



The Regent's Canal is managed by the Canals & Rivers Trust. The Canals & Rivers Trust ensures that the canal does not overtop its banks by controlling the water levels in the canal via the lock systems on the Regent's Canal. High water levels within canals can be managed by moving the water through the locks down to unaffected lock reaches.

4.20. No further artificial sources of flooding have been identified within the vicinity of the site.

Flood Warning and Emergency Access/Egress

The flood risk to the site is considered to be low from all sources, however there is a residual risk from surface water flooding in the event of an extreme rainfall event (e.g. > 0.1% annual probability) which exceeds the designed capacity of the onsite surface water drainage system. The proposals include commercial uses in the basement levels and the following information has been identified on the LBC website⁷:

Businesses and residents in basements are advised to:

- Take note of weather forecasts for heavy rainfall identified as red alert,
- Sign up for emergency text alerts on Camden's alert system this will endeavour to relay high risk warnings when Camden are made aware of them, but this will not be a 24/7 service,
- Have an emergency plan for taking you and your family or colleagues out of harm's way to a higher floor so that you are not at risk.

This information should be supplied to any future owners and occupants of the basement units, and they should be encouraged to sign up for the emergency text alerts described in the previous paragraph.

4.24.

4.23.

Climate Change

The predicted increase in frequency and severity of rainfall events as a result of climate change will increase the likelihood of flooding from rivers, land, sewers and artificial bodies as storage becomes overwhelmed. In line with the latest guidance⁸, a climate change factor of +40% has been applied to the 1% annual probability rainfall event in the design of the surface water management system.

⁷ <u>www.camden.gov.uk/ccm/content/policing-and-public-safety/emergencies/flooding/</u> Accessed 21/04/2017

⁸ <u>www.gov.uk/guidance/flood-risk-assessments-climate-change-allowances</u> Accessed 24/04/2017



5. SURFACE WATER MANAGEMENT

In accordance with the NPPF, as a minimum requirement, run-off rates and volumes should not increase from any site following development, to prevent an increase in flood risk elsewhere as a result of the development.

The proposed development falls under the classification of 'major development', 5.1. therefore, under The Town and Country Planning (Development Management Procedure) (England) Order 2015, the site must adopt a sustainable drainage approach, through the use of SuDS.

Additional guidance to the requirements of London Plan Policy 5.13 are presented in the Sustainable Design and Construction Supplementary Planning Guidance (SPG)⁹, which states that a 50% attenuation of pre-development runoff rate is "the minimum expectation from

5.3. that a 50% attenuation of pre-development runoff r development proposals".

Existing Site Runoff

- The site is considered to be entirely impermeable, predominantly consisting of a large flat roof with hard paving around the site boundary. There is a small raised bed of shrubs to the south west of the site, however, due to the nature of its design, it is expected to have negligible effects on the site runoff.
- 5.5. Source Control (Microdrainage 2017) was used to calculate design rainfall intensities and resulting runoff rates with input rainfall ratio, R of 0.41 and expected rainfall M5-60 of 20.6 mm/h from FSR based on the site location. Calculation sheets are provided in Appendix C.

The existing peak runoff rates for the 1-year, 30-year and 100-year return period rainfall events are as follows:

Return Period (year)	1 30		100
Discharge rate (l/s)	101	247	322

 $^{^{\}rm 9}$ Mayor of London, Sustainable Design and Construction SPG, April 2014



Greenfield Runoff

The greenfield runoff rates for the site were calculated using IoH124 methodology and the online tools provided by HR Wallingford on the UK SuDS website¹⁰, and are as follows (calculation sheet provided in Appendix C):

	Return Period (year)	Qbar	1	30	100
5.7.	Discharge rate (l/s)	4.77	4.05	10.96	15.21

Existing Site Drainage

5.8.

A site visit undertaken by Water Environment Ltd on 16th March 2017 confirmed the existing roof drains by gravity through gutters along the front and rear of the building and several downpipes before joining the underground drainage network.

- A CCTV survey of the existing site drainage was undertaken by Drainage Technical Services 5.9. Ltd on 2nd April 2017. Based on the survey, all surface water drainage from the site, including on the canal-side, is assumed to flow into the public combined sewer under St Pancras Way via a connection between plot A and B.
- 5.10. The TWUL asset location plans show three existing lateral connections to the combined sewer under St Pancras Way. There are no existing surface water outfalls to Regent's Canal from the site, and from visual inspection during a site visit, no other developments in the area appear to have outfalls to the canal.

5.11. Proposed Surface Water Drainage System

Surface water will be managed on site through the provision of Sustainable Drainage
 ^{5.12.} Systems (SuDS) where possible in line with national policy. No attenuation of surface water exists on the site, and currently all runoff discharges directly to the public sewer network.

The site is entirely hardstanding and the underlying London Clay geology is unlikely to be appropriate for direct infiltration of surface water. Surface water can therefore only discharge from the site via Regent's Canal or the Thames Water combined sewer network. Both Thames Water and the Canal & River Trust have been consulted in order to agree discharge rates into each respective network.

¹⁰ www.uksuds.com/drainage-calculation-tools/greenfield-runoff-rate-estimation Accessed 24/04/2017



Regent's Canal runs to the northeast of the site with an approximate water level of 23.13 m AOD, which is at a higher level than the majority of external areas on the proposed site. Underground attenuation storage is therefore unable to discharge directly to the canal by gravity. Surface water runoff from all external areas would therefore require pumping in order to discharge to the canal. Pumped systems are considered the least sustainable of systems with the highest maintenance liability and the highest chance of failure, and should therefore be avoided in so far as possible.

The following guiding principles were used in developing the proposed drainage strategy:

- attenuating surface water using SuDS wherever possible;
- reducing the peak surface water runoff by a minimum 50% of the existing rate including an allowance for future climate change;
 - ensuring the peak runoff requirement is met by plots A, B and C independently to accommodate phased construction and independent future ownership;
 - maximising the proportion of surface water runoff discharging to the canal, alleviating the pressure on the local public sewer network;
 - avoiding a pumped system.
- ^{5.15.} The proposed development consists of approximately 72% roof area and 28% hard landscaping. Only the roof areas are high enough to drain to the canal by gravity and due to spatial restrictions at ground level, attenuation storage is proposed in the form of paved-over blue roofs and *combination biodiverse/blue roofs*. The term *combination biodiverse/blue roofs*. The term *combination biodiverse/blue roof* is used here to describe a biodiverse roof with additional attenuation storage beneath it.

Paved-over blue roofs and combination biodiverse/blue roofs have been included on all buildings across the site wherever possible (refer to SuDS drawing in Appendix A). Some roof areas are reserved for plant and have to be drained to the public combined sewer. Since it is not possible to provide attenuation storage beneath the plant at roof level, it will

5.17. therefore drain to below-ground attenuation storage before discharging to the public sewer at a reduced rate. Similarly, some roof terraces cannot accommodate the blue roof buildup depth whilst maintaining a level threshold with the internal finished floor level and therefore will also drain to below ground attenuation storage.

All external areas at ground level will also drain to below-ground attenuation storage.

Page: 17

5.14.

5.13.



Due to the high relative water level of the canal and the spatial restrictions adjacent to it, below-ground attenuation storage discharging to the canal is not possible unless a pumped system is installed. In order to avoid this, all below-ground attenuation storage will discharge to the combined sewer, while all biodiverse/blue roofs will discharge to the canal.

5.18.

In order to satisfy the 50% reduction in pre-development runoff rates during phased construction, each plot will have separate attenuation storage for runoff discharging to the combined sewer. Plot A will have underground cellular crate storage beneath the basement cycle store; Plot B will have underground cellular crate storage beneath the basement car parking; and Plot C will have a 150 mm depth cellular crate storage beneath the external paved areas, above the basement level. All design proposals are subject to review at the detailed design stage, however the principles of the drainage strategy will remain unchanged.

The proposed discharge rates for the 100-year rainfall event including an allowance for 5.20. future climate change are shown for each plot in Table 1. The proposed discharge rates represent a reduction of 50% from the existing 100-year rainfall event (no climate change) and are subject to agreement with Thames Water and the Canal & River Trust.

	Plot A	Plot B	Plot C	Whole site
Area (as % of site)	15%	22%	63%	100%
Discharge to canal (l/s)	9.5	13.1	18.6	41
Discharge to sewer (l/s)	14.6	22.6	82.5	120
Total discharge (l/s)	24.2	35.7	101.1	161

5.21.

The proposed discharge rate for the 100-year event +40% allowance for climate change for the whole site is 161 l/s, which complies with the 50% of existing runoff rate requirement of the London Plan. The system will be designed such that runoff from the 100-year event +40% for future climate change is fully retained on the site within attenuation storage and discharged at a controlled rate. Runoff rates will be controlled by flow control devices for every outfall from the site and are to be designed to reduce runoff rates for the 1, 30 and 100 year return periods by a minimum 50% of existing rates.



ABG have provided specifications for the proposed blue roofs and combination biodiverse/blue roofs including storage volumes and discharge rates. MicroDrainage (Source Control) has been used to calculate the volumes of below-ground attenuation storage required. A summary of the attenuation storage volumes is presented in Table 2. Calculation sheets are included in Appendix C.

5.22.

5.26.

Table 2: Proposed attenuation storage volumes

	Plot A	Plot B	Plot C	Whole site
Blue roof volume (m ³)	36.7	52.9	71.6	161
Below ground storage volume (m ³)	22.8	34.2	147.3	204
Total attenuation volume (m ³)	59.5	87.1	218.9	365

For extreme events greater than the 100-year event +40%, the below ground storage may 5.23. reach full capacity, in which case surface water would backup and overflow onto the site before flowing overland into the drainage system in St Pancras Way.

5.24. The site will remain 100% hard standing post-development, however, the proposed array of biodiverse roofs will result in a significant reduction of hard roof area and will reduce the volume of surface water discharging from the site.

5.25. Sustainable Drainage Systems (SuDS)

The London Plan sets out a SuDS multi-functional benefits hierarchy, outlining solutions from the most sustainable drainage methods to the least sustainable methods as shown in Figure 5. The objective of the SuDS hierarchy is to ensure that surface water run-off is managed as close to its source as possible.

The aim of Sustainable Urban Drainage Systems (SuDS) is to emulate natural processes with the result that watercourses and storage areas receive the hydrological profiles under which they evolved, and that water quality in local ecosystems is protected or improved. The best practice guide states that a sustainable drainage system will¹¹:

- reduce the impact of additional urbanisation on the frequency and size of floods;
- protect or enhance river and groundwater quality;

¹¹ CIRIA C523 - Sustainable Urban Drainage Systems - Best Practice Manual



- be sympathetic to the needs of the local environment and community; and
- encourage natural groundwater recharge.

A large proportion of the site area is occupied by roof space, and following the SuDS hierarchy shown in Figure 5, biodiverse roofs are included wherever possible on all the major buildings.

Most Sustainab 5.27	SUDS technique	Flood Reduction	Pollution Reduction	Landscape & Wildlife Benefit
	Living roofs	4	~	~
1	Basins and ponds - Constructed wetlands - Balancing ponds - Detention basins - Retention ponds	~		V
	Filter strips and swales	~	~	v
	Infiltration devices - soakaways - infiltration trenches and basins	~	~	V
V	Permeable surfaces and filter drains - gravelled areas - solid paving blocks - porous paviors	V	~	
Least Sustainab	Tanked systems - over-sized pipes/tanks - storms cells	V		

5.28. Figure 5 - SuDS Hierarch

Green roofs are considered amongst the most sustainable of all the SuDS techniques, providing similar benefits as greenfield land such as:

- reduced rainwater runoff;
- enhanced roof insulation properties;
- attractive visual appearance;
- reduction in urban heat island effect;
- enhanced roof lifespan by protecting underlying waterproofing system; and,

5.30.

5.29.

• provision of green space in urban areas and encouragement of biodiversity.

It should be noted that green roofs are suitable for use in combination with photovoltaics. The presence of a green roof beneath photovoltaic cells has been shown to cool the ambient air temperature around the photovoltaic cells making them more efficient.

Due to the constrained nature of the site, there is very limited space for the provision of basins or ponds and it is not feasible to include these SuDS elements into the design.

5.31.

5.32.



Additionally, the geology beneath the site is not suited to the use of infiltration devices as a means of discharging surface water directly to the ground. Figure 4c in Appendix B of the SFRA shows the site is "not within a zone of high or probable compatibility for infiltration SuDS; however bespoke solutions may be applicable".

The first basement level extends beneath most of the site. The strip of land along the side of the canal is not capable of supporting any SuDS elements and is reserved for the ongoing maintenance and support of the canal. The remaining external areas change in elevation by approximately 2m from the canal to the road, which makes the use of permeable surfaces with a granular sub-base unsuitable.

The remaining choice for storage attenuation is within an underground storage structure, which is proposed to attenuate any surface water not captured by the blue roofs, discharging to the TWUL sewer network.

SuDS Management and Maintenance

- Management and maintenance of the drainage network, including the biodiverse roof areas ^{5.33.} and underground storage tank, will be the responsibility of the freeholder of the site. Management and maintenance agreements and plans will be arranged prior to completion of development.
- ^{5.34.} Management and maintenance of the SuDS elements should be carried out in accordance with the supplier's guidance and specification.



6. SUMMARY OF FLOOD RISK ASSESSMENT

1. Development site and location				
a. Where is the development site located?	2 - 6 St Pancras Way, London, NW1 0TB			
b. What is the current use of the site?	Office space, Ted Baker HQ, data centre			
c. Which Flood Zone (for river or sea flooding) is the site within?	Flood Zone 1			
2. Development proposals				
a. What are the development proposal(s) for this site? Will this involve a change of use of the site and, if so, what will that change be?	Following demolition of the Ugly Brown Building, proposals to erect multiple mixed use buildings comprising of business floorspace, hotel, retail units, and residential accommodation.			
b. In terms of vulnerability to flooding, what is the vulnerability classification of the proposed development?	More vulnerable due to residential component			
c. What is the expected or estimated lifetime of the proposed development likely to be?	100 years			
3. Sequential test				
a. What other locations with a lower risk of flooding have you considered for the proposed development?	N/A			
b. If you have not considered any other locations, what are the reasons for this?	N/A			
c. Explain why you consider the development cannot reasonably be located within an area with the lowest probability of flooding (Flood Zone 1); and, if your chosen site is within Flood Zone 3, explain why you consider the development cannot reasonably be located in Flood Zone 2.	N/A			
d. As well as flood risk from rivers or the sea, have you taken account of the risk from any other sources of flooding in selecting the location for the development?	N/A			
4. Climate Change				
How is flood risk at the site likely to be affected by climate change?	Extreme rainfall events will become more frequent and more intense. An increase in rainfall of 40% has been used in the assessment in line with national guidance.			



5. Site specific flood risk				
a. What is/ are the main source(s) of flood risk to the site?	Surface water flooding			
b. What is the probability of the site flooding, taking account of the maps of flood risk available from the Environment Agency, the local planning authority's Strategic Flood Risk Assessment and any further flood risk information?	Less than 0.1% annual probability of flooding from rivers or the sea. EA online map indicates the site is at very low risk from surface water, however St Pancras Way adjacent to the site is at low to medium risk. The site is also within a critical drainage area. The risk of flooding from all other sources is considered to be very low			
c. Are you aware of any other sources of flooding that may affect the site?	No			
d. What is the expected depth and level for the design flood?	No flooding expected for the 1% annual probability event including climate change due to the proposed surface water management plan			
e. Are properties expected to flood internally in the design flood and to what depth?	No			
f. How will the development be made safe from flooding and the impacts of climate change, for its lifetime?	The surface water management system will be maintained for its lifetime to ensure the development is safe from flooding.			
g. How will you ensure that the development and any measures to protect the site from flooding will not cause any increase in flood risk off-site and elsewhere? Have you taken into account the impacts of climate change, over the expected lifetime of the development?	Surface water will be attenuated significantly reducing the pre-development peak runoff rate using flow control devices.			
h. Are there any opportunities offered by the development to reduce the causes and impacts of flooding?	The site currently has no surface water attenuation measures and is 100% hardstanding. The proposals will include significant surface water attenuation.			
6. Surface water management				
a. What are the existing surface water drainage arrangements for the site?	The existing site drains entirely to the TWUL combined sewer network			
b. If known, what (approximately) are the existing rates and volumes of surface water run-off generated by the site?	The peak storm runoff for the 100 year event is estimated at 322 l/s			
c. What are the proposals for managing and discharging surface water from the site, including any measures for restricting discharge rates?	Runoff from roofs will be attenuated and stored on using combination biodiverse/blue roof systems and flow control devices into the canal. Runoff from remaining areas will be attenuated in below ground attenuation storage with a flow control devices limiting discharge into the public sewer network.			

