

SURFACE WATER DRAINAGE ASSESSMENT & OUTLINE SUDS STRATEGY

**39 FITZJOHNS AVENUE
CAMDEN**



LBH GEO

LBH4498suds

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		Darcy Kitson-Boyce MEng (Hons) GMICE FGS FRGS	Seamus Lefroy-Brooks BSc(hons) MSc CEng MICE CGeol FGS CEnv MEnvSc FRGS SiLC NQMS SQP DoWCoP QP RoGEP UK Registered Ground Engineering Adviser
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LBHGEO Ltd.

12 Little Balmer

Buckingham

MK18 1TF

Tel: 01280 308160

email: enquiry@LBHGEO.co.uk

website: www.LBHGEO.co.uk

Company registered in England No. 4922494

LBHGEO

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FOREWORD-GUIDANCE NOTES

GENERAL

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The observations and conclusions described in this report are based solely upon the agreed scope of work. LBHGEO has not performed any observations, investigations, studies or testing not specifically set out in the agreed scope of work and cannot accept any liability for the existence of any condition, the discovery of which would require performance of services beyond the agreed scope of work.

VALIDITY

Any use of or reliance upon the report in circumstances other than those for which it was commissioned shall be at the client's sole risk. The passage of time may result in changes in site conditions, regulatory or other legal provisions, technology or economic conditions which could render the report inaccurate or unreliable. The information and conclusions contained in this report should therefore not be relied upon in such altered circumstances.

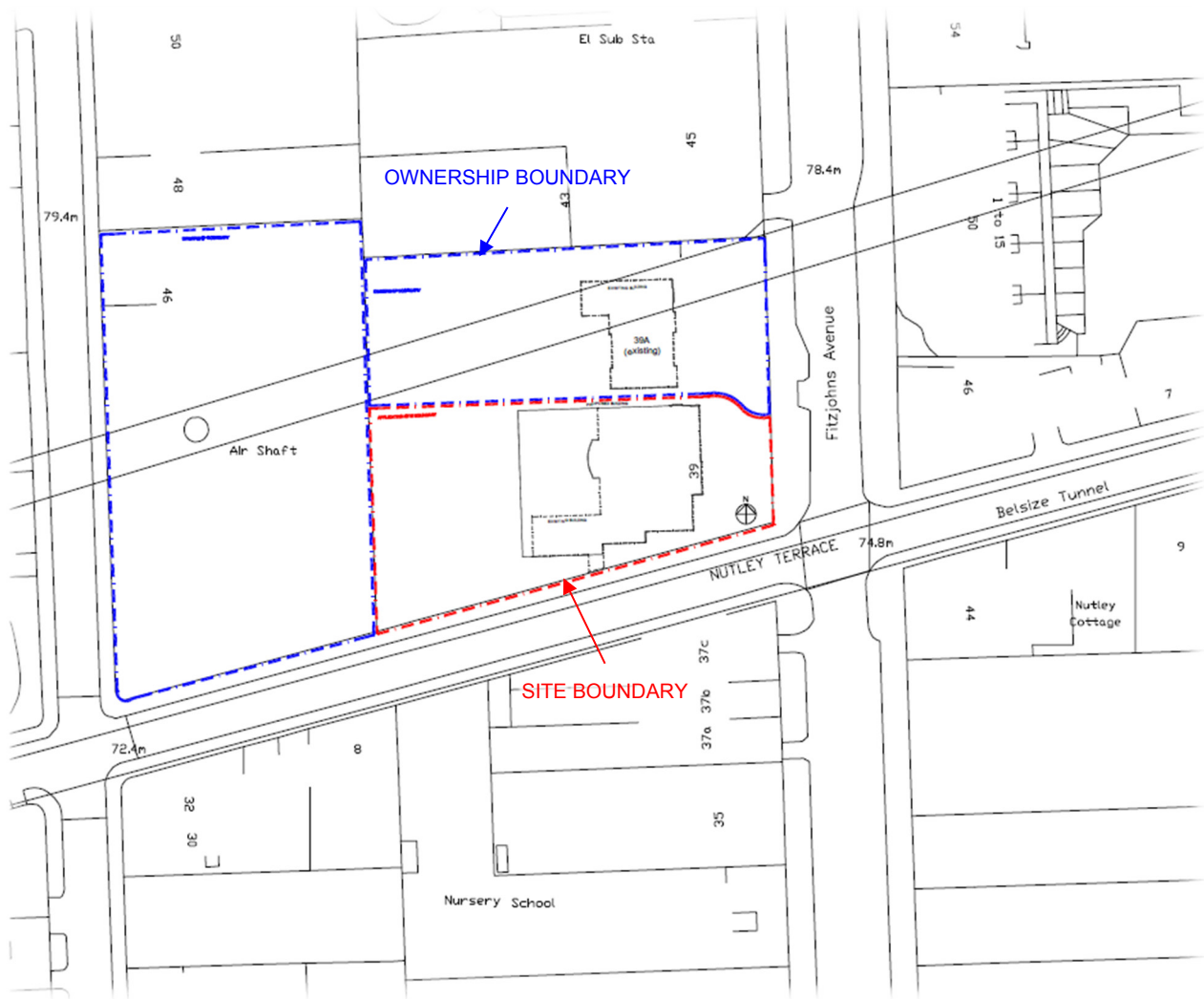
THIRD PARTY INFORMATION

The report may present an opinion based upon information received from third parties. However, no liability can be accepted for any inaccuracies or omissions in that information.

1. INTRODUCTION

1.1 BACKGROUND

It is proposed to re-build a large Victorian property at No. 39 Fitzjohn's Avenue, which will include the construction of a basement beneath the full extent of the building that will also extend into the rear garden.



SITE LOCATION PLAN

A previous planning application for the development, submitted to the London Borough of Camden Council (Ref. 2018/2415/P), was accompanied by an Outline Suds Strategy.

The scheme was revised in 2019 to reduce the depth and area of basement excavation and later to increase the propose number of housing units to thirty five together with minor additions to the front and side lightwells and a rearrangement of the proposed basement level patio.

A planning application for the altered scheme has been submitted to London Borough of Camden Council and was registered on 4th of August 2020 (Planning Ref. 2020/2169/P).

1.2 BRIEF

LBHGEO have been appointed to prepare an updated Surface Water Drainage Assessment & Outline SuDS Strategy to support the new planning application submitted to the London Borough of Camden.

1.3 SUDS GUIDANCE

The government advice is that developers should seek opportunities to reduce the overall level of flood risk through the appropriate application of sustainable drainage systems.

Sustainable drainage systems are designed to control surface water run off close to where it falls and mimic natural drainage as closely as possible. They provide opportunities to:

- reduce the causes and impacts of flooding;
- remove pollutants from urban run-off at source;
- combine water management with green space with benefits for amenity, recreation and wildlife.

The aim is to discharge surface run off as high up the following hierarchy of drainage options as reasonably practicable:

1. into the ground (infiltration);
2. to a surface water body;
3. to a surface water sewer, highway drain, or another drainage system;
4. to a combined sewer.

The London Borough of Camden requires drainage solutions to incorporate SuDS principles as laid out in the Non-Statutory Technical Standards¹ for Sustainable Drainage Systems and the London Plan².

For redevelopment sites where there is a net increase in impermeable area, development must include at least one 'source control' SuDS measure. Examples of potential Source Control measures include:

- blue/green roof
- rainwater harvesting
- bio-retention
- rain garden
- permeable paving

Underground storage/attenuation tanks are not encouraged and are to be used only as a last resort.

The Camden Local plan provides guidance for water and flooding under Policy CC3, where the council will seek to ensure a development reduces the risk of flooding where possible and will require a development to utilise Sustainable Drainage Systems (SuDS) in line with the drainage hierarchy to achieve a greenfield run-off rate where feasible.

Additionally, the Camden Planning Guidance for Sustainability (CPG3) (July 2015, updated March 2018) states the following:

¹ DEFRA March 2015 Non-Statutory Technical Standards (NSTS) for sustainable drainage systems

² London Plan Chapter Five - London's Responses to Climate Change Policy 5.1.3 Sustainable Drainage

"All developments are expected to manage drainage and surface water on-site or as close to the site as possible, using Sustainable Drainage Systems (SUDS) and the hierarchy set out below.

The Council will expect plans and application documents to describe how water will be managed within the development, including an explanation of the proposed SUDS, the reasons why certain SUDS have been ruled out and detailed information on materials and landscaping.

The Council will expect developments to achieve a greenfield surface water run-off rate once SUDS have been installed. As a minimum, surface water run-off rates should be reduced by 50% across the development."

1.4 REPORT STRUCTURE

This report describes the site characteristics and the proposed development, following which consideration is given to the feasibility of different SuDS techniques for this site, in line with the SuDS hierarchy.

An analysis is then presented of surface water run-off and of the attenuation volume that will be required to achieve the required reduction in the predicted run-off rates, taking into account increased rainfall rates due to anticipated climatic change.

A SuDS strategy is then developed including information about the proposed SuDS types, with an aim to reduce the drainage discharge rates as far as can be reasonably achieved in the proposed post-development scenario.

The report is accompanied by detailed calculations and a summary sustainable drainage pro-forma.

2. THE SITE

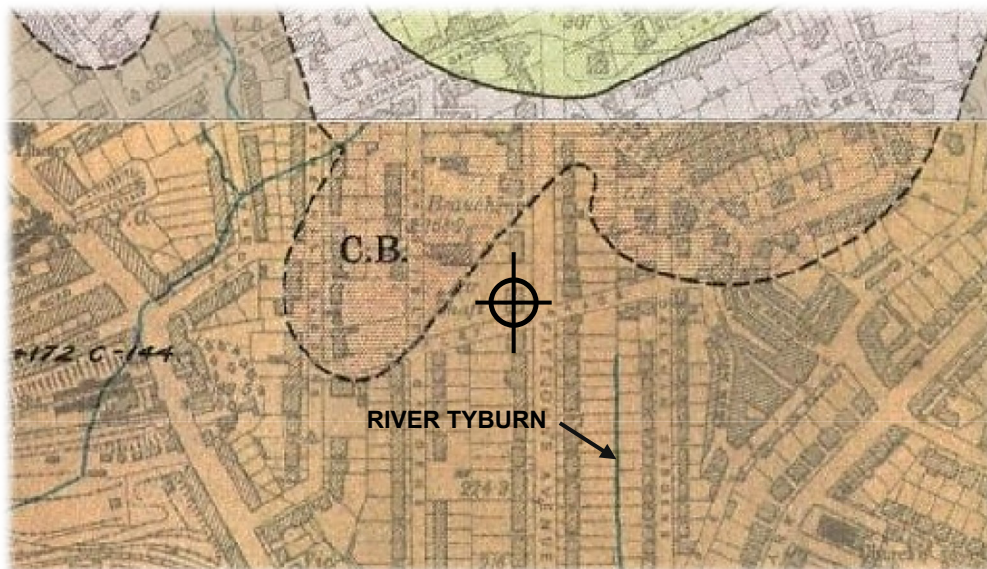
2.1 SITE LOCATION

The site is situated on the corner of Fitzjohn's Avenue and Nutley Terrace side of Kentish Town Road, approximately 400m to the northeast of Finchley Road underground station.

The site may be located approximately by postcode NW3 5JY or by National Grid Reference 526510, 185000.

2.2 TOPOGRAPHICAL SETTING

The area lies on a gentle southern slopes of Hampstead Hill falling towards the headwaters of the River Tyburn which are located approximately a short distance from the site. The area is this naturally sloping ground that has been terraced.



2.3 GROUND CONDITIONS

The site is directly underlain by the London Clay Formation, which is essentially impermeable.

A site specific ground investigation has confirmed that London Clay is present beneath a limited depth of made ground.

2.4 SITE DESCRIPTION

The site is occupied by a large three storey Victorian house.



MAIN VICTORIAN HOUSE (LEFT) AND NORTHERN WING EXTENSION (RIGHT)

Owing to the relative drop in ground level between the north and south of the site, the lower ground floor opens out onto Nutley Terrace that borders the south of the site.

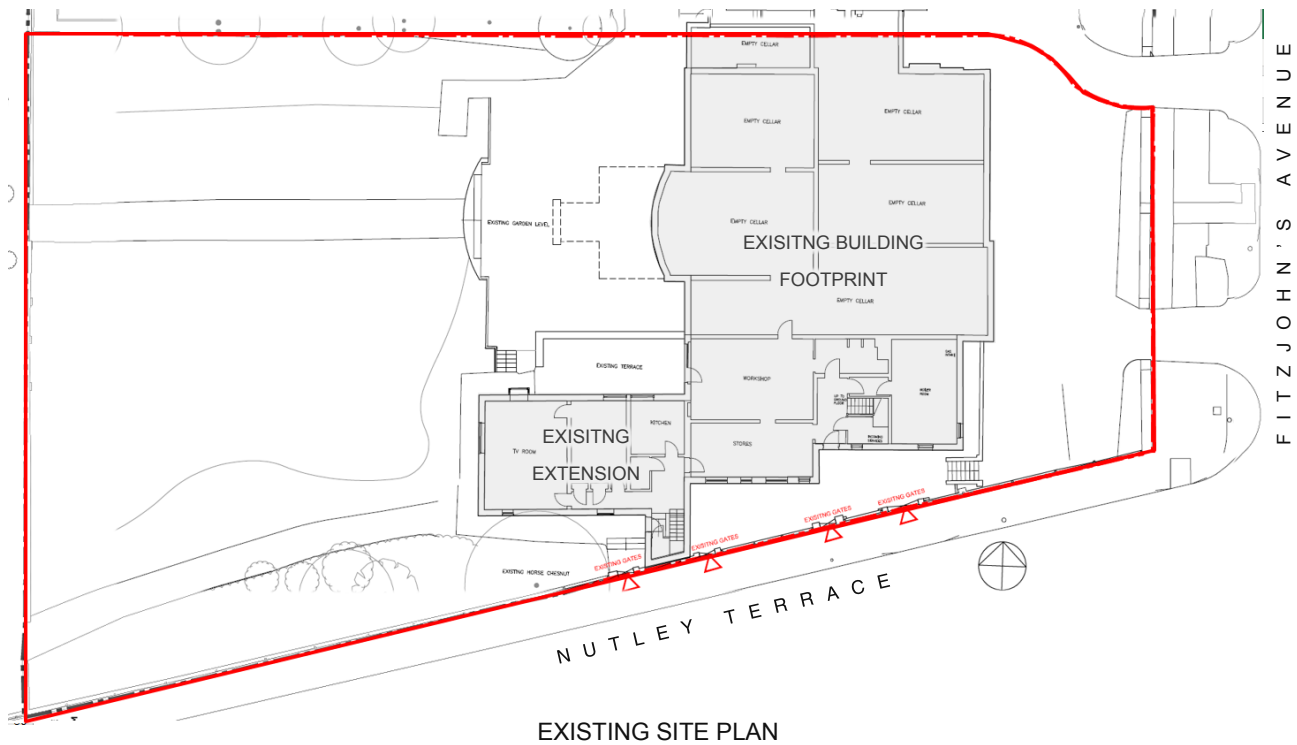
There are two 1950s extensions to the building; a three storey northern wing, which is connected to the Victorian building by a three storey link corridor and a three storey wing that adjoins to the west.



