

## Asbestos Management Survey Report

18a Frognal Gardens  
Hampstead  
NW3 6XA



## Contents:

1. Executive Summary [Conclusions and actions]
2. Contract Review
3. Introduction - Purpose, Aims and Objectives
4. Desk Top Review and Survey Planning
5. Survey Method
6. Exclusions and Caveats
7. Sampling and Analysis
8. Survey Results - Interpretation
9. Recommendations

### **APPENDICES - Survey Results**

Appendix 1 - Asbestos Register - Results

Appendix 2 - Survey Data Sheets

Appendix 3 - Areas Surveyed

Appendix 4 - Analysis Certificates

Appendix 5 - Plans

# 1.0 Executive Summary:

Asbestos containing materials have been identified during the Asbestos Management Survey and the specific areas are shown below in order according to the initial Material Risk Assessment made by Artisan Surveyors Ltd.

Building	Floor	Room	Item	Material	Risk assessment Score	Recommendations
18a Frognal Gardens	Z-Sub Level 1	Boiler room Z107	Insulation board ceiling panels	Asbestos Insulating Board	MEDIUM (7)	B - Immediate Encapsulation
18a Frognal Gardens	External	Roof E01	Cement cowl	Asbestos Cement	LOW (5)	D - No Attention Required, Label
18a Frognal Gardens	External	Roof E01	Cement lid to metal tank	Asbestos Cement	LOW (5)	D - No Attention Required, Label

# 1.0 Executive Summary (Cont):

## AREAS OF NO ACCESS



Asbestos Containing Materials have been presumed as being present to the following areas where access could not be gained. A management policy and plan needs to identify that these areas require inspection once access can be provided. These areas require re-inspection for accessibility prior to further works

Building	Floor	Room/Area	Comments	Recommendation
18a Frogna Gardens	1st Floor	Bathroom 108	No intrusive access behind ceramic tiles and within ceramic tiled boxing behind toilet	E - Inspect Prior to Disturbance
18a Frogna Gardens	1st Floor	Bathroom 108	No intrusive access beneath bath without causing potential damage to bath panel	E - Inspect Prior to Disturbance
18a Frogna Gardens	1st Floor	En-suite shower room 107	No intrusive access behind ceramic tiles to boxing	E - Inspect Prior to Disturbance
18a Frogna Gardens	Ground Floor	Hallway cupboard G04	No intrusive access within timber vertical boxing	E - Inspect Prior to Disturbance
18a Frogna Gardens	Z-Sub Level 1	Boiler room Z107	No intrusive access within boiler	E - Inspect Prior to Disturbance
18a Frogna Gardens	Z-Sub Level 1	Garage Z106	No intrusive access within chipboard ceiling boxing	E - Inspect Prior to Disturbance
18a Frogna Gardens	Z-Sub Level 1	Lobby Z101	No intrusive access within boxing	E - Inspect Prior to Disturbance
18a Frogna Gardens	Z-Sub Level 1	Shower room Z104	No intrusive access behind hatch panel - fixed in place by boxing behind toilet	E - Inspect Prior to Disturbance

## EXTERNAL DESCRIPTION

The building consists of Modern roofing felt to roof and front porch areas, brick walls supported by concrete structure, metal window frames, timber soffit and fascia to entrance porch, plaster soffit above front door

## 2.0 Contract Review:

Name and address of site:	18a Frognal Gardens, Hampstead		
Name and address of client:	Progress UK, 18a Frognal Gardens, Hampstead		
Client contact:	Nathalie Bagnoud		
Type of survey:	Asbestos Management Survey (with MA only)		
Date of survey:	21 Mar 2019		
Report Revision Number:	1		
TEAMS internal job number:	J000215		
Lead surveyor[s]:	Jon Mackay	Signature:	
Technically reviewed by:	Jon Mackay	Signature:	
Report issue date:	27 Mar 2019		
Company name and address:	Artisan Surveyors Ltd F4 Fareham Heights, Standard Way, Fareham, Hampshire, PO16 8XT		
Company details:	Email: office@artisansurveyors.co.uk Tel: 023 8098 2598		

## 3.0 Introduction & Objectives:

Artisan Surveyors Ltd received an order of confirmation to undertake an Asbestos Management Survey from Progress UK. This order has been accepted on the basis of the original quotation and our terms and conditions of business.

The order relates to an Asbestos Management Survey of:

18a Frognal Gardens  
Hampstead  
NW3 6XA

The survey was carried out by Jon Mackay.

### **3.1 Purpose of Survey**

The purpose of this Management Survey is to help the duty holder manage asbestos in these premises. It provides sufficient information for an asbestos register to be generated in accordance with HSG 264 so that the duty holder can carry out a risk assessment and prepare a suitable management plan in accordance with regulation of the Control of Asbestos Regulations 2012 (CAR 2012).

### **3.2 Aim of Survey**

The aim of the survey was to;

1. Locate and record the location, extent, and product type as far as reasonably practicable of known or presumed ACM's.
2. Inspect and record information on the accessibility, condition and surface treatment of know or presumed ACM's
3. Determine and record the asbestos type based on sampling or by making a presumption based on product type and appearance

## 3.0 Introduction & Objectives (Cont):

### 3.3 Type of Survey – Management Survey

This management survey is required for the normal occupation and use of the building to ensure continued management of any ACM's in situ, and is the standard survey type.

Its purpose is to locate as far as is reasonably practicable, the presence and extent of any suspect ACM's in the building which could be damaged or disturbed during normal occupancy, including foreseeable maintenance and installation and to assess their condition.

All areas have been accessed as far as is reasonably practicable. Any areas that it was not possible to access have been presumed to contain asbestos and documented within this report. This survey involved sampling and analysis to confirm the presence or absence of asbestos containing materials, however presumptions may have also been used within this report to presume or strongly presume the presence of ACM's.

Management surveys will involve minor intrusive work and some disturbance. The extent of the intrusion will vary between premises and depend on what is reasonably practicable for individual properties eg type of building, nature of construction, etc.

The survey report can be used as a basis to start developing a management plan and prioritise actions, but in itself does not constitute a management plan as required under CAR 2012.

In order for the building occupier under regulation 4 of CAR 2012 they must implement a management policy and plan for confirmed or presumed asbestos containing materials.

This management survey includes a material assessment of the identified or presumed ACM's which relates to their condition and their potential to release fibres. This material assessment will provide the duty holder with an initial guide to the priority for managing ACM's as it will identify those ACM's which will most readily release fibres if they are disturbed.

## 4.0 Desk Top Review and Survey Planning:

Details of information requested from the Duty Holder by Artisan Surveyors Ltd in order to carry out a desk top review and plan the survey in accordance with HSG 264 were recorded on our pre-survey questionnaire, along with details of all the information that were provided by Nathalie Bagnoud on behalf of the client.

The Information provided was assessed during the desktop review and a survey plan, and risk assessment was produced for the survey of:

18a Frogna! Gardens  
Hampstead  
NW3 6XA

### SCOPE OF WORKS

The survey was carried out to A 3 storey residential property. A management asbestos survey was carried out to all accessible areas.

Where information was provided regarding the presence of known or presumed asbestos materials then this has been validated during the course of the survey, and recorded within this report.

Detailed drawing were provided by the client at the time of the survey.

A decontamination unit was not needed onsite during the survey.

Utilities and services were still live at the time of the survey.

Access equipment for working at heights was not required.

The survey did not involve confined space working.

The client did not inform Artisan Surveyors Ltd of any chemical/biological hazards.



## 5.0 Survey Method

**5.1** This survey has been undertaken in accordance with HSG264 and Artisan Surveyors Ltd in house procedures.

**5.2** Clients of Artisan Surveyors that have signed our terms and conditions are deemed to have agreed, and accepted, our surveying approach, our sampling strategy, and our standard planning, surveying and reporting format unless they have made specific requests to the contrary.

**5.3** The information provided by the client or their representative are recorded in the planning document and has been used to define the scope of the survey.

**5.4** Photographs of suspected ACM's will be taken at the time of the survey unless the client expressly requests otherwise. Sampling points and suspected ACM's will not be identified with labels unless the client expressly requests otherwise.

**5.5** All fibrous materials and item will be included in the survey unless, in the surveyors professional opinion, these items can be excluded (eg. Wood, wallpaper, man-made mineral fibre). Samples of all thermoplastic floor coverings will be taken unless, in the surveyors professional opinion, such items can be excluded. All textured coatings and novel bituminous will be sampled.

**5.6** Areas that could not be accessed were presumed to have ACM's present until proven otherwise. Each area requiring further inspection is documented within the Executive summary (Inaccessible areas). Inaccessible areas are also shown on the plan drawings (Appendix 5)

**5.7** Materials that could not be accessed and in the surveyors opinion can be dismissed will be presumed to be ACM unless proven otherwise. Materials that are not sampled but, in the surveyors opinion, have a similar appearance, location and function as a previously sampled material will be strongly presumed to be similar to the sampled material.

**5.8** The quantity of samples taken may have been minimised by using 'strongly presumed' as defined above. Materials that are 'strongly presumed' to be similar to a material that has already been sampled will be recorded in the comments section of the survey and referenced against the original sampled material.

**5.9** Our surveyor has made every attempt to avoid causing damage during the management surveys whilst attempting to identify possible ACM's. Minor repairs will be made and any areas accessed will be left in a safe condition.

**5.10** Intrusive damage that is required to gain access to an area/location that is within the scope of the survey has been agreed with the client or the clients representative. Any remedial action will be put in place before such action is attempted. If remedial action cannot be arranged, no attempt to access the area will be made and the reasons recorded. The area/location will be presumed to have ACM's present until proven otherwise.

**5.11** Non fibrous materials and item known not to contain asbestos (eg Breeze block, plaster, plasterboard plastics and non textured paints) will be excluded from the survey unless the surveyor suspects that these materials have been contaminated with asbestos from other sources or specifically requested by the client.

**5.12** Older electrical equipment, which cannot be shown to contain ACM's, has been presumed to have ACM's present unless, in the surveyors professional opinion, such items can be excluded.

## 6.0 Exclusions and Caveats:

**6.1** For safety reasons it is not possible to inspect internal areas of plant and machinery.

Where areas have been designated as 'no access' or 'restricted access', unless further inspection/sampling proves otherwise, the presumption has been made that these structures/areas contain asbestos materials.

During the course of the survey it may not have been possible to access all areas of the site. Details of areas requiring further access are identified within the Data Sheets of this report. In accordance with HSG 264, asbestos is presumed to be present within these areas and should be treated accordingly until further inspection and analysis of building fabric and services proves otherwise.

It is recommended that further intrusive inspection and sampling be carried out where site refurbishment, maintenance, or similar may disturb Asbestos Containing Materials that have remained inaccessible during this survey, this should be a refurbishment/demolition survey as described in HSG 264.

Textured Coatings such as "Artex" may contain a trace quantity of Chrysotile asbestos. Due to this low asbestos content, applications of this product may be non-homogenous and may elicit both positive and negative samples. Where both positive and negative samples are obtained the client should presume that the textured coating contains Chrysotile throughout even though a non-detected result has been obtained.

This report does not include investigations into land contamination associated with asbestos or any other contaminant.

### **6.2 Specific caveats**

It was agreed with the client that access above or behind known ACM's was not required within the survey.

Underground services were not included in the survey.

It has been agreed with Progress UK that there was not any unsafe structures on site.

## 7.0 Sampling and Analysis:

**7.1** The object of bulk sampling is to identify the nature and extent of any visible ACM.

**7.2** Bulk sampling is undertaken inline with the recognised safe procedures in order to cause minimal possible nuisance and potential risk to health of the building occupants and visitors. Bulk samples are taken in accordance with documented in house procedures, following guidelines detailed in HSG264 'The Survey Guide' and HSG248 'The Analyst Guide'. The quantity of samples taken will be minimised by using 'strongly presumed'. Materials that are 'strongly presumed' to be similar to a material that has already been sampled will be recorded in the comments section of the survey record and referenced against the original sampled material.

**7.3** Bulk samples are returned to the appointed bulk analysis laboratory with the appropriate sample / report reference number. Where appropriate; a label will be left on site adjacent to the sample location.

**7.4** The label will indicate the sample number and the date taken. This label can be used along with the report for cross reference purposes.

**7.5** Bulk sample analysis is carried out in accordance with HSE document HSG 248 'The Analysts Guide' by a UKAS accredited laboratory. Samples are examined under a low magnification stereomicroscope and the fibres teased apart. The fibres are then mounted in liquids of known refractive indices and examined under high magnification using polarised light and dispersion staining in accordance with HSG 248 'The Analysts Guide'.

**7.6** The bulk sample description and analysis results can be found in Appendix 4 of this report – The analysis certificate.

### Key to Analysis Results:

Chrysotile - White Asbestos

Amosite - Brown Asbestos

Crocidolite - Blue Asbestos

Tremolite - Rare Asbestos

Actinolite - Rare Asbestos

Anthophyllite - Rare Asbestos

## 8.0 Survey Results - Interpretation:

### Survey Results

**8.1** The results of the survey inspections and sampling undertaken are recorded on the enclosed Survey Data Sheets (appendix 2), Asbestos Register (appendix 1) and Room Register (appendix 3). Where asbestos containing material have been identified or presumed to be present then a Material Assessment Algorithm has been calculated as detailed in HSG 264 and reproduced in the table below:

**8.2** Within the survey data sheets the individual scores in brackets, for each sample variable, are added together to form the final material/priority risk assessment algorithm score.

## 8.0 Survey Results - Interpretation (Cont):

### Material Risk Assessment Algorithm

#### Product type [or debris from product]

Score	Examples of scores
1	Asbestos reinforced composites [plastics, resins, mastics, roofing felts, vinyl floor tiles, semi- rigid paint, decorative finishes and asbestos cement etc]
2	Asbestos insulating board, mill boards, other low-density boards, textiles, gaskets, ropes and woven materials and asbestos paper.
3	Thermal insulation [e.g. pipe and boiler lagging], sprayed asbestos, loose asbestos, asbestos mattresses and packing.

#### Extent of damage/deterioration

Score	Examples of scores
0	Good condition: no visible damage
1	Low damage: a few scratches or surface marks, broken edges on boards or tiles, etc.
2	Moderate damage: significant breakage of materials or several small areas where material has been damaged exposing fibrous edges.
3	High damage or deterioration of materials, sprays and thermal insulation. Visible asbestos contamination by debris or residues.

#### Surface treatment

Score	Examples of scores
0	Composite materials containing asbestos, reinforced plastics, resins, vinyl tiles
1	Enclosed sprays or insulation, AIB [with exposed face encapsulated], cement sheets, etc.
2	Unsealed AIB, encapsulated insulation and sprays.
3	Unsealed insulation and sprays.

#### Asbestos Type

Score	Examples of scores
1	Chrysotile
2	Amphibole asbestos (excluding Crocidolite)
3	Crocidolite

## Material Risk Assessment Score

Risk Category	Risk	Score Range	Fibre release potential
A	HIGH	Material Score 10 and above or Priority Score of 18-24	High risk with a high potential to release fibres if disturbed
B	MEDIUM	Material Score Between 7 and 9 or Priority Score of 12-17	Medium risk with a medium potential to release fibres if disturbed
C	LOW	Material Score Between 5 and 6 or Priority score of 9-11	Low risk with and having low potential to release fibres if disturbed
D	VERY LOW	Material Score 4 and below or Priority Score of less than 8	Very low risk with and having very low potential to release fibres if disturbed

## 9.0 Recommendations:

**9.1** To comply with and ensure that the requirements of section 2 & 3 of the Health and Safety at Work Act (as amended) 1974, the Management of Health and Safety at Work Regulations 1999, the Control of Asbestos Regulations 2012 and the Control of Substances Hazardous to Health 2002 are met, the following recommendations should be implemented:

**9.2** Undertake suitable and sufficient Risk Assessments of identified asbestos containing materials against normal occupation and maintenance operations, in compliance with Regulations 3 of the Management of Health & Safety at Work Regulations 1999 and Regulation 6 of the Control of Asbestos Regulations 2012.

**9.3** The findings of the survey be brought to the attention of those persons who are likely to come in contact with asbestos, in compliance with Section 2 and 3 of the Health and Safety at Work Act (as amended) 1974 and Regulation 10 of the Control of Asbestos Regulations 2012.

**9.4** Implement an Asbestos Management Policy, Plan and review process in compliance Regulation 4 of the Control of Asbestos Regulations 2012.

**9.5** Instigate regular inspections, to record and update details of retained asbestos containing materials.

**9.6** Review the arrangement under the management plan in accordance with regulation 4 of the CAR 2012.

**9.7** During the course of the survey it may not have been possible to access all areas of the site. Details of areas requiring further access are identified within the Data Sheets of this report. In accordance with HSG 264, asbestos has been presumed to be present within these areas and should be treated accordingly until further inspection and analysis of building fabric and services proves otherwise.

**9.8** Where asbestos debris or asbestos in poor condition has been found it is recommended that access is restricted and or controlled to these areas in accordance with Regulation 11 and Regulation 16 of the Control of Asbestos Regulations 2012.

**9.9** If we have identified asbestos materials in poor condition, it is recommended that air monitoring is carried out within a number of areas where asbestos materials have been identified in order to assess airborne fibre levels within adjacent occupied areas in relation to the clearance indicator, as documented by HSG 248 the Analyst Guide.

**9.10** All identified asbestos to be appropriately identified and subject to risk assessment, management, and re-inspection.

**9.11** Site specific recommendations in respect to the location and condition of asbestos materials identified during the course of this inspection are detailed in the Survey Data Sheets and Asbestos register. In considering the management of asbestos materials identified to date, these recommendations should be taken into consideration.

**9.12** In accordance with the Control of Asbestos Regulations 2012 the removal of ACM's fall into one of the three categories below:

### Licensed Asbestos Removal

Is defined as any work, which is undertaken on a friable asbestos product or which is likely to exceed the control limit of 0.1f/cm<sup>3</sup>. A licensed asbestos removal contractor must undertake this work and a 14-day notice must be given to the HSE prior to the commencement of the work.

### Notifiable Non Licensed Works

If work on an ACM causes the deterioration of the matrix material in which the asbestos fibres are firmly linked, then these works are Notifiable Non Licensed Work (NNLW). Work of this type does not require an asbestos removal licence, but the company undertaking the work must have the following:

- Notification of the work to the relevant enforcing authority prior to the work commencing.
- Medical examinations to assess each worker's state of health to be carried out, before any possible – exposure to asbestos. Then re-examinations every three years.
- Insurance for working with asbestos containing materials.
- A register of work to be kept by the employer for each employee exposed to asbestos.

### Non Notifiable Non Licensed work

-Non-Licensed Works Is defined as any work, which involves short, non-continuous maintenance activities, during which only nonfriable materials are removed. It can also involve the removal of non-friable materials for refurbishment purposes. However, work of this type is only applicable where the matrix material in which the asbestos fibres are firmly linked remains intact.

- If a non-licensed contractor is appointed to undertake the removal works on the above materials, the following points must be adhered to:
- All operatives undertaking work on the material must have asbestos awareness training and practical asbestos training.

**9.13** It is recommended that further intrusive investigations and sampling be carried out in accordance with HSG.264, where any major refurbishment, maintenance, installation or similar activity may expose asbestos materials that have remained inaccessible during the survey. This should be as a refurbishment/demolition survey as documented in HSG264.

**9.14** The findings of this report should not be solely relied upon in obtaining costs for proposed asbestos abatement work. Any proposed abatement/removal of the asbestos should be undertaken against a detailed specification.

# Appendix 1 - Asbestos Register



Building	Floor	Location /Room	S,P,SP,AS Sample No	Product Type	Condition	Surface Treatment	Asbestos Type	Quantity	Accessibility	Material Score	Recommendation	Additional Comments
18a Frogmal Gardens	Ground Floor	Hallway cupboard G04, Timber vertical boxing	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access within timber vertical boxing
18a Frogmal Gardens	1st Floor	En-suite shower room 107, Ceramic tiled boxing	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access behind ceramic tiles to boxing
18a Frogmal Gardens	1st Floor	Bathroom 108, Ceramic tiled boxing	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access behind ceramic tiles and within ceramic tiled boxing behind toilet
18a Frogmal Gardens	1st Floor	Bathroom 108, Beneath bath	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access beneath bath without causing potential damage to bath panel
18a Frogmal Gardens	Z-Sub Level 1	Lobby Z101, Timber boxings to ceiling	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access within boxing
18a Frogmal Gardens	Z-Sub Level 1	Shower room Z104, Wall void behind timber hatch	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access behind hatch panel - fixed in place by boxing behind toilet
18a Frogmal Gardens	Z-Sub Level 1	Garage Z106, Chipboard ceiling boxing adjoining boiler room	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access within chipboard ceiling boxing
18a Frogmal Gardens	Z-Sub Level 1	Boiler room Z107, Boiler unit	P Visual	N/A	N/A	N/A	N/A	N/A	N/A	N/A	E - Inspect Prior to Disturbance	No intrusive access within boiler
18a Frogmal Gardens	Z-Sub Level 1	Boiler room Z107, Insulation board ceiling panels to ceiling	S AA001021	Asbestos Insulating Board	Low Damage	Unsealed	Chrysotile + Amosite	5m <sup>2</sup>	Occasionally likely to be disturbed	7	B - Immediate Encapsulation	N/A
18a Frogmal Gardens	External	Roof E01, Cement cowl to top of vent pipe	S AA001024	Asbestos Cement	Low Damage	Surface Sealed	Chrysotile + Amosite	1no.	Occasionally likely to be disturbed	5	D - No Attention Required, Label	N/A

## KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample



# Appendix 1 - Asbestos Register (cont)



Building	Floor	Location /Room	S,P,SP,AS Sample No	Product Type	Condition	Surface Treatment	Asbestos Type	Quantity	Accessibility	Material Score	Recommendation	Additional Comments
18a Frogna Gardens	External	Roof E01, Cement lid to metal tank to top of vent pipe	SP As AA001024	Asbestos Cement	Low Damage	Surface Sealed	Chrysotile + Amosite	2m <sup>2</sup>	Occasionally likely to be disturbed	5	D - No Attention Required, Label	N/A


KEY:


S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

# Appendix 2 – Survey Data Sheets

<b>Service Type</b>	<b>Asbestos Management Survey</b>		
<b>Report Revision Number</b>	1	<b>Surveyors</b>	Jon Mackay
<b>TEAMS Job Number</b>	J000215	<b>Survey Date</b>	21 Mar 2019
<b>Site Address:</b>	18a Frognal Gardens Hampstead NW3 6XA	<b>Bulk Analysis Laboratory</b>	N/A
		<b>Sample Analysis Date</b>	26 Mar 2019

## Survey Data Sheets


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Ground Floor	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Hallway cupboard G04	Timber vertical boxing	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access within timber vertical boxing				

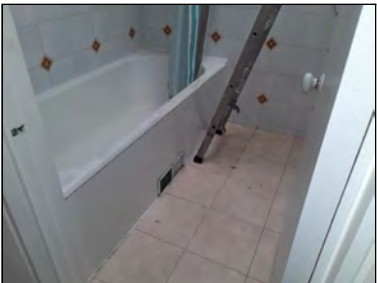
	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	1st Floor	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	En-suite shower room 107	Ceramic tiled boxing	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access behind ceramic tiles to boxing				

KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

## Survey Data Sheets (cont)


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	1st Floor	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Bathroom 108	Ceramic tiled boxing	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access behind ceramic tiles and within ceramic tiled boxing behind toilet				


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	1st Floor	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Bathroom 108	Beneath bath	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access beneath bath without causing potential damage to bath panel				

KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

## Survey Data Sheets (cont)


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	No Asbestos Detected
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Understairs cupboard Z102	Loose insulation to floor within void beneath stairs	2m <sup>2</sup>	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	AA001019 (S)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	No further action required				
<b>Surveyor comments</b>	N/A				


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	No Asbestos Detected
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Lobby Z101	Vinyl tile covering to floor	8m <sup>2</sup>	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	AA001020 (S)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	No further action required				
<b>Surveyor comments</b>	N/A				

KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

## Survey Data Sheets (cont)


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Lobby Z101	Timber boxings to ceiling	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access within boxing				


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	No Asbestos Detected
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Utility cupboard Z103	Vinyl tile covering to floor	1m <sup>2</sup>	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	As AA001020 (SP)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	No further action required				
<b>Surveyor comments</b>	N/A				

## KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

Survey Data Sheets (cont)


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a FrognaI Gardens	Shower room Z104	Wall void behind timber hatch	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access behind hatch panel - fixed in place by boxing behind toilet				


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a FrognaI Gardens	Garage Z106	Chipboard ceiling boxing adjoining boiler room	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access within chipboard ceiling boxing				

**KEY:**

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

## Survey Data Sheets (cont)

	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	N/A
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frognal Gardens	Boiler room Z107	Boiler unit	N/A	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	Visual (P)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	Inspection Required				
<b>Surveyor comments</b>	No intrusive access within boiler				


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	Chrysotile + Amosite (2)
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frognal Gardens	Boiler room Z107	Insulation board ceiling panels to ceiling	5m <sup>2</sup>	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	AA001021 (S)	Asbestos Insulating Board (2)	Unsealed (2)	Low Damage (1)	Occasionally likely to be disturbed
	<b>Material Risk Score</b>				
7					
<b>Recommended action</b>	B - Immediate Encapsulation				
<b>Surveyor comments</b>	N/A				


**KEY:**

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample



Survey Data Sheets (cont)


	Survey Date:	Lead Surveyor	Survey Type	Floor	Analysis
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	No Asbestos Detected
	Building	Room	Item	Quantity	
	18a Frogna! Gardens	Boiler room Z107	Bitumenous pads to brick where ducting enters wall void behind boiler	1m <sup>2</sup>	
	Sample No (S,SP,P,As)	Product Type	Surface Treatment	Condition	Accessibility
	AA001022 (S)	N/A	N/A	N/A	N/A
	Material Risk Score	N/A			
N/A					
Recommended action	No further action required				
Surveyor comments	N/A				


	Survey Date:	Lead Surveyor	Survey Type	Floor	Analysis
	21 Mar 2019	Jon Mackay	Management Survey	Z-Sub Level 1	No Asbestos Detected
	Building	Room	Item	Quantity	
	18a Frogna! Gardens	Shower room Z104	Vinyl tile floor covering to floor	4m <sup>2</sup>	
	Sample No (S,SP,P,As)	Product Type	Surface Treatment	Condition	Accessibility
	As AA001020 (SP)	N/A	N/A	N/A	N/A
	Material Risk Score	N/A			
N/A					
Recommended action	No further action required				
Surveyor comments	N/A				

KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

## Survey Data Sheets (cont)


	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	External	No Asbestos Detected
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Roof E01	Bitumen seal to skylight lid between timber upstand and skylight casing	3no.	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	AA001023 (S)	N/A	N/A	N/A	N/A
	<b>Material Risk Score</b>				
N/A					
<b>Recommended action</b>	No further action required				
<b>Surveyor comments</b>	N/A				

	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	External	Chrysotile + Amosite (2)
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Roof E01	Cement cowl to top of vent pipe	1no.	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	AA001024 (S)	Asbestos Cement (1)	Surface Sealed (1)	Low Damage (1)	Occasionally likely to be disturbed
	<b>Material Risk Score</b>				
5					
<b>Recommended action</b>	D - No Attention Required, Label				
<b>Surveyor comments</b>	N/A				

KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

## Survey Data Sheets (cont)

	<b>Survey Date:</b>	<b>Lead Surveyor</b>	<b>Survey Type</b>	<b>Floor</b>	<b>Analysis</b>
	21 Mar 2019	Jon Mackay	Management Survey	External	Chrysotile + Amosite (2)
	<b>Building</b>	<b>Room</b>	<b>Item</b>	<b>Quantity</b>	
	18a Frogna Gardens	Roof E01	Cement lid to metal tank to top of vent pipe	2m <sup>2</sup>	
	<b>Sample No (S,SP,P,As)</b>	<b>Product Type</b>	<b>Surface Treatment</b>	<b>Condition</b>	<b>Accessibility</b>
	As AA001024 (SP)	Asbestos Cement (1)	Surface Sealed (1)	Low Damage (1)	Occasionally likely to be disturbed
	<b>Material Risk Score</b>				
5					
<b>Recommended action</b>	D - No Attention Required, Label				
<b>Surveyor comments</b>	N/A				

KEY:

S – Sampled, P – Presumed, SP – Strongly Presumed, AS – Cross reference to former sample

# Appendix 3 - Room Register

Building	Floor	Room No:	Room Type	Item
18a Frogna Gardens	External	E01	Roof	Modern roofing felt to flat roof, felted timber housing to metal roof tank, PVC skylight lids
18a Frogna Gardens	External	E02	Garden shed	Timber floor, timber walls with paper lining, timber pitched roof, modern felt covers pitched roof
18a Frogna Gardens	External	E03	Crawl space beneath house	Concrete floor, brick walls, fibreboard ceiling panels, mmmf insulation to timber ceiling, mmmf insulated metal ducting, foam and hessian insulated pipework
18a Frogna Gardens	Z-Sub Level 1	Z101	Lobby	Concrete floor with modern vinyl tile covering, brick and plasterboard walls, plasterboard ceiling, plasterboard ceiling boxings
18a Frogna Gardens	Z-Sub Level 1	Z102	Understairs cupboard	N/A
18a Frogna Gardens	Z-Sub Level 1	Z103	Utility cupboard	Concrete floor, vinyl floor tiles, brick walls, timber and plasterboard wall partition adjoining stairs, plaster ceiling
18a Frogna Gardens	Z-Sub Level 1	Z104	Shower room	Concrete floor with vinyl tile covering, ceramic tiles to all walls, plasterboard ceiling, ceramic WC cistern, timber hatch panel adjacent wc
18a Frogna Gardens	Z-Sub Level 1	Z105	Bedroom 5	Concrete floor with carpet covering, plasterboard walls, plaster ceiling, built -in MDF wardrobes, modern electric wall heater, timber window sill
18a Frogna Gardens	Z-Sub Level 1	Z106	Garage	Painted concrete floor, brick walls, timber wall panelling adjoining bedroom 5, timber wall panelling adjoining shower room, plasterboard ceiling, chipboard boxing to ceiling
18a Frogna Gardens	Z-Sub Level 1	Z107	Boiler room	Concrete floor, brick walls, insulation board ceiling panels, exposed metal pipework, metal ducting, modern water heater

# Appendix 3 - Room Register (cont)

Building	Floor	Room No:	Room Type	Item
18a Frogna Gardens	Ground Floor	G01	Entrance lobby	Concrete floor with ceramic tile covering, timber staircase to raised ground floor, brick and plaster walls, plaster ceiling, timber inset to ceiling skylight, plaster surround to secondary glazed window frame.
18a Frogna Gardens	Ground Floor	G02	Wc	Wooden floor with wood laminate flooring, brick and plaster walls, plaster ceiling, timber window sill, ceramic WC cistern
18a Frogna Gardens	Ground Floor	G03	Hallway	Timber floor, brick and plaster walls, plaster ceiling, timber skirting
18a Frogna Gardens	Ground Floor	G04	Hallway cupboard	Timber floor, brick and plaster walls, plaster ceiling, timber vertical boxing, modern electrical box
18a Frogna Gardens	Ground Floor	G05	Kitchen	Timber floor with wood laminate floor covering, brick and plaster walls, ceramic tile wall coverings, plaster ceiling, laminated timber window sill,
18a Frogna Gardens	Ground Floor	G06	Dining area	Raised timber floor, brick and plaster walls, plaster ceiling, metal framed windows with plaster soffit.
18a Frogna Gardens	Ground Floor	G07	Lounge	Timber floor with carpet covering, brick and plaster walls, plaster ceiling, brick fire place with marble effect hearth and mantelpiece, metal window frames with plaster soffit, plasterboard boxing housing heating grills x2.
18a Frogna Gardens	Ground Floor	G08	Bedroom 1	Timber floor, brick and plaster walls, plaster ceiling, metal window frames with plaster reveals within secondary glazing, plaster boxing housing heating grill.
18a Frogna Gardens	1st Floor	101	Stairwell cupboard	Timber floor, brick and plaster walls, plaster ceiling, timber shelving
18a Frogna Gardens	1st Floor	102	Landing	Timber floor, carpet covering, brick and plaster walls, plasterboard wall panelling, plaster ceiling

# Appendix 3 - Room Register (cont)

Building	Floor	Room No:	Room Type	Item
18a Frogna Gardens	1st Floor	103	Cupboard	Timber floor with carpet covering, brick and plaster and plasterboard walls, plaster ceiling, timber shelving
18a Frogna Gardens	1st Floor	104	Airing cupboard	Timber floor with carpet covering, brick, plaster and plasterboard walls, plaster ceiling, low level metal ducting
18a Frogna Gardens	1st Floor	105	Bedroom 2	Timber floor with carpet covering, brick and plaster walls, plasterboard wall partition adjoining en-suite, plaster ceiling, metal window frames with plaster reveals within secondary glazing
18a Frogna Gardens	1st Floor	106	Bedroom 2 dressing room	Timber floor with carpet covering, brick and plaster walls, plaster ceiling, metal window frames with plaster reveals within secondary glazing
18a Frogna Gardens	1st Floor	107	En-suite shower room	Timber floor with tile effect laminate flooring, plaster walls with ceramic tile covering, plaster ceiling, ceramic WC cistern, ceramic tiled boxing, timber skylight surround
18a Frogna Gardens	1st Floor	108	Bathroom	Timber floor with tile effect laminate flooring, ceramic tile covering to all walls, plaster ceiling, ceramic tiled boxing, timber skylight surround
18a Frogna Gardens	1st Floor	109	Bedroom 3	Timber floor with carpet covering, brick and plaster walls, plasterboard wall partition adjoining bedroom 4, plaster ceiling, metal window frames with plaster reveals within secondary glazing
18a Frogna Gardens	1st Floor	110	Bedroom 4	Timber floor with carpet covering, brick and plaster walls, plasterboard wall partition adjoining hallway cupboard, fibreboard wall panelling adjoining bedroom 3, plaster ceiling, metal window frames with plaster reveals within secondary glazing

# Appendix 4 – Analysis Certificates



Our Ref: J164012 FI: 6  
Your Ref:  
Date: 26/03/2019

**ENVIROCHEM**  
**Analytical Laboratories Ltd.**  
12 The Gardens  
Broadcut, Fareham  
Hampshire  
PO16 8SS



Tel: (01329) 287777  
Fax: (01329) 287755  
www.envirochem.co.uk  
office@envirochem.co.uk

## Asbestos Fibre Identification Report

**Client:** Artisan Surveyors Ltd  
F4 Fareham Heights, Standard Way, Fareham, Hampshire, PO16 8XT

**Site Address:** 18a Frognaal Gardens Hampstead, NW3 6XA

**Sampled By:** Artisan Surveyors Ltd

**Date sampled/received:** 22nd March 2019

**Date analysed:** 26th March 2019

**Analyst/s:** Ewelina Kowalczyk Pariyar

**Analysis Location:** 12 The Gardens, Broadcut, Fareham, Hampshire, PO16 8SS

### ANALYTICAL PROCEDURE

Fibre identification was carried out in accordance with the documented 'in-house' methods based on the HSE Guidance Note HSG 248. These employed stereo microscopy, polarized microscopy and dispersion staining techniques.

### RESULTS

Sample No.	Sample Ref.	Location	Asbestos Detected	Asbestos Type
AA001019	BS543352	Z-Sub Level 1, Understairs cupboard, Loose insulation to floor	No	
AA001020	BS543353	Z-Sub Level 1, Lobby, Vinyl tile covering	No	
AA001021	BS543354	Z-Sub Level 1, Boiler room, Insulation board ceiling panels	Yes	Chrysotile Amosite
AA001022	BS543355	Z-Sub Level 1, Boiler room, Bitumenous pads to brick where ducting enters wall void	No	

NOTES:

1. Sample(s) were examined for the presence of 6 types of asbestos fibres: crocidolite (blue), amosite (brown), chrysotile (white), anthophyllite, actinolite and tremolite.
2. Samples collected by the client are evaluated using information provided by the client. For samples collected by the client the date of receipt is deemed to be the same as the date sampled.
3. Envirochem is a UKAS accredited laboratory for sampling and identification of asbestos containing materials.
4. Comments, observations and opinions are outside the scope of UKAS accreditation.
5. The analytical method in the HSG248 does not quantify the amount of asbestos present, therefore UKAS accreditation does not permit quantification.
6. If, during fibre identification, only 1 or 2 fibres are seen and identified as asbestos, then the term 'trace asbestos identified' is used.

SIGNATURE:

Authorised signatory

PRINT NAME: Frances Scott

Reg. No. 2378228 England. Registered Office: Envirochem, 12 The Gardens, Broadcut, Fareham, Hampshire, PO16 8SS.





Our Ref: J164012 FI: 6  
Your Ref:  
Date: 26/03/2019

**ENVIROCHEM**  
**Analytical Laboratories Ltd.**  
12 The Gardens  
Broadcut, Fareham  
Hampshire  
PO16 8SS



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office@envirochem.co.uk

## Asbestos Fibre Identification Report

**Client:** Artisan Surveyors Ltd  
F4 Fareham Heights, Standard Way, Fareham, Hampshire, PO16 8XT

**Site Address:** 18a Frognaal Gardens Hampstead, NW3 6XA

**Sampled By:** Artisan Surveyors Ltd

**Date sampled/received:** 22nd March 2019

**Date analysed:** 26th March 2019

**Analyst/s:** Ewelina Kowalczyk Pariyar

**Analysis Location:** 12 The Gardens, Broadcut, Fareham, Hampshire, PO16 8SS

### ANALYTICAL PROCEDURE

Fibre identification was carried out in accordance with the documented 'in-house' methods based on the HSE Guidance Note HSG 248. These employed stereo microscopy, polarized microscopy and dispersion staining techniques.

### RESULTS

Sample No.	Sample Ref.	Location	Asbestos Detected	Asbestos Type
AA001023	BS543356	External, Roof, Bitumen seal to skylight lid	No	
AA001024	BS543357	External, Roof, Cement cowl	Yes	Chrysotile Amosite

NOTES:

1. Sample(s) were examined for the presence of 6 types of asbestos fibres: crocidolite (blue), amosite (brown), chrysotile (white), anthophyllite, actinolite and tremolite.
2. Samples collected by the client are evaluated using information provided by the client. For samples collected by the client the date of receipt is deemed to be the same as the date sampled.
3. Envirochem is a UKAS accredited laboratory for sampling and identification of asbestos containing materials.
4. Comments, observations and opinions are outside the scope of UKAS accreditation.
5. The analytical method in the HSG248 does not quantify the amount of asbestos present, therefore UKAS accreditation does not permit quantification.
6. If, during fibre identification, only 1 or 2 fibres are seen and identified as asbestos, then the term 'trace asbestos identified' is used.

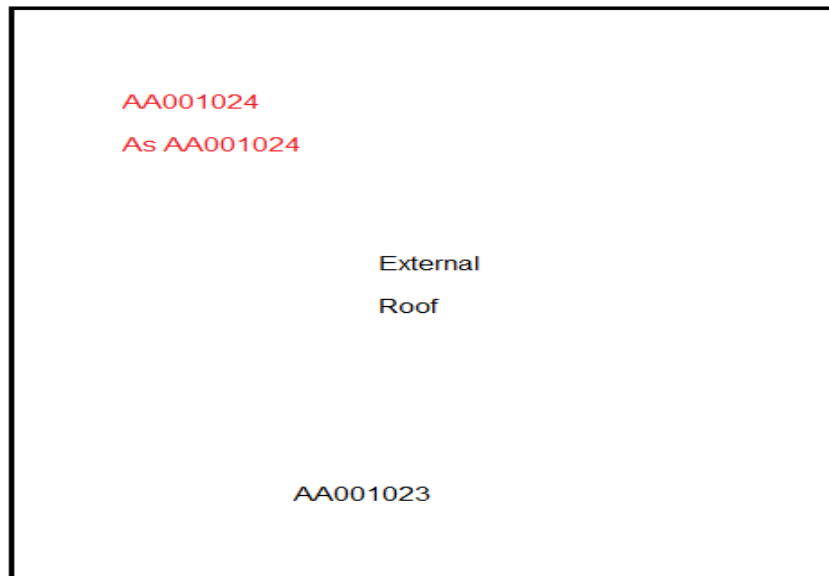
SIGNATURE:

Authorised signatory

PRINT NAME: Frances Scott

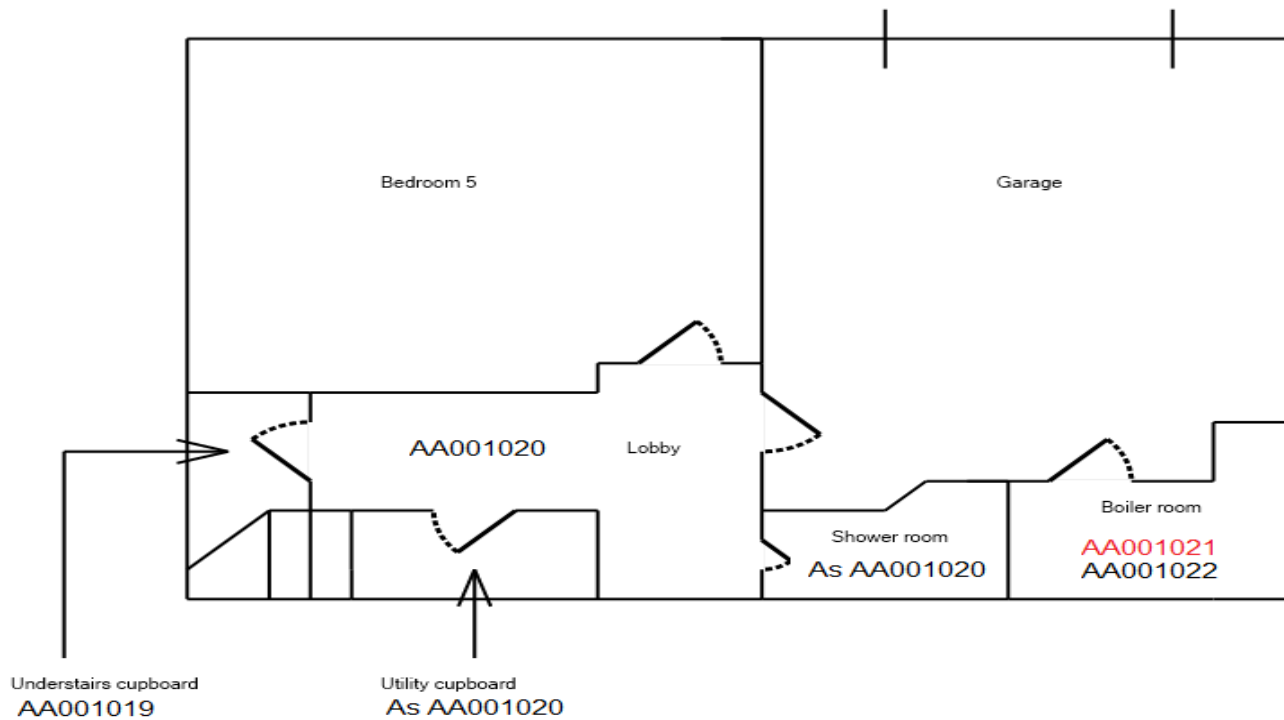
**Reg. No. 2378228 England. Registered Office: Envirochem, 12 The Gardens, Broadcut, Fareham, Hampshire, PO16 8SS.**

# Appendix 5 – Plans

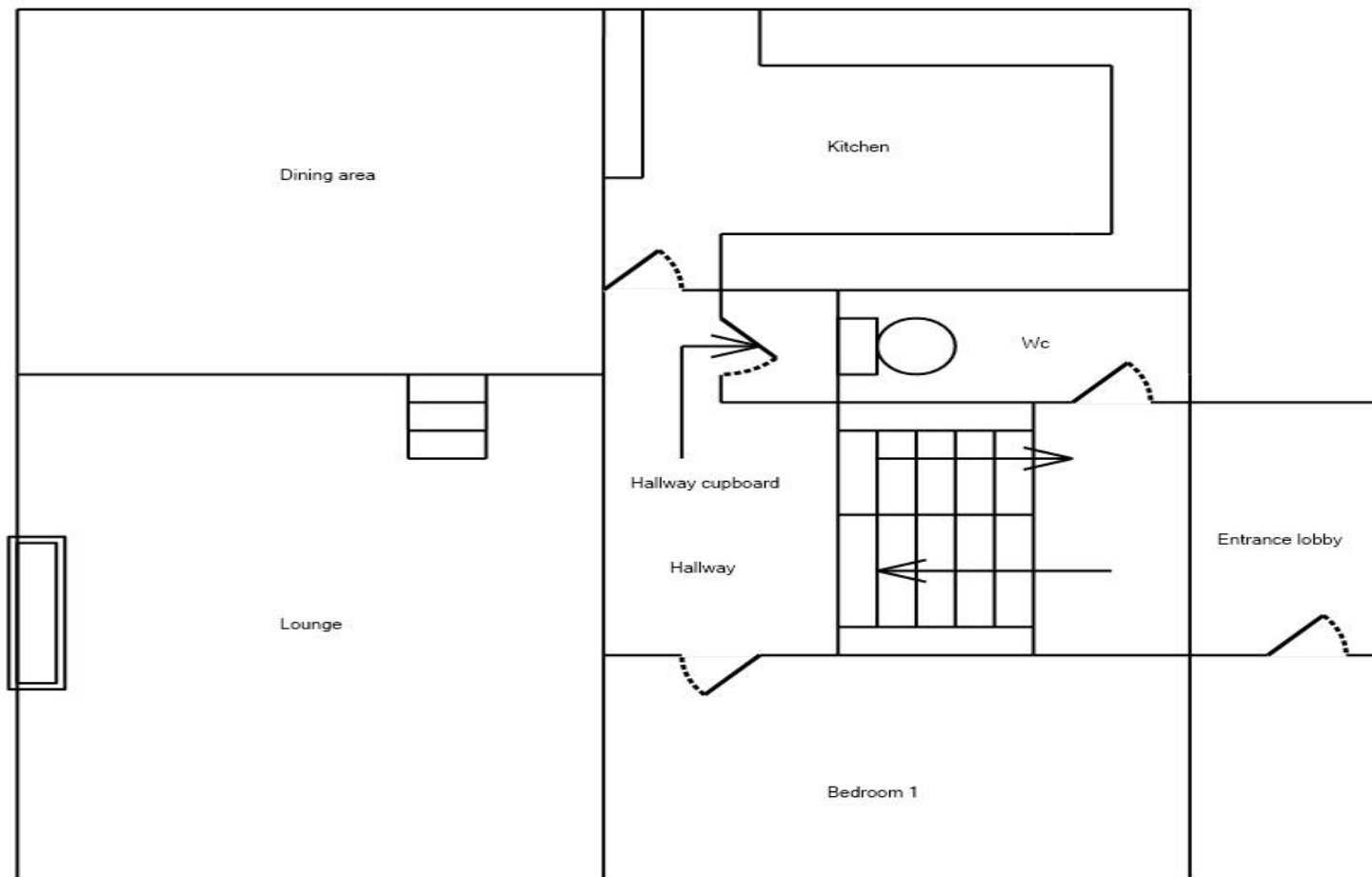


Client: Progress UK  
Site: 18a Frogna Gardens  
Floor: External  
UPRN No: N/A

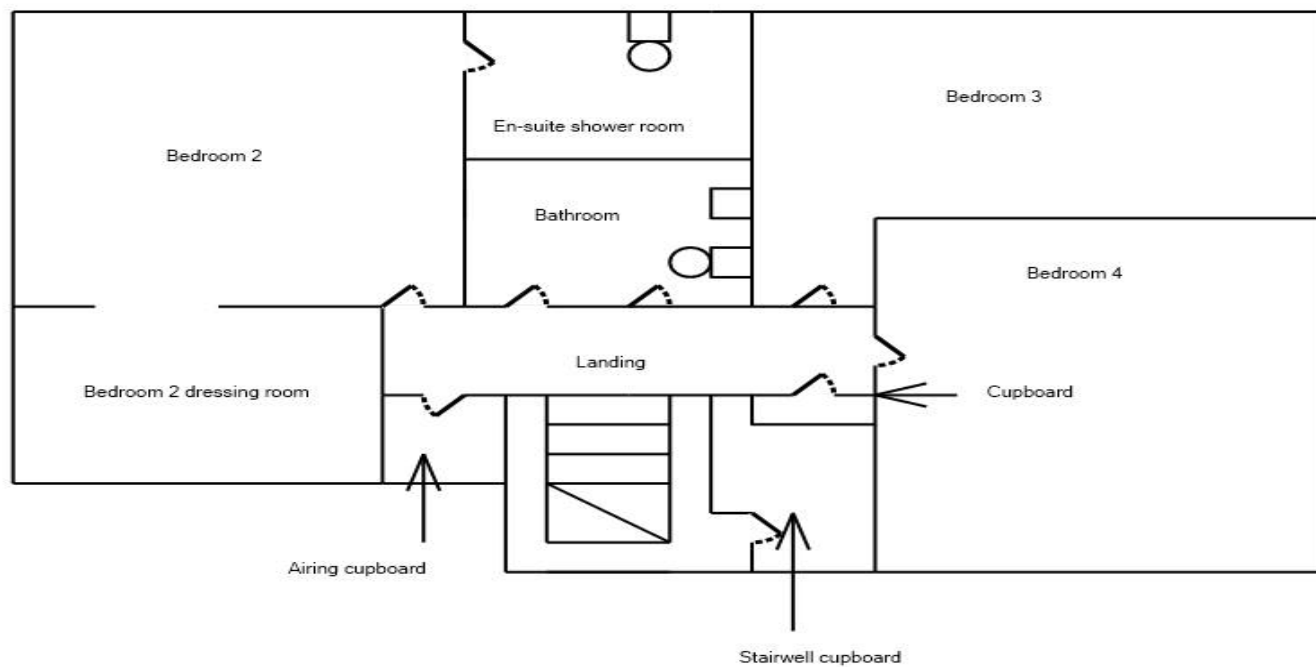
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Client: Progress UK  
Site: 18a Frogna Gardens  
Floor: Z-Sub Level 1  
UPRN No: N/A



Client: Progress UK  
Site: 18a Frogal Gardens  
Floor: Ground Floor  
UPRN No: N/A

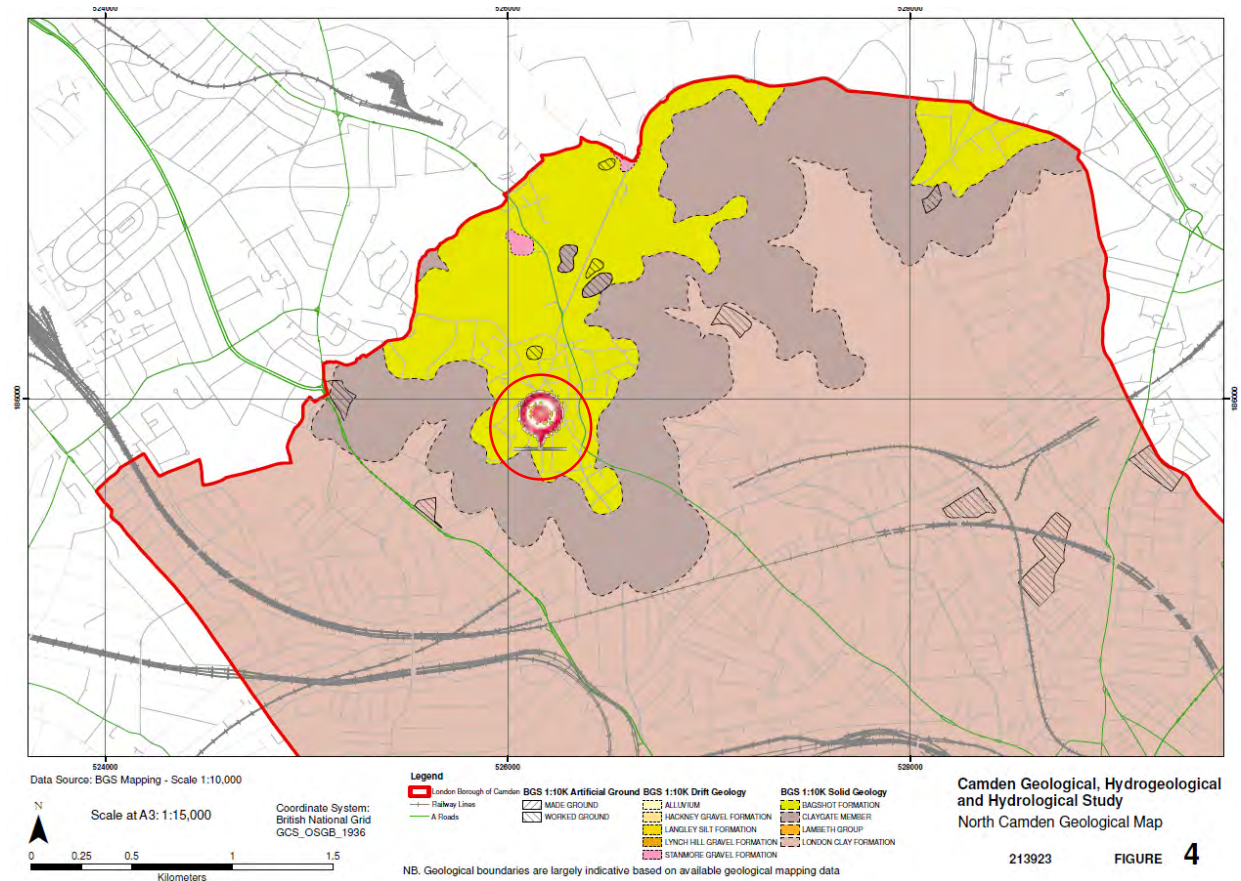
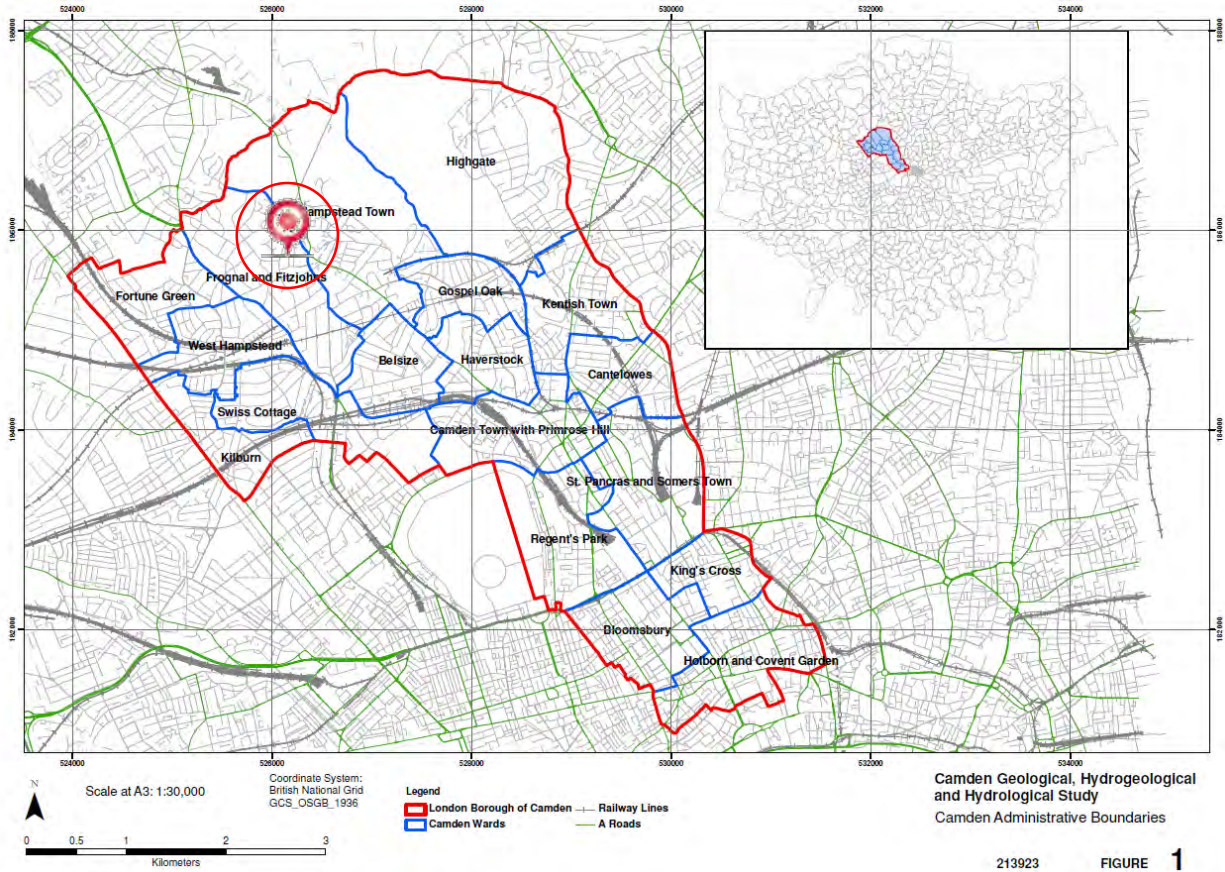


