

No. 8

OAKHILL AVENUE

LONDON

STRUCTURAL CALCULATIONS

Basement Design

## Design Loads

### • Roof

- Slates, timber battens & felt
- Timber rafters & insulation
- Ceiling & services
- Snow

DL	U
0.55	-
0.2	-
0.15	-
-	0.6
0.9	0.6

### • Typical floor

- boards / ply
- joists
- Ceiling & services
- Domestic

0.15	-
0.20	-
0.15	-
-	1.5
0.75	1.5

### • Flat roof (Green)

- Green extensive
- boards & ply
- joists
- Ceiling & services
- snow

1.78	
0.2	
0.2	
0.15	
-	0.6
2.33	0.6

## Design Loads

### • Ground floor slab over basement

- Assume 200 thick RC slab

- Assume 75 'screed

- Assume 25mm tiles

- Ceiling & services

- Domestic + partitions

DL	u
5	-
1.875	-
0.63	-
0.3	-
-	2.5
7.81	2.5

### • 350 THK WALL

- 350 wall

- Plaster

7	-
0.15	-
7.15	-

### • 230 THK WALL

- 230 brick

- Plaster both sides

4.6	-
0.3	-
4.9	-

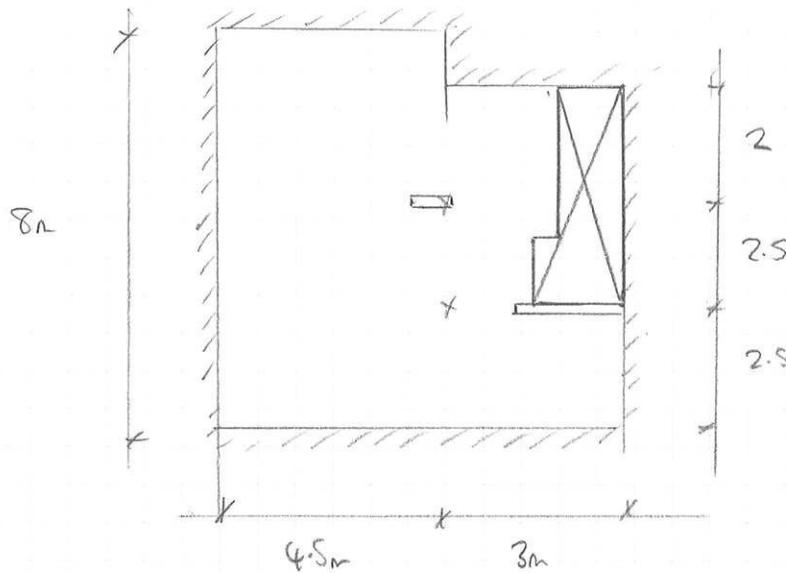
### • 100 THK WALL

- 100 brick

- Plaster both sides

2	-
0.3	-
2.3	-

Ground floor slab over basement



Design loads  $w_a = 7.81$   $w_u = 2.5$

Use 200 Rr Slab  
with A393 Mesh T&B

Refer to spreadsheet

Project: 8 Oakhill Avenue

Client: N/A

Location: Ground Floor Slab from grids 1 to 2

FLAT SLAB ANALYSIS &amp; DESIGN to BS 8110:1997

Originated from RCC33.xls v2.2 on CD

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## REINFORCED CONCRETE COUNCIL

Made by	Date	Page
AS	28-Jan-20	06
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-	-	28373

## MATERIALS

fcu	32	N/mm <sup>2</sup>	h agg	20	mm
fyl	460	N/mm <sup>2</sup>	ys	105	steel
fyv	460	N/mm <sup>2</sup>	yc	150	concrete

## COVERS

	mm	TO LAYER
Top cover	25	1
Btm cover	25	1

## SPANS

	L (m)
SPAN 1	4.500
SPAN 2	3.000
SPAN 3	
SPAN 4	
SPAN 5	
SPAN 6	

## GEOMETRY

Bay type	EDGE
Slab depth, h	200 mm
Edge Panel width, b	1000 mm
Edge distance	300 mm to C/L
End distance	300 from supt 1
End distance	300 from supt 3

PERIMETER LOADS *characteristic*

kn/m outside supports 1 & 3  
kn/m along bay edge

## LOADING PATTERN

	min	max
DEAD	1.0	1.4
IMPOSED		1.6

## SUPPORTS

	ABOVE (m)	H (mm)	B (mm)	End Cond	BELOW (m)	H (mm)	B (mm)	End Cond
Support 1					1	200	800	E
Support 2					1	200	800	E
Support 3					1	200	800	E
Support 4								
Support 5								
Support 6								
Support 7								

## LOADING

UDLs (kN/m<sup>2</sup>) PLs (kN/m) Position (m)

	Dead Load	Imposed Load	Position from left	Loaded Length		Dead Load	Imposed Load	Position from left	Loaded Length
Span 1					Span 4				
UDL	7.81	2.50	~~~~~	~~~~~	UDL			~~~~~	~~~~~
PL 1				~~~~~	PL 1				~~~~~
PL 2				~~~~~	PL 2				~~~~~
Part UDL					Part UDL				
Span 2					Span 5				
UDL	7.81	2.50	~~~~~	~~~~~	UDL			~~~~~	~~~~~
PL 1				~~~~~	PL 1				~~~~~
PL 2				~~~~~	PL 2				~~~~~
Part UDL					Part UDL				
Span 3					Span 6				
UDL			~~~~~	~~~~~	UDL			~~~~~	~~~~~
PL 1				~~~~~	PL 1				~~~~~
PL 2				~~~~~	PL 2				~~~~~
Part UDL					Part UDL				

## LOADING DIAGRAM





Project 8 Oakhill Avenue  
 Client N/A  
 Location Ground Floor Slab, from grids 1 to 2  
 FLAT SLAB ANALYSIS & DESIGN to BS 8110:1997