REAR GARDEN VIEW SHOWING REAR ELEVATION

The northern wing extension and the garden to the rear of this are located outside of the boundaries of the proposed amended development.

A large garden is situated to the rear of the Victorian house and gently slopes from approximately +78m OD in the north, to approximately +75m OD in the south. The garden is predominantly vacant, aside from a row of trees present at the southern boundary of the site with Nutley Terrace.



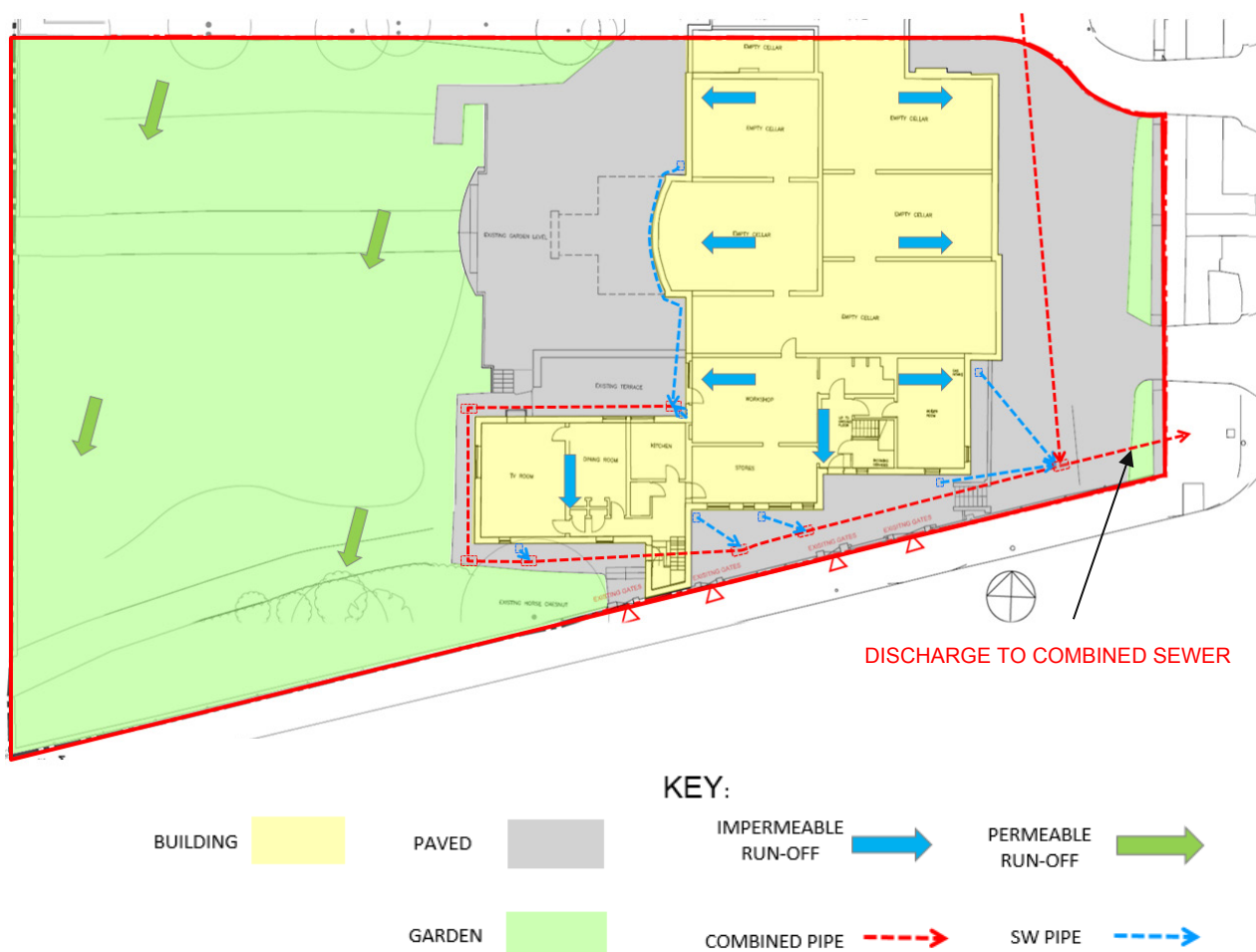
2.5 EXISTING SURFACE WATER DRAINAGE

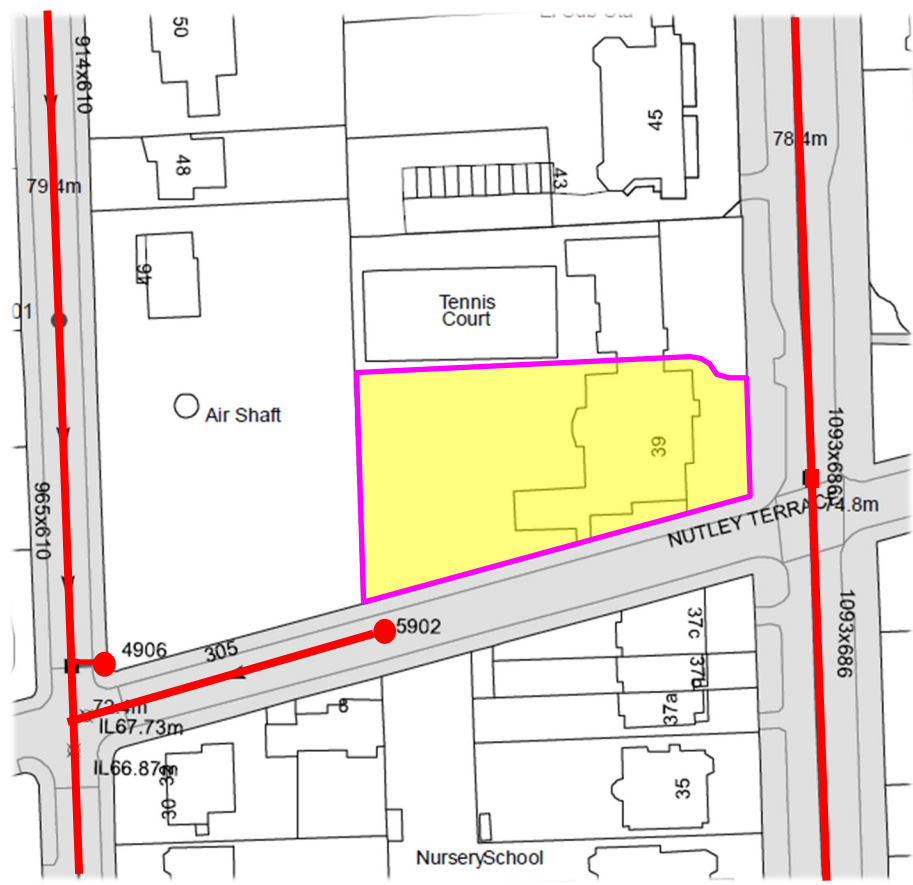
The site comprises a large building with a hard surfacing at the front and rear of this, in the form of a paved driveway and a rear patio, respectively, with a soft landscape garden present towards the rear.

The runoff from the site is ultimately drained towards a public combined sewer running southwards below Fitzjohn's Avenue.

The rainfall incident on the buildings and hard surfacing on site is directed through a series of drains and manholes leading from the rear of the 1950s extension to the building towards the front of the site. The drains collect both the surface water and foul water. The final discharge manhole, located in the southeastern corner of the site, also collects combined runoff from the northern extension to the building before discharging to the combined sewer.

The rear garden slopes away from the building and the front of the site so it should be assumed that majority of the rainfall incident on the garden will follow this slope and flow away from the existing drainage system on site.





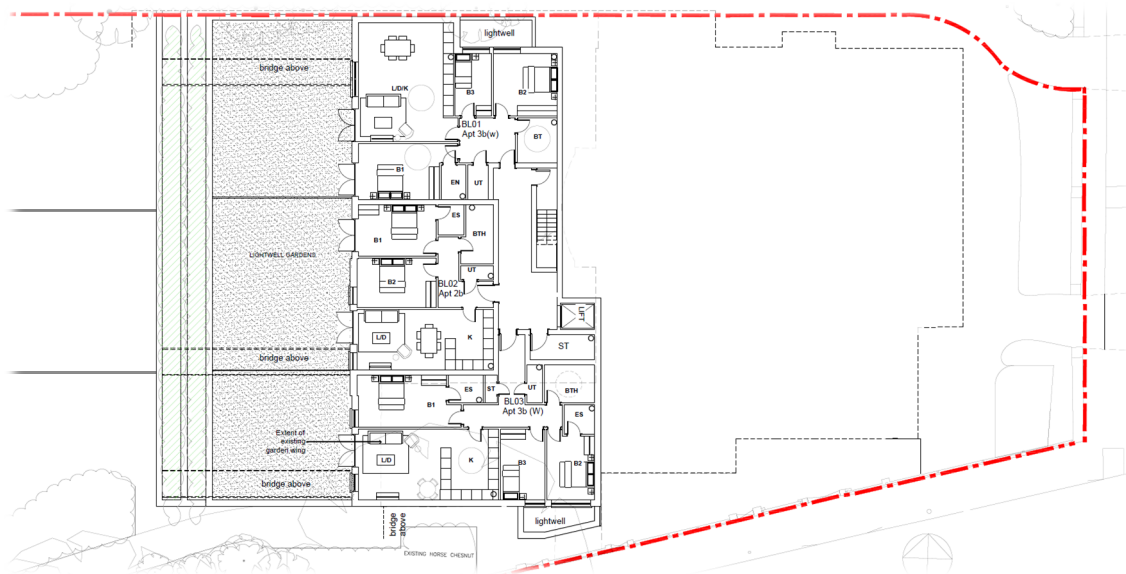
PUBLIC SEWER NETWORK IN THE VICINITY OF THE SITE

3. PROPOSED DEVELOPMENT

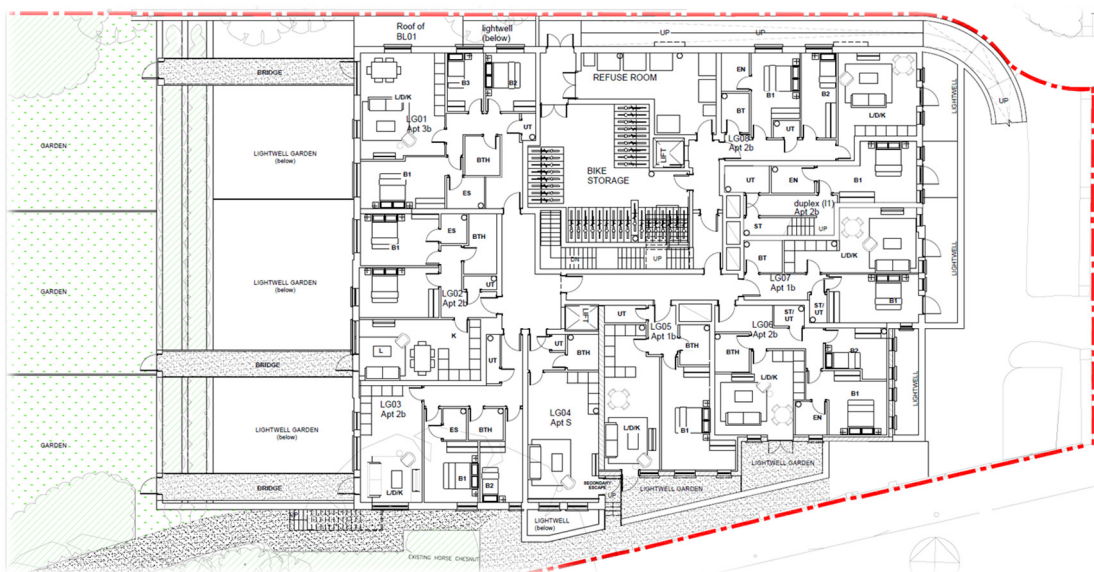
It is proposed to replace the existing Victorian property with a new four storey building with a basement. The front and side facades to the building will be retained and restored.

The new building will extend into the present rear garden with the new basement opening out onto a basement level patio that will link to the remaining rear garden by means of stepped planting.

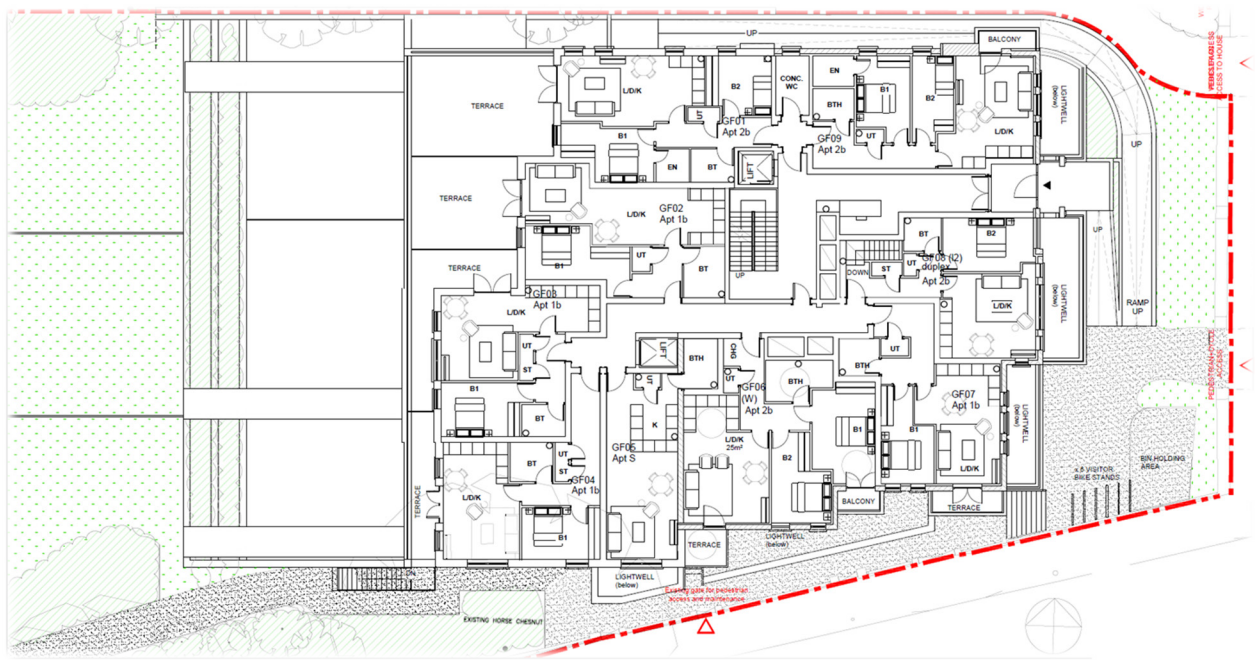
As part of the proposed development, the existing western wing and the link corridor to the northern will be removed.