Client: Progress UK  
Site: 18a Frogna Gardens  
Floor: 1st Floor  
UPRN No: N/A

## **APPENDIX F**

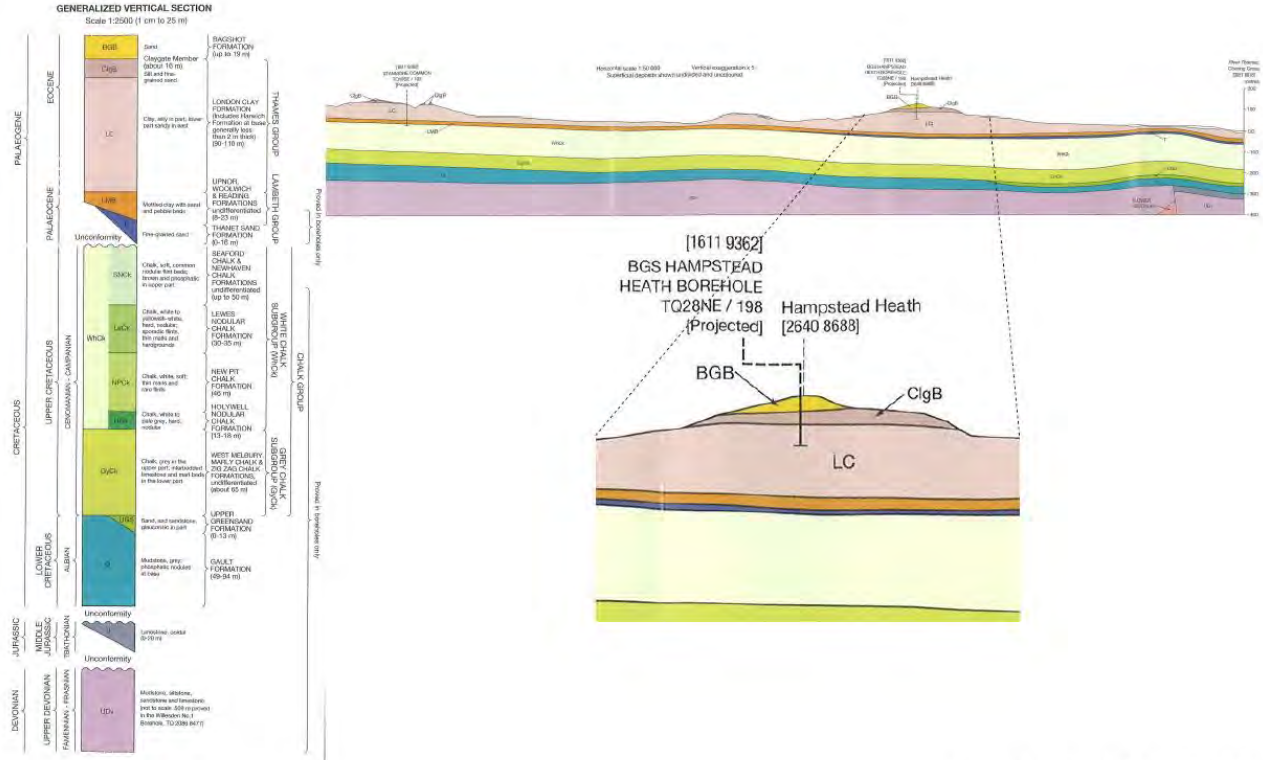
 Arup Figures for BIA Land Stability Assessment

**Arup Figs for BIA**





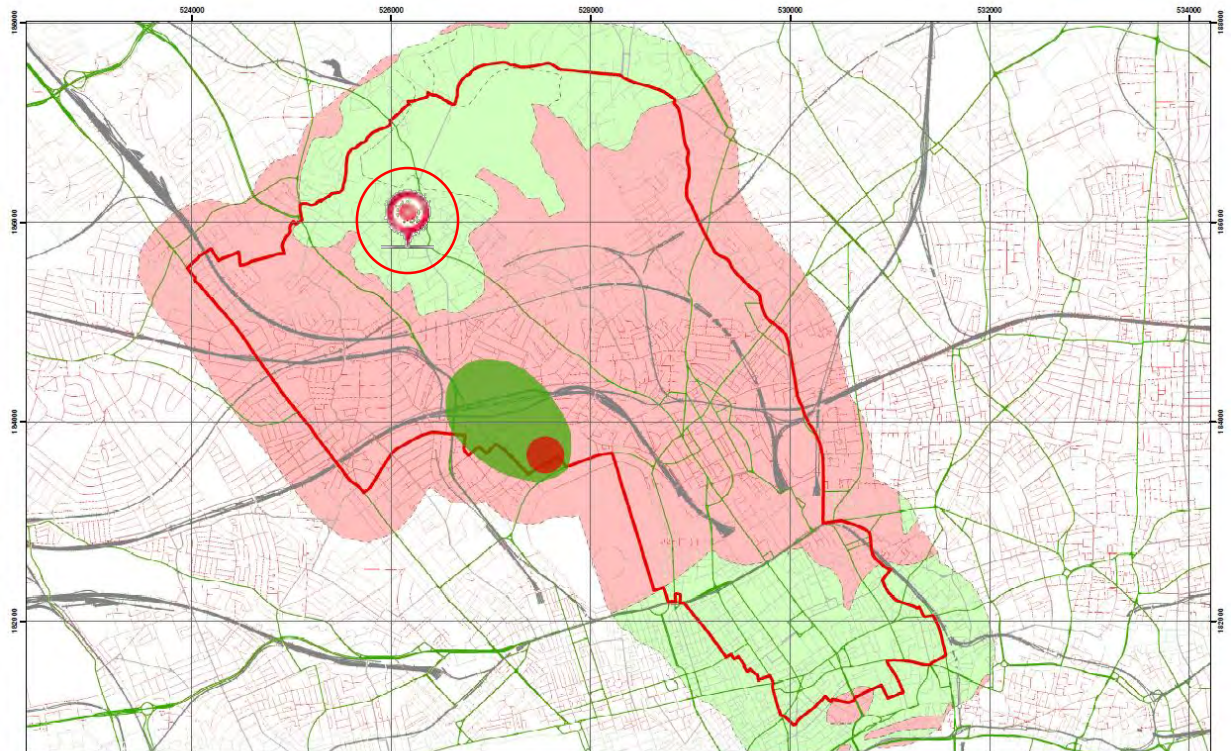
**Arup Figs for BIA**



Camden Geological, Hydrogeological and Hydrological Study  
Geological Long Section (NW - SE)

213923

FIGURE 7

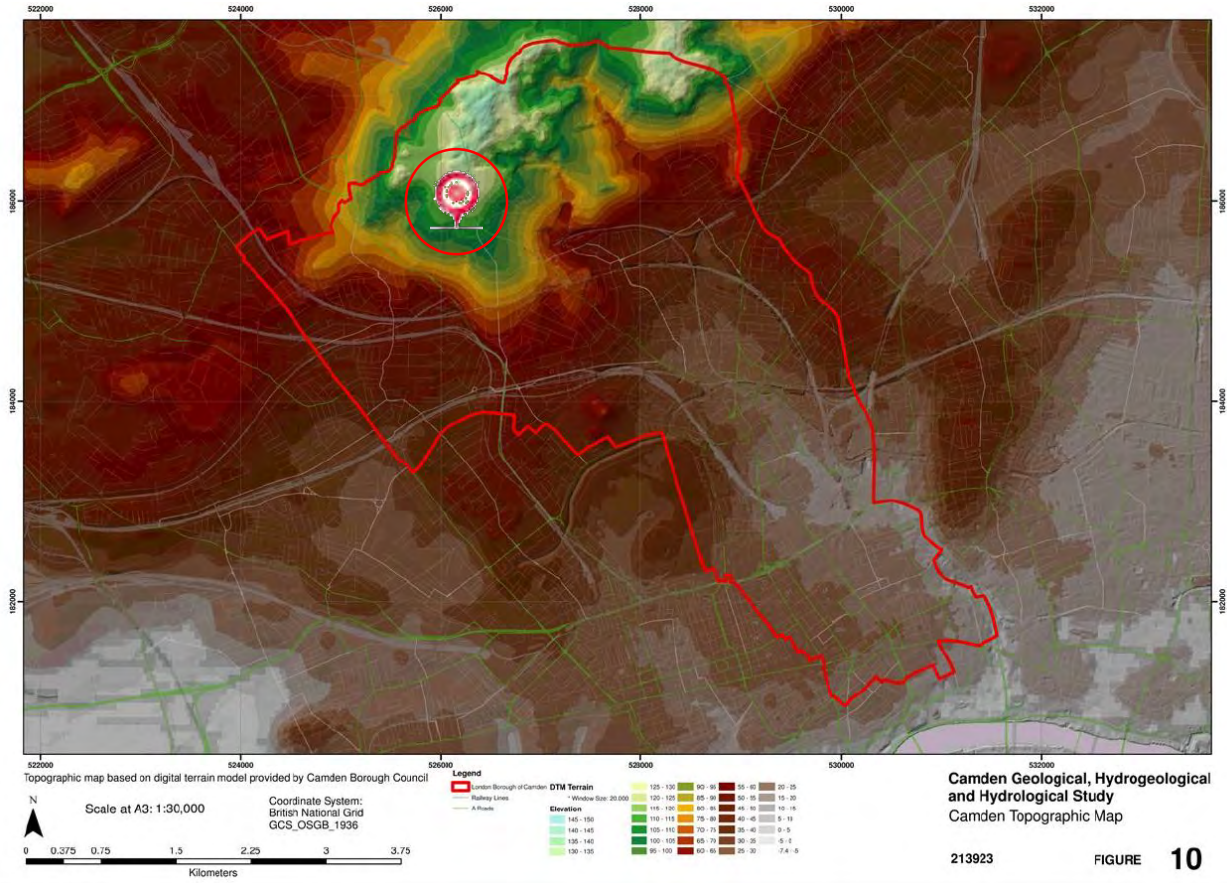


Camden Geological, Hydrogeological and Hydrological Study  
Camden Aquifer Designation Map

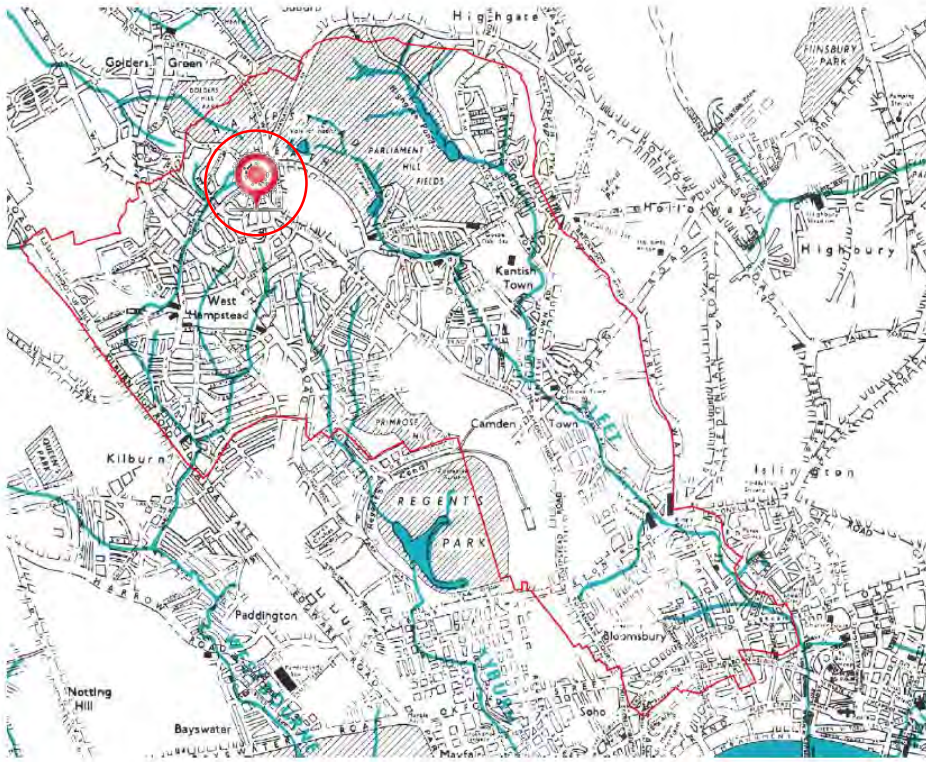
213923

FIGURE 8

**Arup Figs for BIA**



**Arup Figs for BIA**

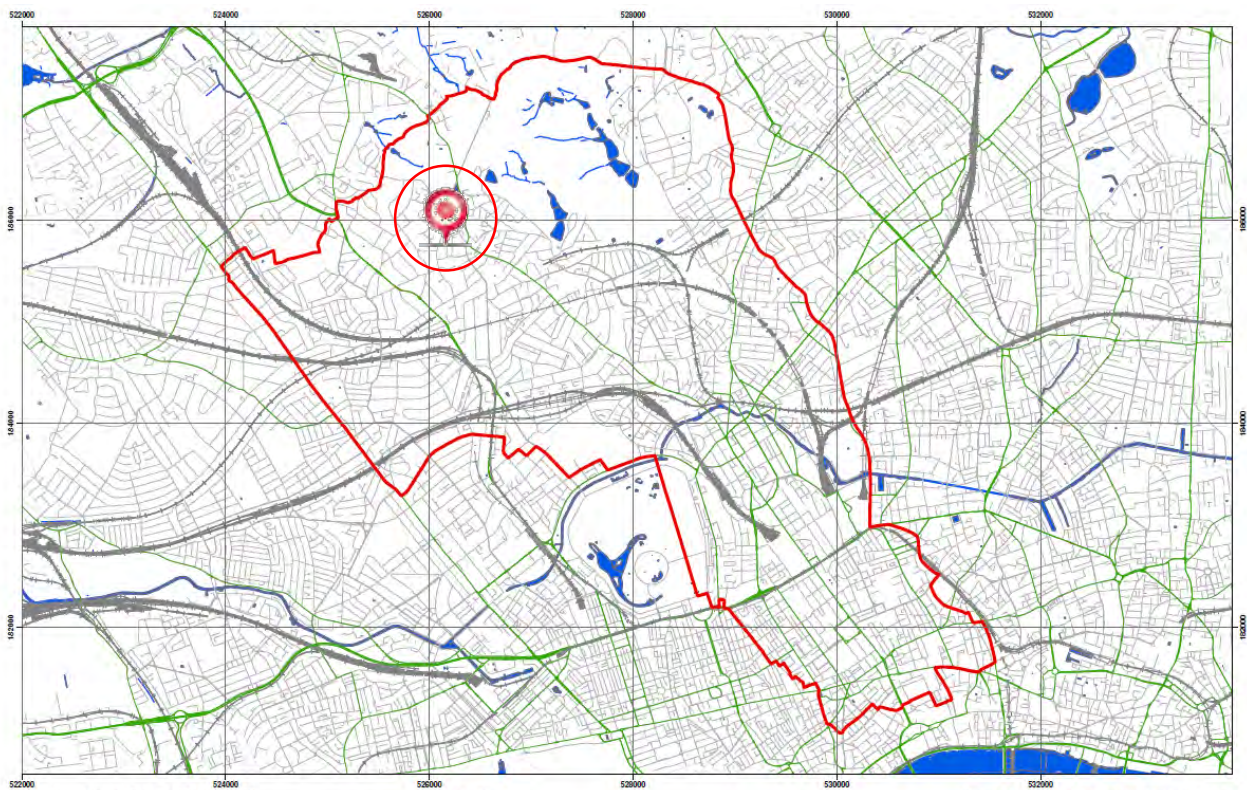


Source - Barton, Lost Rivers of London

Camden Geological, Hydrogeological and Hydrological Study Watercourses

213923

**FIGURE 11**



Data Source: London Borough of Camden, 2010

Scale at A3: 1:30,000

Coordinate System:  
British National Grid  
GCS\_OSGB\_1996

**Legend**

- London Borough of Camden
- Railway Lines
- A Roads
- Surface water



Camden Geological, Hydrogeological and Hydrological Study  
Camden Surface Water Features

213923

**FIGURE 12**

**Arup Figs for BIA**

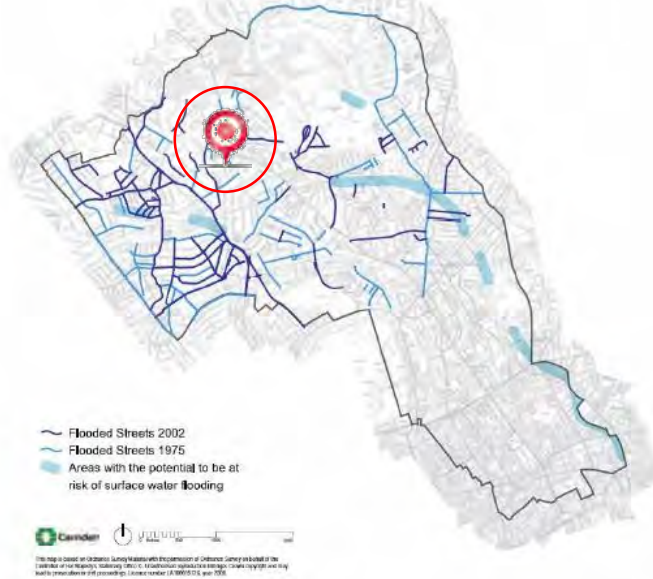
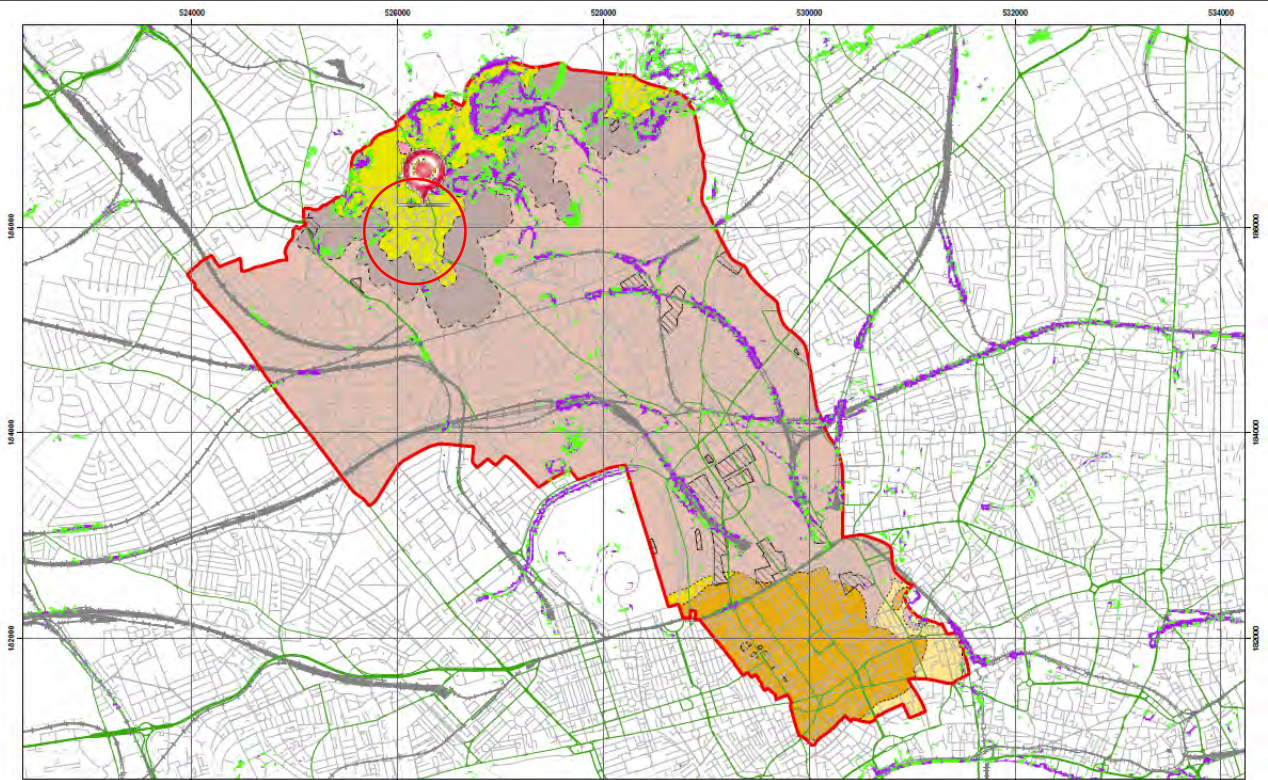


Figure 5 from Core Strategy, London Borough of Camden

**Camden Geological, Hydrogeological and Hydrological Study**  
**Flood Map**

213923

**FIGURE 15**



Slope Angles calculated from Digital Terrain Model Provided By Camden Borough Council

Scale at A3: 1:30,000  
 1:10,000 BGS Mapping  
 Coordinate System:  
 British National Grid  
 GOS\_OSGB\_1936

**Legend**  
 Slope: 0°-2° (Green), 2°-10° (Yellow), >10° (Red)  
 London Borough of Camden (Red outline)  
 BGS 1:10K Artificial Ground (Grey)  
 MADE GROUND (Grey)  
 WORKED GROUND (Grey)  
 BGS 1:10K Drift Geology: ALLUVIUM (Light Green), HACKNEY GRAVEL FORMATION (Light Green), LANSLEY HILL FORMATION (Light Green), STAMFORD GRAVEL FORMATION (Light Green)  
 BGS 1:10K Solid Geology: BAUGHOT FORMATION (Yellow), CLAYTON MEMBER (Yellow), LAMBETH GROUP (Yellow), LONDON CLAY FORMATION (Yellow)

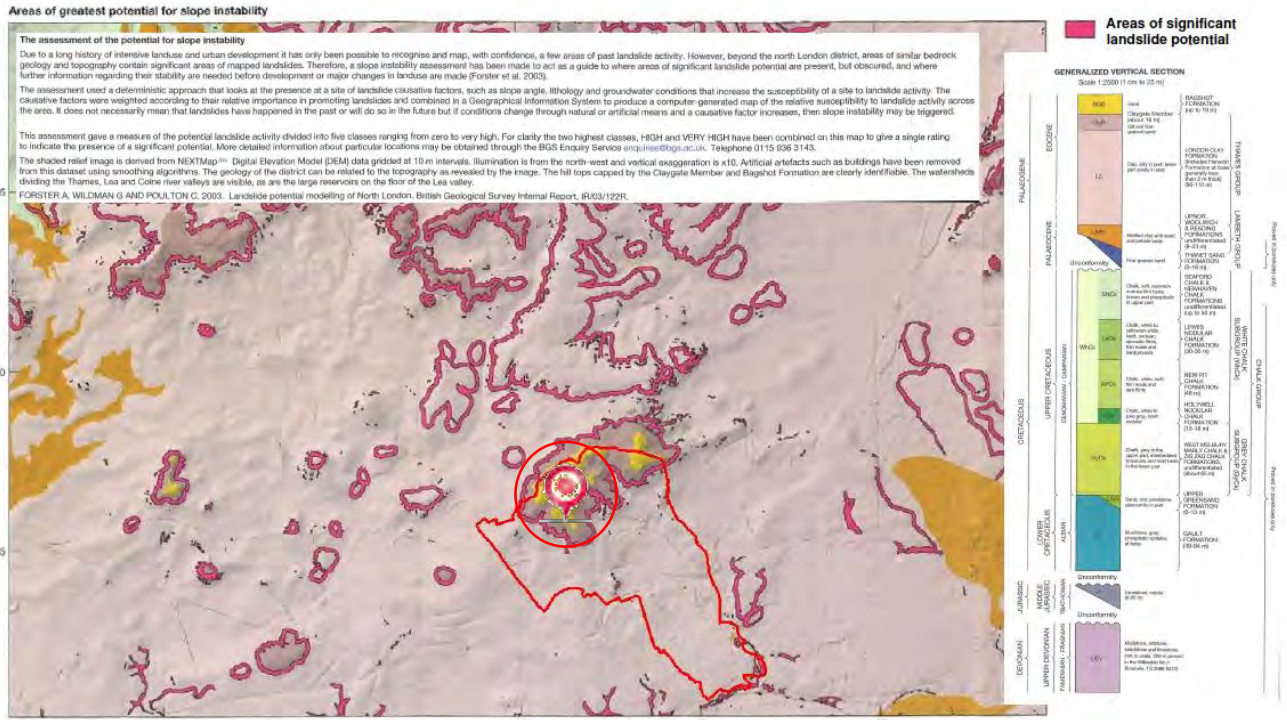
**Camden Geological, Hydrogeological and Hydrological Study**  
**Slope Angle Map**

213923

**FIGURE 16**

NB. Geological boundaries are largely indicative based on available geological mapping data

**Arup Figs for BIA**



Source - British Geological Society, 1:50,000 Series England and Wales Sheet 256 - North London

**Camden Geological, Hydrogeological and Hydrological Study**  
Areas of landslide potential

213923 **FIGURE 17**



Source - London Borough of Camden, January 2010. Camden Core Strategy Proposed Submission.

**Camden Geological, Hydrogeological and Hydrological Study**  
Transport Infrastructure

213923 **FIGURE 18**

## **APPENDIX G**

✚ CSG Usher's Ltd, 'Tree report in accordance with BS 5837:2012', ref: 031682, date: 28<sup>th</sup> August 2019




Unit 13 Waterways Business Centre  
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## Tree report in accordance with BS 5837:2012

Site Address: 18a Frognal Gardens, London, NW3 6XA  
Ref: 031682/v2

Arboriculturist: James Forrest / CSG (Usher's) Ltd. (07983443387)  
Architect: Ayesha Khan / Alison Brooks Architects (02072679777)  
Client: Nadine Majaro (07831392676)

Signed: 

Report Date: 28<sup>th</sup> August 2019 (v1) / 25<sup>th</sup> October 2020 (v2)





## TABLE OF CONTENTS

TOP SHEET .....	1
TABLE OF CONTENTS .....	2
<b>1.0 INSTRUCTIONS</b> .....	3
1.2 V2 CHANGES .....	3
<b>2.0 THE SITE</b> .....	4-6
<b>3.0 ARBORICULTURAL IMPACT ASSESSMENT (AIA)</b> .....	7-11
<b>4.0 ARBORICULTURAL METHOD STATEMENT (AMS)</b> .....	12-15

## APPENDICES

APPENDIX 1: TREE SURVEY SCHEDULE	
APPENDIX 1A: TREE SURVEY KEY	
APPENDIX 1B: RPA TABLE	
APPENDIX 2: TREE PROTECTION PLAN (TPP)	



## **Demolition of existing structure and construction of a new 4-storey dwelling in its place**

### **1.0 Instructions**

1.1 I have been instructed by the client, Nadine Majaro, via telephone with regards to a planning application to be made by themselves in respect to the above construction project. I shall report on the following in accordance with BS 5837:2012 'Trees in Relation to design, demolition and construction – recommendations':

1. Tree survey [Appendix 1]
2. Arboricultural Impact Assessment (AIA) [Section 3.0]
3. To produce an Arboricultural Method Statement (AMS) to include a Tree Protection Plan (TPP) [Section 4.0]

Following a visit (6<sup>th</sup> February 2019) to survey the trees knowing the location of the new dwelling, the following arboricultural information is provided in support of the application.

1.2 This report is based on a previous report that was withdrawn and replaced with this v2 to reflect changes to the previously submitted proposal. These alterations included:

- Height to top of chimney reduced by 850mm
- Height to top of roof reduced by 350mm
- Curved 1220mm setback to east gable wall
- 230mm setback to top floor front wall
- 450mm top floor setback from east gable wall
- 1<sup>st</sup> and 2<sup>nd</sup> floor levels reduced 150mm
- Side wall height reduced by 450mm
- Window height reduced by 650mm
- Front GF projection set back by 1575mm
- More opaque planting to boundary with 18

Fundamentally, none of these changes have materially altered the impact the proposal will have on the retained trees. If anything, the slight footprint reduction has lessened the impact, albeit by a negligible degree. As a result, the only difference between this version of the arboricultural report, when compared to the original, is a new Tree Protection Plan (attached as Appendix 2).

## 2.0 The site

- 2.1.1 The proposed development as per drawings provided by the architects is for the construction of a new 4-storey dwelling in place of the structure currently in place.

The project will involve the demolition of the existing building. The plan is to then construct a new house on the same site but with an increase in building footprint. Deep excavation will be required to create living space below the level of the ground.

Landscaping of both the front and rear garden areas will be undertaken post construction.

- 2.1.2 An accurate, to scale map of the site was provided by the client [ABA-2473-20-003]. I have annotated this drawing to produce a TPP [CSG/TPP/FG2] and attach this to the report as Appendix 2. This plan presents the proposed layout opposed to the site as it currently exists.
- 2.1.3 As the current building is being demolished, site access will allow for heavy plant machinery on to site. The trees do not pose a height restriction to what can enter the site. Parking of construction vehicles will be on Frogmal Gardens itself, comfortably outside the RPA of T10.

## 2.2 Trees around the site

- 2.2.1 There are several significant trees located around this site, both part of 18a Frogmal Gardens and 3<sup>rd</sup> party trees. The wider visual impact of the some of the larger trees is dampened by them being set back from public view but, nonetheless, they provide visual amenity in combination enriching the area as a whole. A schedule of the significant trees, their condition and category of retention is attached as Appendix 1.
- 2.2.2 The property and neighbouring properties contains a mix of young, semi mature, early mature and mature species including lime, sycamore and horse chestnut. 18a Frogmal Gardens also has a wide array of mature shrubs both in the front and rear gardens. These have not been surveyed but have been acknowledged.

2.2.3 This report includes only those trees around the proposal that require assessment as to the impact the process of construction works may have on them and what effect the trees will have on the project in the future.

Any trees that are not within a distance 12x their stem diameter may not have not been considered for this report for this reason.

2.2.4 The most significant tree with respect to the proposal is a lime (T10) [Figure 1] located towards the rear boundary of 18a Frognal Gardens' rear garden. No works are planned to occur within the RPA of this tree.

Figure 1 T10



- 2.2.5 Through a check with the Local Authority (London Borough of Camden), there is a Tree Preservation Order (TPO) on a tree within the front garden (not marked on survey), mixed in amongst mature shrubbery. This is a false acacia (*Robinia pseudoacacia*) that was felled by CSG (Usher's) due to poor health in late 2006. The stump is currently regenerating despite past works to prevent this. There is little in the way of amenity remaining in its current state and its complete removal is recommended to facilitate the proposal. Planting planned for the front garden area will serve to mitigate against this loss.
- 2.2.6 All recommended tree works considered necessary for health and safety reasons or to facilitate the development will be agreed with the Local Planning Authority and undertaken in accordance with the planning conditions attached to the planning consent. They will be undertaken in accordance with British Standard 3998:2010 'Recommendations for Tree Works', unless otherwise specified with clear justification for any deviation from the British Standard. This will be undertaken by an arboricultural contractor approved by the Local Authority.

### 2.3 New structures

- 2.3.1 New dwelling to be sited and constructed as per architectural drawings.

### **3.0 Arboricultural Impact Assessment (AIA)**

#### **3.1 Presence of Tree Preservation Orders (TPO) or Conservation Area Designation**

3.1.1 I have checked on the London Borough of Camden's website and confirmed the site is located within a designated Conservation Area. An e-mail request to the Local Authority seeking to confirm the presence of TPOs on or around this site was been placed by the architect. It was confirmed that a TPO was attached to a tree within the front garden (*Robinia pseudoacacia*). This tree was felled in 2006 with the stump retained (see 2.2.5).

#### **3.2 Effects on amenity value of the trees from development and facilitation pruning**

3.2.1 No facilitation works are currently planned to retained trees. No impact on amenity value of the area as a result.

3.2.2 T2, T7, T8 and T9 are recommended for removal for reasons already stated (see schedule with Appendix 1b). It is anticipated that the overall loss in amenity will be minor given T7-T9 are located within the rear garden, away from public view.

The removal of the majority of the mature shrubbery both in the front and rear gardens will have the greater impact on the overall amenity. These items are being removed to facilitate development as well as clearing the way for re-landscaping where extensive planting has been planned to restore any amenity that may have been lost.

#### **3.3 Potential incompatibilities between the layout and the trees proposed for retention**

3.3.1 Construction activity will technically enter the RPA of T1 when drawn as a nominal circle. Given the established hard standing (pavement, tree surround and tarmac driveway to eastern side of property) in between T1 and the front garden of 18a, it is not anticipated that any significant roots from T1 exist within the section of the RPA that clips the front corner of the rear garden. There is very little in the way of root-induced disturbance of these surfaces that might suggest root encroachment into the RPA.

Excavation works to accommodate the basement level will occur outside the RPA of T10 as drawn as a nominal circle. There is no reason to deviate from a nominal circle. From that point of view, there is no incompatibility between T10 and the new structure. New decking will be laid to the rear of the proposed dwelling that will exist very slightly in the southern portion of T10's RPA. This will not involve extensive ground excavation and will be done by hand-only. Measures laid out within the AMS will be followed should roots from this tree be encountered.

Landscaping works will have no impact within the front garden as roots from T1 are not likely to be encountered. Landscaping works within the rear garden will not involve an alteration to level or grade of the soil and will not involve any significant groundworks that might impact on T10. T10's location in a raised area behind a retaining wall with an existing hard standing surround means that little root disruption is foreseeable despite landscaping works being planned within the RPA.

There is a proposal to remove and rebuild the retaining wall directly adjacent to T10. The demolition will be done by hand only and arboricultural advice will be sought should any significant roots impede the rebuilding of this wall. The existing paving slabs directly to the south of T10 will be lifted by hand and replaced with mulch. This will be of benefit to T10 providing an improved rooting environment. The wall will then serve as a physical barrier between T10 and the worksite.

T4, T5 and T6 are 3<sup>rd</sup> party trees whose RPA clips the north-eastern corner of the site. Similar to T1, there is not an anticipation that significant roots will be found in this portion of the garden given the presence of a boundary wall and an established tarmac driveway [Figure 2] between the two.

Figure 2 Established driveway between 18a and 3<sup>rd</sup> party trees to the east



- 3.3.2 Measures have been laid in within the AMS for procedures to follow should roots be encountered in this area but, given factors previously mentioned, there is not an anticipation that any significant roots (over 25mm in diameter) will be encountered. Resultantly, the long-term health of these trees is highly unlikely to be compromised during ground disturbance caused by the demolition and excavation works.
- 3.3.3 The house will connect to the existing rainwater, soil and waste drainage which is located under the driveway in the front garden (marked as storage area on TPP). A tank will also be installed under the driveway to provide additional attenuation to the sewer. All lie in the centre of the current drive outside of the RPA of any retained trees.

### 3.4 Infrastructure requirements – highway visibility, lighting, CCTV, services etc

3.4.1 There is no requirement for any tree removal or pruning to create adequate highway visibility. There will be no requirement for street lighting or CCTV visibility or services close to any of the retained trees. Should that not be the case, any below-ground services that are installed within or pass through the RPAs of retained trees will be done in accordance with NJUG Volume 4 “Guidance for the planning, installation and maintenance of utility services in proximity of trees” to minimise the disturbance to the retained trees’ root systems.

3.4.2 No services (unless otherwise highlighted in 3.4.1) or other infrastructure requirements will have any impact on the retained trees as far as I know.

### 3.5 Mitigating tree loss/new planting

3.5.1 There are sufficient trees of greater value within and surrounding this site to mitigate against the loss of the low value trees being removed.

Replacement tree plantings will be carried out to mitigate against the complete removal of the protected tree previously felled down to stump level.

### 3.6 Proximity of trees to structures

3.6.1 The impact of trees on buildings and vice versa and allowance for future growth need to be considered when designing the foundations and they need to be suitable to withstand the potential indirect damage roots from this tree, and others in the surrounding area, could have. Therefore, foundation design needs to be in accordance with NHBC Chapter 4.2 ‘Building near trees’.

Given the proposal includes a basement level, the foundations will be of a depth that, going forward, roots would not ordinarily be encountered at.

The canopies of retained trees will not overhang the roof of the proposed structure.



3.6.2 As T1 is south-east of the proposal and close enough to have an effect, a certain level of shading to the property will be present at the start of the day. The size and number of windows will need to be designed in acceptance of this fact to allow as much natural light in as possible while still retaining the tree without modification.

The remainder of the retained trees are due north of the proposal and, therefore, shading is not an issue

3.6.3 Following a prediction derived from previously stated factors, it is not considered likely that significant roots from any retained trees of a diameter greater than 25mm will be encountered within the construction site. Any severance of a small number of minor roots will have an insignificant effect on the future growth and health of the retained trees. Where more significant roots are encountered, procedures laid out in the AMS should be adhered to.

3.6.4 Overall the processes of construction should not have a detrimental impact on the trees provided care is taken and the AMS is adhered to.

### 3.7 Issues to be addressed by the arboricultural method statement (AMS)

- Protective fencing to be established around the retained trees
- Ground protection measures around the RPA of retained trees where work access is required
- Site access
- Contractors parking, welfare facilities and storage areas
- Hard surfaces within the RPA of retained trees
- Remedial tree work
- Construction within the modified RPA of retained trees

## 4.0 Arboricultural Method Statement (AMS) for Tree Protection Throughout the Duration of Demolition and Construction Works

Arboricultural Method Statement includes a Tree Protection Plan to identify:

- Trees to be retained – identified with a continuous black line
- Protective fence positions therefore the Construction Exclusion Zones
- Measurements to identify fence positioning in relation to centre of tree
- Contractor huts and storage areas

### 4.1 Construction Exclusion Zones (CEZ)

4.1.1 No need for the setting up a CEZ using protective fencing for this site. Rebuilding of retaining wall adjacent to T10 to be done prior to any other rear garden landscape works. This will then serve as a physical barrier between T10 and the work site. T1 and T4-T6 detached from the project enough to not warrant physical fencing.

### 4.2 Access Details

4.2.1 Access for construction traffic will be via Frogna! Gardens. No plant machinery will have access in to the RPA of any retained trees.

4.2.2 Where incursion into RPAs is unavoidable within non hard-standing areas this will be restricted only to persons. Ground protection for pedestrians within the RPA will consist of single thickness scaffold boards on a scaffold frame on top of 100mm of woodchip laid on a geotextile membrane.

### 4.3 Contractors car parking

4.3.1 Parking limited to Frogna! Gardens. This is a tarmacked highway. Any technical incursion into T1's RPA is not considered an issue.

### 4.4 Site Huts and Toilets

4.4.1 Likely to be within the front garden or on Frogna! Gardens. In any case, will not be within T1's RPA.

#### 4.5 Storage Space

- 4.5.1 A designated storage area will be located within front of the property or garden area outside of RPA. Marked on Tree Protection Plan.

#### 4.6 Additional Precautions

- 4.6.1 No storage of materials, lighting of fires will take place within any construction Exclusion Zone. No mixing or storage of materials will take place up a slope where they may leak into a Construction Exclusion Zone.
- 4.6.2 No fires will be lit within 20 metres of any tree stem and will take into account fire size and wind direction so that, no flames come within 5m of any foliage.
- 4.6.3 No notice boards, cables or other services will be attached to any tree.
- 4.6.4 Materials which may contaminate the soil will not be discharged within 10m of any tree stem. When undertaking the mixing of materials it is essential that, any slope of the ground does not allow contaminates to run towards a tree root area. This includes fuels, oils, concrete mix etc.
- 4.6.5 All services, including drainage and soakaways, to be installed outside the RPA of retained trees. Where unavoidable, any below-ground services that are installed within or pass through the RPAs of retained trees will be done in accordance with NJUG Volume 4 “Guidance for the planning, installation and maintenance of utility services in proximity of trees” to minimise the disturbance to the retained trees’ root systems.

#### 4.7 Demolition / Excavation

- 4.7.1 Excavation of existing hard surface within the RPA of all retained trees to be done by hand only. Exposed roots to be wrapped in dry, clean hessian sacking to prevent desiccation and adverse temperature change. Appointed arboriculturist to be called to site to make an assessment on the implication of damage to the roots encountered.

Only roots smaller than 25mm in diameter may be pruned back but must be with a clean suitable cutting tool and, preferably, pruned to a side branch. To be done in accordance with NJUG Volume 4 "Guidance for the planning, installation and maintenance of utility services in proximity of trees". Prior to backfill, hessian wrap must be removed and retained roots must be surrounded by sharp sand prior to soil replacement. Replacement topsoil must comply with BS 3882:2007 'Specification for topsoil and requirements for use'

#### 4.8 Hard Surfaces

- 4.8.1 New hard surfacing to the front of the property.

#### 4.9 Soft Landscaping / Use of Herbicides

- 4.9.1 No soft landscaping within 2 metres of the base of retained trees. Only mulch to be placed within this area. Any mulch used must be BS EN 4790:1997 certified and be applied to a depth of no more than 100mm. Mulching material must be kept away from directly contacting the bark of any tree stems.

- 4.9.2 Any herbicide used prior to construction phase shall be systemic, spot applied, and mixed according to manufacturer's recommendations.

#### 4.10 Contingency Plan

- 4.10.1 Water will be made readily available on site and will be used to flush spilt materials through the soil and avoid contamination to tree roots. At the time of any spillage the main contractor will contact an arboriculturist for advice.

#### 4.11 Remedial Tree Works

4.11.1 Tree works (see section 3.2 of AMS) to be done prior to construction phase. All tree works are to be carried out in accordance with BS 3998 (British Standard Recommendations for Tree Work 2010).

#### 4.12 Responsibilities

4.12.1 It will be the responsibility of the main contractor to ensure that the planning conditions attached to planning consent are adhered to at all times and that a monitoring regime in regards to tree protection is adopted on site.

4.12.2 The main contractor will be responsible for contacting the Local Planning Authority at any time issues are raised related to the trees on site.

4.12.3 If at any time pruning works are required permission must be sought from the Local Planning Authority first and then carried out in accordance with BS 3998:2010 'Recommendations for Tree Works'.

4.12.4 The main contractor will ensure the build sequence is appropriate to ensure that no damage occurs to the trees during the construction processes. Protective fences will remain in position until completion of ALL construction works on the site.

4.12.5 Any fencing and signage must be maintained in position at all times and checked on a regular basis by an on-site person designated that responsibility.

4.12.6 The main contractor will be responsible for ensuring sub-contractors do not carry out any process or operation that is likely to adversely impact upon any tree on site.

4.12.7 Appointed arboriculturist must inspect the site at the start of the works and monitor it throughout. They must be on hand to assist and advise on any further arboricultural issues that may arise during the construction phase. All relevant persons must be briefed prior to works commencing laying out the arboricultural protection in place and the measures that must be adhered to so that the trees are protected

<b>Surveyor:</b> James Forrest	<b>Client:</b> Nadine Majaro	<b>Site:</b> 18a Frogna Gardens, NW3 6XA
<b>Survey Date:</b> 6th February 2019	<b>Weather:</b> Cloudy, Windy	<b>Reference:</b> 031682

Tree No.	Species	Height (m)	Estimated Crown spread (m)	stem diameter (mm)	Existing height of (m)		Life stage	Condition		Preliminary management	Estimated remaining contribution (Years)	Category grading
					First significant branch	Canopy		Physiological	Structural			
T1	Horse chestnut ( <i>Aesculus hippocastanum</i> )	16#	N 6 S 7 E 7 W 6.5	890	4.0-S#	5.5#	M	<u>Fair</u> . Local Authority tree. Bleeding canker present but not advanced at this moment in time	<u>Fair</u>	None	20+	B1/2
T2	Holm oak ( <i>Quercus ilex</i> )	4#	N 1.5 S 0.5 E 1 W 1	80	2.0-W#	2.0#	Y	<u>Fair</u>	<u>Fair</u>	None	10+	C1
G3	Mixed species	9#	N/A	N/A	N/A	N/A	N/A	<u>Fair</u>	<u>Fair</u> . Small 3rd party trees / shrubs that may affect access for larger vehicles using access road to the side of the site	None	10+	C2
T4	Sycamore ( <i>Acer pseudoplatanus</i> )	13#	N 4 S 4 E 4 W 4	650#	N/A (restricted view)	N/A (restricted view)	EM	Limited access to view and assess fully	3rd party tree with limited access to fully view. Been reduced recently and does not overhang the site	None	20+	B1*

Tree No.	Species	Height (m)	Estimated Crown spread (m)	stem diameter (mm)	Existing height of (m)		Life stage	Condition		Preliminary management	Estimated remaining contribution (Years)	Category grading
					First significant branch	Canopy		Physiological	Structural			
T5	Sycamore ( <i>Acer pseudoplatanus</i> )	13#	N 4 S 4 E 4 W 4	650#	N/A (restricted view)	N/A (restricted view)	EM	Limited access to view and assess fully	3rd party tree with limited access to fully view. Been reduced recently and does not overhang the site	None	20+	B1*
T6	Sycamore ( <i>Acer pseudoplatanus</i> )	18#	N 7 S 7 E 7 W 7	600# / 600#	N/A (restricted view)	N/A (restricted view)	EM	Limited access to view and assess fully	3rd party tree with limited access to fully view. Canopy overhangs the tarmac access road but not the site itself	None	20+	B1*
T7	Evergreen magnolia ( <i>Magnolia grandiflora</i> )	5.5#	N 3 S 1.5 E 2.5 W 1.5	300 (at 1.3m AGL - low crown break)	1.5-N#	1.5#	EM	<u>Fair</u>	Ivy obscuring view of mid-crown. Decay noted to stem at 1.3m - relatively minor. Pruning stubs present. Previous reduction history	None	10+	C1
T8	Hazel ( <i>Corylus avellana</i> )	6#	N 2 S 2.5 E 2 W 2	140	1.0-W#	1.5#	SM	<u>Fair</u>	<u>Fair</u>	None	10+	C1
T9	Elder ( <i>Sambucus nigra</i> )	5#	N 0 S 4 E 1 W 1	250# (restricted access to measure)	2.0-S#	1.0#	SM	Stems have died back post-pruning	Ivy obscuring inspection of base and trunk. Leaning markedly to the south	Remove	<10	U

Tree No.	Species	Height (m)	Estimated Crown spread (m)	stem diameter (mm)	Existing height of (m)		Life stage	Condition		Preliminary management	Estimated remaining contribution (Years)	Category grading
					First significant branch	Canopy		Physiological	Structural			
T10	Lime ( <i>Tilia</i> sp.)	18#	N 6 S 6 E 6 W 6	850# (restricted access to measure)	6.0-E#	6.0#	M	Appears adequate but there was restricted access preventing a view of the tree from all angles	Ivy, basal + epicormic shoots obscuring inspection of base and trunk. Fence restricting access to northern side of trunk. Decay potentially present in old pollard point on northern side - limited view to assess	Strip ivy from lowest 2m of trunk + remove basal + epicormic shoots to allow fuller inspection / Carry out aerial inspection of crown from a climbed position - condition of old pollard points of particular interest	20+	B1*
T11	Privet ( <i>Ligustrum</i> sp.)	4#	N 1.5 S 2 E 1.5 W 2.5	150 / 120	1.5-S#	1.5#	EM	Fair	Ivy obscuring inspection of base and trunk	None	10+	C2*



**KEY TO TREE SURVEY FORM**

<b>Tree No.</b>	Refer to plan
<b>Species</b>	Common name ( <i>scientific name</i> )
<b>Height</b>	Measured in metres from the ground to the top of the crown [Recorded to the nearest half metre for dimensions up to 10m and the nearest whole metre for dimensions over 10m]. When suffixed with a # it denotes that the value has been estimated.
<b>Crown spread</b>	Estimated in metres (N = north / E = east / S = south / W = west) [Rounded up to the nearest half metre for dimensions up to 10m and up to the nearest whole metre for dimensions over 10m].
<b>Stem diameter</b>	Measured at 1.5m above ground level [Rounded to the nearest 10mm]. Where stem diameter has been measured at a different height this will be stated and justified.
<b>Existing height of</b>	<p><u>First significant branch</u> – measured in metres from the ground up. Direction of growth noted (N = north / S = south / E = east / W = west) When suffixed with a # it denotes that the value has been estimated.</p> <p><u>Canopy</u> – measured in metres from the ground up. [Recorded to the nearest half metre for dimensions up to 10m and the nearest whole metre for dimensions over 10m]. When suffixed with a # it denotes that the value has been estimated.</p>
<b>Age class</b>	<p>Y     <u>Young</u> – within 1<sup>st</sup> quarter of species’ life expectancy</p> <p>SM    <u>Semi-mature</u> – within 2<sup>nd</sup> quarter of species’ life expectancy</p> <p>EM    <u>Early mature</u> – within 3<sup>rd</sup> quarter of species’ life expectancy</p> <p>M     <u>Mature</u> – within 4<sup>th</sup> quarter of species’ life expectancy</p> <p>OM    <u>Over-mature</u> – in natural decline</p> <p>V     <u>Veteran</u> – a tree that is of interest biologically, aesthetically or culturally because of its age, size and condition</p>
<b>Condition</b>	<p><u>Physiological</u></p> <p>An assessment of the physiological condition (i.e. health/vitality) of the tree categorised into:</p> <p>GOOD a tree in a healthy condition with no significant problems</p> <p>FAIR a tree generally in good health with some problems that can be remediated</p> <p>POOR a tree in poor health with significant problems that can’t be remediated</p> <p>DEAD a tree without sufficient live material to sustain life</p> <p><u>Structural</u></p> <p>An assessment of the structural/safe condition of the tree categorised into:</p> <p>GOOD a tree in a safe condition with no significant defects</p> <p>FAIR a tree in a safe condition at present but with defects or with significant defects that can be remediated</p> <p>POOR a tree with significant defects that can’t be remediated</p>

Notes related to both physiological and structural condition might follow the categorization in order support the statement and give greater detail on the true quality and value of the tree.

Minor deadwood – less than 25mm in diameter

Moderate deadwood – 25-50mm in diameter

Major deadwood – greater than 50mm in diameter

### **Preliminary management**

These may include further investigations for the presence or extent of decay or climbed inspections, ivy removal or pruning works when access is a non-moveable aspect etc (NB this is **not** intended to be a specification for tree work and further advice maybe required prior to implementation). Trees assessed as being in apparently immediately hazardous condition will be notified to the client separately as soon as possible.

### **Estimated remaining contribution**

An estimate of the remaining life contribution in years that the tree or group of trees is expected to have based on species, condition on the site in its current context. The following bands are used:

<10 - Tree is dead or dying and unlikely to contribute beyond 10 years

10+ - Tree is assessed as being able to contribute to the site for 10+ years

20+ - Tree is assessed as being able to contribute to the site for 20+ years

40+ - Tree is assessed as being able to contribute to the site for 40+ years

### **Category grading**

**A** = Trees of high quality with an estimated remaining life expectancy of at least 40 years

**B** = Trees of moderate quality with an estimated remaining life expectancy of at least 20 years

**C** = Trees of low quality with an estimated life expectancy of at least 10 years, or young trees with a stem diameter below 150mm

**U** = Trees in such a condition that they cannot realistically be retained as living trees in the context of the current land use for >10 years

**1** = Mainly arboricultural qualities

**2** = Mainly landscape qualities

**3** = Mainly cultural values, including conservation

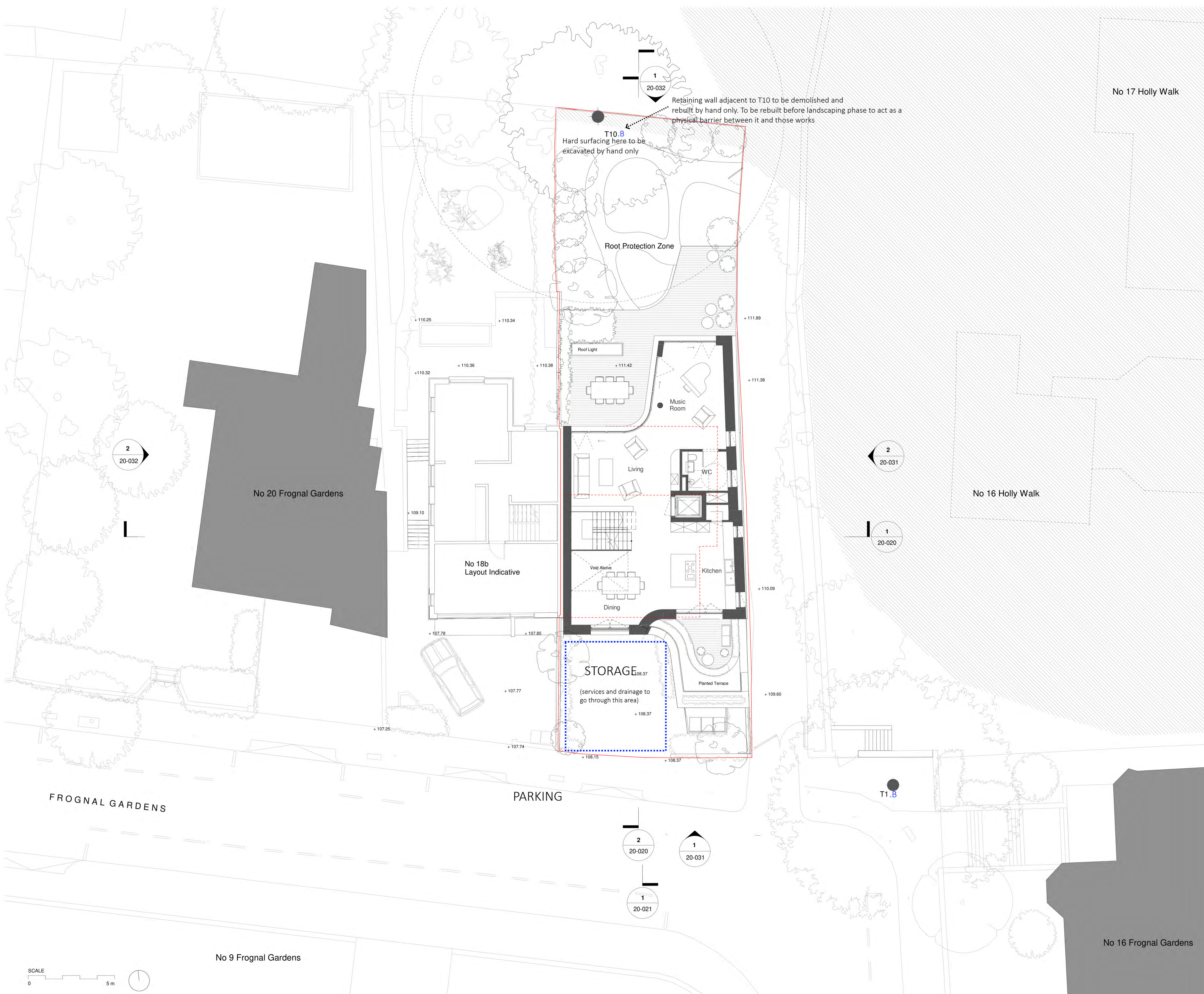
\* = denotes that the category grading is temporary and requires additional measures (e.g. climbed inspection, removal of ivy, full access all around the tree etc.) before a true grading can be assigned

**ROOT PROTECTION AREA (RPA) TABLE FOR RETAINED TREES**

<b>TREE NUMBER</b>	<b>RADIUS OF NOMINAL CIRCLE (m) [as per table D.1 (p.40 BS 5837:2012)]</b>	<b>RPA (m<sup>2</sup>) [as per table D.1 (p.40 BS 5837:2012)]</b>	<b>20% offset</b>	<b>OWNERSHIP STATUS</b>
1	10.80	366	N/A	3 <sup>rd</sup> party (Local Authority)
4	7.80	191	N/A	3 <sup>rd</sup> party (private)
5	7.80	191	N/A	3 <sup>rd</sup> party (private)
6	8.50	226	N/A	3 <sup>rd</sup> party (private)
10	10.20	327	N/A	18a Frognal Gardens
11	1.90	12	N/A	18a Frognal Gardens

**TREES SCHEDULED FOR REMOVAL**

<b>TREE NUMBER</b>	<b>REASON FOR REMOVAL RECOMMENDATION</b>
T9	Tree condition
T2	To facilitate construction
T7	To facilitate construction
T8	To facilitate construction

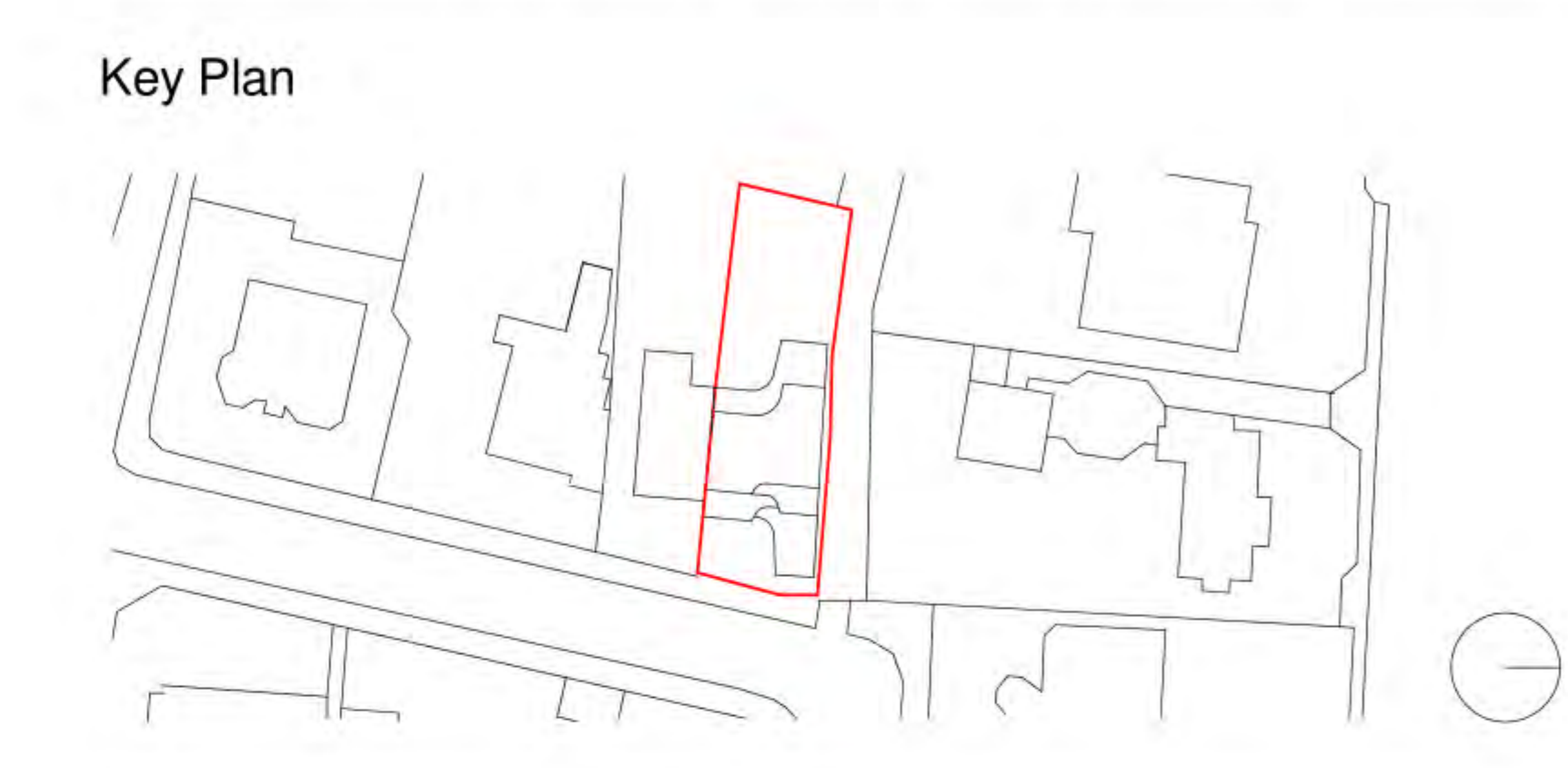


Notes  
 Boundary Line

031682/v2 Appendix 2  
 Tree Protection Plan  
 CSG/TPP/FG2

Rev	Date	Description
-----	------	-------------

Note  
 Do not scale from this drawing. To be read in conjunction with all relevant Architects', Services and Structural Engineer' information. Architect to be immediately notified of discrepancies.