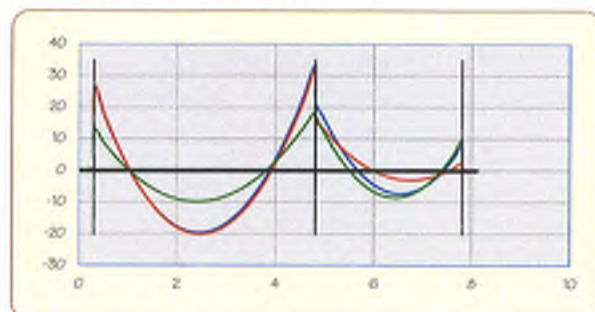
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REINFORCED CONCRETE  
COUNCIL

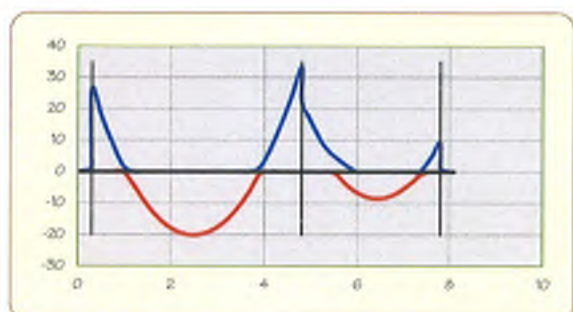
Made by AS	Date 28-Jan-20	Page 07
Checked -	Revision -	Job No 28373

#### BENDING MOMENT DIAGRAMS (kNm)



Elastic Moments

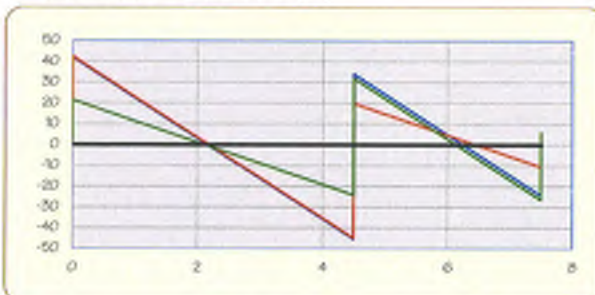
SUPPORT No	1	2	3				
Elastic M	26.2	33.3	9.4	~	~	~	~
Redistributed M	26.2	33.3	9.4	~	~	~	~
6b	1.000	1.000	1.000	~	~	~	~
Redistribution							
End support reinf. 8 mm	12		12				



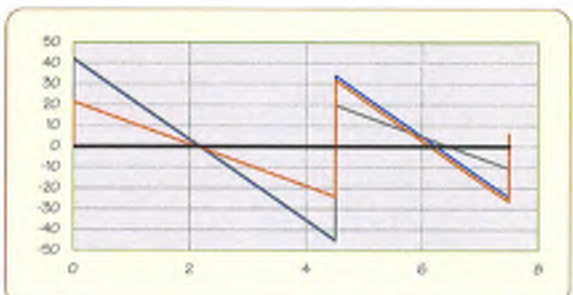
Redistributed Envelope

SPAN No	1	2				
Elastic M	20.1	8.5	~	~	~	~
Redistributed M	20.1	8.5	~	~	~	~
6b	1.000	1.000	~	~	~	~

#### SHEARS FORCE DIAGRAMS (kN)



Elastic Shears



Redistributed Shears

SPAN No	1	2				
Elastic V	42.4	45.4	34.0	26.4	~	~
Redistributed V	42.4	45.4	34.0	26.4	~	~

SPAN No						
Elastic V	~	~	~	~	~	~
Redistributed V	~	~	~	~	~	~

#### REACTIONS (kN)

SUPPORT	1	2	3
ALL SPANS LOADED	47.8	79.3	30.1
ODD SPANS LOADED	48.3	64.8	13.6
EVEN SPANS LOADED	24.6	56.0	32.2
V <sub>eff</sub> for punching	60.3	111.3	40.2
Characteristic Dead	25.0	41.5	15.7
Characteristic Imposed	8.3	13.3	6.3

#### COLUMN MOMENTS (kNm)

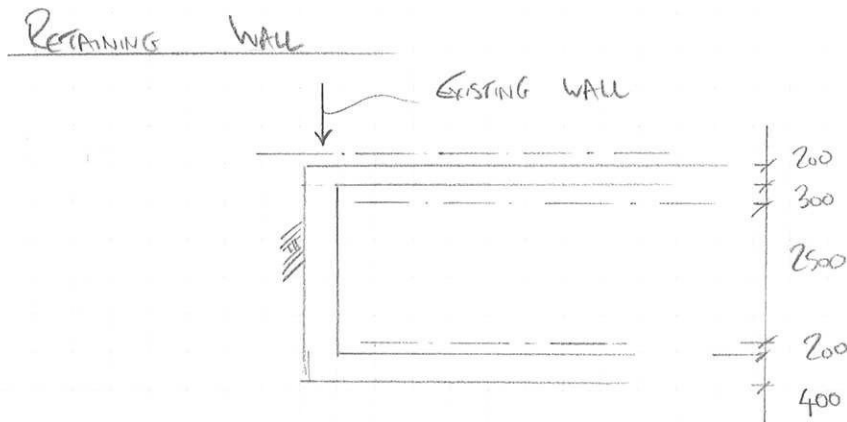
		1	2	3
ALL SPANS	Above			
LOADED	Below	24.9	-10.9	-7.0
ODD SPANS	Above			
LOADED	Below	25.8	-15.4	-1.7
EVEN SPANS	Above			
LOADED	Below	12.1	-1.2	-8.9