PROPOSED BASEMENT PLAN



PROPOSED LOWER GROUND FLOOR PLAN



PROPOSED GROUND FLOOR LEVEL PLAN

SCHEDULE OF ESTIMATED AREAS										
	EXISTING					PROPOSED				
		Cv	%		%	Proposed	Cv	%		%
FRONT AREAS	310sqm	0.9	14.4%	%IMP	52.6%	270sqm	0.9	12.6%	%IMP	60.0%
BUILDING	550sqm	0.9	25.6%			660sqm	0.9	30.7%		
REAR PATIOS	270sqm	0.9	12.6%			360sqm	0.9	16.7%		
GARDENS	1020sqm	0.4	47.4%	%PER	47.4%	860sqm	0.4	40.0%	%PER	40.0%
TOTAL DEVELOPMENT AREA	2150sqm		100.0%		100.0%	2150sqm		100.0%		100.0%

4. SURFACE WATER MANAGEMENT

4.1 SURFACE WATER MANAGEMENT (SWM) OBJECTIVES

The drainage strategy follows the guidance set out in the 2015 CIRIA C753 SuDS Manual; the principle of SuDS design is that surface water runoff is managed for maximum benefit.

4.2 SUDS DISCHARGE HIERARCHY

The surface water runoff should be managed using the following techniques, as outlined in order of priority by the following drainage hierarchy:

SuDS Drainage Hierarchy	Suitable for the site? (Y/N)	Comment
Store rainwater for later use	Y	There is limited space for rainwater harvesting. Small water butts could be included within the proposed basement patio.
Use infiltration techniques	N	The London Clay is unsuitable for soakaway infiltration.
Attenuate rainwater in ponds or open water features for gradual release	Y	There may be space to introduce open water features in the form of swales or rain garden at the rear garden of the site
Attenuate rainwater by storing in tanks or sealed water features for gradual release	Y	There is scope for attenuation storage within a cellular storage layer underlying the proposed permeable paving. A larger underground attenuation storage tank can also be considered.
Discharge rainwater direct to a watercourse	N	There is no available watercourse.
Discharge rainwater to a surface water sewer/drain	N	There is no surface water sewer serving the site.
Discharge rainwater to the combined sewer	Y	The site currently discharges to the combined sewer beneath Fitzjohn's Avenue.

The objective is to control the quantity of runoff to support the management of flood risk and maintain and protect the natural water cycle. The hierarchy seeks to ensure that surface water runoff is controlled as near to its source as possible to mimic natural drainage systems and retain water on or near to the site.

Before disposal of surface water to the public sewer is considered, all other options set out in the above hierarchy need to be exhausted.

4.3 FEASIBLE SUDS COMPONENTS

SUDS Component	Description	Suitable for the site? (Y/N)	Comment
Rainwater harvesting	Collection of rainwater runoff from roofs or impermeable areas for reuse.	Y	Water butts could potentially be included within the basement level patio.
Green roofs	Vegetated areas installed on the top of buildings provide visual and ecological benefits in addition to surface water runoff reduction and enhanced building performance.	Y	The proposed development provides new areas of flat roof which may be repurposed with a green roof cover.
Blue roofs	Roof design intended to store water providing attenuation storage.	Y	There is a limited scope to install blue roof storage at the same flat roof areas.
Infiltration systems	Infiltration can contribute to reducing runoff rates and volumes while supporting base flow and groundwater recharge processes.	N	The London Clay is not suitable for infiltration.
Proprietary treatment systems	Proprietary treatment systems are manufactured products which remove specified pollutants from surface water runoff.	N	Not required.
Filter strips/drains	Filter strips are gently sloping strips of grass that provide treatment of runoff from adjacent impermeable areas. Filter drains are gravel or stone filled trenches which provide temporary subsurface storage for attenuation conveyance and filtration of surface water runoff.	Y	There is scope to introduce a form of filter strips at the proposed development site, potentially within the basement level patio.
Swales	Swales are shallow, flat bottomed, vegetated open channels designed to convey, treat, and attenuate surface water runoff.	Y	There is limited scope to introduce swales within the retained rear garden of the site.
Bioretention systems	Rain gardens or shallow landscaped depressions that may reduce surface water runoff rates and volumes and/or treat pollution using engineered soils and vegetation.	Y	There is limited scope to introduce rain gardens or similar within the retained rear garden of the site.

Trees	Trees aid surface water management through transpiration, interception, infiltration and phytoremediation.	Y	There is scope for new planting to be introduced in the retained rear garden.
Pervious Pavements	Pervious pavements facilitate the infiltration of surface water into a subsurface structure where filtration, adsorption, biodegradation or sedimentation may also provide treatment of the runoff.	Y	There is scope to introduce a significant area of permeable paving beneath the proposed hard surfacing at the southern part of the site. Such paving will only be feasible when underlain by a proprietary cellular storage layer.
Attenuation storage tanks	Attenuation storage tanks provide below-ground void space for the temporary storage of surface water before infiltration, controlled release or use.	Y	Construction of attenuation storage tanks is feasible within the front area of the site.
Detention basins	Attenuation storage in the form of dry landscaped depressions.	N	There is a very limited scope to introduce such features in the retained rear garden.
Ponds and wetlands	Permanent water filled ponds or wetlands that provide attenuation storage or treatment of surface water runoff.	N	There is a very limited scope to introduce such features in the retained rear garden.

4.4 BENEFITS

The types of benefits that may be achieved by utilising SuDS are categorised by the design objectives outlined in the following section.

4.4.1 WATER QUANTITY

The proposed development will reduce the areas of soft landscaping on site and attenuation storage will be required in order to reduce the surface water discharge from the site into the public sewer.

In order to provide this, a majority of the proposed hard surfacing at ground level, at the southern part of the site, is to be constructed as permeable paving, with a proprietary, cellular storage layer underlying this for storage of surface water runoff.

It is expected that the majority of the runoff from the proposed building as well as the basement level patio can be directed towards the attenuation storage volume provided by the permeable paving.

Prior to final discharge to a combined sewer, an underground collector tank will be constructed to provide a facility for the orifice flow control discharge. It is expected that any additional required attenuation storage can also be provided by this tank.

The aim is to provide attenuation storage sufficient to limit the discharge rates and volumes to 50% better than the existing runoff rates, in consideration of the predicted effect of climate change.

4.4.2 WATER QUALITY

The water quality design objective is to manage the quality of runoff to prevent pollution, supporting the management of water quality in the receiving surface waters and groundwater and design system resilience to cope with future change.

The permeable paving will provide an effective filter of larger particles before routing to the underlying storage. Petroleum interceptors will be installed at the front of the site, where vehicular access and parking will be provided.

Any additional areas of green roof and/or rear garden SuDS features will offer additional scope for filtering of the surface water.

4.4.3 AMENITY

The amenity design objective is to create and sustain better places for people by implementing the following criteria for the site:

- Maximise multi-functionality
- Enhance visual character
- Deliver safe surface water management systems
- Support development resilience/adaptability to future change
- Maximise legibility
- Support community environmental learning

There is limited scope to introduce further amenity objectives on site. It is, however, expected that these can be fulfilled by providing rain garden features within the basement level patio. It is expected that the proposed stepped planter leading towards the retained rear garden may provide the best opportunity for this.

4.4.4 BIODIVERSITY

The biodiversity design objective is to create and sustain better places for nature by implementing the following criteria for the site:

- Support and protect natural local habitats and species
- Contribute to the delivery of local biodiversity objectives
- Contribute to habitat connectivity
- Create diverse, self-sustaining and resilient ecosystems.

Similarly, there is limited scope to introduce further biodiversity features on site. It is, however, expected that these can be fulfilled by providing rain garden features within the rear garden and the basement level patio as well as any green or sedum roof introduced at the flat roof areas of the proposed structure.

4.5 SUDS CONSTRUCTION

It is proposed to provide sufficient attenuation storage at the rear of the site in order to reduce the overall discharge rate from the entire site.

The majority of the required storage volume is expected to be feasibly provided by cellular storage directly underlying the permeable paving in the southern part of the site. This area is proposed to be relatively flat

and situated at approximately the garden level of the site, approx. 2.5m below the front driveway.

The driveway can also be feasibly underlain by storage tanks underlying pervious paving.

An underground storage tank is likely to be required to be installed at the front of the site in order to capture the attenuated runoff and provide further attenuation volume itself, to fulfil the calculated requirement. It will be important to ensure that the top of this tank is situated at a lower level than the storage areas present within the garden level hard surfacing in the southern part of the site. This will ensure feasibility of gravity drainage from other attenuation areas.

The new basement terrace will need to drain to a sump, from where water will be pumped up to either the storage underlying the permeable paving or directly to the attenuation tank situated beneath the front parking area.

The attenuated flow can then be discharged from the tank via an orifice flow control towards the combined sewer beneath Fitzjohn's Avenue.

4.6 MAINTENANCE

There is a need to introduce clear arrangements in place for on-going maintenance over the lifetime of the development.

The SuDS features will require some regular inspection and maintenance to clear any accumulated sediment or debris which may reduce the storage capacity as well as to ensure the inlets and outlets are clear and do not impede the water flow.

Maintenance activities can be broadly categorised as:

- Regular maintenance consists of inspections and basic tasks carried out to a frequent schedule (more frequently than once per year) including inspections, silt, litter or debris removal and vegetation management.
- Occasional maintenance comprises tasks that are required on a much less frequent and predictable basis (e.g. annual checks)
- Remedial maintenance describes the intermittent tasks that may be required to rectify faults associated with the system such as inlet and outlet repairs, infiltration surface rehabilitation, replacement of blocked filter materials/fabrics, system rehabilitation immediately following a pollution event.

5. INITIAL DESIGN CONSIDERATIONS

An analysis has been undertaken of the pre- and post- development surface water run-off rates and volumes over a range of storm intensities and durations.

5.1 GREENFIELD RUNOFF RATE

The Greenfield runoff rates from the site have been calculated using the UK SuDS online tool and the Institute of Hydrology (IoH) 124 methodology.

Greenfield Rates:	
Qbar:	0.93 l/sec
1 in 1	0.79 l/sec
1 in 30	2.15 l/sec
1 in 100	2.98 l/sec
1 in 200	3.50 l/sec

5.2 EXISTING RUNOFF RATE

The site comprises a total area of approximately 2150m² of which approx. 52.6% is impermeably surfaced. The proposed development will increase the proportion of impermeable areas to an estimated approx. 60.0%. There is considered to be no SuDS features present at the existing site.

The existing peak storm runoff for the 1% (1 in 100 year) annual probability 15 min rainfall event on the site is estimated to be 51.1 l/sec. The calculation was based on the Wallingford Procedure and the resulting runoff was calculated using the Modified Rational Method with an M5-60 of 20mm, an 'r' value of 0.42 and a critical rainfall intensity of 99.3 mm/hr.

The rainfall runoff volume for the 1% (1 in 100 year) annual probability, 6 hour duration storm from the existing site is estimated to be 116.9 m³.

6. PROPOSED SURFACE WATER DRAINAGE SCHEME

Attenuation storage is to be provided predominantly beneath the hard surfaced areas at the southern part of the site.

Calculations indicate that some 45m³ of attenuation storage will be required for the 1 in 100 year rainfall event, in consideration of up to 40% climate change allowance, in order to reduce the proposed discharge rate to 50% of the existing.

It is envisaged that this could potentially be provided as follows:

- 200mm thick storage layer, underlying 150m² permeable paving, providing 30m³ of attenuation storage
- An underground attenuation tank at the front of the site providing 15m³ of storage

Small rainwater harvesting butts, as well as rain gardens or filtration strip features, can also be provided within the rear basement patio.

A schematic plan of the proposed SuDS features on site, which would provide the necessary attenuation storage, is presented overleaf.