**ALISON BROOKS ARCHITECTS**

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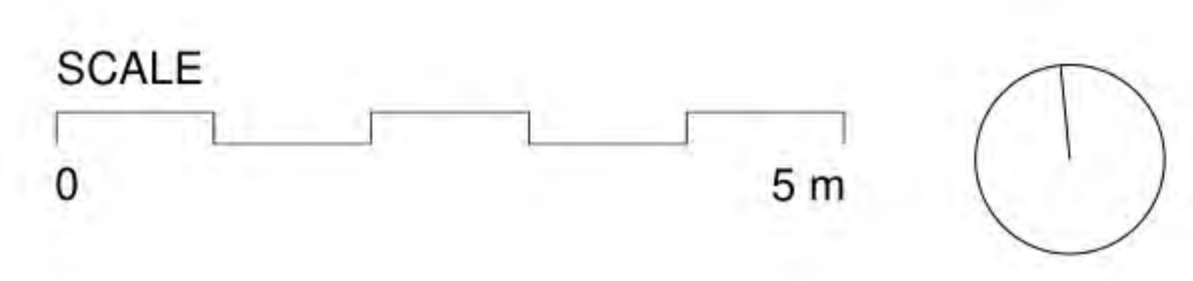
Project:  
**18a Frogna Gardens**

Client:  
**Roger Pilgrim & Nadine Majaro**

Project Number:  
**2473** Status:  
**For Approval**

Drawing Title:  
**Floor plan - Ground Floor Upper**

Date:	12/10/2020 16:18:50	Drawn:	AK
Scale:	1 : 100 @A1	Checked:	NB
	1 : 200 @A3		
Drawing No:	ABA-2473-20-003		Rev:





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CONSULTING ENGINEERS

# 18A FROGNAL GARDENS DRAINAGE REPORT

OCTOBER 2020

EEP REF: 3849

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# CONTENTS

<b>INTRODUCTION</b>	<b>1</b>
<b>SURFACE AREA CALCULATION – EXISTING AND PROPOSED</b>	<b>2</b>
<b>RUN-OFF RATE CALCULATIONS</b>	<b>4</b>
<b>ATTENUATION TANK CAPACITY CALCULATIONS</b>	<b>5</b>
<b>PROTECTED TREE ROOT ZONE</b>	<b>6</b>
<b>RAINWATER ATTENUATION</b>	<b>7</b>
<b>CONCLUSIONS</b>	<b>8</b>

## APPENDIX – CCTV SURVEY REPORT

Author	Revision	Date
TSD	A	16 October 2020
TSD	B	29 October 2020



# INTRODUCTION

Where projects are proposing to incorporate a below ground level basement, in accordance with the Camden Local Plan these projects are required to submit a drainage report where the following information is required:

- Identification of flood risk (by Akera Engineers)
- Assessment of existing run-off rates
- Calculation of greenfield run-off rates
- Identification of measures, in line with the drainage hierarchy, to reduce run-off rates
- Calculation of proposed run-off rates

## Existing Drainage Connection

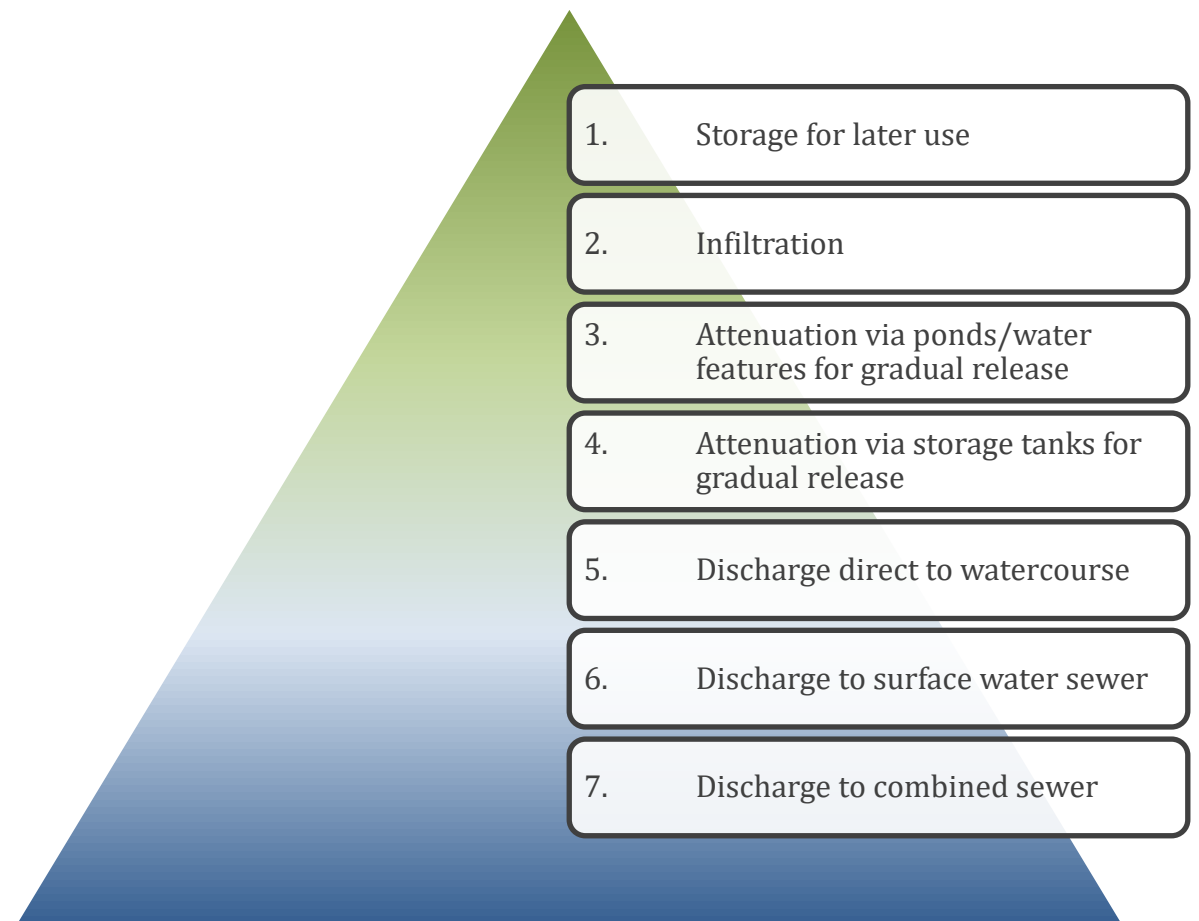
Currently, the rainwater drainage plus the soil and waste drainage from the building are combined and discharge directly to the Thames Water Sewer located beneath the Frognaal Gardens road, the drainage combines within an existing manhole located within the front of house private drive/car parking area.

Accordingly, as it is known that the existing connection to the sewer is via a 'combined' drain, which has been confirmed to be Ø150 mm. However, the drainage connection from 18A connects to the drainage from 18B (Ø100 mm pipework) before connecting to the sewer. The connection between the two buildings can be seen at the manhole located on the property of 18B.

Please see a recent CCTV report of the existing drainage system in the Appendix of this report.

It is assumed that the existing rainwater drainage system would have been designed using a rainfall intensity of 75mm/hour.

## Drainage Hierarchy



# SURFACE AREA CALCULATION – EXISTING AND PROPOSED

Existing Areas m <sup>2</sup>		
GF	18.8	Drains to garden
	131.0	Garden
	47.9	
	71.1	Drains to street
	30.2	Garden
Roof	104.6	

Proposed Areas m <sup>2</sup>		
GF Lower	43.7	Drains to street
	4.5	
	11.1	Garden
GF Upper	131.1	Garden
	28.0	
	26.1	17.0m <sup>2</sup> Green Roof
01	12.9	
02	33.1	19.3m <sup>2</sup> Green Roof
	13.2	
Roof	99.9	
Total	403.6	

<b>Total</b>	403.6
--------------	-------

<b>161.2m<sup>2</sup> Garden</b>
----------------------------------

<b>Impermeable</b>	152.5
--------------------	-------

<b>Permeable</b>	180.0
------------------	-------

<b>To street</b>	71.1
------------------	------

<b>131.1m<sup>2</sup> Garden</b>
----------------------------------

<b>36.3m<sup>2</sup> Green Roof</b>
-------------------------------------

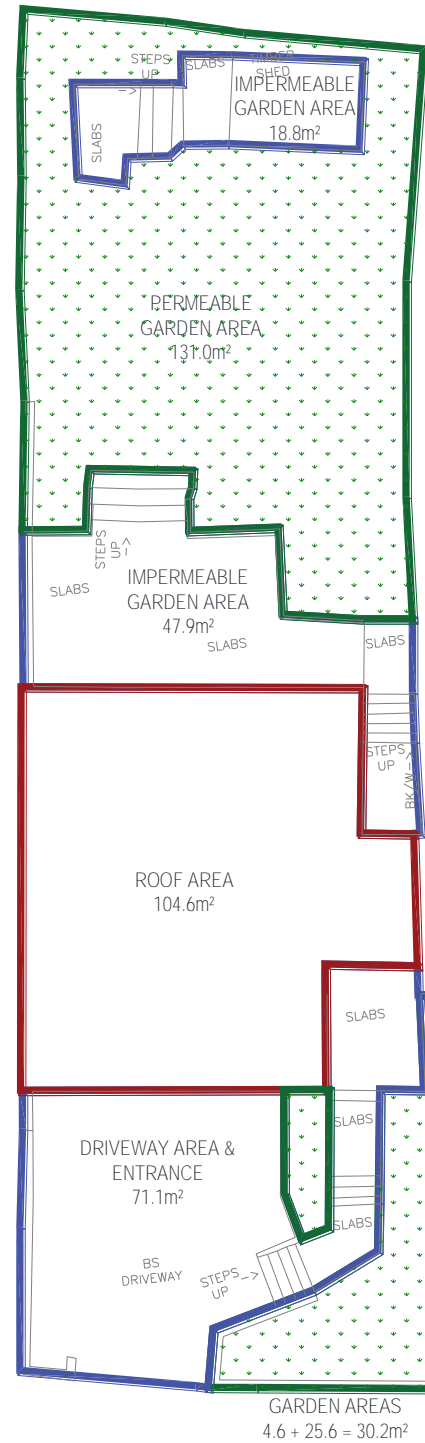
<b>Impermeable</b>	158.5
--------------------	-------

<b>Permeable</b>	142.2
------------------	-------

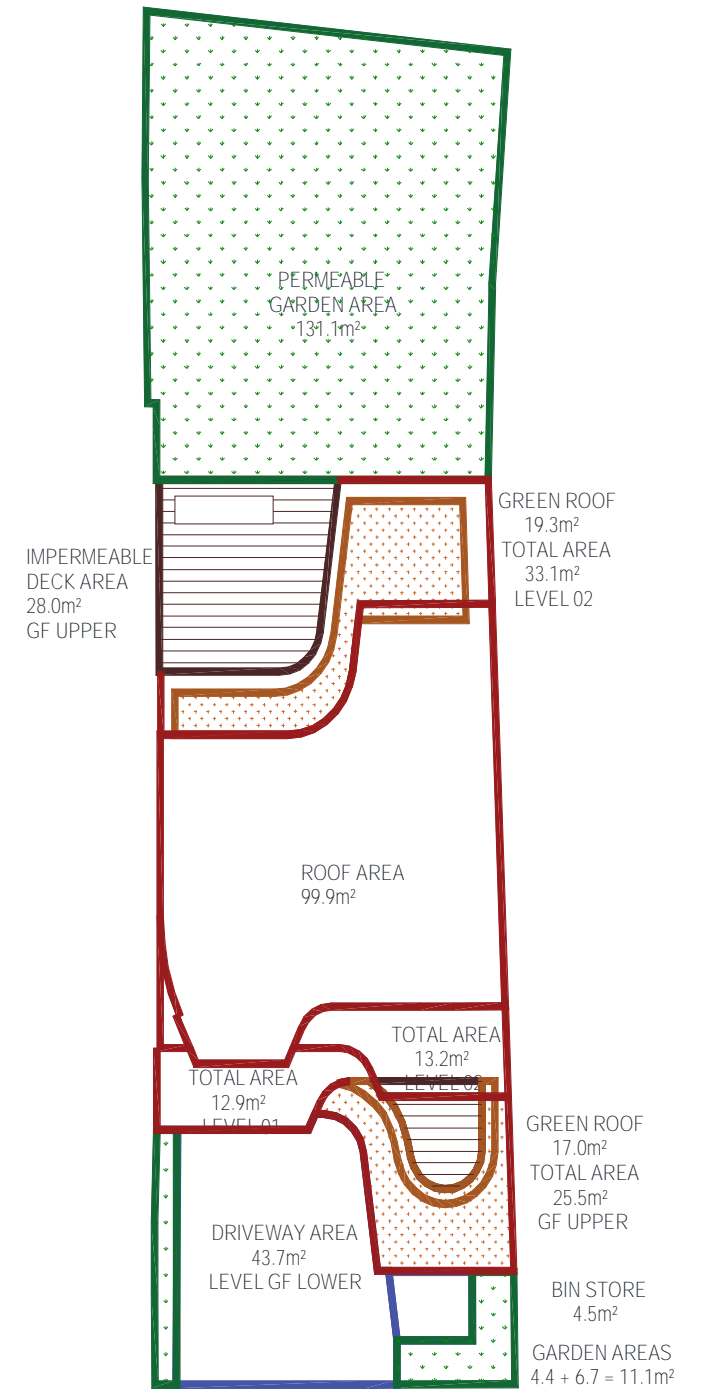
<b>Semi Permeable</b>	59.2
-----------------------	------

<b>To street</b>	43.7
------------------	------

Existing



Proposed





## SURFACE AREA CALCULATION – EXISTING AND PROPOSED

### Existing Building:

a) Impermeable area	=	152.5m <sup>2</sup>
b) Permeable area	=	180.0m <sup>2</sup>
c) Discharges to street	=	71.1m <sup>2</sup>
<b>Total</b>		<b>403.6m<sup>2</sup></b>

### Proposed Building:

c) Impermeable area	=	158.5m <sup>2</sup>
d) Permeable area	=	142.2m <sup>2</sup>
e) Semi-permeable Green Roof area	=	59.2m <sup>2</sup>
f) Discharges to street	=	48.2m <sup>2</sup>
<b>Total</b>		<b>403.6m<sup>2</sup></b>

As can be seen from table 6 within the CIBSE Guide KS11 the rainfall water retention will be 50% (TBC) which affectively increases the “permeable area” by 29.6 m<sup>2</sup> (59.2 m<sup>2</sup> ÷ 2 = 29.6 m<sup>2</sup> or 50%), therefore the new site areas simplified for run-off calculation purposes we can adjust the areas as follows:-

### Proposed Building (Simplified):

f) Impermeable area	=	188.1m <sup>2</sup> (158.5 + 29.6)
g) Permeable area	=	171.8m <sup>2</sup> (142.2 + 29.6)
h) Discharges to street	=	48.2m <sup>2</sup>
<b>Total</b>		<b>403.6m<sup>2</sup></b>

Substrate depth / mm	Vegetation	Average annual water retention / %	Average annual rainfall run off / %
20–40	Moss, sedums	40	60
40–60	Sedums and moss	45	55
60–100	Sedums, moss and herbs	50	50
100–150	Sedums, herbs and grass	55	45
150–200	Grass and herbs	60	40

Water retention in extensive green roofs (based on 650–800 mm annual rainfall).  
CIBSE KS11 – Green Roofs, Table 6.

# RUN-OFF RATE CALCULATIONS

The rainfall intensity stipulated within Clause 3.8 of the March 2019 version of the 'Camden Planning Guidance – Water & Flooding' for a residential development the required 'Protection Years' are for a 100 year return period, using BS EN 12056-3 this results in a design intensity of 250mm/hour (0.069 litres/second/metre<sup>2</sup>).

Run-off Calculations			
		Area m <sup>2</sup>	Run-off l/s
Existing	Impermeable	152.5	10.52
	Permeable	180.0	12.42
Proposed	Impermeable	188.1	12.98
	Permeable	171.8	11.85

23%	% Change
-----	----------

## Rainfall intensity calculations for 18a FROGNAL GARDENS, LONDON.

Based on Category 2 values from BS EN 12056 part 3

BASIC DATA	
Nearest geographical town	London
Building life span required	100 years

Calculations data based on BS EN 12056 part 3 Category 2			
Protection years (T) (1.5 x life span)	150	years	
Fig. NB.6 value (return period in years)	4.5	(based on 2min M5)	
From Table NB.1, fraction for 2 min. storm = 1.00			
Therefore 2 min. M5 rainfall =	4.5	X	1 = 4.5
Factor from Fig. NB.7 using protection years	150	(M5=2)	= 1.9
Using return period year factor for 2 min M5 =	1.85	X	4.5 = 8.325

Calculated Flowrates			
Rainfall intensity in mm/hour	30	X	8.325 = 250 mm/hour
Run off in litres per second	0.069	per square metre	



# ATTENUATION TANK CAPACITY CALCULATIONS

In order to maintain the building's original rainwater discharge to the sewer any design for the attenuation and controlled release of rainwater shall not exceed the discharge rate of the original design. It is assumed that the rainfall intensity used for the original design was based on 75mm per hour/m<sup>2</sup>.

Therefore, following the guidance from the Camden Planning Guidance documents and methodology provided in the BRE Digest 365 – Soakaway Design, and The Wallingford Procedure, the following equations can be used to size the rainwater attenuation tank:

Run-off Calculations Based on original building design (75mm/Hr/m <sup>2</sup> )		
	Area m <sup>2</sup>	Run-off l/s
Impermeable	152.5	3.20

maximum allowable discharge to sewer

## NOMENCLATURE

$MX-D_{min}$ :  $X$ =return period (years)  
 $D$ =storm duration (min)

Z1: rainfall factor taken from figure 1 and table 1 – BRE Digest 365

Z2: growth factor taken from table 2 – BRE Digest 365

$d$  = discharge rate(l/s)

$T$  = time (s)

$I$  = inflow (m<sup>3</sup>)

$O$  = outflow (m<sup>3</sup>)

$S$  = storage (m<sup>3</sup>)

## EQUATIONS

$$M5-D_{min} = M5-60_{min} \text{ rainfall} \times Z1$$

$$M10-D_{min} = M5-D_{min} \times Z2$$

$$O = d \times M10-D_{min}$$

$$I = d \times T$$

$$I_{140\%} = I \times 1.4$$

$$S = I_{140\%} - O$$

Area m <sup>2</sup>	Duration	Rainfall factor Z1	M5 rainfalls mm	Growth factor Z2 (M10)	M10 year rainfall mm	Growth factor Z2 (M100)	M100 year rainfall mm	M100 year rainfall + 40% mm	Inflow m <sup>3</sup>	Inflow (@140%) m <sup>3</sup>	Outflow m <sup>3</sup>	Storage required m <sup>3</sup>
188.1	5 mins	0.38	7.6	1.19	9.0	1.96	14.9	20.9	2.8	3.9	1.0	3.0
	10 mins	0.53	10.6	1.22	12.9	2.00	21.2	29.7	4.0	5.6	1.9	3.7
	15 mins	0.64	12.8	1.24	15.9	1.96	25.1	35.1	4.7	6.6	2.9	3.7
	30 mins	0.81	16.2	1.24	20.1	2.00	32.4	45.4	6.1	8.5	5.8	2.8
	1 hour	1.00	20	1.24	24.8	2.03	40.6	56.8	7.6	10.7	11.5	0.0
	2 hours	1.20	24	1.22	29.3	2.01	48.2	67.5	9.1	12.7	23.1	0.0
	4 hours	1.42	28.4	1.19	33.8	1.97	55.9	78.3	10.5	14.7	46.1	0.0
	6 hours	1.57	31.4	1.17	36.7	1.96	61.5	86.2	11.6	16.2	69.2	0.0
	10 hours	1.74	34.8	1.14	39.7	1.92	66.8	93.5	12.6	17.6	115.3	0.0
24 hours	2.16	43.2	1.13	48.8	1.86	80.4	112.5	15.1	21.2	276.7	0.0	



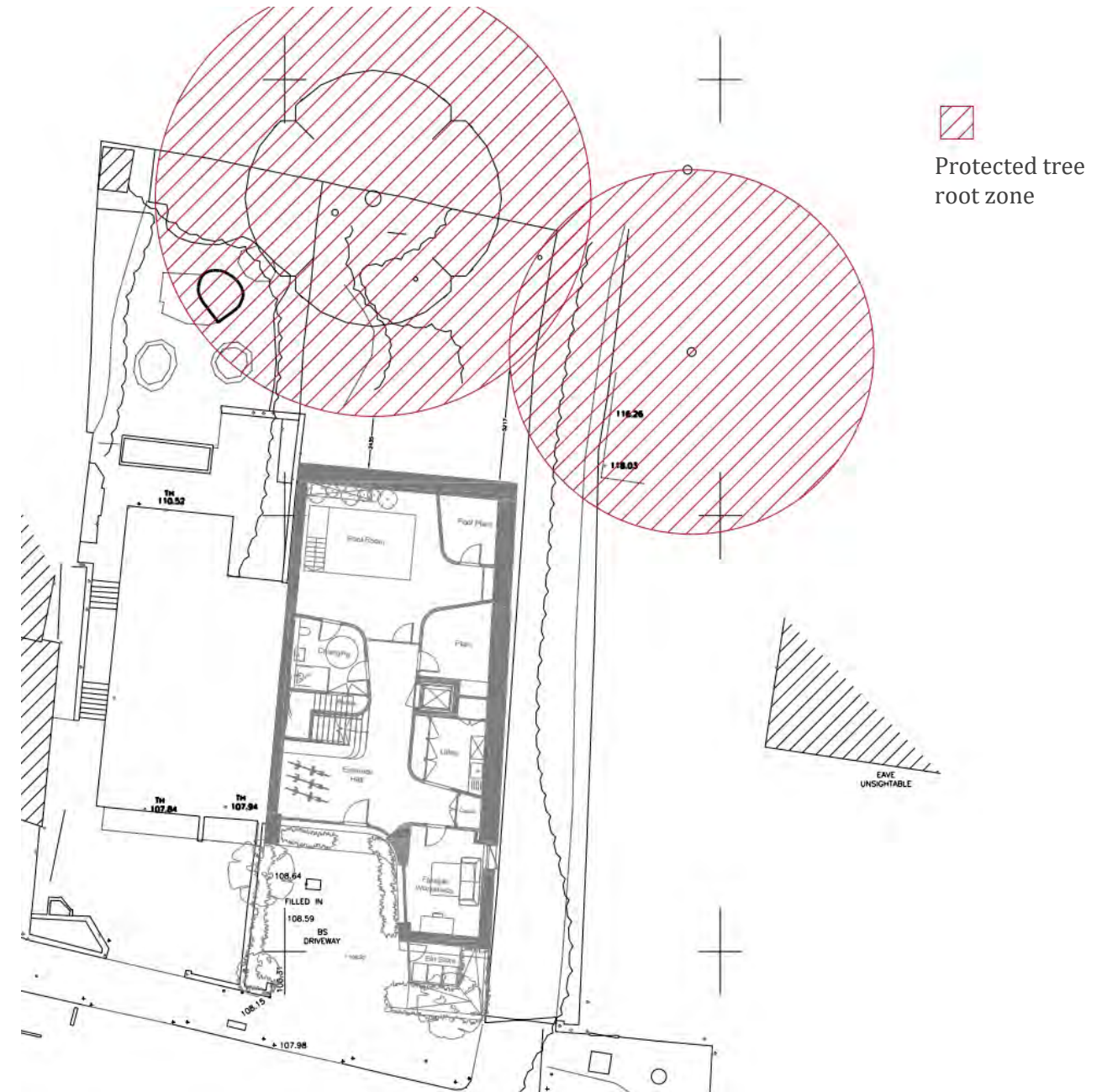
# PROTECTED TREE ROOT ZONE

At 18A Frognal Gardens at the rear of the property are a number of fully established trees, a soakaway, if used, must be located outside of the root protection zone.

Building Regulations Part H and good practice requires that any soakaway be located not closer than 5m to the nearest building and section 3.20 within the 'Camden Planning Guidance – Water & Flooding' states any infiltration measures located within 5m must be designed to avoid harm to the building, in accordance with the Building Regulations.

A survey of the existing root area shows that distance of the building from the root protection zone varies from approximately 2.4m to 5.2m, this provides little or no room for the inclusion of a soakaway system of any meaningful size.

Therefore, rainwater run-off and drainage shall be addressed using a combination of solutions to be discussed in the sections to follow.



# RAINWATER INFILTRATION & ATTENUATION

The proposed architectural design shows extensive green roofing to be installed to some terrace and roof areas, however, it is noted that section 3.14 within the 'Camden Planning Guidance – Water & Flooding' states:

*However, green roofs cannot be considered a permeable soil and should be assumed to be saturated at the point of intense storms (i.e. storms that are more intense than a 1 in 10 year storm). Due to the sporadic nature of water consumption, rainwater harvesting tanks should also be assumed to be full at the point of a storm event. Both of these systems are generally not intended to control peak run-off rate during critical events, and are mainly useful during medium and small events to capture run-off and thus reduce the volume of water entering the drainage system during these smaller events.*

But section 3.15 also states:

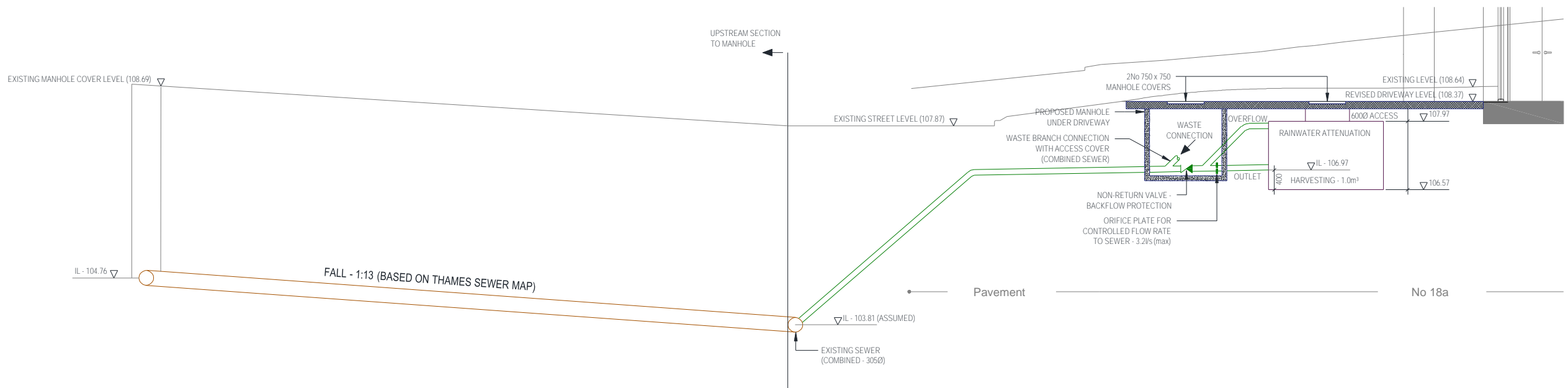
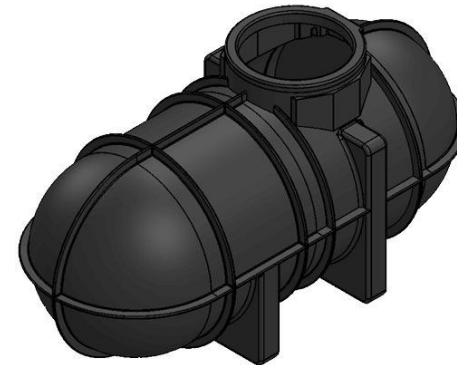
*Some rainwater harvesting tanks can incorporate an attenuation chamber/ overflow with controlled release, and green roofs can incorporate an attenuation layer ("blue roof") or be designed to be substantially thick, allowing the associated attenuation volume to be included within the modelling. The Council will consider inclusion of these SuDS in developments favourably due to their additional environmental benefits.*

Therefore, the proposal for mitigating the impact of the proposed development to the local sewer network shall be through the attenuation and controlled release of surface water to the sewer. The discharge to the sewer shall be designed to meet the criteria used for the original building, therefore, any additional impact due to climate and increased surface run-off shall be dealt with on site.

The inclusion of several areas of "green roofing" shall serve to provide additional attenuation to the sewer, with the guidance provided in CIBSE Guide KS11, 50% of these areas have been included in the sizing of the attenuation tank.

In order to facilitate the sustainability ambitions of the project, and in line with the drainage hierarchy, it is proposed to maintain a level of water at the bottom of the tank for the provision of harvested rainwater to be reused for irrigation of the green roofs and landscape gardens.

This will require the addition of submersible pumps to the tank that will be serviceable from the manhole cover provided. The tank shall not include a mains water backup, therefore, at times when the tank is empty irrigation will need to come from a Category 5 protected mains water supply.



## CONCLUSIONS

Due to the revised layout of 18A Froggnal Gardens the surface water run-off is expected to increase by 23% when compared with the volume currently coming from the building.

Due to this increase, and in order to meet the expectations of the Camden Policy Guidance documents, the following measures are proposed to relieve pressure on the local drainage system:

- Green roof attenuation – to control the flow of rainwater from the building
- Rainwater attenuation (3.7m<sup>3</sup> minimum) and controlled release – a hybrid underground system located to the front of the building that will be used to control the flow discharging to the combined sewer with additional harvesting capacity for reuse through irrigation.

With these measures in place we expect to mitigate the impact of any changes to the impermeable run-off surfaces whilst also addressing the future demands owing to climate change. The discharge rate from the attenuation tank shall be designed to be no worse than the original peak discharge for the current building's original design (based on 75mm/Hr/m<sup>2</sup>).



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CONSULTING ENGINEERS

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# APPENDIX – CCTV SURVEY REPORT







## Table of Contents

Project Name	Project Number	Project Date
04.09.19 18A Frogmal Gardens, London		04/09/2019

Project Information .....	P-1
Section: 1; MH1 > MH2 (MH1X) .....	1
Section: 2; A/MH1 > MH1 (A/MH1X) .....	3
Section: 3; MH2 > D/SMH2 (MH2X) .....	5
Section: 4; JUNCTION > D/S JN (JUNCTIONX) .....	7



## Project Information

Project Name	Project Number	Project Date
04.09.19 18A Frogna Gardens, London		04/09/2019

### Client

**Company:** Environmental Engineering Partnership  
**Street:** The Chapel House, High Street  
**Town or City:** West Wycombe, HP14 3AG

### Site

**Company:** EEP  
**Street:** 18A Frogna Gardens  
**Town or City:** London, NW3 6XA

### Contractor

**Company:** Aqua-Jet Specialist Drainage Contractors Ltd  
**Contact:** Rob Wilkinson  
**Street:** Yard 21 Hilton Ind Est, Sutton Lane  
**Town or City:** Hilton, Derbyshire, DE65 5FE  
**Phone:** 01283 730333  
**Email:** aquajetltd@aol.com

## Section Inspection - 04/09/2019 - MH1X

Section 1	Inspection 1	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR MH1X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	MH1
Road:	18A Frognal Gardens	Inspected Length:	10.00 m	Upstream Pipe Depth:	
Location:		Total Length:	10.00 m	Downstream Node:	MH2
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Cast iron		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

Comments:  
 Recommendations:

Scale:	1:87	Position [m]	Code	Observation	MPEG	Photo	Grade																																			
<div style="display: flex; align-items: center;"> <div style="margin-right: 20px;"> <p>Depth: m</p> <p>MH1</p> <p>Depth: m</p> </div> <table border="1" style="margin-left: 20px; border-collapse: collapse;"> <tr> <td style="width: 10%;">0.00</td> <td style="width: 10%;">MH</td> <td style="width: 40%;">Start node type, manhole, reference number: MH1</td> <td style="width: 10%;">00:00:00</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="width: 10%;">0.00</td> <td style="width: 10%;">WL</td> <td style="width: 40%;">Water level, 0% of the vertical dimension</td> <td style="width: 10%;">00:00:01</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="width: 10%;">0.10</td> <td style="width: 10%;">S01</td> <td style="width: 40%;">DEE Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION</td> <td style="width: 10%;">00:00:06</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="width: 10%;">9.90</td> <td style="width: 10%;">F01</td> <td style="width: 40%;">DEE Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION</td> <td style="width: 10%;">00:01:22</td> <td></td> <td></td> <td style="width: 10%;">2</td> </tr> <tr> <td style="width: 10%;">10.00</td> <td style="width: 10%;">MHF</td> <td style="width: 40%;">Finish node type, manhole, reference number: MH2</td> <td style="width: 10%;">00:01:23</td> <td></td> <td></td> <td></td> </tr> </table> </div>								0.00	MH	Start node type, manhole, reference number: MH1	00:00:00				0.00	WL	Water level, 0% of the vertical dimension	00:00:01				0.10	S01	DEE Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:06				9.90	F01	DEE Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22			2	10.00	MHF	Finish node type, manhole, reference number: MH2	00:01:23			
0.00	MH	Start node type, manhole, reference number: MH1	00:00:00																																							
0.00	WL	Water level, 0% of the vertical dimension	00:00:01																																							
0.10	S01	DEE Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:06																																							
9.90	F01	DEE Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22			2																																				
10.00	MHF	Finish node type, manhole, reference number: MH2	00:01:23																																							

Structural Defects

Construction Features

Service & Operational Observations

Miscellaneous Features

STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	1.0	1.0	10.0	2.0

### Section Pictures - 04/09/2019 - MH1X

Section	Inspection Direction	PLR	Client's Job Ref	Contractor's Job Ref
1	Downstream	MH1X		



MH1X\_697d6ba7-1a86-43ea-9b00-4985f68a1723\_20190906\_095824\_558.jpg, 00:00:06, 0.10 m  
Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start

## Section Inspection - 04/09/2019 - A/MH1X

Section 2	Inspection 2	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR A/MH1X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village: London	Inspection Direction: Upstream	Upstream Node: A/MH1
Road: 18A Frognal Gardens	Inspected Length: 7.50 m	Upstream Pipe Depth:
Location:	Total Length: 7.50 m	Downstream Node: MH1
Surface Type:	Joint Length: 0.00 m	Downstream Pipe Depth:
Use: Combined	Pipe Shape: Circular	
Type of Pipe: Gravity drain/sewer	Dia/Height: 100 mm	
Year Constructed:	Pipe Material: Cast iron	
Flow Control: No flow control	Lining Type: No Lining	
Inspection Purpose:	Lining Material: No Lining	

**Comments:**  
**Recommendations:**

Scale:	1:66	Position [m]	Code	Observation	MPEG	Photo	Grade
		0.00	MH	Start node type, manhole, reference number: MH1	00:00:00		
		0.00	WL	Water level, 5% of the vertical dimension	00:00:01		
		0.10	S01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:03		
		7.40	F01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22		2
		7.50	MHF	Finish node type, manhole, reference number: A/MH1	00:01:22		

Structural Defects					Construction Features				
Service & Operational Observations					Miscellaneous Features				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	1.0	1.1	8.0	2.0

**Section Pictures - 04/09/2019 - A/MH1X**

Section 2	Inspection Direction Upstream	PLR A/MH1X	Client's Job Ref	Contractor's Job Ref
--------------	----------------------------------	---------------	------------------	----------------------



A\_MH1X\_7069cf84-8557-4d21-aaf6-a844871a4e0a\_20190906\_100331\_033.jpg, 00:00:03, 0.10 m  
 Attached deposits, encrustation from 12 o'clock to 12 o'clock,  
 5% cross-sectional area loss, start

## Section Inspection - 04/09/2019 - MH2X

Section 3	Inspection 3	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR MH2X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	MH2
Road:	18A Frognal Gardens	Inspected Length:	7.30 m	Upstream Pipe Depth:	
Location:		Total Length:	7.30 m	Downstream Node:	D/S MH2
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Vitrified clay pipe (i.e. all clayware)		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale:	1:64	Position [m]	Code	Observation	MPEG	Photo	Grade																																																
<div style="display: flex; align-items: flex-start;"> <div style="flex: 1;"> <p>Depth: m MH2</p> </div> <table border="1" style="margin-left: 10px; border-collapse: collapse;"> <tr> <td style="text-align: right;">0.00</td> <td style="text-align: left;">MH</td> <td style="text-align: left;">Start node type, manhole, reference number: MH2: SURVEY THROUGH TOP ACCESS HOLE OF TRAP</td> <td style="text-align: right;">00:00:00</td> <td></td> <td></td> </tr> <tr> <td style="text-align: right;">0.00</td> <td style="text-align: left;">WL</td> <td style="text-align: left;">Water level, 5% of the vertical dimension</td> <td style="text-align: right;">00:00:01</td> <td></td> <td></td> </tr> <tr> <td style="text-align: right;">0.20</td> <td style="text-align: left;">JN</td> <td style="text-align: left;">Junction at 6 o'clock, diameter: 100mm: BOTTOM OUTLET OF TRAP</td> <td style="text-align: right;">00:00:09</td> <td></td> <td></td> </tr> <tr> <td style="text-align: right;">0.30</td> <td style="text-align: left;">SC</td> <td style="text-align: left;">Size changes, new size(s), 150mm high</td> <td style="text-align: right;">00:00:15</td> <td></td> <td></td> </tr> <tr> <td style="text-align: right;">1.80</td> <td style="text-align: left;">CCJ</td> <td style="text-align: left;">Crack, circumferential at joint from 8 o'clock to 3 o'clock</td> <td style="text-align: right;">00:00:33</td> <td></td> <td style="text-align: right;">2</td> </tr> <tr> <td style="text-align: right;">2.70</td> <td style="text-align: left;">LD</td> <td style="text-align: left;">Line deviates down</td> <td style="text-align: right;">00:00:41</td> <td></td> <td></td> </tr> <tr> <td style="text-align: right;">6.80</td> <td style="text-align: left;">LR</td> <td style="text-align: left;">Line deviates right</td> <td style="text-align: right;">00:01:23</td> <td></td> <td></td> </tr> <tr> <td style="text-align: right;">7.30</td> <td style="text-align: left;">SA</td> <td style="text-align: left;">Survey abandoned: JOINS MAIN BLIND</td> <td style="text-align: right;">00:01:28</td> <td></td> <td></td> </tr> </table> </div>								0.00	MH	Start node type, manhole, reference number: MH2: SURVEY THROUGH TOP ACCESS HOLE OF TRAP	00:00:00			0.00	WL	Water level, 5% of the vertical dimension	00:00:01			0.20	JN	Junction at 6 o'clock, diameter: 100mm: BOTTOM OUTLET OF TRAP	00:00:09			0.30	SC	Size changes, new size(s), 150mm high	00:00:15			1.80	CCJ	Crack, circumferential at joint from 8 o'clock to 3 o'clock	00:00:33		2	2.70	LD	Line deviates down	00:00:41			6.80	LR	Line deviates right	00:01:23			7.30	SA	Survey abandoned: JOINS MAIN BLIND	00:01:28		
0.00	MH	Start node type, manhole, reference number: MH2: SURVEY THROUGH TOP ACCESS HOLE OF TRAP	00:00:00																																																				
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Structural Defects				Construction Features																																																			
Service & Operational Observations				Miscellaneous Features																																																			
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade																																														
1	10.0	1.4	10.0	2.0	0	0.0	0.0	0.0	1.0																																														

**Section Pictures - 04/09/2019 - MH2X**

Section 3	Inspection Direction Downstream	PLR MH2X	Client's Job Ref	Contractor's Job Ref
--------------	------------------------------------	-------------	------------------	----------------------



MH2X\_99a95e93-e9bd-4658-b633-a5a8b0b76c35\_20190906  
 \_101510\_209.jpg, 00:00:33, 1.80 m  
 Crack, circumferential at joint from 8 o'clock to 3 o'clock



## Section Inspection - 04/09/2019 - JUNCTIONX

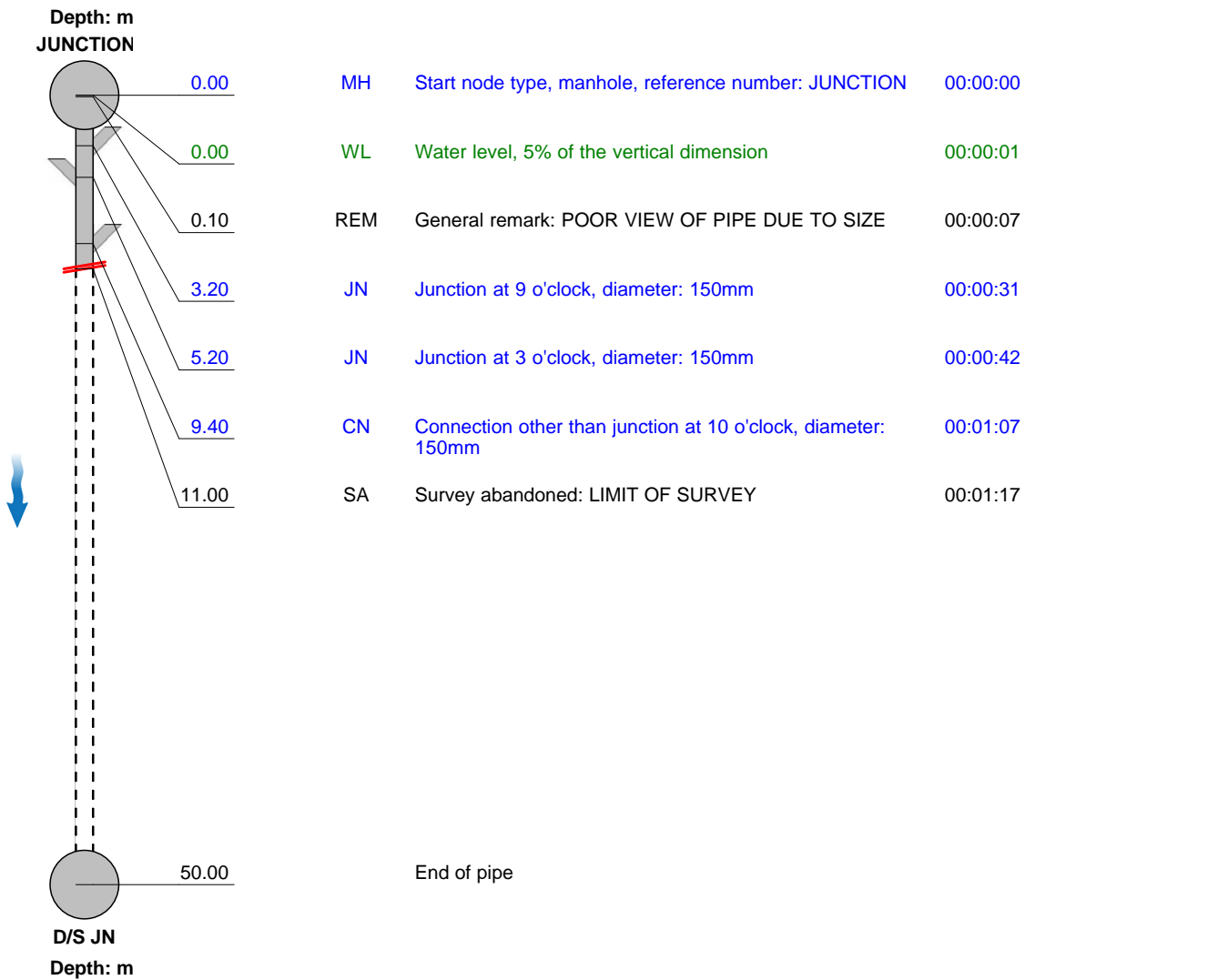
Section 4	Inspection 4	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned N	PLR JUNCTIONX
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	JUNCTION
Road:	18A Frognal Gardens	Inspected Length:	11.00 m	Upstream Pipe Depth:	
Location:		Total Length:	50.00 m	Downstream Node:	D/S JN
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	300 mm		
Year Constructed:		Pipe Material:	Vitrified clay pipe (i.e. all clayware)		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**

**Recommendations:**

Scale: 1:435    Position [m]    Code    Observation    MPEG    Photo    Grade



Structural Defects

Construction Features

Service & Operational Observations

Miscellaneous Features

STR No.	Def	STR Peak	STR Mean	STR Total	STR Grade	SER No.	Def	SER Peak	SER Mean	SER Total	SER Grade
0		0.0	0.0	0.0	1.0	0		0.0	0.0	0.0	1.0

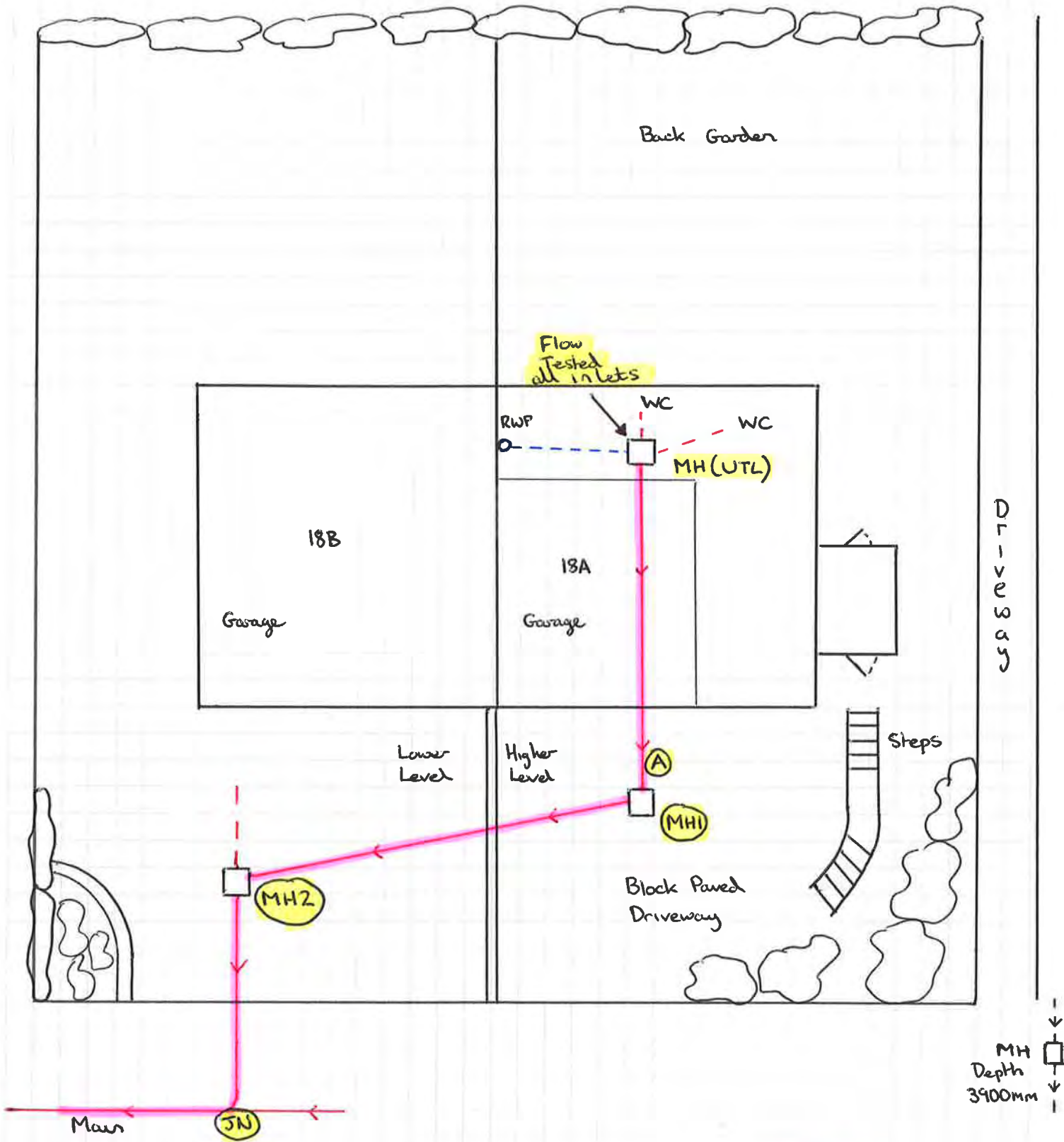
### Manhole Information

REFERENCE: <b>MH 1</b>	DUTY: <b>CB</b>	REFERENCE: <b>MH2</b>	DUTY: <b>CB</b>
DIAGRAM: 		DIAGRAM: 	
DEPTH AT OUTLET: <b>1740mm</b>		DEPTH AT OUTLET: <b>1400mm</b>	
MH SIZE <b>900mm x 500mm</b>		MH SIZE <b>950mm x 600mm</b>	
MH MATERIAL <b>Brick / Render</b>		MH MATERIAL <b>Brick</b>	
OBSERVATIONS/ COMMENTS:		OBSERVATIONS/ COMMENTS:	
REFERENCE:	DUTY:	REFERENCE:	DUTY:
DIAGRAM:		DIAGRAM:	
DEPTH AT OUTLET:		DEPTH AT OUTLET:	
MH SIZE		MH SIZE	
MH MATERIAL		MH MATERIAL	
OBSERVATIONS/ COMMENTS:		OBSERVATIONS/ COMMENTS:	

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# APPENDIX – CCTV SURVEY REPORT





## Table of Contents

Project Name	Project Number	Project Date
04.09.19 18A Frogmal Gardens, London		04/09/2019

Project Information .....	P-1
Section: 1; MH1 > MH2 (MH1X) .....	1
Section: 2; A/MH1 > MH1 (A/MH1X) .....	3
Section: 3; MH2 > D/SMH2 (MH2X) .....	5
Section: 4; JUNCTION > D/S JN (JUNCTIONX) .....	7



## Project Information

Project Name	Project Number	Project Date
04.09.19 18A Frogna Gardens, London		04/09/2019

### Client

**Company:** Environmental Engineering Partnership  
**Street:** The Chapel House, High Street  
**Town or City:** West Wycombe, HP14 3AG

### Site

**Company:** EEP  
**Street:** 18A Frogna Gardens  
**Town or City:** London, NW3 6XA

### Contractor

**Company:** Aqua-Jet Specialist Drainage Contractors Ltd  
**Contact:** Rob Wilkinson  
**Street:** Yard 21 Hilton Ind Est, Sutton Lane  
**Town or City:** Hilton, Derbyshire, DE65 5FE  
**Phone:** 01283 730333  
**Email:** aquajetltd@aol.com

## Section Inspection - 04/09/2019 - MH1X

Section 1	Inspection 1	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR MH1X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	MH1
Road:	18A Frognal Gardens	Inspected Length:	10.00 m	Upstream Pipe Depth:	
Location:		Total Length:	10.00 m	Downstream Node:	MH2
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Cast iron		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale:	1:87	Position [m]	Code	Observation	MPEG	Photo	Grade																				
<div style="display: flex; align-items: center;"> <div style="flex: 1;"> <p style="text-align: center;">Depth: m</p> <p style="text-align: center;">MH1</p> <p style="text-align: center;">Depth: m</p> </div> <table border="1" style="margin-left: 20px; border-collapse: collapse;"> <tr> <td style="width: 10%;">0.00</td> <td style="width: 10%;">MH</td> <td style="width: 40%;">Start node type, manhole, reference number: MH1</td> <td style="width: 10%;">00:00:00</td> </tr> <tr> <td style="width: 10%;">0.00</td> <td style="width: 10%;">WL</td> <td style="width: 40%;">Water level, 0% of the vertical dimension</td> <td style="width: 10%;">00:00:01</td> </tr> <tr> <td style="width: 10%;">0.10</td> <td style="width: 10%;">S01 DEE</td> <td style="width: 40%;">Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION</td> <td style="width: 10%;">00:00:06</td> </tr> <tr> <td style="width: 10%;">9.90</td> <td style="width: 10%;">F01 DEE</td> <td style="width: 40%;">Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION</td> <td style="width: 10%;">00:01:22</td> </tr> <tr> <td style="width: 10%;">10.00</td> <td style="width: 10%;">MHF</td> <td style="width: 40%;">Finish node type, manhole, reference number: MH2</td> <td style="width: 10%;">00:01:23</td> </tr> </table> </div>								0.00	MH	Start node type, manhole, reference number: MH1	00:00:00	0.00	WL	Water level, 0% of the vertical dimension	00:00:01	0.10	S01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:06	9.90	F01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22	10.00	MHF	Finish node type, manhole, reference number: MH2	00:01:23
0.00	MH	Start node type, manhole, reference number: MH1	00:00:00																								
0.00	WL	Water level, 0% of the vertical dimension	00:00:01																								
0.10	S01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:06																								
9.90	F01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22																								
10.00	MHF	Finish node type, manhole, reference number: MH2	00:01:23																								

Structural Defects					Construction Features				
Service & Operational Observations					Miscellaneous Features				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	1.0	1.0	10.0	2.0

### Section Pictures - 04/09/2019 - MH1X

Section	Inspection Direction	PLR	Client's Job Ref	Contractor's Job Ref
1	Downstream	MH1X		



MH1X\_697d6ba7-1a86-43ea-9b00-4985f68a1723\_20190906\_095824\_558.jpg, 00:00:06, 0.10 m  
Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start

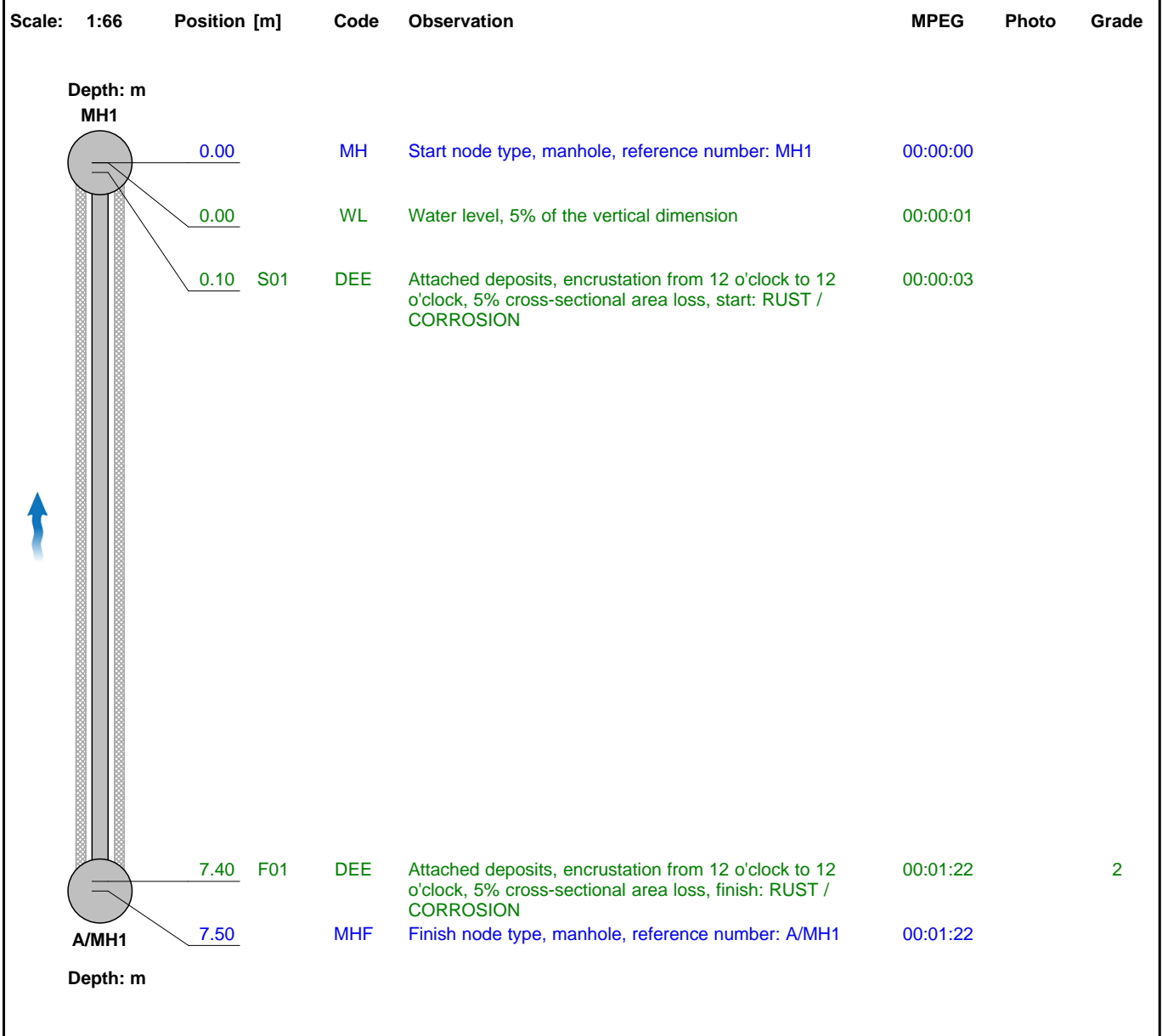


## Section Inspection - 04/09/2019 - A/MH1X

Section 2	Inspection 2	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR A/MH1X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Upstream	Upstream Node:	A/MH1
Road:	18A Frognal Gardens	Inspected Length:	7.50 m	Upstream Pipe Depth:	
Location:		Total Length:	7.50 m	Downstream Node:	MH1
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Cast iron		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**