Project	8 Oakhill Avenue	 <b>REINFORCED CONCRETE COUNCIL</b>	<b>REINFORCED CONCRETE COUNCIL</b>		
Client	N/A		Made by	AS	Date
Location	Ground Floor Slab, from grids 1 to 2		Checked	-	Revision
FLAT SLAB ANALYSIS & DESIGN to BS 8110:1997					Page
Originated from RCCS.xls v2.2 on CD © 1998-2005 BCA for RCC					08
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SPAN 1			LEFT	CENTRE	RIGHT
ACTIONS	ℓ <sub>b</sub>		1,000	1,000	1,000
	ℓ <sub>e</sub>		900		800
	Total M	kNm	22.1	20.1	28.9
	Mt. max	kNm	123.4		109.7
MIDDLE STRIP	Width	mm	500	500	500
	M	kNm	0.3	9.1	7.2
	d	mm	169.0	169.0	169.0
	A <sub>s</sub>	mm <sup>2</sup> /m	10	258	205
	A <sub>s</sub> deflection	mm <sup>2</sup> /m		258	205
	A <sub>s</sub> prov	mm <sup>2</sup> /m	Provide T12 @ 400 T1	Provide T12 @ 400 B1	Provide T12 @ 400 T1
	Top steel		283	283	283
	Deflection			Provide T12 @ 400 T1	
			L/d = 4,500 / 169.0 = 26.627 < 26.0 x 1.622 x 1.053 x 0.9 = 39.968		
					OK
COLUMN STRIP	Width	mm	800	800	800
	M	kNm	22.1	11.1	21.6
	d	mm	169.0	169.0	169.0
	A <sub>s</sub>	mm <sup>2</sup> /m	383	197	385
	A <sub>s</sub> deflection	mm <sup>2</sup> /m		197	385
	A <sub>s</sub> prov	mm <sup>2</sup> /m	Provide T12 @ 275 T1	Provide T12 @ 400 B1	Provide T12 @ 200:400 T1
	Top steel		411	283	424
	Deflection			Provide T12 @ 400 T1	
			L/d = 4,500 / 169.0 = 26.627 < 26.0 x 2.000 x 1.053 x 0.9 = 49.272		
					OK
CHECKS	% A <sub>s</sub>		ok	ok	ok
	Singly reinforced		ok	ok	ok
	max S		ok	ok	ok

SPAN 2			LEFT	CENTRE	RIGHT
ACTIONS	ℓ <sub>b</sub>		1,000	1,000	1,000
	ℓ <sub>e</sub>		800		900
	Total M	kNm	28.9	8.5	6.8
	Mt. max	kNm	109.7		123.4
MIDDLE STRIP	Width	mm	500	500	500
	M	kNm	7.2	3.8	0.3
	d	mm	169.0	169.0	169.0
	A <sub>s</sub>	mm <sup>2</sup> /m	205	109	10
	A <sub>s</sub> deflection	mm <sup>2</sup> /m	205	109	
	A <sub>s</sub> prov	mm <sup>2</sup> /m	Provide T12 @ 400 T1	Provide T12 @ 400 B1	Provide T12 @ 400 T1
	Top steel		283	283	283
	Deflection			Provide T12 @ 400 T1	
			L/d = 3,000 / 169.0 = 17.751 < 26.0 x 2.000 x 1.053 x 0.9 = 49.272		
					OK
COLUMN STRIP	Width	mm	800	800	800
	M	kNm	21.6	4.7	6.8
	d	mm	169.0	169.0	169.0
	A <sub>s</sub>	mm <sup>2</sup> /m	385	83	122
	A <sub>s</sub> deflection	mm <sup>2</sup> /m	385	83	
	A <sub>s</sub> prov	mm <sup>2</sup> /m	Provide T12 @ 200:400 T1	Provide T12 @ 400 B1	Provide T12 @ 425 T1
	Top steel		424	283	266
	Deflection			Provide T12 @ 400 T1	
			L/d = 3,000 / 169.0 = 17.751 < 26.0 x 2.000 x 1.053 x 0.9 = 49.272		
					OK
CHECKS	% A <sub>s</sub>		ok	ok	ok
	Singly reinforced		ok	ok	ok
	max S		ok	ok	ok





Height = 3300mm

Design loads

- Ground floor slab  $w_{dl} = 7.81 \text{ kN/m}^2, w_{ul} = 2.5 \text{ kN/m}^2$

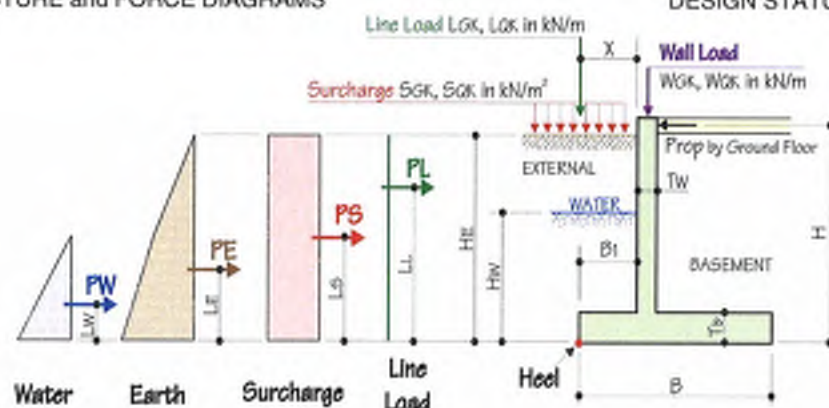
EXISTING BUILDING

element	width (m) / height	dl ( $\text{kN/m}^2$ )	u	DL ( $\text{kN/m}$ )	U
Roof	3.7	0.9	0.6	3.33	2.22
Second	$3.92/2 = 1.96$	0.75	1.5	1.5	2.95
First	"	"	"	1.5	2.95
Ground	ln normal (assumed ground bearing) slab	3.75	1.5	3.75	1.5
Wall	$6 + \text{ln bgl} = 7$	7.15	-	50	-
				60.1	9.62