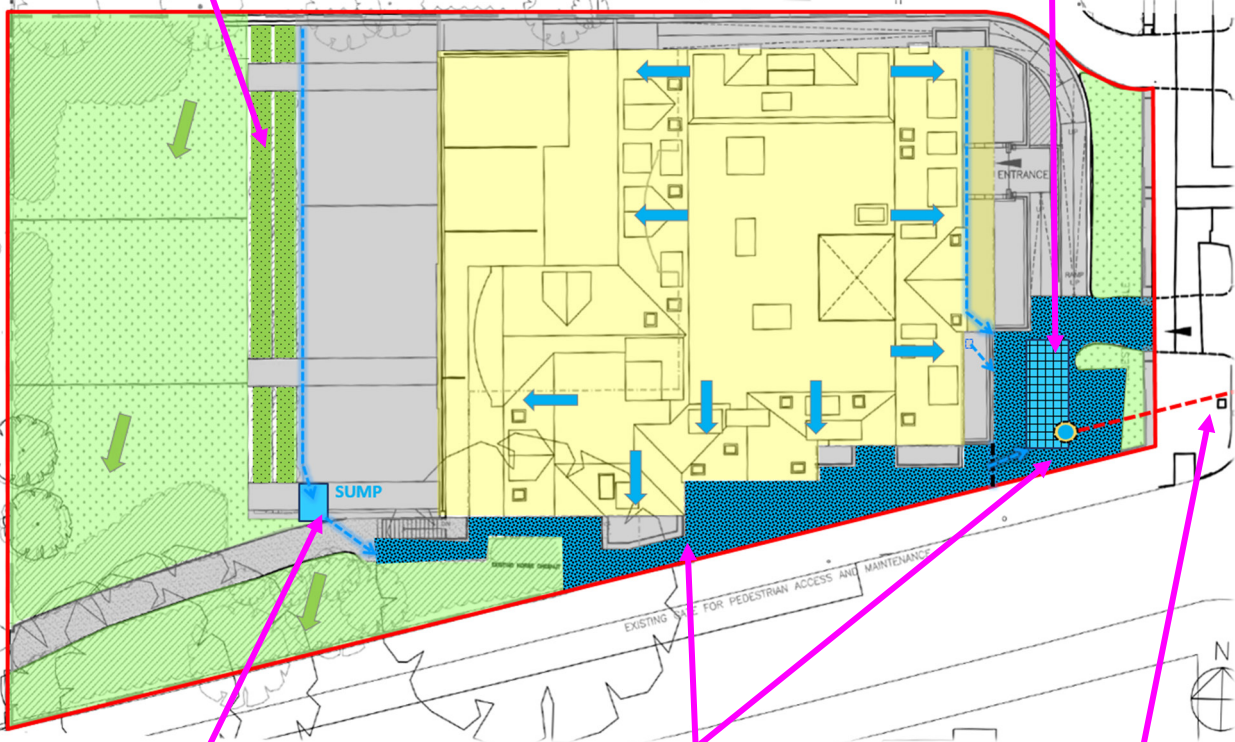
A schematic section of the proposed SuDS features is also provided, illustrating the envisaged required levels of the storage features in order to ensure feasibility of gravity drainage towards the final attenuation tank.

Not shown on plan:

- Possible rainwater harvesting butts in the basement patio

New stepped planting with a possibility of providing a small rain garden feature

Underground attenuation storage tank providing approx. 15m³ of storage

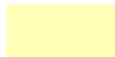


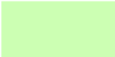




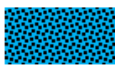



Basement level sump & pump leading runoff from the basement patio area towards the attenuation storage underlying the permeable paving

Garden level and front street level permeable paving with an underlying, 200mm thick storage layer providing a total of approx. 30m³ of attenuation storage

Final discharge to the public combined sewer

SUDS KEY :

BUILDING		PAVED		RUN-OFF	
GARDEN		FLOW CONTROL		SEWER	
DEVELOPMENT AREA		SW PIPE			
PERMEABLE PAVING UNDERLAIN BY STORAGE LAYER		ATTENAUTION STORAGE TANK			



Schematic section showing the approximate arrangement of the proposed attenuation storage SuDS features, showing the levels of the features in relation to each other.

7. CONCLUSION

This assessment has demonstrated that the developer has sought opportunities to reduce the overall level of flood risk through the appropriate application of sustainable drainage systems.

This assessment demonstrates that there is scope for various SuDS features that can restrain run-off, in accordance with Policy CC3 of the Camden Local Plan, to mitigate the risk of future surface water flooding, taking into account potential climate change.

APPENDIX

SUSTAINABLE DRAINAGE PRO-FORMA
PRELIMINARY DRAINAGE CALCULATIONS

1. Project & Site Details	Project / Site Name (including sub-catchment / stage / phase where appropriate)	39 FITZJOHN'S AVENUE
	Address & post code	
	OS Grid ref. (Easting, Northing)	E 525585 N 183920
	LPA reference (if applicable)	
	Brief description of proposed work	Construction of a new rear basement extension as well as a front basement level lightwell.
	Total site Area for Attenuation	2150 m ²
	Total existing impervious area	1130 m ²
	Total proposed impervious area	1290 m ²
	Is the site in a surface water flood risk catchment (ref. local Surface Water Management Plan)?	No
	Existing drainage connection type and location	Combined Sewer beneath Fitzjohn's Avenue
	Designer Name	S R L B
	Designer Position	Principal
Designer Company	LBHGEO	

2. Proposed Discharge Arrangements	2a. Infiltration Feasibility		
	Superficial geology classification	N/A	
	Bedrock geology classification	London Clay	
	Site infiltration rate	1.E-09 m/s	
	Depth to groundwater level	No groundwater table present	
	Is infiltration feasible?	No	
	2b. Drainage Hierarchy		
		<i>Feasible (Y/N)</i>	<i>Proposed (Y/N)</i>
	1 store rainwater for later use	Y	Y
	2 use infiltration techniques, such as porous surfaces in non-clay areas	N	N
	3 attenuate rainwater in ponds or open water features for gradual release	Y	N
	4 attenuate rainwater by storing in tanks or sealed water features for gradual release	Y	Y
	5 discharge rainwater direct to a watercourse	N	N
	6 discharge rainwater to a surface water sewer/drain	N	N
	7 discharge rainwater to the combined sewer.	Y	Y
2c. Proposed Discharge Details			
Proposed discharge location	Combined Sewer beneath Fitzjohn's Avenue		
Has the owner/regulator of the discharge location been consulted?	No - as there will be a reduction in the volume and rate of water entering the TW sewer		

3. Drainage Strategy	3a. Discharge Rates & Required Storage				
		<i>Greenfield (GF) runoff rate (l/s)</i>	<i>Existing discharge rate (l/s)</i>	<i>Required storage for GF rate (m³)</i>	<i>Proposed discharge rate (l/s)</i>
	<i>Q_{bar}</i>	0.93			
	<i>1 in 1</i>	0.79	16.34	25.45	0.79
	<i>1 in 30</i>	2.15	39.90	56.38	2.15
	<i>1 in 100</i>	2.98	51.15	73.93	2.98
	<i>1 in 100 + CC</i>			112.09	2.98
	<i>Climate change allowance used</i>		40%		
	3b. Principal Method of Flow Control		Orifice		
	3c. Proposed SuDS Measures				
		<i>Catchment area (m²)</i>	<i>Plan area (m²)</i>	<i>Storage vol. (m³)</i>	
	Rainwater harvesting	0		0	
	Infiltration systems	0		0	
	Green roofs	0	0	0	
	Blue roofs	0	0	0	
	Filter strips	0	0	0	
	Filter drains	0	0	0	
	Bioretention / tree pits	0	0	0	
	Pervious pavements	1290	150	30	
	Swales	0	0	0	
Basins/ponds	0	0	0		
Attenuation tanks	1290		15		
Total	2580	150	45		

4. Supporting Information	4a. Discharge & Drainage Strategy	<i>Page/section of drainage report</i>
	Infiltration feasibility (2a) – geotechnical factual and interpretive reports, including infiltration results	Appendix to the SuDS Assessment
	Drainage hierarchy (2b)	Section 4
	Proposed discharge details (2c) – utility plans, correspondence / approval from owner/regulator of discharge location	Discharge is to be via existing manhole and existing sewer connection - there will be no new connection and a reduction in the volume and rate of water entering the TW sewer
	Discharge rates & storage (3a) – detailed hydrologic and hydraulic calculations	Appendix to the SuDS Assessment
	Proposed SuDS measures & specifications (3b)	Section 6
	4b. Other Supporting Details	<i>Page/section of drainage report</i>
	Detailed Development Layout	P12
	Detailed drainage design drawings, including exceedance flow routes	P21
	Detailed landscaping plans	P12
	Maintenance strategy	Section 4.6
	Demonstration of how the proposed SuDS measures improve:	SuDS Assessment report
	a) water quality of the runoff?	Section 4.4
	b) biodiversity?	
	c) amenity?	

GREENFIELD RUNOFF

Catchment Area: 2150sqm 0.215ha

PO Code : 0

Hydrological Region: 6 From Wallingford on-line tool

SAAR: 650mm From Wallingford on-line tool

SOIL type: 4 From Wallingford on-line tool

SPR: 0.47 Derived as follows:

SOIL	Sand	Clayey Sand	Sandy Clay	Clay	Rock
SPR	1	2	3	4	5
	0.1	0.3	0.37	0.47	0.53



From Wallingford on-line tool using IH 124 Method

Qbar: 217.37 Calculated from SPR and SAAR

Greenfield Peak

Run-off Rate:		Growth curve Factor
1 in 1	184.8 l/sec	0.85
1 in 30	500.0 l/sec	2.30
1 in 100	693.4 l/sec	3.19
1 in 200	813.0 l/sec	3.74

Qbar: 0.93 l/sec

Greenfield

Peak Run-off Rate:

1 in 1	0.79 l/sec
1 in 30	2.15 l/sec
1 in 100	2.98 l/sec
1 in 200	3.50 l/sec

National Non-Statutory Guidance:

For greenfield developments, the peak runoff rate from the development to any highway drain, sewer or surface water body for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event should never exceed the peak greenfield runoff rate for the same event.

For developments which were previously developed, the peak runoff rate from the development to any drain, sewer or surface water body for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event should be as close as reasonably practicable to the greenfield runoff rate from the development for the same rainfall event, but should never exceed the rate of discharge from the development prior to redevelopment for that event.

Where reasonably practicable, for greenfield development, the runoff volume from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event should never exceed the greenfield runoff volume for the same event.

Where reasonably practicable, for developments which have been previously developed, the runoff volume from the development to any highway drain, sewer or surface water body in the 1 in 100 year, 6 hour rainfall event must be constrained to a value as close as is reasonably practicable to the greenfield runoff volume for the same event, but should never exceed the runoff volume from the development site prior to redevelopment for that event.

SuDs CALCULATIONS	
Project: 39 FITZJOHN'S AVENUE	
GREENFIELD RUNOFF	
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LBHGEO

RAINFALL PEAK INTENSITY (i)

								D Duration		Z1	M5-D
								5min	5min	0.38	7.6mm
M5-60 :		20	From Wallingford Fig A1				10min		10min	0.55	11.0mm
r:		0.42	From Wallingford Fig A2				15min		15min	0.65	13.0mm
							30min		30min	0.75	15.0mm
							1hr		60min	1.00	20.0mm
							2hr		120min	1.20	24.0mm
							4hr		240min	1.40	28.0mm
							6hr		360min	1.60	32.0mm
							10hr		600min	1.70	34.0mm
							24hr		1440min	2.20	44.0mm
							48hr		2880min	2.50	50.0mm
Z2											
D Duration		M5-D	M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	7.6mm	0.62	0.79	0.89	0.97	1.02	1.19	1.36	1.43	1.79
10min	10min	11.0mm	0.61	0.79	0.90	0.97	1.03	1.22	1.41	1.49	1.91
15min	15min	13.0mm	0.61	0.79	0.90	0.97	1.03	1.22	1.41	1.49	1.91
30min	30min	15.0mm	0.62	0.81	0.90	0.97	1.03	1.24	1.44	1.53	1.99
1hr	60min	20.0mm	0.64	0.81	0.90	0.97	1.03	1.24	1.45	1.54	2.03
2hr	120min	24.0mm	0.64	0.81	0.90	0.97	1.03	1.24	1.45	1.54	2.03
4hr	240min	28.0mm	0.66	0.82	0.91	0.97	1.03	1.24	1.44	1.53	2.01
6hr	360min	32.0mm	0.68	0.83	0.91	0.97	1.03	1.22	1.42	1.51	1.97
10hr	600min	34.0mm	0.68	0.83	0.91	0.97	1.03	1.22	1.42	1.51	1.97
24hr	1440min	44.0mm	0.70	0.84	0.92	0.97	1.02	1.19	1.38	1.47	1.89
48hr	2880min	50.0mm	0.72	0.85	0.93	0.98	1.02	1.17	1.34	1.42	1.81
MT-D											
D Duration		M5-D	M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	7.6mm	4.7mm	6.0mm	6.8mm	7.4mm	7.8mm	9.0mm	10.3mm	10.8mm	13.6mm
10min	10min	11.0mm	6.7mm	8.7mm	9.9mm	10.7mm	11.3mm	13.4mm	15.5mm	16.4mm	21.0mm
15min	15min	13.0mm	7.9mm	10.3mm	11.7mm	12.6mm	13.4mm	15.9mm	18.3mm	19.4mm	24.8mm
30min	30min	15.0mm	9.3mm	12.2mm	13.5mm	14.6mm	15.5mm	18.6mm	21.6mm	22.9mm	29.9mm
1hr	60min	20.0mm	12.8mm	16.2mm	18.0mm	19.4mm	20.6mm	24.8mm	29.0mm	30.9mm	40.6mm
2hr	120min	24.0mm	15.4mm	19.4mm	21.6mm	23.3mm	24.7mm	29.8mm	34.8mm	37.0mm	48.7mm
4hr	240min	28.0mm	18.5mm	23.0mm	25.5mm	27.2mm	28.8mm	34.7mm	40.3mm	42.9mm	56.3mm
6hr	360min	32.0mm	21.8mm	26.6mm	29.1mm	31.0mm	33.0mm	39.0mm	45.4mm	48.4mm	63.0mm
10hr	600min	34.0mm	23.1mm	28.2mm	30.9mm	33.0mm	35.0mm	41.5mm	48.3mm	51.5mm	67.0mm
24hr	1440min	44.0mm	30.8mm	37.0mm	40.5mm	42.7mm	44.9mm	52.4mm	60.7mm	64.5mm	83.2mm
48hr	2880min	50.0mm	36.0mm	42.5mm	46.5mm	49.0mm	51.0mm	58.5mm	67.0mm	71.0mm	90.5mm
Intensity i											
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	56.5mm/hr	72.0mm/hr	81.2mm/hr	88.5mm/hr	93.0mm/hr	108.5mm/hr	124.0mm/hr	130.1mm/hr	163.2mm/hr
10min	10min	0.17hr	40.3mm/hr	52.1mm/hr	59.4mm/hr	64.0mm/hr	68.0mm/hr	80.5mm/hr	93.1mm/hr	98.3mm/hr	126.1mm/hr
15min	15min	0.25hr	31.7mm/hr	41.1mm/hr	46.8mm/hr	50.4mm/hr	53.6mm/hr	63.4mm/hr	73.3mm/hr	77.5mm/hr	99.3mm/hr
30min	30min	0.50hr	18.6mm/hr	24.3mm/hr	27.0mm/hr	29.1mm/hr	30.9mm/hr	37.2mm/hr	43.2mm/hr	45.8mm/hr	59.7mm/hr
1hr	60min	1.00hr	12.8mm/hr	16.2mm/hr	18.0mm/hr	19.4mm/hr	20.6mm/hr	24.8mm/hr	29.0mm/hr	30.9mm/hr	40.6mm/hr
2hr	120min	2.00hr	7.7mm/hr	9.7mm/hr	10.8mm/hr	11.6mm/hr	12.4mm/hr	14.9mm/hr	17.4mm/hr	18.5mm/hr	24.4mm/hr
4hr	240min	4.00hr	4.6mm/hr	5.7mm/hr	6.4mm/hr	6.8mm/hr	7.2mm/hr	8.7mm/hr	10.1mm/hr	10.7mm/hr	14.1mm/hr
6hr	360min	6.00hr	3.6mm/hr	4.4mm/hr	4.9mm/hr	5.2mm/hr	5.5mm/hr	6.5mm/hr	7.6mm/hr	8.1mm/hr	10.5mm/hr
10hr	600min	10.00hr	2.3mm/hr	2.8mm/hr	3.1mm/hr	3.3mm/hr	3.5mm/hr	4.1mm/hr	4.8mm/hr	5.1mm/hr	6.7mm/hr
24hr	1440min	24.00hr	1.3mm/hr	1.5mm/hr	1.7mm/hr	1.8mm/hr	1.9mm/hr	2.2mm/hr	2.5mm/hr	2.7mm/hr	3.5mm/hr
48hr	2880min	48.00hr	0.6mm/hr	0.8mm/hr	0.8mm/hr	0.9mm/hr	0.9mm/hr	1.1mm/hr	1.3mm/hr	1.3mm/hr	1.7mm/hr
48hr	2880min	48.00hr	0.8mm/hr	0.9mm/hr	1.0mm/hr	1.0mm/hr	1.1mm/hr	1.2mm/hr	1.4mm/hr	1.5mm/hr	1.9mm/hr