Structural Defects					Construction Features				
Service & Operational Observations					Miscellaneous Features				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	1.0	1.1	8.0	2.0

**Section Pictures - 04/09/2019 - A/MH1X**

Section 2	Inspection Direction Upstream	PLR A/MH1X	Client's Job Ref	Contractor's Job Ref
--------------	----------------------------------	---------------	------------------	----------------------



A\_MH1X\_7069cf84-8557-4d21-aaf6-a844871a4e0a\_20190906\_100331\_033.jpg, 00:00:03, 0.10 m  
 Attached deposits, encrustation from 12 o'clock to 12 o'clock,  
 5% cross-sectional area loss, start

## Section Inspection - 04/09/2019 - MH2X

Section 3	Inspection 3	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR MH2X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	MH2
Road:	18A Frognal Gardens	Inspected Length:	7.30 m	Upstream Pipe Depth:	
Location:		Total Length:	7.30 m	Downstream Node:	D/S MH2
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Vitrified clay pipe (i.e. all clayware)		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale:	1:64	Position [m]	Code	Observation	MPEG	Photo	Grade
		Depth: m MH2					
		0.00	MH	Start node type, manhole, reference number: MH2: SURVEY THROUGH TOP ACCESS HOLE OF TRAP	00:00:00		
		0.00	WL	Water level, 5% of the vertical dimension	00:00:01		
		0.20	JN	Junction at 6 o'clock, diameter: 100mm: BOTTOM OUTLET OF TRAP	00:00:09		
		0.30	SC	Size changes, new size(s), 150mm high	00:00:15		
		1.80	CCJ	Crack, circumferential at joint from 8 o'clock to 3 o'clock	00:00:33		2
		2.70	LD	Line deviates down	00:00:41		
		6.80	LR	Line deviates right	00:01:23		
		7.30	SA	Survey abandoned: JOINS MAIN BLIND	00:01:28		

Structural Defects					Construction Features				
Service & Operational Observations					Miscellaneous Features				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
1	10.0	1.4	10.0	2.0	0	0.0	0.0	0.0	1.0

**Section Pictures - 04/09/2019 - MH2X**

Section 3	Inspection Direction Downstream	PLR MH2X	Client's Job Ref	Contractor's Job Ref
--------------	------------------------------------	-------------	------------------	----------------------



MH2X\_99a95e93-e9bd-4658-b633-a5a8b0b76c35\_20190906\_101510\_209.jpg, 00:00:33, 1.80 m  
 Crack, circumferential at joint from 8 o'clock to 3 o'clock

## Section Inspection - 04/09/2019 - JUNCTIONX

Section 4	Inspection 4	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned N	PLR JUNCTIONX
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	JUNCTION
Road:	18A Frognal Gardens	Inspected Length:	11.00 m	Upstream Pipe Depth:	
Location:		Total Length:	50.00 m	Downstream Node:	D/S JN
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	300 mm		
Year Constructed:		Pipe Material:	Vitrified clay pipe (i.e. all clayware)		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale: 1:435	Position [m]	Code	Observation	MPEG	Photo	Grade
	0.00	MH	Start node type, manhole, reference number: JUNCTION	00:00:00		
	0.00	WL	Water level, 5% of the vertical dimension	00:00:01		
	0.10	REM	General remark: POOR VIEW OF PIPE DUE TO SIZE	00:00:07		
	3.20	JN	Junction at 9 o'clock, diameter: 150mm	00:00:31		
	5.20	JN	Junction at 3 o'clock, diameter: 150mm	00:00:42		
	9.40	CN	Connection other than junction at 10 o'clock, diameter: 150mm	00:01:07		
	11.00	SA	Survey abandoned: LIMIT OF SURVEY	00:01:17		
	50.00		End of pipe			

Structural Defects					Construction Features				
Service & Operational Observations					Miscellaneous Features				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	0	0.0	0.0	0.0	1.0

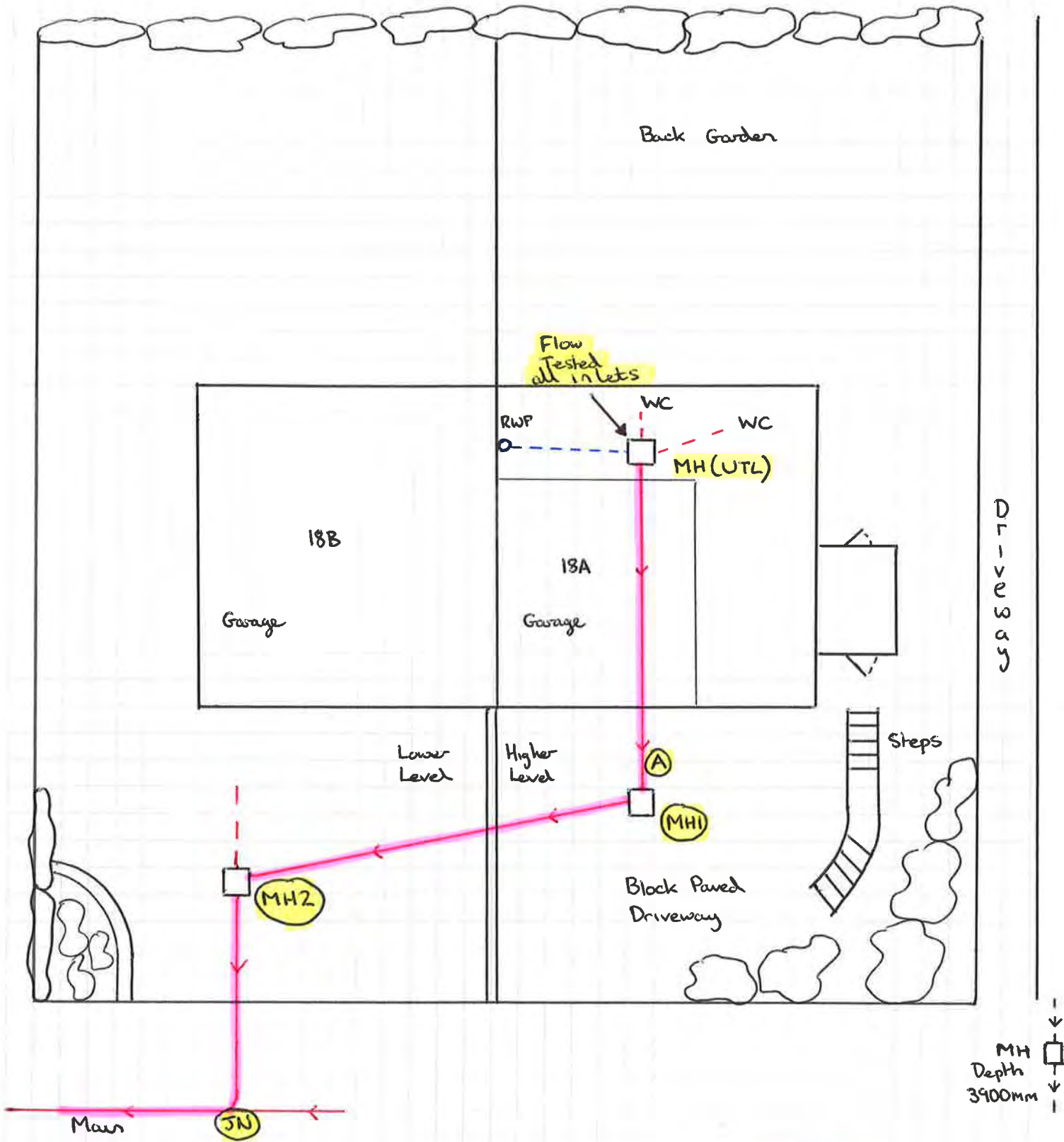
### Manhole Information

REFERENCE: <b>MH 1</b>	DUTY: <b>CB</b>	REFERENCE: <b>MH2</b>	DUTY: <b>CB</b>
DIAGRAM: 		DIAGRAM: 	
DEPTH AT OUTLET: <b>1740mm</b>		DEPTH AT OUTLET: <b>1400mm</b>	
MH SIZE <b>900mm x 500mm</b>		MH SIZE <b>950mm x 600mm</b>	
MH MATERIAL <b>Brick / Render</b>		MH MATERIAL <b>Brick</b>	
OBSERVATIONS/ COMMENTS:		OBSERVATIONS/ COMMENTS:	
REFERENCE:	DUTY:	REFERENCE:	DUTY:
DIAGRAM:		DIAGRAM:	
DEPTH AT OUTLET:		DEPTH AT OUTLET:	
MH SIZE		MH SIZE	
MH MATERIAL		MH MATERIAL	
OBSERVATIONS/ COMMENTS:		OBSERVATIONS/ COMMENTS:	

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Sketch not to Scale ————— CCTV Completed

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Aqua-Jet Specialist Drainage Contractors Ltd, Yard 21, Hilton Industrial Estate, Hilton, Derbyshire, DE65 5FE

# APPENDIX ñ CCTV SURVEY REPORT







## Table of Contents

Project Name	Project Number	Project Date
04.09.19 18A Frogmal Gardens, London		04/09/2019

Project Information .....	P-1
Section: 1; MH1 > MH2 (MH1X) .....	1
Section: 2; A/MH1 > MH1 (A/MH1X) .....	3
Section: 3; MH2 > D/S MH2 (MH2X) .....	5
Section: 4; JUNCTION > D/S JN (JUNCTIONX) .....	7



## Project Information

Project Name	Project Number	Project Date
04.09.19 18A Frogna Gardens, London		04/09/2019

### Client

**Company:** Environmental Engineering Partnership  
**Street:** The Chapel House, High Street  
**Town or City:** West Wycombe, HP14 3AG

### Site

**Company:** EEP  
**Street:** 18A Frogna Gardens  
**Town or City:** London, NW3 6XA

### Contractor

**Company:** Aqua-Jet Specialist Drainage Contractors Ltd  
**Contact:** Rob Wilkinson  
**Street:** Yard 21 Hilton Ind Est, Sutton Lane  
**Town or City:** Hilton, Derbyshire, DE65 5FE  
**Phone:** 01283 730333  
**Email:** aquajetltd@aol.com

## Section Inspection - 04/09/2019 - MH1X

Section 1	Inspection 1	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR MH1X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	MH1
Road:	18A Frognal Gardens	Inspected Length:	10.00 m	Upstream Pipe Depth:	
Location:		Total Length:	10.00 m	Downstream Node:	MH2
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Cast iron		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

Comments:  
 Recommendations:

Scale:	1:87	Position [m]	Code	Observation	MPEG	Photo	Grade																																			
<div style="display: flex; align-items: center;"> <div style="text-align: center; margin-right: 20px;"> <p>Depth: m</p> <p>MH1</p> </div> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 10%;"></td> <td style="width: 10%;">0.00</td> <td style="width: 10%;">MH</td> <td style="width: 40%;">Start node type, manhole, reference number: MH1</td> <td style="width: 10%;">00:00:00</td> <td></td> <td></td> </tr> <tr> <td></td> <td>0.00</td> <td>WL</td> <td>Water level, 0% of the vertical dimension</td> <td>00:00:01</td> <td></td> <td></td> </tr> <tr> <td></td> <td>0.10</td> <td>S01 DEE</td> <td>Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION</td> <td>00:00:06</td> <td></td> <td></td> </tr> <tr> <td></td> <td>9.90</td> <td>F01 DEE</td> <td>Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION</td> <td>00:01:22</td> <td></td> <td style="text-align: center;">2</td> </tr> <tr> <td></td> <td>10.00</td> <td>MH2 MHF</td> <td>Finish node type, manhole, reference number: MH2</td> <td>00:01:23</td> <td></td> <td></td> </tr> </table> </div>									0.00	MH	Start node type, manhole, reference number: MH1	00:00:00				0.00	WL	Water level, 0% of the vertical dimension	00:00:01				0.10	S01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:06				9.90	F01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22		2		10.00	MH2 MHF	Finish node type, manhole, reference number: MH2	00:01:23		
	0.00	MH	Start node type, manhole, reference number: MH1	00:00:00																																						
	0.00	WL	Water level, 0% of the vertical dimension	00:00:01																																						
	0.10	S01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:06																																						
	9.90	F01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22		2																																				
	10.00	MH2 MHF	Finish node type, manhole, reference number: MH2	00:01:23																																						

**Structural Defects**

**Construction Features**

Service & Operational Observations

Miscellaneous Features

STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	1.0	1.0	10.0	2.0

### Section Pictures - 04/09/2019 - MH1X

Section	Inspection Direction	PLR	Client's Job Ref	Contractor's Job Ref
1	Downstream	MH1X		



MH1X\_697d6ba7-1a86-43ea-9b00-4985f68a1723\_20190906\_095824\_558.jpg, 00:00:06, 0.10 m  
Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start

## Section Inspection - 04/09/2019 - A/MH1X

Section 2	Inspection 2	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR A/MH1X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Upstream	Upstream Node:	A/MH1
Road:	18A Frognal Gardens	Inspected Length:	7.50 m	Upstream Pipe Depth:	
Location:		Total Length:	7.50 m	Downstream Node:	MH1
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Cast iron		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale:	1:66	Position [m]	Code	Observation	MPEG	Photo	Grade
		0.00	MH	Start node type, manhole, reference number: MH1	00:00:00		
		0.00	WL	Water level, 5% of the vertical dimension	00:00:01		
		0.10	S01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, start: RUST / CORROSION	00:00:03		
		7.40	F01 DEE	Attached deposits, encrustation from 12 o'clock to 12 o'clock, 5% cross-sectional area loss, finish: RUST / CORROSION	00:01:22		2
		7.50	MHF	Finish node type, manhole, reference number: A/MH1	00:01:22		

Structural Defects					Construction Features				
Service & Operational Observations					Miscellaneous Features				
STR No. Def	STR Peak	STR Mean	STR Total	STR Grade	SER No. Def	SER Peak	SER Mean	SER Total	SER Grade
0	0.0	0.0	0.0	1.0	1	1.0	1.1	8.0	2.0

**Section Pictures - 04/09/2019 - A/MH1X**

Section 2	Inspection Direction Upstream	PLR A/MH1X	Client's Job Ref	Contractor's Job Ref
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A\_MH1X\_7069cf84-8557-4d21-aaf6-a844871a4e0a\_20190906\_100331\_033.jpg, 00:00:03, 0.10 m  
 Attached deposits, encrustation from 12 o'clock to 12 o'clock,  
 5% cross-sectional area loss, start

## Section Inspection - 04/09/2019 - MH2X

Section 3	Inspection 3	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned Y	PLR MH2X
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	MH2
Road:	18A Frognal Gardens	Inspected Length:	7.30 m	Upstream Pipe Depth:	
Location:		Total Length:	7.30 m	Downstream Node:	D/S MH2
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	100 mm		
Year Constructed:		Pipe Material:	Vitrified clay pipe (i.e. all clayware)		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale:	1:64	Position [m]	Code	Observation	MPEG	Photo	Grade																																																								
<div style="display: flex; align-items: flex-start;"> <div style="flex: 1;"> <p>Depth: m MH2</p> </div> <table style="flex: 4; border-collapse: collapse;"> <tr> <td style="text-align: right; padding-right: 5px;">0.00</td> <td style="padding-right: 5px;">MH</td> <td style="padding-right: 5px;">Start node type, manhole, reference number: MH2: SURVEY THROUGH TOP ACCESS HOLE OF TRAP</td> <td style="text-align: right; padding-right: 5px;">00:00:00</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">0.00</td> <td style="padding-right: 5px;">WL</td> <td style="padding-right: 5px;">Water level, 5% of the vertical dimension</td> <td style="text-align: right; padding-right: 5px;">00:00:01</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">0.20</td> <td style="padding-right: 5px;">JN</td> <td style="padding-right: 5px;">Junction at 6 o'clock, diameter: 100mm: BOTTOM OUTLET OF TRAP</td> <td style="text-align: right; padding-right: 5px;">00:00:09</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">0.30</td> <td style="padding-right: 5px;">SC</td> <td style="padding-right: 5px;">Size changes, new size(s), 150mm high</td> <td style="text-align: right; padding-right: 5px;">00:00:15</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">1.80</td> <td style="padding-right: 5px;">CCJ</td> <td style="padding-right: 5px;">Crack, circumferential at joint from 8 o'clock to 3 o'clock</td> <td style="text-align: right; padding-right: 5px;">00:00:33</td> <td></td> <td></td> <td style="text-align: center;">2</td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">2.70</td> <td style="padding-right: 5px;">LD</td> <td style="padding-right: 5px;">Line deviates down</td> <td style="text-align: right; padding-right: 5px;">00:00:41</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">6.80</td> <td style="padding-right: 5px;">LR</td> <td style="padding-right: 5px;">Line deviates right</td> <td style="text-align: right; padding-right: 5px;">00:01:23</td> <td></td> <td></td> <td></td> </tr> <tr> <td style="text-align: right; padding-right: 5px;">7.30</td> <td style="padding-right: 5px;">SA</td> <td style="padding-right: 5px;">Survey abandoned: JOINS MAIN BLIND</td> <td style="text-align: right; padding-right: 5px;">00:01:28</td> <td></td> <td></td> <td></td> </tr> </table> </div>								0.00	MH	Start node type, manhole, reference number: MH2: SURVEY THROUGH TOP ACCESS HOLE OF TRAP	00:00:00				0.00	WL	Water level, 5% of the vertical dimension	00:00:01				0.20	JN	Junction at 6 o'clock, diameter: 100mm: BOTTOM OUTLET OF TRAP	00:00:09				0.30	SC	Size changes, new size(s), 150mm high	00:00:15				1.80	CCJ	Crack, circumferential at joint from 8 o'clock to 3 o'clock	00:00:33			2	2.70	LD	Line deviates down	00:00:41				6.80	LR	Line deviates right	00:01:23				7.30	SA	Survey abandoned: JOINS MAIN BLIND	00:01:28			
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6.80	LR	Line deviates right	00:01:23																																																												
7.30	SA	Survey abandoned: JOINS MAIN BLIND	00:01:28																																																												

Structural Defects					Construction Features						
Service & Operational Observations					Miscellaneous Features						
STR No.	Def	STR Peak	STR Mean	STR Total	STR Grade	SER No.	Def	SER Peak	SER Mean	SER Total	SER Grade
1		10.0	1.4	10.0	2.0	0		0.0	0.0	0.0	1.0

**Section Pictures - 04/09/2019 - MH2X**

Section 3	Inspection Direction Downstream	PLR MH2X	Client's Job Ref	Contractor's Job Ref
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MH2X\_99a95e93-e9bd-4658-b633-a5a8b0b76c35\_20190906\_101510\_209.jpg, 00:00:33, 1.80 m  
 Crack, circumferential at joint from 8 o'clock to 3 o'clock



## Section Inspection - 04/09/2019 - JUNCTIONX

Section 4	Inspection 4	Date 04/09/19	Time	Client's Job Ref Not Specified	Weather No Rain Or Snow	Pre Cleaned N	PLR JUNCTIONX
Operator RR/MD		Vehicle FJ17 ZDS		Camera Flexi	Preset Length Not Specified	Legal Status Not Specified	Alternative ID Not Specified

Town or Village:	London	Inspection Direction:	Downstream	Upstream Node:	JUNCTION
Road:	18A Frognal Gardens	Inspected Length:	11.00 m	Upstream Pipe Depth:	
Location:		Total Length:	50.00 m	Downstream Node:	D/S JN
Surface Type:		Joint Length:	0.00 m	Downstream Pipe Depth:	
Use:	Combined	Pipe Shape:	Circular		
Type of Pipe:	Gravity drain/sewer	Dia/Height:	300 mm		
Year Constructed:		Pipe Material:	Vitrified clay pipe (i.e. all clayware)		
Flow Control:	No flow control	Lining Type:	No Lining		
Inspection Purpose:		Lining Material:	No Lining		

**Comments:**  
**Recommendations:**

Scale: 1:435	Position [m]	Code	Observation	MPEG	Photo	Grade
	0.00	MH	Start node type, manhole, reference number: JUNCTION	00:00:00		
	0.00	WL	Water level, 5% of the vertical dimension	00:00:01		
	0.10	REM	General remark: POOR VIEW OF PIPE DUE TO SIZE	00:00:07		
	3.20	JN	Junction at 9 o'clock, diameter: 150mm	00:00:31		
	5.20	JN	Junction at 3 o'clock, diameter: 150mm	00:00:42		
	9.40	CN	Connection other than junction at 10 o'clock, diameter: 150mm	00:01:07		
	11.00	SA	Survey abandoned: LIMIT OF SURVEY	00:01:17		
	50.00		End of pipe			

Structural Defects					Construction Features						
Service & Operational Observations					Miscellaneous Features						
STR No.	Def	STR Peak	STR Mean	STR Total	STR Grade	SER No.	Def	SER Peak	SER Mean	SER Total	SER Grade
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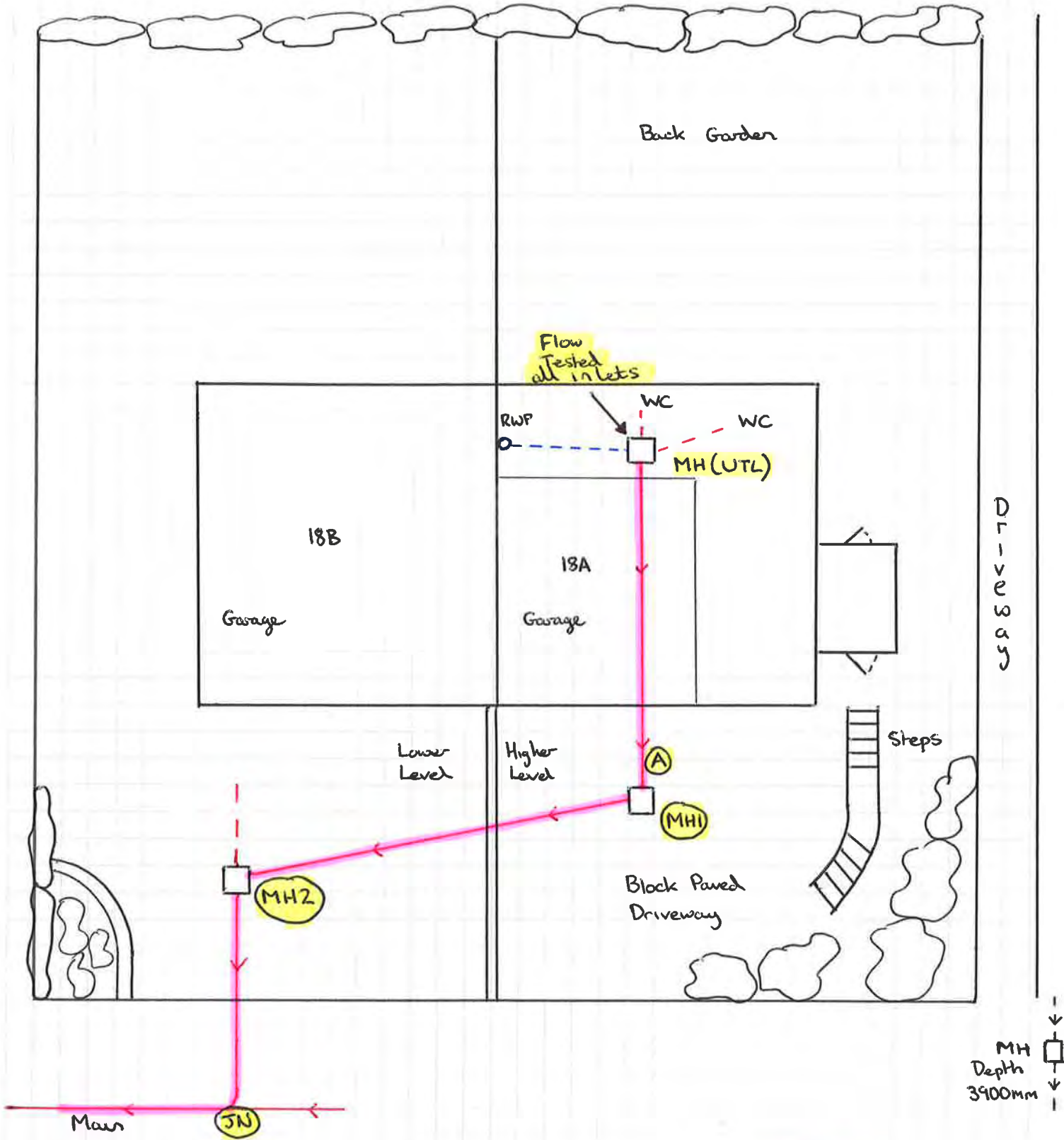
### Manhole Information

REFERENCE: <b>MH 1</b>	DUTY: <b>CB</b>	REFERENCE: <b>MH2</b>	DUTY: <b>CB</b>
DIAGRAM: 		DIAGRAM: 	
DEPTH AT OUTLET: <b>1740mm</b>		DEPTH AT OUTLET: <b>1400mm</b>	
MH SIZE <b>900mm x 500mm</b>		MH SIZE <b>950mm x 600mm</b>	
MH MATERIAL <b>Brick / Render</b>		MH MATERIAL <b>Brick</b>	
OBSERVATIONS/ COMMENTS:		OBSERVATIONS/ COMMENTS:	
REFERENCE:	DUTY:	REFERENCE:	DUTY:
DIAGRAM:		DIAGRAM:	
DEPTH AT OUTLET:		DEPTH AT OUTLET:	
MH SIZE		MH SIZE	
MH MATERIAL		MH MATERIAL	
OBSERVATIONS/ COMMENTS:		OBSERVATIONS/ COMMENTS:	

Jetting • Vacuumation • Camera Inspection • Excavation & Repairs • Septic Tanks

Tel: 01283 730333 Fax: 01283 730144 www.aquajettd.co.uk aquajettd@aol.com

Aqua-Jet Specialist Drainage Contractors Ltd, Yard 21, Hilton Industrial Estate, Sutton Lane, Hilton, Derbyshire, DE65 5FE



Sketch not to Scale ————— CCTV Completed

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Tel: 01283 730333 Fax: 01283 730444 [www.aquajetltd.co.uk](http://www.aquajetltd.co.uk) [aquajetltd@aol.com](mailto:aquajetltd@aol.com)

Aqua-Jet Specialist Drainage Contractors Ltd, Yard 21, Hilton Industrial Estate, Hilton, Derbyshire, DE65 5FE



A-squared Studio

# 18A Frognal Gardens

## Ground Movement Assessment Report

July 2020

1125-A2S-XX-XX-RP-Y-0001-01





Project Name	18A Frognal Gardens
Project Number	1125
Client	Soil Consultants Ltd
Document Name	Ground Movement Assessment Report

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Director 

Document Reference	Status	Revision	Issued by	Date
1125-A2S-XX-XX-RP-Y-0001-00	First Issue	00	SB	15.10.2019
1125-A2S-XX-XX-RP-Y-0001-01	Revised based on feedback from project team	01	HS	17.07.2020



## Contents

1.	Introduction.....	1
2.	The Site & Development.....	2
3.	Geology .....	4
4.	Impact Assessment Methodology.....	5
5.	Conclusions & Closing Remarks.....	14

## Appendices

Appendix A: Selected Supporting Information



# 1. Introduction

A-squared Studio Engineers Ltd (A-squared) has been appointed Soil Consultants Ltd (SCL) to undertake a Ground Movement Assessment (GMA) for the 18A Frognal Gardens development in London.

The A-squared scope comprises an assessment of the potential impact of the proposed redevelopment works on the various neighbouring properties.

## 1.1. Study Aims & Objectives

A ground movement and impact assessment has been carried out in order to estimate the potential damage induced by the proposed redevelopment at 18A Frognal Gardens on the neighbouring properties.

The scheme involves the demolition of the existing two- to three-storey property, excavation of an extended basement, and construction of a proposed four-storey residential structure. The depth of excavation ranges from 1.0m to 6.275m due to sloping ground from the northeast to the southwest and a localised deepening for a pool. Secant piled walls have been selected as the ground retention system for the northern and eastern sides of the excavation while mass concrete underpins have been selected for the north-western side.

The assessment encompasses properties located within the zone of influence of the proposed scheme. The GMA assessment is based on *greenfield* ground movements which are unlikely to be exceeded. The adopted assessment methodology provides a robust and conservative assessment representative of current industry best practice, as detailed in Section 0.

The assessment carried out and described herein aims to:

- Assess the impact of ground movements induced by the proposed works on properties adjacent to the development under consideration.
- Inform Party Wall awards.
- Provide performance criteria and inform aspects of substructure construction and design.

This report provides a detailed description of the:

- Site and proposed development.
- Modelling parameters and input.
- Analyses and results.



## 2. The Site & Development

### 2.1. Site Location and Proposed Development

The proposed development is located at 18A Frogna! Gardens, Hampstead, London, NW3 6XA, as shown in Figure 2.1. The site is approximately located at British National Grid coordinates 526168E,185768N, falling within administrative boundaries of the London Borough of Camden. Hampstead Underground Station is located approximately 220m east of the site.

The site is gently sloping, with elevations ranging from approximately +108.7mOD in the southwest to +112.5mOD in the northeast.



**Figure 2.1** 18A Frogna! Gardens site location

The existing structure occupying the site is a two- to three-storey residence with a lowest level that cuts into the natural topography. This structure will be demolished, and a two- to four-storey residence will be constructed in its place. The proposed development involves several excavations over a large portion of the site footprint to create the lower ground floor and pool area.

The excavation will be supported by secant piled walls on the northern and eastern sides and mass concrete underpins installed sequentially in a hit-and-miss fashion on the north-western side. The lower ground floor excavation will extend from a minimum depth of 1.0m on the southern side and maximum depth of 6.275m, representing the pool area in the northern section of the property. In this area, trench sheeting will be used to reach the required formation level beneath the underpins founded at a 3.9m depth.

The locations of each of the retention systems are shown in Figure 2.2. Scheme drawings (current at the time of writing) are presented in Appendix A.





- Underpinning to 3.9mBGL
- Underpinning to 3.9mBGL followed by trench sheeting to 6.6mBGL.
- Secant piled wall

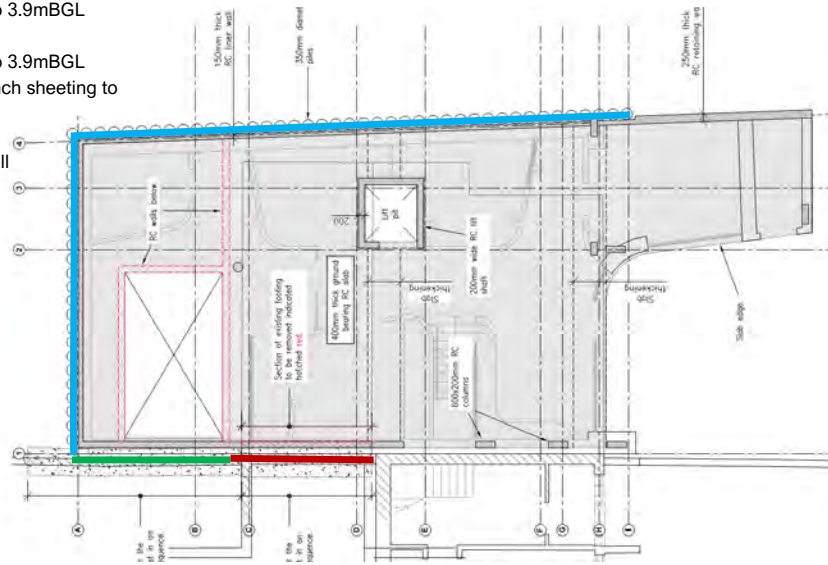


Figure 2.2 Sketch showing the locations of each proposed excavation retention system



### 3. Geology

Site-specific ground investigation works were carried out on the project site by Soil Consultants Ltd in August 2019. The ground conditions were found to comprise the following (in order of increasing depth):

- Made Ground – anthropogenic deposits of undifferentiated silty clays, sands and gravels.
- Bagshot Formation – loose brown slightly clayey SILT/SAND with occasional clay lenses
- Claygate Beds – firm grey mottled brown sandy silty CLAY with sand horizons
- London Clay Formation – stiff to very stiff fissured brown CLAY with occasional rare bands of silty sand.

The above include the strata of engineering interest and significance, taking cognisance of the scale of the proposed development and zone of influence. The ground model adopted for this assessment is presented in Table 3.1.

**Table 3.1 Ground model and geotechnical parameters adopted for analysis purposes**

Stratum	Depth (mBGL)	Thickness (m)	Undrained Young's Modulus, $E_u$ [2] (MPa)	Drained Young's Modulus, $E'$ [2] (MPa)
Made Ground	0.0	1.0	-	10.0
Bagshot Formation	1.0	6.0	-	18.0
Claygate Beds + London Clay <sup>[3]</sup>	7.0	27.0 <sup>[4]</sup>	14.4 + 3.2z <sup>[5]</sup>	11.5 + 2.5z <sup>[5]</sup>

1. Ground model based on previous site-specific ground investigation undertaken by Soil Consultants Ltd. This data has been interpreted specifically for the scope of the GMA presented herein.
2. Stiffness data ( $E_u$  and  $E'$ ) has been evaluated empirically from in-situ testing data taking into consideration the nature of the geotechnical/soil-structure interaction mechanisms and level of anticipated strain within the soil mass.
3. Claygate Beds and London Clay are assumed to follow a continuous stiffness profile.
4. *Rigid boundary* assumed at 34.0mBGL for analytical purposes.
5. z refers to the depth in metres below the top of the Claygate Beds + London Clay formation.



## 4. Impact Assessment Methodology

### 4.1. Assessment Details

The assessment has been undertaken using proprietary spreadsheets and the commercially available software Oasys Pdisp and Xdisp, which consider the three-dimensional ground movement field induced by the proposed excavation works.

Ground movements will arise as a result of various mechanisms which are mobilised as part of the construction works for the proposed scheme. The demolition of the existing building and lower ground floor excavation process will induce ground movements arising from the overburden removal and installation of the proposed retention systems. The permanent condition loading will partially reinstate a portion of the removed overburden, yielding settlements across the foundation system. The induced ground movements will extend over a given zone of influence surrounding the building/excavation footprint

A series of three-dimensional models of the proposed scheme have been developed in Oasys Xdisp / Pdisp and combined by means of superposition in order to enable ground movement assessments to be carried out representing the various construction stages. The ground movement displacement fields were separated in two groups (A & B) based on the approach followed, as detailed below:

#### Group A – Unloading/loading ground movements

- A1. Building demolition (short term).
- A2. Building demolition and basement excavation (short term).
- A3. Building demolition, basement excavation, and application of the proposed building loading (long term).

#### Group B – CIRIA-based ground movements

- B1. Secant wall and underpin installation and basement excavation.
- B2. Secant wall and underpin installation, basement excavation, and application of the proposed building loading (long term)

The Group A assessments are based on *greenfield* ground movements evaluated from linear half-space (Pdisp) analyses and focus on vertical ground movements induced by the overburden removal unloading and reloading processes.

Demolition unloading pressures of 30kPa and 45kPa have been applied over the footprint of the existing building on site, as shown in Figure 4.1 (approximately 15kPa per storey).

Excavation unloading pressures have been modelled at the basement formation level representing the removal of approximately 1.0m (20kPa) and 4.2m (85kPa) of overburden to create the lower ground floor. A further unloading pressure of 126kPa (6.275m overburden), representing the excavation of the pool area, was also modelled at formation level in the northern section of the property.

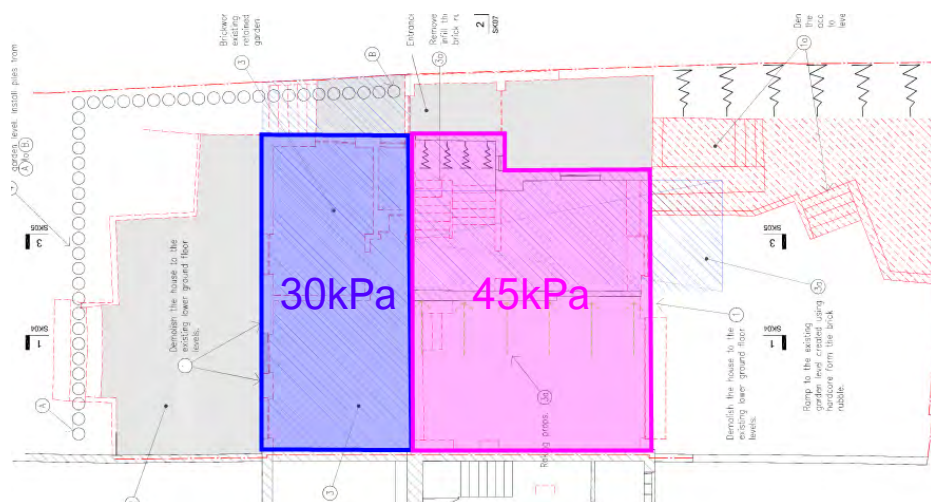
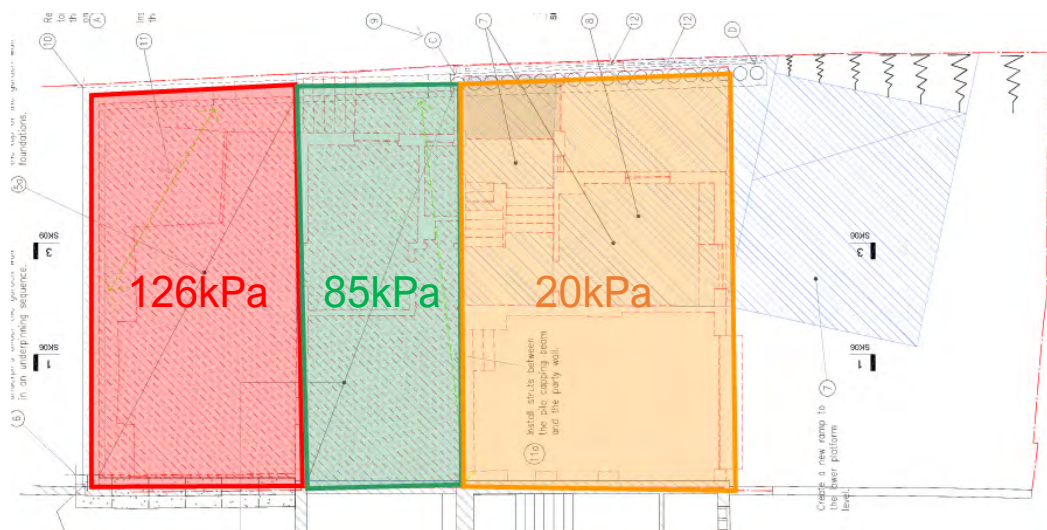
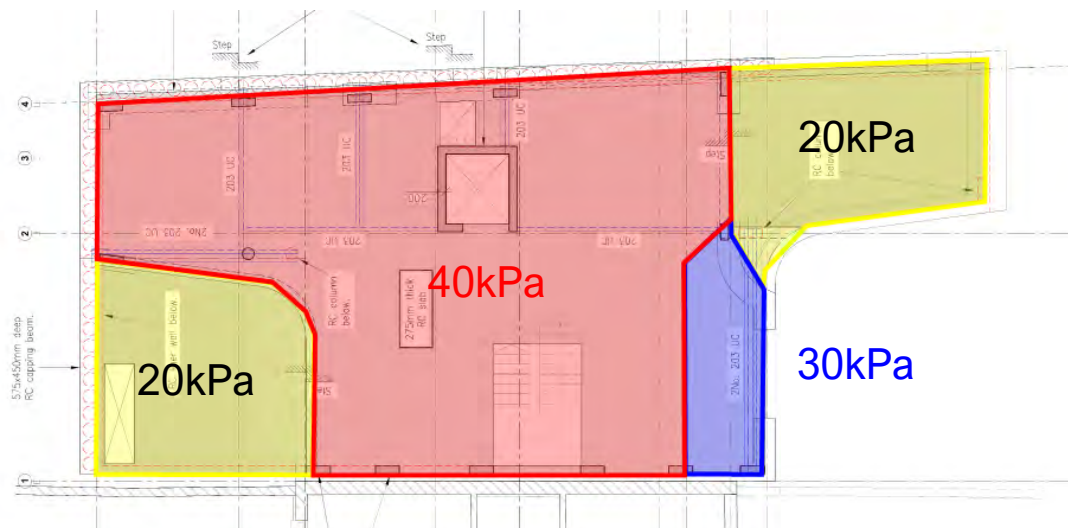


Figure 4.1 Modelled demolition area in Pdisp



**Figure 4.2 Modelled excavation area in Pdisp**

The proposed residential structure will have two to four storeys. Based on an assumed surcharge of ~10kPa per storey, four uniformly distributed loading zones have been modelled at basement formation level, as shown in Figure 4.3.



**Figure 4.3 Proposed building loading areas**

The Group B assessments adopt the normalised ground displacement curves reported in CIRIA C760. In addition to the effects arising from the excavation, the ground movement effects associated with the installation of the secant wall and underpinning have been considered. The following CIRIA C760 normalised ground movement curves were adopted to assess ground movements due to retention system installation and excavation works:

- *Underpin installation:* Installation of planar diaphragm wall in stiff clay.
- *Secant wall and trench sheeting:* Installation of contiguous bored pile wall in stiff clay.
- *Excavation to formation:* Excavation in front of a high stiffness wall in stiff clay.

The empirical data set for diaphragm wall installation is not strictly compatible with the construction technologies adopted in underpinning. However, it is assessed that the ground movement mechanisms are reasonably well-matched and, in lieu of better empirical relationships, the diaphragm wall curves are considered to provide a satisfactory and conservative approximation.

The "Installation of contiguous bored pile wall in stiff clay" CIRIA C760 curve has been adopted for all embedded wall installations (including trench sheeting) as it provides a more representative ground movement field for this assessment. It is widely accepted in

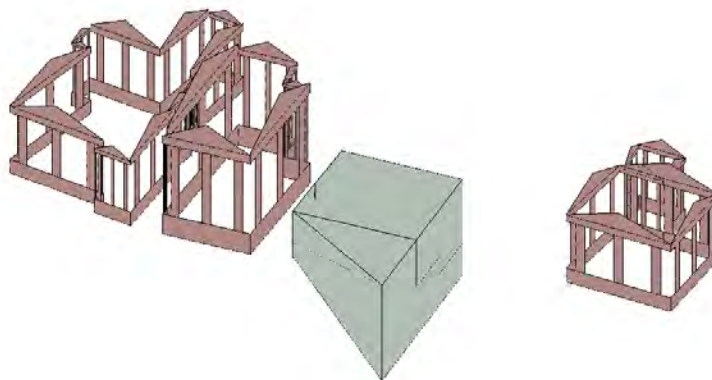


industry that the “Installation of secant bored pile wall in stiff clay” dataset is an upper bound for the movements induced by embedded pile wall installations – based on data measured in the field – and the contiguous curve presents a better fit to the empirical data set. For this reason, the contiguous pile wall curve has been adopted for the analysis presented herein.

As part of the underpin installation process, the load redistribution from the existing shallow foundations supporting the Party Wall to the new underpins on the west boundary has been modelled as a pressure acting at the base of the new underpins, assumed to be 1m wide. The weight of the adjacent structure acting on the underpins has been modelled as 114kPa, equivalent to the tributary area of the Party Wall supporting a 30kPa surcharge (approximately 10kPa per storey for 18B Froggnal Gardens). This represents the redistribution of the stress bulb induced by the building loading on the Party Wall / underpins to lower strata.

In the B2 assessment, the CIRIA ground movements are combined with the long-term settlements induced by the proposed building loading (evaluated in Pdisp).

The two sets of analyses enabled the production of an envelope of damage classification results, with the worst-case results presented herein. A representative geometry has been adopted for defining the excavation/installation geometry implemented in the 3D modelling efforts.



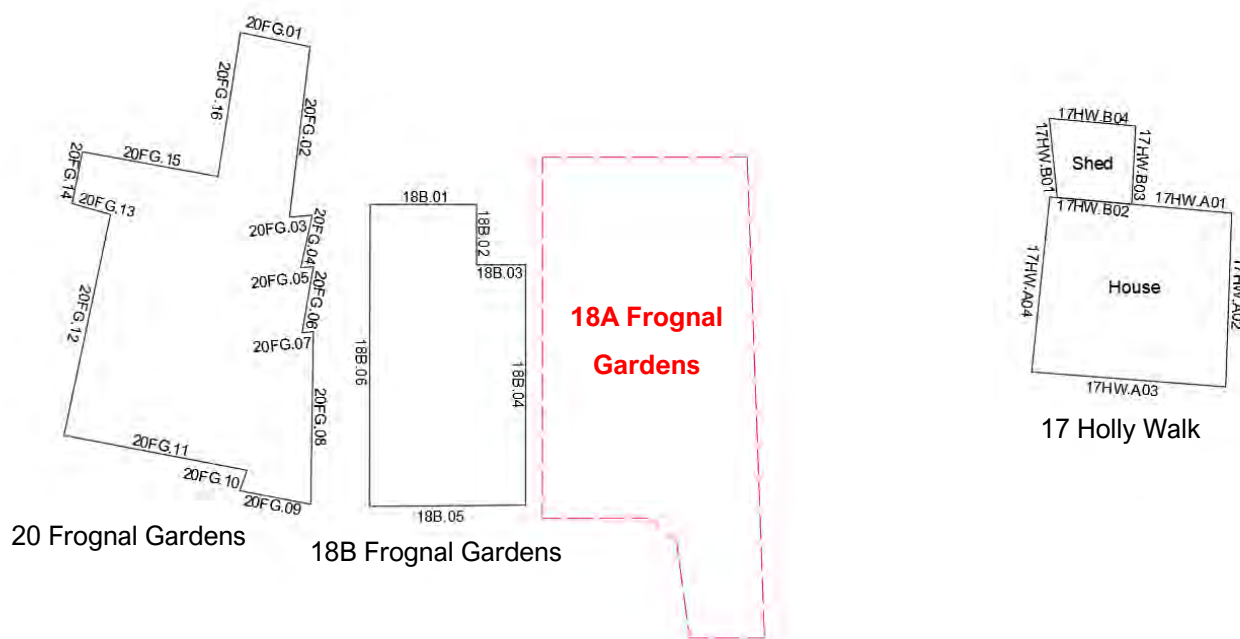
**Figure 4.4** Indicative plot of the three-dimensional analytical model using the Oasys Xdisp software suite

## 4.2. Impact Assessment

### 4.2.1. General

The potential impact / damage induced on primary façade / wall elements of the buildings around the proposed scheme (including retained party walls forming part of the proposed development) have been evaluated on the basis of the calculated ground movement fields. The masonry walls of concern are shown in Figure 4.5, including the wall nomenclature / reference system adopted. The arrangement is based on the currently available survey information and presents an array of masonry façades running both perpendicular and parallel to the proposed lower ground floor (covering the key deformation mechanisms). In total, 31 façades of the neighbouring buildings were considered for the current study and these are grouped in the following manner:

- 18B.01 – 18B.07: 18B Froggnal Gardens
- 20FG.01 – 20FG.16: 20 Froggnal Gardens
- 17HW.A01 – 17HW.A04: 17 Holly Walk house
- 17HW.B01 – 17HW.B04: 17 Holly Walk shed

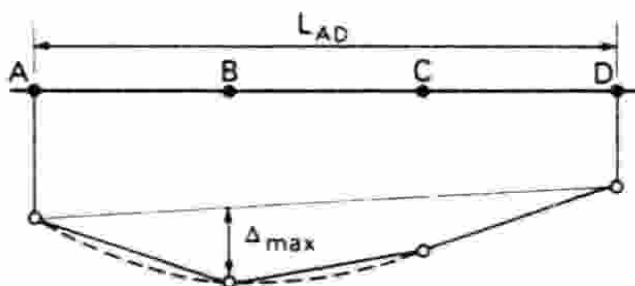


**Figure 4.5** Simplified scheme and nomenclature for each building façade/masonry wall element

Each wall has been assumed to behave as an equivalent beam subject to a bending and extension/compression deformation mechanism, based on the evaluated greenfield ground movement, as outlined previously.

Tensile strains induced within the building masonry walls have been evaluated based on the deflection ratios  $\Delta/L$  and horizontal extension mechanisms estimated from the analyses. The assessment considers the well-established Burland (1997) damage classification method, as presented and summarised in Figure 4.6 and Figure 4.7. This method involves a relatively simple but robust means of assessment, which is widely adopted and is considered to comprise an industry standard / best practice basis for impact assessments of this typology.

Potential damage categories are directly related to the tensile strains induced by the proposed construction stages, arising from a combination of direct tension and bending induced tension mechanisms. The evaluated damage categories correspond to an unlikely to be exceeded scenario (on the basis of the data sets adopted and greenfield assumptions).



**Figure 4.6** Definition of relative deflection  $\Delta$  and deflection ratio  $\Delta/L$



Category of damage	Description of typical damage (ease of repair is underlined)	Approximate crack width (mm)	Limiting tensile strain $\epsilon_{lim}$ (per cent)
0 Negligible	Hairline cracks of less than about 0.1 mm are classed as negligible.	< 0.1	0.0–0.05
1 Very slight	<u>Fine cracks that can easily be treated during normal decoration.</u> Perhaps isolated slight fracture in building. Cracks in external brickwork visible on inspection.	< 1	0.05–0.075
2 Slight	<u>Cracks easily filled. Redecoration probably required.</u> Several slight fractures showing inside of building. Cracks are visible externally and <u>some repointing may be required externally</u> to ensure weathertightness. Doors and windows may stick slightly.	< 5	0.075–0.15
3 Moderate	<u>The cracks require some opening up and can be patched by a mason. Recurrent cracks can be masked by suitable linings. Repointing of external brickwork and possibly a small amount of brickwork to be replaced.</u> Doors and windows sticking. Service pipes may fracture. Weathertightness often impaired.	5–15 or a number of cracks > 3	0.15–0.3
4 Severe	<u>Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows.</u> Windows and frames distorted, floor sloping noticeably. Walls leaning or bulging noticeably, some loss of bearing in beams. Service pipes disrupted.	15–25 but also depends on number of cracks	> 0.3
5 Very severe	<u>This requires a major repair involving partial or complete rebuilding.</u> Beams lose bearings, walls lean badly and require shoring. Windows broken with distortion. Danger of instability.	usually > 25 but depends on number of cracks.	

After Burland et al. 1977, Boscardin and Cording 1989, and Burland 2001.

**Figure 4.7 Building damage classification – relationship between category of damage and limiting strain  $\epsilon_{lim}$**

#### 4.2.2. Results

The results of the assessment are presented in Table 4.1. Note that the results presented in this table represent the worst-case output arising from all analysis runs. Damage category results are presented in Figure 4.8 for the affected façades. Figure 4.9 and Figure 4.10 depict the vertical and horizontal displacements, respectively, induced by the secant wall and underpin/trench sheet installation and excavation calculated as per CIRIA C760 datasets (assessment B1).

**Table 4.1 Evaluated damage categories extracted from Xdisp**

Façade Reference	Analysis Scenario				
	A1	A2	A3	B1	B2
18B.01	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 1 – Very Slight	Category 1 – Very Slight
18B.02	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible

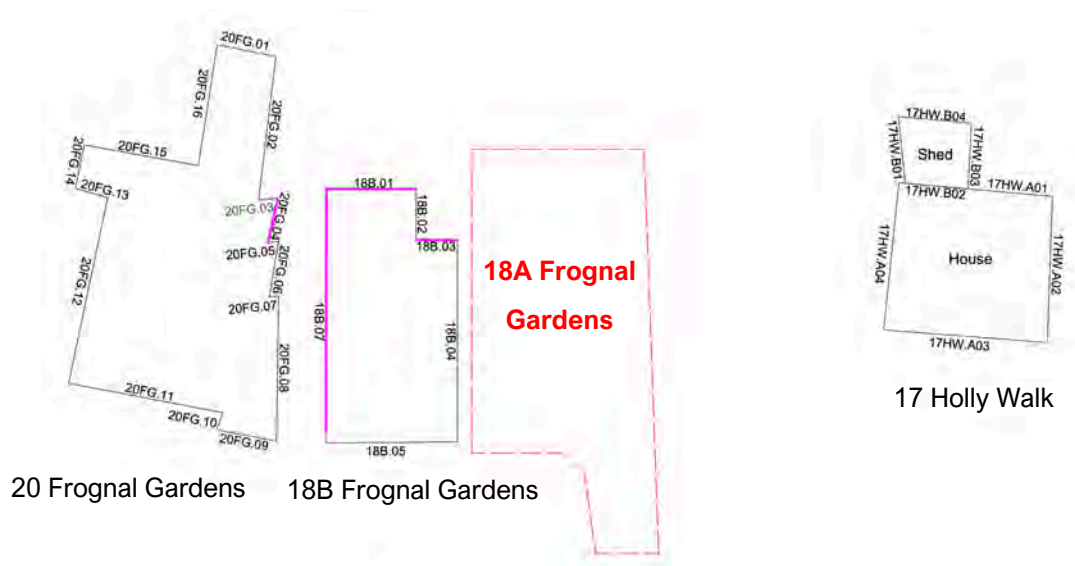


Façade Reference	Analysis Scenario				
	A1	A2	A3	B1	B2
18B.03	Category 0 – Negligible	Category 1 – Very Slight	Category 1 – Very Slight	Category 1 – Very Slight	Category 1 – Very Slight
18B.04	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
18B.05	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
18B.06	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
18B.07	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 1 – Very Slight	Category 1 – Very Slight
20FG.01	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.02	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.03	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.04	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 1 – Very Slight	Category 1 – Very Slight
20FG.05	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.06	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.07	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.08	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.09	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.10	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.11	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.12	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.13	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible





Façade Reference	Analysis Scenario				
	A1	A2	A3	B1	B2
20FG.14	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.15	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
20FG.16	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.A01	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 1 – Very Slight
17HW.A02	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.A03	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.A04	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.B01	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.B02	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.B03	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible
17HW.B04	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible	Category 0 – Negligible



Purple – Category 1 (Very Slight)

**Figure 4.8** Damage category results after analyses A3 and B2

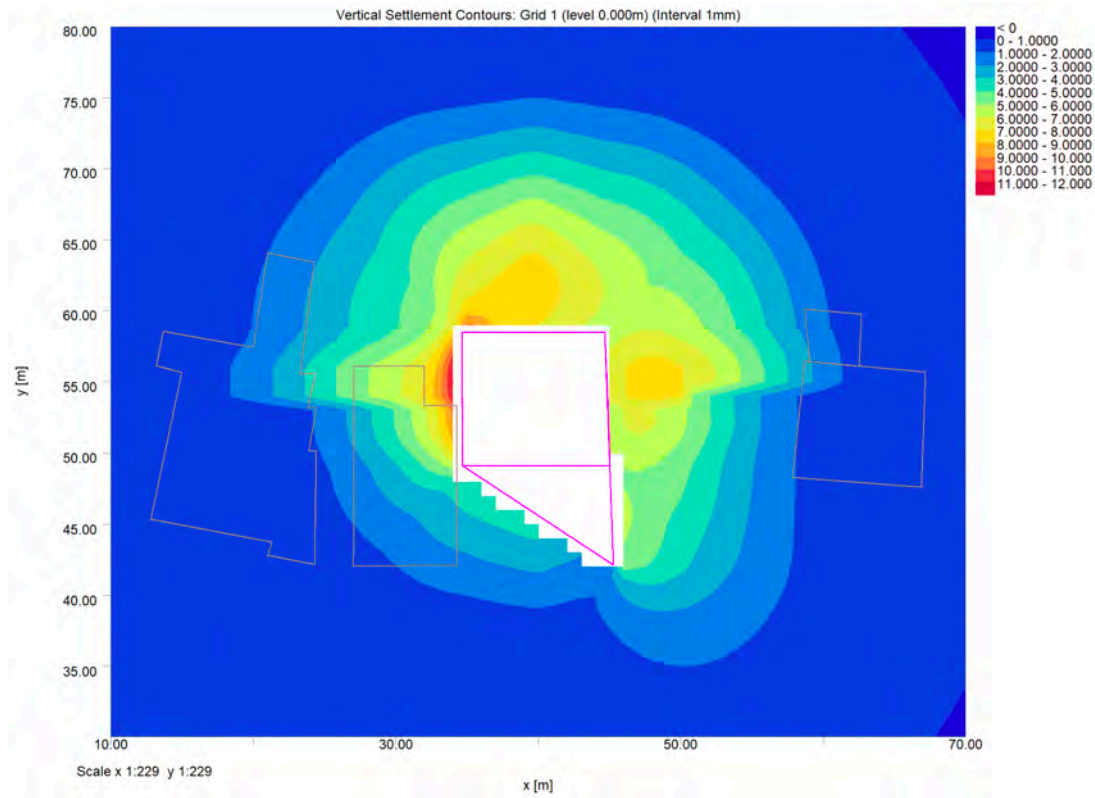


Figure 4.9 Resultant Xdisp vertical displacement contours for scenario B1 – units in mm – secant wall and underpin/trench sheet installation and excavation (CIRIA C760)

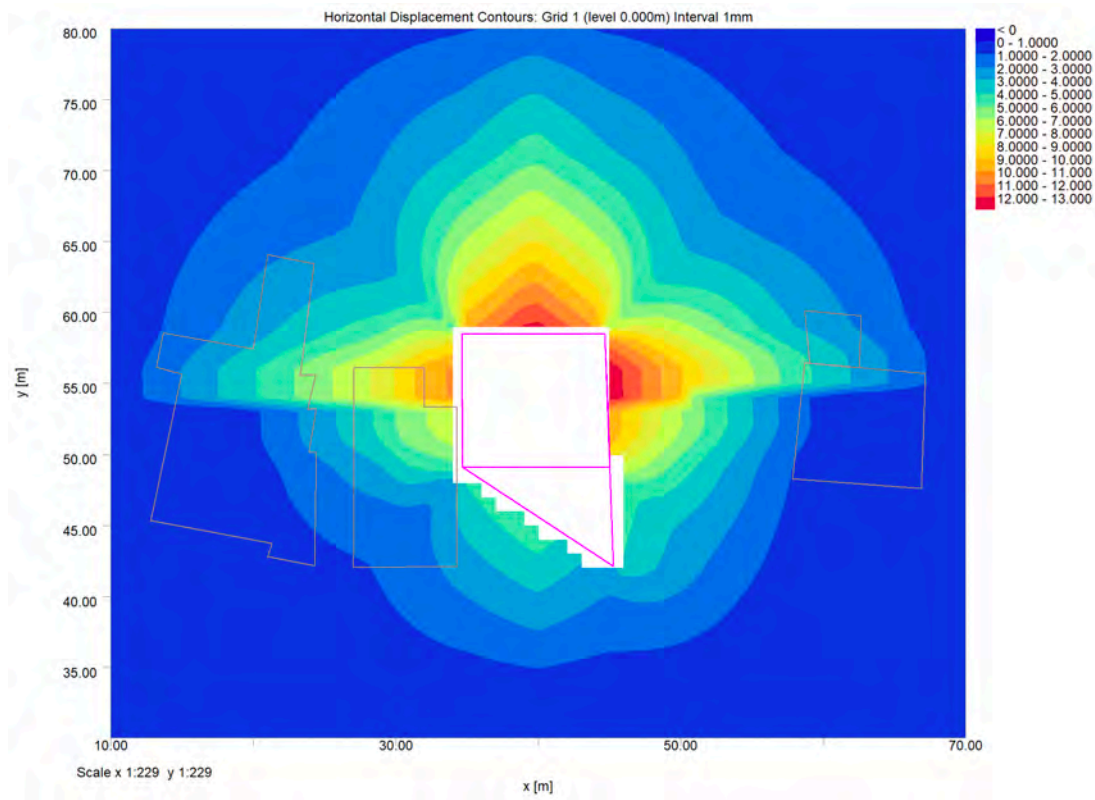


Figure 4.10 Resultant Xdisp horizontal displacement contours for scenario B1 – units in mm – secant wall and underpin/trench sheet installation and excavation (CIRIA C760)



### 4.2.3. Basement Excavation Criteria

The results of this analysis show that all buildings fall within the acceptable damage classification if the ground movements caused by the site development are limited to the values presented in Table 4.2. The ground movements below present the maximum movements directly adjacent to the secant piled wall and underpins. Specific wall/façade deflection limits and trigger levels may be developed as part of the proposed monitoring regime, on the basis of the ground movement field presented herein.