Project	Oakhill Avenue		REINFORCED CONCRETE COUNCIL		
Client			Made by	Date	Page
Location	Basement Retaining Wall		AS	28-Jan-2020	10
Basement wall design to BS5100:1997, BS5002:1994, BS 8004:1986 etc.		Checked	Revision	Job No	
Originated from 'RCCB1 Basement Wall.xls' v2.1 © 1999-20002 BCA for RCC			-	28373	

# IDEALISED STRUCTURE and FORCE DIAGRAMS

DESIGN STATUS: **VALID**



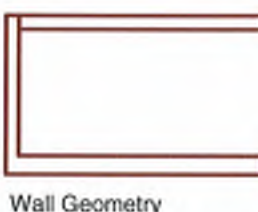
## DIMENSION (mm)

H =	3300	B =	5000	Tw =	250
Hw =	2300	B1 =	0	Tb =	400
He =	3300				

## MATERIAL PROPERTIES

$f_{cu}$ =	35	N/mm <sup>2</sup>	$\gamma_m$ =	1.50	concrete
$f_y$ =	460	N/mm <sup>2</sup>	$\gamma_m$ =	1.05	steel
Cover to tension reinforcement ( $c_o$ ) =	75	mm			
Max. allowable design surface crack width ( $W$ ) =	0.2	mm			
Concrete density =	24.0	kN/m <sup>3</sup>			

(0.2 or 0.3 mm only)



Wall Geometry

## SOIL PROPERTIES

Design angle of int'l friction of retained mat'l ( $\phi$ ) =	25	degree	
Design cohesion of retained mat'l ( $c$ ) =	0	kN/m <sup>2</sup>	(Only granular backfill considered, ie "C" = 0)
Density of retained mat'l ( $q$ ) =	19	kN/m <sup>3</sup>	
Submerged Density of retained mat'l ( $q_s$ ) =	12.67	kN/m <sup>3</sup>	(default = 2/3 of $q$ ), only apply when $H_w > 0$
Design angle of int'l friction of base mat'l ( $\phi_b$ ) =	25	degree	
Design cohesion of base mat'l ( $c_b$ ) =	0	kN/m <sup>2</sup>	
Density of base mat'l ( $q_b$ ) =	19	kN/m <sup>3</sup>	
Allowable gross ground bearing pressure (GBP) =	125	kN/m <sup>2</sup>	

## LOADINGS (unfactored)

Surcharge load -- live (SQK) =	10	kN/m <sup>2</sup>	
Surcharge load -- dead (SGK) =	0	kN/m <sup>2</sup>	
Line load -- live (LQK) =	0	kN/m	
Line load -- dead (LGK) =	0	kN/m	
Distance of line load from wall ( $X$ ) =	0	mm	
Wall load -- live (WQK) =	60	kN/m	
Wall load -- Dead (WGK) =	10	kN/m	

## LATERAL FORCES

$K_o$ =	0.40	default $K_o = (1 - \sin \phi) =$	0.58
$K_{ac}$ =	1.26	$= 2K_o^{0.5}$	

Force (kN)	Lever arm (m)	$\gamma_r$	Ultimate Force (kN)
PE =	34.68	LE = 1.164	48.55
PS(GK) =	0.00	LS = 1.65	0.00
PS(QK) =	13.20	LS = 1.65	21.12
PL(GK) =	0.00	LL = 3.30	0.00
PL(QK) =	0.00	LL = 3.30	0.00
PW =	26.45	LW = 0.77	37.03
Total	74.33		106.70

Project	Oakhill Avenue		REINFORCED CONCRETE COUNCIL		
Client	0		Made by	Date	Page
Location	Basement Retaining Wall		AS	28-Jan-2020	11
Basement wall design to BS8110:1997, BS8002:1994, BS 8004:1994			Checked	Revision	Job No
Originated from 'RCCER Basement Walling' v2.1 © 1999-20002 BCA for RCC				-	28373

## EXTERNAL STABILITY

STABILITY CHECK : OK

### ANALYSIS - Assumptions & Notes

- 1) Wall idealised as a propped cantilever ( i.e. pinned at top and fixed at base )
- 2) Wall is braced.
- 3) Maximum slenderness of wall is limited to 15,  $L_e \leq 0.9 \cdot (H_e - T_b/2) / T_w < 15$
- 4) Maximum Ultimate axial load on wall is limited to 0.1fcu times the wall cross-sectional area
- 5) Design Span (Effective wall height) =  $H_e - (T_b/2)$
- 6) -ve moment is hogging ( i.e. tension at external face of wall )  
+ve moment is sagging ( i.e. tension at internal face of wall )
- 7) " Wall MT. " is maximum +ve moment on the wall.
- 8) Estimated lateral deflections are used for checking the  $P\Delta$  effect.