GREENFIELD PEAK RUNOFF

Hydrological Region: 6 From Wallingford on-line tool Qbar: 0.93 l/sec

			Run-Off Q								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
10min	10min	0.17hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
15min	15min	0.25hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
30min	30min	0.50hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
1hr	60min	1.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
2hr	120min	2.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
4hr	240min	4.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
6hr	360min	6.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
10hr	600min	10.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
24hr	1440min	24.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec
48hr	2880min	48.00hr	0.79 l/sec	0.82 l/sec	0.95 l/sec	1.07 l/sec	1.20 l/sec	1.51 l/sec	1.84 l/sec	2.24 l/sec	2.98 l/sec

			Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	0.2 m3	0.2 m3	0.3 m3	0.3 m3	0.4 m3	0.5 m3	0.6 m3	0.7 m3	0.9 m3
10min	10min	0.17hr	0.5 m3	0.5 m3	0.6 m3	0.6 m3	0.7 m3	0.9 m3	1.1 m3	1.3 m3	1.8 m3
15min	15min	0.25hr	0.7 m3	0.7 m3	0.9 m3	1.0 m3	1.1 m3	1.4 m3	1.7 m3	2.0 m3	2.7 m3
30min	30min	0.50hr	1.4 m3	1.5 m3	1.7 m3	1.9 m3	2.2 m3	2.7 m3	3.3 m3	4.0 m3	5.4 m3
1hr	60min	1.00hr	2.9 m3	3.0 m3	3.4 m3	3.9 m3	4.3 m3	5.5 m3	6.6 m3	8.1 m3	10.7 m3
2hr	120min	2.00hr	5.7 m3	5.9 m3	6.8 m3	7.7 m3	8.6 m3	10.9 m3	13.2 m3	16.2 m3	21.5 m3
4hr	240min	4.00hr	11.4 m3	11.8 m3	13.6 m3	15.4 m3	17.2 m3	21.8 m3	26.5 m3	32.3 m3	42.9 m3
6hr	360min	6.00hr	17.2 m3	17.8 m3	20.5 m3	23.2 m3	25.8 m3	32.7 m3	39.7 m3	48.5 m3	64.4 m3
10hr	600min	10.00hr	28.6 m3	29.6 m3	34.1 m3	38.6 m3	43.1 m3	54.5 m3	66.2 m3	80.8 m3	107.3 m3
24hr	1440min	24.00hr	68.6 m3	71.1 m3	81.8 m3	92.6 m3	103.4 m3	130.8 m3	158.8 m3	193.8 m3	257.6 m3
48hr	2880min	48.00hr	137.3 m3	142.1 m3	163.7 m3	185.2 m3	206.7 m3	261.7 m3	317.6 m3	387.6 m3	515.2 m3

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EXISTING PEAK RUNOFF

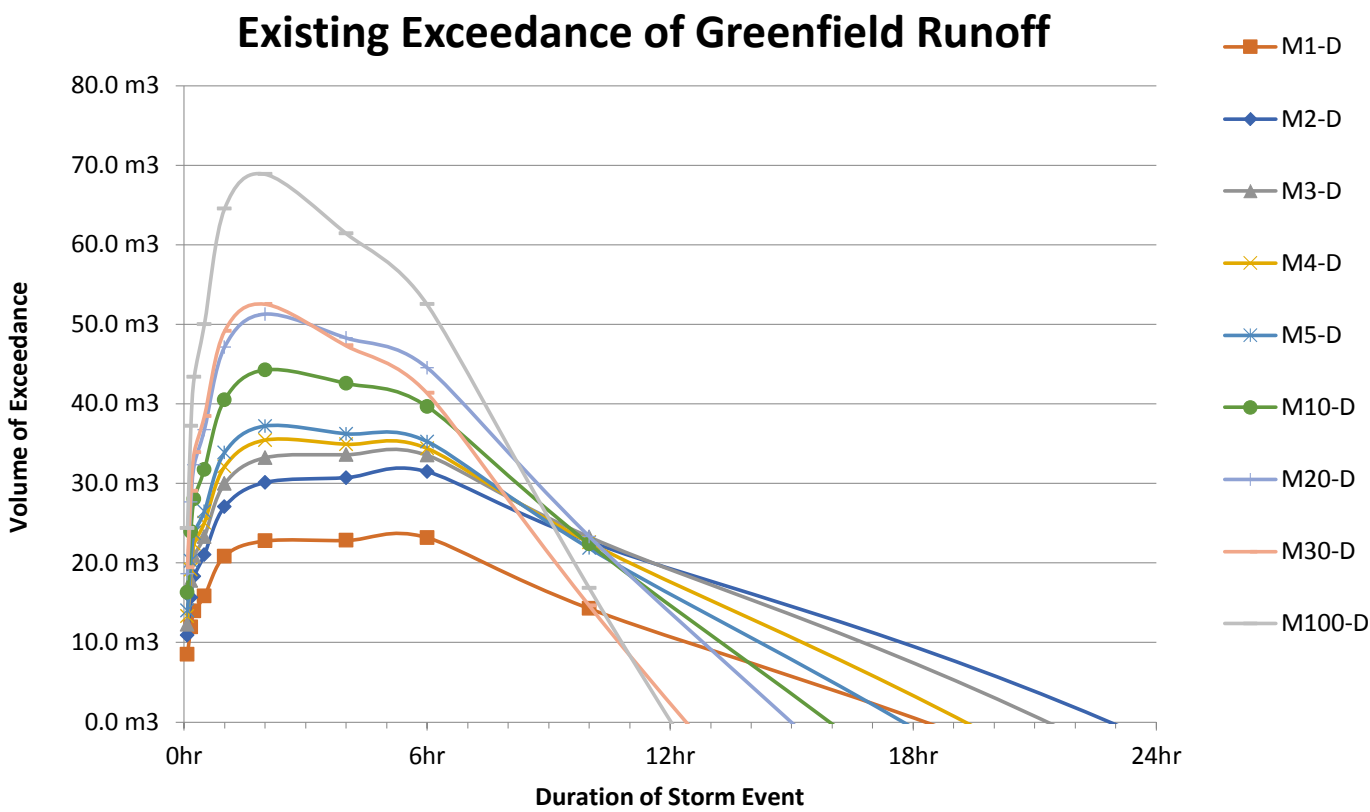
C _V :	0.66	Volumetric Run-Off Coefficient
C _R :	1.3	Routing Coefficient

			Run-Off Q								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	29.1 l/sec	37.1 l/sec	41.8 l/sec	45.6 l/sec	47.9 l/sec	55.9 l/sec	63.9 l/sec	67.0 l/sec	84.1 l/sec
10min	10min	0.17hr	20.7 l/sec	26.9 l/sec	30.6 l/sec	33.0 l/sec	35.0 l/sec	41.5 l/sec	47.9 l/sec	50.6 l/sec	64.9 l/sec
15min	15min	0.25hr	16.3 l/sec	21.2 l/sec	24.1 l/sec	26.0 l/sec	27.6 l/sec	32.7 l/sec	37.8 l/sec	39.9 l/sec	51.1 l/sec
30min	30min	0.50hr	9.6 l/sec	12.5 l/sec	13.9 l/sec	15.0 l/sec	15.9 l/sec	19.2 l/sec	22.2 l/sec	23.6 l/sec	30.7 l/sec
1hr	60min	1.00hr	6.6 l/sec	8.3 l/sec	9.3 l/sec	10.0 l/sec	10.6 l/sec	12.8 l/sec	14.9 l/sec	15.9 l/sec	20.9 l/sec
2hr	120min	2.00hr	4.0 l/sec	5.0 l/sec	5.6 l/sec	6.0 l/sec	6.4 l/sec	7.7 l/sec	9.0 l/sec	9.5 l/sec	12.5 l/sec
4hr	240min	4.00hr	2.4 l/sec	3.0 l/sec	3.3 l/sec	3.5 l/sec	3.7 l/sec	4.5 l/sec	5.2 l/sec	5.5 l/sec	7.2 l/sec
6hr	360min	6.00hr	1.9 l/sec	2.3 l/sec	2.5 l/sec	2.7 l/sec	2.8 l/sec	3.4 l/sec	3.9 l/sec	4.2 l/sec	5.4 l/sec
10hr	600min	10.00hr	1.2 l/sec	1.5 l/sec	1.6 l/sec	1.7 l/sec	1.8 l/sec	2.1 l/sec	2.5 l/sec	2.6 l/sec	3.4 l/sec
24hr	1440min	24.00hr	0.7 l/sec	0.8 l/sec	0.9 l/sec	0.9 l/sec	1.0 l/sec	1.1 l/sec	1.3 l/sec	1.4 l/sec	1.8 l/sec
48hr	2880min	48.00hr	0.4 l/sec	0.5 l/sec	0.5 l/sec	0.5 l/sec	0.5 l/sec	0.6 l/sec	0.7 l/sec	0.8 l/sec	1.0 l/sec

			Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	8.7 m3	11.1 m3	12.5 m3	13.7 m3	14.4 m3	16.8 m3	19.2 m3	20.1 m3	25.2 m3
10min	10min	0.17hr	12.4 m3	16.1 m3	18.4 m3	19.8 m3	21.0 m3	24.9 m3	28.8 m3	30.4 m3	39.0 m3
15min	15min	0.25hr	14.7 m3	19.0 m3	21.7 m3	23.4 m3	24.8 m3	29.4 m3	34.0 m3	35.9 m3	46.0 m3
30min	30min	0.50hr	17.2 m3	22.5 m3	25.0 m3	27.0 m3	28.6 m3	34.5 m3	40.0 m3	42.5 m3	55.3 m3
1hr	60min	1.00hr	23.7 m3	30.0 m3	33.4 m3	36.0 m3	38.2 m3	46.0 m3	53.8 m3	57.2 m3	75.3 m3
2hr	120min	2.00hr	28.5 m3	36.0 m3	40.0 m3	43.2 m3	45.8 m3	55.2 m3	64.5 m3	68.7 m3	90.3 m3
4hr	240min	4.00hr	34.3 m3	42.6 m3	47.2 m3	50.4 m3	53.5 m3	64.4 m3	74.8 m3	79.6 m3	104.3 m3
6hr	360min	6.00hr	40.3 m3	49.2 m3	54.0 m3	57.5 m3	61.1 m3	72.4 m3	84.2 m3	89.8 m3	116.9 m3
10hr	600min	10.00hr	42.9 m3	52.3 m3	57.4 m3	61.1 m3	64.9 m3	76.9 m3	89.5 m3	95.4 m3	124.2 m3
24hr	1440min	24.00hr	57.1 m3	68.5 m3	75.0 m3	79.1 m3	83.2 m3	97.1 m3	112.6 m3	119.6 m3	154.2 m3
48hr	2880min	48.00hr	66.7 m3	78.8 m3	86.2 m3	90.8 m3	94.6 m3	108.5 m3	124.2 m3	131.6 m3	167.8 m3

			Exceedance of Greenfield Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	8.5 m3	10.9 m3	12.3 m3	13.3 m3	14.0 m3	16.3 m3	18.6 m3	19.4 m3	24.3 m3
10min	10min	0.17hr	12.0 m3	15.6 m3	17.8 m3	19.1 m3	20.3 m3	24.0 m3	27.7 m3	29.0 m3	37.2 m3
15min	15min	0.25hr	14.0 m3	18.3 m3	20.8 m3	22.4 m3	23.7 m3	28.0 m3	32.3 m3	33.9 m3	43.4 m3
30min	30min	0.50hr	15.8 m3	21.0 m3	23.3 m3	25.0 m3	26.5 m3	31.8 m3	36.7 m3	38.4 m3	50.0 m3
1hr	60min	1.00hr	20.9 m3	27.1 m3	30.0 m3	32.1 m3	33.9 m3	40.5 m3	47.1 m3	49.2 m3	64.5 m3
2hr	120min	2.00hr	22.8 m3	30.1 m3	33.2 m3	35.4 m3	37.2 m3	44.3 m3	51.3 m3	52.5 m3	68.9 m3
4hr	240min	4.00hr	22.8 m3	30.7 m3	33.6 m3	34.9 m3	36.2 m3	42.6 m3	48.3 m3	47.3 m3	61.4 m3
6hr	360min	6.00hr	23.2 m3	31.5 m3	33.5 m3	34.4 m3	35.3 m3	39.7 m3	44.5 m3	41.3 m3	52.5 m3
10hr	600min	10.00hr	14.3 m3	22.7 m3	23.3 m3	22.6 m3	21.9 m3	22.4 m3	23.3 m3	14.6 m3	16.8 m3
24hr	1440min	24.00hr	-11.5 m3	-2.5 m3	-6.8 m3	-13.5 m3	-20.2 m3	-33.8 m3	-46.2 m3	-74.2 m3	-103.4 m3
48hr	2880min	48.00hr	-70.5 m3	-63.3 m3	-77.5 m3	-94.4 m3	-112.2 m3	-153.2 m3	-193.4 m3	-256.0 m3	-347.4 m3