Flood Risk Assessment and SuDS Strategy



d. How will you prevent run-off from the completed development causing an impact elsewhere?	The surface water management system has been designed to the 100-year rainfall event including an allowance for climate change and provides a significant reduction on pre-development runoff rates.		
e. Where applicable, what are the plans for the ongoing operation and/or maintenance of the surface water drainage systems?	An appropriate maintenance plan will be provided prior to construction		
7. Occupants and users of the developme	ent		
a. Will the development proposals increase the overall number of occupants and/or people using the building or land, compared with the current use? If this is the case, by approximately how many will the number(s) increase?	The number of occupants will increase post development due to the new residential units and increased density. However, the flood risk to the site is considered to be very low, and therefore no increase to occupants is anticipated.		
b. Will the proposals change the nature or times of occupation or use, such that it may affect the degree of flood risk to these people?	The flood risk is considered very low and therefore the proposals do not have an effect on flood risk		
c. Where appropriate, are you able to demonstrate how the occupants and users that may be more vulnerable to the impact of flooding (e.g., residents who will sleep in the building; people with health or mobility issues; etc.,) will be located primarily in the parts of the building and site that are at lowest risk of flooding? If not, are there any overriding reasons why this approach is not being followed?	N/A		
8. Exception test			
a. Would the proposed development provide wider sustainability benefits to the community? If so, could these benefits be considered to outweigh the flood risk to and from the proposed development?	N/A		
b. How can it be demonstrated that the proposed development will remain safe over its lifetime without increasing flood risk elsewhere?	N/A		
c. Will it be possible for the development to reduce flood risk overall (e.g. through the provision of improved drainage)?	N/A		

Flood Risk Assessment and SuDS Strategy



9. Residual risk		
a. What flood related risks will remain after the flood risk management and mitigation measures have been implemented?	There remains a residual risk to parts of the site from surface water/sewer flooding in extreme rainfall events of greater than 0.1% annual probability.	
b. How, and by whom, will these risks be managed over the lifetime of the development?	Maintenance of the SuDS elements will be managed by an appropriate management group for the lifetime of the development.	
10. Flood risk assessment credentials		
a. Who has undertaken the flood risk assessment?	Water Environment Ltd on behalf of GD Partnership	
b. When was the flood risk assessment completed?	March 2018	



7. <u>CONCLUSIONS</u>

The risk of flooding to the site has been considered from all sources and is assessed to be low. The greatest risk is from surface water flooding as a result of exceedance of the onsite drainage system, however the surface water management plan is designed to contain the 1% annual probability +40% climate change event within SuDS elements.

- 7.1. A reduction in runoff rates from the existing site of 50% will be achieved by attenuating the 1% annual probability +40% event using paved-over blue roofs, combination biodiverse/blue roof systems and below ground storage. The site has very limited space and options for the
- 7.2. use of SuDS, however the reduction in runoff rates achieved on the proposed development is in line with the London Plan Policy 5.13 and significantly decreases the risk of flooding elsewhere. Discharge to the canal will also help alleviate pressure on the TWUL sewer network within the local area.

A suitable management and maintenance plan will be necessary in order to guarantee the 7.3. effectiveness of the SuDS elements and ensure that a low risk of flooding to the site, and surrounding third-party land, is maintained.

7.4. Future owners and occupants of the basement units should be encouraged to sign up for the emergency text alerts provided by the London Borough of Camden.



APPENDIX A - DRAWINGS

Drawing 1- Topographic Survey				
Clugston Survey Services Drawing Nos. 3948/10/001 and 3948/10/002				
Topographic survey of the site showing existing levels, buildings and infrastructure.				
Drawing 2 - Proposed Basement Plan B2				
Bennetts Associates Architects Drawing No. 1603_P_098 Rev E				
Proposed level 2 basement layout plan				
Drawing 3 - Proposed Basement Plan B1				
Bennetts Associates Architects Drawing No. 1603_P_099 Rev H				
Proposed level 1 basement layout plan				
Drawing 4 - Proposed Level 00				
Bennetts Associates Architects Drawing No. 1603_P_100 Rev J				
Proposed ground floor level and landscaping				
Drawing 5 - Proposed Roof Plan				
Bennetts Associates Architects Drawing No. 1603_P_RP Rev E				
Proposed roof layout plan				
Drawing 6 - Proposed Drainage Strategy				
GDP Drawing No. 16-017-SK01 Rev 4				
Layout of the proposed SuDS elements				



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BP Boundary Post GP BS Bus Stop GAS	Gate Post I Gas Cover I	RE Rodding Eye RS Road Sign	TL Traffic Light TP Telephone Pole
CATV Cable TV Cover KO CCTV Close Circuit TV LB	Kerb Offlet I Lighting Beacon I	RS(L) Road Sign (Lit) RWP Rain Water Pipe	VP Vent Pipe WM Water Meter
CP Concrete Post LP DWB Dog Waste Bin ME	Lamp Post Meter	SP Sign Post SP(L) Sign Post (Lit)	WV Water Valve UC: Unknown Cover
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Drawing Title Proposed Basement Le	vel B1	
Drawing Number 1603_P_099		Revision H
Scale @ A3 1:500	Scale @A1 1:250	Revision Date 180223







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Flood Risk Assessment and SuDS Strategy



APPENDIX B - THAMES WATER ASSET SEARCH



Based on the Ordnance Survey Map with the Sanction of the controller of H.M. Stationery Office, License no. 100019345 Crown Copyright Reserved.

NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no surv	ey information	is available
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Manhole Reference	Manhole Cover Level	Manhole Invert Level
36DI	n/a	n/a
3501 36EB	22.84 n/a	8.17 n/a
4602	n/a	n/a
471A	n/a	n/a
4701 4721	23.71 23.86	13.66 n/a
4614	n/a	n/a
5718	20.05	17.31
5704	19.71 21 24	16.96 14 4
55AE	n/a	n/a
5702	n/a	n/a
55AJ 6601	n/a 19.88	n/a 14.88
6501	n/a	n/a
6701	n/a	n/a
7604 7803	23.2 26.85	22.52 23.93
7606	n/a	n/a
7701	27.5	24.8
7702	27.5 n/a	25 n/a
7601	23.22	22.53
7602	n/a	n/a
7703	27.5 n/a	25.4 n/a
8508	n/a	n/a
8506	19.98	19.05
8505	20.03	19.46
8504	20.07	19.31
8503	20.23	19.28
5501	18.95	15.59
55AI 55AF	n/a n/a	n/a n/a
8510	n/a	n/a
8509	n/a	n/a
59DH	n/a n/a	n/a n/a
59FH	n/a	n/a
59FI	n/a	n/a
59AF	n/a	n/a
59FD 59FG	n/a	n/a n/a
5801	n/a	n/a
59AE	n/a	n/a
59DG	n/a	n/a n/a
59AD	n/a	n/a
59BA	n/a	n/a
59BB	n/a n/a	n/a n/a
59AC	n/a	n/a
59AB	n/a	n/a
59EG	n/a	n/a
59EF	n/a	n/a
59EH	n/a	n/a
6902	27.75	23.25 22.6
6903	26.5	23.55
6904	26.5	22
7801	26.5	21.44 23.9
49DF	n/a	n/a
50EC	n/a	n/a
3814 4902∆	23.94 n/a	n/a n/a
49DI	n/a	n/a
4901B	21.24	19.17
490C 49DG	n/a n/a	n/a n/a
49CD	n/a	n/a
49AJ	n/a	n/a
4802 49CB	21.26	17.29
59EC	n/a	n/a
59AH	n/a	n/a
5803	21.36	16.99
59EB	n/a n/a	n/a n/a
59AG	n/a	n/a
59FJ	n/a	n/a
3001	25.29	12.67
The position of the apparatus shown on this plan	is given without obligation and warranty, and the acc	suracy cannot be guaranteed. Service pipes are not

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.



ALS Sewer Map Key

Thames Water <u>Thames Water Utilities Ltd.</u> Property Searches, PO Box 3189, Slough SL 1 4W, DX 151280 Slough 13 T 0845 070 9148 E searches@thameswater.co.uk I www.thameswater.propertysearches.co.uk

Page 8 of 12

Sewer Flooding History Enquiry



GD Partnership Ltd

Search address supplied

Ted Baker Ltd 6a St. Pancras Way London NW1 0TB

Your reference	6a StPancrass Way
Our reference	SFH/SFH Standard/2016_3265554
Received date	24 February 2016
Search date	24 February 2016

Thames Water Utilities Ltd

Property Searches PO Box 3189 Slough SL1 4WW

DX 151280 Slough 13

T 0118 925 1504

E searches@thameswater.co.uk www.thameswaterpropertysearches.co.uk

Registered in England and Wales No. 2366661, Registered office Clearwater Court, Vastern Road Reading RG1 8DB

Sewer Flooding History Enquiry



Search address supplied: Ted Baker Ltd,6a,St. Pancras Way,London,NW1 0TB

This search is recommended to check for any sewer flooding in a specific address or area

- TWUL, trading as Property Searches, are responsible in respect of the following:-
- (i) any negligent or incorrect entry in the records searched;
- (ii) any negligent or incorrect interpretation of the records searched;
- (iii) and any negligent or incorrect recording of that interpretation in the search report
- (iv) compensation payments

Thames Water Utilities Ltd

Property Searches PO Box 3189 Slough SL1 4WW

DX 151280 Slough 13

T 0118 925 1504

E searches@thameswater.co.uk I www.thameswaterpropertysearches.co.uk

Registered in England and Wales No. 2366661, Registered office Clearwater Court, Vastern Road Reading RG1 8DB

Sewer Flooding History Enquiry



History of Sewer Flooding

Is the requested address or area at risk of flooding due to overloaded public sewers?

The flooding records held by Thames Water indicate that there have been no incidents of flooding in the requested area as a result of surcharging public sewers.

For your guidance:

- A sewer is "overloaded" when the flow from a storm is unable to pass through it due to a permanent problem (e.g. flat gradient, small diameter). Flooding as a result of temporary problems such as blockages, siltation, collapses and equipment or operational failures are excluded.
- "Internal flooding" from public sewers is defined as flooding, which enters a building or passes below a suspended floor. For reporting purposes, buildings are restricted to those normally occupied and used for residential, public, commercial, business or industrial purposes.
- "At Risk" properties are those that the water company is required to include in the Regulatory Register that is presented annually to the Director General of Water Services. These are defined as properties that have suffered, or are likely to suffer, internal flooding from public foul, combined or surface water sewers due to overloading of the sewerage system more frequently than the relevant reference period (either once or twice in ten years) as determined by the Company's reporting procedure.
- Flooding as a result of storm events proven to be exceptional and beyond the reference period of one in ten years are not included on the At Risk Register.
- Properties may be at risk of flooding but not included on the Register where flooding incidents have not been reported to the Company.
- Public Sewers are defined as those for which the Company holds statutory responsibility under the Water Industry Act 1991.
- It should be noted that flooding can occur from private sewers and drains which are not the responsibility of the Company. This report excludes flooding from private sewers and drains and the Company makes no comment upon this matter.
- For further information please contact Thames Water on Tel: 0800 316 9800 or website www.thameswater.co.uk

Thames Water Utilities Ltd

Property Searches PO Box 3189 Slough SL1 4WW

DX 151280 Slough 13

T 0118 925 1504

E searches@thameswater.co.uk www.thameswaterpropertysearches.co.uk

Registered in England and Wales No. 2366661, Registered office Clearwater Court, Vastern Road Reading RG1 8DB



APPENDIX C - CALCULATION SHEETS

- UK SuDS Greenfield Calculator greenfield runoff
- MicroDrainage Existing runoff
- MicroDrainage Proposed discharge to TW sewer and attenuation storage
- ABG Proposed combination biodiverse/blue roof discharge rates to Regent's Canal and attenuation storage



Calculated by:	Water Environment
Site name:	Ugly Brown Building
Site location:	NW1 0TB

This is an estimation of the greenfield runoff rate limits that are needed to meet normal best practice criteria in line with Environment Agency guidance "Preliminary rainfall runoff management for developments", W5-074/A/TR1/1 rev. E (2012) and the SuDS Manual, C753 (Ciria, 2015). This information on greenfield runoff rates may be the basis for setting consents for the drainage of surface water runoff from sites.

Greenfield runoff estimation for sites

www.uksuds.com | Greenfield runoff tool

Site coordinates

Latitude:	51.53783° N
Longitude:	0.13244° W
Reference:	5906391
Date:	2017-03-16T10:22:42

Methodology	IH124				
Site characteristics					
Total site area (ha)			1.138		
Methodology					
Qbar estimation metho	Calculate fro	om SPR a	nd SAAR		
SPR estimation method Calculate fro			om SOIL type		
			Default	Edited	
SOIL type			4	4	
HOST class					
SPR/SPRHOST			0.47	0.47	
Hydrological charact	eristic	s	Default	Edited	
SAAR (mm)			620	620	
Hydrological region			6	6	
Growth curve factor: 1 year			0.85	0.85	
Growth curve factor: 30 year			2.3	2.3	
Growth curve factor: 1	00 yea	ar	3.19	3.19	

Notes:

(1) Is Q_{BAR} < 2.0 l/s/ha?

(2) Are flow rates < 5.0 l/s?

Where flow rates are less than 5.0 l/s consents are usually set at 5.0l/s if blockage from vegetation and other materials is possible. Lower consent flow rates may be set in which case blockage work must be addressed by using appropriate drainage elements (3) Is SPR/SPRHOST \leq 0.3?

 Greenfield runoff rates
 Default
 Edited

 Qbar (I/s)
 4.77
 4.77

 1 in 1 year (I/s)
 4.05
 4.05

 1 in 30 years (I/s)
 10.96
 10.96

 1 in 100 years (I/s)
 15.21
 15.21

L

1

1

This report was produced using the greenfield runoff tool developed by HR Wallingford and available at www.uksuds.com. The use of this tool is subject to the UK SuDS terms and conditions and licence agreement, which can both be found at http://uksuds.com/terms-and-conditions.htm. The outputs from this tool have been used to estimate storage volume requirements. The use of these results is the responsibility of the users of this tool. No liability will be accepted by HR Wallingford, the Environment Agency, CEH, Hydrosolutions or any other organisation for use of this data in the design or operational characteristics of any drainage scheme.

GD Partnership Ltd					Page 1
The Cart Lodge					
Lullingstone Lane					4
Eynsford DA4 0HZ					Micro
Date 11/05/2017 19:53	Des	ianed by	WaterEnvi	onment	
File 17015 existing 1v FSR srcx	Che	cked by		onnene	Drainage
Micro Drainage	Sou	rce Contr	ol 2017 1		
	500		012017.1		
Summary of R	2 Poculto	for 1 ve	ar Return P	eriod	
<u>Summary or re</u>	Counts			chou	
Storm	Max	Max	Max Max	Status	
Event	Level	Depth Co	ntrol Volum	e	
	(m)	(m) (1/s) (m³)		
15 min Summer	20.258	0.258	88.9 4.	0 ОК	
30 min Summer	20.262	0.262	91.9 4.	1 0 K	
60 Min Summer	20.252	0.252	84.4 3.	8 OK	
120 min Summer	20.217	0.217	51 2 2	2 OK	
240 min Summer	20.178	0.178	43.3 1.	2 0 K 8 0 K	
360 min Summer	20.156	0.156	33.3 1.	3 0 K	
480 min Summer	20.141	0.141	27.6 1.	1 0 K	
600 min Summer	20.131	0.131	23.8 0.	9 ОК	
720 min Summer	20.123	0.123	20.9 0.	8 ОК	
960 min Summer	20.107	0.107	16.8 0.	6 ОК	
1440 min Summer	20.089	0.089	12.5 0.	4 ОК	
2160 min Summer	20.075	0.075	9.3 0.	3 O K	
2880 min Summer	20.067	0.067	7.6 0.	2 ОК	
4320 min Summer	20.059	0.059	5.6 0.	2 O K	
5760 min Summer	20.055	0.055	4.8 0.	2 O K	
7200 min Summer	20.052	0.052	4.0 0.	1 O K	
8640 min Summer	20.050	0.050	3.5 0.	1 OK	
10080 min Summer	20.047	0.04/	3.1 0.	1 0 K	
Storm	Rain	Flooded	Discharge [·]	Time-Peak	
Event ((mm/hr)) Volume	Volume	(mins)	
		(m³)	(m³)		
15 min Summer	32.223	3 0.0	68.9	14	
30 min Summer	20.981	L 0.0	89.7	22	
60 min Summer	13.233	3 0.0	113.2	36	
120 min Summer	8.176	o 0.0	139.8	66	
180 min Summer	6.139	9 0.0	15/.5	96	
240 min Summer 360 min Summer	2.005		100 0	120	
180 min Summon	3 010	, U.U A A A	190.0 190.0	100 216	
600 min Summer	2.553	3 0.0	203.9	306	
720 min Summer	2,233	3 0.0	229.1	366	
960 min Summer	1.806	5 0.0	247.1	488	
1440 min Summer	1.340	0.0	275.0	726	
2160 min Summer	0.995	5 0.0	306.3	1080	
2880 min Summer	0.805	5 0.0	330.2	1460	
4320 min Summer	0.597	7 0.0	367.3	2184	
5760 min Summer	0.483	3 0.0	396.3	2928	
7200 min Summer	0.410	0.0	420.5	3640	
8640 min Summer	0.359	9 0.0	441.5	4400	
10080 min Summer	0.320	0.0	460.1	5120	
<u></u>	87_70	17 YD Sol	lutions		
	02-20	11 VL 20			