### UNFACTORED LOADS AND FORCES

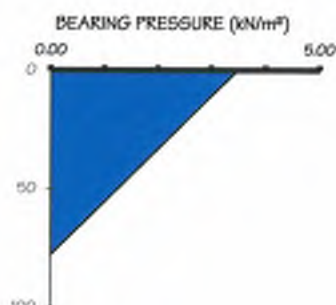
Lateral Force	Force (kN)	Lever arm to base (m)	Base MT. (kNm)	Wall MT. (kNm)	Reaction at Base (kN)	Reaction at Top (kN)	Estimated Elastic Deflection $\Delta$ (mm)
PE =	30.93	1.09	-12.90	6.50	24.18	6.75	0.3
PS(GK) =	0.00	1.55	0.00	#DIV/0!	0.00	0.00	0.0
PS(QK) =	12.40	1.55	-4.81	2.70	7.75	4.65	0.1
PL(GK) =	0.00	3.10	0.00	0.00	0.00	0.00	0.0
PL(QK) =	0.00	3.10	0.00	0.00	0.00	0.00	0.0
PW =	22.05	0.70	-8.66	3.15	19.86	2.19	0.1
Total	65.38		-26.36	#DIV/0!	51.80	13.59	0.5

### GROUND BEARING FAILURE

LOAD CASE: Wall Load MAX  
Surcharge MAX

Taking moments about centre of base (anticlockwise "+")

Vertical FORCES (kN)	Lever arm (m)	Moment (kNm)
Wall load = 70	2.37	166.2499993
Wall (sw) = 17.40	2.37	41.32
Base = 48.00	0.00	0.00
Earth = 0.00	2.50	0.00
Water = 0.00	2.50	0.00
Surcharge = 0.00	2.50	0.00
Line load = 0.00	2.50	0.00
<b><math>\Sigma V = 135.40</math></b>		<b><math>\Sigma M_v = 207.58</math></b>



MOMENT due to LATERAL FORCES,  $M_o = -26.36$  kNm

RESULTANT MOMENT,  $M = M_v + M_o = 181.21$  kNm

ECCENTRICITY FROM BASE CENTRE,  $M / V = 1.34$  m

MAXIMUM GROSS BEARING PRESSURE =  $77.71$  kN/m<sup>2</sup> < 125 OK

SLIDING AT BASE (using overall factor of safety instead of partial safety fact F.O.S. = 1.00

SUM of LATERAL FORCES,  $P = 51.80$  kN

BASE FRICTION,  $F_b = - (V \tan \phi + B \cdot c_b) = -63.14$  kN

Factor of Safety,  $F_b / P = 1.22 > 1.00$  OK



Project	Oakhill Avenue		REINFORCED CONCRETE COUNCIL					
Client	0		Made by	AS	Date	28-Jan-2020	Page	12
Location	Basement Retaining Wall		Checked	0	Revision	-	Job No	28373
Basement wall design to BS8110:1997, BS8002:1994, BS 8004:1986 Originated from "YCC61 Basement Wall.xls" v2.1 © 1999-20002 BCA for RCC								

#### OUTER BASE ( per metre length )

BS8110  
reference

$\gamma_r = 1.50$  (ASSUMED)  
 Ult. Shear = 34.27 kN (AT d from FACE of WALL)  
 Ult. MT. = 0.00 kNm TENSION - TOP FACE

BOTTOM REINFORCEMENT :  
 Min.  $A_s = 520$  mm<sup>2</sup>  
 $\phi = 16$  mm  
 centres = 150 mm < 725 OK  
 $A_s = 1340$  mm<sup>2</sup> > 520 OK

Table 3.25

MOMENT of RESISTANCE :  
 $d = 317$  mm  
 $Z = 298$  mm  
 $A_s' = 0$  mm<sup>2</sup>  
 $M_{res} = 175.12$  kNm > 0.00 OK

3.4.4.4

SHEAR RESISTANCE:  
 $100A_s/bd = 0.80\%$   
 $v_c = 0.56$  N/mm<sup>2</sup>  
 $V_{res} = 178.29$  kN > 34.27 OK

Table 3.8  
3.5.5.2

CHECK CRACK WIDTH IN ACCORDANCE WITH BS8100/80 Temp & shrinkage effects not included  
 $X = 94.72$  mm  
 $A_{cr} = 103.87$  mm<sup>2</sup>  
 $\epsilon_m = -0.0008$   
 $W = -0.20$  mm < 0.20 OK  
 NO CRACKING

BS8007  
App. B.2

#### INNER BASE ( per metre length )

Ult. Shear = -79.77 kN (AT d from FACE of WALL)  
 Ult. MT. = 39.54 kNm TENSION - BOTTOM FACE

BOTTOM REINFORCEMENT :  
 Min.  $A_s = 520$  mm<sup>2</sup>  
 $\phi = 16$  mm  
 centres = 150 mm < 725 OK  
 $A_s = 1340$  mm<sup>2</sup> > 520 OK

Table 3.25

MOMENT of RESISTANCE :  
 $d = 317$  mm  
 $Z = 298$  mm  
 $A_s' = 0$  mm<sup>2</sup>  
 $M_{res} = 175.12$  kNm > 39.54 OK

3.4.4.4

SHEAR RESISTANCE:  
 $100A_s/bd = 0.42\%$   
 $v_c = 0.56$  N/mm<sup>2</sup>  
 $V_{res} = 178.29$  kN > 79.77 OK

Table 3.8  
3.5.5.2

CHECK CRACK WIDTH IN ACCORDANCE WITH BS8100/80 Temp & shrinkage effects not included  
 $X = 94.72$  mm  
 $A_{cr} = 103.87$  mm<sup>2</sup>  
 $\epsilon_m = -0.0003$   
 $W = -0.08$  mm < 0.20 OK  
 NO CRACKING

BS8007  
App. B.2

#### REINFORCEMENT SUMMARY for BASE

	Type	$\phi$ mm	centres mm	$A_s$ mm <sup>2</sup>	Min. $A_s$ mm <sup>2</sup>	
TOP	T	16	150	1340	520	OK
BOTTOM	T	16	150	1340	520	OK
TRANSVERSE	T	16	150	1340	520	OK



Ground Floor - Central Column Adjacent to Basement  
Stairs

Element	Area	dl	ll	dl	ll
Roof	-				
Second	$5.5/2 \times 7/2$ = 9.63	0.75	1.5	7.22	14.5
First	9.63	"	"	7.22	14.5
Self weight steel work	$(5.5/2 + 7/2) \times 2$ + 6	1	-	12.3	-
				26.74	29