			C _V :
Catchment Area:	2150sqm	100%	
Permeable:	1020sqm	47%	0.40
Impermeable:	1130sqm	53%	0.90
			0.66



SuDs CALCULATIONS	
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Project Reference: LBH4498	
Date: 04/02/2021	Rev: 1
Client:	Godfrey London

LBHGEO

POST- DEVELOPMENT PEAK RUNOFF

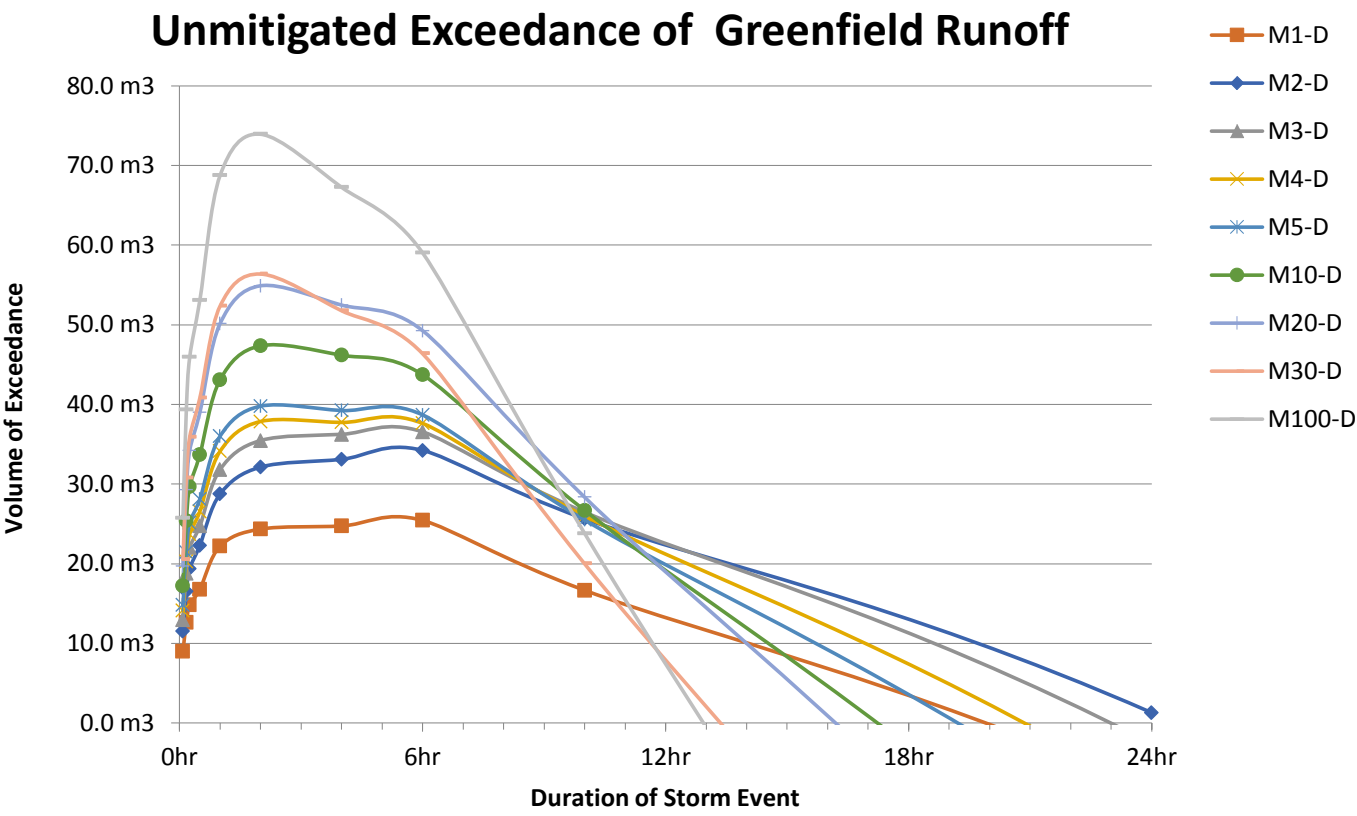
C _V :	0.70	Volumetric Run-Off Coefficient	Climate Change Allowance:	0%
C _R :	1.3	Routing Coefficient		

			Run-Off Q								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	30.8 l/sec	39.2 l/sec	44.1 l/sec	48.1 l/sec	50.6 l/sec	59.0 l/sec	67.5 l/sec	70.8 l/sec	88.8 l/sec
10min	10min	0.17hr	21.9 l/sec	28.4 l/sec	32.3 l/sec	34.8 l/sec	37.0 l/sec	43.8 l/sec	50.6 l/sec	53.5 l/sec	68.6 l/sec
15min	15min	0.25hr	17.3 l/sec	22.3 l/sec	25.5 l/sec	27.4 l/sec	29.1 l/sec	34.5 l/sec	39.9 l/sec	42.1 l/sec	54.0 l/sec
30min	30min	0.50hr	10.1 l/sec	13.2 l/sec	14.7 l/sec	15.8 l/sec	16.8 l/sec	20.2 l/sec	23.5 l/sec	24.9 l/sec	32.5 l/sec
1hr	60min	1.00hr	7.0 l/sec	8.8 l/sec	9.8 l/sec	10.6 l/sec	11.2 l/sec	13.5 l/sec	15.8 l/sec	16.8 l/sec	22.1 l/sec
2hr	120min	2.00hr	4.2 l/sec	5.3 l/sec	5.9 l/sec	6.3 l/sec	6.7 l/sec	8.1 l/sec	9.5 l/sec	10.1 l/sec	13.2 l/sec
4hr	240min	4.00hr	2.5 l/sec	3.1 l/sec	3.5 l/sec	3.7 l/sec	3.9 l/sec	4.7 l/sec	5.5 l/sec	5.8 l/sec	7.7 l/sec
6hr	360min	6.00hr	2.0 l/sec	2.4 l/sec	2.6 l/sec	2.8 l/sec	3.0 l/sec	3.5 l/sec	4.1 l/sec	4.4 l/sec	5.7 l/sec
10hr	600min	10.00hr	1.3 l/sec	1.5 l/sec	1.7 l/sec	1.8 l/sec	1.9 l/sec	2.3 l/sec	2.6 l/sec	2.8 l/sec	3.6 l/sec
24hr	1440min	24.00hr	0.7 l/sec	0.8 l/sec	0.9 l/sec	1.0 l/sec	1.0 l/sec	1.2 l/sec	1.4 l/sec	1.5 l/sec	1.9 l/sec
48hr	2880min	48.00hr	0.4 l/sec	0.5 l/sec	0.5 l/sec	0.6 l/sec	0.6 l/sec	0.7 l/sec	0.8 l/sec	0.8 l/sec	1.0 l/sec

			Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	9.2 m3	11.8 m3	13.2 m3	14.4 m3	15.2 m3	17.7 m3	20.2 m3	21.2 m3	26.6 m3
10min	10min	0.17hr	13.1 m3	17.0 m3	19.4 m3	20.9 m3	22.2 m3	26.3 m3	30.4 m3	32.1 m3	41.1 m3
15min	15min	0.25hr	15.5 m3	20.1 m3	22.9 m3	24.7 m3	26.2 m3	31.1 m3	35.9 m3	37.9 m3	48.6 m3
30min	30min	0.50hr	18.2 m3	23.8 m3	26.4 m3	28.5 m3	30.3 m3	36.4 m3	42.3 m3	44.8 m3	58.4 m3
1hr	60min	1.00hr	25.1 m3	31.7 m3	35.2 m3	38.0 m3	40.3 m3	48.6 m3	56.8 m3	60.4 m3	79.5 m3
2hr	120min	2.00hr	30.1 m3	38.1 m3	42.3 m3	45.6 m3	48.4 m3	58.3 m3	68.1 m3	72.5 m3	95.4 m3
4hr	240min	4.00hr	36.2 m3	45.0 m3	49.9 m3	53.2 m3	56.5 m3	68.0 m3	78.9 m3	84.1 m3	110.2 m3
6hr	360min	6.00hr	42.6 m3	52.0 m3	57.0 m3	60.8 m3	64.5 m3	76.4 m3	89.0 m3	94.8 m3	123.4 m3
10hr	600min	10.00hr	45.3 m3	55.3 m3	60.6 m3	64.6 m3	68.6 m3	81.2 m3	94.5 m3	100.7 m3	131.2 m3
24hr	1440min	24.00hr	60.3 m3	72.4 m3	79.3 m3	83.6 m3	87.9 m3	102.5 m3	118.9 m3	126.4 m3	162.8 m3
48hr	2880min	48.00hr	70.5 m3	83.2 m3	91.1 m3	95.9 m3	99.9 m3	114.5 m3	131.2 m3	139.0 m3	177.2 m3

			Exceedance of Greenfield Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	9.0 m3	11.5 m3	13.0 m3	14.1 m3	14.8 m3	17.3 m3	19.7 m3	20.6 m3	25.7 m3
10min	10min	0.17hr	12.7 m3	16.5 m3	18.8 m3	20.2 m3	21.5 m3	25.4 m3	29.3 m3	30.7 m3	39.3 m3
15min	15min	0.25hr	14.8 m3	19.4 m3	22.1 m3	23.7 m3	25.1 m3	29.7 m3	34.2 m3	35.9 m3	45.9 m3
30min	30min	0.50hr	16.8 m3	22.3 m3	24.7 m3	26.6 m3	28.1 m3	33.7 m3	39.0 m3	40.8 m3	53.1 m3
1hr	60min	1.00hr	22.2 m3	28.8 m3	31.8 m3	34.1 m3	36.0 m3	43.1 m3	50.2 m3	52.4 m3	68.8 m3
2hr	120min	2.00hr	24.4 m3	32.1 m3	35.5 m3	37.9 m3	39.8 m3	47.4 m3	54.9 m3	56.4 m3	73.9 m3
4hr	240min	4.00hr	24.7 m3	33.1 m3	36.3 m3	37.7 m3	39.2 m3	46.2 m3	52.5 m3	51.8 m3	67.3 m3
6hr	360min	6.00hr	25.4 m3	34.2 m3	36.6 m3	37.6 m3	38.7 m3	43.7 m3	49.3 m3	46.4 m3	59.0 m3
10hr	600min	10.00hr	16.7 m3	25.6 m3	26.5 m3	26.0 m3	25.5 m3	26.7 m3	28.4 m3	20.0 m3	23.8 m3
24hr	1440min	24.00hr	-8.3 m3	1.3 m3	-2.6 m3	-9.0 m3	-15.5 m3	-28.3 m3	-39.9 m3	-67.5 m3	-94.8 m3
48hr	2880min	48.00hr	-66.8 m3	-58.9 m3	-72.6 m3	-89.3 m3	-106.9 m3	-147.1 m3	-186.5 m3	-248.6 m3	-338.0 m3
			25.4 m3							56.4 m3	73.9 m3

			C _V :	
Catchment Area:	2150sqm	100%		
Permeable Garden	860sqm	40%	0.40	
Impermeable:	1290sqm	60%	0.90	
			0.70	



SuDs CALCULATIONS	
Project: 39 FITZJOHN'S AVENUE	
POST-DEV. PEAK RUNOFF	
Sheet 5 of 8	
Project Reference: LBH4498	
Date: 04/02/2021	Rev: 1
Client:	Godfrey London

LBHGEO

POST- DEVELOPMENT PEAK RUNOFF + CC

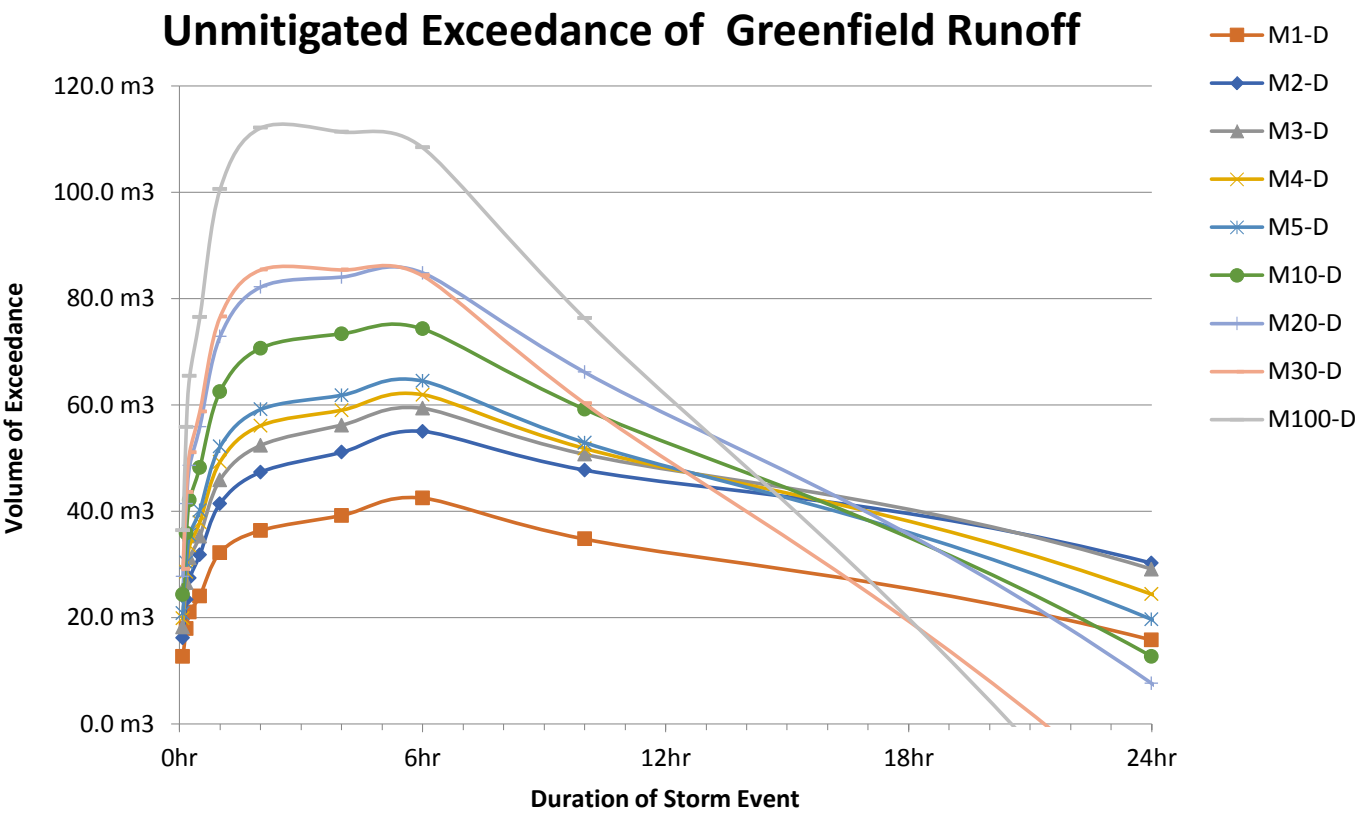
C _V :	0.70	Volumetric Run-Off Coefficient	Climate Change Allowance:	40%
C _R :	1.3	Routing Coefficient		