GD Partnership Ltd		P	age 2
The Cart Lodge		ſ	
Lullingstone Lane		7	1
Evnsford DA4 0HZ			Jun
Date 11/05/2017 19:53	Designed by WaterF	invironment	
File 17015 existing 1v FSR srcx	Checked by		Jiainage
Micro Drainage	Source Control 2017	/ 1	
		•1	
Summary of F	sults for 1 year Retu	n Period	
<u>Summary or n</u>	Suits for I year Retur	<u>IT F CHOU</u>	
Storm	Max Max Max	Max Status	
Event	evel Depth Control V	olume	
	(m) (m) (1/s)	(m³)	
15 min Winter	0.274 0.274 100.5	4.5 O K	
30 min Winter	0.273 0.273 99.7 0.244 0.244 70.4	4.5 O K	
60 min Winter	$0.244 \ 0.244 \ 78.4$	3.6 UK	
120 Min Winter	0.190 0.190 52.8 3 173 0 173 10 6	2.2 UK 17 OK	
240 min Winter	A 156 0 156 33 3	1.7 OK 1.3 OK	
360 min Winter	a. 134 0. 134 24.9	1.0 OK	
480 min Winter	0.122 0.122 20.3	0.8 O K	
600 min Winter	0.109 0.109 17.3	0.6 O K	
720 min Winter	0.100 0.100 15.1	0.5 ОК	
960 min Winter	0.087 0.087 12.2	0.4 O K	
1440 min Winter	0.074 0.074 9.1	0.3 O K	
2160 min Winter	0.064 0.064 6.9	0.2 O K	
2880 min Winter	0.058 0.058 5.5	0.2 O K	
4320 min Winter	0.052 0.052 4.1	0.1 OK	
5760 min Winter	0.049 0.049 3.3	0.1 OK	
7200 min Winter	0.045 0.045 2.8	0.1 OK	
8640 min Winter	$0.041 \ 0.041 \ 2.5$	0.1 OK	
10080 WIN WINCER	0.038 0.038 2.2	0.1 UK	
Storm	Rain Flooded Dischar	ge Time-Peak	
Event	m/hr) Volume Volum	e (mins)	
	(m ³) (m ³)		
15 min Winter	2.223 0.0 77	.1 14	
30 min Winter	0.981 0.0 100	.5 22	
60 min Winter	3.233 0.0 126	.7 36	
120 min Winter	8.176 0.0 156	.6 68	
180 min Winter	6.139 0.0 176	96	
240 min Winter	5.003 0.0 191	.6 126	
360 min Winter	3.720 0.0 213	184	
480 min Winter	3.010 0.0 230	246	
500 min Winter	2.555 0.0 244	··> 300	
960 min Winter	2.235 U.U 250		
1440 min Winter	1,340 0.0 2/0	., 4 04 .0 712	
2160 min Winter	0.995 0.0 343	.1 1092	
2880 min Winter	0.805 0.0 369	.9 1432	
4320 min Winter	0.597 0.0 411	.4 2168	
5760 min Winter	0.483 0.0 443	.9 2832	
7200 min Winter	0.410 0.0 471	.0 3576	
8640 min Winter	0.359 0.0 494	.4 4400	
10080 min Winter	0.320 0.0 515	.3 5040	
©19	2-2017 XP Solutions		

GD Partnership Ltd		Page 3
The Cart Lodge		
Lullingstone Lane		Y_
Eynsford DA4 0HZ		Mirro
Date 11/05/2017 19:53	Designed by WaterEnvironment	Drainage
File 17015_existing_1y_FSR.srcx	Checked by	brainage
Micro Drainage	Source Control 2017.1	
	Rainfall Details	
Rainfall Model Return Period (years) Region Engla M5-60 (mm) Ratio R Summer Storms	FSR Winter Storms Y 1 Cv (Summer) 0.7 and and Wales Cv (Winter) 0.8 20.600 Shortest Storm (mins) 0.410 Longest Storm (mins) 100 Yes Climate Change %	es 50 40 15 80 +0
<u> </u>	<u>me Area Diagram</u>	
Tot	al Area (ha) 1.140	
Time (mins) Area Ti From: To: (ha) Fr	ime (mins) Area Time (mins) Area om: To: (ha) From: To: (ha)	
0 4 0.380	4 8 0.380 8 12 0.380	
· ·	1	
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GD Partnership Ltd		Page 1
The Cart Lodge		
Lullingstone Lane		4
Evnsford DA4 0HZ		Maria
Date 11/05/2017 19:53	Designed by WaterEnviron	ment MILLIU
File 17015 existing 30v FSR srcv	Checked by	Drainage
Micro Drainage	Source Control 2017 1	
	Source control 2017.1	
Summary of	esults for 30 year Return Per	iod
<u>Summary or r</u>		100
Storm	Max Max Max Max	Status
Event	Level Depth Control Volume	
	(m) (m) (1/s) (m ³)	
15 min Summer	20.406 0.406 218.9 8.5	О К
30 min Summer	20.412 0.412 225.9 8.6	0 К
60 min Summer	20.393 0.393 202.3 8.1	O K
120 min Summer	20.339 0.339 149.0 6.5	U K
240 min Summer	20.290 0.290 110.9 5.2	0 K
360 min Summer	20.209 0.209 97.1 4.4	
480 min Summer	20.209 0.209 59.5 2.6	0 K
600 min Summer	20.192 0.192 50.7 2.1	O K
720 min Summer	20.180 0.180 44.3 1.8	0 K
960 min Summer	20.161 0.161 35.3 1.4	0 K
1440 min Summer	20.136 0.136 25.7 1.0	0 К
2160 min Summer	20.115 0.115 18.7 0.7	ОК
2880 min Summer	20.099 0.099 14.8 0.5	ОК
4320 min Summer	20.081 0.081 10.8 0.3	О К
5760 min Summer	20.072 0.072 8.7 0.3	0 К
7200 min Summer	20.066 0.066 7.3 0.2	ОК
8640 min Summer	20.062 0.062 6.3 0.2	ОК
10080 min Summer	20.059 0.059 5.6 0.2	ОК
Storm	Rain Flooded Discharge Tim	ne-Peak
Event	(mm/hr) Volume Volume (mins)
	(m ³) (m ³)	
15 min Summer	79.107 0.0 169.1	13
30 min Summer	51.269 0.0 219.2	21
60 min Summer	31.749 0.0 271.5	36
120 min Summer	19.074 0.0 326.2	66
180 min Summer	14.006 0.0 359.3	96
240 min Summer	11.200 0.0 383.1	126
360 min Summer	8.170 0.0 419.1	188
480 min Summer	6.525 0.0 446.3	248
600 min Summer	5.477 0.0 468.3	306
720 min Summer	4./46 0.0 487.0	368
960 min Summer	3.783 U.U 517.6	486 720
1440 Min Summer	2.740 U.U 563.4 1 990 0.0 612 7	1088
2100 min Summer	1.583 0.0 612./	1444
4320 min Summer	1,146 0,0 705 3	2176
5760 min Summer	0.910 0.0 747.1	2856
7200 min Summer	0.761 0.0 781.0	3568
8640 min Summer	0.658 0.0 809.6	4400
10080 min Summer	0.581 0.0 834.5	5136
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GD Partnership Ltd		Page 2
The Cart Lodge		(C)
Lullingstone Lane		4
Evnsford DA4 0HZ		Mission
Date 11/05/2017 19:53	Designed by WaterEnvironment	
File 17015 existing 30v FSR srcv	Checked by	Drainage
Micro Drainago	Source Control 2017 1	
	Source control 2017.1	
Summary of P	cults for 30 year Peturn Period	
<u>Summary of Re</u>	suits for 50 year Return Periou	
Storm	Max Max Max Max Status	
Event	Level Depth Control Volume	
	(m) (m) (l/s) (m³)	
15 min Winter 2	0.429 0.429 247.6 9.0 O K	
30 min Winter 2	0.426 0.426 244.4 9.0 O K	
60 min Winter 2	0.383 0.383 189.5 7.9 O K	
120 min Winter 2	0.304 0.304 123.2 5.4 O K	
180 min Winter 2	0.263 0.263 92.2 4.2 O K	
240 min Winter 2	0.237 0.237 74.4 3.4 O K	
360 min Winter 2	0.200 0.200 54.7 2.3 O K	
480 min Winter 2	0.180 0.180 44.1 1.8 O K	
600 min Winter 2	0.165 0.165 37.0 1.5 0 K	
720 min Winter 2	0.152 0.152 32.0 1.3 0 K	
960 min Winter . 1440 min Winter .	0.135 0.135 25.5 1.0 UK	
2160 min Winter 2		
2100 Mill Willer 2 2880 min Winter 2	0.095 0.095 15.5 0.4 0 K	
4320 min Winter 2	0.001 0.001 10.7 0.5 0 K	
5760 min Winter	0.061 0.061 6.2 0.2 0 K	
7200 min Winter 2	0.057 0.057 5.3 0.2 0 K	
8640 min Winter 2	0.054 0.054 4.6 0.2 0 K	
10080 min Winter 2	0.052 0.052 4.1 0.1 O K	
Storm	Kain Flooded Discharge Time-Peak	
Event (nm/nr) volume volume (mins) (m ³) (m ³)	
15 min Winter	79.107 0.0 189.4 14	
30 min Winter	51.269 0.0 245.5 21	
60 min Winter	31.749 0.0 304.0 36	
120 min Winter	19.0/4 0.0 365.3 66	
240 min Winter	14.006 0.0 402.4 96	
360 min Winter	8 170 0 0 469 4 186	
480 min Winter	6.525 0.0 499.8 244	
600 min Winter	5.477 0.0 524.5 306	
720 min Winter	4.746 0.0 545.4 362	
960 min Winter	3.783 0.0 579.7 484	
1440 min Winter	2.746 0.0 631.0 726	
2160 min Winter	1.990 0.0 686.2 1104	
2880 min Winter	1.583 0.0 727.7 1464	
4320 min Winter	1.146 0.0 789.9 2148	
5760 min Winter	0.910 0.0 836.8 2848	
7200 min Winter	0.761 0.0 874.7 3640	
8640 min Winter	0.658 0.0 906.7 4208	
10080 min Winter	0.581 0.0 934.6 5208	
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The Cart Lodge Lullingstone Lane Eynsford DA4 0HZ Designed by WaterEnvironment Date 11/05/2017 19:53 Checked by File 17015_existing_30y_FSR.srcx Designed by WaterEnvironment Micro Drainage Source Control 2017.1 Rainfall Model FSR Winter Storms Return Period (years) 30 Cv (Summer) 0.750 Region England and Wales Cv (Winter) 0.8440 M5-60 (mm) 20.600 Shortest Storm (mins) 15 Ratio R 0.410 Longest Storm (mins) 15 Summer Storms Yes Climate Change % +0 Time Area Diagram Total Area (ha) 1.140 Time (mins) Area From: To: (ha) 0 4 0.380 4 8 0.380 8 12 0.380
Lullingstone Lane Eynsford DA4 0HZ Date 11/05/2017 19:53 File 17015_existing_30y_FSR.srcx Designed by WaterEnvironment Checked by Micro Drainage Source Control 2017.1 Rainfall Model FSR Winter Storms Region England and Wales Cv (Summer) 0.750 Region England and Wales Cv (Winter) 0.840 M5-60 (mm) 20.600 Shortest Storm (mins) 15 Ratio R 0.600 Shortest Storm (mins) 15 Summer Storms Yes Climate Change % +0 Time Area Diagram Total Area (ha) 1.140 Time (mins) Area From: To: (ha) 0 4 0.380 4 8 0.380 8 12 0.380
Eynsford DA4 0HZ Designed by WaterEnvironment Date 11/05/2017 19:53 Designed by WaterEnvironment File 17015_existing_30y_FSR.srcx Checked by Micro Drainage Source Control 2017.1 Relation of the second of the sec
Date 11/05/2017 19:53 Designed by WaterEnvironment File 17015_existing_30y_FSR.srcx Decided by Micro Drainage Source Control 2017.1 Rainfall Model FSR Return Period (years) 30 CV (Summer) 0.750 Return Period (years) 30 CV (Winter) 0.840 M5-60 (mm) 20.600 Shortest Storm (mins) 15 Ratio R 0.410 Longest Storm (mins) 10080 Summer Storms Yes Climate Change % +0 Time Area Diagram Total Area (ha) 1.140 Time (mins) Area From: To: (ha) 0 4 8 0.380 8 12 0.380
File 17015_existing_30y_FSR.srcx Checked by Checked by Micro Drainage Source Control 2017.1 Rainfall Model FSR Winter Storms Yes Return Period (years) 30 Cv (Summer) 0.750 Region England and Wales CV (Winter) 0.840 M5-60 (mm) 20.600 Shortest Storm (mins) 15 Ratio R 0.410 Longest Storm (mins) 10080 Summer Storms Yes Climate Change % +0 Time Area Diagram Total Area (ha) 1.140 Time (mins) Area From: To: (ha) From: To: (ha) 8 12 0.380 0 4 0.380 4 8 0.380 8 12 0.380 12 0.380
Micro Drainage Source Control 2017.1 Rainfall Model FSR Winter Storms Yes Return Period (years) 30 Cv (Summer) 0.750 Region England and Wales Cv (Winter) 0.840 M5-60 (mm) 20.600 Shortest Storm (mins) 15 Ratio R 0.410 Longest Storm (mins) 10080 Summer Storms Yes Climate Change % +0 <u>Time Area Diagram</u> Total Area (ha) 1.140 Time (mins) Area From: To: (ha) 0 4 0.380 4 8 0.380 8 12 0.380
Endinal DetailsMainfall ModelFSRWinter StormsYesRegion England and WalesCv (Summer) 0.750Magion England and WalesCv (Winter) 0.840MS-60 (mm)20.600Shortest Storm (mins) 1080Summer StormsYesClimate Change %Summer StormsYesClimate Change %Time (mins) AreaTime (mins) AreaTime (mins) AreaFrom:To:(ha)From:To:04 0.38048 0.380812 0.380
Rainfall ModelFSR 30Winter Storms (Summer) 0.750 Cv (Winter) 0.840 M5-60 (mm)20.600 Shortest Storm (mins) 15 Ratio R0.410 Longest Storm (mins) 10080 Summer StormsYes Yes Climate Change % +0Time Area Diagram Total Area (ha) 1.140Time (mins) Area From: To:Time (mins) Area From: To:Time (mins) Area From: To:Time (mins) Area From: To:Time (mins) Area A 8 0.380Summer Stores
Time Area DiagramTotal Area (ha) 1.140Time (mins) Area From: To: (ha)Time (mins) Area From: To: (ha)Time (mins) Area From: To: (ha)040.380480.3808120.380040.380480.3808120.380
Total Area (ha) 1.140 Time (mins) Area From: To: (ha) 0 4 0.380 4 8 0.380 8 12 0.380
Time (mins)Area From:Time (mins)Area From:Time (mins)Area From:040.380480.3808120.380
0 40.380 4 80.380 8 120.380
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GD Partnership Ltd		Page 1
The Cart Lodge		(C)
Lullingstone Lane		4
Evnsford DA4 0HZ		Mission
Date 11/05/2017 19:37	Designed by WaterEnvironment	MILIU
File 17015 existing 100v FSR srcv	Checked by	Drainage
Micro Drainage	Source Control 2017 1	
	5001Ce C010101 2017.1	
Summary of Re	esults for 100 year Return Period	
Storm	May May May May Status	
Event	Level Depth Control Volume (m) (m) (1/s) (m ³)	
15 min Summer	20.458 0.458 284.7 9.6 OK	
30 min Summer	20.466 0.466 295.6 9.7 O K	
60 min Summer	20.444 0.444 267.5 9.3 O K	
120 min Summer	20.388 0.388 195.9 8.0 0 K	
240 min Summer	20.308 0.308 126.2 5.6 0 K	
360 min Summer	20.267 0.267 95.2 4.3 0 K	
480 min Summer	20.241 0.241 76.8 3.5 O K	
600 min Summer	20.220 0.220 65.3 2.9 O K	
720 min Summer	20.203 0.203 56.6 2.4 0 K	
960 min Summer	20.182 0.182 45.1 1.9 0 K 20.154 0.154 32.6 1.3 0 K	
2160 min Summer	20.130 0.130 23.4 0.9 0 K	
2880 min Summer	20.115 0.115 18.5 0.7 O K	
4320 min Summer	20.092 0.092 13.3 0.4 O K	
5760 min Summer	20.080 0.080 10.6 0.3 O K	
7200 min Summer	20.073 0.073 9.0 0.3 0 K	
10080 min Summer	20.063 0.063 6.7 0.2 0 K	
Storm	Rain Flooded Discharge Time-Peak	
Event	(mm/hr) Volume Volume (mins) (m³) (m³)	
15 min Summer 3	102.810 0.0 219.8 13	
30 min Summer	67.170 0.0 287.2 22 41.754 0.0 257.2 22	
60 MIN SUMMER 120 min Summer	41.754 0.0 357.0 36 25.051 0.0 228.4 66	
180 min Summer	18.324 0.0 470.0 96	
240 min Summer	14.589 0.0 498.9 126	
360 min Summer	10.583 0.0 542.9 186	
480 min Summer	8.418 0.0 575.8 246	
600 min Summer	/.044 0.0 602.3 306 6.087 0.0 634.6 366	
960 min Summer	4.831 0.0 660.9 484	
1440 min Summer	3.483 0.0 714.7 726	
2160 min Summer	2.507 0.0 771.6 1088	
2880 min Summer	1.983 0.0 813.8 1464	
4320 min Summer	1.423 0.0 876.3 2184 1.124 0.0 022.5 2022	
5/60 min Summer 7200 min Summer	1.124 0.0 922.6 2920 0.935 0.0 959 7 3552	
8640 min Summer	0.805 0.0 990.8 4392	
10080 min Summer	0.708 0.0 1017.6 4960	
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GD Partnership Ltd					Page 2
The Cart Lodge					E
Lullingstone Lane					4
Evnsford DA4 0HZ					Marcon
Date 11/05/2017 19:37	Desic	ned by	WaterEnvi	ironment	MILIU
File 17015 existing 100v FSR srcv	Chec	ked by			Drainage
Micro Drainage	Sour	ce Contr	ol 2017 1		
	5001		012017.1		
Summary of Re	esults fo	or 100 ye	ear Return	Period	
		·			
Storm	Max	Max Donth Co	Max Max	Status	
Event	(m)	uepth Co (m) (ntroi voiu l/s) (m³	me)	
	()	(, (_, _, _, _, _,		
15 min Winter	20.492	0.492 0.492	321.2 10 321 7 10	.1 0 K	
60 min Winter	20.430	0.430	249.6 9	.1 0 K	
120 min Winter	20.356	0.356	161.7 7	.1 0 K	
180 min Winter	20.301	0.301	121.0 5	.4 O K	
240 min Winter	20.269	0.269	97.1 4	.4 O K	
360 min Winter	20.230	0.230	70.7 3	.2 ОК	
480 min Winter	20.203	0.203	56.6 2	.4 ОК	
600 min Winter	20.186	0.186	47.2 2	.0 ОК	
720 min Winter	20.174	0.174	41.1 1	.7 O K	
960 min Winter	20.154	0.154	32.6 1	.3 ОК	
1440 min Winter	20.130	0.130	23.6 0	.9 OK	
2160 min Winter	20.108	0.108	16.9 0	.6 OK	
2880 min Winter	20.093	0.093	13.5 0	.4 OK	
4320 min Winter	20.076	0.076	9.7 0	.3 O K	
5760 min Winter	20.068	0.068	7.8 0	.2 O K	
/200 min Winter	20.063	0.063	6.5 0	.2 OK	
8640 Min Winter	20.059	0.059	5.6 0	.2 UK	
TOOOD WITH MILLER.	20.050	0.050	4.9 0	.2 0 K	
Storm	Rain	Flooded	Discharge	Time-Peak	
Event	(mm/hr)	Volume	Volume	(mins)	
		(m²)	(m²)		
15 min Winter	102.810	0.0	246.1	14	
30 min Winter	67.170	0.0	321.6	21	
60 min Winter	41.754	0.0	399.9	36	
120 min Winter	25.051	0.0	479.8	66	
180 min Winter	18.324	0.0	526.4	96	
240 min Winter 360 min Winter	10 502	0.0	550.0	120	
480 min Winter	8 418	0.0	644 9	248	
600 min Winter	7 044	0.0 0 0	674 6	308	
720 min Winter	6.087	0.0	699.5	364	
960 min Winter	4.831	0.0	740.2	488	
1440 min Winter	3.483	0.0	800.4	728	
2160 min Winter	2.507	0.0	864.1	1108	
2880 min Winter	1.983	0.0	911.5	1468	
4320 min Winter	1.423	0.0	981.4	2128	
5760 min Winter	1.124	0.0	1033.3	2896	
7200 min Winter	0.935	0.0	1074.9	3600	
8640 min Winter	0.805	0.0	1109.7	4264	
10080 min Winter	0.708	0.0	1139.7	5000	
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GD Partnership Ltd		Page 3
The Cart Lodge		
Lullingstone Lane		Ly .
Eynsford DA4 0HZ		Mirro
Date 11/05/2017 19:37	Designed by WaterEnvironment	Drainage
File 17015_existing_100y_FSR.srcx	Checked by	enemilage
Micro Drainage	Source Control 2017.1	
	Rainfall Details	
Rainfall Model Return Period (years) Region Engla M5-60 (mm) Ratio R Summer Storms	FSR Winter Storms Y 100 Cv (Summer) 0.7 and and Wales Cv (Winter) 0.8 20.600 Shortest Storm (mins) 0.410 Longest Storm (mins) 100 Yes Climate Change %	es 50 40 15 80 +0
Tir	<u>ne Area Diagram</u>	
Tot	al Area (ha) 1.140	
Time (mins) Area Ti From: To: (ha) Fr	ime (mins) Area Time (mins) Area om: To: (ha) From: To: (ha)	
0 4 0.380	4 8 0.380 8 12 0.380	
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Water Environment Lt	d							Page 1
6 Coppergate Mews								
Brighton Road								4
Surbiton KT6 5NE								- Cu
D_{2} to $02/03/2018$ 15.4	6		Dociano	dh	. Cabrial	Fuo		MICLO
Date 02/03/2010 13:4	0 		Charles	u D <u>'</u>	y Gabilei	L.Eve		Drainage
File 17015_PlotA_sto	rage_100	•••	Спескеа	Уd				and the second s
Micro Drainage			Source (Cont	trol 2010	.1.1		
Summary	of Result	ts fo	<u>or 100 y</u>	ear	Return 1	Period	(+40응)	_
	Hal	f Dra	in Time :	14	minutes.			
Storm	Max M	lax	Max		Max	Max	Max	Status
Event	Level De	pth I	nfiltrati	ion	Control E	Outflow	Volume	200000
	(m) ((m)	(1/s)		(1/s)	(1/s)	(m³)	
15 min Summer	16.430 0.	430	(0.0	14.5	14.5	16.3	ОК
30 min Summer	16.514 0.	514 402	(J.U	14.5	14.5	19.5	O K
120 min Summer	16 360 0	493 360	(J.U	14.5 17 5	14.5 17 5	⊥ŏ./ 13 7	0 K
120 min Summer	16 252 0	200	(11 E	14.3 17 F	13.1 0 c	0 K
240 min Summer	16 190 0	292 180	().U	14.J	1/ 0	9.0 7 0	0 K
240 min Summer	16 140 0	1109 110	(⊥4.∠ 11 ⊑	14.Z	/.Z	OK
180 min Summer	16 120 0	120 120	(TT•2	C.TT	5./	OK
480 min Summer	16.129 0.	110	(.0	9.4	9.4	4.9	OK
600 min Summer	16.116 0.	107	(.0	8.0	8.0	4.4	O K
720 min Summer	16.10/ 0.	107	(J.U	7.0	7.0	4.1	OK
960 min Summer	16.094 0.	094	().0	5.6	5.6	3.6	OK
1440 min Summer	16.078 0.	0/8	().0	4.1	4.1	3.0	OK
2160 min Summer	16.066 0.	066	().0	3.0	3.0	2.5	ΟK
2880 min Summer	16.058 0.	058	(0.0	2.3	2.3	2.2	OK
4320 min Summer	16.048 0.	048	().0	1.7	1.7	1.8	ΟK
5760 min Summer	16.043 0.	043	(0.0	1.3	1.3	1.6	OK
/200 min Summer	16.039 0.	039	().0	1.1	1.1	1.5	OK
8640 min Summer	16.036 0.	036	().0	1.0	1.0	1.4	OK
10080 min Summer	16.034 0.	034	(0.0	0.8	0.8	1.3	OK
15 min Winter	16.504 0.	504	(0.0	14.5	14.5	19.2	ΟK
	Storm	Ra	ain Floo	oded	Discharge	Time-Pe	ak	
	Event	(mm	/hr) Vol	ume	Volume	(mins)	
			(m	1 ³)	(m³)			
		1 4 0	0.2.4	0 0	07.0		2.0	
15	min Summe	r 143	020	0.0	27.8) 1	∠∪ 20	
30	min Summe	r 94	.038	0.0	36.3)	29 16	
60	min Summe	r 58	.456	0.0	45.1		46	
120	min Summe	r 35	.0/2	0.0	54.2	_	/6	
180	min Summe	r 25	.654	0.0	59.4	- 1	.06	
240	min Summe	r 20	.424	0.0	63.1	. 1	.32	
360	min Summe	r 14	.816	0.0	68.7	1	.90	
480	min Summe	r 11	./86	0.0	72.8	2	:50	
600	min Summe	r 9	.862	0.0	76.2	3	310 10	
720	min Summe	r 8	.522	0.0	79.0	. 3	570	
960	min Summe	r 6	./64	0.0	83.6	, 4	192	
1440	min Summe	r 4	.8/6	0.0	90.4	. 7	34	
2160	min Summe	r 3	.509	0.0	97.6) 10	196	
2880	min Summe	r 2	. / / 6	0.0	102.9	14	156	
4320	min Summe	r 1	.993	0.0	110.8	22	204	
5760	min Summe	r 1	.574	0.0	116.7	29	04	
7200	min Summe	r 1	.310	0.0	121.4	36	0/2	
8640	min Summe	r 1	.12/	0.0	125.3	43	92	
10080	min Summe	r 0	.992	0.0	128.7	50	196	
15	mın Winte	r 143	.934	0.0	31.1		ZI	