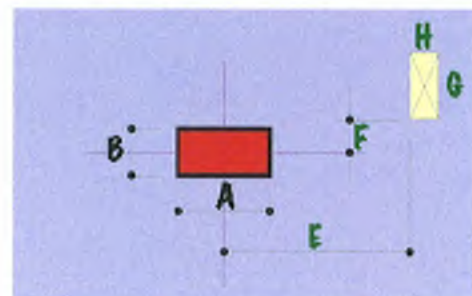
Project	Oakhill Avenue	 <b>REINFORCED CONCRETE COUNCIL</b> <b>INTERNAL COLUMN</b>	<b>PRICE &amp; MYERS</b>		
Client	-		Made by	Date	Page
Location	Basement Central Column		AS	28-Jan-2020	14
PUNCHING SHEAR to BS8110:1997			Checked	Revision	Job No
Originated from <b>ECCT5.xls</b> v2.2 on CD				-	28373
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**MATERIALS**

$f_{cu}$  N/mm<sup>2</sup> 40  
 $f_{yv}$  N/mm<sup>2</sup> 460  
link  $\phi$  mm 10

**STATUS**  
VALID DESIGN

Legend



**DIMENSIONS**

A mm 200  
B mm 800  
G mm 0

E mm 0  
F mm 0  
H mm 0

**LOADING**

$V_t$  kN 113  
ult UDL kN/m<sup>2</sup> 78.80

$V_{eff} =$  kN 113.0

**SLAB**

h mm 200  
dx mm 152.5  
dy mm 127.5  
ave d mm 140

$A_{sx}$  mm<sup>2</sup>/m 393  
 $A_{sy}$  mm<sup>2</sup>/m 393  
ave  $A_s$  % 0.283

**RESULTS**

$V_{eff} = 113.0$  kN  
At col. face,  $v$  max =  $0.359$  N/mm<sup>2</sup>

$v_c = 0.6309$  N/mm<sup>2</sup>  
At  $1.5d$  perimeter,  $v = 0.1036$  N/mm<sup>2</sup>  
At  $0d$  perimeter,  $v = 0.0308$  N/mm<sup>2</sup>

(Table 3.8)

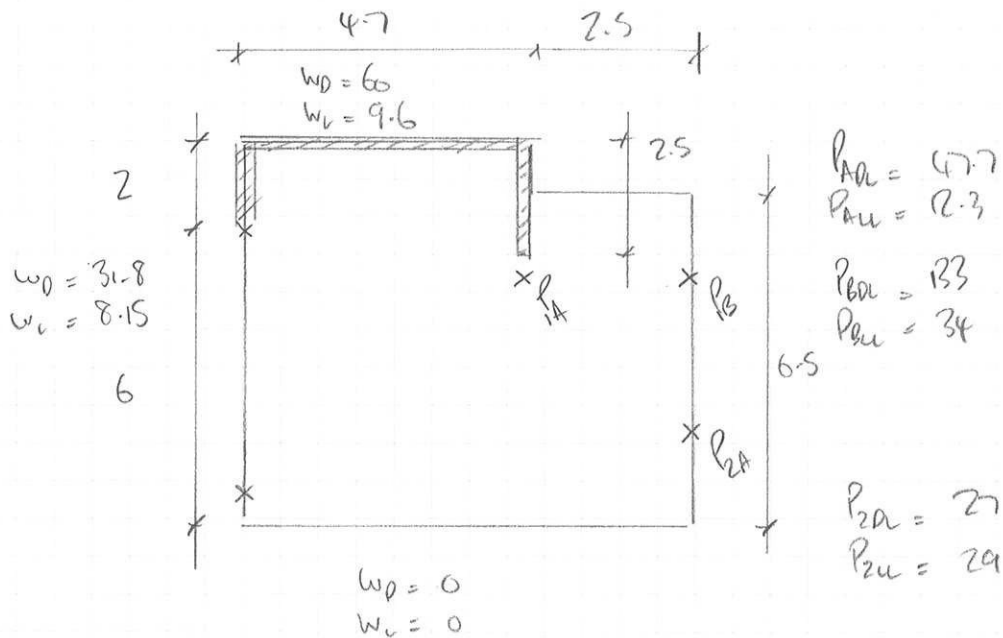
PROVIDE LINKS ☐ Links not required

Plan



# Basement Buoyancy

Basement excavation relative to external ground level = 3.3m



Superimposed loads on to basement not including basement & ground floor slab

$\sum DL$	$=$	$60 \times (4.7 + 2 + 2.5)$	$\sum UL$	$=$	$9.6 \times (4.7 + 2 + 2.5)$
		$31.8 \times (6)$			$8.15 \times (6)$
		47.7			12.3
		133			34
		27			29
		<hr/>			<hr/>
		950.5 kN			22.5 kN

Water uplift =  $3.3 - 1.0 = 2m \times 10 kN/m^3 = 20 kN/m^2$   
 $\times$  Basement Area =  $20 \times 53.9 = 1078 kN$