**Table 4.2 Limiting ground movement values at various construction stages**

Stage	Maximum Cumulative Ground Movement (mm)	
	Vertical	Horizontal
Secant Wall Installation	4	4
Underpin/Trench Sheet Installation	8	2
Excavation	12	13
Long-Term Condition	20	13



## 5. Conclusions & Closing Remarks

The interaction between the proposed 18A Frogna Gardens development and the neighbouring properties within the zone of influence of the scheme has been reviewed as part of the GMA study presented herein.

The proposed development construction operations comprise three stages: demolition of the existing property, installation of the secant wall and underpinning/trench sheeting, and bulk excavation. The impact of the construction stages has been reviewed on the basis of two alternative methods, i.e. evaluating the effects of unloading/overburden removal using  $P_{disp}$  and simulating the excavation induced ground movements using empirical CIRIA curves in  $X_{disp}$ . In the latter case, a propped retaining wall solution (during the temporary works stage) has been considered, utilising the CIRIA C760 ground movement curves for high stiffness walls in stiff clay.

These two different scenarios have been considered in order to bind the potential ground movements arising from excavation operations (i.e. maximum potential heave and settlement respectively). This strategy ensures a robust evaluation of potential impact in light of the bespoke, intricate and workmanship-dependent construction methodology. Both short-term (undrained) and long-term (drained) conditions have been assessed by adopting the relevant soil stiffness parameters for each case.

In order to best limit ground movements in proximity to movement sensitive neighbouring buildings, due consideration may be given to suitable means and methods of construction. For example, reducing the extent of temporary excavations during earth removal operations in close proximity to buildings considered to be at most risk of damage.

The results from the GMA analyses are presented in Table 4.1 (denoting the evaluated damage categorisation in accordance with the Burland criteria described herein). It is observed that the maximum damage classification for the neighbouring properties is Category 1 – Very Slight. Specific wall / façade deflection limits / trigger levels may be developed as part of the proposed monitoring regime (based on the findings presented herein).

It is noted that the predicted ground movements, the associated wall tensile strains, and the level of damage categorisation are considered to be moderately conservative in view of the relatively cautious data selection and greenfield nature of the assessment undertaken.

It is also noted that the GMA will be supplemented by a project-specific monitoring regime and Action Plan, which will delineate lines of responsibility, trigger levels in accordance with those presented in this GMA and appropriate mitigation measures. The assessment presented herein is dependent and reliant on the works being undertaken by an experienced contractor, high quality workmanship, and appropriate supervision of construction means and methods by experienced personnel.

In particular, the ultimate and serviceability limit state performance of the proposed underpins supporting the building loading in the temporary and long-term conditions should be assessed and monitored by an experienced engineer.

It is recommended that this report is reviewed and understood in full by the project team and major stakeholders. Where significant changes are made to items such as construction sequencing, temporary propping arrangements and scheme design the engineer should thoroughly review the discrepancy and evaluate any potential impacts on ground movement and building damage. If necessary, the building damage categories should be re-evaluated.

It is critical that the permanent and temporary works designs are carried out in a coordinated manner between performance specified elements and substructure contractors, with the aim to ensure that such design elements are in alignment with the assumptions/findings of the GMA and overall design intent.



## Appendix A: Selected Supporting Information

**Soils Consultants Limited - Site investigation Report and the appendices**  
**Akera Engineers - Proposed Construction sequence and Proposed drawings**



A-squared Studio

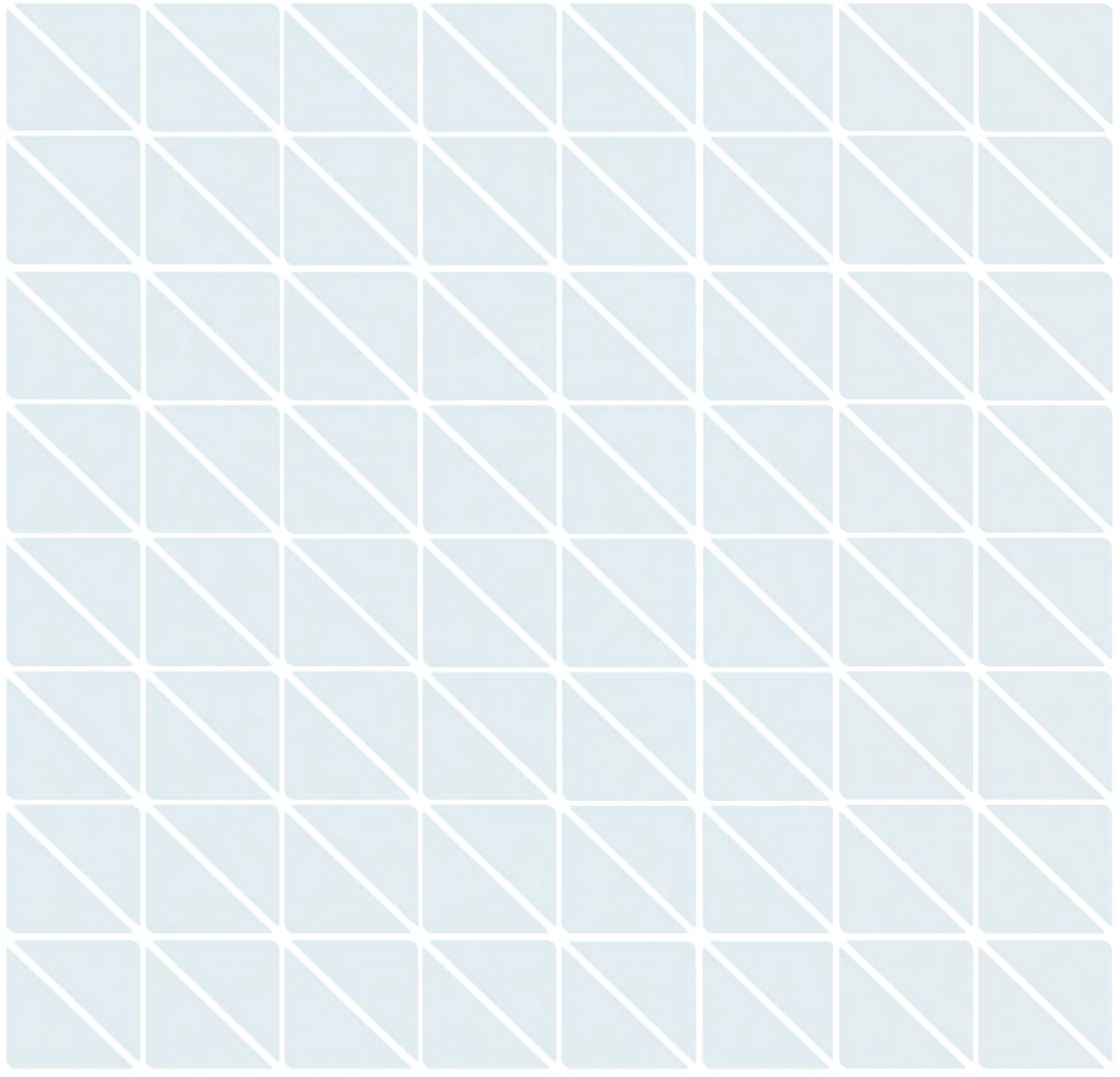
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**Project** 18A Frognal Gardens  
**Project No.** 1125  
**Subject** Ground Movement Assessment Report - Addendum  
**Client** Soil Consultants Ltd

Document Reference	Status	Revision	Issued	Checked	Approved	Date
1125-A2S-XX-XX-TN-Y-0001-00	First Issue – to be read in conjunction with 1125-A2S-XX-XX-RP-Y-0001-01	00	HS	PS	AN	14.10.2020

## 1. Introduction

This document is an addendum to 1125-A2S-XX-XX-RP-Y-0001-01 *Ground Movement Assessment Report* prepared by A-squared Studio Engineers Ltd (A-squared) on 17 July 2020. This addendum includes the supplementary information to the *Ground Movement Assessment Report* requested by Campbell Reith Hill Limited (Campbell Reith) on behalf of the London Borough of Camden.

## 2. Campbell Reith Comments

The following comments with regards to the *Ground Movement Assessment Report* were received from Campbell Reith by the project team on 1 September 2020:

1. *Can the full input and output data be provided for the PDisp and XDisp analysis please?*
2. *Regarding the use of the CIRIA C760 curve for “Installation of secant bored pile wall in stiff clay”, while we appreciate that, as stated in the BIA, this curve represents an upper bound for the data set, it is a requirement by LBC that the ground movement assessment adopts a moderately conservative approach. As such, the XDisp analysis should be amended to use the ground movement curve for a secant pile wall for the embedded retaining walls using this method of installation.*

## 3. Information Provided

Based on the comments above, the following information has been appended to this document:

- **Appendix A:** Pdisp input and output data for all modelled construction stages.
- **Appendix B:** Xdisp input and output data for all modelled construction stages.
- **Appendix C:** Plots showing discontinuity and peak smoothing of selected façades.

It is noted that the Xdisp input and output data for construction stages B01 and B02 incorporate the CIRIA C760 curve for “Installation of secant bored pile wall in stiff clay” instead of the curve for “Installation of contiguous bored pile wall in stiff clay” adopted in the *Ground Movement Assessment Report*. Sensitivity checks comparing the ground movements associated with each curve indicate that there is no significant additional impact on surrounding façades related to the adoption of the secant bored pile installation curve, as shown in the output data in Appendix B.



## Appendix A: Pdisp Input and Output Data





# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
Building GMA  
PDisp A01 - Demolition

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

### Titles

Job No.: 1125  
 Job Title: 18A Froggnal Gardens  
 Sub-title: Building GMA  
 Calculation Heading: PDisp A01 - Demolition  
 Initials: SB  
 Checker:  
 Date Saved:  
 Date Checked:  
 Notes:  
 File Name: PDisp A01.pdd  
 File Path: \\Mac\Dropbox for Business\A2-projects\1125 - 18a Froggnal Gardens\03 - Calculations\Issue 01\Pdisp

### History

Date	Time	By	Notes
14-Oct-2020	14:15	hamed	<history cleared>
14-Oct-2020	14:18	hamed	

### Analysis Options

#### General

Global Poisson's ratio: 0.50  
 Maximum allowable ratio between values of E: 1.5  
 Horizontal rigid boundary level: -34.00 [m OD]  
 Displacements at load centroids: Yes  
 GSA piled raft data: No

#### Elastic

Elastic: Yes  
 Analysis: Boussinesq  
 Stiffness for horizontal displacement calculations: Weighted average  
 Using legacy heave correction factor: No

#### Consolidation

Consolidation: No

### Soil Profiles Soil Profile 1

Layer ref.	Name	Level at top	Number of intermediate displacement levels	Youngs Modulus : Top	Youngs Modulus : Btm.	Poissons ratio	Non-linear curve
		[mOD]		[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]		
1	Made Ground	0.0	5	10000.	10000.	0.20000	None
2	Bagshot Formation	-1.0000	5	18000.	18000.	0.20000	None
3	London Clay	-7.0000	5	14400.	99450.	0.50000	None

### Soil Zones

Zone	Name	X min [m]	X max [m]	Y min [m]	Y max [m]	Profile
1	1	0.0	80.000	0.0	100.00	Soil Profile 1

### Polygonal Load Data

Load ref.	Name	Position : Level	Position : Polygon : Coords.	Position : Polygon : Rect. : Rect. tolerance	No. of Rectangles	Value : Normal (local z)	
		[m]	[m]	[%]		[kN/m <sup>2</sup> ]	
1	Demo - 3F	-2.75000	(34.7,49.1) (43.8,49.1) (43.8,46.4) (42.8,46.4) (42.8,42.3) (34.9,42.3) (34.7,42.3) (34.7,49.1)		10.000	2	-45.000
2	Demo - 2F	0.00000	(34.7,53.3) (43.8,53.3) (43.7,49.1) (34.7,49.1) (34.7,53.3)		10.000	1	-30.000

### Polygonal Loads' Rectangles

No.	Centre x	Centre y	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
<b>Load 1 : Demo - 3F</b> (Edge 7 optimal)					
1	38.75214	44.36162	90.266	4.0939	8.0366
2	39.27445	47.75430	90.266	2.6865	9.0839
<b>Load 2 : Demo - 2F</b> (Edge 4 optimal)					
1	39.23550	51.18897	179.84	8.9951	4.1869

### Displacement Lines

Name	X1 [m]	Y1 [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]	Intervals [No.]	Calculate	Detailed Results
18B.01	27.06970	56.10310	0.00000	32.02050	56.10310	0.00000	10	Yes	Yes
18B.02	32.02050	56.10310	0.00000	32.02020	53.28900	0.00000	6	Yes	Yes
18B.03	32.02020	53.28900	0.00000	34.29880	53.28910	0.00000	6	Yes	Yes
18B.04	34.29880	53.28910	0.00000	34.29900	42.12610	0.00000	24	Yes	Yes
18B.05	34.29900	42.12610	0.00000	27.03130	42.06780	0.00000	16	Yes	Yes
18B.06	27.03130	42.06780	0.00000	27.03130	42.81150	0.00000	2	Yes	Yes
18B.07	27.03130	42.81150	0.00000	27.06970	56.10310	0.00000	28	Yes	Yes
20FG.01	21.02660	64.09150	0.00000	24.26740	63.42960	0.00000	8	Yes	Yes
20FG.02	24.26740	63.42960	0.00000	23.31400	55.50790	0.00000	16	Yes	Yes
20FG.03	23.31400	55.50790	0.00000	24.37380	55.60010	0.00000	4	Yes	Yes
20FG.04	24.37380	55.60010	0.00000	23.83670	53.15770	0.00000	6	Yes	Yes
20FG.05	23.83670	53.15770	0.00000	24.42370	53.20880	0.00000	2	Yes	Yes
20FG.06	24.42370	53.20880	0.00000	23.90190	50.14280	0.00000	8	Yes	Yes
20FG.07	23.90190	50.14280	0.00000	24.42370	50.18820	0.00000	2	Yes	Yes
20FG.08	24.42370	50.18820	0.00000	24.30050	42.16640	0.00000	18	Yes	Yes
20FG.09	24.30050	42.16640	0.00000	20.99250	42.79780	0.00000	8	Yes	Yes
20FG.10	20.99250	42.79780	0.00000	21.33710	43.74710	0.00000	4	Yes	Yes
20FG.11	21.33710	43.74710	0.00000	12.81700	45.36940	0.00000	18	Yes	Yes
20FG.12	12.81700	45.36940	0.00000	14.97910	55.63720	0.00000	22	Yes	Yes
20FG.13	14.97910	55.63720	0.00000	13.19400	56.13840	0.00000	4	Yes	Yes
20FG.14	13.19400	56.13840	0.00000	13.67460	58.54420	0.00000	6	Yes	Yes
20FG.15	13.67460	58.54420	0.00000	19.98620	57.39750	0.00000	14	Yes	Yes
20FG.16	19.98620	57.39750	0.00000	21.02660	64.09150	0.00000	14	Yes	Yes
17HW.A01	58.70070	56.44780	0.00000	67.17010	55.69590	0.00000	18	Yes	Yes
17HW.A02	67.17010	55.69590	0.00000	66.89130	47.62280	0.00000	18	Yes	Yes
17HW.A03	66.89130	47.62280	0.00000	57.85650	48.31820	0.00000	20	Yes	Yes
17HW.A04	57.85650	48.31820	0.00000	58.70070	56.44780	0.00000	18	Yes	Yes



**A-SQUARED STUDIO ENGINEERS LTD**

**18A Froggnal Gardens Building GMA PDisp A01 - Demolition**

Job No. Sheet No. Rev.

**1125**

Drg. Ref.

Made by SB

Date

Checked

Name	X1	Y1	Z1	X2	Y2	Z2	Intervals	Calculate	Detailed Results
[m]	[m]	[m]	[m]	[m]	[m]	[m]	[No.]		
17HW.B01	58.67890	60.09730	0.00000	59.04640	56.41710	0.00000	8	Yes	Yes
17HW.B02	59.04640	56.41710	0.00000	62.51490	56.10130	0.00000	8	Yes	Yes
17HW.B03	62.51490	56.10130	0.00000	62.69950	59.74720	0.00000	8	Yes	Yes
17HW.B04	62.69950	59.74720	0.00000	58.67890	60.09730	0.00000	10	Yes	Yes

**Results : Immediate : Load Centres : Polygonal**

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
1	Demo - 3F	38.97665	45.80077	-2.75000	-14.37462	-3.2813	-46.738	-124.19	-0.0017360
2	Demo - 2F	39.23031	51.19083	0.00000	-11.46353	-0.083333	-29.999	-87.486	-0.0018502

**Results : Consolidation : Load Centres : Polygonal**

None

**Results : Total : Load Centres : Polygonal**

None

**Results : Immediate : Displacement Data : Lines**

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
1	18B.01	27.06970	56.10310	0.00000	-0.20141	-0.083333	-1.3325E-6	-0.024271	489.26E-9
1	18B.01	27.19550	42.8905	0.00000	-2.23934	-0.083333	-1.6448E-6	-0.027342	546.65E-9
1	18B.01	28.05986	56.10310	0.00000	-0.27546	-0.083333	-2.0472E-6	-0.030933	618.42E-9
1	18B.01	28.55494	56.10310	0.00000	-0.31917	-0.083333	-2.5706E-6	-0.035151	702.72E-9
1	18B.01	29.05002	56.10310	0.00000	-0.36796	-0.083333	-3.2579E-6	-0.040129	802.19E-9
1	18B.01	29.54510	56.10310	0.00000	-0.42233	-0.083333	-4.1693E-6	-0.046031	920.13E-9
1	18B.01	30.04018	56.10310	0.00000	-0.48077	-0.083333	-5.3903E-6	-0.053060	1.0605E-6
1	18B.01	30.53526	56.10310	0.00000	-0.54979	-0.083333	-7.0417E-6	-0.061460	1.2294E-6
1	18B.01	31.03034	56.10310	0.00000	-0.62380	-0.083333	-9.2947E-6	-0.071530	1.4295E-6
1	18B.01	31.52542	56.10310	0.00000	-0.70515	-0.083333	-12.389E-6	-0.083617	1.6708E-6
1	18B.01	32.02050	56.10310	0.00000	-0.79401	-0.083333	-16.652E-6	-0.098104	1.9601E-6
2	18B.02	32.02055	59.75802	0.00000	-1.34329	-0.083333	-65.601E-6	-0.19691	3.3033E-6
2	18B.02	32.02045	55.63408	0.00000	-0.88967	-0.083333	-22.091E-6	-0.11322	2.2617E-6
2	18B.02	32.02040	55.16507	0.00000	-0.99318	-0.083333	-29.412E-6	-0.13079	2.6122E-6
2	18B.02	32.02035	54.69605	0.00000	-1.10406	-0.083333	-39.050E-6	-0.15087	3.0128E-6
2	18B.02	32.02030	54.22703	0.00000	-1.22131	-0.083333	-51.220E-6	-0.17319	3.4576E-6
2	18B.02	32.02020	53.28900	0.00000	-1.46782	-0.083333	-81.101E-6	-0.22063	4.4029E-6
3	18B.03	32.02020	53.28900	0.00000	-1.46782	-0.083333	-81.101E-6	-0.22063	4.4029E-6
3	18B.03	32.39997	53.28902	0.00000	-1.65016	-0.083333	-131.63E-6	-0.28045	5.5933E-6
3	18B.03	32.77973	53.28903	0.00000	-1.85857	-0.083333	-230.31E-6	-0.36707	7.3137E-6
3	18B.03	33.15950	42.8905	0.00000	-2.23934	-0.083333	-49.15E-6	-0.50027	9.9516E-6
3	18B.03	33.53927	53.28907	0.00000	-2.38239	-0.083333	-0.0010388	-0.72476	14.371E-6
3	18B.03	33.91903	53.28908	0.00000	-2.72600	-0.083333	-0.0032586	-1.1669	22.948E-6
3	18B.03	34.29880	53.28910	0.00000	-3.17392	-0.083333	-0.020383	-2.3752	45.059E-6
4	18B.04	34.29880	53.28910	0.00000	-3.17392	-0.083333	-0.020383	-2.3752	45.059E-6
4	18B.04	34.29882	52.35885	0.00000	-4.04851	-0.083333	-0.039582	-3.9774	74.798E-6
4	18B.04	34.29883	51.89372	0.00000	-4.38699	-0.083333	-0.040638	-4.2068	79.259E-6
4	18B.04	34.29883	51.42860	0.00000	-4.68105	-0.083333	-0.041185	-4.3062	81.182E-6
4	18B.04	34.29884	50.96347	0.00000	-4.94391	-0.083333	-0.041548	-4.3204	81.423E-6
4	18B.04	34.29885	49.98325	0.00000	-5.18566	-0.083333	-0.041722	-4.2486	79.964E-6
4	18B.04	34.29886	50.03323	0.00000	-5.41506	-0.083333	-0.041357	-4.0425	75.888E-6
4	18B.04	34.29887	49.56810	0.00000	-5.64189	-0.083333	-0.038253	-3.5412	66.234E-6
4	18B.04	34.29888	49.10298	0.00000	-5.87198	-0.083333	-0.021310	-2.4054	45.550E-6
4	18B.04	34.29888	48.63785	0.00000	-6.08406	-0.083333	-0.0045358	-1.2696	24.847E-6
4	18B.04	34.29889	48.17272	0.00000	-6.2437	-0.083333	-0.001175	-0.74456	14.750E-6
4	18B.04	34.29890	47.70760	0.00000	-6.34222	-0.083333	-437.41E-6	-0.49264	9.8002E-6
4	18B.04	34.29891	47.24247	0.00000	-6.39518	-0.083333	-203.20E-6	-0.35175	7.0106E-6
4	18B.04	34.29892	46.77735	0.00000	-6.40587	-0.083333	-108.78E-6	-0.26402	5.2673E-6
4	18B.04	34.29892	46.31222	0.00000	-6.37782	-0.083333	-64.105E-6	-0.20524	4.0970E-6
4	18B.04	34.29894	45.84710	0.00000	-6.30594	-0.083333	-40.472E-6	-0.1374	3.269E-6
4	18B.04	34.29894	45.38197	0.00000	-6.18633	-0.083333	-26.907E-6	-0.13328	2.6624E-6
4	18B.04	34.29895	44.91685	0.00000	-6.01817	-0.083333	-18.621E-6	-0.11025	2.2027E-6
4	18B.04	34.29896	44.45172	0.00000	-5.79787	-0.083333	-13.306E-6	-0.092403	1.8465E-6
4	18B.04	34.29897	43.98660	0.00000	-5.51860	-0.083333	-9.7596E-6	-0.078309	1.5650E-6
4	18B.04	34.29897	43.52148	0.00000	-5.18922	-0.083333	-7.3164E-6	-0.06696	1.3390E-6
4	18B.04	34.29898	43.05635	0.00000	-4.73504	-0.083333	-5.5870E-6	-0.057790	1.1551E-6
4	18B.04	34.29899	42.59123	0.00000	-4.19096	-0.083333	-4.3345E-6	-0.050211	1.0037E-6
4	18B.04	34.29900	42.12610	0.00000	-3.56190	-0.083333	-3.4095E-6	-0.043908	877.75E-9
5	18B.05	34.29900	42.12610	0.00000	-3.56190	-0.083333	-3.4095E-6	-0.043908	877.75E-9
5	18B.05	33.84477	42.12446	0.00000	-2.95241	-0.083333	-3.1123E-6	-0.0382	729.46E-9
5	18B.05	33.9054	42.11881	0.00000	-2.48791	-0.083333	-2.8225E-6	-0.039068	681.02E-9
5	18B.05	32.93631	42.11517	0.00000	-2.11384	-0.083333	-2.5433E-6	-0.036667	733.02E-9
5	18B.05	32.48208	42.11153	0.00000	-1.80501	-0.083333	-2.2790E-6	-0.034316	686.04E-9
5	18B.05	32.02784	42.10788	0.00000	-1.54662	-0.083333	-2.0324E-6	-0.032037	640.50E-9
5	18B.05	32.52625	42.08240	0.00000	-2.35932	-0.083333	-1.8050E-6	-0.029850	596.78E-9
5	18B.05	31.11938	42.10059	0.00000	-1.14339	-0.083333	-1.5976E-6	-0.027766	555.12E-9
5	18B.05	30.66515	42.09695	0.00000	-0.98540	-0.083333	-1.4103E-6	-0.025794	515.71E-9
5	18B.05	30.21092	42.09331	0.00000	-0.85008	-0.083333	-1.2424E-6	-0.023940	478.64E-9
5	18B.05	29.75669	42.08966	0.00000	-0.73378	-0.083333	-1.0930E-6	-0.022204	443.95E-9
5	18B.05	29.30246	42.08602	0.00000	-0.63348	-0.083333	-960.65E-9	-0.020596	411.61E-9
5	18B.05	28.84822	42.08237	0.00000	-0.54673	-0.083333	-843.98E-9	-0.019084	381.57E-9
5	18B.05	28.39399	42.07873	0.00000	-0.47147	-0.083333	-741.47E-9	-0.017692	353.75E-9
5	18B.05	27.93976	42.07509	0.00000	-0.40600	-0.083333	-651.63E-9	-0.016406	328.04E-9
5	18B.05	27.48553	42.07144	0.00000	-0.34888	-0.083333	-573.03E-9	-0.015219	304.32E-9
5	18B.05	27.03130	42.06780	0.00000	-0.29992	-0.083333	-504.36E-9	-0.014126	282.46E-9
6	18B.06	27.03130	42.06780	0.00000	-0.29992	-0.083333	-504.36E-9	-0.014126	282.46E-9
6	18B.06	27.03130	42.43965	0.00000	-0.31445	-0.083333	-551.38E-9	-0.014854	297.01E-9
6	18B.06	27.03130	42.81150	0.00000	-0.32956	-0.083333	-602.64E-9	-0.015615	312.23E-9
7	18B.07	27.03130	42.81150	0.00000	-0.32956	-0.083333	-602.64E-9	-0.015615	312.23E-9
7	18B.07	27.03130	43.18335	0.00000	-0.34469	-0.083333	-674.92E-9	-0.016619	332.71E-9
7	18B.07	27.03404	43.76090	0.00000	-0.36582	-0.083333	-755.07E-9	-0.017717	354.24E-9
7	18B.07	27.03541	44.23560	0.00000	-0.38209	-0.083333	-843.43E-9	-0.018844	376.77E-9
7	18B.07	27.03679	44.71030	0.00000	-0.39685	-0.083333	-940.17E-9	-0.020016	400.20E-9
7	18B.07	27.03816	45.18500	0.00000	-0.40988	-0.083333	-1.0452E-6	-0.021225	424.38E-9
7	18B.07	27.03953	45.65970	0.00000	-0.42104	-0.083333	-1.1579E-6	-0.022462	449.14E-9
7	18B.07	27.04090	46.13440	0.00000	-0.43018	-0.083333	-1.2776E-6	-0.023715	474.14E-9
7	18B.07	27.04227	46.60910	0.00000	-0.43719	-0.083333	-1.4026E-6	-0.024966	499.15E-9
7	18B.07	27.04364	47.08380	0.00000	-0.44200	-0.083333	-1.5310E-6	-0.026199	523.79E-9
7	18B.07	27.04501	47.55850	0.00000	-0.44455	-0.083333	-1.6600E-6	-0.027390	547.61E-9
7	18B.07	27.04639	48.03320	0.00000	-0.44483	-0.083333	-1.7865E-6	-0.028518	570.14E-9
7	18B.07	27.04776	48.50790	0.00000	-0.44284	-0.083333	-1.9066E-6	-0.029556	590.90E-9
7	18B.07	27.04913	48.98260	0.00000	-0.43862	-0.083333	-2.0164E-6	-0.030480	609.35E-9
7	18B.07	27.05050	49.45730	0.00000	-0.43224	-0.083333	-2.1117E-6	-0.031264	625.02E-9
7	18B.07	27.05187	49.93200	0.00000	-0.42379	-0.083333	-2.1887E-6	-0.031886	637.46E-9
7	18B.07	27.05324	50.40670	0.00000	-0.41326	-0.083333	-2.244		



# A-SQUARED STUDIO ENGINEERS LTD

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

18A FrognaI Gardens  
Building GMA  
PDisp A01 - Demolition

Ref.	Name	x	y	z	δz	Stress: Calc.	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
	[m]	[m]	[mOD]	[mm]		Level [mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[μ]
7	18B.07	27.06421	54.20430	0.00000	-0.28018	-0.083333	-1.8408E-6	-0.028991	579.60E-9
7	18B.07	27.06559	54.67900	0.00000	-0.26033	-0.083333	-1.7166E-6	-0.027900	557.79E-9
7	18B.07	27.06696	55.15370	0.00000	-0.24047	-0.083333	-1.5883E-6	-0.026734	534.48E-9
7	18B.07	27.06833	55.62840	0.00000	-0.22078	-0.083333	-1.4593E-6	-0.025516	510.15E-9
7	18B.07	27.06970	56.10310	0.00000	-0.20141	-0.083333	-1.3325E-6	-0.024271	485.26E-9
8	20FG.01	21.02660	64.09550	0.00000	0.05550	-0.083333	-64.576E-9	-0.004561	85.115E-9
8	20FG.01	21.43170	64.00876	0.00000	0.05364	-0.083333	-70.567E-9	-0.0044851	89.694E-9
8	20FG.01	21.83680	63.92602	0.00000	0.05156	-0.083333	-77.211E-9	-0.0047298	94.587E-9
8	20FG.01	22.24190	63.84329	0.00000	0.04923	-0.083333	-84.588E-9	-0.0049916	99.822E-9
8	20FG.01	22.64700	63.76055	0.00000	0.04664	-0.083333	-92.791E-9	-0.0052718	105.44E-9
8	20FG.01	23.05210	63.67781	0.00000	0.04376	-0.083333	-101.92E-9	-0.0055719	111.43E-9
8	20FG.01	23.45720	63.59508	0.00000	0.04058	-0.083333	-112.10E-9	-0.0058937	117.86E-9
8	20FG.01	23.86230	63.51234	0.00000	0.03707	-0.083333	-123.46E-9	-0.0062387	124.76E-9
8	20FG.01	24.26740	63.42960	0.00000	0.03322	-0.083333	-136.15E-9	-0.0066091	132.17E-9
9	20FG.02	24.26740	63.42960	0.00000	0.03322	-0.083333	-136.15E-9	-0.0066091	132.17E-9
9	20FG.02	24.20781	62.93449	0.00000	0.02960	-0.083333	-147.27E-9	-0.0069144	138.27E-9
9	20FG.02	24.14823	62.43939	0.00000	0.02575	-0.083333	-159.12E-9	-0.0072281	144.54E-9
9	20FG.02	24.08864	61.94428	0.00000	0.02169	-0.083333	-171.68E-9	-0.0075494	150.97E-9
9	20FG.02	24.02905	61.44917	0.00000	0.01741	-0.083333	-184.94E-9	-0.0078769	157.52E-9
9	20FG.02	23.96946	60.95407	0.00000	0.01294	-0.083333	-198.84E-9	-0.0082091	164.16E-9
9	20FG.02	23.90987	60.45896	0.00000	0.00829	-0.083333	-213.37E-9	-0.0085441	170.86E-9
9	20FG.02	23.85029	59.96386	0.00000	0.00348	-0.083333	-228.33E-9	-0.0088799	177.57E-9
9	20FG.02	23.79070	59.46875	0.00000	-0.00147	-0.083333	-243.73E-9	-0.0092140	184.25E-9
9	20FG.02	23.73111	58.97364	0.00000	-0.00654	-0.083333	-259.38E-9	-0.0095437	190.84E-9
9	20FG.02	23.67152	58.47854	0.00000	-0.01168	-0.083333	-275.12E-9	-0.0098660	197.29E-9
9	20FG.02	23.61194	57.98343	0.00000	-0.01682	-0.083333	-290.76E-9	-0.0101779	203.52E-9
9	20FG.02	23.55235	57.48833	0.00000	-0.02204	-0.083333	-306.07E-9	-0.0104755	209.46E-9
9	20FG.02	23.49276	56.99322	0.00000	-0.02719	-0.083333	-320.82E-9	-0.0107555	215.06E-9
9	20FG.02	23.43317	56.49811	0.00000	-0.03224	-0.083333	-334.74E-9	-0.0110103	220.23E-9
9	20FG.02	23.37359	56.00301	0.00000	-0.03717	-0.083333	-347.58E-9	-0.0112447	224.90E-9
9	20FG.02	23.31399	55.50790	0.00000	-0.04191	-0.083333	-359.07E-9	-0.0114525	229.00E-9
10	20FG.03	23.31400	55.50790	0.00000	-0.04191	-0.083333	-359.07E-9	-0.0114525	229.00E-9
10	20FG.03	23.25795	55.03095	0.00000	-0.04982	-0.083333	-391.29E-9	-0.012034	240.63E-9
10	20FG.03	23.84390	55.55400	0.00000	-0.05823	-0.083333	-426.98E-9	-0.012654	253.03E-9
10	20FG.03	24.10885	55.57705	0.00000	-0.06715	-0.083333	-466.60E-9	-0.013317	266.29E-9
10	20FG.03	24.37180	55.60010	0.00000	-0.07662	-0.083333	-510.65E-9	-0.014026	280.46E-9
11	20FG.04	24.37380	55.60010	0.00000	-0.07662	-0.083333	-510.65E-9	-0.014026	280.46E-9
11	20FG.04	24.28428	55.19303	0.00000	-0.08033	-0.083333	-518.04E-9	-0.014133	282.60E-9
11	20FG.04	24.19477	54.78597	0.00000	-0.08370	-0.083333	-523.11E-9	-0.014204	284.03E-9
11	20FG.04	24.10525	54.37890	0.00000	-0.08669	-0.083333	-525.75E-9	-0.014239	284.71E-9
11	20FG.04	24.01573	53.97183	0.00000	-0.08929	-0.083333	-525.48E-9	-0.014222	284.64E-9
11	20FG.04	23.92622	53.56477	0.00000	-0.09145	-0.083333	-523.59E-9	-0.014194	283.81E-9
11	20FG.04	23.83670	53.15770	0.00000	-0.09317	-0.083333	-518.81E-9	-0.014115	282.25E-9
12	20FG.05	23.83670	53.15770	0.00000	-0.09317	-0.083333	-518.81E-9	-0.014115	282.25E-9
12	20FG.05	24.13020	53.18325	0.00000	-0.10653	-0.083333	-578.47E-9	-0.015023	300.38E-9
12	20FG.05	24.41901	53.20980	0.00000	-0.12090	-0.083333	-646.63E-9	-0.016010	320.12E-9
13	20FG.06	24.42370	53.20880	0.00000	-0.12090	-0.083333	-646.63E-9	-0.016010	320.12E-9
13	20FG.06	24.35847	52.82555	0.00000	-0.12360	-0.083333	-643.66E-9	-0.015964	319.20E-9
13	20FG.06	24.29325	52.44230	0.00000	-0.12584	-0.083333	-637.84E-9	-0.015878	317.49E-9
13	20FG.06	24.22803	52.05905	0.00000	-0.12760	-0.083333	-629.28E-9	-0.015754	315.01E-9
13	20FG.06	24.16281	51.67580	0.00000	-0.12887	-0.083333	-618.15E-9	-0.015599	307.86E-9
13	20FG.06	24.09757	51.29255	0.00000	-0.12964	-0.083333	-604.60E-9	-0.015396	307.86E-9
13	20FG.06	24.03235	50.90930	0.00000	-0.12991	-0.083333	-588.93E-9	-0.015167	303.28E-9
13	20FG.06	23.96712	50.52605	0.00000	-0.12967	-0.083333	-571.36E-9	-0.014908	298.10E-9
13	20FG.06	23.90190	50.14280	0.00000	-0.12893	-0.083333	-552.20E-9	-0.014622	292.37E-9
14	20FG.07	24.16281	52.28280	0.00000	-0.12967	-0.083333	-571.36E-9	-0.014908	298.10E-9
14	20FG.07	24.16280	50.16550	0.00000	-0.14411	-0.083333	-610.73E-9	-0.015488	309.69E-9
14	20FG.07	24.42370	50.18820	0.00000	-0.16041	-0.083333	-677.02E-9	-0.016426	328.45E-9
14	20FG.07	24.42370	50.18820	0.00000	-0.16041	-0.083333	-677.02E-9	-0.016426	328.45E-9
15	20FG.08	24.41686	49.74254	0.00000	-0.16346	-0.083333	-664.08E-9	-0.016250	324.92E-9
15	20FG.08	24.41686	49.74254	0.00000	-0.16346	-0.083333	-664.08E-9	-0.016250	324.92E-9
15	20FG.08	24.40317	48.85123	0.00000	-0.16729	-0.083333	-628.07E-9	-0.015751	314.95E-9
15	20FG.08	24.39632	48.40558	0.00000	-0.16804	-0.083333	-605.83E-9	-0.015437	308.66E-9
15	20FG.08	24.38948	47.95992	0.00000	-0.16800	-0.083333	-581.40E-9	-0.015085	301.63E-9
15	20FG.08	24.38263	47.51427	0.00000	-0.16716	-0.083333	-555.26E-9	-0.014702	293.97E-9
15	20FG.08	24.37579	47.06861	0.00000	-0.16553	-0.083333	-527.90E-9	-0.014291	285.76E-9
15	20FG.08	24.36894	46.62296	0.00000	-0.16332	-0.083333	-499.78E-9	-0.013859	277.12E-9
15	20FG.08	24.36210	46.17730	0.00000	-0.15997	-0.083333	-471.31E-9	-0.013410	268.15E-9
15	20FG.08	24.35526	45.73164	0.00000	-0.15610	-0.083333	-442.89E-9	-0.012950	258.94E-9
15	20FG.08	24.34841	45.28599	0.00000	-0.15155	-0.083333	-414.83E-9	-0.012481	249.58E-9
15	20FG.08	24.34157	44.84033	0.00000	-0.14629	-0.083333	-387.40E-9	-0.012010	240.15E-9
15	20FG.08	24.33472	44.39468	0.00000	-0.14059	-0.083333	-360.89E-9	-0.011538	230.77E-9
15	20FG.08	24.32788	43.94902	0.00000	-0.13428	-0.083333	-335.40E-9	-0.011070	221.36E-9
15	20FG.08	24.32103	43.50337	0.00000	-0.12751	-0.083333	-311.09E-9	-0.010608	212.13E-9
15	20FG.08	24.31419	43.05771	0.00000	-0.12033	-0.083333	-288.04E-9	-0.010155	203.06E-9
15	20FG.08	24.30734	42.61206	0.00000	-0.11287	-0.083333	-266.29E-9	-0.009711	194.20E-9
15	20FG.08	24.30050	42.16640	0.00000	-0.10500	-0.083333	-245.88E-9	-0.0092805	185.58E-9
16	20FG.09	24.30050	42.16640	0.00000	-0.10500	-0.083333	-245.88E-9	-0.0092805	185.58E-9
16	20FG.09	23.88700	42.24533	0.00000	-0.08710	-0.083333	-223.80E-9	-0.0087818	175.61E-9
16	20FG.09	23.47350	42.32425	0.00000	-0.07089	-0.083333	-203.74E-9	-0.0083111	166.20E-9
16	20FG.09	23.05910	42.40318	0.00000	-0.05541	-0.083333	-185.58E-9	-0.0078672	157.32E-9
16	20FG.09	22.64650	42.48210	0.00000	-0.04293	-0.083333	-169.06E-9	-0.0074489	148.36E-9
16	20FG.09	22.23300	42.56103	0.00000	-0.03091	-0.083333	-154.11E-9	-0.0070550	141.08E-9
16	20FG.09	21.81950	42.63995	0.00000	-0.02003	-0.083333	-140.57E-9	-0.0066843	133.67E-9
16	20FG.09	21.40600	42.71888	0.00000	-0.01020	-0.083333	-128.30E-9	-0.0063354	126.69E-9
16	20FG.09	21.03500	42.79780	0.00000	0.00117	-0.083333	-117.19E-9	-0.0060000	120.61E-9
17	20FG.10	20.99250	42.79780	0.00000	0.00131	-0.083333	-117.19E-9	-0.0060071	120.13E-9
17	20FG.10	21.07865	43.03513	0.00000	-0.00457	-0.083333	-123.13E-9	-0.0061816	123.62E-9
17	20FG.10	21.16480	43.27245	0.00000	-0.00790	-0.083333	-129.39E-9	-0.0063614	127.21E-9
17	20FG.10	21.25095	43.50978	0.00000	-0.01131	-0.083333	-135.97E-9	-0.0065467	130.92E-9
17	20FG.10	21.33710	43.74710	0.00000	-0.01478	-0.083333	-142.90E-9	-0.0067344	134.73E-9
18	20FG.11	21.33710	43.74710	0.00000	-0.01478	-0.083333	-142.90E-9	-0.0067374	134.73E-9
18	20FG.11	20.86376	43.83723	0.00000	-0.00396	-0.083333	-127.99E-9	-0.0063163	126.31E-9
18	20FG.11	20.39042							



# A-SQUARED STUDIO ENGINEERS LTD

Job No.	Sheet No.	Rev.
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1125		
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Drg. Ref.	
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Made by SB	Date	Checked
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Ref.	Name	x	y	z	dz	Stress: Calc.	Stress: Vertical Level	Stress: Sum Princ.	Vert. Strain
	[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m²]	[kN/m²]	[µ]	
19	20FG.12	14.78255	54.70376	0.00000	0.06174	-0.083333	-39.719E-9	-0.0031728	63.452E-9
19	20FG.12	14.88082	55.17048	0.00000	0.06175	-0.083333	-39.911E-9	-0.0031822	63.640E-9
19	20FG.12	14.97910	55.63720	0.00000	0.06179	-0.083333	-40.019E-9	-0.0031878	63.750E-9
20	20FG.13	14.97910	55.63720	0.00000	0.06179	-0.083333	-40.019E-9	-0.0031878	63.750E-9
20	20FG.13	14.53283	55.76250	0.00000	0.06299	-0.083333	-36.264E-9	-0.0030093	60.162E-9
20	20FG.13	14.08655	55.88780	0.00000	0.06396	-0.083333	-32.927E-9	-0.0028422	56.840E-9
20	20FG.13	13.64028	56.01310	0.00000	0.06471	-0.083333	-29.953E-9	-0.0026881	53.759E-9
20	20FG.13	13.19400	56.13840	0.00000	0.06528	-0.083333	-27.299E-9	-0.0025451	50.899E-9
21	20FG.14	13.19400	56.13840	0.00000	0.06528	-0.083333	-27.299E-9	-0.0025451	50.899E-9
21	20FG.14	13.27410	56.53937	0.00000	0.06527	-0.083333	-27.282E-9	-0.0025445	50.886E-9
21	20FG.14	13.34420	56.94033	0.00000	0.06527	-0.083333	-27.229E-9	-0.0025419	50.834E-9
21	20FG.14	13.43430	57.34130	0.00000	0.06527	-0.083333	-27.141E-9	-0.0025374	50.744E-9
21	20FG.14	13.51440	57.74227	0.00000	0.06528	-0.083333	-27.018E-9	-0.0025309	50.615E-9
21	20FG.14	13.59450	58.14323	0.00000	0.06528	-0.083333	-26.860E-9	-0.0025226	50.449E-9
21	20FG.14	13.67460	58.54420	0.00000	0.06529	-0.083333	-26.670E-9	-0.0025124	50.245E-9
22	20FG.15	14.02827	58.64666	0.00000	0.06529	-0.083333	-26.670E-9	-0.0025124	50.245E-9
22	20FG.15	14.12543	58.46229	0.00000	0.06486	-0.083333	-29.207E-9	-0.0026508	53.012E-9
22	20FG.15	14.57626	58.38039	0.00000	0.06425	-0.083333	-32.040E-9	-0.0027995	55.986E-9
22	20FG.15	15.02709	58.29848	0.00000	0.06347	-0.083333	-35.212E-9	-0.0029596	59.188E-9
22	20FG.15	15.47791	58.21657	0.00000	0.06249	-0.083333	-38.771E-9	-0.0031323	62.641E-9
22	20FG.15	15.92874	58.13466	0.00000	0.06128	-0.083333	-42.771E-9	-0.0033187	66.368E-9
22	20FG.15	16.37957	58.05276	0.00000	0.05983	-0.083333	-47.285E-9	-0.0035202	70.399E-9
22	20FG.15	16.83040	57.97085	0.00000	0.05810	-0.083333	-52.383E-9	-0.0037386	74.765E-9
22	20FG.15	17.28123	57.88894	0.00000	0.05606	-0.083333	-58.161E-9	-0.0039755	79.502E-9
22	20FG.15	17.73206	57.80704	0.00000	0.05369	-0.083333	-64.725E-9	-0.0042329	84.650E-9
22	20FG.15	18.18289	57.72513	0.00000	0.05124	-0.083333	-72.206E-9	-0.0045132	90.259E-9
22	20FG.15	18.63371	57.64322	0.00000	0.04777	-0.083333	-80.757E-9	-0.0048190	96.370E-9
22	20FG.15	19.08454	57.56131	0.00000	0.04414	-0.083333	-90.562E-9	-0.0051532	103.05E-9
22	20FG.15	19.53537	57.47941	0.00000	0.03998	-0.083333	-101.84E-9	-0.0055193	110.37E-9
22	20FG.15	19.98620	57.39750	0.00000	0.03525	-0.083333	-114.86E-9	-0.0059211	118.41E-9
23	20FG.16	20.43703	57.31560	0.00000	0.03052	-0.083333	-129.86E-9	-0.0063927	127.13E-9
23	20FG.16	20.06051	57.87564	0.00000	0.03671	-0.083333	-112.02E-9	-0.0058377	116.74E-9
23	20FG.16	20.13483	58.35379	0.00000	0.03821	-0.083333	-108.92E-9	-0.0057456	114.90E-9
23	20FG.16	20.20914	58.83193	0.00000	0.03975	-0.083333	-105.61E-9	-0.0056455	112.90E-9
23	20FG.16	20.28346	59.31007	0.00000	0.04129	-0.083333	-102.11E-9	-0.0055384	110.76E-9
23	20FG.16	20.35777	59.78821	0.00000	0.04287	-0.083333	-98.471E-9	-0.0054219	108.49E-9
23	20FG.16	20.43209	60.26636	0.00000	0.04440	-0.083333	-94.727E-9	-0.0053061	106.11E-9
23	20FG.16	20.50640	60.74450	0.00000	0.04594	-0.083333	-90.912E-9	-0.0051828	103.64E-9
23	20FG.16	20.58071	61.22264	0.00000	0.04744	-0.083333	-87.058E-9	-0.0050557	101.10E-9
23	20FG.16	20.65503	61.70079	0.00000	0.04892	-0.083333	-83.194E-9	-0.0049257	98.503E-9
23	20FG.16	20.72934	62.17893	0.00000	0.05039	-0.083333	-79.349E-9	-0.0047934	95.859E-9
23	20FG.16	20.80366	62.65707	0.00000	0.05173	-0.083333	-75.544E-9	-0.0046597	93.186E-9
23	20FG.16	20.87797	63.13521	0.00000	0.05305	-0.083333	-71.802E-9	-0.0045252	90.496E-9
23	20FG.16	20.95229	63.61336	0.00000	0.05430	-0.083333	-68.141E-9	-0.0043905	87.802E-9
23	20FG.16	21.02660	64.09150	0.00000	0.05558	-0.083333	-64.576E-9	-0.0042561	85.115E-9
24	17HW.A01	58.39517	59.28780	0.00000	0.03459	-0.083333	-117.44E-9	-0.0049137	113.65E-9
24	17HW.A01	59.17122	56.40603	0.00000	0.03918	-0.083333	-104.39E-9	-0.0055951	111.89E-9
24	17HW.A01	59.64174	56.36426	0.00000	0.04325	-0.083333	-93.021E-9	-0.0052303	104.60E-9
24	17HW.A01	60.11227	56.32248	0.00000	0.04684	-0.083333	-83.092E-9	-0.0048959	97.908E-9
24	17HW.A01	60.58279	56.28071	0.00000	0.05000	-0.083333	-74.395E-9	-0.0045889	91.769E-9
24	17HW.A01	61.05332	56.23894	0.00000	0.05277	-0.083333	-66.735E-9	-0.0043072	85.232E-9
24	17HW.A01	61.52383	56.19717	0.00000	0.05519	-0.083333	-60.034E-9	-0.0040465	80.923E-9
24	17HW.A01	61.99436	56.15539	0.00000	0.05728	-0.083333	-54.100E-9	-0.0038066	76.126E-9
24	17HW.A01	62.46488	56.11362	0.00000	0.05907	-0.083333	-48.850E-9	-0.0035850	71.695E-9
24	17HW.A01	62.93540	56.07185	0.00000	0.06060	-0.083333	-44.196E-9	-0.0033801	67.597E-9
24	17HW.A01	63.40592	56.03008	0.00000	0.06235	-0.083333	-39.702E-9	-0.0031905	63.805E-9
24	17HW.A01	63.87644	55.98831	0.00000	0.06294	-0.083333	-36.377E-9	-0.0030142	60.279E-9
24	17HW.A01	64.34697	55.94653	0.00000	0.06381	-0.083333	-33.090E-9	-0.0028507	57.009E-9
24	17HW.A01	64.81749	55.90476	0.00000	0.06449	-0.083333	-30.151E-9	-0.0026986	53.969E-9
24	17HW.A01	65.28801	55.86299	0.00000	0.06500	-0.083333	-27.519E-9	-0.0025571	51.139E-9
24	17HW.A01	65.75853	55.82122	0.00000	0.06537	-0.083333	-25.156E-9	-0.0024252	48.500E-9
24	17HW.A01	66.22906	55.77944	0.00000	0.06560	-0.083333	-23.031E-9	-0.0023021	46.039E-9
24	17HW.A01	66.69958	55.73767	0.00000	0.06571	-0.083333	-21.117E-9	-0.0021871	43.739E-9
24	17HW.A01	67.17010	55.69590	0.00000	0.06571	-0.083333	-19.389E-9	-0.0020796	41.589E-9
25	17HW.A02	67.17010	55.69590	0.00000	0.06571	-0.083333	-19.389E-9	-0.0020796	41.589E-9
25	17HW.A02	67.64062	55.65413	0.00000	0.06571	-0.083333	-17.702E-9	-0.0019911	39.509E-9
25	17HW.A02	67.13912	54.99889	0.00000	0.06583	-0.083333	-19.994E-9	-0.0021173	42.343E-9
25	17HW.A02	67.12363	54.35038	0.00000	0.06588	-0.083333	-20.264E-9	-0.0021340	42.677E-9
25	17HW.A02	67.10814	53.90188	0.00000	0.06593	-0.083333	-20.510E-9	-0.0021491	42.980E-9
25	17HW.A02	67.09266	53.45337	0.00000	0.06597	-0.083333	-20.731E-9	-0.0021626	43.250E-9
25	17HW.A02	67.07717	52.90487	0.00000	0.06600	-0.083333	-20.926E-9	-0.0021745	43.488E-9
25	17HW.A02	67.06168	52.55636	0.00000	0.06604	-0.083333	-21.093E-9	-0.0021847	43.691E-9
25	17HW.A02	67.04619	52.10786	0.00000	0.06607	-0.083333	-21.232E-9	-0.0021931	43.860E-9
25	17HW.A02	67.03070	51.65935	0.00000	0.06611	-0.083333	-21.342E-9	-0.0021997	43.992E-9
25	17HW.A02	67.01521	51.21084	0.00000	0.06614	-0.083333	-21.421E-9	-0.0022046	44.089E-9
25	17HW.A02	66.99972	50.76234	0.00000	0.06617	-0.083333	-21.471E-9	-0.0022076	44.149E-9
25	17HW.A02	66.98423	50.31383	0.00000	0.06620	-0.083333	-21.489E-9	-0.0022087	44.172E-9
25	17HW.A02	66.96874	49.86533	0.00000	0.06624	-0.083333	-21.477E-9	-0.0022080	44.158E-9
25	17HW.A02	66.95326	49.41682	0.00000	0.06627	-0.083333	-21.434E-9	-0.0022055	44.107E-9
25	17HW.A02	66.93777	48.96832	0.00000	0.06631	-0.083333	-21.360E-9	-0.0022011	44.019E-9
25	17HW.A02	66.92228	48.51981	0.00000	0.06635	-0.083333	-21.257E-9	-0.0021949	43.895E-9
25	17HW.A02	66.90679	48.07131	0.00000	0.06639	-0.083333	-21.124E-9	-0.0021869	43.735E-9
25	17HW.A02	66.89130	47.62280	0.00000	0.06644	-0.083333	-20.962E-9	-0.0021772	43.541E-9
26	17HW.A03	66.89130	47.62280	0.00000	0.06644	-0.083333	-20.962E-9	-0.0021772	43.541E-9
26	17HW.A03	66.43956	47.65757	0.00000	0.06614	-0.083333	-22.843E-9	-0.0022904	45.805E-9
26	17HW.A03	65.98782	47.69234	0.00000	0.06594	-0.083333	-24.411E-9	-0.0024153	48.231E-9
26	17HW.A03	65.53608	47.72711	0.00000	0.06508	-0.083333	-27.254E-9	-0.0025418	50.832E-9
26	17HW.A03	65.08434	47.76188	0.00000	0.06427	-0.083333	-29.845E-9	-0.0026815	53.626E-9
26	17HW.A03	64.63260	47.79665	0.00000	0.06326	-0.083333	-32.739E-9	-0.0028317	56.629E-9
26	17HW.A03	64.18086	47.83142	0.00000	0.06201	-0.083333	-35.979E-9	-0.0029934	59.864E-9
26	17HW.A03	63.72912	47.86619	0.00000	0.06057	-0.083333	-39.635E-9	-0.0031798	63.351E-9
26	17HW.A03	63.27738	47.90096	0.00000	0.05871	-0.083333	-43.706E-9	-0.0033561	67.118E-9
26	17HW.A03	62.82564	47.						



**A-SQUARED STUDIO  
ENGINEERS LTD**

**18A Froggnal Gardens  
Building GMA  
PDisp A01 - Demolition**

Job No.	Sheet No.	Rev.
<b>1125</b>		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
28	17HW_B01	59.00046	56.87712	0.00000	0.03925	-0.083333	-105.21E-9	-0.0056228	112.44E-9
28	17HW_B01	59.04640	56.41710	0.00000	0.03801	-0.083333	-107.67E-9	-0.0056974	113.93E-9
29	17HW_B02	59.04640	56.41710	0.00000	0.03801	-0.083333	-107.67E-9	-0.0056974	113.93E-9
29	17HW_B02	59.47996	56.37762	0.00000	0.04190	-0.083333	-96.762E-9	-0.0053524	107.04E-9
29	17HW_B02	59.91352	56.33815	0.00000	0.04537	-0.083333	-87.136E-9	-0.0050340	100.67E-9
29	17HW_B02	60.34709	56.29868	0.00000	0.04846	-0.083333	-78.624E-9	-0.0047400	94.790E-9
29	17HW_B02	60.78065	56.25920	0.00000	0.05120	-0.083333	-71.080E-9	-0.0044679	89.349E-9
29	17HW_B02	61.21421	56.21972	0.00000	0.05363	-0.083333	-64.380E-9	-0.0042159	84.310E-9
29	17HW_B02	61.64777	56.18025	0.00000	0.05576	-0.083333	-58.417E-9	-0.0039822	79.636E-9
29	17HW_B02	62.08134	56.14078	0.00000	0.05762	-0.083333	-53.099E-9	-0.0037651	75.296E-9
29	17HW_B02	62.51490	56.10130	0.00000	0.05924	-0.083333	-48.347E-9	-0.0035633	71.260E-9
30	17HW_B03	62.51490	56.10130	0.00000	0.05924	-0.083333	-48.347E-9	-0.0035633	71.260E-9
30	17HW_B03	62.53797	56.55704	0.00000	0.05976	-0.083333	-47.000E-9	-0.0035053	70.100E-9
30	17HW_B03	62.56105	57.01278	0.00000	0.06027	-0.083333	-45.613E-9	-0.0034449	68.892E-9
30	17HW_B03	62.58413	57.46851	0.00000	0.06077	-0.083333	-44.196E-9	-0.0033822	67.640E-9
30	17HW_B03	62.60720	57.92425	0.00000	0.06125	-0.083333	-42.756E-9	-0.0033177	66.350E-9
30	17HW_B03	62.63027	58.37999	0.00000	0.06170	-0.083333	-41.302E-9	-0.0032517	65.028E-9
30	17HW_B03	62.65335	58.83573	0.00000	0.06213	-0.083333	-39.842E-9	-0.0031842	63.680E-9
30	17HW_B03	62.67643	59.29146	0.00000	0.06253	-0.083333	-38.381E-9	-0.0031158	62.311E-9
30	17HW_B03	62.69950	59.74720	0.00000	0.06290	-0.083333	-36.928E-9	-0.0030465	60.925E-9
31	17HW_B04	62.69950	59.74720	0.00000	0.06290	-0.083333	-36.928E-9	-0.0030465	60.925E-9
31	17HW_B04	62.29744	59.78221	0.00000	0.06215	-0.083333	-39.889E-9	-0.0031884	63.762E-9
31	17HW_B04	61.89538	59.81722	0.00000	0.06128	-0.083333	-43.129E-9	-0.0033387	66.768E-9
31	17HW_B04	61.49332	59.85223	0.00000	0.06026	-0.083333	-46.677E-9	-0.0034980	69.955E-9
31	17HW_B04	61.09126	59.88724	0.00000	0.05911	-0.083333	-50.567E-9	-0.0036670	73.334E-9
31	17HW_B04	60.68920	59.92225	0.00000	0.05779	-0.083333	-54.834E-9	-0.0038463	76.920E-9
31	17HW_B04	60.28714	59.95726	0.00000	0.05631	-0.083333	-59.521E-9	-0.0040367	80.728E-9
31	17HW_B04	59.88508	59.99227	0.00000	0.05466	-0.083333	-64.673E-9	-0.0042390	84.772E-9
31	17HW_B04	59.48302	60.02728	0.00000	0.05281	-0.083333	-70.342E-9	-0.0044539	89.070E-9
31	17HW_B04	59.08096	60.06229	0.00000	0.05076	-0.083333	-76.586E-9	-0.0046825	93.640E-9
31	17HW_B04	58.67890	60.09730	0.00000	0.04849	-0.083333	-83.468E-9	-0.0049256	98.502E-9

**Results : Consolidation : Displacement Data : Lines**

None

**Results : Total : Displacement Data : Lines**

None



# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
Building GMA  
PDisp A02 - Demolition and Excavation

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

### Titles

Job No.: 1125  
 Job Title: 18A Froggnal Gardens  
 Sub-title: Building GMA  
 Calculation Heading: PDisp A02 - Demolition and Excavation  
 Initials: SB  
 Checker:  
 Date Saved:  
 Date Checked:  
 Notes:  
 File Name: PDisp A02 new.pdd  
 File Path: \\Mac\Dropbox for Business\A2-projects\1125 - 18a Froggnal Gardens\03 - Calculations\Issue 01\Pdisp

### History

Date	Time	By	Notes
14-Oct-2020	14:19	hamed	<history cleared>
14-Oct-2020	14:19	hamed	<history cleared>

### Analysis Options

#### General

Global Poisson's ratio: 0.50  
 Maximum allowable ratio between values of E: 1.5  
 Horizontal rigid boundary level: -34.00 [m OD]  
 Displacements at load centroids: Yes  
 GSA piled raft data: No

#### Elastic

Elastic: Yes  
 Analysis: Boussinesq  
 Stiffness for horizontal displacement calculations: Weighted average  
 Using legacy heave correction factor: No

#### Consolidation

Consolidation: No

#### Soil Profiles Soil Profile 1

Layer ref.	Name	Level at top [mOD]	Number of intermediate displacement levels	Youngs Modulus : Top [kN/m <sup>2</sup> ]	Youngs Modulus : Btm. [kN/m <sup>2</sup> ]	Poissons ratio	Non-linear curve
1	Made Ground	0.0	5	10000.	10000.	0.20000	None
2	Bagshot Formation	-1.0000	5	18000.	18000.	0.20000	None
3	London Clay	-7.0000	5	14400.	99450.	0.50000	None

#### Soil Zones

Zone	Name	X min [m]	X max [m]	Y min [m]	Y max [m]	Profile
1	1	0.0	80.000	0.0	100.00	Soil Profile 1

#### Polygonal Load Data

Load ref.	Name	Position : Level [m]	Position : Polygon : Coords. [m]	Position : Polygon Rectangles : Rect. tolerance [%]	No. of Rectangles	Value : Normal (local z) [kN/m <sup>2</sup> ]
1	Demo - 3F	-2.75000	(34.7,49.1) (43.8,49.1) (43.8,46.4) (42.8,46.4) (42.8,42.3) (34.9,42.3) (34.7,42.3) (34.7,49.1)		10.000	2 -45.000
2	Demo - 2F	0.00000	(34.7,53.3) (43.8,53.3) (43.7,49.1) (34.7,49.1) (34.7,53.3)		10.000	1 -30.000
3	Excav - Pool	-6.27500	(34.6,58.5) (44.7,58.5) (44.9,53.8) (34.7,53.8) (34.6,58.5)		10.000	1 -126.00
4	Excav A	-4.21000	(44.9,53.8) (45,49.1) (34.7,49.1) (34.7,53.8) (44.9,53.8)		10.000	5 -84.200
5	Excav B	-4.21000	(45,49.1) (45.3,42.1) (34.7,42.2) (34.7,49.1) (45,49.1)		10.000	2 -20.200

#### Polygonal Loads' Rectangles

No.	Centre : x [m]	Centre : y [m]	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
<b>Load 1 : Demo - 3F</b> (Edge 7 optimal)					
1	38.75214	44.36162	90.266	4.0939	8.0366
2	39.27445	47.75430	90.266	2.6865	9.0839
<b>Load 2 : Demo - 2F</b> (Edge 4 optimal)					
1	39.23550	51.18897	179.84	8.9951	4.1869
<b>Load 3 : Excav - Pool</b> (Edge 3 optimal)					
1	39.70473	56.14037	-89.757	4.6515	10.116
<b>Load 4 : Excav A</b> (Edge 1 optimal)					
1	34.69186	52.61612	0.11868	0.065647	2.3542
2	39.79234	51.44430	0.11868	10.130	4.6978
3	44.88383	51.05898	0.11868	0.050930	3.9061
4	44.93638	50.27787	0.11868	0.050930	2.3437
5	44.98893	49.49676	0.11868	0.050930	0.78122
<b>Load 5 : Excav B</b> (Edge 2 optimal)					
1	39.93896	45.64899	-89.978	6.8759	10.411
2	42.64040	42.16538	-89.978	0.093440	5.2693

#### Displacement Lines

Name	X1 [m]	Y1 [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]	Intervals [No.]	Calculate	Detailed Results
18B.01	27.06970	56.10310	0.00000	32.02050	56.10310	0.00000	10	Yes	Yes
18B.02	32.02050	56.10310	0.00000	32.02020	53.28900	0.00000	6	Yes	Yes
18B.03	32.02020	53.28900	0.00000	34.29880	53.28910	0.00000	6	Yes	Yes



# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
Building GMA  
PDisp A02 - Demolition and Excavation

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by	Date	Checked
SB		

Name	X1	Y1	Z1	X2	Y2	Z2	Intervals	Calculate	Detailed Results
	[m]	[m]	[m]	[m]	[m]	[m]	[No.]		
18B.04	34.29880	53.28910	0.00000	34.29900	42.12610	0.00000	24	Yes	Yes
18B.05	34.29900	42.12610	0.00000	27.03130	42.06780	0.00000	16	Yes	Yes
18B.06	27.03130	42.06780	0.00000	27.03130	42.81150	0.00000	2	Yes	Yes
18B.07	27.03130	42.81150	0.00000	27.06970	56.10310	0.00000	28	Yes	Yes
20FG.01	21.02660	64.09150	0.00000	24.26740	63.42960	0.00000	8	Yes	Yes
20FG.02	24.26740	63.42960	0.00000	23.31400	55.50790	0.00000	16	Yes	Yes
20FG.03	23.31400	55.50790	0.00000	24.37380	55.60010	0.00000	4	Yes	Yes
20FG.04	24.37380	55.60010	0.00000	23.83670	53.15770	0.00000	6	Yes	Yes
20FG.05	23.83670	53.15770	0.00000	24.42370	53.20880	0.00000	2	Yes	Yes
20FG.06	24.42370	53.20880	0.00000	23.90190	50.14280	0.00000	8	Yes	Yes
20FG.07	23.90190	50.14280	0.00000	24.42370	50.18820	0.00000	2	Yes	Yes
20FG.08	24.42370	50.18820	0.00000	24.30050	42.16640	0.00000	18	Yes	Yes
20FG.09	24.30050	42.16640	0.00000	20.99250	42.79780	0.00000	8	Yes	Yes
20FG.10	20.99250	42.79780	0.00000	21.33710	43.74710	0.00000	4	Yes	Yes
20FG.11	21.33710	43.74710	0.00000	12.81700	45.36940	0.00000	18	Yes	Yes
20FG.12	12.81700	45.36940	0.00000	14.97910	55.63720	0.00000	22	Yes	Yes
20FG.13	14.97910	55.63720	0.00000	13.19400	56.13840	0.00000	4	Yes	Yes
20FG.14	13.19400	56.13840	0.00000	13.67460	58.54420	0.00000	6	Yes	Yes
20FG.15	13.67460	58.54420	0.00000	19.98620	57.39750	0.00000	14	Yes	Yes
20FG.16	19.98620	57.39750	0.00000	21.02660	64.09150	0.00000	14	Yes	Yes
17HW.A01	58.70070	56.44780	0.00000	67.17010	55.69590	0.00000	18	Yes	Yes
17HW.A02	67.17010	55.69590	0.00000	66.89130	47.62280	0.00000	18	Yes	Yes
17HW.A03	66.89130	47.62280	0.00000	57.85650	48.31820	0.00000	20	Yes	Yes
17HW.A04	57.85650	48.31820	0.00000	58.70070	56.44780	0.00000	18	Yes	Yes
17HW.B01	58.67890	60.09730	0.00000	59.04640	56.41710	0.00000	8	Yes	Yes
17HW.B02	59.04640	56.41710	0.00000	62.69950	59.74720	0.00000	8	Yes	Yes
17HW.B03	62.69950	59.74720	0.00000	62.69950	59.74720	0.00000	8	Yes	Yes
17HW.B04	62.69950	59.74720	0.00000	58.67890	60.09730	0.00000	10	Yes	Yes

## Results : Immediate : Load Centres : Polygonal

Ref.	Name	x	y	z	δz	Stress Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
1	Demo - 3F	38.97665	45.80077	-2.75000	-22.92773	-3.2813	-46.738	-124.19	-0.0017360
2	Demo - 2F	39.23031	51.19083	0.00000	-35.98943	-0.083333	-29.999	-87.486	-0.0018502
3	Excav - Pool	39.70523	56.13408	-6.27500	-29.74068	-6.6375	-136.81	-375.72	-0.0049463
4	Excav A	39.81036	51.44102	-4.21000	-20.09516	-4.6750	-99.376	-250.24	-0.0038446
5	Excav B	39.95369	45.61566	-4.21000	-19.61963	-4.6750	-63.716	-141.38	-0.0026768

## Results : Consolidation : Load Centres : Polygonal

None

## Results : Total : Load Centres : Polygonal

None

## Results : Immediate : Displacement Data : Lines

Ref.	Name	x	y	z	δz	Stress Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
1	18B.01	27.06970	56.10310	0.00000	-0.57436	-0.083333	-1.3325E-6	-0.024271	485.26E-9
1	18B.01	27.56478	56.10310	0.00000	-0.70943	-0.083333	-1.6448E-6	-0.027342	546.65E-9
1	18B.01	28.05986	56.10310	0.00000	-0.86597	-0.083333	-2.0472E-6	-0.030933	618.42E-9
1	18B.01	28.55494	56.10310	0.00000	-1.04804	-0.083333	-2.5706E-6	-0.035151	702.72E-9
1	18B.01	29.05002	56.10310	0.00000	-1.26079	-0.083333	-3.2579E-6	-0.040129	802.19E-9
1	18B.01	29.54510	56.10310	0.00000	-1.51087	-0.083333	-4.1693E-6	-0.046031	920.13E-9
1	18B.01	30.04018	56.10310	0.00000	-1.80715	-0.083333	-5.3903E-6	-0.053060	1.0605E-6
1	18B.01	30.53526	56.10310	0.00000	-2.16199	-0.083333	-7.0417E-6	-0.061460	1.2284E-6
1	18B.01	31.03034	56.10310	0.00000	-2.59366	-0.083333	-9.2947E-6	-0.071530	1.4295E-6
1	18B.01	31.52542	56.10310	0.00000	-3.13086	-0.083333	-12.389E-6	-0.083617	1.6708E-6
1	18B.01	32.02050	56.10310	0.00000	-3.82093	-0.083333	-16.652E-6	-0.098104	1.9601E-6
2	18B.02	32.02050	56.10310	0.00000	-3.82093	-0.083333	-16.652E-6	-0.098104	1.9601E-6
2	18B.02	32.02045	55.63408	0.00000	-4.04559	-0.083333	-22.091E-6	-0.11322	2.2617E-6
2	18B.02	32.02040	55.16507	0.00000	-4.25554	-0.083333	-29.412E-6	-0.13079	2.6122E-6
2	18B.02	32.02035	54.69605	0.00000	-4.44996	-0.083333	-39.050E-6	-0.15087	3.0128E-6
2	18B.02	32.02030	54.22703	0.00000	-4.62783	-0.083333	-51.220E-6	-0.17319	3.4576E-6
2	18B.02	32.02025	53.75802	0.00000	-4.78800	-0.083333	-65.601E-6	-0.19691	3.9303E-6
2	18B.02	32.02020	53.28900	0.00000	-4.92899	-0.083333	-81.101E-6	-0.22063	4.4029E-6
3	18B.03	32.02020	53.28900	0.00000	-4.92899	-0.083333	-81.101E-6	-0.22063	4.4029E-6
3	18B.03	32.02015	52.82002	0.00000	-5.75205	-0.083333	-131.63E-6	-0.28045	5.9333E-6
3	18B.03	32.02010	52.35104	0.00000	-6.75313	-0.083333	-230.31E-6	-0.36707	7.3137E-6
3	18B.03	33.15950	53.28905	0.00000	-7.98599	-0.083333	-449.16E-6	-0.50027	9.9516E-6
3	18B.03	33.53927	53.28907	0.00000	-9.52089	-0.083333	-0.0010388	-0.72476	14.371E-6
3	18B.03	33.91903	53.28908	0.00000	-11.44505	-0.083333	-0.0032586	-1.1669	22.948E-6
3	18B.03	34.29889	53.28910	0.00000	-13.91370	-0.083333	-0.020383	-2.3752	45.059E-6
4	18B.04	34.29880	53.28910	0.00000	-13.93770	-0.083333	-0.020383	-2.3752	45.059E-6
4	18B.04	34.29881	52.82397	0.00000	-14.16517	-0.083333	-0.036036	-3.4689	65.054E-6
4	18B.04	34.29882	52.35885	0.00000	-14.30914	-0.083333	-0.039582	-3.9774	74.798E-6
4	18B.04	34.29883	51.89372	0.00000	-14.38870	-0.083333	-0.040638	-4.2068	79.259E-6
4	18B.04	34.29883	51.42860	0.00000	-14.37495	-0.083333	-0.041185	-4.3062	81.182E-6
4	18B.04	34.29884	50.96347	0.00000	-14.28484	-0.083333	-0.041548	-4.3204	81.423E-6
4	18B.04	34.29885	50.49835	0.00000	-14.13006	-0.083333	-0.041722	-4.2486	79.964E-6
4	18B.04	34.29886	50.03323	0.00000	-13.87122	-0.083333	-0.041357	-4.0425	75.888E-6
4	18B.04	34.29887	49.56810	0.00000	-13.49095	-0.083333	-0.038253	-3.5412	66.234E-6
4	18B.04	34.29887	49.10298	0.00000	-12.99391	-0.083333	-0.021310	-2.4054	45.505E-6
4	18B.04	34.29888	48.63785	0.00000	-12.46341	-0.083333	-0.0045358	-1.2696	24.847E-6
4	18B.04	34.29889	48.17272	0.00000	-11.97752	-0.083333	-0.0011775	-0.74456	14.750E-6
4	18B.04	34.29890	47.70760	0.00000	-11.53998	-0.083333	-437.41E-6	-4.49264	9.8002E-6
4	18B.04	34.29891	47.24247	0.00000	-11.14616	-0.083333	-203.20E-6	-0.35175	7.0106E-6
4	18B.04	34.29892	46.77735	0.00000	-10.78680	-0.083333	-108.70E-6	-0.26402	5.2673E-6
4	18B.04	34.29892	46.31222	0.00000	-10.40832	-0.083333	-64.105E-6	-0.20524	4.0970E-6
4	18B.04	34.29893	45.84710	0.00000	-10.04319	-0.083333	-40.472E-6	-0.16374	3.2699E-6
4	18B.04	34.29894	45.38197	0.00000	-9.65818	-0.083333	-26.907E-6	-0.13328	2.6624E-6
4	18B.04	34.29895	44.91685	0.00000	-9.24295	-0.083333	-18.621E-6	-0.11025	2.2027E-6
4	18B.04	34.29896	44.45172	0.00000	-8.78501	-0.083333	-13.306E-6	-0.092403	1.8465E-6
4	18B.04	34.29897	43.98660	0.00000	-8.26902	-0.083333	-9.7596E-6	-0.078309	1.5650E-6
4	18B.04	34.29897	43.52148	0.00000	-7.76752	-0.083333	-7.3164E-6	-0.066996	1.3390E-6
4	18B.04	34.29898	43.05635	0.00000	-6.97944	-0.083333	-5.5870E-6	-0.057790	1.1551E-6
4	18B.04	34.29899	42.59123	0.00000	-6.14948	-0.083333	-4.3345E-6	-0.050211	1.0037E-6
4	18B.04	34.29900	42.12610	0.00000	-5.21278	-0.083333	-3.4095E-6	-0.043908	877.75E-9
5	18B.05	34.29900	42.12610	0.00000	-5.21278	-0.083333	-3.4095E-6	-0.043908	877.75E-9
5	18B.05	33.84477	42.12246	0.00000	-4.32171	-0.083333	-3.1128E-6	-0.041492	829.46E-9
5	18B.05	33.39054	42.11881	0.00000	-3.63222	-0.083333	-2.8225E-6	-0.039068	781.02E-9
5	18B.05	32.93631	42.11517	0.00000	-3.07368	-0.083333	-2.5433E-6	-0.036667	733.02E-9
5	18B.05	32.48208	42.11153	0.00000	-2.61820	-0.083333	-2.2790E-6	-0.034316	686.04E-9
5	18B.05	32.02784	42.10788	0.00000	-2.22231	-0.083333	-2.0324E-6	-0.032037	640.50E-9
5	18B.05	31.57361	42.10424	0.00000	-1.89274	-0.083333	-1.8050E-6	-0.029850	596.78E-9
5	18B.05	31.11938	42.10059	0.00000	-1.61182	-0.083333	-1.5976E-6	-0.027766	555.12E-9
5	18B.05	30.66515	42.09695	0.00000	-1.37095	-0.083333	-1.4103E-6	-0.025794	515.71E-9
5	18B.05	30.21092	42.09331	0.00000	-1.16517	-0.083			



A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens Building GMA PDisp A02 - Demolition and Excavation

Job No. Sheet No. Rev. 1125 Drg. Ref. Made by Date Checked SB

Main data table with columns: Ref., Name, x, y, z, dz, Stress Calc. Level, Stress Vertical, Stress Sum Princ., Vert. Strain. Contains 100 rows of numerical data.





# A-SQUARED STUDIO ENGINEERS LTD

**18A Frognal Gardens**  
Building GMA  
PDisp A02 - Demolition and Excavation

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m²]	[kN/m²]	[µ]
18 20FG.11	15.65703	44.82263	0.00000	0.27021	-0.083333	-41.907E-9	-0.0032782	65.538E-9	
18 20FG.11	15.18369	44.91876	0.00000	0.27210	-0.083333	-38.190E-9	-0.0031036	62.067E-9	
18 20FG.11	14.71036	45.00889	0.00000	0.27333	-0.083333	-34.850E-9	-0.0029406	58.807E-9	
18 20FG.11	14.23702	45.09902	0.00000	0.27397	-0.083333	-31.845E-9	-0.0027883	55.761E-9	
18 20FG.11	13.76368	45.18914	0.00000	0.27408	-0.083333	-29.137E-9	-0.0026458	52.913E-9	
18 20FG.11	13.29034	45.27927	0.00000	0.27489	-0.083333	-26.694E-9	-0.0025125	50.247E-9	
18 20FG.11	12.81700	45.36940	0.00000	0.27292	-0.083333	-24.486E-9	-0.0023877	47.751E-9	
19 20FG.12	12.81700	45.36940	0.00000	0.27292	-0.083333	-24.486E-9	-0.0023877	47.751E-9	
19 20FG.12	12.91528	45.83612	0.00000	0.27358	-0.083333	-25.447E-9	-0.0024422	48.840E-9	
19 20FG.12	13.01355	46.30284	0.00000	0.27416	-0.083333	-26.415E-9	-0.0024962	49.922E-9	
19 20FG.12	13.11183	46.76955	0.00000	0.27468	-0.083333	-27.387E-9	-0.0025497	50.990E-9	
19 20FG.12	13.21011	47.23627	0.00000	0.27513	-0.083333	-28.359E-9	-0.0026023	52.043E-9	
19 20FG.12	13.30839	47.70299	0.00000	0.27551	-0.083333	-29.326E-9	-0.0026540	53.077E-9	
19 20FG.12	13.40666	48.16971	0.00000	0.27584	-0.083333	-30.284E-9	-0.0027045	54.086E-9	
19 20FG.12	13.50494	48.63643	0.00000	0.27612	-0.083333	-31.227E-9	-0.0027536	55.068E-9	
19 20FG.12	13.60322	49.10315	0.00000	0.27634	-0.083333	-32.151E-9	-0.0028011	56.018E-9	
19 20FG.12	13.70150	49.56986	0.00000	0.27652	-0.083333	-33.050E-9	-0.0028468	56.931E-9	
19 20FG.12	13.79977	50.03658	0.00000	0.27667	-0.083333	-33.919E-9	-0.0028904	57.804E-9	
19 20FG.12	13.89805	50.50330	0.00000	0.27678	-0.083333	-34.751E-9	-0.0029318	58.633E-9	
19 20FG.12	13.99633	50.97002	0.00000	0.27686	-0.083333	-35.541E-9	-0.0029708	59.412E-9	
19 20FG.12	14.09460	51.43674	0.00000	0.27691	-0.083333	-36.283E-9	-0.0030072	60.139E-9	
19 20FG.12	14.19288	51.90345	0.00000	0.27695	-0.083333	-36.972E-9	-0.0030407	60.809E-9	
19 20FG.12	14.29116	52.37017	0.00000	0.27697	-0.083333	-37.603E-9	-0.0030711	61.418E-9	
19 20FG.12	14.38944	52.83689	0.00000	0.27699	-0.083333	-38.170E-9	-0.0030984	61.964E-9	
19 20FG.12	14.48771	53.30361	0.00000	0.27700	-0.083333	-38.669E-9	-0.0031224	62.444E-9	
19 20FG.12	14.58599	53.77033	0.00000	0.27701	-0.083333	-39.096E-9	-0.0031432	62.852E-9	
19 20FG.12	14.68427	54.23705	0.00000	0.27703	-0.083333	-39.447E-9	-0.0031597	63.189E-9	
19 20FG.12	14.78255	54.70376	0.00000	0.27706	-0.083333	-39.719E-9	-0.0031728	63.452E-9	
19 20FG.12	14.88082	55.17048	0.00000	0.27709	-0.083333	-39.911E-9	-0.0031822	63.640E-9	
19 20FG.12	14.97910	55.63720	0.00000	0.27714	-0.083333	-40.019E-9	-0.0031878	63.750E-9	
20 20FG.13	15.07738	56.10392	0.00000	0.27749	-0.083333	-40.019E-9	-0.0031878	63.750E-9	
20 20FG.13	14.53283	55.76250	0.00000	0.27828	-0.083333	-36.264E-9	-0.0030083	60.162E-9	
20 20FG.13	14.08655	55.88780	0.00000	0.27877	-0.083333	-32.927E-9	-0.0028422	56.840E-9	
20 20FG.13	13.64028	56.01310	0.00000	0.27871	-0.083333	-29.953E-9	-0.0026881	53.759E-9	
20 20FG.13	13.19400	56.13840	0.00000	0.27815	-0.083333	-27.299E-9	-0.0025451	50.899E-9	
21 20FG.14	13.69172	56.26370	0.00000	0.27891	-0.083333	-27.299E-9	-0.0025451	50.899E-9	
21 20FG.14	13.27410	56.53937	0.00000	0.27824	-0.083333	-27.282E-9	-0.0025445	50.886E-9	
21 20FG.14	13.35420	56.94033	0.00000	0.27833	-0.083333	-27.229E-9	-0.0025419	50.834E-9	
21 20FG.14	13.43430	57.34130	0.00000	0.27839	-0.083333	-27.141E-9	-0.0025374	50.744E-9	
21 20FG.14	13.51440	57.74227	0.00000	0.27844	-0.083333	-27.018E-9	-0.0025309	50.615E-9	
21 20FG.14	13.59450	58.14324	0.00000	0.27849	-0.083333	-26.860E-9	-0.0025226	50.449E-9	
21 20FG.14	13.67460	58.54420	0.00000	0.27850	-0.083333	-26.670E-9	-0.0025124	50.245E-9	
22 20FG.15	13.67460	58.54420	0.00000	0.27850	-0.083333	-26.670E-9	-0.0025124	50.245E-9	
22 20FG.15	14.12543	58.46229	0.00000	0.27912	-0.083333	-29.207E-9	-0.0026508	53.012E-9	
22 20FG.15	14.57626	58.38039	0.00000	0.27927	-0.083333	-32.040E-9	-0.0027995	55.986E-9	
22 20FG.15	15.02709	58.29848	0.00000	0.27961	-0.083333	-35.213E-9	-0.0029567	59.189E-9	
22 20FG.15	15.47791	58.21657	0.00000	0.27885	-0.083333	-38.771E-9	-0.0031323	62.641E-9	
22 20FG.15	15.92874	58.13466	0.00000	0.27614	-0.083333	-42.773E-9	-0.0033187	66.368E-9	
22 20FG.15	16.37957	58.05276	0.00000	0.27366	-0.083333	-47.285E-9	-0.0035202	70.399E-9	
22 20FG.15	16.83040	57.97085	0.00000	0.27032	-0.083333	-52.383E-9	-0.0037386	74.765E-9	
22 20FG.15	17.28123	57.88894	0.00000	0.26704	-0.083333	-57.459E-9	-0.0039565	79.502E-9	
22 20FG.15	17.73206	57.80704	0.00000	0.26601	-0.083333	-64.725E-9	-0.0042329	84.650E-9	
22 20FG.15	18.18289	57.72513	0.00000	0.25400	-0.083333	-72.206E-9	-0.0045132	90.256E-9	
22 20FG.15	18.63371	57.64322	0.00000	0.24602	-0.083333	-80.757E-9	-0.0048190	96.370E-9	
22 20FG.15	19.08454	57.56131	0.00000	0.23653	-0.083333	-90.562E-9	-0.0051532	103.055E-9	
22 20FG.15	19.53537	57.47940	0.00000	0.22911	-0.083333	-101.741E-9	-0.0055171	110.677E-9	
22 20FG.15	19.98620	57.39750	0.00000	0.21221	-0.083333	-114.862E-9	-0.0059211	118.414E-9	
23 20FG.16	19.98620	57.39750	0.00000	0.21221	-0.083333	-114.862E-9	-0.0059211	118.414E-9	
23 20FG.16	20.06051	57.87564	0.00000	0.21421	-0.083333	-112.022E-9	-0.0058377	116.746E-9	
23 20FG.16	20.13483	58.35379	0.00000	0.21646	-0.083333	-108.922E-9	-0.0057456	114.902E-9	
23 20FG.16	20.20914	58.83193	0.00000	0.21916	-0.083333	-105.611E-9	-0.0056455	112.964E-9	
23 20FG.16	20.28346	59.31007	0.00000	0.22162	-0.083333	-102.111E-9	-0.0055384	110.762E-9	
23 20FG.16	20.35777	59.78821	0.00000	0.22448	-0.083333	-98.471E-9	-0.0054250	108.492E-9	
23 20FG.16	20.43209	60.26636	0.00000	0.22749	-0.083333	-94.727E-9	-0.0053061	106.116E-9	
23 20FG.16	20.50640	60.74450	0.00000	0.23062	-0.083333	-90.912E-9	-0.0051828	103.642E-9	
23 20FG.16	20.58072	61.22264	0.00000	0.23394	-0.083333	-87.058E-9	-0.0050557	101.110E-9	
23 20FG.16	20.65503	61.70079	0.00000	0.23713	-0.083333	-83.194E-9	-0.0049257	98.503E-9	
23 20FG.16	20.72934	62.17893	0.00000	0.24045	-0.083333	-79.348E-9	-0.0047934	95.859E-9	
23 20FG.16	20.80366	62.65707	0.00000	0.24378	-0.083333	-75.544E-9	-0.0046597	93.186E-9	
23 20FG.16	20.87797	63.13521	0.00000	0.24708	-0.083333	-71.802E-9	-0.0045252	90.496E-9	
23 20FG.16	20.95229	63.61336	0.00000	0.25048	-0.083333	-68.141E-9	-0.0043905	87.802E-9	
23 20FG.16	21.02660	64.09150	0.00000	0.25349	-0.083333	-64.576E-9	-0.0042561	85.115E-9	
24 17HW.A01	58.70070	56.44780	0.00000	0.18788	-0.083333	-117.444E-9	-0.0059937	119.862E-9	
24 17HW.A01	59.17122	56.40603	0.00000	0.20433	-0.083333	-104.399E-9	-0.0055951	111.899E-9	
24 17HW.A01	59.64174	56.36426	0.00000	0.21856	-0.083333	-93.021E-9	-0.0052303	104.602E-9	
24 17HW.A01	60.11226	56.32249	0.00000	0.23019	-0.083333	-83.092E-9	-0.0048190	97.909E-9	
24 17HW.A01	60.58279	56.28071	0.00000	0.24122	-0.083333	-74.395E-9	-0.0045889	91.769E-9	
24 17HW.A01	61.05331	56.23894	0.00000	0.25006	-0.083333	-66.758E-9	-0.0043065	86.123E-9	
24 17HW.A01	61.52383	56.19717	0.00000	0.25747	-0.083333	-60.034E-9	-0.0040465	80.923E-9	
24 17HW.A01	61.99436	56.15539	0.00000	0.26358	-0.083333	-54.100E-9	-0.0038066	76.126E-9	
24 17HW.A01	62.46488	56.11362	0.00000	0.26895	-0.083333	-48.850E-9	-0.0035869	71.665E-9	
24 17HW.A01	62.93540	56.07185	0.00000	0.27248	-0.083333	-44.196E-9	-0.0033801	67.597E-9	
24 17HW.A01	63.40592	56.03008	0.00000	0.27548	-0.083333	-40.060E-9	-0.0031903	63.800E-9	
24 17HW.A01	63.87644	55.98831	0.00000	0.27766	-0.083333	-36.377E-9	-0.0030142	60.279E-9	
24 17HW.A01	64.34697	55.94653	0.00000	0.27909	-0.083333	-33.090E-9	-0.0028507	57.009E-9	
24 17HW.A01	64.81749	55.90476	0.00000	0.27984	-0.083333	-29.471E-9	-0.0026969	54.962E-9	
24 17HW.A01	65.28801	55.86299	0.00000	0.28004	-0.083333	-27.519E-9	-0.0025571	51.139E-9	
24 17HW.A01	65.75853	55.82122	0.00000	0.27969	-0.083333	-25.156E-9	-0.0024252	48.500E-9	
24 17HW.A01	66.22906	55.77944	0.00000	0.27888	-0.083333	-23.031E-9	-0.0023021	46.039E-9	
24 17HW.A01	66.69958	55.73767	0.00000	0.27764	-0.083333	-21.117E-9	-0.0021871	43.739E-9	
24 17HW.A01	67.17010	55.69590	0.00000	0.27600	-0.083333	-19.389E-9	-0.0020796	41.589E-9	
25 17HW.A02	67.15461	55.24739	0.00000	0.27628	-0.083333	-19.702E-9	-0.0020991	41.980E-9	
25 17HW.A02	67.13912	54.79889	0.00000	0.27647	-0.083333	-19.994E-9	-0.0021173	42.343E-9	
25 17HW.A02	67.12363	54.35038	0.00000	0.27663	-0.083333	-20.264E-9	-0.0021340	42.677E-9	
25 17HW.A02	67.10814	53.90188	0.00000	0.27682	-0.083333	-20.519E-9	-0.0021491	42.980E-9	
25 17HW.A02	67.09266	53.45337	0.00000						



# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
Building GMA  
PDisp A02 - Demolition and Excavation

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc.	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
26	17HW.A03	57.85650	48.31820	0.00000	0.12825	-0.083333	-172.49E-9	-0.0074839	149.66E-9
27	17HW.A04	57.85650	48.31820	0.00000	0.12825	-0.083333	-172.49E-9	-0.0074839	149.66E-9
27	17HW.A04	57.90340	48.76984	0.00000	0.12793	-0.083333	-173.64E-9	-0.0075114	150.21E-9
27	17HW.A04	57.95030	49.22149	0.00000	0.12810	-0.083333	-174.20E-9	-0.0075239	150.46E-9
27	17HW.A04	57.99720	49.67313	0.00000	0.12878	-0.083333	-174.14E-9	-0.0075213	150.41E-9
27	17HW.A04	58.04410	50.12478	0.00000	0.12995	-0.083333	-173.47E-9	-0.0075037	150.05E-9
27	17HW.A04	58.09100	50.57642	0.00000	0.13162	-0.083333	-172.19E-9	-0.0074711	149.40E-9
27	17HW.A04	58.13790	51.02807	0.00000	0.13377	-0.083333	-170.33E-9	-0.0074240	148.46E-9
27	17HW.A04	58.18480	51.47971	0.00000	0.13639	-0.083333	-167.92E-9	-0.0073628	147.24E-9
27	17HW.A04	58.23170	51.93136	0.00000	0.13945	-0.083333	-164.98E-9	-0.0072880	145.74E-9
27	17HW.A04	58.27860	52.38300	0.00000	0.14294	-0.083333	-161.55E-9	-0.0072005	143.99E-9
27	17HW.A04	58.32550	52.83464	0.00000	0.14682	-0.083333	-157.70E-9	-0.0071010	142.00E-9
27	17HW.A04	58.37240	53.28629	0.00000	0.15106	-0.083333	-153.46E-9	-0.0069905	139.79E-9
27	17HW.A04	58.41930	53.73793	0.00000	0.15563	-0.083333	-148.88E-9	-0.0068700	137.38E-9
27	17HW.A04	58.46620	54.18958	0.00000	0.16050	-0.083333	-144.03E-9	-0.0067404	134.79E-9
27	17HW.A04	58.51310	54.64122	0.00000	0.16562	-0.083333	-138.95E-9	-0.0066028	132.04E-9
27	17HW.A04	58.56000	55.09287	0.00000	0.17096	-0.083333	-133.71E-9	-0.0064583	129.15E-9
27	17HW.A04	58.60690	55.54451	0.00000	0.17648	-0.083333	-128.34E-9	-0.0063079	126.14E-9
27	17HW.A04	58.65380	55.99616	0.00000	0.18213	-0.083333	-122.90E-9	-0.0061527	123.04E-9
27	17HW.A04	58.70070	56.44780	0.00000	0.18788	-0.083333	-117.44E-9	-0.0059937	119.86E-9
28	17HW.B01	58.67890	60.09730	0.00000	0.22359	-0.083333	-83.46E-9	-0.0049256	98.502E-9
28	17HW.B01	58.72484	59.67327	0.00000	0.22007	-0.083333	-86.851E-9	-0.0050392	100.77E-9
28	17HW.B01	58.77078	59.17725	0.00000	0.21667	-0.083333	-90.188E-9	-0.0051493	102.98E-9
28	17HW.B01	58.81671	58.71722	0.00000	0.21341	-0.083333	-93.452E-9	-0.0052552	105.09E-9
28	17HW.B01	58.86265	58.25720	0.00000	0.21032	-0.083333	-96.615E-9	-0.0053562	107.11E-9
28	17HW.B01	58.90859	57.79717	0.00000	0.20743	-0.083333	-99.648E-9	-0.0054516	109.02E-9
28	17HW.B01	58.95452	57.33715	0.00000	0.20476	-0.083333	-102.52E-9	-0.0055407	110.80E-9
28	17HW.B01	59.00046	56.87712	0.00000	0.20235	-0.083333	-105.21E-9	-0.0056228	112.44E-9
28	17HW.B01	59.04640	56.41710	0.00000	0.20020	-0.083333	-107.67E-9	-0.0056974	113.93E-9
29	17HW.B02	59.04640	56.41710	0.00000	0.20020	-0.083333	-107.67E-9	-0.0056974	113.93E-9
29	17HW.B02	59.47996	56.37762	0.00000	0.21390	-0.083333	-96.76E-9	-0.0053524	107.04E-9
29	17HW.B02	59.91352	56.33815	0.00000	0.22584	-0.083333	-87.13E-9	-0.0050340	100.67E-9
29	17HW.B02	60.34709	56.29868	0.00000	0.23619	-0.083333	-78.624E-9	-0.0047400	94.790E-9
29	17HW.B02	60.78065	56.25920	0.00000	0.24511	-0.083333	-71.080E-9	-0.0044679	89.349E-9
29	17HW.B02	61.21421	56.21972	0.00000	0.25273	-0.083333	-64.380E-9	-0.0042159	84.310E-9
29	17HW.B02	61.64777	56.18025	0.00000	0.25918	-0.083333	-58.417E-9	-0.0039822	79.636E-9
29	17HW.B02	62.08134	56.14078	0.00000	0.26457	-0.083333	-53.099E-9	-0.0037651	75.296E-9
29	17HW.B02	62.51490	56.10130	0.00000	0.26900	-0.083333	-48.347E-9	-0.0035633	71.260E-9
30	17HW.B03	62.51490	56.10130	0.00000	0.26900	-0.083333	-48.347E-9	-0.0035633	71.260E-9
30	17HW.B03	62.53797	56.55704	0.00000	0.27005	-0.083333	-47.000E-9	-0.0035053	70.100E-9
30	17HW.B03	62.56105	57.01278	0.00000	0.27110	-0.083333	-45.613E-9	-0.0034449	68.892E-9
30	17HW.B03	62.58413	57.46851	0.00000	0.27214	-0.083333	-44.196E-9	-0.0033822	67.640E-9
30	17HW.B03	62.60720	57.92425	0.00000	0.27315	-0.083333	-42.756E-9	-0.0033177	66.350E-9
30	17HW.B03	62.63027	58.37999	0.00000	0.27414	-0.083333	-41.302E-9	-0.0032517	65.028E-9
30	17HW.B03	62.65335	58.83573	0.00000	0.27508	-0.083333	-39.842E-9	-0.0031842	63.680E-9
30	17HW.B03	62.67643	59.29146	0.00000	0.27597	-0.083333	-38.381E-9	-0.0031159	62.311E-9
30	17HW.B03	62.69950	59.74720	0.00000	0.27679	-0.083333	-36.928E-9	-0.0030465	60.925E-9
31	17HW.B04	62.69950	59.74720	0.00000	0.27679	-0.083333	-36.928E-9	-0.0030465	60.925E-9
31	17HW.B04	62.29744	59.78221	0.00000	0.27473	-0.083333	-39.889E-9	-0.0031884	63.762E-9
31	17HW.B04	61.89538	59.81722	0.00000	0.27209	-0.083333	-43.129E-9	-0.0033387	66.768E-9
31	17HW.B04	61.49332	59.85223	0.00000	0.26884	-0.083333	-46.677E-9	-0.0034980	69.955E-9
31	17HW.B04	61.09126	59.88724	0.00000	0.26492	-0.083333	-50.567E-9	-0.0036670	73.334E-9
31	17HW.B04	60.68920	59.92225	0.00000	0.26026	-0.083333	-54.834E-9	-0.0038463	76.920E-9
31	17HW.B04	60.28714	59.95726	0.00000	0.25481	-0.083333	-59.521E-9	-0.0040367	80.728E-9
31	17HW.B04	59.88508	59.99227	0.00000	0.24849	-0.083333	-64.673E-9	-0.0042390	84.772E-9
31	17HW.B04	59.48302	60.02728	0.00000	0.24124	-0.083333	-70.342E-9	-0.0044539	89.070E-9
31	17HW.B04	59.08096	60.06229	0.00000	0.23297	-0.083333	-76.586E-9	-0.0046825	93.640E-9
31	17HW.B04	58.67890	60.09730	0.00000	0.22359	-0.083333	-83.468E-9	-0.0049256	98.502E-9

Results : Consolidation : Displacement Data : Lines

None

Results : Total : Displacement Data : Lines

None



# A-SQUARED STUDIO ENGINEERS LTD

18A Frognal Gardens  
Building GMA  
PDisp A03 - Long Term

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

### Titles

Job No.: 1125  
 Job Title: 18A Frognal Gardens  
 Sub-title: Building GMA  
 Calculation Heading: PDisp A03 - Long Term  
 Initials: SB  
 Checker:  
 Date Saved:  
 Date Checked:  
 Notes:  
 File Name: PDisp A03 new.pdd  
 File Path: \\Mac\Dropbox for Business\A2-projects\1125 - 18a Frognal Gardens\03 - Calculations\Issue 01\Pdisp

### History

Date	Time	By	Notes
14-Oct-2020	14:22	hamed	<history cleared>
14-Oct-2020	14:22	hamed	

### Analysis Options

#### General

Global Poisson's ratio: 0.20  
 Maximum allowable ratio between values of E: 1.5  
 Horizontal rigid boundary level: -34.00 [m OD]  
 Displacements at load centroids: Yes  
 GSA piled raft data: No

#### Elastic

Elastic: Yes  
 Analysis: Boussinesq  
 Stiffness for horizontal displacement calculations: Weighted average  
 Using legacy heave correction factor: No

#### Consolidation

Consolidation: No

#### Soil Profiles Soil Profile 1

Layer ref.	Name	Level at top [mOD]	Number of intermediate displacement levels	Youngs Modulus : Top [kN/m <sup>2</sup> ]	Youngs Modulus : Btm. [kN/m <sup>2</sup> ]	Poissons ratio	Non-linear curve
1	Made Ground	0.0	5	10000.	10000.	0.20000	None
2	Bagshot Formation	-1.0000	5	18000.	18000.	0.20000	None
3	London Clay	-7.0000	5	11520.	79560.	0.20000	None

#### Non-linear Curve Coordinates - Non-linear Curve 1

Point Strain Factor [%]

#### Soil Zones

Zone	Name	X min [m]	X max [m]	Y min [m]	Y max [m]	Profile
1	1	0.0	80.000	0.0	100.00	Soil Profile 1

#### Polygonal Load Data

Load ref.	Name	Position : Level [m]	Position : Polygon : Coords. : Rect. : Rect. tolerance [m]	No. of Polygon Rectangles	Value : Normal (local z) [kN/m <sup>2</sup> ]
1	Demo - 3F	-2.75000	(34.7,49.1) (43.9,49.1) (43.8,46.4) (42.8,46.4) (42.8,42.3) (34.9,42.3) (34.7,42.3) (34.7,49.1)	2	-45.000
2	Demo - 2F	0.00000	(34.7,53.3) (43.8,53.3) (43.7,49.1) (34.7,49.1) (34.7,53.3)	1	-30.000
3	Excav - Pool	-6.27500	(34.6,58.5) (44.7,58.5) (44.9,53.8) (34.7,53.8) (34.6,58.5)	1	-126.00
4	Excav A	-4.21000	(44.9,53.8) (45.49,1) (34.7,49.1) (34.7,53.8) (44.9,53.8)	5	-84.200
5	Excav B	-4.21000	(45.49,1) (45.3,42.1) (34.7,42.2) (34.7,49.1) (45.49,1)	2	-20.200
6	Loading - 4F	-4.21000	(35.1,43.3) (35.1,53) (38.6,53) (39.9,54.3) (40.4,58.3) (44.6,58.3) (45.2,42.4) (41.6,42.4) (40.4,43.3) (35.1,43.3)	4	40.000
7	Loading - 3F	-4.21000	(41.6,42.4) (40.5,42.4) (39.4,41.5) (35.1,41.5) (35.1,43.3) (40.4,43.3) (40.4,58.3) (35.1,53) (38.6,53) (39.9,54.3) (40.4,58.3)	2	30.000
8	Loading - 2FA	-4.21000	(40.4,58.3) (35.1,58.3) (35.1,53) (38.6,53) (39.9,54.3) (40.4,58.3)	2	20.000
9	Loading - 2FB	-4.21000	(39.4,41.5) (40.5,42.4) (45.2,42.4) (45.4,36) (41.9,36) (41.3,40.4) (40.4,1.5) (39.4,41.5)	8	20.000

#### Polygonal Loads' Rectangles

No.	Centre x	Centre y	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
Load 1 : Demo - 3F (Edge 7 optimal)					
1	38.15214	44.36162	90.266	4.0939	8.0366
2	39.27445	47.75430	90.266	2.6865	9.0839
Load 2 : Demo - 2F (Edge 4 optimal)					
1	39.23550	51.18897	179.84	8.9951	4.1869
Load 3 : Excav - Pool (Edge 3 optimal)					
1	39.70473	56.14037	-89.757	4.6515	10.116
Load 4 : Excav A (Edge 1 optimal)					



# A-SQUARED STUDIO ENGINEERS LTD

18A Frogнал Gardens  
Building GMA  
PDisp A03 - Long Term

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

No.	Centre x	Centre y	Angle of local x from global x	Width	Depth
1	34.69186	52.61612	0.11868	0.065647	2.3542
2	39.79234	51.44430	0.11868	10.130	4.6978
3	44.88383	51.05898	0.11868	0.050930	3.9061
4	44.93638	50.27787	0.11868	0.050930	2.3437
5	44.98893	49.49676	0.11868	0.050930	0.78122
<b>Load 5 : Excav B</b> (Edge 2 optimal)					
1	39.93896	45.64899	-89.978	6.8759	10.411
2	42.64040	42.16538	-89.978	0.093440	5.2693
<b>Load 6 : Loading - 4F</b> (Edge 4 optimal)					
1	43.07710	42.87167	-89.900	0.89811	4.1902
2	42.41853	56.32179	-89.900	3.9427	4.5336
3	42.00406	53.68886	-89.900	1.3217	5.5531
4	40.03279	48.17461	-89.900	9.6999	9.8946
<b>Load 7 : Loading - 3F</b> (Edge 1 optimal)					
1	38.04638	42.86936	-90.305	0.86120	5.9090
2	37.54178	41.98003	-90.305	0.91179	4.9093
<b>Load 8 : Loading - 2FA</b> (Edge 2 optimal)					
1	37.61788	56.31890	-90.138	3.9338	5.0665
2	37.15328	53.68971	-90.138	1.3268	4.1500
<b>Load 9 : Loading - 2FB</b> (Edge 6 optimal)					
1	44.98559	35.96963	92.070	0.062969	0.87111
2	44.11278	36.00110	92.070	0.062969	2.6133
3	43.48428	38.25599	92.070	4.4893	3.7066
4	42.95451	41.05182	92.070	1.1370	4.5635
5	42.54506	41.97525	92.070	0.69779	5.3152
6	42.39331	42.34682	92.070	0.055844	4.0465
7	41.65598	42.37605	92.070	0.055844	2.4279
8	40.91866	42.40528	92.070	0.055844	0.80931

### Displacement Lines

Name	X1	Y1	Z1	X2	Y2	Z2	Intervals	Calculate	Detailed Results
[m]	[m]	[m]	[m]	[m]	[m]	[m]	[No.]		
18B.01	27.06970	56.10310	0.00000	32.02050	56.10310	0.00000	10	Yes	Yes
18B.02	32.02050	56.10310	0.00000	32.02020	53.28900	0.00000	6	Yes	Yes
18B.03	32.02020	53.28900	0.00000	34.29880	53.28910	0.00000	6	Yes	Yes
18B.04	34.29880	53.28910	0.00000	34.29900	42.12610	0.00000	24	Yes	Yes
18B.05	34.29900	42.12610	0.00000	27.03130	42.06780	0.00000	16	Yes	Yes
18B.06	27.03130	42.06780	0.00000	27.03130	42.81150	0.00000	2	Yes	Yes
18B.07	27.03130	42.81150	0.00000	27.06970	56.10310	0.00000	28	Yes	Yes
20FG.01	21.02660	64.09150	0.00000	24.26740	63.42960	0.00000	8	Yes	Yes
20FG.02	24.26740	63.42960	0.00000	23.31400	55.50790	0.00000	16	Yes	Yes
20FG.03	23.31400	55.50790	0.00000	24.37380	55.60010	0.00000	4	Yes	Yes
20FG.04	24.37380	55.60010	0.00000	23.83670	53.15770	0.00000	6	Yes	Yes
20FG.05	23.83670	53.15770	0.00000	24.42370	53.20880	0.00000	2	Yes	Yes
20FG.06	24.42370	53.20880	0.00000	23.90190	50.14280	0.00000	8	Yes	Yes
20FG.07	23.90190	50.14280	0.00000	24.42370	50.18820	0.00000	2	Yes	Yes
20FG.08	24.42370	50.18820	0.00000	24.30050	42.16640	0.00000	18	Yes	Yes
20FG.09	24.30050	42.16640	0.00000	20.99250	42.79780	0.00000	8	Yes	Yes
20FG.10	20.99250	42.79780	0.00000	21.33710	43.74710	0.00000	4	Yes	Yes
20FG.11	21.33710	43.74710	0.00000	12.81700	45.36940	0.00000	18	Yes	Yes
20FG.12	12.81700	45.36940	0.00000	14.97910	55.63720	0.00000	22	Yes	Yes
20FG.13	14.97910	55.63720	0.00000	13.19400	56.13840	0.00000	4	Yes	Yes
20FG.14	13.19400	56.13840	0.00000	13.67460	58.54420	0.00000	6	Yes	Yes
20FG.15	13.67460	58.54420	0.00000	19.98620	57.39750	0.00000	14	Yes	Yes
20FG.16	19.98620	57.39750	0.00000	21.02660	64.09150	0.00000	14	Yes	Yes
17HW.A01	58.70070	56.44780	0.00000	67.17010	55.69590	0.00000	18	Yes	Yes
17HW.A02	67.17010	55.69590	0.00000	66.89130	47.62280	0.00000	18	Yes	Yes
17HW.A03	66.89130	47.62280	0.00000	57.85650	48.31820	0.00000	20	Yes	Yes
17HW.A04	57.85650	48.31820	0.00000	58.70070	56.44780	0.00000	18	Yes	Yes
17HW.B01	58.67890	60.09730	0.00000	59.04640	56.41710	0.00000	8	Yes	Yes
17HW.B02	59.04640	56.41710	0.00000	62.51490	56.10310	0.00000	8	Yes	Yes
17HW.B03	62.51490	56.10310	0.00000	62.69950	59.74720	0.00000	8	Yes	Yes
17HW.B04	62.69950	59.74720	0.00000	58.67890	60.09730	0.00000	10	Yes	Yes

### Results : Immediate : Load Centres : Polygonal

Ref.	Name	x	y	z	dz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
[m]	[m]	[m]	[m]	[m]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[μ]
1	Demo - 3F	38.97665	45.80077	-2.75000	-13.76653	-3.2813	-46.738	-99.349	-0.0020120
2	Demo - 2F	39.23031	51.19083	0.00000	-31.47103	-0.083333	-29.999	-69.988	-0.0022001
3	Excav - Pool	39.71053	56.13408	-6.27500	-36.80563	-6.6375	-112.22	-260.28	-0.0045890
4	Excav A	39.81036	51.44102	-4.21000	-25.36943	-4.6750	-59.424	-112.18	-0.002152
5	Excav B	39.95369	45.61566	-4.21000	-10.37274	-4.6750	-23.753	-25.123	-0.0013044
6	Loading - 4F	40.57994	49.47071	-4.21000	-20.96106	-4.6750	-62.498	-99.732	-0.0030584
7	Loading - 3F	37.82069	42.45519	-4.21000	-5.46702	-4.6750	-10.557	-9.5224	-0.0018016
8	Loading - 2FA	37.52464	55.78655	-4.21000	-36.55990	-4.6750	16.027	28.807	748.36E-6
9	Loading - 2FB	43.22027	39.42394	-4.21000	2.65534	-4.6750	19.007	34.124	887.97E-6

### Results : Consolidation : Load Centres : Polygonal

None

### Results : Total : Load Centres : Polygonal

None

### Results : Immediate : Displacement Data : Lines

Ref.	Name	x	y	z	dz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
[m]	[m]	[m]	[m]	[m]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[μ]
1	18B.01	27.06970	56.10310	0.00000	-2.01261	-0.083333	-1.3325E-6	-0.019417	388.17E-9
1	18B.01	27.56478	56.10310	0.00000	-2.23258	-0.083333	-1.6448E-6	-0.021874	437.28E-9
1	18B.01	28.05986	56.10310	0.00000	-2.48256	-0.083333	-2.0472E-6	-0.024747	494.69E-9
1	18B.01	28.55494	56.10310	0.00000	-2.76807	-0.083333	-2.5706E-6	-0.028121	562.11E-9
1	18B.01	29.05002	56.10310	0.00000	-3.09612	-0.083333	-3.2579E-6	-0.032103	641.68E-9
1	18B.01	29.54510	56.10310	0.00000	-3.47973	-0.083333	-4.1693E-6	-0.036825	736.00E-9
1	18B.01	30.04018	56.10310	0.00000	-3.91894	-0.083333	-5.3903E-6	-0.042448	848.31E-9
1	18B.01	30.53526	56.10310	0.00000	-4.44243	-0.083333	-7.0417E-6	-0.049168	982.52E-9
1	18B.01	31.03034	56.10310	0.00000	-5.07040	-0.083333	-9.2947E-6	-0.057224	1.1434E-6
1	18B.01	31.52542	56.10310	0.00000	-5.83984	-0.083333	-12.389E-6	-0.066893	1.3364E-6
1	18B.01	32.02050	56.10310	0.00000	-6.80951	-0.083333	-16.652E-6	-0.078483	1.5677E-6
2	18B.02	32.02050	56.10310	0.00000	-6.80951	-0.083333	-16.652E-6	-0.078483	1.5677E-6
2	18B.02	32.02045	55.63408	0.00000	-7.02412	-0.083333	-22.091E-6	-0.090572	1.8088E-6
2	18B.02	32.02040	55.16507	0.00000	-7.19710	-0.083333	-29.412E-6	-0.10463	2.0891E-6
2	18B.02	32.02035	54.69605	0.00000	-7.32890	-0.083333	-39.050E-6	-0.12070	2.4093E-6
2	18B.02	32.02030	54.22703	0.00000	-7.42112	-0.083333	-51.220E-6	-0.13855	2.7648E-6
2	18B.02	32.02025	53.75802	0.00000	-7.47661	-0.083333	-65.601E-6	-0.15753	3.1427E-6
2	18B.02	32.02020	53.28900	0.00000	-7.49795	-0.083333	-81.101E-6	-0.17651	3.5204E-6
3	18B.03	32.02020	53.28900	0.00000	-7.49795	-0.083333	-81.101E-6	-0.17651	3.5204E-6



A-SQUARED STUDIO ENGINEERS LTD

Job No. Sheet No. Rev.

1125

Drg. Ref.

Made by Date Checked

18A Frogna Gardens Building GMA PDisp A03 - Long Term

Table with 10 columns: Ref., Name, x, y, z, Δz, Stress Calc., Stress Vertical, Stress Sum Princ., Vert. Strain. Contains a large list of numerical data points for structural analysis.