Water Environment Lt	d						Page 2
6 Coppergate Mews							C
Brighton Road							4
Surbiton KT6 5NE							- m
Date 02/03/2018 15.4	6	Desi	aned by	v Gabriel	Eve		MICLO
File 17015 Plota sto	rage 100	Chec	rked by	y capitor			Drainage
Micro Drainage		Sour	Ce Cont	trol 2016	5 1 1		
		5001					
Summary	of Results	s for 1)0 vear	Return 1	Period	(+40%)	
<u>Bananar y</u>		<u>, 101 1</u>	<u>year</u>	<u>Itte curri</u>	01104	(100)	
Storm	Max Ma	x N	lax	Max	Max	Max	Status
Event	Level Dep	th Infil	tration	Control E	Outflow	Volume	
	(m) (m	.) (1	l/s)	(l/s)	(l/s)	(m³)	
30 min Winter	16.590 0.5	90	0.0	14.5	14.5	22.4	ОК
60 min Winter	16.539 0.5	39	0.0	14.5	14.5	20.5	0 K
120 min Winter	16.322 0.3	22	0.0	14.5	14.5	12.2	0 K
180 min Winter	16.189 0.1	89	0.0	14.2	14.2	7.2	O K
240 min Winter	16.154 0.1	54	0.0	12.0	12.0	5.9	ОК
360 min Winter	16.124 0.1	24 09	0.0	8.9	8.9	4.7	OK
400 min Winter 600 min Winter	16.097 0 0	97	0.0	/.⊥ 6 0	/.1 6 0	4.⊥ 3.7	OK
720 min Winter	16.089 0.0	89	0.0	5.2	5.2	3.4	0 K
960 min Winter	16.078 0.0	78	0.0	4.1	4.1	3.0	O K
1440 min Winter	16.066 0.0	66	0.0	3.0	3.0	2.5	O K
2160 min Winter	16.055 0.0	55	0.0	2.2	2.2	2.1	O K
2880 min Winter	16.049 0.0	49	0.0	1.7	1.7	1.8	O K
4320 min Winter 5760 min Winter	16.041 0.0	41 36	0.0	1.2	1.2	1.5	OK
7200 min Winter	16.033 0.0	33	0.0	0.8	0.8	1.2	OK
8640 min Winter	16.031 0.0	31	0.0	0.7	0.7	1.2	0 K
10080 min Winter	16.029 0.0	29	0.0	0.6	0.6	1.1	0 K
	C to a sum	Daia	5 1	Diselar a		- 1-	
	Storm	Rain (mm/hr)	Flooded	Discharge	Time-Pe	ak	
	Evenc	(1111/111)	(m ³)	(m ³)	(mins)	,	
			()	()			
30) min Winter	94.038	0.0	40.7		30	
60) min Winter	58.456	0.0	50.6		48	
100	min Winter	33.072	0.0	6U./	1	0U 04	
240) min Winter	20.424	0.0	70.7	1	32	
360	min Winter	14.816	0.0	76.9	1	92	
480	min Winter	11.786	0.0	81.6	2	52	
600	min Winter	9.862	0.0	85.3	3	10	
720	min Winter	8.522	0.0	88.5	3	72	
960) min Winter	6.764	0.0	93.6	4	96 26	
2160) min Winter	4.0/0	0.0	101.2	10	20 96	
2880) min Winter	2.776	0.0	115.3	14	60	
4320) min Winter	1.993	0.0	124.1	21	80	
5760) min Winter	1.574	0.0	130.7	28	72	
7200) min Winter	1.310	0.0	135.9	36	72	
8640	min Winter	1.127	0.0	140.3	44 50	00 40	
10080	, mith willer	0.992	0.0	144.1		- U	