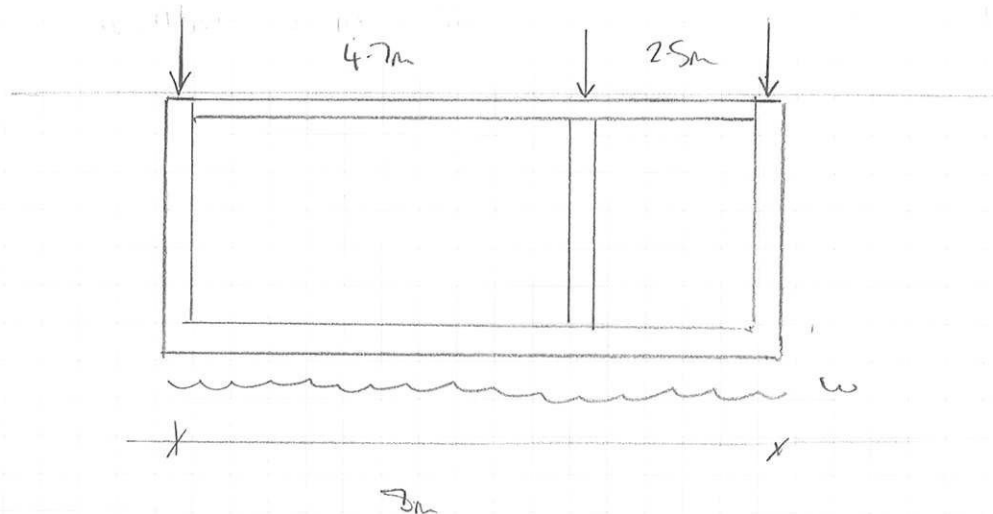
Resistance to uplift

Ground slab	$(4.7 \times 8) + (2.5 \times 6.5)$ $= 53.9 \text{ m}^2$	7.81	2.5	421	134.8
Basement slab	$53.9 \text{ m}^2$	12.81	2.5	421	134.8
Basement walls	$(4.7 + 2.5 + 1.5 + 6.5$ $+ 7.2 + 8) \times 3$ $= 91.2$	7.5	-	684	-
				1526	270

$$1078 \ll 1526 (+ 950.5) \quad \therefore \text{OKAY}$$



Basement Slab



$$\begin{aligned} \Sigma D &= 1526 + 950 \\ &= 2476 \end{aligned}$$

$$\begin{aligned} \Sigma U &= 270 + 212 \\ &= 482 \end{aligned}$$

$$w_{DL} = \frac{2476}{53.9} = 46 \text{ kN/m}^2$$

$$w_{UL} = \frac{482}{53.9} = 9 \text{ kN/m}^2$$

} Loads approximated as  
UDL spread across  
basement footprint

Check basement slab as flat slab, see spreadsheet over.

Use 400 THK

with #16's @ 200 c/c's

/ 100 GPa over column  
hogging locations

Project 8 Oakhill Avenue

Client N/A

Location Basement Floor Slab from grids 1 to 2

FLAT SLAB ANALYSIS &amp; DESIGN to BS 8110:1997

Originated from RCC33.xls v2.2 on CD

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## REINFORCED CONCRETE COUNCIL

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## MATERIALS

fcu	32	N/mm <sup>2</sup>	h agg	20	mm
fyl	460	N/mm <sup>2</sup>	γs	1.05	steel
fyv	460	N/mm <sup>2</sup>	γc	1.50	concrete

## COVERS

	mm	TO LAYER
Top cover	75	1
Btm cover	50	1

## SPANS

	L (m)
SPAN 1	4.700
SPAN 2	2.700
SPAN 3	
SPAN 4	
SPAN 5	
SPAN 6	

## GEOMETRY

Bay type	EDGE
Slab depth, h	400 mm
Edge Panel width, b	1000 mm
Edge distance	300 mm to C/L
End distance	300 from supt 1
End distance	300 from supt 3

PERIMETER LOADS *characteristic*

kN/m outside supports 1 & 3  
kN/m along bay edge

## LOADING PATTERN

	min	max
DEAD	1.0	1.4
IMPOSED		1.6

## SUPPORTS

	ABOVE (m)	H (mm)	B (mm)	End Cond	BELOW (m)	H (mm)	B (mm)	End Cond
Support 1					1	200	800	E
Support 2					1	200	800	E
Support 3					1	200	800	E
Support 4								
Support 5								
Support 6								
Support 7								

## LOADING

UDLs (kN/m<sup>2</sup>) PLs (kN/m) Position (m)

	Dead Load	Imposed Load	Position from left	Loaded Length		Dead Load	Imposed Load	Position from left	Loaded Length
Span 1					Span 4				
UDL	46.00	9.00	~~~~~	~~~~~	UDL			~~~~~	~~~~~
PL 1				~~~~~	PL 1				~~~~~
PL 2				~~~~~	PL 2				~~~~~
Part UDL					Part UDL				
Span 2					Span 5				
UDL	46.00	9.00	~~~~~	~~~~~	UDL			~~~~~	~~~~~
PL 1				~~~~~	PL 1				~~~~~
PL 2				~~~~~	PL 2				~~~~~
Part UDL					Part UDL				
Span 3					Span 6				
UDL			~~~~~	~~~~~	UDL			~~~~~	~~~~~
PL 1				~~~~~	PL 1				~~~~~
PL 2				~~~~~	PL 2				~~~~~
Part UDL					Part UDL				

## LOADING DIAGRAM





Project 8 Oakhill Avenue  
 Client N/A  
 Location Basement Floor Slab, from grids 1 to 2  
 FLAT SLAB ANALYSIS & DESIGN to BS 8110:1997

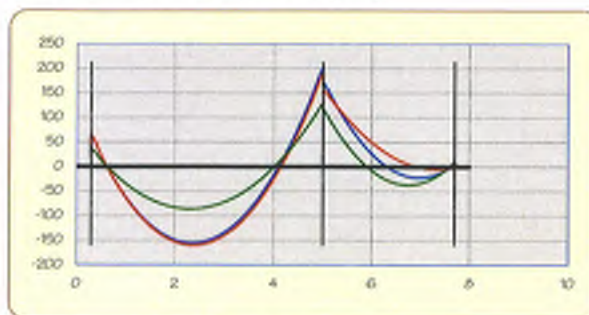


REINFORCED CONCRETE  
COUNCIL

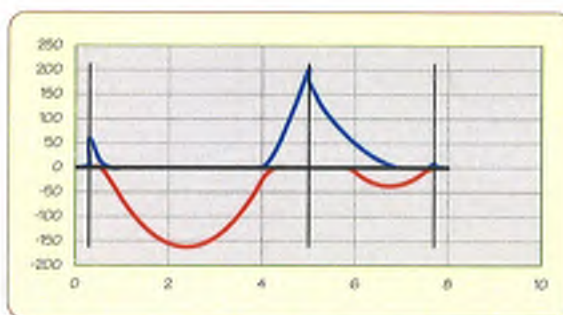
Made by AS	Date 28-Jan-20	Page 19
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#### BENDING MOMENT DIAGRAMS (kNm)