**A-SQUARED STUDIO**  
**ENGINEERS LTD**

**18A Frogнал Gardens**  
**Building GMA**  
**PDISP A03 - Long Term**

Job No.	Sheet No.	Rev.
<b>1125</b>		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc.	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
	[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]	
14	20FG.07	23.90190	50.14280	0.00000	-1.12488	-0.083333	-552.20E-9	-0.011698	233.89E-9
14	20FG.07	24.16280	50.16550	0.00000	-1.18279	-0.083333	-610.73E-9	-0.012391	247.74E-9
14	20FG.07	24.42370	50.18820	0.00000	-1.24411	-0.083333	-677.02E-9	-0.013141	262.74E-9
15	20FG.08	24.41686	49.74254	0.00000	-1.22766	-0.083333	-664.08E-9	-0.013000	259.92E-9
15	20FG.08	24.41001	49.29689	0.00000	-1.18279	-0.083333	-610.73E-9	-0.012391	256.30E-9
15	20FG.08	24.40317	48.85123	0.00000	-1.18827	-0.083333	-628.07E-9	-0.012601	251.94E-9
15	20FG.08	24.39632	48.40558	0.00000	-1.16561	-0.083333	-605.83E-9	-0.012349	246.91E-9
15	20FG.08	24.38948	47.95992	0.00000	-1.14120	-0.083333	-581.40E-9	-0.012068	241.29E-9
15	20FG.08	24.38263	47.51427	0.00000	-1.11519	-0.083333	-555.26E-9	-0.011761	235.16E-9
15	20FG.08	24.37579	47.06861	0.00000	-1.08776	-0.083333	-527.90E-9	-0.011433	228.60E-9
15	20FG.08	24.36210	46.17730	0.00000	-1.02927	-0.083333	-471.31E-9	-0.010728	214.51E-9
15	20FG.08	24.35526	45.73164	0.00000	-0.99856	-0.083333	-442.89E-9	-0.010360	207.14E-9
15	20FG.08	24.34841	45.28599	0.00000	-0.96708	-0.083333	-414.83E-9	-0.0099851	199.65E-9
15	20FG.08	24.34157	44.84033	0.00000	-0.93500	-0.083333	-387.43E-9	-0.0096077	192.11E-9
15	20FG.08	24.33472	44.39468	0.00000	-0.90248	-0.083333	-360.89E-9	-0.0092306	184.57E-9
15	20FG.08	24.32788	43.94902	0.00000	-0.86967	-0.083333	-335.40E-9	-0.0088561	177.08E-9
15	20FG.08	24.32103	43.50337	0.00000	-0.83671	-0.083333	-311.09E-9	-0.0084866	169.69E-9
15	20FG.08	24.31419	43.05771	0.00000	-0.80374	-0.083333	-288.04E-9	-0.0081238	162.44E-9
15	20FG.08	24.30734	42.61206	0.00000	-0.77089	-0.083333	-266.29E-9	-0.0077694	155.36E-9
15	20FG.08	24.30050	42.16640	0.00000	-0.73828	-0.083333	-245.88E-9	-0.0074244	148.46E-9
16	20FG.09	24.30050	42.16640	0.00000	-0.73828	-0.083333	-245.88E-9	-0.0074244	148.46E-9
16	20FG.09	23.89700	42.24533	0.00000	-0.69595	-0.083333	-223.80E-9	-0.0070254	140.48E-9
16	20FG.09	23.47350	42.32425	0.00000	-0.65594	-0.083333	-203.74E-9	-0.0066488	132.95E-9
16	20FG.09	23.05000	42.40317	0.00000	-0.61638	-0.083333	-185.59E-9	-0.0062819	125.80E-9
16	20FG.09	22.64650	42.48210	0.00000	-0.58239	-0.083333	-169.06E-9	-0.0059591	119.16E-9
16	20FG.09	22.23300	42.56103	0.00000	-0.54862	-0.083333	-154.11E-9	-0.0056440	112.86E-9
16	20FG.09	21.81950	42.63995	0.00000	-0.51671	-0.083333	-140.57E-9	-0.0053474	106.93E-9
16	20FG.09	21.40600	42.71888	0.00000	-0.48658	-0.083333	-128.30E-9	-0.0050683	101.35E-9
16	20FG.09	20.99250	42.79780	0.00000	-0.45811	-0.083333	-117.19E-9	-0.0048057	96.100E-9
17	20FG.10	21.07865	43.03513	0.00000	-0.47297	-0.083333	-123.13E-9	-0.0049453	98.891E-9
17	20FG.10	21.16480	43.27245	0.00000	-0.48820	-0.083333	-129.39E-9	-0.0050891	101.77E-9
17	20FG.10	21.25095	43.50978	0.00000	-0.50379	-0.083333	-135.97E-9	-0.0052373	104.73E-9
17	20FG.10	21.33710	43.74710	0.00000	-0.51976	-0.083333	-142.90E-9	-0.0053899	107.78E-9
18	20FG.11	21.33710	43.74710	0.00000	-0.51976	-0.083333	-142.90E-9	-0.0053899	107.78E-9
18	20FG.11	20.86376	43.83723	0.00000	-0.48393	-0.083333	-127.99E-9	-0.0050530	101.05E-9
18	20FG.11	20.39042	43.92736	0.00000	-0.45050	-0.083333	-114.79E-9	-0.0047410	94.806E-9
18	20FG.11	19.91708	44.01748	0.00000	-0.41931	-0.083333	-103.11E-9	-0.0044518	89.023E-9
18	20FG.11	19.44374	44.10761	0.00000	-0.39025	-0.083333	-92.748E-9	-0.0041937	83.663E-9
18	20FG.11	18.97041	44.19774	0.00000	-0.36304	-0.083333	-83.552E-9	-0.0039350	78.630E-9
18	20FG.11	18.49707	44.28787	0.00000	-0.33769	-0.083333	-75.379E-9	-0.0037042	74.075E-9
18	20FG.11	18.02373	44.37799	0.00000	-0.31403	-0.083333	-68.106E-9	-0.0034898	69.789E-9
18	20FG.11	17.55039	44.46812	0.00000	-0.29195	-0.083333	-61.625E-9	-0.0032906	65.805E-9
18	20FG.11	17.07705	44.55825	0.00000	-0.27134	-0.083333	-55.841E-9	-0.0031102	62.105E-9
18	20FG.11	16.60371	44.64838	0.00000	-0.25211	-0.083333	-50.674E-9	-0.0029329	58.652E-9
18	20FG.11	16.13037	44.73851	0.00000	-0.23416	-0.083333	-46.050E-9	-0.0027723	55.440E-9
18	20FG.11	15.65703	44.82863	0.00000	-0.21740	-0.083333	-41.907E-9	-0.0026225	52.446E-9
18	20FG.11	15.18369	44.91876	0.00000	-0.20175	-0.083333	-38.190E-9	-0.0024829	49.653E-9
18	20FG.11	14.71035	45.00889	0.00000	-0.18735	-0.083333	-34.850E-9	-0.0023519	47.045E-9
18	20FG.11	14.23702	45.09902	0.00000	-0.17352	-0.083333	-31.845E-9	-0.0022306	44.608E-9
18	20FG.11	13.76368	45.18914	0.00000	-0.16080	-0.083333	-29.137E-9	-0.0021167	42.330E-9
18	20FG.11	13.29034	45.27927	0.00000	-0.14892	-0.083333	-26.694E-9	-0.0020100	40.197E-9
18	20FG.11	12.81700	45.36940	0.00000	-0.13784	-0.083333	-24.486E-9	-0.0019101	38.200E-9
19	20FG.12	12.71700	45.36940	0.00000	-0.13784	-0.083333	-24.486E-9	-0.0019101	38.200E-9
19	20FG.12	12.91528	45.83612	0.00000	-0.14295	-0.083333	-25.447E-9	-0.0019537	39.072E-9
19	20FG.12	13.01355	46.30284	0.00000	-0.14806	-0.083333	-26.415E-9	-0.0019970	39.937E-9
19	20FG.12	13.11183	46.76955	0.00000	-0.15317	-0.083333	-27.387E-9	-0.0020397	40.792E-9
19	20FG.12	13.21011	47.23627	0.00000	-0.15825	-0.083333	-28.359E-9	-0.0020819	41.634E-9
19	20FG.12	13.30839	47.70299	0.00000	-0.16329	-0.083333	-29.326E-9	-0.0021232	42.461E-9
19	20FG.12	13.40666	48.16971	0.00000	-0.16828	-0.083333	-30.284E-9	-0.0021636	43.268E-9
19	20FG.12	13.50494	48.63643	0.00000	-0.17319	-0.083333	-31.227E-9	-0.0022029	44.054E-9
19	20FG.12	13.60322	49.10315	0.00000	-0.17801	-0.083333	-32.151E-9	-0.0022409	44.813E-9
19	20FG.12	13.70150	49.56986	0.00000	-0.18273	-0.083333	-33.050E-9	-0.0022774	45.544E-9
19	20FG.12	13.79977	50.03658	0.00000	-0.18731	-0.083333	-33.919E-9	-0.0023123	46.243E-9
19	20FG.12	13.89805	50.50330	0.00000	-0.19176	-0.083333	-34.751E-9	-0.0023455	46.905E-9
19	20FG.12	13.99633	50.97002	0.00000	-0.19604	-0.083333	-35.541E-9	-0.0023767	47.529E-9
19	20FG.12	14.09460	51.43674	0.00000	-0.20014	-0.083333	-36.283E-9	-0.0024057	48.110E-9
19	20FG.12	14.19288	51.90345	0.00000	-0.20404	-0.083333	-36.972E-9	-0.0024325	48.646E-9
19	20FG.12	14.29115	52.37017	0.00000	-0.20784	-0.083333	-37.603E-9	-0.0024569	49.134E-9
19	20FG.12	14.38942	52.83689	0.00000	-0.21118	-0.083333	-38.170E-9	-0.0024787	49.570E-9
19	20FG.12	14.48771	53.30361	0.00000	-0.21438	-0.083333	-38.669E-9	-0.0024979	49.953E-9
19	20FG.12	14.58599	53.77033	0.00000	-0.21731	-0.083333	-39.096E-9	-0.0025143	50.281E-9
19	20FG.12	14.68427	54.23705	0.00000	-0.22097	-0.083333	-39.447E-9	-0.0025278	50.550E-9
19	20FG.12	14.78255	54.70276	0.00000	-0.22349	-0.083333	-39.719E-9	-0.0025389	50.761E-9
19	20FG.12	14.88082	55.17048	0.00000	-0.22437	-0.083333	-39.911E-9	-0.0025458	50.911E-9
19	20FG.12	14.97910	55.63720	0.00000	-0.22609	-0.083333	-40.019E-9	-0.0025502	50.999E-9
20	20FG.13	14.97910	55.63720	0.00000	-0.22609	-0.083333	-40.019E-9	-0.0025502	50.999E-9
20	20FG.13	14.53283	55.76250	0.00000	-0.20868	-0.083333	-36.264E-9	-0.0024067	48.129E-9
20	20FG.13	14.08656	55.88780	0.00000	-0.19256	-0.083333	-32.927E-9	-0.0022737	45.134E-9
20	20FG.13	13.64028	56.01310	0.00000	-0.17765	-0.083333	-29.953E-9	-0.0021505	43.007E-9
20	20FG.13	13.19400	56.13840	0.00000	-0.16383	-0.083333	-27.299E-9	-0.0020361	40.719E-9
21	20FG.14	13.19400	56.13840	0.00000	-0.16383	-0.083333	-27.299E-9	-0.0020361	40.719E-9
21	20FG.14	13.74110	56.53937	0.00000	-0.16447	-0.083333	-27.282E-9	-0.0020356	40.708E-9
21	20FG.14	14.28821	56.94033	0.00000	-0.16511	-0.083333	-27.222E-9	-0.0020325	40.667E-9
21	20FG.14	14.83430	57.34130	0.00000	-0.16522	-0.083333	-27.141E-9	-0.0020299	40.594E-9
21	20FG.14	15.38039	57.74227	0.00000	-0.16534	-0.083333	-27.018E-9	-0.0020247	40.492E-9
21	20FG.14	15.92648	58.14323	0.00000	-0.16527	-0.083333	-26.860E-9	-0.0020181	40.358E-9
21	20FG.14	16.47257	58.54420	0.00000	-0.16503	-0.083333	-26.670E-9	-0.0020099	40.196E-9
22	20FG.15	16.47257	58.54420	0.00000	-0.16503	-0.083333	-26.670E-9	-0.0020099	40.196E-9
22	20FG.15	14.12543	58.46229	0.00000	-0.17894	-0.083333	-29.207E-9	-0.0021206	42.409E-9
22	20FG.15	14.57626	58.38039	0.00000	-0.19396	-0.083333	-32.040E-9	-0.0022396	44.788E-9
22	20FG.15	15.02709	58.29848	0.00000	-0.21019	-0.083333	-35.212E-9	-0.0023677	47.350E-9
22	20FG.15	15.47791	58.21657	0.00000	-0.22774	-0.083333	-38.771E-9	-0.0025058	50.111E-9
22	20FG.15								



**A-SQUARED STUDIO  
ENGINEERS LTD**

**18A Froggnal Gardens  
Building GMA  
PDisp A03 - Long Term**

Job No.	Sheet No.	Rev.
<b>1125</b>		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc. Level [MPa]	Stress: Vertical [kN/m²]	Stress: Sum Princ. [kN/m²]	Vert. Strain [μ]
24	17HW.A01	63.40592	56.03008	0.00000	-0.22264	-0.083333	-60.060E-9	-0.0025522	51.039E-9
24	17HW.A01	63.87644	55.98831	0.00000	-0.20506	-0.083333	-36.377E-9	-0.0024113	48.223E-9
24	17HW.A01	64.34697	55.94653	0.00000	-0.18882	-0.083333	-33.090E-9	-0.0022805	45.607E-9
24	17HW.A01	64.81749	55.90476	0.00000	-0.17382	-0.083333	-30.151E-9	-0.0021589	43.174E-9
24	17HW.A01	65.28801	55.86299	0.00000	-0.15995	-0.083333	-27.519E-9	-0.0020457	40.910E-9
24	17HW.A01	65.75853	55.82122	0.00000	-0.14732	-0.083333	-25.155E-9	-0.0019401	38.800E-9
24	17HW.A01	66.22906	55.77944	0.00000	-0.13527	-0.083333	-23.031E-9	-0.0018417	36.831E-9
24	17HW.A01	66.69958	55.73767	0.00000	-0.12430	-0.083333	-21.117E-9	-0.0017497	34.991E-9
24	17HW.A01	67.17010	55.69590	0.00000	-0.11414	-0.083333	-19.389E-9	-0.0016637	33.271E-9
25	17HW.A02	67.17010	55.69590	0.00000	-0.11414	-0.083333	-19.389E-9	-0.0016637	33.271E-9
25	17HW.A02	67.17010	55.69590	0.00000	-0.11414	-0.083333	-19.389E-9	-0.0016637	33.271E-9
25	17HW.A02	67.13912	54.79889	0.00000	-0.11604	-0.083333	-19.994E-9	-0.0016938	33.874E-9
25	17HW.A02	67.12363	54.35038	0.00000	-0.11676	-0.083333	-20.264E-9	-0.0017072	34.141E-9
25	17HW.A02	67.10814	53.90188	0.00000	-0.11733	-0.083333	-20.510E-9	-0.0017193	34.383E-9
25	17HW.A02	67.09266	53.45337	0.00000	-0.11774	-0.083333	-20.731E-9	-0.0017301	34.600E-9
25	17HW.A02	67.07717	53.00487	0.00000	-0.11799	-0.083333	-20.926E-9	-0.0017396	34.790E-9
25	17HW.A02	67.06168	52.55636	0.00000	-0.11807	-0.083333	-21.093E-9	-0.0017477	34.952E-9
25	17HW.A02	67.04619	52.10786	0.00000	-0.11800	-0.083333	-21.232E-9	-0.0017545	35.087E-9
25	17HW.A02	67.03070	51.65935	0.00000	-0.11777	-0.083333	-21.342E-9	-0.0017598	35.193E-9
25	17HW.A02	67.01521	51.21084	0.00000	-0.11737	-0.083333	-21.421E-9	-0.0017637	35.271E-9
25	17HW.A02	66.99972	50.76234	0.00000	-0.11714	-0.083333	-21.477E-9	-0.0017660	35.318E-9
25	17HW.A02	66.98423	50.31383	0.00000	-0.11610	-0.083333	-21.489E-9	-0.0017670	35.337E-9
25	17HW.A02	66.96874	49.86533	0.00000	-0.11523	-0.083333	-21.477E-9	-0.0017664	35.326E-9
25	17HW.A02	66.95326	49.41682	0.00000	-0.11421	-0.083333	-21.434E-9	-0.0017644	35.285E-9
25	17HW.A02	66.93777	48.96832	0.00000	-0.11305	-0.083333	-21.360E-9	-0.0017609	35.215E-9
25	17HW.A02	66.92229	48.51981	0.00000	-0.11174	-0.083333	-21.257E-9	-0.0017559	35.116E-9
25	17HW.A02	66.90679	48.07131	0.00000	-0.11029	-0.083333	-21.124E-9	-0.0017495	34.988E-9
25	17HW.A02	66.89130	47.62280	0.00000	-0.10871	-0.083333	-20.962E-9	-0.0017417	34.832E-9
26	17HW.A03	66.89130	47.62280	0.00000	-0.10871	-0.083333	-20.962E-9	-0.0017417	34.832E-9
26	17HW.A03	66.43956	47.65757	0.00000	-0.11805	-0.083333	-22.843E-9	-0.0018323	36.644E-9
26	17HW.A03	66.42408	47.69229	0.00000	-0.11814	-0.083333	-22.919E-9	-0.0018394	36.798E-9
26	17HW.A03	65.53608	47.72711	0.00000	-0.13894	-0.083333	-27.254E-9	-0.0020334	40.665E-9
26	17HW.A03	65.08434	47.76188	0.00000	-0.15063	-0.083333	-29.845E-9	-0.0021452	42.900E-9
26	17HW.A03	64.63260	47.79665	0.00000	-0.16323	-0.083333	-32.739E-9	-0.0022653	45.303E-9
26	17HW.A03	64.18086	47.83142	0.00000	-0.17683	-0.083333	-35.979E-9	-0.0023947	47.890E-9
26	17HW.A03	63.72912	47.86619	0.00000	-0.19159	-0.083333	-39.615E-9	-0.0025464	50.682E-9
26	17HW.A03	63.27738	47.90096	0.00000	-0.20738	-0.083333	-43.706E-9	-0.0026849	53.693E-9
26	17HW.A03	62.82564	47.93573	0.00000	-0.22451	-0.083333	-48.319E-9	-0.0028479	56.952E-9
26	17HW.A03	62.37390	47.97050	0.00000	-0.24304	-0.083333	-53.534E-9	-0.0030245	60.483E-9
26	17HW.A03	61.92216	48.00527	0.00000	-0.26309	-0.083333	-59.447E-9	-0.0032161	64.315E-9
26	17HW.A03	61.47042	48.04004	0.00000	-0.28479	-0.083333	-66.169E-9	-0.0034244	68.481E-9
26	17HW.A03	61.01868	48.07481	0.00000	-0.30829	-0.083333	-73.835E-9	-0.0036514	73.018E-9
26	17HW.A03	60.56694	48.10958	0.00000	-0.33378	-0.083333	-82.604E-9	-0.0038990	77.971E-9
26	17HW.A03	60.11520	48.14435	0.00000	-0.36142	-0.083333	-92.668E-9	-0.0041699	83.387E-9
26	17HW.A03	59.66346	48.17912	0.00000	-0.39143	-0.083333	-104.266E-9	-0.0044668	89.323E-9
26	17HW.A03	59.21172	48.21389	0.00000	-0.42405	-0.083333	-117.655E-9	-0.0047929	95.844E-9
26	17HW.A03	58.75998	48.24866	0.00000	-0.45952	-0.083333	-133.202E-9	-0.0051520	103.022E-9
26	17HW.A03	58.30824	48.28343	0.00000	-0.49814	-0.083333	-151.30E-9	-0.0055484	110.95E-9
26	17HW.A03	57.85650	48.31820	0.00000	-0.54023	-0.083333	-172.49E-9	-0.0059871	119.72E-9
27	17HW.A04	57.85650	48.31820	0.00000	-0.54023	-0.083333	-172.49E-9	-0.0059871	119.72E-9
27	17HW.A04	57.40476	48.25297	0.00000	-0.58768	-0.083333	-199.65E-9	-0.0065169	130.16E-9
27	17HW.A04	57.95030	49.22149	0.00000	-0.55407	-0.083333	-174.20E-9	-0.0060191	120.36E-9
27	17HW.A04	57.99720	49.67313	0.00000	-0.55935	-0.083333	-174.14E-9	-0.0060171	120.32E-9
27	17HW.A04	58.04410	50.12478	0.00000	-0.56351	-0.083333	-173.47E-9	-0.0060029	120.04E-9
27	17HW.A04	58.09100	50.57642	0.00000	-0.56652	-0.083333	-172.19E-9	-0.0059769	119.52E-9
27	17HW.A04	58.13790	51.02807	0.00000	-0.56937	-0.083333	-170.23E-9	-0.0059292	118.76E-9
27	17HW.A04	58.18480	51.47971	0.00000	-0.56906	-0.083333	-167.92E-9	-0.0058902	117.78E-9
27	17HW.A04	58.23170	51.93136	0.00000	-0.56858	-0.083333	-164.98E-9	-0.0058304	116.59E-9
27	17HW.A04	58.27860	52.38300	0.00000	-0.56695	-0.083333	-161.55E-9	-0.0057604	115.19E-9
27	17HW.A04	58.32550	52.83464	0.00000	-0.56419	-0.083333	-157.70E-9	-0.0056808	113.60E-9
27	17HW.A04	58.37240	53.28629	0.00000	-0.56034	-0.083333	-153.46E-9	-0.0055924	111.83E-9
27	17HW.A04	58.41930	53.73793	0.00000	-0.55542	-0.083333	-148.88E-9	-0.0054960	109.90E-9
27	17HW.A04	58.46620	54.18958	0.00000	-0.54948	-0.083333	-144.03E-9	-0.0053923	107.83E-9
27	17HW.A04	58.51310	54.64122	0.00000	-0.54256	-0.083333	-138.95E-9	-0.0052822	105.63E-9
27	17HW.A04	58.56000	55.09287	0.00000	-0.53472	-0.083333	-133.71E-9	-0.0051666	103.32E-9
27	17HW.A04	58.60690	55.54451	0.00000	-0.52603	-0.083333	-128.34E-9	-0.0050463	100.91E-9
27	17HW.A04	58.65380	55.99616	0.00000	-0.51653	-0.083333	-122.90E-9	-0.0049222	98.428E-9
27	17HW.A04	58.70070	56.44780	0.00000	-0.50630	-0.083333	-117.44E-9	-0.0047949	95.885E-9
28	17HW.B01	58.67890	60.09730	0.00000	-0.43377	-0.083333	-83.468E-9	-0.0039405	78.799E-9
28	17HW.B01	58.72484	59.63727	0.00000	-0.44172	-0.083333	-86.851E-9	-0.0040314	80.617E-9
28	17HW.B01	58.77078	59.17725	0.00000	-0.44902	-0.083333	-90.188E-9	-0.0041195	82.378E-9
28	17HW.B01	58.81671	58.71722	0.00000	-0.45560	-0.083333	-93.452E-9	-0.0042042	84.072E-9
28	17HW.B01	58.86265	58.25720	0.00000	-0.46142	-0.083333	-96.615E-9	-0.0042849	85.687E-9
28	17HW.B01	58.90859	57.79717	0.00000	-0.46645	-0.083333	-99.648E-9	-0.0043613	87.213E-9
28	17HW.B01	58.95452	57.33715	0.00000	-0.47064	-0.083333	-102.52E-9	-0.0044325	88.638E-9
28	17HW.B01	59.00046	56.87712	0.00000	-0.47407	-0.083333	-105.22E-9	-0.0044977	89.952E-9
28	17HW.B01	59.04640	56.41710	0.00000	-0.47640	-0.083333	-107.67E-9	-0.0045579	91.145E-9
29	17HW.B02	59.04640	56.41710	0.00000	-0.47640	-0.083333	-107.67E-9	-0.0045579	91.145E-9
29	17HW.B02	59.47996	56.37762	0.00000	-0.44149	-0.083333	-96.762E-9	-0.0042819	85.626E-9
29	17HW.B02	59.91352	56.33815	0.00000	-0.40923	-0.083333	-87.136E-9	-0.0040272	80.534E-9
29	17HW.B02	60.34709	56.29868	0.00000	-0.37928	-0.083333	-78.624E-9	-0.0037920	75.830E-9
29	17HW.B02	60.78065	56.25920	0.00000	-0.35176	-0.083333	-71.080E-9	-0.0035743	71.478E-9
29	17HW.B02	61.21421	56.21972	0.00000	-0.32617	-0.083333	-64.380E-9	-0.0033727	67.447E-9
29	17HW.B02	61.64777	56.18025	0.00000	-0.30247	-0.083333	-58.417E-9	-0.0031857	63.708E-9
29	17HW.B02	62.08134	56.14078	0.00000	-0.28049	-0.083333	-53.099E-9	-0.0030121	60.235E-9
29	17HW.B02	62.51490	56.10130	0.00000	-0.26019	-0.083333	-48.347E-9	-0.0028506	57.007E-9
30	17HW.B03	62.51490	56.10130	0.00000	-0.26010	-0.083333	-48.347E-9	-0.0028506	57.007E-9
30	17HW.B03	62.53797	56.55704	0.00000	-0.25647	-0.083333	-47.000E-9	-0.0028042	56.079E-9
30	17HW.B03	62.56105	57.01278	0.00000	-0.25251	-0.083333	-45.613E-9	-0.0027559	55.112E-9
30	17HW.B03	62.58413	57.46851	0.00000	-0.24822	-0.083333	-44.196E-9	-0.0027058	54.111E-9
30	17HW.B03	62.60720	57.92425	0.00000	-0.24364	-0.083333	-42.756E-9	-0.0026542	53.079E-9
30	17HW.B03	62.63027	58.37999	0.00000	-0.23879	-0.083333	-41.302E-9	-0.0026013	52.022E-9
30	17HW.B03	62.65335	58.83573	0.00000	-0.23370	-0.083333	-39.842E-9	-0.0025474	5



# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
Building GMA  
PDisp B01 - Underpin Loading

Job No. Sheet No. Rev.

1125

Drg. Ref.

Made by Date Checked  
SB

### Titles

Job No.: 1125  
Job Title: 18A Froggnal Gardens  
Sub-title: Building GMA  
Calculation Heading: PDisp B01 - Underpin Loading  
Initials: SB  
Checker:  
Date Saved:  
Date Checked:  
Notes:  
File Name: PDisp B01 new.pdd  
File Path: \\Mac\Dropbox for Business\A2-projects\1125 - 18a Froggnal Gardens\03 - Calculations\Issue 01\Pdisp

### History

Date	Time	By	Notes
14-Oct-2020	14:23	hamed	<history cleared>
14-Oct-2020	14:23	hamed	

### Analysis Options

#### General

Global Poisson's ratio: 0.20  
Maximum allowable ratio between values of E: 1.5  
Horizontal rigid boundary level: -34.00 [m OD]  
Displacements at load centroids: Yes  
GSA piled raft data: No

#### Elastic

Elastic: Yes  
Analysis: Boussinesq  
Stiffness for horizontal displacement calculations: Weighted average  
Using legacy heave correction factor: No

#### Consolidation

Consolidation: No

### Soil Profiles Soil Profile 1

Layer ref.	Name	Level at top	Number of intermediate displacement levels	Youngs Modulus : Top	Youngs Modulus : Btm.	Poissons ratio	Non-linear curve
	[mOD]			[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]		
1	Made Ground	0.0	5	10000.	10000.	0.20000	None
2	Bagshot Formation	-1.0000	5	18000.	18000.	0.20000	None
3	London Clay	-7.0000	5	11520.	79560.	0.20000	None

### Soil Zones

Zone	Name	X min [m]	X max [m]	Y min [m]	Y max [m]	Profile
1	1	0.0	80.000	0.0	100.00	Soil Profile 1

### Polygonal Load Data

Load ref.	Name	Position : Level	Position : Polygon : Coords. : Rect. tolerance	No. of Polygon Rectangles	Value : Normal (local z)
		[m]	[m]	[#]	[kN/m <sup>2</sup> ]
1	Party wall loading	-4.00000	(34.6,49.3) (35.6,53.8)	10.000	114.00
2	Party wall loading	-6.60000	(34.5,58.5) (35.5,58.5)	10.000	114.00

### Polygonal Loads' Rectangles

No.	Centre x	Centre y	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
Load 1 : Party wall loading (Edge 2 optimal)					
1	35.07988	51.55120	90.365	4.4777	0.99983
Load 2 : Party wall loading (Edge 1 optimal)					
1	35.05053	56.14105	-89.633	4.6894	0.99993

### Displacement Lines

Name	X1 [m]	Y1 [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]	Intervals [No.]	Calculate	Detailed Results
18B.01	27.06970	56.10310	0.00000	32.02050	56.10310	0.00000	10	Yes	Yes
18B.02	32.02050	56.10310	0.00000	32.02020	53.28900	0.00000	6	Yes	Yes
18B.03	32.02020	53.28900	0.00000	34.29880	53.28910	0.00000	6	Yes	Yes
18B.04	34.29880	53.28910	0.00000	34.29900	42.12610	0.00000	24	Yes	Yes
18B.05	34.29900	42.12610	0.00000	27.03130	42.06780	0.00000	16	Yes	Yes
18B.06	27.03130	42.06780	0.00000	27.03130	42.81150	0.00000	2	Yes	Yes
18B.07	27.03130	42.81150	0.00000	27.06970	56.10310	0.00000	28	Yes	Yes
20FG.01	21.02660	64.09150	0.00000	24.26740	63.42960	0.00000	8	Yes	Yes
20FG.02	24.26740	63.42960	0.00000	23.31400	55.50790	0.00000	16	Yes	Yes
20FG.03	23.31400	55.50790	0.00000	24.37380	55.60010	0.00000	4	Yes	Yes
20FG.04	24.37380	55.60010	0.00000	23.83670	53.15770	0.00000	12	Yes	Yes
20FG.05	23.83670	53.15770	0.00000	24.42370	53.20880	0.00000	2	Yes	Yes
20FG.06	24.42370	53.20880	0.00000	23.90190	50.14280	0.00000	8	Yes	Yes
20FG.07	23.90190	50.14280	0.00000	24.42370	50.18820	0.00000	2	Yes	Yes
20FG.08	24.42370	50.18820	0.00000	24.30050	42.16640	0.00000	18	Yes	Yes
20FG.09	24.30050	42.16640	0.00000	20.99250	42.79780	0.00000	8	Yes	Yes
20FG.10	20.99250	42.79780	0.00000	21.33710	43.74710	0.00000	4	Yes	Yes
20FG.11	21.33710	43.74710	0.00000	12.81700	45.36940	0.00000	18	Yes	Yes
20FG.12	12.81700	45.36940	0.00000	14.97910	55.63720	0.00000	22	Yes	Yes
20FG.13	14.97910	55.63720	0.00000	13.19400	56.13840	0.00000	4	Yes	Yes
20FG.14	13.19400	56.13840	0.00000	13.67460	58.54420	0.00000	6	Yes	Yes
20FG.15	13.67460	58.54420	0.00000	19.98620	57.39750	0.00000	14	Yes	Yes
20FG.16	19.98620	57.39750	0.00000	21.02660	64.09150	0.00000	14	Yes	Yes
17HW.A01	58.70070	56.44780	0.00000	67.17010	55.69590	0.00000	18	Yes	Yes
17HW.A02	67.17010	55.69590	0.00000	66.89130	47.62280	0.00000	18	Yes	Yes
17HW.A03	66.89130	47.62280	0.00000	57.85650	48.31820	0.00000	20	Yes	Yes
17HW.A04	57.85650	48.31820	0.00000	58.70070	56.44780	0.00000	18	Yes	Yes
17HW.B01	58.67890	60.09730	0.00000	59.04640	56.41710	0.00000	8	Yes	Yes
17HW.B02	59.04640	56.41710	0.00000	62.51490	56.10130	0.00000	8	Yes	Yes
17HW.B03	62.51490	56.10130	0.00000	62.69950	59.74720	0.00000	8	Yes	Yes
17HW.B04	62.69950	59.74720	0.00000	58.67890	60.09730	0.00000	10	Yes	Yes





# A-SQUARED STUDIO ENGINEERS LTD

18A Frogнал Gardens  
Building GMA  
PDisp B01 - Underpin Loading

Job No. Sheet No. Rev.

1125

Drg. Ref.

Made by  
SB

Date

Checked

Name	X1	Y1	Z1	X2	Y2	Z2	Intervals	Calculate	Detailed Results
[m]	[m]	[m]	[m]	[m]	[m]	[m]	[No.]		

### Results : Immediate : Load Centres : Polygonal

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[m]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[μ]
1	Party wall loading	35.07987	51.55124	-4.00000	12.48152	-4.5000	93.160	132.65	0.0047368
2	Party wall loading	35.05052	56.14109	-6.60000	11.79900	-6.8000	113.46	210.12	0.0052290

### Results : Consolidation : Load Centres : Polygonal

None

### Results : Total : Load Centres : Polygonal

None

### Results : Immediate : Displacement Data : Lines

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[μ]
1	18B.01	27.06970	56.10310	0.00000	0.48430	-0.083333	0.0	0.0	0.0
1	18B.01	27.56478	56.10310	0.00000	0.44687	-0.083333	0.0	0.0	0.0
1	18B.01	28.05986	56.10310	0.00000	0.61993	-0.083333	0.0	0.0	0.0
1	18B.01	28.55494	56.10310	0.00000	0.70584	-0.083333	0.0	0.0	0.0
1	18B.01	29.05002	56.10310	0.00000	0.80761	-0.083333	0.0	0.0	0.0
1	18B.01	29.54510	56.10310	0.00000	0.92928	-0.083333	0.0	0.0	0.0
1	18B.01	30.04018	56.10310	0.00000	1.07641	-0.083333	0.0	0.0	0.0
1	18B.01	30.53526	56.10310	0.00000	1.25704	-0.083333	0.0	0.0	0.0
1	18B.01	31.03034	56.10310	0.00000	1.48372	-0.083333	0.0	0.0	0.0
1	18B.01	31.52542	56.10310	0.00000	1.77755	-0.083333	0.0	0.0	0.0
1	18B.01	32.02050	56.10310	0.00000	2.17648	-0.083333	0.0	0.0	0.0
2	18B.02	32.02050	56.10310	0.00000	2.17648	-0.083333	0.0	0.0	0.0
2	18B.02	32.02045	55.63408	0.00000	2.26561	-0.083333	0.0	0.0	0.0
2	18B.02	32.02040	55.16507	0.00000	2.33773	-0.083333	0.0	0.0	0.0
2	18B.02	32.02035	54.69605	0.00000	2.39262	-0.083333	0.0	0.0	0.0
2	18B.02	32.02030	54.22703	0.00000	2.43005	-0.083333	0.0	0.0	0.0
2	18B.02	32.02025	53.75802	0.00000	2.45006	-0.083333	0.0	0.0	0.0
2	18B.02	32.02020	53.28900	0.00000	2.45281	-0.083333	0.0	0.0	0.0
3	18B.03	32.39997	53.28902	0.00000	2.87167	-0.083333	0.0	0.0	0.0
3	18B.03	32.77973	52.28903	0.00000	3.32873	-0.083333	0.0	0.0	0.0
3	18B.03	33.15950	53.28905	0.00000	4.07511	-0.083333	0.0	0.0	0.0
3	18B.03	33.53927	53.28907	0.00000	4.95852	-0.083333	0.0	0.0	0.0
3	18B.03	33.91903	53.28908	0.00000	6.15399	-0.083333	0.0	0.0	0.0
3	18B.03	34.29880	53.28910	0.00000	8.12328	-0.083333	0.0	0.0	0.0
4	18B.04	34.29880	53.28910	0.00000	8.12328	-0.083333	0.0	0.0	0.0
4	18B.04	34.29881	52.82397	0.00000	7.87956	-0.083333	0.0	0.0	0.0
4	18B.04	34.29882	52.35885	0.00000	7.63511	-0.083333	0.0	0.0	0.0
4	18B.04	34.29883	51.89372	0.00000	7.41723	-0.083333	0.0	0.0	0.0
4	18B.04	34.29883	51.42860	0.00000	7.18473	-0.083333	0.0	0.0	0.0
4	18B.04	34.29884	50.96347	0.00000	6.95167	-0.083333	0.0	0.0	0.0
4	18B.04	34.29885	50.49835	0.00000	6.49058	-0.083333	0.0	0.0	0.0
4	18B.04	34.29886	50.03323	0.00000	5.91579	-0.083333	0.0	0.0	0.0
4	18B.04	34.29887	49.56810	0.00000	5.02588	-0.083333	0.0	0.0	0.0
4	18B.04	34.29888	49.10298	0.00000	3.77189	-0.083333	0.0	0.0	0.0
4	18B.04	34.29888	48.63785	0.00000	2.83464	-0.083333	0.0	0.0	0.0
4	18B.04	34.29889	48.17272	0.00000	2.22781	-0.083333	0.0	0.0	0.0
4	18B.04	34.29890	47.70760	0.00000	1.79530	-0.083333	0.0	0.0	0.0
4	18B.04	34.29891	47.24247	0.00000	1.47254	-0.083333	0.0	0.0	0.0
4	18B.04	34.29892	46.77735	0.00000	1.22426	-0.083333	0.0	0.0	0.0
4	18B.04	34.29892	46.31222	0.00000	1.02914	-0.083333	0.0	0.0	0.0
4	18B.04	34.29893	45.84710	0.00000	0.87341	-0.083333	0.0	0.0	0.0
4	18B.04	34.29894	45.38197	0.00000	0.74761	-0.083333	0.0	0.0	0.0
4	18B.04	34.29895	44.91685	0.00000	0.64491	-0.083333	0.0	0.0	0.0
4	18B.04	34.29896	44.45172	0.00000	0.56023	-0.083333	0.0	0.0	0.0
4	18B.04	34.29897	43.98660	0.00000	0.48976	-0.083333	0.0	0.0	0.0
4	18B.04	34.29897	43.52148	0.00000	0.43060	-0.083333	0.0	0.0	0.0
4	18B.04	34.29898	43.05635	0.00000	0.38051	-0.083333	0.0	0.0	0.0
4	18B.04	34.29899	42.59123	0.00000	0.33777	-0.083333	0.0	0.0	0.0
4	18B.04	34.29900	42.12610	0.00000	0.30104	-0.083333	0.0	0.0	0.0
5	18B.05	34.29900	42.12610	0.00000	0.30104	-0.083333	0.0	0.0	0.0
5	18B.05	33.84477	42.12246	0.00000	0.29725	-0.083333	0.0	0.0	0.0
5	18B.05	33.39054	42.11881	0.00000	0.29203	-0.083333	0.0	0.0	0.0
5	18B.05	32.93631	42.11517	0.00000	0.28551	-0.083333	0.0	0.0	0.0
5	18B.05	32.48208	42.11153	0.00000	0.27787	-0.083333	0.0	0.0	0.0
5	18B.05	32.02784	42.10789	0.00000	0.26928	-0.083333	0.0	0.0	0.0
5	18B.05	31.57361	42.10424	0.00000	0.25994	-0.083333	0.0	0.0	0.0
5	18B.05	31.11938	42.10059	0.00000	0.25003	-0.083333	0.0	0.0	0.0
5	18B.05	30.66515	42.09695	0.00000	0.23972	-0.083333	0.0	0.0	0.0
5	18B.05	30.21092	42.09331	0.00000	0.22916	-0.083333	0.0	0.0	0.0
5	18B.05	29.75669	42.08966	0.00000	0.21849	-0.083333	0.0	0.0	0.0
5	18B.05	29.30246	42.08602	0.00000	0.20783	-0.083333	0.0	0.0	0.0
5	18B.05	28.84822	42.08237	0.00000	0.19728	-0.083333	0.0	0.0	0.0
5	18B.05	28.39399	42.07873	0.00000	0.18693	-0.083333	0.0	0.0	0.0
5	18B.05	27.93976	42.07509	0.00000	0.17683	-0.083333	0.0	0.0	0.0
5	18B.05	27.48553	42.07144	0.00000	0.16703	-0.083333	0.0	0.0	0.0
5	18B.05	27.03130	42.06780	0.00000	0.15758	-0.083333	0.0	0.0	0.0
6	18B.06	27.03130	42.06780	0.00000	0.15758	-0.083333	0.0	0.0	0.0
6	18B.06	27.03130	42.43965	0.00000	0.16726	-0.083333	0.0	0.0	0.0
6	18B.06	27.03130	42.81150	0.00000	0.17747	-0.083333	0.0	0.0	0.0
7	18B.07	27.03130	42.81150	0.00000	0.17747	-0.083333	0.0	0.0	0.0
7	18B.07	27.03267	43.28620	0.00000	0.19134	-0.083333	0.0	0.0	0.0
7	18B.07	27.03404	43.76090	0.00000	0.20613	-0.083333	0.0	0.0	0.0
7	18B.07	27.03541	44.23560	0.00000	0.22184	-0.083333	0.0	0.0	0.0
7	18B.07	27.03679	44.71030	0.00000	0.23847	-0.083333	0.0	0.0	0.0
7	18B.07	27.03816	45.18500	0.00000	0.25599	-0.083333	0.0	0.0	0.0
7	18B.07	27.03953	45.65970	0.00000	0.27432	-0.083333	0.0	0.0	0.0
7	18B.07	27.04090	46.13440	0.00000	0.29339	-0.083333	0.0	0.0	0.0
7	18B.07	27.04227	46.60910	0.00000	0.31308	-0.083333	0.0	0.0	0.0
7	18B.07	27.04364	47.08380	0.00000	0.33322	-0.083333	0.0	0.0	0.0
7	18B.07	27.04501	47.55850	0.00000	0.35391	-0.083333	0.0	0.0	0.0
7	18B.07	27.04639	48.03320	0.00000	0.37403	-0.083333	0.0	0.0	0.0
7	18B.07	27.04776	48.50790	0.00000	0.39421	-0.083333	0.0	0.0	0.0
7	18B.07	27.04913	48.98260	0.00000	0.41385	-0.083333	0.0	0.0	0.0
7	18B.07	27.05050	49.45730	0.00000	0.43266	-0.083333	0.0	0.0	0.0
7	18B.07	27.05187	49.93200	0.00000	0.45021	-0.083333	0.0	0.0	0.0
7	18B.07	27.05324	50.40670	0.00000	0.46650	-0.083333	0.0	0.0	0.0
7	18B.07	27.05461	50.88140	0.00000	0.48095	-0.083333	0.0	0.0	0.0
7	18B.07	27.05599	51.35610	0.00000	0.49340	-0.083333	0.0	0.0	0.0
7	18B.07	27.05736	51.83080	0.00000	0.50364	-0.083333	0.0	0.0	0.0
7	18B.07	27.05873	52.30550	0.00000	0.51222	-0.083333	0.0	0.0	0.0
7	18B.07	27.06010	52.78020	0.00000	0.51686	-0.083333	0.0	0.0	0.0
7	18B.07	27.06147	53.25490	0.00000	0.51965	-0.083333	0.0	0.0	0.0
7	18B.07	27.06284	53.72960	0.00000	0.51985	-0.083333	0.0	0.0	0.0
7	18B.07	27.06421	54.20430	0.00000	0.51748	-0.083333	0.0	0.0	0.0
7	18B.07	27.06559	54.67900	0.00000	0.51262	-0.083333	0.0	0.0	0.0
7	18B.07	27.06696	55.15370	0.00000	0.50537	-0.083333	0.0	0.0	0.0
7	18B.07	27.06833	55.62840	0.00000	0.49587	-0.083333	0.0	0.0	0.0



# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
 Building GMA  
 PDisp B01 - Underpin Loading

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc. Level [MPa]	Stress: Vertical [kN/m <sup>2</sup> ]	Stress: Sum Princ. [kN/m <sup>2</sup> ]	Vert. Strain [μ]
		[m]	[m]	[mOD]	[mm]				
7	18B_07	27.06970	56.10310	0.00000	0.48430	-0.083333	0.0	0.0	0.0
8	20FG_01	21.02660	64.09150	0.00000	0.07722	-0.083333	0.0	0.0	0.0
8	20FG_01	21.43170	64.00876	0.00000	0.08288	-0.083333	0.0	0.0	0.0
8	20FG_01	21.83680	63.92602	0.00000	0.08898	-0.083333	0.0	0.0	0.0
8	20FG_01	22.24190	63.84329	0.00000	0.09556	-0.083333	0.0	0.0	0.0
8	20FG_01	22.64700	63.76055	0.00000	0.10264	-0.083333	0.0	0.0	0.0
8	20FG_01	23.05210	63.67781	0.00000	0.11027	-0.083333	0.0	0.0	0.0
8	20FG_01	23.45720	63.59508	0.00000	0.11851	-0.083333	0.0	0.0	0.0
8	20FG_01	23.86230	63.51234	0.00000	0.12741	-0.083333	0.0	0.0	0.0
8	20FG_01	24.26740	63.42960	0.00000	0.13702	-0.083333	0.0	0.0	0.0
9	20FG_02	24.27400	63.42960	0.00000	0.13702	-0.083333	0.0	0.0	0.0
9	20FG_02	24.20781	62.93449	0.00000	0.14406	-0.083333	0.0	0.0	0.0
9	20FG_02	24.14823	62.43939	0.00000	0.15112	-0.083333	0.0	0.0	0.0
9	20FG_02	24.08864	61.94428	0.00000	0.15813	-0.083333	0.0	0.0	0.0
9	20FG_02	24.02905	61.44917	0.00000	0.16504	-0.083333	0.0	0.0	0.0
9	20FG_02	23.96946	60.95407	0.00000	0.17197	-0.083333	0.0	0.0	0.0
9	20FG_02	23.90987	60.45896	0.00000	0.17826	-0.083333	0.0	0.0	0.0
9	20FG_02	23.85029	59.96386	0.00000	0.18445	-0.083333	0.0	0.0	0.0
9	20FG_02	23.79070	59.46875	0.00000	0.19025	-0.083333	0.0	0.0	0.0
9	20FG_02	23.73111	58.97364	0.00000	0.19559	-0.083333	0.0	0.0	0.0
9	20FG_02	24.42370	50.18954	0.00000	0.20542	-0.083333	0.0	0.0	0.0
9	20FG_02	23.61194	57.98343	0.00000	0.20467	-0.083333	0.0	0.0	0.0
9	20FG_02	23.55235	57.48833	0.00000	0.20829	-0.083333	0.0	0.0	0.0
9	20FG_02	23.49276	56.99322	0.00000	0.21122	-0.083333	0.0	0.0	0.0
9	20FG_02	23.43317	56.49811	0.00000	0.21344	-0.083333	0.0	0.0	0.0
9	20FG_02	23.37359	56.00301	0.00000	0.21490	-0.083333	0.0	0.0	0.0
9	20FG_02	23.31400	55.50790	0.00000	0.21559	-0.083333	0.0	0.0	0.0
10	20FG_03	23.31400	55.50790	0.00000	0.21559	-0.083333	0.0	0.0	0.0
10	20FG_03	23.57895	55.53095	0.00000	0.22758	-0.083333	0.0	0.0	0.0
10	20FG_03	23.84390	55.55400	0.00000	0.24036	-0.083333	0.0	0.0	0.0
10	20FG_03	24.10885	55.57705	0.00000	0.25398	-0.083333	0.0	0.0	0.0
10	20FG_03	24.37380	55.60010	0.00000	0.26852	-0.083333	0.0	0.0	0.0
11	20FG_04	24.37380	55.60010	0.00000	0.26852	-0.083333	0.0	0.0	0.0
11	20FG_04	24.32904	55.39657	0.00000	0.26763	-0.083333	0.0	0.0	0.0
11	20FG_04	24.28428	55.19303	0.00000	0.26655	-0.083333	0.0	0.0	0.0
11	20FG_04	24.23952	54.98949	0.00000	0.26547	-0.083333	0.0	0.0	0.0
11	20FG_04	24.19477	54.78597	0.00000	0.26387	-0.083333	0.0	0.0	0.0
11	20FG_04	24.15001	54.58243	0.00000	0.26227	-0.083333	0.0	0.0	0.0
11	20FG_04	24.10525	54.37890	0.00000	0.26051	-0.083333	0.0	0.0	0.0
11	20FG_04	24.06049	54.17537	0.00000	0.25859	-0.083333	0.0	0.0	0.0
11	20FG_04	24.01573	53.97183	0.00000	0.25652	-0.083333	0.0	0.0	0.0
11	20FG_04	23.97097	53.76830	0.00000	0.25430	-0.083333	0.0	0.0	0.0
11	20FG_04	23.92622	53.56477	0.00000	0.25193	-0.083333	0.0	0.0	0.0
11	20FG_04	23.88146	53.36123	0.00000	0.24943	-0.083333	0.0	0.0	0.0
11	20FG_04	23.83670	53.15770	0.00000	0.24680	-0.083333	0.0	0.0	0.0
12	20FG_05	24.42370	53.15770	0.00000	0.24680	-0.083333	0.0	0.0	0.0
12	20FG_05	24.13020	53.18325	0.00000	0.26288	-0.083333	0.0	0.0	0.0
12	20FG_05	24.42370	53.20880	0.00000	0.28022	-0.083333	0.0	0.0	0.0
13	20FG_06	24.42370	53.20880	0.00000	0.28022	-0.083333	0.0	0.0	0.0
13	20FG_06	24.35847	52.82555	0.00000	0.27528	-0.083333	0.0	0.0	0.0
13	20FG_06	24.29321	52.44230	0.00000	0.26941	-0.083333	0.0	0.0	0.0
13	20FG_06	24.22803	52.05905	0.00000	0.26385	-0.083333	0.0	0.0	0.0
13	20FG_06	24.16280	51.67580	0.00000	0.25745	-0.083333	0.0	0.0	0.0
13	20FG_06	24.09757	51.29255	0.00000	0.25068	-0.083333	0.0	0.0	0.0
13	20FG_06	24.03235	50.90930	0.00000	0.24358	-0.083333	0.0	0.0	0.0
13	20FG_06	23.96710	50.52605	0.00000	0.23620	-0.083333	0.0	0.0	0.0
13	20FG_06	23.90190	50.14280	0.00000	0.22862	-0.083333	0.0	0.0	0.0
14	20FG_07	23.90190	50.14280	0.00000	0.22862	-0.083333	0.0	0.0	0.0
14	20FG_07	24.16280	50.16550	0.00000	0.24156	-0.083333	0.0	0.0	0.0
14	20FG_07	24.42370	50.18820	0.00000	0.25538	-0.083333	0.0	0.0	0.0
15	20FG_08	24.38441	50.18820	0.00000	0.25538	-0.083333	0.0	0.0	0.0
15	20FG_08	24.41686	49.74254	0.00000	0.24850	-0.083333	0.0	0.0	0.0
15	20FG_08	24.41001	49.29689	0.00000	0.24110	-0.083333	0.0	0.0	0.0
15	20FG_08	24.40317	48.85123	0.00000	0.23326	-0.083333	0.0	0.0	0.0
15	20FG_08	24.39632	48.40558	0.00000	0.22507	-0.083333	0.0	0.0	0.0
15	20FG_08	24.38948	47.95992	0.00000	0.21661	-0.083333	0.0	0.0	0.0
15	20FG_08	24.38263	47.51427	0.00000	0.20796	-0.083333	0.0	0.0	0.0
15	20FG_08	24.37579	47.06861	0.00000	0.19919	-0.083333	0.0	0.0	0.0
15	20FG_08	24.36894	46.62296	0.00000	0.19038	-0.083333	0.0	0.0	0.0
15	20FG_08	24.36210	46.17730	0.00000	0.18158	-0.083333	0.0	0.0	0.0
15	20FG_08	24.35525	45.73164	0.00000	0.17286	-0.083333	0.0	0.0	0.0
15	20FG_08	24.34841	45.28599	0.00000	0.16428	-0.083333	0.0	0.0	0.0
15	20FG_08	24.34157	44.84033	0.00000	0.15586	-0.083333	0.0	0.0	0.0
15	20FG_08	24.33472	44.39468	0.00000	0.14765	-0.083333	0.0	0.0	0.0
15	20FG_08	24.32788	43.94902	0.00000	0.13969	-0.083333	0.0	0.0	0.0
15	20FG_08	24.32103	43.50337	0.00000	0.13198	-0.083333	0.0	0.0	0.0
15	20FG_08	24.31419	43.05771	0.00000	0.12456	-0.083333	0.0	0.0	0.0
15	20FG_08	24.30734	42.61206	0.00000	0.11743	-0.083333	0.0	0.0	0.0
15	20FG_08	24.30050	42.16640	0.00000	0.11061	-0.083333	0.0	0.0	0.0
16	20FG_09	24.30050	42.16640	0.00000	0.11061	-0.083333	0.0	0.0	0.0
16	20FG_09	23.97097	42.24583	0.00000	0.10542	-0.083333	0.0	0.0	0.0
16	20FG_09	23.47350	42.32425	0.00000	0.10039	-0.083333	0.0	0.0	0.0
16	20FG_09	23.06000	42.40318	0.00000	0.09550	-0.083333	0.0	0.0	0.0
16	20FG_09	22.64650	42.48210	0.00000	0.09077	-0.083333	0.0	0.0	0.0
16	20FG_09	22.23300	42.56103	0.00000	0.08621	-0.083333	0.0	0.0	0.0
16	20FG_09	21.81950	42.63995	0.00000	0.08181	-0.083333	0.0	0.0	0.0
16	20FG_09	21.40600	42.71888	0.00000	0.07759	-0.083333	0.0	0.0	0.0
16	20FG_09	20.99250	42.79780	0.00000	0.07353	-0.083333	0.0	0.0	0.0
17	20FG_10	20.99250	42.79780	0.00000	0.07353	-0.083333	0.0	0.0	0.0
17	20FG_10	21.07865	43.03513	0.00000	0.07638	-0.083333	0.0	0.0	0.0
17	20FG_10	21.16480	43.27245	0.00000	0.07934	-0.083333	0.0	0.0	0.0
17	20FG_10	21.25095	43.50978	0.00000	0.08239	-0.083333	0.0	0.0	0.0
17	20FG_10	21.33710	43.74710	0.00000	0.08556	-0.083333	0.0	0.0	0.0
18	20FG_11	21.33710	43.74710	0.00000	0.08556	-0.083333	0.0	0.0	0.0
18	20FG_11	20.86376	43.83723	0.00000	0.08036	-0.083333	0.0	0.0	0.0
18	20FG_11	20.39042	43.92736	0.00000	0.07505	-0.083333	0.0	0.0	0.0
18	20FG_11	19.91708	44.01748	0.00000	0.07023	-0.083333	0.0	0.0	0.0
18	20FG_11	19.44374	44.10761	0.00000	0.06567	-0.083333	0.0	0.0	0.0
18	20FG_11	18.97041	44.19774	0.00000	0.06138	-0.083333	0.0	0.0	0.0
18	20FG_11	18.49707	44.28787	0.00000	0.05734	-0.083333	0.0	0.0	0.0
18	20FG_11	18.02373	44.37799	0.00000	0.05353	-0.083333	0.0	0.0	0.0
18	20FG_11	17.55039	44.46812	0.00000	0.04996	-0.083333	0.0	0.0	0.0
18	20FG_11	17.07705	44.55825	0.00000	0.04660	-0.083333	0.0	0.0	0.0
18	20FG_11	16.60371	44.64838	0.00000	0.04344	-0.083333	0.0	0.0	0.0
18	20FG_11	16.13037	44.73851	0.00000	0.04048	-0.083333	0.0	0.0	0.0
19	20FG_12	15.65703	44.82863	0.00000	0.03770	-0.083333	0.0	0.0	0.0
19	20FG_12	15.18369	44.91876	0.00000	0.03510	-0.083333	0.0	0.0	0.0
19	20FG_12	14.71036	45.00889	0.00000	0.03266	-0.083333	0.0	0.0	0.



# A-SQUARED STUDIO ENGINEERS LTD

**18A Froggnal Gardens**  
**Building GMA**  
**PDisp B01 - Underpin Loading**

Job No.	Sheet No.	Rev.
<b>1125</b>		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc. Level [MOD]	Stress: Vertical [kN/m <sup>2</sup> ]	Stress: Sum Princ. [kN/m <sup>2</sup> ]	Vert. Strain [μ]
		[m]	[m]	[MOD]	[mm]				
19	20FG.12	14.58959	53.77033	0.00000	0.04274	-0.083333	0.0	0.0	0.0
19	20FG.12	14.68427	54.23705	0.00000	0.04344	-0.083333	0.0	0.0	0.0
19	20FG.12	14.78255	54.70376	0.00000	0.04406	-0.083333	0.0	0.0	0.0
19	20FG.12	14.88082	55.17048	0.00000	0.04462	-0.083333	0.0	0.0	0.0
19	20FG.12	14.97910	55.63720	0.00000	0.04510	-0.083333	0.0	0.0	0.0
20	20FG.13	14.97910	55.63720	0.00000	0.04510	-0.083333	0.0	0.0	0.0
20	20FG.13	14.53283	55.76250	0.00000	0.04158	-0.083333	0.0	0.0	0.0
20	20FG.13	14.08655	55.88780	0.00000	0.03834	-0.083333	0.0	0.0	0.0
20	20FG.13	13.64028	56.01310	0.00000	0.03536	-0.083333	0.0	0.0	0.0
20	20FG.13	13.19400	56.13840	0.00000	0.03260	-0.083333	0.0	0.0	0.0
21	20FG.14	13.19400	56.13840	0.00000	0.03260	-0.083333	0.0	0.0	0.0
21	20FG.14	13.27410	56.53937	0.00000	0.03279	-0.083333	0.0	0.0	0.0
21	20FG.14	13.35420	56.94033	0.00000	0.03295	-0.083333	0.0	0.0	0.0
21	20FG.14	13.43430	57.34130	0.00000	0.03306	-0.083333	0.0	0.0	0.0
21	20FG.14	13.51440	57.74227	0.00000	0.03313	-0.083333	0.0	0.0	0.0
21	20FG.14	13.59450	58.14323	0.00000	0.03316	-0.083333	0.0	0.0	0.0
21	20FG.14	13.67460	58.54420	0.00000	0.03315	-0.083333	0.0	0.0	0.0
22	20FG.15	13.67460	58.54420	0.00000	0.03315	-0.083333	0.0	0.0	0.0
22	20FG.15	14.12543	58.46229	0.00000	0.03597	-0.083333	0.0	0.0	0.0
22	20FG.15	14.57626	58.38039	0.00000	0.03902	-0.083333	0.0	0.0	0.0
22	20FG.15	15.02709	58.29848	0.00000	0.04233	-0.083333	0.0	0.0	0.0
22	20FG.15	15.47791	58.21657	0.00000	0.04594	-0.083333	0.0	0.0	0.0
22	20FG.15	15.92874	58.13466	0.00000	0.04986	-0.083333	0.0	0.0	0.0
22	20FG.15	16.37957	58.05276	0.00000	0.05412	-0.083333	0.0	0.0	0.0
22	20FG.15	16.83040	57.97085	0.00000	0.05877	-0.083333	0.0	0.0	0.0
22	20FG.15	17.28123	57.88894	0.00000	0.06384	-0.083333	0.0	0.0	0.0
22	20FG.15	17.73206	57.80704	0.00000	0.06937	-0.083333	0.0	0.0	0.0
22	20FG.15	18.18289	57.72513	0.00000	0.07541	-0.083333	0.0	0.0	0.0
22	20FG.15	18.63371	57.64322	0.00000	0.08202	-0.083333	0.0	0.0	0.0
22	20FG.15	19.08454	57.56131	0.00000	0.08926	-0.083333	0.0	0.0	0.0
22	20FG.15	19.53537	57.47941	0.00000	0.09720	-0.083333	0.0	0.0	0.0
22	20FG.15	19.98620	57.39750	0.00000	0.10592	-0.083333	0.0	0.0	0.0
23	20FG.16	19.98620	57.39750	0.00000	0.10592	-0.083333	0.0	0.0	0.0
23	20FG.16	20.06051	57.87564	0.00000	0.10518	-0.083333	0.0	0.0	0.0
23	20FG.16	20.13483	58.35379	0.00000	0.10418	-0.083333	0.0	0.0	0.0
23	20FG.16	20.20915	58.83193	0.00000	0.10294	-0.083333	0.0	0.0	0.0
23	20FG.16	20.28346	59.31007	0.00000	0.10145	-0.083333	0.0	0.0	0.0
23	20FG.16	20.35777	59.78821	0.00000	0.09974	-0.083333	0.0	0.0	0.0
23	20FG.16	20.43209	60.26636	0.00000	0.09783	-0.083333	0.0	0.0	0.0
23	20FG.16	20.50640	60.74450	0.00000	0.09572	-0.083333	0.0	0.0	0.0
23	20FG.16	20.58071	61.22264	0.00000	0.09344	-0.083333	0.0	0.0	0.0
23	20FG.16	20.65503	61.70079	0.00000	0.09100	-0.083333	0.0	0.0	0.0
23	20FG.16	20.72934	62.17893	0.00000	0.08843	-0.083333	0.0	0.0	0.0
23	20FG.16	20.80366	62.65707	0.00000	0.08575	-0.083333	0.0	0.0	0.0
23	20FG.16	20.87797	63.13521	0.00000	0.08297	-0.083333	0.0	0.0	0.0
23	20FG.16	20.95229	63.61336	0.00000	0.08012	-0.083333	0.0	0.0	0.0
23	20FG.16	21.02660	64.09150	0.00000	0.07722	-0.083333	0.0	0.0	0.0
24	17HW.A01	58.70070	56.44780	0.00000	0.02371	-0.083333	0.0	0.0	0.0
24	17HW.A01	59.17122	56.40603	0.00000	0.02183	-0.083333	0.0	0.0	0.0
24	17HW.A01	59.64174	56.36426	0.00000	0.02008	-0.083333	0.0	0.0	0.0
24	17HW.A01	60.11226	56.32248	0.00000	0.01847	-0.083333	0.0	0.0	0.0
24	17HW.A01	60.58279	56.28071	0.00000	0.01698	-0.083333	0.0	0.0	0.0
24	17HW.A01	61.05331	56.23894	0.00000	0.01560	-0.083333	0.0	0.0	0.0
24	17HW.A01	61.52383	56.19717	0.00000	0.01432	-0.083333	0.0	0.0	0.0
24	17HW.A01	61.99436	56.15539	0.00000	0.01313	-0.083333	0.0	0.0	0.0
24	17HW.A01	62.46489	56.11362	0.00000	0.01204	-0.083333	0.0	0.0	0.0
24	17HW.A01	62.93540	56.07185	0.00000	0.01102	-0.083333	0.0	0.0	0.0
24	17HW.A01	63.40592	56.03008	0.00000	0.01009	-0.083333	0.0	0.0	0.0
24	17HW.A01	63.87644	55.98831	0.00000	0.00921	-0.083333	0.0	0.0	0.0
24	17HW.A01	64.34697	55.94653	0.00000	0.00841	-0.083333	0.0	0.0	0.0
24	17HW.A01	64.81749	55.90476	0.00000	0.00766	-0.083333	0.0	0.0	0.0
24	17HW.A01	65.28801	55.86299	0.00000	0.00697	-0.083333	0.0	0.0	0.0
24	17HW.A01	65.75853	55.82122	0.00000	0.00632	-0.083333	0.0	0.0	0.0
24	17HW.A01	66.22906	55.77944	0.00000	0.00573	-0.083333	0.0	0.0	0.0
24	17HW.A01	66.69958	55.73767	0.00000	0.00518	-0.083333	0.0	0.0	0.0
24	17HW.A01	67.17010	55.69590	0.00000	0.00466	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.17010	55.69590	0.00000	0.00466	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.15461	55.24739	0.00000	0.00471	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.13912	54.79889	0.00000	0.00475	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.12363	54.35038	0.00000	0.00478	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.10814	53.90188	0.00000	0.00480	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.09266	53.45337	0.00000	0.00482	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.07717	53.00487	0.00000	0.00483	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.06168	52.55636	0.00000	0.00484	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.04619	52.10786	0.00000	0.00484	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.03070	51.65935	0.00000	0.00483	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.01521	51.21084	0.00000	0.00482	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.99972	50.76234	0.00000	0.00480	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.98423	50.31383	0.00000	0.00477	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.96874	49.86533	0.00000	0.00474	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.95325	49.41682	0.00000	0.00470	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.93777	48.96832	0.00000	0.00466	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.92228	48.51981	0.00000	0.00460	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.90679	48.07131	0.00000	0.00455	-0.083333	0.0	0.0	0.0
25	17HW.A02	66.89130	47.62280	0.00000	0.00449	-0.083333	0.0	0.0	0.0
26	17HW.A03	66.89130	47.62280	0.00000	0.00449	-0.083333	0.0	0.0	0.0
26	17HW.A03	66.43956	47.65757	0.00000	0.00496	-0.083333	0.0	0.0	0.0
26	17HW.A03	65.98782	47.69234	0.00000	0.00548	-0.083333	0.0	0.0	0.0
26	17HW.A03	65.53608	47.72711	0.00000	0.00603	-0.083333	0.0	0.0	0.0
26	17HW.A03	65.08434	47.76188	0.00000	0.00663	-0.083333	0.0	0.0	0.0
26	17HW.A03	64.63260	47.79665	0.00000	0.00727	-0.083333	0.0	0.0	0.0
26	17HW.A03	64.18086	47.83142	0.00000	0.00796	-0.083333	0.0	0.0	0.0
26	17HW.A03	63.72912	47.86619	0.00000	0.00870	-0.083333	0.0	0.0	0.0
26	17HW.A03	63.27738	47.90096	0.00000	0.00950	-0.083333	0.0	0.0	0.0
26	17HW.A03	62.82564	47.93573	0.00000	0.01037	-0.083333	0.0	0.0	0.0
26	17HW.A03	62.37390	47.97050	0.00000	0.01129	-0.083333	0.0	0.0	0.0
26	17HW.A03	61.92216	48.00527	0.00000	0.01229	-0.083333	0.0	0.0	0.0
26	17HW.A03	61.47042	48.04004	0.00000	0.01337	-0.083333	0.0	0.0	0.0
26	17HW.A03	61.01868	48.07481	0.00000	0.01453	-0.083333	0.0	0.0	0.0
26	17HW.A03	60.56694	48.10958	0.00000	0.01578	-0.083333	0.0	0.0	0.0
26	17HW.A03	60.11520	48.14435	0.00000	0.01712	-0.083333	0.0	0.0	0.0
26	17HW.A03	59.66346	48.17912	0.00000	0.01858	-0.083333	0.0	0.0	0.0
26	17HW.A03	59.21172	48.21389	0.00000	0.02014	-0.083333	0.0	0.0	0.0
26	17HW.A03	58.75998	48.24866	0.00000	0.02183	-0.083333	0.0	0.0	0.0
26	17HW.A03	58.30824	48.28343	0.00000	0.02366	-0.083333	0.0	0.0	0.0
26	17HW.A03	57.85650	48.31820	0.00000	0.02563	-0.083333	0.0	0.0	0.0
27	17HW.A04	57.85650	48.31820	0.00000	0.02563	-0.083333	0.0	0.0	0.0
27	17HW.A04	57.90340	48.76984	0.00000					



**A-SQUARED STUDIO  
ENGINEERS LTD**

**18A Froggnal Gardens  
Building GMA  
PDisp B01 - Underpin Loading**

Job No.	Sheet No.	Rev.
<b>1125</b>		
Drg. Ref.		
Made by SB	Date	Checked

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
28	17HW_B01	58.90859	57.79717	0.00000	0.02210	-0.083333	0.0	0.0	0.0
28	17HW_B01	58.95452	57.33715	0.00000	0.02221	-0.083333	0.0	0.0	0.0
28	17HW_B01	59.00046	56.87712	0.00000	0.02228	-0.083333	0.0	0.0	0.0
28	17HW_B01	59.04640	56.41710	0.00000	0.02231	-0.083333	0.0	0.0	0.0
29	17HW_B02	59.04640	56.41710	0.00000	0.02231	-0.083333	0.0	0.0	0.0
29	17HW_B02	59.47996	56.37762	0.00000	0.02067	-0.083333	0.0	0.0	0.0
29	17HW_B02	59.91352	56.33815	0.00000	0.01914	-0.083333	0.0	0.0	0.0
29	17HW_B02	60.34709	56.29868	0.00000	0.01771	-0.083333	0.0	0.0	0.0
29	17HW_B02	60.78065	56.25920	0.00000	0.01638	-0.083333	0.0	0.0	0.0
29	17HW_B02	61.21421	56.21972	0.00000	0.01515	-0.083333	0.0	0.0	0.0
29	17HW_B02	61.64777	56.18025	0.00000	0.01400	-0.083333	0.0	0.0	0.0
29	17HW_B02	62.08134	56.14078	0.00000	0.01293	-0.083333	0.0	0.0	0.0
29	17HW_B02	62.51490	56.10130	0.00000	0.01193	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.51490	56.10130	0.00000	0.01193	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.53797	56.55704	0.00000	0.01178	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.56105	57.01278	0.00000	0.01162	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.58413	57.46851	0.00000	0.01144	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.60720	57.92425	0.00000	0.01126	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.63027	58.37999	0.00000	0.01106	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.65335	58.83573	0.00000	0.01085	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.67643	59.29146	0.00000	0.01063	-0.083333	0.0	0.0	0.0
30	17HW_B03	62.69950	59.74720	0.00000	0.01040	-0.083333	0.0	0.0	0.0
31	17HW_B04	62.69950	59.74720	0.00000	0.01040	-0.083333	0.0	0.0	0.0
31	17HW_B04	62.29744	59.78221	0.00000	0.01119	-0.083333	0.0	0.0	0.0
31	17HW_B04	61.89538	59.81722	0.00000	0.01204	-0.083333	0.0	0.0	0.0
31	17HW_B04	61.49332	59.85223	0.00000	0.01294	-0.083333	0.0	0.0	0.0
31	17HW_B04	61.09126	59.88724	0.00000	0.01390	-0.083333	0.0	0.0	0.0
31	17HW_B04	60.68920	59.92225	0.00000	0.01492	-0.083333	0.0	0.0	0.0
31	17HW_B04	60.28714	59.95726	0.00000	0.01601	-0.083333	0.0	0.0	0.0
31	17HW_B04	59.88508	59.99227	0.00000	0.01717	-0.083333	0.0	0.0	0.0
31	17HW_B04	59.48302	60.02728	0.00000	0.01841	-0.083333	0.0	0.0	0.0
31	17HW_B04	59.08096	60.06229	0.00000	0.01972	-0.083333	0.0	0.0	0.0
31	17HW_B04	58.67890	60.09730	0.00000	0.02112	-0.083333	0.0	0.0	0.0

**Results : Consolidation : Displacement Data : Lines**

None

**Results : Total : Displacement Data : Lines**

None



# A-SQUARED STUDIO ENGINEERS LTD

18A Froggnal Gardens  
Building GMA  
PDisp B02 - LT Loading

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

### Titles

Job No.: 1125  
 Job Title: 18A Froggnal Gardens  
 Sub-title: Building GMA  
 Calculation Heading: PDisp B02 - LT Loading  
 Initials: SB  
 Checker:  
 Date Saved:  
 Date Checked:  
 Notes:  
 File Name: PDisp B02 new.pdd  
 File Path: \\Mac\Dropbox for Business\A2-projects\1125 - 18a Froggnal Gardens\03 - Calculations\Issue 01\Pdisp

### History

Date	Time	By	Notes
14-Oct-2020	14:25	hamed	<history cleared>
14-Oct-2020	14:25	hamed	

### Analysis Options

#### General

Global Poisson's ratio: 0.20  
 Maximum allowable ratio between values of E: 1.5  
 Horizontal rigid boundary level: -34.00 [m OD]  
 Displacements at load centroids: Yes  
 GSA piled raft data: No

#### Elastic

Elastic: Yes  
 Analysis: Boussinesq  
 Stiffness for horizontal displacement calculations: Weighted average  
 Using legacy heave correction factor: No

#### Consolidation

Consolidation: No

### Soil Profiles Soil Profile 1

Layer ref.	Name	Level at top	Number of intermediate displacement levels	Youngs Modulus : Top	Youngs Modulus : Btm.	Poissons ratio	Non-linear curve
		[mOD]		[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]		
1	Made Ground	0.0	5	10000.	10000.	0.20000	None
2	Bagshot Formation	-1.0000	5	18000.	18000.	0.20000	None
3	London Clay	-7.0000	5	11520.	79560.	0.20000	None

### Soil Zones

Zone	Name	X min [m]	X max [m]	Y min [m]	Y max [m]	Profile
1	1	0.0	80.000	0.0	100.00	Soil Profile 1

### Polygonal Load Data

Load ref.	Name	Position : Level	Position : Polygon : Coords.	Position : Polygon Rectangles : Rect. tolerance [%]	No. of Rectangles	Value : Normal (local z) [kN/m <sup>2</sup> ]
1	Loading - 4F	-4.21000	(35.1,43.3) (35.1,53) (38.6,53) (39.9,54.3) (40.4,58.3) (44.6,58.3) (45.2,42.4) (41.6,42.4)		4	40.000
2	Loading - 3F	-4.21000	(40.4,43.3) (35.1,43.3) (41.6,42.4) (40.5,42.4) (39.4,41.5) (35.1,41.5)		2	30.000
3	Loading - 2FA	-4.21000	(40.4,58.3) (35.1,58.3) (35.1,53) (38.6,53) (39.9,54.3) (40.4,58.3)		2	20.000
4	Loading - 2FB	-4.21000	(39.4,41.5) (40.5,42.4) (45.2,42.4) (45.4,36) (41.9,36) (41.3,40.4) (40.4,1.5) (39.4,41.5)		8	20.000
5	Party wall loading	-4.00000	(34.6,49.3) (34.6,53.8) (35.6,53.8) (35.6,49.3)		1	114.00
6	Party wall loading	-6.60000	(34.5,58.5) (34.6,53.8) (35.6,53.8) (35.5,58.5)		1	114.00

### Polygonal Loads' Rectangles

No.	Centre x	Centre y	Angle of local x from global X [Degrees]	Width [m]	Depth [m]
<b>Load 1 : Loading - 4F</b> (Edge 4 optimal)					
1	43.07710	42.87167	-89.900	0.89811	4.1902
2	42.41853	56.32179	-89.900	3.9427	4.5336
3	42.00406	53.68886	-89.900	1.3217	5.5531
4	40.03279	48.17461	-89.900	9.6999	9.8946
<b>Load 2 : Loading - 3F</b> (Edge 1 optimal)					
1	38.04638	42.86936	-90.305	0.86120	5.9090
2	37.54178	41.98003	-90.305	0.91179	4.9093
<b>Load 3 : Loading - 2FA</b> (Edge 2 optimal)					
1	37.61788	56.31890	-90.138	3.9338	5.0665
2	37.15328	53.68971	-90.138	1.3268	4.1500
<b>Load 4 : Loading - 2FB</b> (Edge 6 optimal)					
1	44.98559	35.96963	92.070	0.062969	0.87111
2	44.11278	36.00110	92.070	0.062969	2.6133
3	43.48429	38.25599	92.070	4.4893	3.7066
4	42.95451	41.05182	92.070	1.1370	4.5635
5	42.54506	41.97525	92.070	0.69779	5.3152
6	42.39331	42.34682	92.070	0.055844	4.0465
7	41.65598	42.37605	92.070	0.055844	2.4279
8	40.91866	42.40528	92.070	0.055844	0.80931
<b>Load 5 : Party wall loading</b> (Edge 2 optimal)					
1	35.07988	51.55120	90.365	4.4777	0.99983
<b>Load 6 : Party wall loading</b> (Edge 1 optimal)					



# A-SQUARED STUDIO ENGINEERS LTD

18A Frognal Gardens  
Building GMA  
PDisp B02 - LT Loading

Job No.	Sheet No.	Rev.
1125		
Drg. Ref.		
Made by SB	Date	Checked

No.	Centre x	Centre y	Angle of local x from global x	Width x	Depth y
1	35.05053	56.14105	-89.633	4.6894	0.99993

### Displacement Lines

Name	X1 [m]	Y1 [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]	Intervals [No.]	Calculate	Detailed Results
18B.01	27.06970	56.10310	0.00000	32.02050	56.10310	0.00000	10	Yes	Yes
18B.02	32.02050	56.10310	0.00000	32.02020	53.28900	0.00000	6	Yes	Yes
18B.03	32.02020	53.28900	0.00000	34.29880	53.28910	0.00000	6	Yes	Yes
18B.04	34.29880	53.28910	0.00000	34.29900	42.12610	0.00000	2	Yes	Yes
18B.05	34.29900	42.12610	0.00000	27.03130	42.06780	0.00000	16	Yes	Yes
18B.06	27.03130	42.06780	0.00000	27.03130	42.81150	0.00000	2	Yes	Yes
18B.07	27.03130	42.81150	0.00000	27.06970	56.10310	0.00000	28	Yes	Yes
20FG.01	21.02660	64.09150	0.00000	24.26740	63.42960	0.00000	8	Yes	Yes
20FG.02	24.26740	63.42960	0.00000	23.31400	53.50790	0.00000	16	Yes	Yes
20FG.03	23.31400	53.50790	0.00000	24.37380	53.60010	0.00000	4	Yes	Yes
20FG.04	24.37380	53.60010	0.00000	23.83670	53.15770	0.00000	6	Yes	Yes
20FG.05	23.83670	53.15770	0.00000	24.42370	53.20880	0.00000	2	Yes	Yes
20FG.06	24.42370	53.20880	0.00000	23.90190	50.14280	0.00000	8	Yes	Yes
20FG.07	23.90190	50.14280	0.00000	24.42370	50.18820	0.00000	2	Yes	Yes
20FG.08	24.42370	50.18820	0.00000	24.30050	42.16640	0.00000	18	Yes	Yes
20FG.09	24.30050	42.16640	0.00000	20.99250	42.79780	0.00000	8	Yes	Yes
20FG.10	20.99250	42.79780	0.00000	21.33710	43.74710	0.00000	4	Yes	Yes
20FG.11	21.33710	43.74710	0.00000	12.81700	45.36940	0.00000	18	Yes	Yes
20FG.12	12.81700	45.36940	0.00000	14.97910	53.63720	0.00000	22	Yes	Yes
20FG.13	14.97910	53.63720	0.00000	13.19400	56.13840	0.00000	4	Yes	Yes
20FG.14	13.19400	56.13840	0.00000	13.67460	58.54420	0.00000	6	Yes	Yes
20FG.15	13.67460	58.54420	0.00000	19.98620	57.39750	0.00000	14	Yes	Yes
20FG.16	19.98620	57.39750	0.00000	21.02660	64.09150	0.00000	14	Yes	Yes
17HW.A01	58.70070	56.44780	0.00000	67.17010	53.69590	0.00000	18	Yes	Yes
17HW.A02	67.17010	53.69590	0.00000	66.89130	47.62280	0.00000	18	Yes	Yes
17HW.A03	66.89130	47.62280	0.00000	57.85650	48.31820	0.00000	20	Yes	Yes
17HW.A04	57.85650	48.31820	0.00000	58.70070	56.44780	0.00000	18	Yes	Yes
17HW.B01	58.67890	60.09730	0.00000	59.04640	56.41710	0.00000	8	Yes	Yes
17HW.B02	59.04640	56.41710	0.00000	62.51490	56.10130	0.00000	8	Yes	Yes
17HW.B03	62.51490	56.10130	0.00000	62.69950	59.74720	0.00000	10	Yes	Yes
17HW.B04	62.69950	59.74720	0.00000	58.67890	60.09730	0.00000	10	Yes	Yes

### Results : Immediate : Load Centres : Polygonal

Ref.	Name	x	y	z	dz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
1	Loading - 4F	40.57994	49.47071	-4.21000	18.95743	-4.6750	39.991	89.543	0.0016711
2	Loading - 3F	37.82069	42.45519	-4.21000	11.82776	-4.6750	29.348	61.129	0.0012773
3	Loading - 2FA	37.52464	55.78655	-4.21000	13.00571	-4.6750	20.037	46.300	821.35E-6
4	Loading - 2B	29.05002	44.45172	-4.21000	2.08637	-4.6750	19.885	41.780	861.47E-6
5	Party wall loading	35.07987	51.55124	-4.00000	22.70350	-4.5000	113.17	178.24	0.0055641
6	Party wall loading	35.05052	56.14109	-6.60000	16.95576	-6.8000	122.83	229.07	0.0056433

### Results : Consolidation : Load Centres : Polygonal

None

### Results : Total : Load Centres : Polygonal

None

### Results : Immediate : Displacement Data : Lines

Ref.	Name	x	y	z	dz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
1	18B.01	27.06970	56.10310	0.00000	1.36631	-0.083333	0.0	0.0	0.0
1	18B.01	27.56478	56.10310	0.00000	1.51415	-0.083333	0.0	0.0	0.0
1	18B.01	28.05986	56.10310	0.00000	1.68237	-0.083333	0.0	0.0	0.0
1	18B.01	28.55494	56.10310	0.00000	1.87481	-0.083333	0.0	0.0	0.0
1	18B.01	29.05002	56.10310	0.00000	2.08637	-0.083333	0.0	0.0	0.0
1	18B.01	29.54510	56.10310	0.00000	2.35330	-0.083333	0.0	0.0	0.0
1	18B.01	30.04018	56.10310	0.00000	2.65393	-0.083333	0.0	0.0	0.0
1	18B.01	30.53526	56.10310	0.00000	3.00972	-0.083333	0.0	0.0	0.0
1	18B.01	31.03034	56.10310	0.00000	3.43748	-0.083333	0.0	0.0	0.0
1	18B.01	31.52542	56.10310	0.00000	3.93000	-0.083333	0.0	0.0	0.0
1	18B.01	32.02050	56.10310	0.00000	4.43279	-0.083333	0.0	0.0	0.0
2	18B.02	32.02050	56.10310	0.00000	4.63279	-0.083333	0.0	0.0	0.0
2	18B.02	32.02045	55.63408	0.00000	4.84551	-0.083333	0.0	0.0	0.0
2	18B.02	32.02040	55.16507	0.00000	5.03884	-0.083333	0.0	0.0	0.0
2	18B.02	32.02035	54.69605	0.00000	5.21219	-0.083333	0.0	0.0	0.0
2	18B.02	32.02030	54.22703	0.00000	5.36485	-0.083333	0.0	0.0	0.0
2	18B.02	32.02025	53.75802	0.00000	5.49612	-0.083333	0.0	0.0	0.0
2	18B.02	32.02020	53.28900	0.00000	5.60516	-0.083333	0.0	0.0	0.0
3	18B.03	32.02020	53.28900	0.00000	5.60516	-0.083333	0.0	0.0	0.0
3	18B.03	32.39997	49.10298	0.00000	6.35877	-0.083333	0.0	0.0	0.0
3	18B.03	32.77973	53.28903	0.00000	7.26756	-0.083333	0.0	0.0	0.0
3	18B.03	33.15950	53.28905	0.00000	8.38245	-0.083333	0.0	0.0	0.0
3	18B.03	33.53927	53.28907	0.00000	9.77248	-0.083333	0.0	0.0	0.0
3	18B.03	33.91903	53.28908	0.00000	11.55887	-0.083333	0.0	0.0	0.0
4	18B.04	34.29880	53.28910	0.00000	14.22573	-0.083333	0.0	0.0	0.0
4	18B.04	34.29880	53.28910	0.00000	14.22573	-0.083333	0.0	0.0	0.0
4	18B.04	34.29881	52.82397	0.00000	14.25671	-0.083333	0.0	0.0	0.0
4	18B.04	34.29882	52.35885	0.00000	14.26613	-0.083333	0.0	0.0	0.0
4	18B.04	34.29883	51.89372	0.00000	14.26787	-0.083333	0.0	0.0	0.0
4	18B.04	34.29884	51.42860	0.00000	14.21815	-0.083333	0.0	0.0	0.0
4	18B.04	34.29884	50.96347	0.00000	14.07322	-0.083333	0.0	0.0	0.0
4	18B.04	34.29885	50.49835	0.00000	13.78873	-0.083333	0.0	0.0	0.0
4	18B.04	34.29886	50.03323	0.00000	13.30184	-0.083333	0.0	0.0	0.0
4	18B.04	34.29887	49.56810	0.00000	12.47348	-0.083333	0.0	0.0	0.0
4	18B.04	34.29888	49.10298	0.00000	11.25656	-0.083333	0.0	0.0	0.0
4	18B.04	34.29888	48.63785	0.00000	10.33317	-0.083333	0.0	0.0	0.0
4	18B.04	34.29889	48.17272	0.00000	9.71774	-0.083333	0.0	0.0	0.0
4	18B.04	34.29890	47.70760	0.00000	9.25437	-0.083333	0.0	0.0	0.0
4	18B.04	34.29891	47.24247	0.00000	8.87808	-0.083333	0.0	0.0	0.0
4	18B.04	34.29892	46.77735	0.00000	8.55268	-0.083333	0.0	0.0	0.0
4	18B.04	34.29892	46.31222	0.00000	8.25533	-0.083333	0.0	0.0	0.0
4	18B.04	34.29893	45.84710	0.00000	7.97015	-0.083333	0.0	0.0	0.0
4	18B.04	34.29894	45.38197	0.00000	7.68496	-0.083333	0.0	0.0	0.0
4	18B.04	34.29895	44.91685	0.00000	7.38964	-0.083333	0.0	0.0	0.0
4	18B.04	34.29896	44.45172	0.00000	7.07539	-0.083333	0.0	0.0	0.0
4	18B.04	34.29897	43.98660	0.00000	6.73472	-0.083333	0.0	0.0	0.0
4	18B.04	34.29897	43.52148	0.00000	6.36303	-0.083333	0.0	0.0	0.0
4	18B.04	34.29898	43.05635	0.00000	5.96124	-0.083333	0.0	0.0	0.0
4	18B.04	34.29899	42.59123	0.00000	5.53388	-0.083333	0.0	0.0	0.0
4	18B.04	34.29900	42.12610	0.00000	5.08368	-0.083333	0.0	0.0	0.0
5	18B.05	33.84477	42.12246	0.00000	4.44925	-0.083333	0.0	0.0	0.0
5	18B.05	33.39054	42.11881	0.00000	3.93254	-0.083333	0.0	0.0	0.0
5	18B.05	32.93631	42.11517	0.00000	3.50036	-0.083333	0.0	0.0	0.0



# A-SQUARED STUDIO ENGINEERS LTD

18A Frognal Gardens  
Building GMA  
PDisp B02 - LT Loading

Job No. Sheet No. Rev.

1125

Drg. Ref.

Made by Date Checked  
SB

Ref.	Name	x	y	z	$\delta z$	Stress: Calc. Level [MOD]	Stress: Vertical [kN/m <sup>2</sup> ]	Stress: Sum Princ. [kN/m <sup>2</sup> ]	Vert. Strain [μ]
[m]	[m]	[MOD]	[mm]	[MOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[μ]		
5	18B.05	32.49208	42.11153	0.00000	3.13259	-0.083333	0.0	0.0	0.0
5	18B.05	32.02784	42.10788	0.00000	2.81619	-0.083333	0.0	0.0	0.0
5	18B.05	31.57361	42.10424	0.00000	2.54178	-0.083333	0.0	0.0	0.0
5	18B.05	31.11938	42.10059	0.00000	2.30216	-0.083333	0.0	0.0	0.0
5	18B.05	30.66515	42.09695	0.00000	2.09162	-0.083333	0.0	0.0	0.0
5	18B.05	29.21092	42.09331	0.00000	1.90553	-0.083333	0.0	0.0	0.0
5	18B.05	29.75669	42.08966	0.00000	1.74016	-0.083333	0.0	0.0	0.0
5	18B.05	29.30246	42.08602	0.00000	1.59248	-0.083333	0.0	0.0	0.0
5	18B.05	28.84822	42.08237	0.00000	1.46000	-0.083333	0.0	0.0	0.0
5	18B.05	28.39399	42.07873	0.00000	1.34068	-0.083333	0.0	0.0	0.0
5	18B.05	27.93976	42.07509	0.00000	1.23284	-0.083333	0.0	0.0	0.0
5	18B.05	27.48553	42.07144	0.00000	1.13507	-0.083333	0.0	0.0	0.0
5	18B.05	27.03130	42.06780	0.00000	1.04619	-0.083333	0.0	0.0	0.0
6	18B.06	27.03130	42.06780	0.00000	1.04619	-0.083333	0.0	0.0	0.0
6	18B.06	27.03130	42.43965	0.00000	1.08008	-0.083333	0.0	0.0	0.0
6	18B.06	27.03130	42.81150	0.00000	1.11384	-0.083333	0.0	0.0	0.0
7	18B.07	27.03130	42.81150	0.00000	1.11384	-0.083333	0.0	0.0	0.0
7	18B.07	27.03267	43.28620	0.00000	1.15688	-0.083333	0.0	0.0	0.0
7	18B.07	27.03404	43.76090	0.00000	1.19936	-0.083333	0.0	0.0	0.0
7	18B.07	27.03541	44.23560	0.00000	1.24106	-0.083333	0.0	0.0	0.0
7	18B.07	27.03679	44.71030	0.00000	1.28176	-0.083333	0.0	0.0	0.0
7	18B.07	27.03816	45.18500	0.00000	1.32124	-0.083333	0.0	0.0	0.0
7	18B.07	27.03953	45.65970	0.00000	1.35929	-0.083333	0.0	0.0	0.0
7	18B.07	27.04090	46.13440	0.00000	1.39566	-0.083333	0.0	0.0	0.0
7	18B.07	27.04227	46.60910	0.00000	1.43032	-0.083333	0.0	0.0	0.0
7	18B.07	27.04364	47.08380	0.00000	1.46411	-0.083333	0.0	0.0	0.0
7	18B.07	27.04501	47.55850	0.00000	1.49725	-0.083333	0.0	0.0	0.0
7	18B.07	27.04639	48.03320	0.00000	1.51937	-0.083333	0.0	0.0	0.0
7	18B.07	27.04776	48.50790	0.00000	1.54345	-0.083333	0.0	0.0	0.0
7	18B.07	27.04913	48.98260	0.00000	1.56421	-0.083333	0.0	0.0	0.0
7	18B.07	27.05050	49.45730	0.00000	1.58394	-0.083333	0.0	0.0	0.0
7	18B.07	27.05187	49.93200	0.00000	1.59456	-0.083333	0.0	0.0	0.0
7	18B.07	27.05324	50.40670	0.00000	1.60363	-0.083333	0.0	0.0	0.0
7	18B.07	27.05461	50.88140	0.00000	1.60832	-0.083333	0.0	0.0	0.0
7	18B.07	27.05599	51.35610	0.00000	1.60847	-0.083333	0.0	0.0	0.0
7	18B.07	27.05736	51.83080	0.00000	1.60397	-0.083333	0.0	0.0	0.0
7	18B.07	27.05873	52.30550	0.00000	1.59477	-0.083333	0.0	0.0	0.0
7	18B.07	27.06010	52.78020	0.00000	1.58090	-0.083333	0.0	0.0	0.0
7	18B.07	27.06147	53.25490	0.00000	1.56242	-0.083333	0.0	0.0	0.0
7	18B.07	27.06284	53.72960	0.00000	1.53948	-0.083333	0.0	0.0	0.0
7	18B.07	27.06421	54.20430	0.00000	1.51228	-0.083333	0.0	0.0	0.0
7	18B.07	27.06559	54.67900	0.00000	1.48105	-0.083333	0.0	0.0	0.0
7	18B.07	27.06696	55.15370	0.00000	1.44610	-0.083333	0.0	0.0	0.0
7	18B.07	27.06833	55.62840	0.00000	1.40773	-0.083333	0.0	0.0	0.0
7	18B.07	27.06970	56.10310	0.00000	1.36631	-0.083333	0.0	0.0	0.0
8	20FG.01	21.43170	64.00876	0.00000	0.24381	-0.083333	0.0	0.0	0.0
8	20FG.01	21.83680	63.92602	0.00000	0.27942	-0.083333	0.0	0.0	0.0
8	20FG.01	22.24190	63.84329	0.00000	0.29912	-0.083333	0.0	0.0	0.0
8	20FG.01	22.64700	63.76055	0.00000	0.32021	-0.083333	0.0	0.0	0.0
8	20FG.01	23.05210	63.67781	0.00000	0.34280	-0.083333	0.0	0.0	0.0
8	20FG.01	23.45720	63.59508	0.00000	0.36701	-0.083333	0.0	0.0	0.0
8	20FG.01	23.86230	63.51234	0.00000	0.39297	-0.083333	0.0	0.0	0.0
8	20FG.01	24.26740	63.42960	0.00000	0.42081	-0.083333	0.0	0.0	0.0
9	20FG.02	24.26740	63.42960	0.00000	0.42081	-0.083333	0.0	0.0	0.0
9	20FG.02	24.67250	63.34686	0.00000	0.44072	-0.083333	0.0	0.0	0.0
9	20FG.02	24.14823	62.43939	0.00000	0.46074	-0.083333	0.0	0.0	0.0
9	20FG.02	24.08864	61.94428	0.00000	0.48078	-0.083333	0.0	0.0	0.0
9	20FG.02	24.02905	61.44917	0.00000	0.50071	-0.083333	0.0	0.0	0.0
9	20FG.02	23.96946	60.95407	0.00000	0.52042	-0.083333	0.0	0.0	0.0
9	20FG.02	23.90987	60.45896	0.00000	0.53976	-0.083333	0.0	0.0	0.0
9	20FG.02	23.85029	59.96386	0.00000	0.55861	-0.083333	0.0	0.0	0.0
9	20FG.02	23.79070	59.46875	0.00000	0.57682	-0.083333	0.0	0.0	0.0
9	20FG.02	23.73111	58.97364	0.00000	0.59426	-0.083333	0.0	0.0	0.0
9	20FG.02	23.67152	58.47854	0.00000	0.61080	-0.083333	0.0	0.0	0.0
9	20FG.02	23.61194	57.98343	0.00000	0.62659	-0.083333	0.0	0.0	0.0
9	20FG.02	23.55235	57.48833	0.00000	0.64062	-0.083333	0.0	0.0	0.0
9	20FG.02	23.49276	56.99322	0.00000	0.65368	-0.083333	0.0	0.0	0.0
9	20FG.02	23.43317	56.49811	0.00000	0.66536	-0.083333	0.0	0.0	0.0
9	20FG.02	23.37359	56.00301	0.00000	0.67557	-0.083333	0.0	0.0	0.0
9	20FG.02	23.31400	55.50790	0.00000	0.68423	-0.083333	0.0	0.0	0.0
10	20FG.03	23.31400	55.50790	0.00000	0.68423	-0.083333	0.0	0.0	0.0
10	20FG.03	23.57895	55.53095	0.00000	0.71767	-0.083333	0.0	0.0	0.0
10	20FG.03	23.84390	55.55400	0.00000	0.75295	-0.083333	0.0	0.0	0.0
10	20FG.03	24.10885	55.57705	0.00000	0.79018	-0.083333	0.0	0.0	0.0
10	20FG.03	24.37380	55.60010	0.00000	0.82950	-0.083333	0.0	0.0	0.0
11	20FG.04	24.37380	55.60010	0.00000	0.82950	-0.083333	0.0	0.0	0.0
11	20FG.04	24.28428	55.19303	0.00000	0.83140	-0.083333	0.0	0.0	0.0
11	20FG.04	24.19477	54.78597	0.00000	0.83175	-0.083333	0.0	0.0	0.0
11	20FG.04	24.10525	54.37890	0.00000	0.83057	-0.083333	0.0	0.0	0.0
11	20FG.04	24.01574	53.97183	0.00000	0.82789	-0.083333	0.0	0.0	0.0
11	20FG.04	23.92622	53.56477	0.00000	0.82376	-0.083333	0.0	0.0	0.0
11	20FG.04	23.83670	53.15770	0.00000	0.81822	-0.083333	0.0	0.0	0.0
12	20FG.05	23.83670	53.15770	0.00000	0.81822	-0.083333	0.0	0.0	0.0
12	20FG.05	24.13020	53.18325	0.00000	0.86493	-0.083333	0.0	0.0	0.0
12	20FG.05	24.42370	53.20880	0.00000	0.91473	-0.083333	0.0	0.0	0.0
13	20FG.06	24.42370	53.20880	0.00000	0.91473	-0.083333	0.0	0.0	0.0
13	20FG.06	24.35847	52.82555	0.00000	0.91101	-0.083333	0.0	0.0	0.0
13	20FG.06	24.29325	52.44230	0.00000	0.90590	-0.083333	0.0	0.0	0.0
13	20FG.06	24.22803	52.05905	0.00000	0.89944	-0.083333	0.0	0.0	0.0
13	20FG.06	24.16280	51.67580	0.00000	0.89170	-0.083333	0.0	0.0	0.0
13	20FG.06	24.09757	51.29255	0.00000	0.88274	-0.083333	0.0	0.0	0.0
13	20FG.06	24.03235	50.90930	0.00000	0.87263	-0.083333	0.0	0.0	0.0
13	20FG.06	23.96712	50.52605	0.00000	0.86144	-0.083333	0.0	0.0	0.0
13	20FG.06	23.90190	50.14280	0.00000	0.84925	-0.083333	0.0	0.0	0.0
14	20FG.07	24.30190	50.14280	0.00000	0.84925	-0.083333	0.0	0.0	0.0
14	20FG.07	24.16280	50.16550	0.00000	0.89285	-0.083333	0.0	0.0	0.0
14	20FG.07	24.42370	50.18820	0.00000	0.93904	-0.083333	0.0	0.0	0.0
15	20FG.08	24.42370	50.18820	0.00000	0.93904	-0.083333	0.0	0.0	0.0
15	20FG.08	24.41686	49.74254	0.00000	0.93412	-0.083333	0.0	0.0	0.0
15	20FG.08	24.30910	49.29689	0.00000	0.92745	-0.083333	0.0	0.0	0.0
15	20FG.08	24.40317	48.85123	0.00000	0.91911	-0.083333	0.0	0.0	0.0
15	20FG.08	24.39632	48.40558	0.00000	0.90918	-0.083333	0.0	0.0	0.0
15	20FG.08	24.38948	47.95992	0.00000	0.89774	-0.083333	0.0	0.0	0.0
15	20FG.08	24.38263	47.51427	0.00000	0.88490	-0.083333	0.0	0.0	0.0
15	20FG.08	24.37579	47.06861	0.00000	0.87074	-0.083333	0.0	0.0	0.0
15	20FG.08	24.36894	46.62296	0.00000	0.85538	-0.083333	0.0	0.0	0.0
15	20FG.08	24.36210	46.17730	0.00000	0.83890	-0.083333	0.0	0.0	0.0
15	20FG.08	24.35526	45.73164	0.00000	0.82142	-0.083333	0.0	0.0	0.0
15	20FG.08								



# A-SQUARED STUDIO ENGINEERS LTD

Job No. Sheet No. Rev.

1125

Dr. Ref.

Made by  
SB

Date

Checked

18A Frogna Gardens  
Building GMA  
PDisp B02 - LT Loading

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m <sup>2</sup> ]	[kN/m <sup>2</sup> ]	[µ]
17	20FG.10	21.33710	43.74710	0.00000	0.43872	-0.083333	0.0	0.0	0.0
18	20FG.10	21.33710	43.74710	0.00000	0.43872	-0.083333	0.0	0.0	0.0
18	20FG.11	20.86376	43.83723	0.00000	0.40677	-0.083333	0.0	0.0	0.0
18	20FG.11	20.39042	43.92736	0.00000	0.37714	-0.083333	0.0	0.0	0.0
18	20FG.11	19.91708	44.01748	0.00000	0.34965	-0.083333	0.0	0.0	0.0
18	20FG.11	19.44374	44.10761	0.00000	0.32144	-0.083333	0.0	0.0	0.0
18	20FG.11	18.97041	44.19774	0.00000	0.30045	-0.083333	0.0	0.0	0.0
18	20FG.11	18.49707	44.28787	0.00000	0.27846	-0.083333	0.0	0.0	0.0
18	20FG.11	18.02373	44.37799	0.00000	0.25803	-0.083333	0.0	0.0	0.0
18	20FG.11	17.55039	44.46812	0.00000	0.23904	-0.083333	0.0	0.0	0.0
18	20FG.11	17.07705	44.55825	0.00000	0.22140	-0.083333	0.0	0.0	0.0
18	20FG.11	16.60371	44.64838	0.00000	0.20501	-0.083333	0.0	0.0	0.0
18	20FG.11	16.13037	44.73851	0.00000	0.18977	-0.083333	0.0	0.0	0.0
18	20FG.11	15.65703	44.82863	0.00000	0.17560	-0.083333	0.0	0.0	0.0
18	20FG.11	15.18369	44.91876	0.00000	0.16242	-0.083333	0.0	0.0	0.0
18	20FG.11	14.71036	45.00889	0.00000	0.15016	-0.083333	0.0	0.0	0.0
18	20FG.11	14.23702	45.09902	0.00000	0.13877	-0.083333	0.0	0.0	0.0
18	20FG.11	13.76368	45.18914	0.00000	0.12816	-0.083333	0.0	0.0	0.0
18	20FG.11	13.29034	45.27927	0.00000	0.11830	-0.083333	0.0	0.0	0.0
18	20FG.11	12.81700	45.36940	0.00000	0.10912	-0.083333	0.0	0.0	0.0
19	20FG.12	12.34366	45.45953	0.00000	0.10054	-0.083333	0.0	0.0	0.0
19	20FG.12	12.91528	45.83612	0.00000	0.11251	-0.083333	0.0	0.0	0.0
19	20FG.12	13.01355	46.30284	0.00000	0.11586	-0.083333	0.0	0.0	0.0
19	20FG.12	13.11183	46.76955	0.00000	0.11917	-0.083333	0.0	0.0	0.0
19	20FG.12	13.21011	47.23627	0.00000	0.12242	-0.083333	0.0	0.0	0.0
19	20FG.12	13.30839	47.70299	0.00000	0.12560	-0.083333	0.0	0.0	0.0
19	20FG.12	13.40666	48.16971	0.00000	0.12870	-0.083333	0.0	0.0	0.0
19	20FG.12	13.50494	48.63643	0.00000	0.13170	-0.083333	0.0	0.0	0.0
19	20FG.12	13.60322	49.10315	0.00000	0.13460	-0.083333	0.0	0.0	0.0
19	20FG.12	13.70150	49.56986	0.00000	0.13739	-0.083333	0.0	0.0	0.0
19	20FG.12	13.79978	50.03658	0.00000	0.14009	-0.083333	0.0	0.0	0.0
19	20FG.12	13.89805	50.50330	0.00000	0.14256	-0.083333	0.0	0.0	0.0
19	20FG.12	13.99633	50.97002	0.00000	0.14493	-0.083333	0.0	0.0	0.0
19	20FG.12	14.09460	51.43674	0.00000	0.14714	-0.083333	0.0	0.0	0.0
19	20FG.12	14.19288	51.90345	0.00000	0.14918	-0.083333	0.0	0.0	0.0
19	20FG.12	14.29116	52.37017	0.00000	0.15104	-0.083333	0.0	0.0	0.0
19	20FG.12	14.38944	52.83689	0.00000	0.15270	-0.083333	0.0	0.0	0.0
19	20FG.12	14.48771	53.30361	0.00000	0.15417	-0.083333	0.0	0.0	0.0
19	20FG.12	14.58599	53.77033	0.00000	0.15543	-0.083333	0.0	0.0	0.0
19	20FG.12	14.68427	54.23705	0.00000	0.15647	-0.083333	0.0	0.0	0.0
19	20FG.12	14.78255	54.70376	0.00000	0.15729	-0.083333	0.0	0.0	0.0
19	20FG.12	14.88082	55.17048	0.00000	0.15790	-0.083333	0.0	0.0	0.0
19	20FG.12	14.97910	55.63720	0.00000	0.15827	-0.083333	0.0	0.0	0.0
20	20FG.13	14.97910	55.63720	0.00000	0.15827	-0.083333	0.0	0.0	0.0
20	20FG.13	14.53283	55.76250	0.00000	0.14583	-0.083333	0.0	0.0	0.0
20	20FG.13	14.08656	55.88780	0.00000	0.13433	-0.083333	0.0	0.0	0.0
20	20FG.13	13.64028	56.01310	0.00000	0.12369	-0.083333	0.0	0.0	0.0
20	20FG.13	13.19400	56.13840	0.00000	0.11384	-0.083333	0.0	0.0	0.0
21	20FG.14	13.19400	56.13840	0.00000	0.11384	-0.083333	0.0	0.0	0.0
21	20FG.14	13.27410	56.53937	0.00000	0.11379	-0.083333	0.0	0.0	0.0
21	20FG.14	13.35420	56.94033	0.00000	0.11362	-0.083333	0.0	0.0	0.0
21	20FG.14	13.43430	57.34130	0.00000	0.11333	-0.083333	0.0	0.0	0.0
21	20FG.14	13.51440	57.74227	0.00000	0.11293	-0.083333	0.0	0.0	0.0
21	20FG.14	13.59450	58.14323	0.00000	0.11241	-0.083333	0.0	0.0	0.0
21	20FG.14	13.67460	58.54420	0.00000	0.11177	-0.083333	0.0	0.0	0.0
22	20FG.15	13.75470	58.94516	0.00000	0.11103	-0.083333	0.0	0.0	0.0
22	20FG.15	14.12543	58.46229	0.00000	0.12135	-0.083333	0.0	0.0	0.0
22	20FG.15	14.57626	58.38039	0.00000	0.13168	-0.083333	0.0	0.0	0.0
22	20FG.15	15.02709	58.29848	0.00000	0.14284	-0.083333	0.0	0.0	0.0
22	20FG.15	15.47791	58.21657	0.00000	0.15490	-0.083333	0.0	0.0	0.0
22	20FG.15	15.92874	58.13466	0.00000	0.16782	-0.083333	0.0	0.0	0.0
22	20FG.15	16.37957	58.05276	0.00000	0.18202	-0.083333	0.0	0.0	0.0
22	20FG.15	16.83040	57.97085	0.00000	0.19726	-0.083333	0.0	0.0	0.0
22	20FG.15	17.28123	57.88894	0.00000	0.21377	-0.083333	0.0	0.0	0.0
22	20FG.15	17.73206	57.80704	0.00000	0.23165	-0.083333	0.0	0.0	0.0
22	20FG.15	18.18289	57.72513	0.00000	0.25104	-0.083333	0.0	0.0	0.0
22	20FG.15	18.63371	57.64322	0.00000	0.27208	-0.083333	0.0	0.0	0.0
22	20FG.15	19.08454	57.56131	0.00000	0.29493	-0.083333	0.0	0.0	0.0
22	20FG.15	19.53537	57.47941	0.00000	0.31977	-0.083333	0.0	0.0	0.0
22	20FG.15	19.98620	57.39750	0.00000	0.34679	-0.083333	0.0	0.0	0.0
23	20FG.16	19.98620	57.39750	0.00000	0.34679	-0.083333	0.0	0.0	0.0
23	20FG.16	20.06051	57.87564	0.00000	0.34215	-0.083333	0.0	0.0	0.0
23	20FG.16	20.13483	58.35379	0.00000	0.33695	-0.083333	0.0	0.0	0.0
23	20FG.16	20.20914	58.83193	0.00000	0.33121	-0.083333	0.0	0.0	0.0
23	20FG.16	20.28346	59.31007	0.00000	0.32497	-0.083333	0.0	0.0	0.0
23	20FG.16	20.35777	59.78821	0.00000	0.31826	-0.083333	0.0	0.0	0.0
23	20FG.16	20.43209	60.26636	0.00000	0.31112	-0.083333	0.0	0.0	0.0
23	20FG.16	20.50640	60.74450	0.00000	0.30360	-0.083333	0.0	0.0	0.0
23	20FG.16	20.58071	61.22264	0.00000	0.29573	-0.083333	0.0	0.0	0.0
23	20FG.16	20.65503	61.70079	0.00000	0.28757	-0.083333	0.0	0.0	0.0
23	20FG.16	20.72935	62.17893	0.00000	0.27915	-0.083333	0.0	0.0	0.0
23	20FG.16	20.80366	62.65707	0.00000	0.27052	-0.083333	0.0	0.0	0.0
23	20FG.16	20.87797	63.13521	0.00000	0.26172	-0.083333	0.0	0.0	0.0
23	20FG.16	20.95229	63.61336	0.00000	0.25281	-0.083333	0.0	0.0	0.0
23	20FG.16	21.02660	64.09150	0.00000	0.24381	-0.083333	0.0	0.0	0.0
24	17HW.A01	59.11222	56.40603	0.00000	0.44780	-0.083333	0.0	0.0	0.0
24	17HW.A01	59.64174	56.36426	0.00000	0.32180	-0.083333	0.0	0.0	0.0
24	17HW.A01	60.11227	56.32248	0.00000	0.29797	-0.083333	0.0	0.0	0.0
24	17HW.A01	60.58279	56.28071	0.00000	0.27592	-0.083333	0.0	0.0	0.0
24	17HW.A01	61.05331	56.23894	0.00000	0.25549	-0.083333	0.0	0.0	0.0
24	17HW.A01	61.52383	56.19717	0.00000	0.23656	-0.083333	0.0	0.0	0.0
24	17HW.A01	61.99436	56.15539	0.00000	0.21901	-0.083333	0.0	0.0	0.0
24	17HW.A01	62.46488	56.11362	0.00000	0.20272	-0.083333	0.0	0.0	0.0
24	17HW.A01	62.93540	56.07185	0.00000	0.18761	-0.083333	0.0	0.0	0.0
24	17HW.A01	63.40592	56.03008	0.00000	0.17359	-0.083333	0.0	0.0	0.0
24	17HW.A01	63.87644	55.98831	0.00000	0.16056	-0.083333	0.0	0.0	0.0
24	17HW.A01	64.34697	55.94653	0.00000	0.14846	-0.083333	0.0	0.0	0.0
24	17HW.A01	64.81749	55.90476	0.00000	0.13722	-0.083333	0.0	0.0	0.0
24	17HW.A01	65.28801	55.86299	0.00000	0.12677	-0.083333	0.0	0.0	0.0
24	17HW.A01	65.75853	55.82122	0.00000	0.11705	-0.083333	0.0	0.0	0.0
24	17HW.A01	66.22906	55.77944	0.00000	0.10802	-0.083333	0.0	0.0	0.0
24	17HW.A01	66.69958	55.73767	0.00000	0.09961	-0.083333	0.0	0.0	0.0
24	17HW.A01	67.17010	55.69590	0.00000	0.09179	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.17010	55.69590	0.00000	0.09179	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.15141	55.65413	0.00000	0.08356	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.13312	54.79889	0.00000	0.09525	-0.083333	0.0	0.0	0.0
25	17HW.A02	67.12363	54.35038	0.00000	0.09687	-0.083333	0.0	0.0	0.0





**A-SQUARED STUDIO  
ENGINEERS LTD**

**18A Froggnal Gardens  
Building GMA  
PDisp B02 - LT Loading**

Job No. Sheet No. Rev.

**1125**

Dr. Ref.

Made by Date Checked  
SB

Ref.	Name	x	y	z	δz	Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
		[m]	[m]	[mOD]	[mm]	[mOD]	[kN/m²]	[kN/m²]	[µ]
26	17HW.A03	63.72912	47.86619	0.00000	0.18987	-0.083333	0.0	0.0	0.0
26	17HW.A03	63.27738	47.90096	0.00000	0.20532	-0.083333	0.0	0.0	0.0
26	17HW.A03	62.82564	47.93573	0.00000	0.22201	-0.083333	0.0	0.0	0.0
26	17HW.A03	62.37390	47.97050	0.00000	0.24005	-0.083333	0.0	0.0	0.0
26	17HW.A03	61.92216	48.00527	0.00000	0.25955	-0.083333	0.0	0.0	0.0
26	17HW.A03	61.47042	48.04004	0.00000	0.28064	-0.083333	0.0	0.0	0.0
26	17HW.A03	61.01868	48.07481	0.00000	0.30348	-0.083333	0.0	0.0	0.0
26	17HW.A03	60.56694	48.10958	0.00000	0.32823	-0.083333	0.0	0.0	0.0
26	17HW.A03	60.11520	48.14435	0.00000	0.35506	-0.083333	0.0	0.0	0.0
26	17HW.A03	59.66346	48.17912	0.00000	0.38418	-0.083333	0.0	0.0	0.0
26	17HW.A03	59.21172	48.21389	0.00000	0.41580	-0.083333	0.0	0.0	0.0
26	17HW.A03	58.75998	48.24866	0.00000	0.45018	-0.083333	0.0	0.0	0.0
26	17HW.A03	58.30824	48.28343	0.00000	0.48759	-0.083333	0.0	0.0	0.0
26	17HW.A03	57.85650	48.31820	0.00000	0.52835	-0.083333	0.0	0.0	0.0
27	17HW.A04	57.85650	48.31820	0.00000	0.52835	-0.083333	0.0	0.0	0.0
27	17HW.A04	57.90340	48.76984	0.00000	0.52468	-0.083333	0.0	0.0	0.0
27	17HW.A04	57.95030	49.22149	0.00000	0.52028	-0.083333	0.0	0.0	0.0
27	17HW.A04	57.99720	49.67313	0.00000	0.51518	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.04410	50.12478	0.00000	0.50940	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.09100	50.57642	0.00000	0.50296	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.13790	51.02807	0.00000	0.49590	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.18480	51.47971	0.00000	0.48825	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.23170	51.93136	0.00000	0.48003	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.27860	52.38300	0.00000	0.47129	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.32550	52.83464	0.00000	0.46205	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.37240	53.28629	0.00000	0.45237	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.41930	53.73793	0.00000	0.44228	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.46620	54.18958	0.00000	0.43181	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.51310	54.64122	0.00000	0.42102	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.56000	55.09287	0.00000	0.40994	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.60690	55.54451	0.00000	0.39862	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.65380	55.99616	0.00000	0.38709	-0.083333	0.0	0.0	0.0
27	17HW.A04	58.70070	56.44780	0.00000	0.37541	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.67890	60.09730	0.00000	0.29836	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.72484	59.63727	0.00000	0.30646	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.77078	59.17725	0.00000	0.31432	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.81671	58.71722	0.00000	0.32191	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.86265	58.25720	0.00000	0.32920	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.90859	57.79717	0.00000	0.33616	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.95452	57.33715	0.00000	0.34275	-0.083333	0.0	0.0	0.0
28	17HW.B01	58.99946	56.87712	0.00000	0.34895	-0.083333	0.0	0.0	0.0
28	17HW.B01	59.04640	56.41710	0.00000	0.35473	-0.083333	0.0	0.0	0.0
29	17HW.B02	59.04640	56.41710	0.00000	0.35473	-0.083333	0.0	0.0	0.0
29	17HW.B02	59.47996	56.37762	0.00000	0.33044	-0.083333	0.0	0.0	0.0
29	17HW.B02	59.91352	56.33815	0.00000	0.30784	-0.083333	0.0	0.0	0.0
29	17HW.B02	60.34709	56.29868	0.00000	0.28679	-0.083333	0.0	0.0	0.0
29	17HW.B02	60.78065	56.25920	0.00000	0.26718	-0.083333	0.0	0.0	0.0
29	17HW.B02	61.21421	56.21972	0.00000	0.24891	-0.083333	0.0	0.0	0.0
29	17HW.B02	61.64777	56.18025	0.00000	0.23187	-0.083333	0.0	0.0	0.0
29	17HW.B02	62.08134	56.14078	0.00000	0.21597	-0.083333	0.0	0.0	0.0
29	17HW.B02	62.51490	56.10130	0.00000	0.20113	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.51490	56.10130	0.00000	0.20113	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.53797	56.55704	0.00000	0.19631	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.56105	57.01278	0.00000	0.19137	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.58413	57.46851	0.00000	0.18633	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.60720	57.92425	0.00000	0.18120	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.63027	58.37999	0.00000	0.17600	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.65335	58.83573	0.00000	0.17075	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.67643	59.29146	0.00000	0.16547	-0.083333	0.0	0.0	0.0
30	17HW.B03	62.69950	59.74720	0.00000	0.16016	-0.083333	0.0	0.0	0.0
31	17HW.B04	62.69950	59.74720	0.00000	0.16016	-0.083333	0.0	0.0	0.0
31	17HW.B04	62.29744	59.78221	0.00000	0.17062	-0.083333	0.0	0.0	0.0
31	17HW.B04	61.89538	59.81722	0.00000	0.18170	-0.083333	0.0	0.0	0.0
31	17HW.B04	61.49332	59.85223	0.00000	0.19346	-0.083333	0.0	0.0	0.0
31	17HW.B04	61.09126	59.88724	0.00000	0.20593	-0.083333	0.0	0.0	0.0
31	17HW.B04	60.68920	59.92225	0.00000	0.21915	-0.083333	0.0	0.0	0.0
31	17HW.B04	60.28714	59.95726	0.00000	0.23318	-0.083333	0.0	0.0	0.0
31	17HW.B04	59.88508	59.99227	0.00000	0.24806	-0.083333	0.0	0.0	0.0
31	17HW.B04	59.48302	60.02728	0.00000	0.26384	-0.083333	0.0	0.0	0.0
31	17HW.B04	59.08096	60.06229	0.00000	0.28059	-0.083333	0.0	0.0	0.0
31	17HW.B04	58.67890	60.09730	0.00000	0.29836	-0.083333	0.0	0.0	0.0

**Results : Consolidation : Displacement Data : Lines**

None

**Results : Total : Displacement Data : Lines**

None