

| Summary Of Claim Details |                           |  |  |  |  |  |
|--------------------------|---------------------------|--|--|--|--|--|
| Policy Holder            | Unknown                   |  |  |  |  |  |
| Risk Address             | Unknown                   |  |  |  |  |  |
| SI Date                  | 15/10/2019                |  |  |  |  |  |
| Issue Date               | 15/10/2019                |  |  |  |  |  |
| Report Date              | 31/10/2019                |  |  |  |  |  |
| Auger Reference          |                           |  |  |  |  |  |
| Insurance Company        | UK Insurance Partners     |  |  |  |  |  |
| LA Claim Reference       |                           |  |  |  |  |  |
| LA Co. Reference         | Sedgwick International UK |  |  |  |  |  |

This certificate is issued in accordance with the accreditation requirements of the United Kingdom Accreditation Service. The results reported herein relate only to the material supplied to the laboratory. This certificate shall not be reproduced except in full, without the prior written approval of the laboratory.

|  | Checked  | 31/10/2019 | Wayne Honey |  |
|--|----------|------------|-------------|--|
|  | Approved | 31/10/2019 | Paul Evans  |  |



|   | GSTL                 | LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX<br>( BS 1377 : Part 2 : 1990 Method 5 )<br>DESCRIPTIONS | @auger | environmental +<br>claims right +<br>subsidence +<br>drainage + |
|---|----------------------|--|--------|---|
| L | GSTL Contract Number |  |        |   |
|   | Risk Address         |  |        |   |
|   | Auger Reference      |  |        |   |
|   |                      |  |        |   |

| TH<br>Trial Hole | Sample<br>Type | Depth (m) | Sample Description                       |
|------------------|----------------|-----------|--|
| TH1              | D              | 1.80      | Brown fine to medium gravelly silty CLAY |
| TH1              | D              | 2.30      | Brown fine to medium gravelly sitty CLAY |
| TH1              | D              | 2.80      | Brown fine to medium gravelly silty CLAY |
| ,100             |                | 2.00      | Brown line to mediani gravery sirty CEAT |
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| Test Operator | Checked  | 31/10/2019 | Wayne Honey |  |
|---------------|----------|------------|-------------|--|
| Luke Williams | Approved | 31/10/2019 | Paul Evans  |  |



| GSTL                 | LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX<br>( BS 1377 : Part 2 : 1990 Method 5 ) | @auger | environmental +<br>claims mgmt +<br>subsidence +<br>drainage + |
|----------------------|--|--------|--|
| GSTL Contract Number |  |        |  |
| Risk Address         |  |        |  |
| Auger Reference      |  |        |  |
| Remarks              | NP - (Non-Plastic), # - (Liquid Limit and Plastic Limit Wet Sieved)                      |        |  |

| TH<br>Trial Hole | Sample<br>Type | Depth (m) | Moisture<br>Content % | Liquid<br>Limit | Plastic<br>Limit | Plasticity index | Passing<br>.425mm % | NHBC Chapter 4.2 | Remarks                 |
|------------------|----------------|-----------|-----------------------|-----------------|------------------|------------------|---------------------|------------------|-------------------------|
| TH1              | D              | 1.80      | 37                    | %<br>86         | %<br>24          | %<br>62          | 88                  | HIGH VCP         | CV Very High Plasticity |
| TH1              | D              | 2.30      | 37                    | 00              | 24               | 02               | 00                  | nigh vcr         | CV Very High Plasticity |
| TH1              | D              | 2.80      | 39                    | 85              | 28               | 57               | 93                  | HIGH VCP         | CV/Vens High Pleaticits |
| IHI              | D              | 2.80      | 39                    | 85              | 28               | 5/               | 93                  | HIGH VCP         | CV Very High Plasticity |
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: Non Classified

Modified Plasticity Index (PI) <10 Modified PI = 10 to <20 Modified PI = 20 to <40 Modified PI = 40 or greater

: Low volume change potential (LOW VCP)

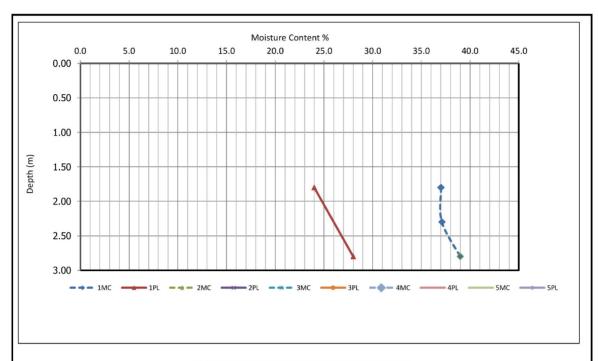
: Medium volume change potential (Med VCP)