Elastic Moments



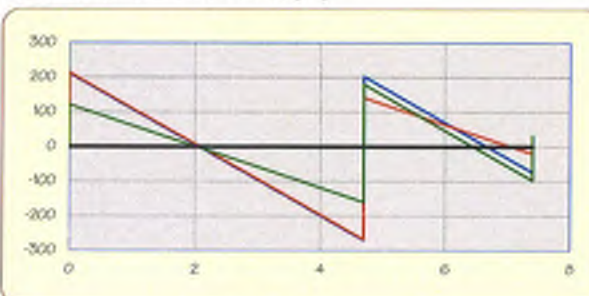
Redistributed Envelope

SUPPORT No	1	2	3				
Elastic M	62.8	201.9	9.3	~	~	~	~
Redistributed M	59.6	201.9	8.9	~	~	~	~
$\phi_b$	0.950	1.000	0.950	~	~	~	~
Redistribution	5.0%		5.0%				
End support reinf. $\phi$ mm	12		12				

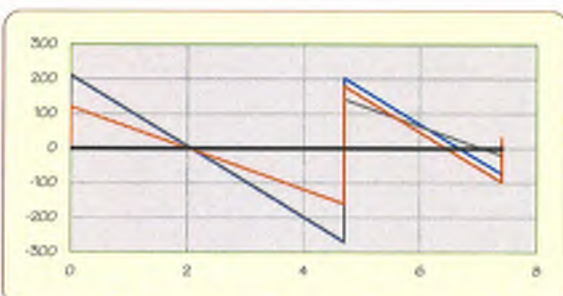
  

SPAN No	1	2				
Elastic M	159.8	36.8	~	~	~	~
Redistributed M	161.5	37.1	~	~	~	~
$\phi_b$	1.011	1.008	~	~	~	~

#### SHEARS FORCE DIAGRAMS (kN)



Elastic Shears



Redistributed Shears

SPAN No	1	2		
Elastic V	213.5	270.4	202.5	97.2
Redistributed V	212.9	271.0	202.5	97.0

SPAN No				
Elastic V	~	~	~	~
Redistributed V	~	~	~	~

#### REACTIONS (kN)

SUPPORT	1	2	3
ALL SPANS LOADED	241.2	473.5	104.9
ODD SPANS LOADED	243.6	409.9	38.1
EVEN SPANS LOADED	138.6	339.9	127.7
$V_{eff}$ for punching	304.5	613.5	159.7
Characteristic Dead	141.1	276.1	61.2
Characteristic Imposed	28.8	54.4	26.3

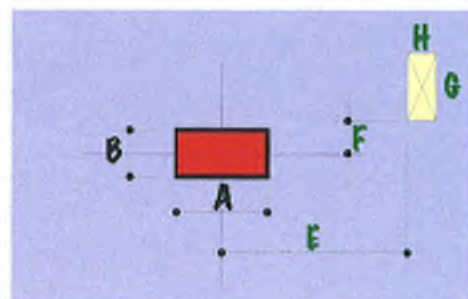
#### COLUMN MOMENTS (kNm)

		1	2	3
ALL SPANS	Above			
LOADED	Below	57.6	-24.0	0.0
ODD SPANS	Above			
LOADED	Below	60.1	-29.2	6.6
EVEN SPANS	Above			
LOADED	Below	31.2	-8.7	-6.6

Project	Oakhill Avenue	 <b>REINFORCED CONCRETE COUNCIL</b> <b>INTERNAL COLUMN</b>	<b>PRICE &amp; MYERS</b>		
Client	-		Made by	Date	Page
Location	Basement Central Column		AS	28-Jan-2020	20
PUNCHING SHEAR to B68110:1997			Checked	Revision	Job No
Originated from RCC3.xls v2.2 on CD				-	28373
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MATERIALS	$f_{cu}$	N/mm <sup>2</sup>	<u>40</u>	STATUS VALID DESIGN		
	$f_{yv}$	N/mm <sup>2</sup>	<u>460</u>			
	link Ø	mm	<u>10</u>			
DIMENSIONS	A	mm	<u>200</u>	E	mm	<u>0</u>
	B	mm	<u>800</u>	F	mm	<u>0</u>
	G	mm	<u>0</u>	H	mm	<u>0</u>

Legend



LOADING	$V_t$	kN	<u>700</u>	$V_{eff} =$	kN	<u>700.0</u>
	ult UDL	kN/m <sup>2</sup>	<u>78.80</u>			

SLAB	h	mm	<u>400</u>	dx	mm	<u>352.5</u>	$A_{sx}$	mm <sup>2</sup> /m	<u>1508</u>
				dy	mm	<u>327.5</u>	$A_{sy}$	mm <sup>2</sup> /m	<u>1508</u>
				ave d	mm	<u>340</u>	ave $A_s$	%	<u>0.444</u>

RESULTS	$V_{eff} =$	700.0	kN	$v_c =$	0.5874	N/mm <sup>2</sup>	(Table 3.8)
	At col. face, $v_{max} =$	1.011	N/mm <sup>2</sup>	At 1.5d perimeter, $v =$	0.2540	N/mm <sup>2</sup>	
				At 0d perimeter, $v =$	0.1385	N/mm <sup>2</sup>	

PROVIDE LINKS ☐

Links not required

Plan