Water Environment Ltd		Page 3
6 Coppergate Mews		C
Brighton Road		Ya
Surbiton KT6 5NE		Misco
Date 02/03/2018 15:46	Designed by Gabriel.Eve	MILIU
File 17015 PlotA storage 100	Checked by	Drainage
Micro Drainage	Source Control 2016.1.1	
Ra	ainfall Details	
Rainfall Model	FSR Winter Storms Ye	s
Return Period (years)	100 Cv (Summer) 0.75	0
Region Engl	and and Wales Cv (Winter) 0.84	0
Ratio R	0.410 Longest Storm (mins) 1008	0
Summer Storms	Yes Climate Change % +4	0
Ti	me Area Diagram	
Tot	al Area (ha) 0.103	
Time (mine) Area I	ime (ming) Area Time (ming) Area	
From: To: (ha) F	com: To: (ha) From: To: (ha)	
0 4 0.034	4 8 0.034 8 12 0.034	
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Water Environment Ltd					Page 4				
6 Coppergate Mews									
Brighton Road					Ly .				
Surbiton KT6 5NE					Mirro				
Date 02/03/2018 15:46	Designed	l by Gab	riel.Eve		Drainage				
File 17015_PlotA_storage_100	Checked	by			Diamage				
Micro Drainage	Source C	ontrol	2016.1.1						
	Madal Dat	aila							
	MODEL DEL	alls							
Storage is Or	nline Cover	Level (m	n) 17.500						
<u>Cellula</u>	<u>ir Storage</u>	<u>e Struct</u>	ure						
Inve	rt Level (m	n) 16.000) Safety Fac	tor 2.0					
Infiltration Coefficient	Base (m/hr) 0.0000) Poros	ity 0.95					
Infiltration Coefficient	Side (m/hr	.) 0.0000	C						
Depth (m) Area (m²) Inf. Ar	ea (m²) Der	oth (m) A	rea (m²) In:	f. Area (1	m²)				
0.000 40.0	0 0	0 601	1 0						
0.600 40.0	0.0	0.001	1.0		0.0				
	I								
<u>Hydro-Brake@</u>) Optimum	Outflow	Control						
Init	- Reference	MD-SHE-0	177-1460-06	00-1460					
Desig	gn Head (m)		117 1400 00	0.600					
Design	Flow (l/s)			14.6					
	Flush-Flo™ Objective	Minimis	Cal cal	culated storage					
2	Application	11111111111		Surface					
Sump	> Available			Yes					
Invert	imeter (mm) Level (m)			16.000					
Minimum Outlet Pipe Dia	ameter (mm)			225					
Suggested Manhole Dia	ameter (mm)			1200					
Control Po	oints	Head (m)	Flow (l/s)						
Design Point (C	alculated)	0.600	14.6						
200191 10110 (0	Flush-Flo™	0.267	14.5						
	Kick-Flo®	0.470	13.0						
Mean Flow over	Head Range	-	11.6						
The hydrological calculations have b	been based	on the He	ad/Discharge	e relation	nship for the				
Hydro-Brake® Optimum as specified.	Should ano	ther type	of control	device of	ther than a				
invalidated	en these st	orage rou	CING CALCULA	ations wi.	II De				
Depth (m) Flow (1/s) Depth (m) Flo	w (1/s) Der	oth (m) F	low (l/s) De	epth (m)	Flow (l/s)				
0.100 6.3 1.200	20.3	3.000	31.5	7.000	47.2				
0.200 14.3 1.400	21.8	3.500	33.9	7.500	48.9				
0.400 13.9 1.800	23.3	4.000	38.3	8.500	50.5 52.1				
0.500 13.4 2.000	25.9	5.000	40.3	9.000	53.6				
0.600 14.6 2.200	27.1	5.500	42.2	9.500	55.1				
0.800 16.7 2.400	28.2	6.000	44.0						
1.000 18.6 2.600 29.4 6.500 45.5									
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Water Environment Lt	d						Page 1
6 Coppergate Mews							C
Brighton Road							4
Surbiton KT6 5NE							1 mm
Data 02/02/2010 10 0	4			<u> </u>			Micro
Date 02/03/2018 16:0	4	Desi	.gned b	y Gabrie.	L.Eve		Drainage
File 17015_PlotB_sto	rage_100	. Chec	cked by				Diamage
Micro Drainage		Sour	ce Con	trol 2010	6.1.1		
Summary of	of Results	for 10	<u>)0 year</u>	Return	Period	(+40%)	_
	Half	Drain Ti	lme : 12	minutes.			
Storm	Max Max	ε M	lax	Max	Max	Max	Status
Event	Level Dept	h Infil	tration	Control S	Outflow	Volume	
	(m) (m)	(1	/s)	(1/s)	(l/s)	(m³)	
15 min Summer	17.949 0.44	19	0.0	23.0	23.0	25.6	ОК
30 min Summer	18.036 0.53	36	0.0	23.0	23.0	30.6	O K
60 min Summer	18.016 0.53	6	0.0	22.9	22.9	29.4	0 K
120 min Summer	17.884 0.38	34	0.0	23.0	23.0	21.9	0 K
180 min Summer	17.777 0.2	7	0.0	22.9	22.9	15.8	ОК
240 min Summer	17.715 0.2	5	0.0	22.3	22.3	12.2	O K
360 min Summer	17.673 0.1	13	0.0	17.7	17.7	9.9	0 K
480 min Summer	17.651 0.1	51	0.0	14.6	14.6	8.6	0 K
600 min Summer	17 636 0 17	36	0.0	12 4	12 4	7 8	0 K
720 min Summer	17 626 0 13	26	0.0	10.8	10 8	7 2	O K
960 min Summer	17 610 0 17	0	0.0	8 7	8 7	63	0 K
1440 min Summer	17 592 0 00	32	0.0	63	63	53	0 K
2160 min Summer	17 577 0 0	72 17	0.0	4 6	4 6	4 4	0 K
2880 min Summer	17 568 0 06	58	0.0	3.6	3.6	39	0 K
4320 min Summer	17 557 0 0	57	0.0	2.6	2.6	3.2	0 K
5760 min Summer	17 551 0.00	51	0.0	2.0	2.0	2.0	O K
7200 min Summer	17 546 0 04	16	0.0	1 7	1 7	2.5	0 K
8640 min Summer	17 543 0 04	13	0.0	1 5	1 5	2.0	O K
10080 min Summer	17 540 0 04	10	0.0	1 3	1 3	2.1	0 K
15 min Winter	18 023 0 52	2	0.0	23 0	23 0	29.8	0 K
	101020 0101		0.0	20.0	20.0	20.0	0 11
	Storm	Rain	Flooded	l Discharge	e Time-Pe	eak	
	Event	(mm/hr)	Volume	Volume	(mins)	
			(m³)	(m³)			
1 5	min Summor	142 031	0 0	121	1	20	
10 20	min Summer	94 038	0.0		-	29	
50	min Summer	58 156	0.0	, 50.4 1 70.1	- 1	46	
120	min Summer	35 070	0.0	, <u>, , , , ,</u> , , , , , , , , , , , , , , ,	-	76	
120	min Summer	25 654	0.0	92 1	- २ 1	104	
240	min Summer	20 121	0.0) 22) 1	132	
240	min Summer	14 816	0.0	1064	ς 1	192	
180	min Summer	11 786	0.0	1131		252	
400	min Summer	4 860 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.0	110	- 2 2 :	212	
720	min Summer	2.00Z 8.522	0.0	100	7 3	372	
960	min Summer	6 76/	0.0	122.	,,, _,, _	492	
1440	min Summer	4 876	0.0	140 4		736	
2160	min Summer	3.509	0.0	151 0	5 11	100	
2100	min Summer	2 776	0.0	159 0	- 1/	444	
4320	min Summer	1 993	0.0	172 1	, <u>1</u> 21	156	
5760		1.555	0.0	101	- 21	 	
3700	min Summer	1.5/4		I I X I ·	· · ·	17.11	
72.00	min Summer min Summer	1.5/4	0.0	181.3	5 36	564	
7200	min Summer min Summer min Summer	1.574 1.310 1.127	0.0	181.3 188.5 194.5	5 36 7 43	520 564 328	
7200 8640 10080	min Summer min Summer min Summer min Summer	1.574 1.310 1.127 0.992	0.0 0.0 0.0	181.3 188.5 194.7 199.9	5 25 5 36 7 43 9 40	564 328 984	
7200 8640 10080 15	min Summer min Summer min Summer min Summer min Winter	1.574 1.310 1.127 0.992 143.934	0.0 0.0 0.0 0.0	181.3 188.5 194.7 199.9 48.3	5 25 5 36 7 43 9 49	520 564 328 984 21	

Water Environment Lto	t t						Page 2
6 Coppergate Mews							
Brighton Road							4
Surbiton KT6 5NE							~~~
Date 02/03/2018 16.04	1	Desi	aned h	v Cabriel	Evo		- Micro
Eile 17015 Pletp stor	100	Char	lyneu D	y Gabilei	L.DVC		Drainage
File 17015_PlotB_Stor	rage_100	. Cnec	скеа ру				
Micro Drainage		Soui	cce Con	trol 2010	5.1.1		
<u>Summary c</u>	of Results	for 1	<u>00 year</u>	<u>Return</u>	Period ((+40%)	
			_				
Storm	Max Max	: I h Tofil	lax	Max Control 5	Max	Max	Status
Event	(m) (m)	······	(/s)	(1/s)	(1/s)	(m ³)	
	(,	·-	-, -,	(_/ _/	(=/ 0/	()	
30 min Winter	18.414 0.91	.4	0.0	28.1	28.1	34.5	O K
60 min Winter	18.061 0.56	51	0.0	23.0	23.0	32.0	ОК
120 min Winter	17 714 0.34	4	0.0	23.0	23.0	19.6 12.2	OK
240 min Winter	17.679 0.17	. - 19	0.0	22.3 18.5	22.3 18.5	10.2	OK
360 min Winter	17.646 0.14	6	0.0	13.7	13.7	8.3	O K
480 min Winter	17.627 0.12	7	0.0	11.0	11.0	7.2	O K
600 min Winter	17.615 0.11	.5	0.0	9.3	9.3	6.5	O K
720 min Winter	17.605 0.10	5	0.0	8.0	8.0	6.0	0 K
960 min Winter	17.593 0.09	13	0.0	6.4	6.4	5.3	OK
2160 min Winter	17 565 0.07	5	0.0	4.0	4.0 २.२	4.4	OK
2880 min Winter	17.558 0.05	58	0.0	2.7	2.7	3.3	0 K
4320 min Winter	17.548 0.04	8	0.0	1.9	1.9	2.7	0 K
5760 min Winter	17.543 0.04	3	0.0	1.5	1.5	2.4	O K
7200 min Winter	17.539 0.03	19	0.0	1.2	1.2	2.2	O K
8640 min Winter	17.536 0.03	6	0.0	1.1	1.1	2.1	ОК
10080 min Winter	17.534 0.03	4	0.0	0.9	0.9	1.9	ΟK
	Storm	Rain	Flooded	l Discharge	Time-Pea	ak	
	Event	(mm/hr)	Volume	Volume	(mins)		
			(m³)	(m³)			
20	and a state of a second	04 020	0.0				
50 60	min Winter	58 456	0.0) 78 5		29 18	
120	min Winter	35.072	0.0) 94.2		78	
180	min Winter	25.654	0.0	103.4	1	04	
240	min Winter	20.424	0.0	109.8	3 13	32	
360	min Winter	14.816	0.0) 119.4	1	92	
480	min Winter	11.786	0.0) 126.7	2:	52 1.2	
720	min Winter	9.862	0.0) 132.5) 3. L 3'	1 Z 7 A	
960	min Winter	6.764	0.0) 145.4	4	90	
1440	min Winter	4.876	0.0	157.2	2. 73	38	
2160	min Winter	3.509	0.0	169.8	108	38	
2880	min Winter	2.776	0.0	179.1	. 140	50	
4320	min Winter	1.993	0.0		s 214	4U 10	
7200	min Winter	1.310	0.0) 203.0	v ∠84 ? 36″	±0 72	
8640	min Winter	1.127	0.0	218.0) 43'	76	
10080	min Winter	0.992	0.0	223.9	502	16	
1							