			Run-Off Q								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	43.1 l/sec	54.9 l/sec	61.8 l/sec	67.4 l/sec	70.8 l/sec	82.6 l/sec	94.4 l/sec	99.1 l/sec	124.3 l/sec
10min	10min	0.17hr	30.7 l/sec	39.7 l/sec	45.2 l/sec	48.7 l/sec	51.8 l/sec	61.3 l/sec	70.9 l/sec	74.9 l/sec	96.0 l/sec
15min	15min	0.25hr	24.2 l/sec	31.3 l/sec	35.6 l/sec	38.4 l/sec	40.8 l/sec	48.3 l/sec	55.8 l/sec	59.0 l/sec	75.6 l/sec
30min	30min	0.50hr	14.2 l/sec	18.5 l/sec	20.6 l/sec	22.2 l/sec	23.5 l/sec	28.3 l/sec	32.9 l/sec	34.9 l/sec	45.5 l/sec
1hr	60min	1.00hr	9.7 l/sec	12.3 l/sec	13.7 l/sec	14.8 l/sec	15.7 l/sec	18.9 l/sec	22.1 l/sec	23.5 l/sec	30.9 l/sec
2hr	120min	2.00hr	5.8 l/sec	7.4 l/sec	8.2 l/sec	8.9 l/sec	9.4 l/sec	11.3 l/sec	13.2 l/sec	14.1 l/sec	18.5 l/sec
4hr	240min	4.00hr	3.5 l/sec	4.4 l/sec	4.9 l/sec	5.2 l/sec	5.5 l/sec	6.6 l/sec	7.7 l/sec	8.2 l/sec	10.7 l/sec
6hr	360min	6.00hr	2.8 l/sec	3.4 l/sec	3.7 l/sec	3.9 l/sec	4.2 l/sec	5.0 l/sec	5.8 l/sec	6.1 l/sec	8.0 l/sec
10hr	600min	10.00hr	1.8 l/sec	2.1 l/sec	2.4 l/sec	2.5 l/sec	2.7 l/sec	3.2 l/sec	3.7 l/sec	3.9 l/sec	5.1 l/sec
24hr	1440min	24.00hr	1.0 l/sec	1.2 l/sec	1.3 l/sec	1.4 l/sec	1.4 l/sec	1.7 l/sec	1.9 l/sec	2.0 l/sec	2.6 l/sec
48hr	2880min	48.00hr	0.6 l/sec	0.7 l/sec	0.7 l/sec	0.8 l/sec	0.8 l/sec	0.9 l/sec	1.1 l/sec	1.1 l/sec	1.4 l/sec

			Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	12.9 m3	16.5 m3	18.5 m3	20.2 m3	21.3 m3	24.8 m3	28.3 m3	29.7 m3	37.3 m3
10min	10min	0.17hr	18.4 m3	23.8 m3	27.1 m3	29.2 m3	31.1 m3	36.8 m3	42.5 m3	44.9 m3	57.6 m3
15min	15min	0.25hr	21.7 m3	28.2 m3	32.1 m3	34.6 m3	36.7 m3	43.5 m3	50.2 m3	53.1 m3	68.1 m3
30min	30min	0.50hr	25.5 m3	33.3 m3	37.0 m3	39.9 m3	42.4 m3	51.0 m3	59.2 m3	62.8 m3	81.8 m3
1hr	60min	1.00hr	35.1 m3	44.4 m3	49.3 m3	53.2 m3	56.5 m3	68.0 m3	79.5 m3	84.6 m3	111.3 m3
2hr	120min	2.00hr	42.1 m3	53.3 m3	59.2 m3	63.8 m3	67.8 m3	81.6 m3	95.4 m3	101.5 m3	133.6 m3
4hr	240min	4.00hr	50.7 m3	62.9 m3	69.8 m3	74.5 m3	79.1 m3	95.2 m3	110.5 m3	117.7 m3	154.3 m3
6hr	360min	6.00hr	59.7 m3	72.8 m3	79.8 m3	85.1 m3	90.4 m3	107.0 m3	124.6 m3	132.8 m3	172.8 m3
10hr	600min	10.00hr	63.4 m3	77.4 m3	84.8 m3	90.4 m3	96.0 m3	113.7 m3	132.3 m3	141.0 m3	183.6 m3
24hr	1440min	24.00hr	84.4 m3	101.3 m3	111.0 m3	117.0 m3	123.0 m3	143.5 m3	166.5 m3	176.9 m3	228.0 m3
48hr	2880min	48.00hr	98.7 m3	116.5 m3	127.5 m3	134.3 m3	139.8 m3	160.4 m3	183.7 m3	194.6 m3	248.1 m3

			Exceedance of Greenfield Run-Off Volume								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	12.7 m3	16.2 m3	18.3 m3	19.9 m3	20.9 m3	24.3 m3	27.8 m3	29.0 m3	36.4 m3
10min	10min	0.17hr	17.9 m3	23.3 m3	26.6 m3	28.6 m3	30.3 m3	35.9 m3	41.4 m3	43.6 m3	55.8 m3
15min	15min	0.25hr	21.0 m3	27.4 m3	31.2 m3	33.6 m3	35.6 m3	42.1 m3	48.6 m3	51.1 m3	65.4 m3
30min	30min	0.50hr	24.1 m3	31.8 m3	35.3 m3	38.0 m3	40.2 m3	48.3 m3	55.9 m3	58.7 m3	76.5 m3
1hr	60min	1.00hr	32.2 m3	41.4 m3	45.9 m3	49.3 m3	52.2 m3	62.5 m3	72.9 m3	76.5 m3	100.6 m3
2hr	120min	2.00hr	36.4 m3	47.4 m3	52.4 m3	56.1 m3	59.2 m3	70.7 m3	82.2 m3	85.4 m3	112.1 m3
4hr	240min	4.00hr	39.2 m3	51.1 m3	56.2 m3	59.0 m3	61.8 m3	73.4 m3	84.1 m3	85.4 m3	111.3 m3
6hr	360min	6.00hr	42.5 m3	55.0 m3	59.4 m3	61.9 m3	64.5 m3	74.3 m3	84.9 m3	84.3 m3	108.4 m3
10hr	600min	10.00hr	34.8 m3	47.7 m3	50.7 m3	51.8 m3	52.9 m3	59.2 m3	66.2 m3	60.3 m3	76.3 m3
24hr	1440min	24.00hr	15.8 m3	30.3 m3	29.1 m3	24.4 m3	19.7 m3	12.7 m3	7.6 m3	-16.9 m3	-29.7 m3
48hr	2880min	48.00hr	-38.6 m3	-25.6 m3	-36.2 m3	-50.9 m3	-66.9 m3	-101.3 m3	-134.0 m3	-193.0 m3	-267.1 m3
112.1 m3											

			C _V :
Catchment Area:	2150sqm	100%	
Permeable Garden	860sqm	40%	0.40
Impermeable:	1290sqm	60%	0.90
			0.70



SuDs CALCULATIONS	
Project: 39 FITZJOHN'S AVENUE	
POST-DEV. PEAK RUNOFF+CC	
Sheet 6 of 8	
Project Reference: LBH4498	
Date: 04/02/2021	Rev: 1
Client:	Godfrey London

LBHGEO

POST- DEVELOPMENT & SOURCE MITIGATION PEAK RUN-OFF + CC STORAGE

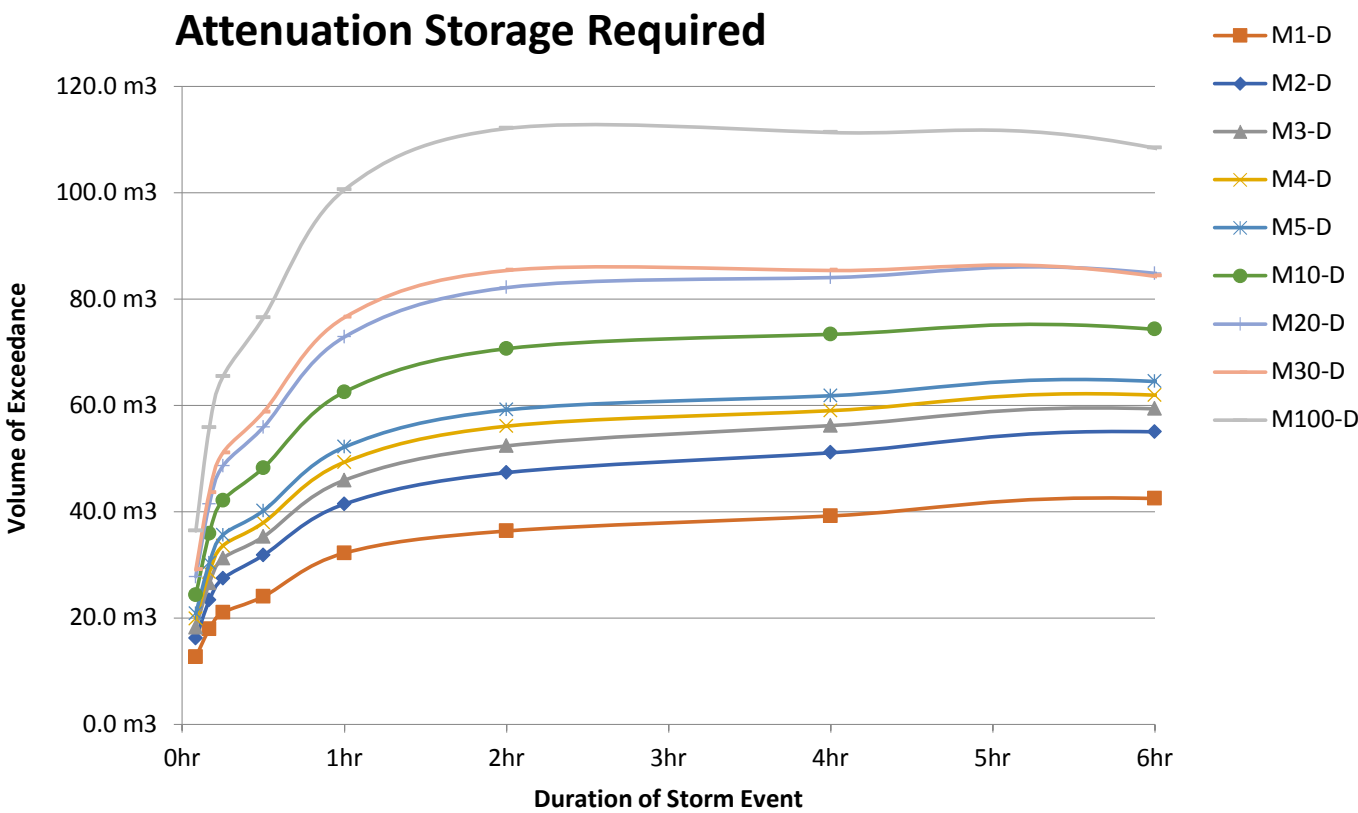
Proposed Discharge Rates: Greenfield x 1

			INFLOW								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	12.9 m3	16.5 m3	18.5 m3	20.2 m3	21.3 m3	24.8 m3	28.3 m3	29.7 m3	37.3 m3
10min	10min	0.17hr	18.4 m3	23.8 m3	27.1 m3	29.2 m3	31.1 m3	36.8 m3	42.5 m3	44.9 m3	57.6 m3
15min	15min	0.25hr	21.7 m3	28.2 m3	32.1 m3	34.6 m3	36.7 m3	43.5 m3	50.2 m3	53.1 m3	68.1 m3
30min	30min	0.50hr	25.5 m3	33.3 m3	37.0 m3	39.9 m3	42.4 m3	51.0 m3	59.2 m3	62.8 m3	81.8 m3
1hr	60min	1.00hr	35.1 m3	44.4 m3	49.3 m3	53.2 m3	56.5 m3	68.0 m3	79.5 m3	84.6 m3	111.3 m3
2hr	120min	2.00hr	42.1 m3	53.3 m3	59.2 m3	63.8 m3	67.8 m3	81.6 m3	95.4 m3	101.5 m3	133.6 m3
4hr	240min	4.00hr	50.7 m3	62.9 m3	69.8 m3	74.5 m3	79.1 m3	95.2 m3	110.5 m3	117.7 m3	154.3 m3
6hr	360min	6.00hr	59.7 m3	72.8 m3	79.8 m3	85.1 m3	90.4 m3	107.0 m3	124.6 m3	132.8 m3	172.8 m3
10hr	600min	10.00hr	63.4 m3	77.4 m3	84.8 m3	90.4 m3	96.0 m3	113.7 m3	132.3 m3	141.0 m3	183.6 m3
24hr	1440min	24.00hr	84.4 m3	101.3 m3	111.0 m3	117.0 m3	123.0 m3	143.5 m3	166.5 m3	176.9 m3	228.0 m3
48hr	2880min	48.00hr	98.7 m3	116.5 m3	127.5 m3	134.3 m3	139.8 m3	160.4 m3	183.7 m3	194.6 m3	248.1 m3

			OUTFLOW								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	0.2 m3	0.2 m3	0.3 m3	0.3 m3	0.4 m3	0.5 m3	0.6 m3	0.7 m3	0.9 m3
10min	10min	0.17hr	0.5 m3	0.5 m3	0.6 m3	0.6 m3	0.7 m3	0.9 m3	1.1 m3	1.3 m3	1.8 m3
15min	15min	0.25hr	0.7 m3	0.7 m3	0.9 m3	1.0 m3	1.1 m3	1.4 m3	1.7 m3	2.0 m3	2.7 m3
30min	30min	0.50hr	1.4 m3	1.5 m3	1.7 m3	1.9 m3	2.2 m3	2.7 m3	3.3 m3	4.0 m3	5.4 m3
1hr	60min	1.00hr	2.9 m3	3.0 m3	3.4 m3	3.9 m3	4.3 m3	5.5 m3	6.6 m3	8.1 m3	10.7 m3
2hr	120min	2.00hr	5.7 m3	5.9 m3	6.8 m3	7.7 m3	8.6 m3	10.9 m3	13.2 m3	16.2 m3	21.5 m3
4hr	240min	4.00hr	11.4 m3	11.8 m3	13.6 m3	15.4 m3	17.2 m3	21.8 m3	26.5 m3	32.3 m3	42.9 m3
6hr	360min	6.00hr	17.2 m3	17.8 m3	20.5 m3	23.2 m3	25.8 m3	32.7 m3	39.7 m3	48.5 m3	64.4 m3
10hr	600min	10.00hr	28.6 m3	29.6 m3	34.1 m3	38.6 m3	43.1 m3	54.5 m3	66.2 m3	80.8 m3	107.3 m3
24hr	1440min	24.00hr	68.6 m3	71.1 m3	81.8 m3	92.6 m3	103.4 m3	130.8 m3	158.8 m3	193.8 m3	257.6 m3
48hr	2880min	48.00hr	137.3 m3	142.1 m3	163.7 m3	185.2 m3	206.7 m3	261.7 m3	317.6 m3	387.6 m3	515.2 m3

			ATTENUATION STORAGE REQUIRED TO MEET PROPOSED DISCHARGE RATE								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	12.7 m3	16.2 m3	18.3 m3	19.9 m3	20.9 m3	24.3 m3	27.8 m3	29.0 m3	36.4 m3
10min	10min	0.17hr	17.9 m3	23.3 m3	26.6 m3	28.6 m3	30.3 m3	35.9 m3	41.4 m3	43.6 m3	55.8 m3
15min	15min	0.25hr	21.0 m3	27.4 m3	31.2 m3	33.6 m3	35.6 m3	42.1 m3	48.6 m3	51.1 m3	65.4 m3
30min	30min	0.50hr	24.1 m3	31.8 m3	35.3 m3	38.0 m3	40.2 m3	48.3 m3	55.9 m3	58.7 m3	76.5 m3
1hr	60min	1.00hr	32.2 m3	41.4 m3	45.9 m3	49.3 m3	52.2 m3	62.5 m3	72.9 m3	76.5 m3	100.6 m3
2hr	120min	2.00hr	36.4 m3	47.4 m3	52.4 m3	56.1 m3	59.2 m3	70.7 m3	82.2 m3	85.4 m3	112.1 m3
4hr	240min	4.00hr	39.2 m3	51.1 m3	56.2 m3	59.0 m3	61.8 m3	73.4 m3	84.1 m3	85.4 m3	111.3 m3
6hr	360min	6.00hr	42.5 m3	55.0 m3	59.4 m3	61.9 m3	64.5 m3	74.3 m3	84.9 m3	84.3 m3	108.4 m3
10hr	600min	10.00hr	34.8 m3	47.7 m3	50.7 m3	51.8 m3	52.9 m3	59.2 m3	66.2 m3	60.3 m3	76.3 m3
24hr	1440min	24.00hr	15.8 m3	30.3 m3	29.1 m3	24.4 m3	19.7 m3	12.7 m3	7.6 m3	-16.9 m3	-29.7 m3
48hr	2880min	48.00hr	-38.6 m3	-25.6 m3	-36.2 m3	-50.9 m3	-66.9 m3	-101.3 m3	-134.0 m3	-193.0 m3	-267.1 m3

ATTENUATION STORAGE REQUIRED: 42.5 m3 55.0 m3 59.4 m3 61.9 m3 64.5 m3 74.3 m3 84.9 m3 85.4 m3 112.1 m3



SuDs CALCULATIONS	
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Client:	Godfrey London

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POST- DEVELOPMENT & SOURCE MITIGATION PEAK RUN-OFF + CC STORAGE

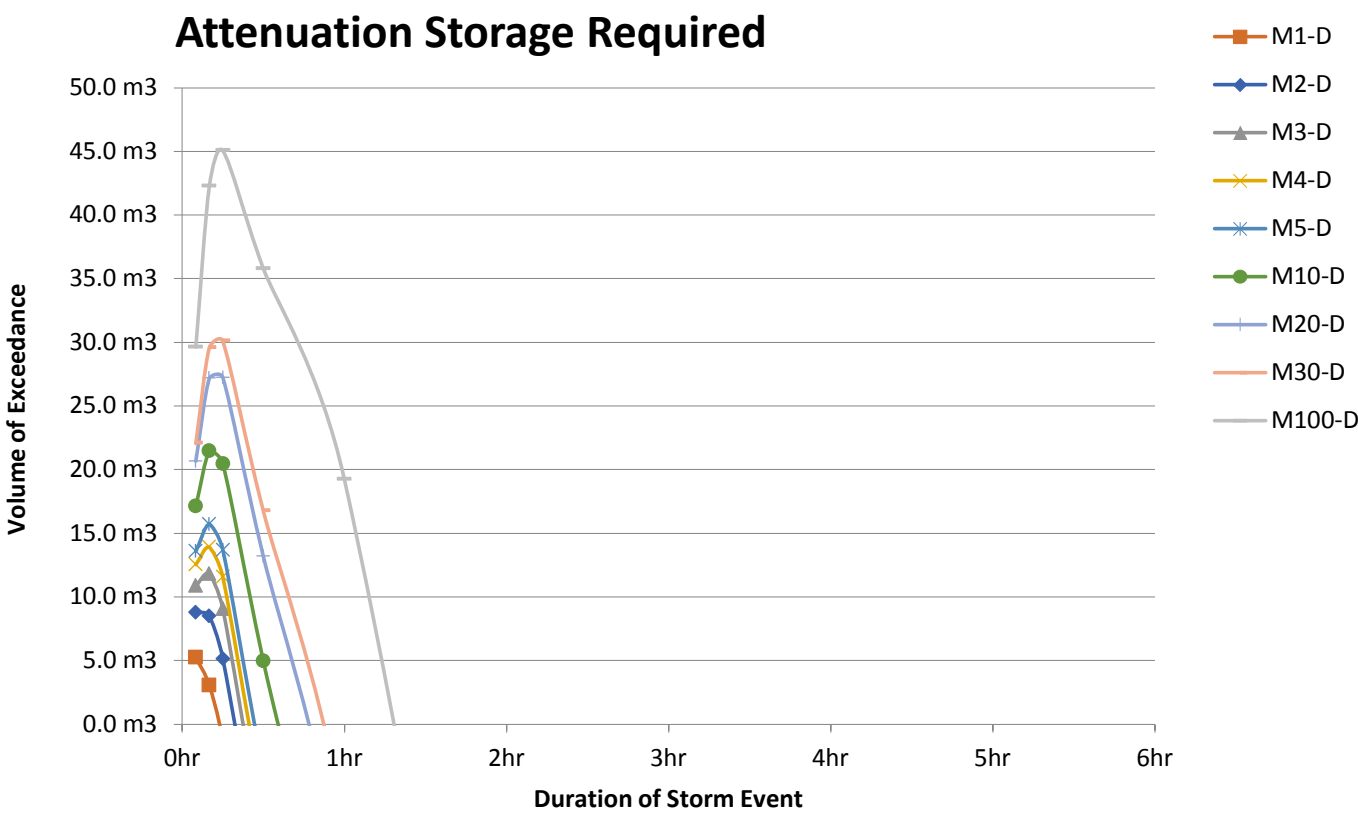
Proposed Discharge Rate: 25.57 l/sec 50% of existing (or greenfield where this is greater)
100 yr 15min
)

			INFLOW								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	12.9 m3	16.5 m3	18.5 m3	20.2 m3	21.3 m3	24.8 m3	28.3 m3	29.7 m3	37.3 m3
10min	10min	0.17hr	18.4 m3	23.8 m3	27.1 m3	29.2 m3	31.1 m3	36.8 m3	42.5 m3	44.9 m3	57.6 m3
15min	15min	0.25hr	21.7 m3	28.2 m3	32.1 m3	34.6 m3	36.7 m3	43.5 m3	50.2 m3	53.1 m3	68.1 m3
30min	30min	0.50hr	25.5 m3	33.3 m3	37.0 m3	39.9 m3	42.4 m3	51.0 m3	59.2 m3	62.8 m3	81.8 m3
1hr	60min	1.00hr	35.1 m3	44.4 m3	49.3 m3	53.2 m3	56.5 m3	68.0 m3	79.5 m3	84.6 m3	111.3 m3
2hr	120min	2.00hr	42.1 m3	53.3 m3	59.2 m3	63.8 m3	67.8 m3	81.6 m3	95.4 m3	101.5 m3	133.6 m3
4hr	240min	4.00hr	50.7 m3	62.9 m3	69.8 m3	74.5 m3	79.1 m3	95.2 m3	110.5 m3	117.7 m3	154.3 m3
6hr	360min	6.00hr	59.7 m3	72.8 m3	79.8 m3	85.1 m3	90.4 m3	107.0 m3	124.6 m3	132.8 m3	172.8 m3
10hr	600min	10.00hr	63.4 m3	77.4 m3	84.8 m3	90.4 m3	96.0 m3	113.7 m3	132.3 m3	141.0 m3	183.6 m3
24hr	1440min	24.00hr	84.4 m3	101.3 m3	111.0 m3	117.0 m3	123.0 m3	143.5 m3	166.5 m3	176.9 m3	228.0 m3
48hr	2880min	48.00hr	98.7 m3	116.5 m3	127.5 m3	134.3 m3	139.8 m3	160.4 m3	183.7 m3	194.6 m3	248.1 m3

			OUTFLOW								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	7.7 m3	7.7 m3	7.7 m3	7.7 m3	7.7 m3	7.7 m3	7.7 m3	7.7 m3	7.7 m3
10min	10min	0.17hr	15.3 m3	15.3 m3	15.3 m3	15.3 m3	15.3 m3	15.3 m3	15.3 m3	15.3 m3	15.3 m3
15min	15min	0.25hr	23.0 m3	23.0 m3	23.0 m3	23.0 m3	23.0 m3	23.0 m3	23.0 m3	23.0 m3	23.0 m3
30min	30min	0.50hr	46.0 m3	46.0 m3	46.0 m3	46.0 m3	46.0 m3	46.0 m3	46.0 m3	46.0 m3	46.0 m3
1hr	60min	1.00hr	92.1 m3	92.1 m3	92.1 m3	92.1 m3	92.1 m3	92.1 m3	92.1 m3	92.1 m3	92.1 m3
2hr	120min	2.00hr	184.1 m3	184.1 m3	184.1 m3	184.1 m3	184.1 m3	184.1 m3	184.1 m3	184.1 m3	184.1 m3
4hr	240min	4.00hr	368.3 m3	368.3 m3	368.3 m3	368.3 m3	368.3 m3	368.3 m3	368.3 m3	368.3 m3	368.3 m3
6hr	360min	6.00hr	552.4 m3	552.4 m3	552.4 m3	552.4 m3	552.4 m3	552.4 m3	552.4 m3	552.4 m3	552.4 m3
10hr	600min	10.00hr	920.7 m3	920.7 m3	920.7 m3	920.7 m3	920.7 m3	920.7 m3	920.7 m3	920.7 m3	920.7 m3
24hr	1440min	24.00hr	2209.6 m3	2209.6 m3	2209.6 m3	2209.6 m3	2209.6 m3	2209.6 m3	2209.6 m3	2209.6 m3	2209.6 m3
48hr	2880min	48.00hr	4419.3 m3	4419.3 m3	4419.3 m3	4419.3 m3	4419.3 m3	4419.3 m3	4419.3 m3	4419.3 m3	4419.3 m3

			ATTENUATION STORAGE REQUIRED TO MEET PROPOSED DISCHARGE RATE								
D Duration			M1-D	M2-D	M3-D	M4-D	M5-D	M10-D	M20-D	M30-D	M100-D
5min	5min	0.08hr	5.2 m3	8.8 m3	10.9 m3	12.5 m3	13.6 m3	17.1 m3	20.7 m3	22.1 m3	29.6 m3
10min	10min	0.17hr	3.0 m3	8.5 m3	11.8 m3	13.9 m3	15.7 m3	21.4 m3	27.2 m3	29.6 m3	42.2 m3
15min	15min	0.25hr	-1.3 m3	5.1 m3	9.1 m3	11.6 m3	13.7 m3	20.5 m3	27.2 m3	30.1 m3	45.0 m3
30min	30min	0.50hr	-20.5 m3	-12.7 m3	-9.0 m3	-6.1 m3	-3.7 m3	5.0 m3	13.2 m3	16.7 m3	35.8 m3
1hr	60min	1.00hr	-57.0 m3	-47.7 m3	-42.7 m3	-38.9 m3	-35.6 m3	-24.1 m3	-12.6 m3	-7.5 m3	19.2 m3
2hr	120min	2.00hr	-142.0 m3	-130.8 m3	-124.9 m3	-120.3 m3	-116.4 m3	-102.6 m3	-88.7 m3	-82.6 m3	-50.6 m3
4hr	240min	4.00hr	-317.6 m3	-305.3 m3	-298.4 m3	-293.8 m3	-289.2 m3	-273.1 m3	-257.7 m3	-250.6 m3	-214.0 m3
6hr	360min	6.00hr	-492.8 m3	-479.6 m3	-472.6 m3	-467.3 m3	-462.1 m3	-445.4 m3	-427.8 m3	-419.7 m3	-379.6 m3
10hr	600min	10.00hr	-857.3 m3	-843.3 m3	-835.9 m3	-830.3 m3	-824.7 m3	-807.0 m3	-788.3 m3	-779.6 m3	-737.1 m3
24hr	1440min	24.00hr	-2125.2 m3	-2108.3 m3	-2098.7 m3	-2092.7 m3	-2086.6 m3	-2066.1 m3	-2043.2 m3	-2032.7 m3	-1981.7 m3
48hr	2880min	48.00hr	-4320.6 m3	-4302.8 m3	-4291.8 m3	-4285.0 m3	-4279.5 m3	-4258.9 m3	-4235.6 m3	-4224.7 m3	-4171.2 m3

ATTENUATION STORAGE REQUIRED: 5.2 m3 8.8 m3 11.8 m3 13.9 m3 15.7 m3 21.4 m3 27.2 m3 30.1 m3 45.0 m3



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