: High volume change potential (HIGH VCP)

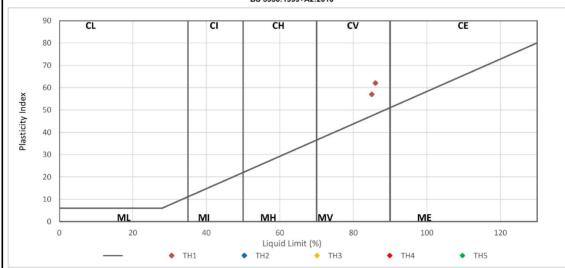
The Atterberg Limits May also be used to classify the volume change potential of fine soils using the National House building system, as given in the NHBC's Standards Chapter 4.2 (2003) "Building Near Trees"

| Test Operator | Checked  | 31/10/2019 | Wayne Honey |  |
|---------------|----------|------------|-------------|--|
| Luke Williams | Approved | 31/10/2019 | Paul Evans  |  |





## PLASTICITY CHART FOR CASAGRANDE CLASSIFICATION BS 5930:1999+A2:2010



Modified Plasticity Index (PI) <10 Modified PI = 10 to <20

: Non Classified

Modified PI = 20 to <40

: Low volume change potential (LOW VCP)
: Medium volume change potential (Med VCP)

Modified PI = 40 or greater

: High volume change potential (HIGH VCP)

The Atterberg Limits May also be used to classify The Atterberg Limits may also be used to classify the volume change potential of fine soils using the National House building system, as given in the NHBC's Standards Chapter 4.2 (2003) "Building Near Trees"

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| GSTL                 | SUMMARY OF SOIL CLASSIFICATION TESTS, BRE Information Paper IP 4/93 February 1993 (CI/SfB p1), BRE Information Paper Digest 412 ci/sFb (A3s) February 1996 | environmental claims mgmt subsidence drainage |
|----------------------|--|---|
| GSTL Contract Number |  |   |
| Risk Address         |  |   |
| Auger Reference      |  |   |
| Remarks              | D - Disturbed (Recompacted 2.5kg Rammer), U - Undisturbed Sample   |   |

| TH<br>Trial Hole | Depth<br>(m) | Filter Paper<br>Location | Filter<br>Paper | Sample<br>Prep<br>Method | Test<br>Duration<br>(Days) | Water<br>Content<br>(%) | Soil<br>Suction Pk<br>(kPa) | Average Soil Suction<br>Pk (kPa) | Cumalative Heave Potential (mm) from bottom of the hole |   |
|------------------|--------------|--------------------------|-----------------|--------------------------|----------------------------|-------------------------|-----------------------------|----------------------------------|---|---|
| TH1              | 1.80         | Тор                      | I               | D                        | 5                          | 63.5                    | 38                          |                                  |   |   |
| TH1              | 1.80         | Middle                   | II              | D                        | 5                          | 61.0                    | 42                          | 38.7                             | 0   |   |
| TH1              | 1.80         | Bottom                   | III             | D                        | 5                          | 64.6                    | 36                          |                                  |   |   |
| TH1              | 2.30         |                          |                 | Ĭ.                       |                            |                         |                             |                                  |   |   |
| TH1              | 2.30         |                          |                 |                          |                            |                         |                             |                                  |   |   |
| TH1              | 2.30         |                          |                 |                          |                            |                         |                             |                                  |   |   |
| TH1              | 2.80         | Тор                      | I               | D                        | 5                          | 36.0                    | 396                         |                                  |   |   |
| TH1              | 2.80         | Middle                   | II              | D                        | 5                          | 39.2                    | 253                         | 315                              | 315 7   | 7 |
| TH1              | 2.80         | Bottom                   | III             | D                        | 5                          | 38.1                    | 294                         |                                  |   |   |
|                  |              |                          |                 |                          |                            |                         |                             |                                  |   |   |
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Heave potential is calculated from the bottom of the hole and heaves above the bottom of the hole are reported as a cumalative value.

The values reported for heave above only apply to the strata the suction and plasticity have been performed on. The shallowest depth reported is assumed to be a strata thickness to GL and Heave is calculated based on that layer thickness, if the next sample is in 0.5m increments the heave is calculated based on the layer thickness of 0.5m and depths 1m from the sample above will include heave over 1m.

Consideration should be made for other stratas where values are not reported and when working out the heave potential over the entire trial hole.

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