a Coppergate News Image: Control of Control 2016.1.1 Subtict NY6 SNB Designed by Gabriel.Eve Date 02/03/2018 16:04 Source Control 2016.1.1 Wicro Drainage Source Control 2016.1.1 Coppergate News Source Control 2016.1.1 Micro Drainage 100 CV (Someer) 0.750 Return Period (years) 100 CV (Someer) 0.750 Return Period Source Control 2016.1.1 Source Control 2016.1.1 Micro Drainage 100 CV (Someer) 0.750 Return Period (years) 100 CV (Someer) 0.750 Summer Storms Yes Clinate Change 8 -40 Summer Storms Yes Clinate Change 8 -40 Summer Storms Yes Clinate Change 8 -40 O 4 0.003 4 0.003 8 12 0.003 0 4 0.003 4 0.003 12 0.003	Water Environment Ltd	Page 3							
Brighton Road Surpliton KYE 5NE Designed by Sabriel.Eve Date 02/03/0318 16:04 Checked by Source Control 2016.1.1 Micro Drainage Source Control 2016.1.1 Source Control 2016.1.1 Micro Drainage 100 Checked by Source Control 2016.1.1 Micro Drainage 0.410 Longest Storm (mins) 10080 Summer Storm (mins) 10080 Summer Storms 0.410 Longest Storm (mins) 10080 Summer Storm (mins) 10080 Summer Storms Checke (he) Store (he) O.15 Store (he) O.15 O 4 0.052 4 8 0.053 8 12 0.053 O 4 0.052 4 8 0.053 8 12 0.053	6 Coppergate Mews								
Surpiton TF6 5NB Date 02/03/2018 16:04 File 17015_PlotB_storage_00 Micro Drainage Source Control 2016.1.1 Checked by Micro Drainage Source Control 2016.1.1 Checked by Micro Drainage Source Control 2016.1.1 Checked by Micro Drainage Checked by Micro Drainage Checked by Micro Drainage Control 2016.1.1 Checked by Micro Drainage Checked by Micro Drainage Checked by Micro Drainage Control 2016.1.1 Checked by Micro Drainage Checked by	Brighton Road								
Date 02/03/2018 16:04 Designed by Gabriel.Eve Decoded by Micro Drainage Source Control 2016.1.1 Source Control 2016.1.1 Minter Storms Ves Return Period (years) 100 CV (Winter) 0.750 Region England and Wales CV (Winter) 0.750 Region England and Wales 101 CV (Winter) 0.750 Region England and Wales CV (Winter) 0.750 Region England and Wales 101 CV (Winter) 0.750 Region England and Wales CV (Winter) 0.750 Region England and Wales 102 Col tem) 2.0400 Shortest Storm (mins) 103 Region England and Wales CV (Winter) 0.740 Region England and Wales 102 Minter Storms 100 CV (Summer) 0.750 Region England and Wales CV (Winter) 0.740 Region England and Wales 103 Lato Region England and Wales CV (Winter) 0.740 Region England and Wales CV (Winter) 0.740 Region England and Wales 103 Lato Region England and Wales CV (Winter) 0.740 Region England And Wales Tree (mins) Area 104 Area (ha) 0.160 Tree (mins) Area Time (mins) Area Time (mins) Area 104 A 0.053 8 12 0.053 8 12 0.053 105 Region England And Wales Region England And Wales Region England And Wales	Surbiton KT6 5NE	- m							
Pile 17015_PlotB_storage_100 Checked by Micro Drainage Source Control 2016.1.1 Enifall Model EX Micro Drainage CN Winter Storms Vecs Return Period (vers) Dig of Ninter Storms Vecs Exe (winter) 0.840 Micro Drainage 20.600 Shortest Storm (wins) 0.000 Exe (winter) 0.840 Micro Drainage 20.600 Shortest Storm (wins) 0.000 Exe (winter) 0.840 Micro Drainage Yes Clinate Changes * 440 Micro Trainage Yes Clinate Changes * 440 Micro Trainage Yes Clinate Change * 400 Micro Trainage Yes Time (mins) Area Time (mins) Area Time (mins) Area From: To: (ha) Yes Yes Yes Yes Yes O 4 0.053 9 12 0.053 Yes Yes Yes Micro Trainage Yes Yes Yes	Date 02/03/2018 16:04	Designed by Gabriel.Eve							
Micro Drainage Source Control 2016.1.1 Rainfall Details Region England and Nules CV (Winter) 0.840 MS-60 (mm England and Nules CV (Winter) 0.840 MS-60 (mm England and Nules CV (Winter) 0.840 MS-60 (mm England and Nules CV (Winter) 0.840 MS-60 (mins) 10080 Summer Storms Yes Climate Change 8 +40 Time Area Diagram Total Area (ha) 0.160 Time (mins) Area Time (mins) Area Time (mins) Area From: To: (ha) Time (mins) Area Time (mins) Area From: To: (ha) 4 8 0.053 8 12 0.053 0 4 0.053 4 8 0.053 8 12 0.053	File 17015 PlotB storage 100	Checked by Drainage							
Britfield Details Frinfield (verie) 10 CV (Summer) 0.750 Defoit Region Regional and Wales CV (Winter) 0.800 Defoit Rung 20.600 Shortbest Storm (mins) 1080 Summer Storm Yes Climate Change 8 + 400 Defoit Rung 20.600 Shortbest Storm (mins) 1080 Summer Storm Time Area Diagram Total Area (ha) 0.101 0 0 4 0.053 4 8 0.053 8 12 0.033	Micro Drainage	Source Control 2016.1.1							
Paintall DecailsMaintall ModelFileWinter Storm MinsMaintall ModelColspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2">Colspan="2"Maintall Colspan="2">Colspan="2"Maintall Colspan="2"Colspan="2">Colspan="2"Maintall Colspan="2"Colspan="2">Colspan="2"Maintall Colspan="2"Colspan="2">Colspan="2"Maintall Colspan="2"Colspan="2"Maintall Colspan="2"Colspan="2"Colspan="2"Maintall Cols									
Rainfall Model FSR Winter Storms / Yes Segior England and Male CY (Winter) 0.840 Stafio B 0.400 Shortest Storm (mins) 105 Summer Storms Yes Clinate Change 6 Junter Storms Yes Clinate Change 6 Summer Storms Yes Clinate Change 6 Junter Storms Yes Storm 7 Yes Junter Storms Yes Storm 7	Ra	ainfall Details							
Rainfall Model FR Minter Storms 'Pe Return Period (years) 100 Cv (Winter) 0.780 No-60 (nn) 20.600 Shortest Storm (nins) 15 Ratia R 0.410 Longest Storm (nins) 1080 Jummer Storms Yes Climate Change N 400 The Area Diagram Totl Area (ha) 0.160 Mine (mins) Area Time (mins) Area									
Notice Field of Sector Sector Sector (sinker) 0.840 Notice Sector Sector (sinker) 0.840 Satio 0.600 Summer Storm Yes Clinate Change 8 4.40 Difference 0.840 Summer Storm Yes Clinate Change 8 4.40 Difference 0.840 Summer Storm Yes Clinate Change 8 4.40 Difference 0.840 Storm Yes Clinate Change 8 4.40 Difference 0.840 O 4.053 A 8.053 Storm 12.053	Rainfall Model	FSR Winter Storms Yes							
MS-60, rml Summer Storm 20.600 Shortest Storm (mins) 105 0.410 Longest Storm (mins) 105 200 Climate Change 8 -440 Clim	Region Engl	and and Wales Cv (Winter) 0.840							
Mails R 0.410 Longest Storm (mins) 1080 Yes Summer Storm Time Area Diaram Tatl Area (ha) 0.160 Totl Area (ha) 0.160 Time (mins) Area Trime (mins) Area Trime (mins) Area Trime (mins) Area (ha) 0.053 8 12 0.053 0 4 0.053 4 0.053 8 12 0.053	M5-60 (mm)	20.600 Shortest Storm (mins) 15							
Time treating Time Area Diagram Total Area (ha) 0.161 Time (mins) Area (ha) Time (nins) Area (ha) (ha) (ha) (ha) (ha) (ha) (ha) (ha	Ratio R Summer Storms	0.410 Longest Storm (mins) 10080							
Time Area DiagramTotal Area (h) 0.101Time (mine) Area (from: To: (ha) (from: T	Summer Storms	165 Climate Change 6 140							
Total Area (ha) 0.160 Time (mins) Area (rea) Tore (real) 0 4 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0	<u>Ti</u>	me Area Diagram							
Time (mins) Area From: Time (mins) Area From: Time (mins) Area From: Time (mins) Area Time (mins) 0 4 0.053 4 8 0.053 8 12 0.053 0 4 0.053 4 8 0.053 8 12 0.053	Tot	al Area (ha) 0.160							
0 4 0.053 4 8 0.053 8 12 0.053	Time (mins) Area T. From: To: (ha) Fr	ime (mins) Area Time (mins) Area rom: To: (ha) From: To: (ha)							
©1982-2016 XP Solutions	0 4 0 052	4 8 0 053 8 12 0 053							
01982-2016 XP Solutions	0 4 0.055	4 0 0.035 0 12 0.035							
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Water Environment	Ltd					Page 4	
6 Coppergate Mews							
Brighton Road						L	
Surbiton KT6 5NE						Miero	
Date 02/03/2018 1	6:04	Designed	l by Gab	riel.Eve			
File 17015_PlotB_	storage_100	Checked	by			Diamage	
Micro Drainage	<u> </u>	Source (Control 2	2016.1.1			
	<u>1</u>	Model Det	<u>ails</u>				
		1. 0	- 1 (. 10 100			
	Storage is Un	lline Cover	Tevel (m	1) 19.100			
	Cellula	r Storage	e Struct	ure			
		-					
	Inve	rt Level (n	n) 17.500) Safety Fac	ctor 2.0		
Infiltr Infiltr	ration Coefficient	Base (m/h) Side (m/h)	r) 0.00000 r) 0.00000) Poros	sity 0.95		
11111101	deron coerrectene	5100 (10/11)	.) 0.00000				
Depth (m)	Area (m ²) Inf. Are	ea (m²) Dej	pth (m) A	rea (m²) In	f. Area ((m²)	
0.000	60.0	0.0	0.601	1.0		0.0	
0.600	60.0	0.0					
	<u>Hydro-Brake®</u>) Optimum	Outilow	Control			
	Unit	Reference	MD-SHE-0	216-2300-06	00-2300		
	Desig	n Head (m)		220 2000 00	0.600		
	Design	Flow (l/s)			23.0		
		Flush-Flo TM		Cal	culated		
		Objective	Minimis	se upstream	storage		
	A	application			Surface		
	Sump	Available			Yes		
	Dia	imeter (mm)			210		
Minim	um Outlet Pipe Dia	meter (mm)			17.300 300		
Sug	gested Manhole Dia	ameter (mm)			1200		
			- 1 ()				
	Control Po	oints	Head (m)	Flow (1/s)			
	Design Point (Ca	alculated)	0.600	23.0			
]	Flush-Flo™	0.311	23.0			
	Mean Flow over 1	Kick-Flo®	0.497	21.0			
	Mean FIOW OVEL 1	neau nange		± / • /			
The hydrological c	alculations have b	been based	on the He	ad/Discharg	e relatio	onship for the	
Hydro-Brake® Optim	um as specified.	Should and	ther type	e of control	device c	other than a	
Hydro-Brake Optimu	m® be utilised the	en these st	orage rou	ting calcul	ations wi	ll be	
invalidated							
Depth (m) Flow (1	/s) Depth (m) Flow	w (1/s) Deg	pth (m) F	low (l/s) D	epth (m)	Flow (l/s)	
0.100	1 000	22 0	2 000	40.0	7 000	74 0	
0.100 2	1.3 1.200 1.1 1.400	32.U 31 5	3.000	49.8	7.000	/4.8	
0.200 2	2 9 1 600	36 8	4 000	57 2	8 000	80 1	
0.400 2	2.5 1 800	38 9	4.500	60 7	8 500	82 6	
0.500 2	1.1 2.000	41.0	5.000	63 9	9,000	85 0	
0.600 2	3.0 2.200	42.9	5.500	66.9	9.500	87.3	
0.800 2	6.4 2.400	44.7	6.000	69.8			
1.000 2	9.4 2.600	46.5	6.500	72.1			
		,		1			
	@1000	-2016 100	Colution				
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Water Environment Ltd							Page 1	
6 Coppergate Mews								C
Brighton Road								4
Surbiton KT6 5NE								m
Date 02/03/2018 16.2	6		Desi	aned h	v Gabrie	l Eve		- MICLO
File 17015 Plote storage 100 Checked by								Drainage
File 1/015_PlotC_storage_100 [Checked by								
Micro Drainage			Sour	ce Con	trol 201	6.1.1		
	6 D	1. 6	1.0	0	5	- · ·	(
Summary	of Resu	ilts i	or 10	0 year	Return	Period	(+40%)	-
			i. mi					
	Н	ali Dra	ain Ti	me : 14	minutes.			
Storm	Max	Max	м	ax	Max	Max	Max	Status
Event	Level	Depth	Infilt	ration	Control E	Outflow	Volume	
	(m)	(m)	(1	/s)	(1/s)	(l/s)	(m³)	
15 min Summer	17.751	0.651		0.0	82.4	82.4	95.8	OK
50 min Summer	17 959	0.759		0.0	82.4	02.4 92.4	111 6	OK
120 min Summer	17 695	0.750		0.0	02.4 92.4	02.4 92.4	96 2	OK
120 min Summer	17 520	0.100		0.0	02.4	02.4	61 6	O K
240 min Summer	17 440	0.439		0.0	01.0	01.0 70 E	04.0 51 /	OK
240 min Summer	17 205	0.349		0.0	19.0	19.5	JI.4	OK
360 min Summer	17.385	0.285		0.0	63.7	63.7	41.9	O K
480 min Summer	17.350	0.250		0.0	52.4	52.4	30.8	O K
600 min Summer	17.326	0.226		0.0	44./	44./	33.3	OK
/20 min Summer	17.308	0.208		0.0	39.1	39.1	30.6	OK
960 min Summer	17.283	0.183		0.0	31.4	31.4	27.0	OK
1440 min Summer	17.254	0.154		0.0	23.0	23.0	22.6	OK
2160 min Summer	17.229	0.129		0.0	16.7	16.7	19.0	OK
2880 min Summer	17.214	0.114		0.0	13.2	13.2	16.7	ΟK
4320 min Summer	17.195	0.095		0.0	9.5	9.5	14.0	ОК
5760 min Summer	17.184	0.084		0.0	7.5	7.5	12.4	OK
7200 min Summer	17.177	0.077		0.0	6.3	6.3	11.3	OK
8640 min Summer	17.171	0.071		0.0	5.4	5.4	10.4	O K
10080 min Summer	17.166	0.066		0.0	4.7	4.7	9.8	ОК
15 min Winter	17.853	0.753		0.0	82.4	82.4	110.9	0 K
	Storm	F	Rain	Flooded	d Discharge	e Time-Pe	eak	
	Event	(m	m/hr)	Volume	Volume	(mins)	
				(m³)	(m³)			
15	min Sum	mer 14	3.934	0.0) 157.1	1	20	
30	min Sum	mer 9	4.038	0.0) 2.05	4	29	
60	min Sum	mer 5	8.456	0.0) 255	5	46	
120	min Sum	mer 3	5.072	0.0) 306 4	-	76	
120	min Sum	mer 2	5.654	0.0) 3364	4 7	106	
240	min Sum	mer 2	0.424	0.0) 357	1 1	132	
360	min Sum	mer 1	4.816	0.0) 388 (- 6 î	192	
480	min Sum	mer 1	1.786	0.0) 412	1 3	252	
600	min Sum	mer	9.862	0.0) 431	1 3	312	
720	min Sum	mer	8.522	0.0) 447 ()	372	
960	min Sum	mer	6.764	0.0) 473 () 4	492	
1440	min Sum	mer	4.876	0.0) 511	5	736	
2160	min Sum	mer	3.509	0.0) 552.1	3 11	100	
2880	min Sum	mer	2.776	0.0) 582 (5 14	456	
4320	min Sum	mer	1.993	0.0) 627 3	2 22	200	
5760	min Sum	mer	1.574	0.0) 660	5 29	372	
7200	min Sum	mer	1.310	0.0) 687.0) 36	632	
8640	min Sum	mer	1.127	0.0	709.3	3 44	400	
10080	min Sum	mer	0.992	0.0) 728.4	4 51	136	
15	min Win	ter 14	3.934	0.0) 176.0	0	21	

Water Environment Lt	d						Page 2
6 Coppergate Mews							
Brighton Road							4
Surbiton KT6 5NE							- m
Date 02/03/2018 16:2	6	Desi	igned b	v Gabrie	l.Eve		MICIO
File 17015 PlotC sto	Drainage						
Micro Drainago	1490_100.	. Cilico		+rol 2010	<u> </u>		
MICIO DIAINAge		5001		101 201	0.1.1		
Cummo ret	of Dogulta	for 1	0.0	Doturn	Doriod	(+10%)	
<u>Summary</u>	JI RESULLS	101 1	<u>oo year</u>	Return	reriou	(+40%)	-
Storm	May May	r 1	lav	Mav	Mav	Max	Status
Event	Level Dept	- th Infil	tration	Control S	Outflow	Volume	beacab
	(m) (m)) (1	l/s)	(l/s)	(1/s)	(m³)	
		-					
30 min Winter	17.997 0.89	97	0.0	82.4	82.4	132.0	OK
60 min Winter 120 min Winter	17 636 0 5	34 36	0.0	82.3 82.4	82.3 82.4	122.8 79 0	OK
180 min Winter	17.452 0.3	52	0.0	79.6	79.6	51.8	0 K
240 min Winter	17.396 0.2	96	0.0	67.1	67.1	43.5	0 K
360 min Winter	17.342 0.24	12	0.0	49.8	49.8	35.6	ОК
480 min Winter	17.311 0.23	11	0.0	40.0	40.0	31.1	ОК
600 min Winter	17.290 0.19	90	0.0	33.5	33.5	28.0	0 K
720 min Winter	17.275 0.1	75	0.0	29.1	29.1	25.8	0 K
960 min Winter	17.254 0.1	54	0.0	23.2	23.2	22.7	ОК
1440 min Winter	17.229 0.12	29	0.0	16.8 12 1	16.8 10.1	19.0	OK
2160 Min Winter 2880 min Winter	17 196 0 01	18	0.0	12.1	96	13.9 14 1	OK
4320 min Winter	17.181 0.08	31	0.0	6.9	6.9	11.9	0 K
5760 min Winter	17.171 0.0	71	0.0	5.4	5.4	10.5	0 K
7200 min Winter	17.165 0.00	65	0.0	4.5	4.5	9.5	ОК
8640 min Winter	17.160 0.0	50	0.0	3.9	3.9	8.8	ОК
10080 min Winter	17.156 0.0	56	0.0	3.4	3.4	8.3	0 K
						_	
	Storm	Rain	Flooded	d Discharge	e Time-Pe	eak	
	Event	(mm/hr)	Volume	volume	(mins)	
			(11-)	(
30	min Winter	94.038	0.0	230.0)	31	
60	min Winter	58.456	0.0	286.2	2	48	
120	min Winter	35.072	0.0	343.4	1	80	
180	min Winter	25.654	0.0	376.8	3 1	L04	
240	min Winter	20.424	0.0	400.0) 1	132	
360	min Winter	11 700	0.0	J 435.2		192	
480	min Winter	11./20 ττ./20	0.0) 401.0 1 / 22.0	ν 2	2.JZ R1.4	
720	min Winter	8.522	0.0) 500.5	, . , .	374	
960	min Winter	6.764	0.0	529.8	3 4	194	
1440	min Winter	4.876	0.0	572.9	9 7	734	
2160	min Winter	3.509	0.0	0 618.6	5 11	L04	
2880	min Winter	2.776	0.0	652.5	5 14	164	
4320	min Winter	1.993	0.0	702.5	5 21	L96	
5760	min Winter	1.574	0.0	J 739.7	/ 28	364	
/200	min Winter	1 107	0.0) /69.5) 701 /) 36 1 ∧≏	040 844	
10080	min Winter	1.12/	0.0) 815 P	- 43 3 51	12	
10000	WINCOL	0.992	0.0	. 010.0			

Water Environment Ltd	Page 3					
6 Coppergate Mews						
Brighton Road	<u> </u>					
Surbiton KT6 5NE						
Date 02/03/2018 16:26	Designed by Gabriel.Eve					
File 17015 PlotC storage 100	Checked by					
Micro Drainage	Source Control 2016.1.1					
Ra	infall Details					
Rainfall Model Return Period (years) Region Engli	FSR Winter Storms Yes 100 Cv (Summer) 0.750 and and Wales Cv (Winter) 0.840					
M5-60 (mm) Ratio R Summer Storms	20.600 Shortest Storm (mins) 15 0.410 Longest Storm (mins) 10080 Yes Climate Change % +40					
	m <u>e Area Diagram</u>					
Tot	al Area (ha) 0.583					
Time (mins) Area Ti From: To: (ha) Fr	ime (mins) Area Time (mins) Area com: To: (ha) From: To: (ha)					
0 4 0.194	4 8 0.194 8 12 0.194					
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Water Environment Ltd			Page 4				
6 Coppergate Mews							
Brighton Road							
Surbiton KT6 5NE			Miero				
Date 02/03/2018 16:26	Designed by Gab	riel.Eve					
File 17015_PlotC_storage_100	Checked by		Diamage				
Micro Drainage	Source Control	2016.1.1					
<u>M</u>	<u>lodel Details</u>						
Storage is On	line Cover Level (m	18.300					
	11110 00001 10001 (., 10.000					
Cellular	<u>r Storage Struct</u>	ure					
Turren	+ T 1 () 17 10(0				
Inver Infiltration Coefficient	t Level (m) 17.100 Base (m/hr) 0.00000) Salety Factor 2.) Porosity 0.9	5				
Infiltration Coefficient	Side (m/hr) 0.00000) D	-				
Donth (m) Area (m^2) Inf Area	(m^2) Donth (m) A	$rop (m^2)$ Inf Arop	(m ²)				
Depth (m) Area (m) Inf. Are		iea (m) ini. Aiea	(
0.000 155.0	0.0 1.001	1.0	0.0				
1.000 155.0	0.0						
Hydro-Brake®	Optimum Outflow	Control					
Unit	Reference MD-SHE-0	364-8250-1000-8250					
Design Design 1	n Head (m) Flow (l/s)	82.5					
	Flush-Flo™	Calculated					
	Objective Minimis	e upstream storage					
Ap	pplication	Surface					
Diar	neter (mm)	364					
Invert	Level (m)	17.100					
Minimum Outlet Pipe Diar	meter (mm)	450					
Suggested Mannole Diar	neter (mm)	2100					
Control Poi	ints Head (m)	Flow (l/s)					
Design Point (Ca	lculated) 1.000	82.5					
F	lush-Flo™ 0.518	82.4					
	Kick-Flo® 0.827	75.2					
Mean Flow over H	ead Range -	63.8					
The hydrological calculations have be	een based on the He	ad/Discharge relati	onship for the				
Hydro-Brake® Optimum as specified.	Should another type	of control device	other than a				
Hydro-Brake Optimum® be utilised then	n these storage rou	ting calculations w	vill be				
Depth (m) Flow (1/s) Depth (m) Flow	(l/s) Depth (m) F	low (l/s) Depth (m)	Flow (l/s)				
0.100 10.4 1.200	90.1 3.000	140.7 7.000	213.1				
0.200 36.5 1.400	97.1 3.500	151.7 7.500	220.4				
0.300 68.3 1.600	103.6 4.000	162.0 8.000	227.5				
	115 5 5 000	180 7 8.500	234.4				
0.600 81.9 2.200	121.0 5.500	189.3 9.500	241.1				
0.800 76.6 2.400	126.2 6.000	197.6	217.0				
1.000 82.5 2.600	131.2 6.500	205.5					
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91902							


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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - A-1 Finish: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	376 m ²	As supplied by Client
Storage area:	376 m ²	As supplied by Client
Maximum allowable runoff:	5.3 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 40 minutes	1.8
10 mins	0.0492	32	1 hour and 10 minutes	2.6
15 mins	0.0397	37	1 hour and 20 minutes	2.9
30 mins	0.0260	45	1 hour and 30 minutes	3.2
1 hour	0.0163	48	1 hour and 40 minutes	3.3
2 hours	0.0097	42	1 hour and 30 minutes	3.1
4 hours	0.0057	27	1 hour and 0 minutes	2.3
6 hours	0.0041	19	0 hours and 40 minutes	1.8
10 hours	0.0028	13	0 hours and 20 minutes	1.2
24 hours	0.0014	9	0 hours and 10 minutes	0.6
48 hours	0.0008	8	0 hours and 0 minutes	0.3

Total storage required: 18 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRG B75		
Description:	BRG B75 - including 20mm reservoir layer to store water for biodiverse roof vegetation		

	m ³
Number of Blue Roof outlets: 2	

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	07/06/2017
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - A-2 Finishes: Paved

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	299 m ²	As supplied by Client
Storage area:	299 m ²	As supplied by Client
Maximum allowable runoff:	4.2 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 40 minutes	1.7
10 mins	0.0492	31	1 hour and 0 minutes	2.3
15 mins	0.0397	37	1 hour and 10 minutes	2.5
30 mins	0.0260	44	1 hour and 30 minutes	2.8
1 hour	0.0163	45	1 hour and 30 minutes	2.9
2 hours	0.0097	38	1 hour and 20 minutes	2.6
4 hours	0.0057	23	0 hours and 50 minutes	1.9
6 hours	0.0041	16	0 hours and 30 minutes	1.4
10 hours	0.0028	11	0 hours and 20 minutes	1.0
24 hours	0.0014	8	0 hours and 0 minutes	0.5
48 hours	0.0008	7	0 hours and 0 minutes	0.3

Total storage required: 13.6 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRB A58	
Description:	ABG blueroof BRB A58 - 58mmdeep system	

Total storage capacity:	14.9 m ³
Number of Blue Roof outlets:	2

Notes:

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Project Name:	Ugly Brown Bu
Prepared for:	Water Enviror
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area

Ugly Brown Building, Camden Water Environment Limited 28/02/2018 11723 MG Drainage Area - B-1 Finishes: BIODIVERSE

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	341 m ²	As supplied by Client
Storage area:	341 m ²	As supplied by Client
Maximum allowable runoff:	4.8 l/s	As supplied by Client

Output - Rainfall Calculation					
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)	
5 mins	0.0602	20	0 hours and 30 minutes	2.4	
10 mins	0.0492	31	0 hours and 50 minutes	3.4	
15 mins	0.0397	36	0 hours and 50 minutes	3.7	
30 mins	0.0260	41	1 hour and 0 minutes	4.1	
1 hour	0.0163	41	1 hour and 0 minutes	4.0	
2 hours	0.0097	31	0 hours and 50 minutes	3.3	
4 hours	0.0057	18	0 hours and 20 minutes	2.2	
6 hours	0.0041	13	0 hours and 10 minutes	1.6	
10 hours	0.0028	10	0 hours and 10 minutes	1.1	
24 hours	0.0014	9	0 hours and 0 minutes	0.5	
48 hours	0.0008	8	0 hours and 0 minutes	0.3	

Total storage required: 14.1 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRB B75		
Description:	75mmdeep system		
Total storage capacity:	19.7 m ³		

Number	of Blue	Roof	outlets:

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - B-2, Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	204 m ²	As supplied by Client
Storage area:	204 m ²	As supplied by Client
Maximum allowable runoff:	2.9 l/s	As supplied by Client

Output - Rainfall Calculation					
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)	
5 mins	0.0602	20	0 hours and 30 minutes	1.4	
10 mins	0.0492	31	0 hours and 50 minutes	1.9	
15 mins	0.0397	36	1 hour and 0 minutes	2.1	
30 mins	0.0260	41	1 hour and 10 minutes	2.3	
1 hour	0.0163	41	1 hour and 10 minutes	2.3	
2 hours	0.0097	31	0 hours and 50 minutes	2.0	
4 hours	0.0057	18	0 hours and 30 minutes	1.3	
6 hours	0.0041	12	0 hours and 20 minutes	1.0	
10 hours	0.0028	9	0 hours and 10 minutes	0.6	
24 hours	0.0014	7	0 hours and 0 minutes	0.3	
48 hours	0.0008	7	0 hours and 0 minutes	0.2	

Total storage required: 8.5 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRB B75		
Description:	75mmdeep system		
Total storage capacity:	11.8 m ³		

	0			
Number	of B	lue Ro	oof ou	utlets

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - B-3 Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	186 m ²	As supplied by Client
Storage area:	186 m ²	As supplied by Client
Maximum allowable runoff:	2.6 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 30 minutes	1.4
10 mins	0.0492	31	0 hours and 50 minutes	1.9
15 mins	0.0397	35	1 hour and 0 minutes	2.1
30 mins	0.0260	40	1 hour and 0 minutes	2.3
1 hour	0.0163	39	1 hour and 0 minutes	2.2
2 hours	0.0097	29	0 hours and 50 minutes	1.8
4 hours	0.0057	16	0 hours and 20 minutes	1.2
6 hours	0.0041	11	0 hours and 20 minutes	0.9
10 hours	0.0028	9	0 hours and 10 minutes	0.6
24 hours	0.0014	7	0 hours and 0 minutes	0.3
48 hours	0.0008	7	0 hours and 0 minutes	0.2

Total storage required: 7.6 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRB B75	
Description:	75mmdeep system	
Total storage capacity:	10.7 m ³	

Total storage capacity:	
Number of Blue Roof outlets:	

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - B-4 Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	107 m ²	As supplied by Client
Storage area:	107 m ²	As supplied by Client
Maximum allowable runoff:	1.5 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 40 minutes	0.8
10 mins	0.0492	31	0 hours and 50 minutes	1.1
15 mins	0.0397	35	1 hour and 0 minutes	1.2
30 mins	0.0260	41	1 hour and 10 minutes	1.3
1 hour	0.0163	40	1 hour and 10 minutes	1.3
2 hours	0.0097	29	0 hours and 50 minutes	1.0
4 hours	0.0057	16	0 hours and 30 minutes	0.7
6 hours	0.0041	11	0 hours and 20 minutes	0.5
10 hours	0.0028	8	0 hours and 10 minutes	0.3
24 hours	0.0014	6	0 hours and 0 minutes	0.2
48 hours	0.0008	6	0 hours and 0 minutes	0.1

Total storage required: 4.4 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRB B75		
Description:	72mmdeep system		
Total storage capacity:	6.2 m ³		

	-	•	
Number of	f Blue	Root	foutlets:

Notes:

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Project Name:	Ugly Brown Building, Camder
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - B-5. Finishes:

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Paved

Input Parameters - Roof Information

Catchment area:	90 m ²	As supplied by Client
Storage area:	90 m ²	As supplied by Client
Maximum allowable runoff:	1.3 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (I/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 40 minutes	0.6
10 mins	0.0492	31	1 hour and 0 minutes	0.8
15 mins	0.0397	36	1 hour and 10 minutes	0.9
30 mins	0.0260	42	1 hour and 20 minutes	1.0
1 hour	0.0163	41	1 hour and 20 minutes	1.0
2 hours	0.0097	32	1 hour and 10 minutes	0.8
4 hours	0.0057	18	0 hours and 40 minutes	0.6
6 hours	0.0041	12	0 hours and 20 minutes	0.4
10 hours	0.0028	8	0 hours and 10 minutes	0.3
24 hours	0.0014	5	0 hours and 0 minutes	0.1
48 hours	0.0008	5	0 hours and 0 minutes	0.1

Total storage required: 3.8 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRB A58		
Description:	56mm deep system		
Total storage capacity:	4.5 m^3		

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Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C1-1 Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	159 m ²	As supplied by Client
Storage area:	159 m ²	As supplied by Client
Maximum allowable runoff:	2.2 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 40 minutes	0.9
10 mins	0.0492	31	1 hour and 10 minutes	1.3
15 mins	0.0397	37	1 hour and 20 minutes	1.4
30 mins	0.0260	43	1 hour and 30 minutes	1.5
1 hour	0.0163	44	1 hour and 30 minutes	1.6
2 hours	0.0097	36	1 hour and 20 minutes	1.4
4 hours	0.0057	22	0 hours and 50 minutes	1.0
6 hours	0.0041	15	0 hours and 30 minutes	0.7
10 hours	0.0028	10	0 hours and 20 minutes	0.5
24 hours	0.0014	7	0 hours and 0 minutes	0.3
48 hours	0.0008	6	0 hours and 0 minutes	0.1

Total storage required: 7.1 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRB B75	
Description:	75mm deep system	
Total storage capacity:	9.2 m ³	

Number of Blue Roof outlets:

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C1-2 Finishes: BIODIVERSE

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	31 m ²	As supplied by Client
Storage area:	31 m ²	As supplied by Client
Maximum allowable runoff:	0.5 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	19	0 hours and 40 minutes	0.3
10 mins	0.0492	30	0 hours and 50 minutes	0.4
15 mins	0.0397	34	1 hour and 0 minutes	0.4
30 mins	0.0260	38	1 hour and 0 minutes	0.4
1 hour	0.0163	36	1 hour and 0 minutes	0.4
2 hours	0.0097	24	0 hours and 40 minutes	0.3
4 hours	0.0057	12	0 hours and 20 minutes	0.2
6 hours	0.0041	8	0 hours and 10 minutes	0.1
10 hours	0.0028	6	0 hours and 10 minutes	0.1
24 hours	0.0014	5	0 hours and 0 minutes	0.0
48 hours	0.0008	4	0 hours and 0 minutes	0.0

Total storage required: 1.2 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRB B75	
Description:	75mm deep system	
Total storage capacity:	1.7 m ³	

Number of Blue Roof outlets:

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	22/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C1-3 . Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	121 m ²	As supplied by Client
Storage area:	121 m ²	As supplied by Client
Maximum allowable runoff:	1.7 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	1 hour and 20 minutes	0.5
10 mins	0.0492	32	2 hours and 0 minutes	0.6
15 mins	0.0397	38	2 hours and 20 minutes	0.7
30 mins	0.0260	47	2 hours and 40 minutes	0.7
1 hour	0.0163	52	2 hours and 50 minutes	0.8
2 hours	0.0097	50	2 hours and 50 minutes	0.8
4 hours	0.0057	37	2 hours and 10 minutes	0.7
6 hours	0.0041	27	1 hour and 40 minutes	0.5
10 hours	0.0028	16	1 hour and 0 minutes	0.4
24 hours	0.0014	7	0 hours and 20 minutes	0.2
48 hours	0.0008	5	0 hours and 0 minutes	0.1

Total storage required: 6.4 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRG B75		
Description:	75mm deep system		
Total storage capacity:	7.0 m ³		

Number of Blue Roof outlets:

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	22/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C1-4 . Finishes:

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Paved

Input Parameters - Roof Information

Catchment area:	228 m ²	As supplied by Client
Storage area:	228 m ²	As supplied by Client
Maximum allowable runoff:	3.2 l/s	As supplied by Client

Output - Rainfall Calculation					
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)	
5 mins	0.0602	20	0 hours and 50 minutes	1.1	
10 mins	0.0492	32	1 hour and 10 minutes	1.5	
15 mins	0.0397	37	1 hour and 30 minutes	1.7	
30 mins	0.0260	45	1 hour and 40 minutes	1.9	
1 hour	0.0163	48	1 hour and 40 minutes	2.0	
2 hours	0.0097	42	1 hour and 30 minutes	1.8	
4 hours	0.0057	27	1 hour and 0 minutes	1.4	
6 hours	0.0041	19	0 hours and 40 minutes	1.1	
10 hours	0.0028	12	0 hours and 20 minutes	0.7	
24 hours	0.0014	8	0 hours and 10 minutes	0.4	
48 hours	0.0008	7	0 hours and 0 minutes	0.2	

Total storage required: 10.9 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRB A58		
Description:	58mm deep system		
Total storage capacity:	11.4 m^3		

	0	•	
Number	of Blue	Roof	outlets

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C2 Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	271 m ²	As supplied by Client
Storage area:	271 m ²	As supplied by Client
Maximum allowable runoff:	3.8 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	1 hour and 20 minutes	0.8
10 mins	0.0492	33	2 hours and 10 minutes	1.1
15 mins	0.0397	39	2 hours and 40 minutes	1.2
30 mins	0.0260	48	3 hours and 10 minutes	1.4
1 hour	0.0163	55	3 hours and 30 minutes	1.5
2 hours	0.0097	54	3 hours and 20 minutes	1.5
4 hours	0.0057	44	2 hours and 50 minutes	1.3
6 hours	0.0041	34	2 hours and 20 minutes	1.1
10 hours	0.0028	21	1 hour and 30 minutes	0.9
24 hours	0.0014	10	0 hours and 30 minutes	0.4
48 hours	0.0008	7	0 hours and 10 minutes	0.2

Total storage required: 14.9 m³

Output - Recommended Blue Roof System			
System Name:	ABG blueroof BRG B75		
Description:	75mm deep system		
Total storage capacity:	15.7 m ³		

Number of Blue Roof outlets:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	22/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C3-1. Finishes: Biodiverse

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	198 m ²	As supplied by Client
Storage area:	198 m ²	As supplied by Client
Maximum allowable runoff:	2.8 l/s	As supplied by Client

Output - Rainfall Calculation					
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)	
5 mins	0.0602	20	1 hour and 10 minutes	0.7	
10 mins	0.0492	32	2 hours and 0 minutes	0.9	
15 mins	0.0397	38	2 hours and 20 minutes	1.0	
30 mins	0.0260	47	2 hours and 40 minutes	1.2	
1 hour	0.0163	53	3 hours and 0 minutes	1.2	
2 hours	0.0097	51	2 hours and 50 minutes	1.2	
4 hours	0.0057	40	2 hours and 20 minutes	1.0	
6 hours	0.0041	29	1 hour and 50 minutes	0.9	
10 hours	0.0028	18	1 hour and 0 minutes	0.6	
24 hours	0.0014	9	0 hours and 20 minutes	0.3	
48 hours	0.0008	7	0 hours and 0 minutes	0.2	

Total storage required: 10.6 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRG B75	
Description:	75mm deep system	
Total storage capacity:	11.4 m^3	

Number of Blue Roof outlets:

Notes:

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Project Name:	Ugly Brown Building, Camden
Prepared for:	Water Environment Limited
Date:	28/02/2018
ABG Project ID:	11723
Prepared by:	MG
Notes/description:	Drainage Area - C3-2. Finishes: Paved

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	229 m ²	As supplied by Client
Storage area:	229 m ²	As supplied by Client
Maximum allowable runoff:	3.2 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 50 minutes	1.1
10 mins	0.0492	32	1 hour and 30 minutes	1.5
15 mins	0.0397	37	1 hour and 40 minutes	1.6
30 mins	0.0260	45	1 hour and 50 minutes	1.8
1 hour	0.0163	49	2 hours and 0 minutes	1.9
2 hours	0.0097	43	1 hour and 50 minutes	1.8
4 hours	0.0057	29	1 hour and 20 minutes	1.4
6 hours	0.0041	20	0 hours and 50 minutes	1.1
10 hours	0.0028	12	0 hours and 30 minutes	0.7
24 hours	0.0014	7	0 hours and 10 minutes	0.4
48 hours	0.0008	6	0 hours and 0 minutes	0.2

Total storage required: 11.2 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRB A58	
Description:	58mm deep system	
Total storage capacity:	11.4 m^3	

Total storage capacity:	11.4 r
Number of Blue Roof outlets:	2

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Ugly Brown Building, Camden
Water Environment Limited
28/02/2018
11723
MG
Drainage Area - C3-3. Finishes: Paved

Input Parameters - Rainfall Information		
Return period:	100 years	As supplied by Client
Allowance for Climate Change:	40 %	As supplied by Client
Rainfall ratio, R:	0.41	From statistics based on location (FSR)
M5-60 expected rainfall:	20.6 mm/h	From statistics based on location (FSR)
Location selected for FSR data:	London (NW)	

Input Parameters - Roof Information

Catchment area:	76 m ²	As supplied by Client
Storage area:	76 m ²	As supplied by Client
Maximum allowable runoff:	1.1 l/s	As supplied by Client

Output - Rainfall Calculation				
Duration	Rainfall (l/s/m ²)	Storage Required (I/m ²)	Time to Empty	Restricted Outflow (I/s)
5 mins	0.0602	20	0 hours and 30 minutes	0.7
10 mins	0.0492	30	0 hours and 50 minutes	0.9
15 mins	0.0397	34	0 hours and 50 minutes	1.0
30 mins	0.0260	39	1 hour and 0 minutes	1.0
1 hour	0.0163	36	0 hours and 50 minutes	1.0
2 hours	0.0097	25	0 hours and 40 minutes	0.8
4 hours	0.0057	13	0 hours and 20 minutes	0.5
6 hours	0.0041	10	0 hours and 10 minutes	0.4
10 hours	0.0028	8	0 hours and 10 minutes	0.2
24 hours	0.0014	6	0 hours and 0 minutes	0.1
48 hours	0.0008	6	0 hours and 0 minutes	0.1

Total storage required: 3 m³

Output - Recommended Blue Roof System		
System Name:	ABG blueroof BRB A58	
Description:	58mm deep system	
Total storage capacity:	3.8 m ³	

Number of Blue Roof outlets:

Notes:

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Flood Risk Assessment and SuDS Strategy



APPENDIX D - CAMDEN SUDS PRO-FORMA

Advice Note on contents of a Surface Water Drainage Statement

London Borough of Camden

1. Introduction

- 1.1 The Government has strengthened planning policy on the provision of sustainable drainage and new consultation arrangements for 'major' planning applications will come into force from 6 April 2015 as defined in the <u>Written</u> <u>Ministerial Statement</u> (18th Dec 2014).
- 1.2 The new requirements make Lead Local Flood Authorises statutory consultees with respect to flood risk and SuDS for all major applications. Previously the Environment Agency had that statutory responsibility for sites above 1ha in flood zone 1.
- 1.3 Therefore all 'major' planning applications submitted from 6 April 2015 are required demonstrate compliance with this policy and we'd encourage this is shown in a **Surface Water Drainage Statement**.
- 1.4 The purpose of this advice note is to set out what information should be included in such statements.

2. Requirements

- 2.1 It is essential that the type of Sustainable Drainage System (SuDS) for a site, along with **details of its extent and position**, is identified within the planning application to clearly demonstrate that the proposed SuDS can be accommodated within the development.
- 2.2 It will now not be acceptable to leave the design of SuDs to a later stage to be dealt with by planning conditions.
- 2.3 The <u>NPPF</u> paragraph 103 requires that developments do not increase flood risk elsewhere, and gives priority to the use of SuDS. Major developments must include SuDS for the management of run-off, unless demonstrated to be inappropriate. The proposed minimum standards of operation must be appropriate and as such, a **maintenance plan** should be included within the Surface Water Drainage Statement, clearly demonstrating that the SuDS have been designed to ensure that the maintenance and operation requirements are economically proportionate Planning Practice Guidance suggests that this should be considered by reference to the costs that would be incurred by consumers for the use of an effective drainage system connecting directly to a public sewer.
- 2.4 Camden Council will use planning conditions or obligations to ensure that there are clear arrangements in place for ongoing maintenance over the lifetime of the development.
- 2.5 Within Camden, SuDS systems must be designed in accordance with London Plan policy 5.13. This requires that developments should utilise sustainable urban drainage systems (SUDS) unless there are practical reasons for not doing so, and should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible in line with the following drainage hierarchy:

- 1 store rainwater for later use
- 2 use infiltration techniques, such as porous surfaces in non-clay areas
- 3 attenuate rainwater in ponds or open water features for gradual release
- 4 attenuate rainwater by storing in tanks or sealed water features for gradual release
- 5 discharge rainwater direct to a watercourse
- 6 discharge rainwater to a surface water sewer/drain
- 7 discharge rainwater to the combined sewer.
- 2.6 The hierarchy above seeks to ensure that surface water run-off is controlled as near to its source as possible to mimic natural drainage systems and retain water on or near to the site, in contrast to traditional drainage approaches, which tend to pipe water off-site as quickly as possible.
- 2.7 Before disposal of surface water to the public sewer is considered all other options set out in the drainage hierarchy should be exhausted. When no other practicable alternative exists to dispose of surface water other than the public sewer, the Water Company or its agents should confirm that there is adequate spare capacity in the existing system taking future development requirements into account.
- 2.8 Best practice guidance within the <u>non-statutory technical standards</u> for the design, maintenance and operation of sustainable drainage systems will also need to be followed. Runoff volumes from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event must be constrained to a value as close as is reasonably practicable to the **greenfield runoff volume** for the same event.
- 2.9 <u>Camden Development Policy 23</u> (Water) requires developments to reduce pressure on combined sewer network and the risk of flooding by limiting the rate of run-off through sustainable urban drainage systems. This policy also requires that developments in areas known to be at risk of surface water flooding are designed to cope with being flooded. <u>Camden's SFRA</u> surface water flood maps, updated SFRA figures 6 (LFRZs), and 4e (increased susceptibility to elevated groundwater), as well as the <u>Environment Agency</u> <u>updated flood maps for surface water (ufmfsw)</u>, should be referred to when determining whether developments are in an area at risk of flooding.
- 2.10 <u>Camden Planning Guidance 3</u> (CPG3) requires developments to achieve a greenfield run off rate once SuDS have been installed. Where it can be demonstrated that this is not feasible, a minimum 50% reduction in run off rate across the development is required. Further guidance on how to reduce the risk of flooding can be found in CPG3 paragraphs 11.4-11.8.
- 2.11 Where an application is part of a larger site which already has planning permission it is essential that the new proposal does not compromise the drainage scheme already approved.

3. Further information and guidance

- 3.1 Applicants are strongly advised to discuss their proposals with the Lead Local Flood Authority at the pre-application stage to ensure that an acceptable SuDS scheme is submitted.
- 3.2 For general clarification of these requirements please Camden's Local Planning Authority or Lead Local Flood Authority

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the Defra/EA guidance on Rainfall Runoff Management and uses the storage calculator on www.UKsuds.com. This pro-forma is based on current industry best practice and focuses on ensuring surface water drainage proposals meet national and local policy requirements. This pro-forma accompanies our advice note on surface water drainage. Developers should complete this form and submit it to the Local Planning Authority, referencing from where in their submission documents this information is taken. The pro-forma is supported by The pro-forma should be considered alongside other supporting SuDS Guidance.

1. Site Details

	le or LPA reference		developed or Greenfield?	in a LFRZ or in an area known to	e or ground water flooding? If yes,	e how this is managed, in line with	ed by drainage system (excluding
Site	Address & post code or LPA reference	Grid reference	Is the existing site developed or Gree	Is the development in a LFRZ or in an	be at risk of surface or ground water f	please demonstrate how this is mana DP23?	Total Site Area served by drainage sy open space) (Ha)*

* The Greenfield runoff off rate from the development which is to be used for assessing the requirements for limiting discharge flow rates and attenuation storage from a site should be calculated for the area that forms the drainage network for the site whatever size of site and type of drainage technique. Please refer to the Rainfall Runoff Management document or CIRIA manual for detail on this.

2. Impermeable Area

	Existing	Proposed	Difference	Notes for developers
			(Proposed-Existing)	
Impermeable area (ha)				If the proposed amount of impermeable surface is greater, then runoff rates and volumes
				will increase. Section 6 must be filled in. If proposed impermeability is equal or less than
				existing, then section 6 can be skipped and section 7 filled in.
Drainage Method			A/N	If different from the existing, please fill in section 3. If existing drainage is by infiltration and
(infiltration/sewer/watercourse)				the proposed is not, discharge volumes may increase. Fill in section 6.

3. Proposing to Discharge Surface Water via

	Yes	No	Evidence that this is possible	Notes for developers
Existing and proposed MicroDrainage calculations				Please provide MicroDrainage calculations of existing and proposed run-off rates and volumes in accordance with a recognised methodology or the results of a full infiltration test
Infiltration				(see line below) if infiltration is proposed. e.g. soakage tests. Section 6 (infiltration) must be filled in if infiltration is proposed.
To watercourse				e.g. Is there a watercourse nearby?
To surface water sewer				Confirmation from sewer provider that sufficient capacity exists for this connection.
Combination of above				e.g. part infiltration part discharge to sewer or watercourse. Provide evidence above.
Has the drainage proposal				Evidence must be provided to demonstrate that the proposed Sustainable Drainage
had regard to the SuDS hierarchy?				strategy has had regard to the SuDS hierarchy as outlined in Section 2.5 above.
Layout plan showing where				Please provide plan reference numbers showing the details of the site layout showing
the sustainable drainage				where the sustainable drainage infrastructure will be located on the site. If the development
infrastructure will be				is to be constructed in phases this should be shown on a separate plan and confirmation
located on site.				should be provided that the sustainable drainage proposal for each phase can be
				constructed and can operate independently and is not reliant on any later phase of
				development.

s) % Difference Notes for developers (difference /existing x 100)	N/A QBAR is approx. 1 in 2 storm event. Provide this if Section 6 (QBAR) is proposed.	Proposed discharge rates (with mitigation) should aim to be equivalent to greenfield rates	for all corresponding storm events. As a minimum, peak discharge rates must be reduced		The proposed 1 in 100 +CC peak discharge rate (with mitigation) should aim to be	equivalent to greenfield rates. As a minimum, proposed 1 in 100 +CC peak discharge rate must be reduced by 50% from the existing 1 in 100 runoff rate sites.
rence (Vs) % Differ sosed- (differ ing) /existi 100)	N/A					
Diffel (Prop Existi	N/A					
Proposed Rates (I/s)	N/A					
Existing Rates (I/s)					N/A	
	Greenfield QBAR	l in 1	l in 30	in 100	in 100 plus	climate change

4. Peak Discharge Rates – This is the maximum flow rate at which storm water runoff leaves the site during a particular storm event.

the amount of stormwater that can go to the ground, so this needs to be controlled so not to make flood risk worse to properties downstream. 5. Calculate additional volumes for storage -The total volume of water leaving the development site. New hard surfaces potentially restrict

	Greenfield	Existing	Proposed ₃	Difference (m ³)	Notes for developers
	runoff volume (m ³)	Volume (m°)	Volume (m°)	(Proposed-Existing)	
1 in 1					Proposed discharge volumes (with mitigation) should be constrained to a value as close as is
1 in 30					reasonably practicable to the greenfield runoff volume wherever practicable and as a
1in 100 6 hour					minimum should be no greater than existing volumes for all corresponding storm events. Any
					increase in volume increases flood risk elsewhere. Where volumes are increased section 6
					must be filled in.
1 in 100 6 hour plus					The proposed 1 in 100 +CC discharge volume should be constrained to a value as close as
climate change					is reasonably practicable to the greenfield runoff volume wherever practicable. As a
					minimum, to mitigate for climate change the proposed 1 in 100 +CC volume discharge from
					site must be no greater than the existing 1 in 100 storm event. If not, flood risk increases
	_				under climate change.

6. Calculate attenuation storage – Attenuation storage is provided to enable the rate of runoff from the site into the receiving watercourse to be limited to an acceptable rate to protect against erosion and flooding downstream. The attenuation storage volume is a function of the degree of development relative to the greenfield discharge rate.

	Notes for developers
Storage Attenuation volume (Flow rate control) required to	Volume of water to attenuate on site if discharging at a greenfield run off rate.
meet greenfield run off rates (m ³)	Can't be used where discharge volumes are increasing
Storage Attenuation volume (Flow rate control) required to	Volume of water to attenuate on site if discharging at a 50% reduction from
reduce rates by 50% (m ³)	existing rates. Can't be used where discharge volumes are increasing
Storage Attenuation volume (Flow rate control) required to	Volume of water to attenuate on site if discharging at a rate different from the
meet [OTHER RUN OFF RATE (as close to greenfield rate as	above – please state in 1 st column what rate this volume corresponds to. On
possible] (m ³)	previously developed sites, runoff rates should not be more than three times the
	calculated greenfield rate. Can't be used where discharge volumes are
	increasing
Storage Attenuation volume (Flow rate control) required to	Volume of water to attenuate on site if discharging at existing rates. Can't be
retain rates as existing (m ³)	used where discharge volumes are increasing
Percentage of attenuation volume stored above ground,	Percentage of attenuation volume which will be held above ground in
	ewales/nonds/hasins/green roofs atc. If 0. please demonstrate why

7. How is Storm Water stored on site?

exceptionally low rate. You can either infiltrate the stored water back to ground, or if this isn't possible hold it back with on site storage. Firstly, Storage is required for the additional volume from site but also for holding back water to slow down the rate from the site. This is known as attenuation storage and long term storage. The idea is that the additional volume does not get into the watercourses, or if it does it is at an can infiltration work on site?

		Notes for developers
	State the Site's Geology and known Source	Avoid infiltrating in made ground. Infiltration rates are highly variable
Infiltration	Protection Zones (SPZ)	and refer to Environment Agency website to identify and source
		protection zones (SPZ)
	Are infiltration rates suitable?	Infiltration rates should be no lower than $1x10^{-6}$ m/s.
	State the distance between a proposed infiltration	Need 1m (min) between the base of the infiltration device & the water
	device base and the ground water (GW) level	table to protect Groundwater quality & ensure GW doesn't enter
		infiltration devices. Avoid infiltration where this isn't possible.

	Were infiltration rates obtained by desk study or infiltration test?	Infiltration rates can be estimated from desk studies at most stages of the planning system if a back up attenuation scheme is provided
	Is the site contaminated? If yes, consider advice from others on whether infiltration can happen.	Advice on contaminated Land in Camden can be found on our supporting documents <u>webpage</u> Water should not be infiltrated through land that is contaminated. The Environment Agency may provide bespoke advice in planning consultations for contaminated sites that should be considered.
In light of the above, is infiltration feasible?	Yes/No? If the answer is No, please identify how the storm water will be stored prior to release	If infiltration is not feasible how will the additional volume be stored?. The applicant should then consider the following options in the next section.
Storage requir	ements	
The developer	must confirm that either of the two methods for dealing with the amount of	water that needs to be stored on site.
Option 1 Simp off rate. This is	Ie – Store both the additional volume and attenuation volume in order to r preferred if no infiltration can be made on site. This very simply satisfies t	nake a final discharge from site at the greenfield run ne runoff rates and volume criteria.
Option 2 Com very low rate of used to slow the	plex – If some of the additional volume of water can be infiltrated back int [.] 2 l/sec/hectare. A combined storage calculation using the partial permiss e runoff from site.	the ground, the remainder can be discharged at a ble rate of 2 l/sec/hectare and the attenuation rate

	Notes for developers
Please confirm what option has been chosen and how much	The developer at this stage should have an idea of the site
storage is required on site.	characteristics and be able to explain what the storage requirements
	are on site and how it will be achieved.

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	Notes for developers
Which Drainage Systems measures have been used,	SUDS can be adapted for most situations even where infiltration
including green roofs?	isn't feasible e.g. impermeable liners beneath some SUDS devices
	allows treatment but not infiltration. See CIKIA SUDS Manual C697.
Drainage system can contain in the 1 in 30 storm event	This a requirement for sewers for adoption & is good practice even
without flooding	where drainage system is not adopted.
Will the drainage system contain the 1 in 100 +CC storm	National standards require that the drainage system is designed so
event? If no please demonstrate how buildings and utility	that flooding does not occur during a 1 in 100 year rainfall event in
plants will be protected.	any part of: a building (including a basement); or in any utility plant
	susceptible to water (e.g. pumping station or electricity substation)
	within the development.
Any flooding between the 1 in 30 & 1 in 100 plus climate	Safely: not causing property flooding or posing a hazard to site
change storm events will be safely contained on site.	users i.e. no deeper than 300mm on roads/footpaths. Flood waters
	must drain away at section 6 rates. Existing rates can be used
	where runoff volumes are not increased.
How will exceedance events be catered on site without	Safely: not causing property flooding or posing a hazard to site
increasing flood risks (both on site and outside the	users i.e. no deeper than 300mm on roads/footpaths. Flood waters
development)?	must drain away at section 6 rates. Existing rates can be used
	where runoff volumes are not increased.
	Events and additional on these leaves the 1 in 100
	Exceedatice events are defined as inoserarger frian file 1 fit 100 +CC event
How are rates being restricted (vortex control orifice etc)	Detail of how the flow control systems have been designed to avoid
	bible blockages and ease of maintenance should be provided.
Please confirm the owners/adopters of the entire drainage	If these are multiple owners then a drawing illustrating exactly what
systems throughout the development. Please list all the	features will be within each owner's remit must be submitted with
owners.	this Proforma.
How is the entire drainage system to be maintained?	If the features are to be maintained directly by the owners as stated
	in answer to the above question please answer yes to this question
	and submit the relevant maintenance schedule for each feature. If it
	is to be maintained by others than above please give details of each
	feature and the maintenance schedule.
	Clear details of the maintenance proposals of all elements of the
	proposed drainage system must be provided. Details must
	demonstrate that maintenance and operation requirements are
	economically proportionate. Poorly maintained drainage can lead to
	l increased flooding problems in the future.

relevant drawings that need to accompany your proforma, in particular exceedance routes and ownership and location of SuDS (maintenance 9. Evidence Please identify where the details quoted in the sections above were taken from. i.e. Plans, reports etc. Please also provide access strips etc

Pro-forma Section	Document reference where details quoted above are taken from	Page Number
Section 2		
Section 3		
Section 4		
Section 5		
Section 6		
Section 7		
Section 8		
The above form sh	ould be completed using evidence from the Flood Risk Assessment and site plans. It should serve as a	ummary sheet of the
drainage proposals	s and should clearly show that the proposed rate and volume as a result of development will not be increa	sing. If there is an

increase in rate or volume, the rate or volume section should be completed to set out how the additional rate/volume is being dealt with.

This form is completed using factual information from the Flood Risk Assessment and Site Plans and can be used as a summary of the surface water drainage strategy on this site.

Form Completed By
Company
Date: