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FLOOD RISK ASSESSMENT AND DRAINAGE STATEMENT

Scheme name:

LAND ADJACENT TO 39 PRIORY TERRACE, LONDON, NW6 4DG

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Foreword

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Some of the information presented within this report is based on third party information which is believed to be correct; no liability will be accepted for any discrepancies in accuracy, mistakes or omissions in such information. The report also assesses the flood risk in relation to the requirements of the Environment Agency and as such assesses the site for a specific flood event and not all flood events. The contents of this document must not be copied or reproduced in whole or in part without the written consent of Infrastruct CS Ltd.



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1.0 Summary

A Flood Risk Assessment (FRA) and drainage strategy has been undertaken to accompany the planning application for the proposed redevelopment at 39 Priory Terrace, Camden, London. This report has been prepared by Infrastruct CS Ltd on behalf of the Client in accordance with the guidelines set out in the National Planning Policy Framework.

The following table is an overview of the flood risk and drainage strategy for the proposed development of the site, based upon currently available information and finds the following –

ITEM	RESPONSE
Site Location	The site is in vacant land, at the junction of Priory Terrace with Abbey Road, London, NW6 4DG, approximately 800m south of West Hampstead Station and 300m east of Kilburn High Road. The approximate grid reference 525685E, 183965N
Size and Current Land Usage	The current site is approximately 121m2 in plan and currently vacant.
Flood Zone	The development site falls entirely within Flood Zone 1, which is classified as low probability of flooding.
Fluvial Flood Risk	Low – Refer to Section 6.1
Overland Flood Risk	Low – Refer to Section 6.2
Groundwater Flood Risk	Medium – Refer to Section 6.3
Sewerage Flood Risk	Low – Refer to Section 6.4
Artificial Flood Risk	Low – Refer to Section 6.5
Proposed Development	The architectural proposals are for the construction of a new 3- storey building including a basement, with a total Gross Internal Area of 143m2.
SuDS Features proposed for this scheme	The proposed SuDS features for this site include an attenuation tank and a flow control device to reduce the runoff flows to maximum of 2.0 l/s. A green roof will cover approximately 25% of the total roof area.

Based on this assessment, it is concluded that in accordance with the Flood risk vulnerability and flood zone compatibility table in Section 5.6 from the Planning Practice Guidance document, the report considers the proposed development appropriate.



2.0 Introduction

2.1 Commission

Old West Hampstead Estates Ltd have commissioned Infrastruct CS Ltd, to prepare a Flood Risk Assessment (FRA) and drainage statement to support a planning application for the re-development at a land next to 39 Priory Terrace, NW6 4DG. The proposed planning layout drawings are contained in Appendix A.

2.2 Guidance

This flood risk assessment has been compiled in accordance with the recommendations of the National Planning Policy Framework (NPPF) and the Planning Practice Guidance (PPG).

2.3 Aims and Objectives

The purpose of this flood risk assessment is to assess the potential flood risks by and to the proposed development. It will identify the flood risk zone, potential sources of flood risk, consider the proposed drainage and will be used to support the proposed planning application.



3.0 Site Details

3.1 Location

The site is in vacant land, at the junction of Priory Terrace with Abbey Road, London, NW6 4DG, approximately 800m south of West Hampstead Station and 300m east of Kilburn High Road.

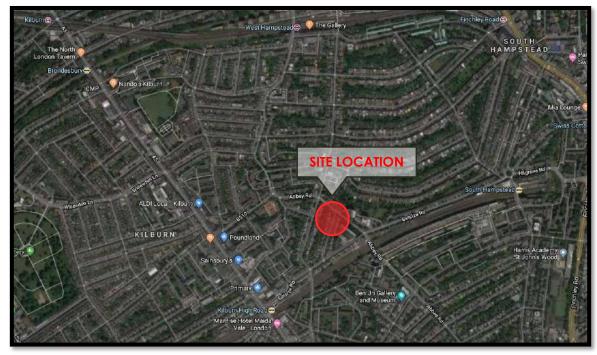


Figure 3.1.1 - Site Context



Figure 3.1.2 - Site location



3.2 Grid Reference

The Ordnance Survey National grid reference for the centre of the site is:

525685E, 183965N (Nat Grid TQ 25685 83965)

3.3 Topography and Site Description

The site covers an approximate brownfield area of 121m².

Levels are consistent along the site boundary, approximately between 38.82mADO and 38.99mAOD. Levels on the road are approximately 150mm lower, reducing even further towards the southeast. These levels at the rim of the survey are around 38.35m. See Appendix F for full document.

3.4 Ground Conditions

Reference to the Geological survey of Great Britain indicates the following strata:

Superficial deposits: N/A

Bedrock geology: London Clay Formation - Clay, Silt And Sand. Sedimentary Bedrock formed approximately 48 to 56 million years ago in the Palaeogene Period. Local environment previously dominated by deep seas. These sedimentary rocks are marine in origin. They are detrital and comprise coarse- to fine-grained slurries of debris from the continental shelf flowing into a deep-sea environment, forming distinctively graded beds.

Intrusive site investigations carried out adjacent/near the development and shown on the British Geological Survey database (BGS ID: TQ28SE380) confirmed the above mentioned.

3.5 Ground Water

Boreholes carried out in the vicinity of the site and shown in the BGS online maps, found no ground water within the trial pits at 15mbgl. In-situ testing is required to confirm the depth of groundwater.

A review of the maps within the Camden SFRA indicate that the site is at a low risk flooding.

3.6 Existing Site Drainage

The Thames Water wastewater plans show combined sewers in the vicinity of the site. There is a 1245x813mm sewer in Abbey Road, to the north and a Ø225mm sewer to the east, along Priory Terrace. The head of this latter network will be used, connecting the new system into manhole 6902. See Appendix B for Thames Water sewer records.



3.7 Existing Watercourses

The nearest main river watercourse to the site is the River Brent, a tributary of the River Thames, which is located 5.2 km to the northwest of the site. River Thames itself is 6Km to the southeast.

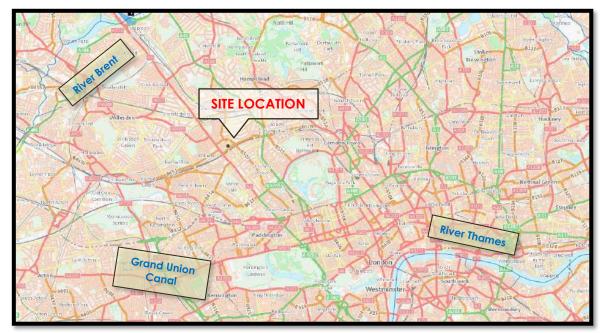


Figure 3.7.1 – Local Rivers

3.8 Environment Agency Groundwater and Aquifer Protection

Reference to the Environment Agency Groundwater protection zone map shows the area is sited outside all groundwater protection zone. The Environment Agency have defined Source Protection Zones (SPZs) for groundwater sources such as wells, boreholes, and springs used for public drinking water supply. These zones show the risk of contamination from any activities that might cause pollution in the area. The closer the activity, the greater the risk.

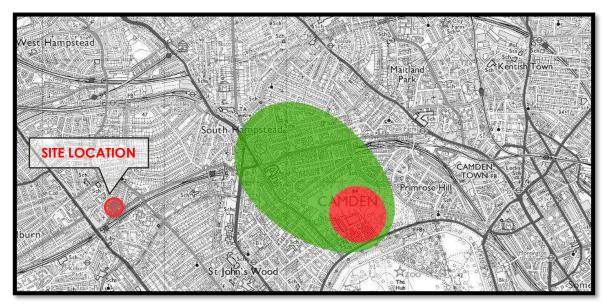


Figure 3.8.1 – Groundwater Protection Zones



The Environment Agency use the zones to set up pollution prevention measures in areas which are at a higher risk, and to monitor the activities of potential polluters nearby.

A study of the aquifer maps on the Environment Agency website revealed the site to be located outside any superficial or bedrock aquifer.

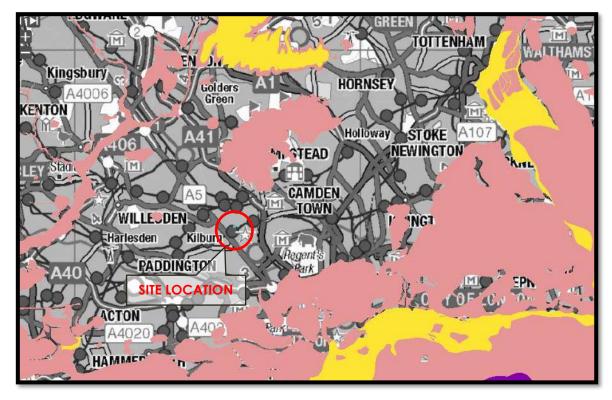


Figure 3.8.2 – Aquifer map from the Natural England MAGIC website.

4.0 Proposed Development

The proposals involve the construction of a 3-storey building including a basement, with a total Gross Internal Area of 143m2. The proposed development plans can be found in Appendix A.



5.0 Flood Risk Policy

5.1 Environment Agency Flood Map

The flood map for the development site shown below suggests that the site wholly falls within flood zone 1, which is defined as land assessed as having a less than 1 in 1000 annual probability of river flooding in any one year.

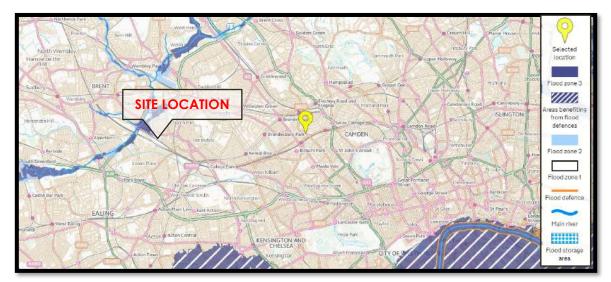


Figure 5.1 - Environment Agency Flood Zone map

5.2 The National Planning Policy Framework

The National Planning Policy Framework (NPPF) and the accompanying Planning Practice Guidance (PPG) gives direction for development with respect to flooding. These documents promote a sequential approach to encourage development away from areas that may be or are susceptible to flooding. In doing so it categorizes flood zones in the context of their probability of flooding, as shown in the table within Section 5.3 below.

5.3 Flood Zone Definition

The National Planning Policy Framework Definition of Flood Zones

Flood zone	Fluvial	Tidal	Probability of flooding
1	< 1 in 1000 year	<1 in 1000 year	Low probability
2	Between < 1 in 1000 year and 1 in 100 year	Between <1 in 1000 year and 1 in 200 year	Medium Probability
3a	> 1 in 100 year	> 1 in 200 year	High probability
3b	Either > 1 in 20 or as agreed between the EA and the LPA	Either > 1 in 20 or as agreed between the EA and the LPA	Functional flood plain



5.4 Flood Zones – Table 1 – Planning Practice Guidance

(Note: These Flood Zones refer to the probability of river and sea flooding, ignoring the presence of defences)

Zone 1 - Low Probability

Definition

This zone comprises land assessed as having a less than 1 in 1000 annual probability of river or sea flooding in any year (<0.1%).

Appropriate uses

All uses of land are appropriate in this zone.

FRA requirements

For development proposals on sites comprising one hectare or above the vulnerability to flooding from other sources as well as from river and sea flooding, and the potential to increase flood risk elsewhere through the addition of hard surfaces and the effect of the development on surface water run-off, should be incorporated in a FRA. This need only be brief unless the factors above or other local considerations require particular attention. See Annex E for minimum requirements.

Policy aims

In this zone, developers and local authorities should seek opportunities to reduce the overall level of flood risk in the area and beyond through the layout and form of the development, and the appropriate application of sustainable drainage techniques.

5.5 Flood Risk Vulnerability Classification - Extract from Table 2 - Planning Practice Guidance (PPG)

More Vulnerable

- Hospitals.
- Residential institutions such as residential care homes, children's homes, social services homes, prisons and hostels.
- Buildings used for: dwelling houses; student halls of residence; drinking establishments; nightclubs; and hotels.
- Non-residential uses for health services, nurseries, and educational establishments.
- Landfill and sites used for waste management facilities for hazardous waste.
- Sites used for holiday or short-let caravans and camping, subject to a specific warning and evacuation plan.



Vulnerability classification flood zone	Essential infrastructure	Water compatible	Highly vulnerable	More vulnerable	Less vulnerable
1	\checkmark	\checkmark	\checkmark	\checkmark	\checkmark
2	\checkmark	\checkmark	Exception test required	\checkmark	\checkmark
3α	Exception test required	\checkmark	X	Exception test required	\checkmark
3Ь	Exception test required	\checkmark	X	Х	x

5.6 Flood Risk Vulnerability & Flood Zone Compatibility Table

 $\sqrt{\text{Development is appropriate x development is not appropriate}}$

The above table, taken from PPG (table 3), confirms that residential properties within flood zones 1 is appropriate development.

5.7 Other Flooding Mechanisms

In addition to the potential for assessing flooding from fluvial and tidal sources NPPF also requires that consideration is given to other mechanisms for flooding:

- Flooding from land intense rainfall, often in short duration, that is unable to soak into the ground or enter drainage systems, can run rapidly off land and result in local flooding.
- Flooding from groundwater occurs when water levels in the ground rise above the surface elevations.
- Flooding from sewers In urban areas, rainwater is frequently drained into surface water sewers or sewers containing both surface and waste water sewers known as combined sewers. Flooding can result causing surcharging when the sewer is overwhelmed by heavy rainfall.
- Flooding from reservoirs, canals and other artificial sources Non-natural or artificial sources of flooding can result from sources such as reservoirs, canals lakes etc, where water is held above natural ground levels.



5.8 Local Strategic Flood Risk Assessment SFRA and Local Policy

London Plan:

<u>Policy 5.11</u>- Green Roofs and Development Site Environs: Major development proposals should be designed to include roof, wall and site planting, especially green roofs and walls where feasible, to deliver as many of the following objectives as possible:

- 1. adaptation to climate change (i.e. Aiding cooling)
- 2. sustainable urban drainage
- 3. mitigation of climate change (i.e. Aiding energy efficiency)
- 4. enhancement of biodiversity
- 5. accessible roof space
- 6. improvements to appearance and resilience of the building
- 7. Growing food.

<u>Policy 5.12</u> - Flood Risk Management: The Mayor will work with all relevant agencies including the Environment Agency to address current and future flood issues and minimise risks in a sustainable and cost effective way.

Development proposals must comply with the flood risk assessment and management requirements set out in the NPPF and the associated technical Guidance on flood risk1 over the lifetime of the development and have regard to measures proposed in Thames Estuary 2100 (TE2100 – see paragraph 5.55) and Catchment Flood Management Plans.

Developments which are required to pass the Exceptions Test set out in the NPPF and the Technical Guidance will need to address flood resilient design and emergency planning by demonstrating that:

- The development will remain safe and operational under flood conditions

- A strategy of either safe evacuation and/or safely remaining in the building is followed under flood conditions

- Key services including electricity, water etc will continue to be provided under flood conditions

- Buildings are designed for quick recovery following a flood.

Development adjacent to flood defences will be required to protect the integrity of existing flood defences and wherever possible should aim to be set back from the banks of watercourses and those defences to allow their management, maintenance and upgrading to be undertaken in a sustainable and cost effective way.

In line with the NPPF and the Technical Guidance, boroughs should, when preparing LDFs, utilise Strategic Flood Risk Assessments to identify areas where particular flood risk issues exist and develop actions and policy approaches aimed at reducing these risks, particularly through redevelopment of sites at risk of flooding and identifying specific opportunities for flood risk management measures.

<u>Policy 5.13</u> - Sustainable Drainage: It is a key policy with regards to flood risk and water resource management. The policy provides the drainage hierarchy to ensure that reasonable measures are taken to sustainably manage and reduce the overall amount of rainfall being discharged from a development site. Developers should take measures to ensure that surface water management features higher up the drainage hierarchy are incorporated.



The current London Plan drainage hierarchy is as follows:

- 1. Store rainwater for later use
- 2. Use infiltration techniques, such as porous surfaces in non-clay areas
- 3. Attenuate rainwater in ponds or open water features for gradual release
- 4. Attenuate rainwater by storing in tanks or sealed water features for gradual release
- 5. Discharge rainwater direct to a watercourse
- 6. Discharge rainwater to a surface water sewer/drain7.Discharge rainwater to the combined sewer

Drainage should be designed and implemented in ways that deliver other policy objectives of this Plan, including water use efficiency and quality, biodiversity, amenity and recreation.

Developers should aim to achieve greenfield runoff rates via their proposed SuDS measures and ensure that surface water runoff is managed as close to the source as possible. The proposed measures should be incorporated in line with the Non-statutory technical standards for sustainable drainage systems, prepared by DEFRA in 2015

LB Camden - Local Plan

<u>Policy CC2: Adapting to Climate Change:</u> The Council will require development to be resilient to climate change. All development should adopt appropriate climate change adaptation measures such as:

the protection of existing green spaces and promoting new appropriate green infrastructure;

- 1. not increasing, and wherever possible reducing, surface water runoff through increasing permeable surfaces and use of Sustainable Drainage Systems
- 2. incorporating bio-diverse roofs, combination green and blue roofs and green walls where appropriate
- 3. measures to reduce the impact of urban and dwelling overheating, including application of the cooling hierarchy.

Any development involving 5 or more residential units or 500 sqm or more of any additional floorspace is required to demonstrate the above in a Sustainability Statement.

<u>Policy CC3: Water and Flooding:</u> The Council will seek to ensure that development does not increase flood risk and reduces the risk of flooding where possible. We will require development to:

- 1. incorporate water efficiency measures
- 2. avoid harm to the water environment and improve water quality
- 3. consider the impact of development in areas at risk of flooding (including drainage)
- 4. incorporate flood resilient measures in areas prone to flooding
- 5. utilise Sustainable Drainage Systems (SuDS) in line with the drainage hierarchy to achieve a greenfield run-off rate where feasible
- 6. not locate vulnerable development in flood-prone areas.

Where an assessment of flood risk is required, developments should consider surface water flooding in detail and groundwater flooding where applicable. The Council will protect the borough's existing drinking water and foul water infrastructure, including the reservoirs at Barrow Hill, Hampstead Heath, Highgate and Kidderpore.



Policy A5 Basements

The Council will only permit basement development where it is demonstrated to its satisfaction that the proposal would not cause harm to:

- a. neighbouring properties;
- b. the structural, ground, or water conditions of the area;
- c. the character and amenity of the area;
- d. the architectural character of the building; and
- e. the significance of heritage assets.

In determining proposals for basements and other underground development, the Council will require an assessment of the scheme's impact on drainage, flooding, groundwater conditions and structural stability in the form of a Basement Impact Assessment and where appropriate, a Basement Construction Plan.

The siting, location, scale and design of basements must have minimal impact on, and be subordinate to, the host building and property. Basement development should:

- f. not comprise of more than one storey;
- g. not be built under an existing basement;
- h. not exceed 50% of each garden within the property;
- be less than 1.5 times the footprint of the host building in area;
- j. extend into the garden no further than 50% of the depth of the host
- building measured from the principal rear elevation;
- k. not extend into or underneath the garden further than 50% of the depth
- of the garden;
- I. be set back from neighbouring property boundaries where it extends
- beyond the footprint of the host building; and
- m. avoid the loss of garden space or trees of townscape or amenity value.

Exceptions to f. to k. above may be made on large comprehensively planned

sites.

The Council will require applicants to demonstrate that proposals for basements:

- n. do not harm neighbouring properties, including requiring the provision of a Basement Impact Assessment which shows that the scheme poses a risk of damage to neighbouring properties no higher than Burland Scale 1 'very slight';
- o. avoid adversely affecting drainage and run-off or causing other damage
- to the water environment;
- p. avoid cumulative impacts;
- q. do not harm the amenity of neighbours;
- r. provide satisfactory landscaping, including adequate soil depth;
- s. do not harm the appearance or setting of the property or the established
- character of the surrounding area;
- t. protect important archaeological remains; and
- u. do not prejudice the ability of the garden to support trees where they are
- part of the character of the area.

The Council will not permit basement schemes which include habitable rooms and other sensitive uses in areas prone to flooding. We will generally require a Construction Management Plan for basement developments.

Given the complex nature of basement development, the Council encourages developers to offer security for expenses for basement development to adjoining neighbours.



Camden Practise Guidance – Water and Flooding (2019)

Flooding: WHAT DOES THE COUNCIL EXPECT?

- Developments must not increase the risk of flooding, and are required to put in place mitigation measures where there is known to be a risk of flooding (Local Plan policies CC2 and CC3).
- Major developments will be required to constrain runoff volumes for a 1 in 100 year, 6 hour rainfall event, where feasible.
- All sites in Camden of one hectare or more require a Flood Risk Assessment in line with the National Planning Policy Framework
- A drainage report is required for all major applications, basement development, and vulnerable development in areas identified as at risk of flooding (details of what this should include can be found in paragraph 8.67 of the Local Plan). The Council will expect plans and application documents to describe how water will be managed within the development, including an explanation of the proposed SuDS, the reasons why certain SuDS have been ruled out and detailed information on materials and landscaping
- The Council will expect developments to achieve a greenfield surface water unoff rate where feasible once SuDS have been installed.



6.0 Flood Risk to The Development

6.1 Flooding from Fluvial Sources

The proposed development site lies entirely within flood zone 1 which is classified as land assessed as having a less than 1 in 1000 annual probability of river or sea flooding and is appropriate to all uses of land.

It is, therefore, the consideration of this FRA that the site has a low risk of flooding from fluvial sources.

6.2 Flooding from Overland Flows

The risk of flooding due to overland flood flows is considered low by the Environment Agency. The surface water flood data for the site, shown below, indicates that there is medium flood risk immediately to the north of the site, near the garages and along Abbey Road, but very low risk within the site itself. There is currently a wall protection the site from water runoff which will be improved. Surrounding levels fall away from the house and into the road, as explained in section 3.3.

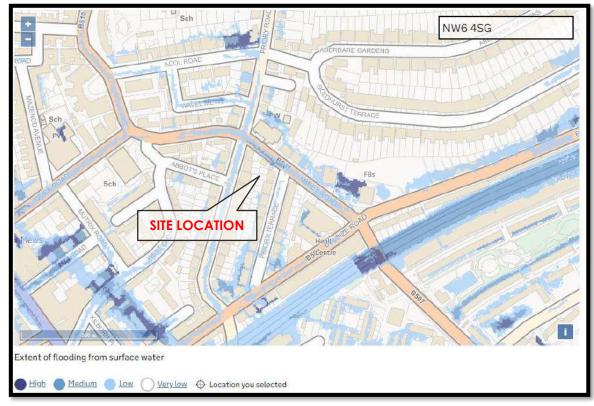


Fig 6.2 – Environment Agency Flood Risk from Surface Water map

It is, therefore, the consideration of this FRA that the site has a low risk of flooding from overland flow.



6.3 Flooding from Rising Groundwater

Groundwater flooding occurs because of the underground water table rising, which can result in water emerging through the ground and causing flooding in extreme circumstances. This source of flooding tends to occur after extensive periods of heavy rainfall. Groundwater flooding can occur in areas where the underlying soil and bedrock can become saturated with water. Therefore, ground composition and aquifer vulnerability are significant influences on the potential rate of groundwater flooding.

A majority of the sub-region is underlain by Thames Group (also referred to as London Clay) bedrock, a composition of silty clay/mudstone, sandy silts and sandy clayey silts of marine origin. This geological unit generally has a <u>low</u> hydraulic conductivity which means water does not easily move through it.

The proposals include a basement and therefore the potential for the water table to raise above the basement level is higher. Since the water table level is unknown, they must be confirmed via groundwater monitoring over a period of time, ideally in winter.

The site is shown outside the "Increased Susceptibility to Elevated Groundwater" area but nearby a location where a groundwater flood incident occurred in the past, identified by the Environment Agency. See map in Appendix E.

It is, therefore, the consideration of this FRA that the site has a medium risk of flooding from rising groundwater levels.

6.4 Flooding from the Local Sewerage Network

Sewer flooding can occur due to sewer infrastructure failure or due to an increased flow and volume of water entering a sewer system which exceeds its hydraulic capacity, causing the system to surcharge. If sewer outfall points are either blocked or submerged due to high water levels, water can back up in a sewer system and cause flooding. These issues can result in water overflowing from gullies and manholes, causing flooding in the local area. Blockages caused by sediment or debris can further exacerbate the probability of sewer flooding.

Drainage in the sub-region is serviced by Thames Water Utilities who provide surface water, foul and combined sewer systems. Modern sewer systems are designed to be separate surface water and foul water systems, typically accommodating up to 1 in 30-year rainfall events. However, sewer system segments across London vary in capacity due to age. Older segments have a smaller capacity and may not be designed to accommodate rainfall events as significant as 1 in 30-year events.

The Thames Water historical sewer flooding dataset provides details on the number of reported sewer flood incidents within a four-digit postcode area. Information on historical sewer flooding is shown in the SFRA indicates no flooding from sewers in the vicinity of the site. Moreover, the site is protected to overland flows with the existing wall, to be retained.

It is, therefore, the consideration of this FRA that the site has a low risk of flooding by surcharging of the local sewer network.



6.5 Flooding from Reservoirs, Canals & Other Artificial Sources

Reservoirs in the UK have an extremely good safety record. The EA is the enforcement authority for the Reservoirs Act 1975 in England and Wales. All large reservoirs must be inspected and supervised by reservoir panel engineers. It is assumed that these reservoirs are regularly inspected and essential safety work is carried out. These reservoirs therefore present a minimal risk.

Flooding may result from the failure of engineering installations including flood defence, land drainage pumps, sluice gates and floodgates. Hard defences may fail through the slow deterioration of structural components such as the rusting of sheet piling, erosion of concrete reinforcement and toe protection or the failure of ground anchors. This deterioration can be difficult to detect, so that failure when it occurs is often sudden and unexpected. Failure is more likely when the structure is under maximum stress, such as extreme fluvial events when pressures on the structure are at its most extreme.

There are no known reservoirs, canals or other artificial sources in the vicinity of the site.

It is, therefore, the consideration of this FRA that the site has a low risk of flooding by reservoirs, canals or other artificial sources.



7.0 Flood Risk As A Result Of The Development

7.1 Effect of The Development Generally

Development by its nature usually has the potential to increase the impermeable area with a resultant increased risk of causing rapid surface water runoff to watercourses and sewers, thereby causing surcharging and potential flooding. There is also the potential for pollutants to be mobilised and consequently flushed into the receiving surface water system.

Increases in both the peak runoff rate (usually measured in litres per second I/s) and runoff volume (cubic metres m³) can result.

7.2 Surface Water Drainage & Sustainable Drainage Systems

Sustainable Drainage techniques (SuDS) covers a range of approaches to manage surface water runoff so that-

'Surface water arising from a developed site should, as far as is practicable, be managed in a sustainable manner to mimic the surface water flows arising from the site prior to the proposed development, while reducing the flood risk to the site itself and elsewhere, taking climate change into account. This should be demonstrated as part of the flood risk assessment.'

7.3 Peak Storm Design Criteria

The proposed sustainable drainage techniques for the development should accommodate the peak rainfall event for a 1 in 100 year storm event with an additional allowance for climate change. Table 5 of NPPG recommends for developments that have a life expectancy beyond 2085 that an additional factor of 40% is applied to the peak volume of runoff.

7.4 Existing Surface Water Runoff Rates

The development site area is approximately 121m2. The site is currently vacant with no visible means of drainage. The existing runoff rates calculated for site are highlighted below:

Return Period	Greenfield Runoff Rate I/s
1 in 1 year	0.1
Qbar	0.1
1 in 30 year	0.2
1 in 100 year	0.2

Table 7.4 Existing Runoff rates

Greenfield runoff rates were calculated using the FSR Method within Microdrainage Software. Calculations can be found in Appendix D.



7.5 Infiltration Testing

It has been assumed, based on local geology information found on the British Geological Survey database, that infiltration is not feasible in this area. Moreover, there is no room for infiltration devices such as soakaways.

7.6 Sustainable Drainage Hierarchy

A hierarchical approach has been undertaken in consideration of the application of SuDS in relation to the development. This is in order to meet the design philosophy of ensuring that surface water run-off is managed as close to its source as possible and the existing situation is replicated as closely as possible.

The following drainage hierarchy has been undertaken with reference to the procedures set out in the SuDS Manual (CIRIA C753, 2015) to assess the viability of the application of SuDS techniques to this scheme:

- Store rainwater for later use: Storing rainwater for later use in water butts is recommended but it is not enough to accommodate the runoff volume from the whole development. After a period of continuous rain, these tanks can be full and therefore its efficacy reduced considerably.
- <u>Use infiltration techniques, such as porous surfaces in permeable strata areas:</u> Soakaways cannot be used due to the lack of space.
- <u>Attenuate rainwater in ponds or open water features for gradual release to a</u> <u>watercourse.</u> There are no watercourses in the vicinity of this site.
- <u>Attenuate rainwater by storing in tanks or sealed water features for gradual release</u> to a watercourse. Not feasible because there are no watercourses in the close vicinity.
- <u>Attenuate rainwater by storing in tanks or sealed water features for gradual release</u> to a surface water sewer. There are no surface water sewers in the vicinity.
- **Discharge rainwater to the combined sewer.** Foul and surface water from the new house will be discharged into the main combined sewer in Priory Terrace.

The sustainable drainage hierarchy shown above is intended to ensure that all practical and reasonable measures are taken to manage surface water higher up the hierarchy (1 being the highest) and that the amount of surface water managed at the bottom of the hierarchy is minimised.

Storing rainwater for later use might be an option but it is not sufficient to accommodate the runoff from the whole development.

The site-specific drainage hierarchy checklist considered for the drainage design for this development is detailed in Table 7.6.



SUDS OPTIONS	Comments	Potential for flow	Volume reduction	Maintenance requirement	Space requirement	Cost	Included in final detailed design
Rainwater	Rainwater from roof runoff	L	М	Н	L	Н	Ν
harvesting	collected for re-use. Cost-benefit considerations						
Water butts	Rainwater collection from roof runoff. Included in final design	L	L	L	L	L	Pos
Living roofs	Vegetated roofs that reduce runoff volume and rate	Μ	L	М	L	Η	Y
Bio-retention	Shallow vegetated areas to retain and treat runoff.	L	L	М	Μ	L	Ν
Constructed	Waterlogged areas that can	М	L	Н	H/M	М	Ν
wetlands	supportaquaticvegetation.Replicates existing conditions andprovides ecological benefit.						
Swales	Shallowgrasseddrainagechannels.Replicatesexistingconditions	Η	Μ	L	M/H	L	Ν
Soakaways	Subsurface structures that dispose of water via infiltration.	Н	Η	L	L	Μ	Ν
Permeable	Surface that infiltrate through	Н	Н	М	L	М	Ν
pavements	surface. Retains pollutants.						
Tanked	Oversized pipes or cellular	Н	L	L	Μ	M/H	Y
storage	storage.						
systems							
Infiltration	Depressions in the ground to store	Н	Н	H/M	Н	M/L	N
basins	and release water through infiltration						
Detention	Temporary retention of runoff with	Н	L	М	Н	M/L	Ν
basins	controlled discharge						

Table 7.6 Drainage design hierarchy (SuDS techniques considered for use in this scheme)

It should be noted that where the SuDS techniques are noted as feasible or possible it does not necessarily follow that they will all be used. Reference should be made to the drainage strategy drawing in Appendix C which indicates the drainage proposals.



7.7 SUDS Techniques Employed

Runoff from the roof will be collected and conveyed via a pipe network into cellular attenuation tank, from where it will be discharged into the combined sewer at a limited flow rate of 21/s. The flow control device can be an orifice plate of Ø34mm diameter or a vortex system. A weir wall is recommended so water can leave the site in case of a blockage.

Runoff from the basement patio will be pumped to ground level. Potential sediments will be trapped using catchpits. Urban creep has not been considered as there is little room for extensions.

Approximately 25% of the total will be green roof, which will help to attenuate and also reduce the runoff. Since the sewer is combined, a non-return valve will be installed before the demarcation chamber to prevent backflows in case the system surcharges.

Return Period	Existing Runoff Rate I/s	Proposed Runoff Rate I/s
1 in 1 year	0.1	2.0
Qbar	0.1	2.0
1 in 30 year	0.2	2.0
1 in 100 year	0.2	2.0

Calculations for the attenuation device can be found in Appendix D.

Table 7.7.A Existing and proposed runoff rates

7.8 Residual Flood Risk & Exceedance

The proposed surface water drainage measures will however be designed to contain the peak storm event that can be expected for a 1 in 100 year situation. A 40% allowance has already been applied to the site to account for future climate change.

7.9 Dry Means of Escape

For basement development it is necessary to provide safe access and egress during a flood. A safe access or exit route must be appropriate for use by occupiers to escape flooding without the intervention of the emergency services.

Based on the Environment Agency flood maps, the main entrance to the building is in Flood Zone 1. Therefore, a safe access/egress will be available through the internal stairs.

8.0 Proposed Foul Water Drainage System

The development proposals will seek to discharge foul water from the development site into the existing combined drainage network running along Priory Terrace, to the east of the property. This will be subject to a Section 106 consents from Local Water Authority, Thames Water. Flows into this system will be via a gravity fed connection.

A pre-development enquiry has been made to Thames Water although at the time of writing no response has been received. No capacity issues are envisaged as it is the head of the line.



9.0 Recommendations and Conclusion

The development proposals together with the site layout have been assessed in relation to the provision of SuDS drainage associated with the works.

The report has assessed the feasibility of implementing the SuDS hierarchal approach and has confirmed that this development is likely to be able to install suitable drainage measures into the design proposals.

Therefore, in line with the recommendations of the National Planning Policy Framework, the development site lies within land classified as Flood Zone 1, which is considered at a low risk of flooding, and therefore appropriate for a development of this nature. Having assessed the other forms of flood risk to and from the development site, this report finds that the site is not considered at high risk from any other sources of flooding. The site is also in line with the Camden Local Plan Policy A5 – Basements, as shown in section 5.8.

9.1 Flood Resistant measures

Provided that the drainage system is appropriately maintained, the risk of flooding from overland flows is low. However, as part of the works associated with the new development it is the recommendation of the report that consideration should be given to flood resistant measures, in particular at the basement level. These are mechanisms which can be implemented by the occupier to provide additional defences against flood water ingress should the drainage system fails. More information can be gained from the CIRIA document 'Improving the flood performance of new buildings'.

9.2 Flood Resilient measures

It is also the recommendation of the report that flood resilient measures are used within the design to minimize the impact an extreme flood event would have on the property. As these works are associated with the construction of the residential dwelling it would mainly involve the sighting of sockets and fuse boxes away from floor level. More information can be gained from the CIRIA document 'Improving the flood performance of new buildings'.

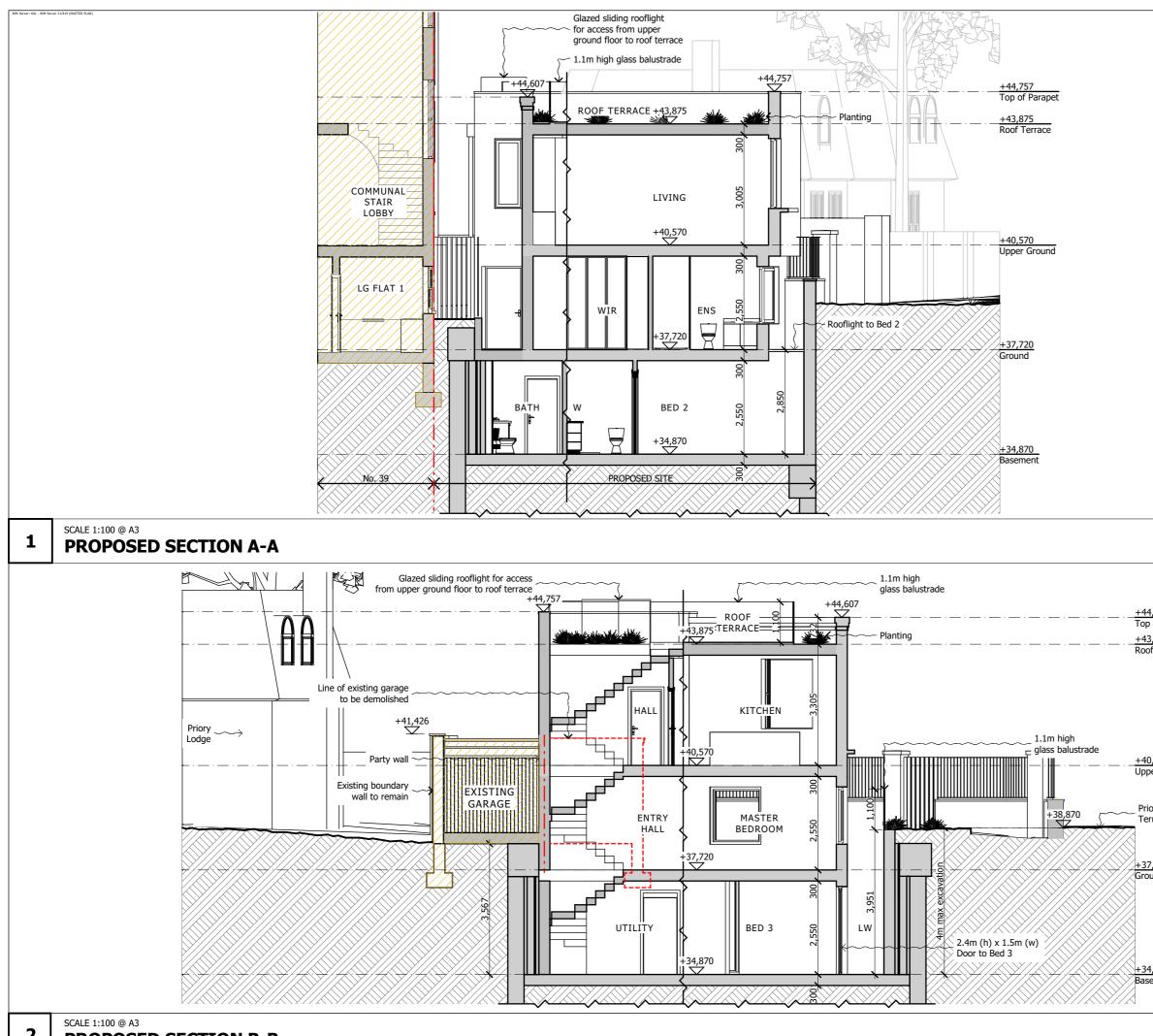


10.0 References & Bibliography

- The National Planning Policy Framework July 2018
- Planning Practice Guidance.
- Environment Agency Rainfall-Runoff Management for Developments
- Environment Agency indicative flood maps https://flood-map-forplanning.service.gov.uk/
- Environment Agency indicative groundwater source protection zone maps http://www.natureonthemap.naturalengland.org.uk/MagicMap.aspx
- Environment Agency indicative Aquifer designation maps
 http://www.natureonthemap.naturalengland.org.uk/MagicMap.aspx
- CIRIA 2007, The Sustainable Drainage Systems (SUDS) Manual C753
- Sewers for adoption 7th edition
- DEFRA Non-statutory technical standards for sustainable drainage
- The London Plan sustainable design and Construction Supplementary Planning Guidance
- Preliminary FRA for London Borough of Camden 2011 by Halcrow
- London Borough of Camden SFRA 2014 by URS
- Managing Flood Risk in Camden 2013 by Camden Council
- Camden Planning Guidance Basements 2018
- Camden Planning Guidance Water and Flooding 2019
- Camden Local Plan 2017
- Flood Estimation Handbook
- Environment Agency Adapting to Climate Change: Advice for the Flood and Coastal Erosion Management Authorities March 2016

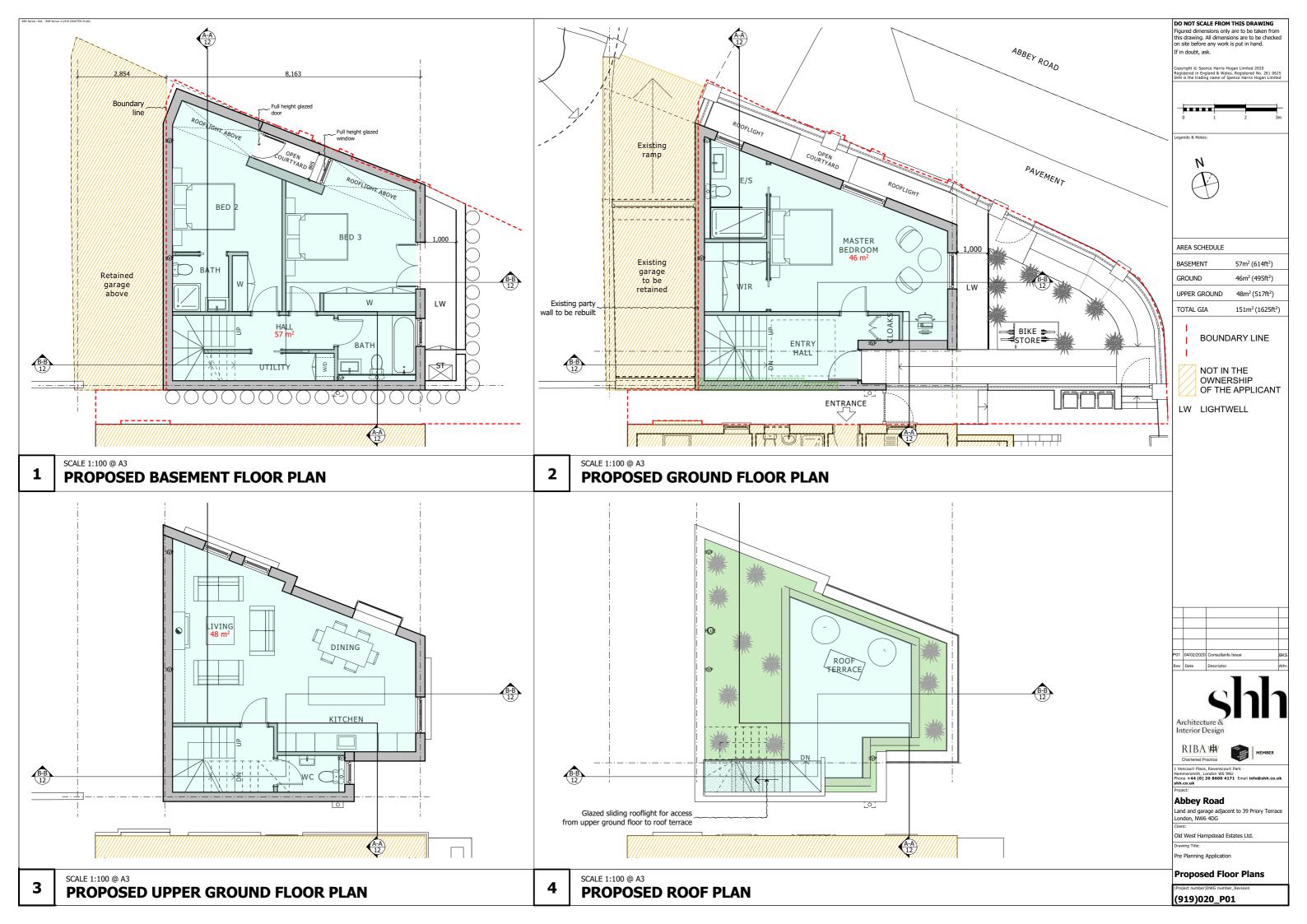


Appendix A - Development Proposals

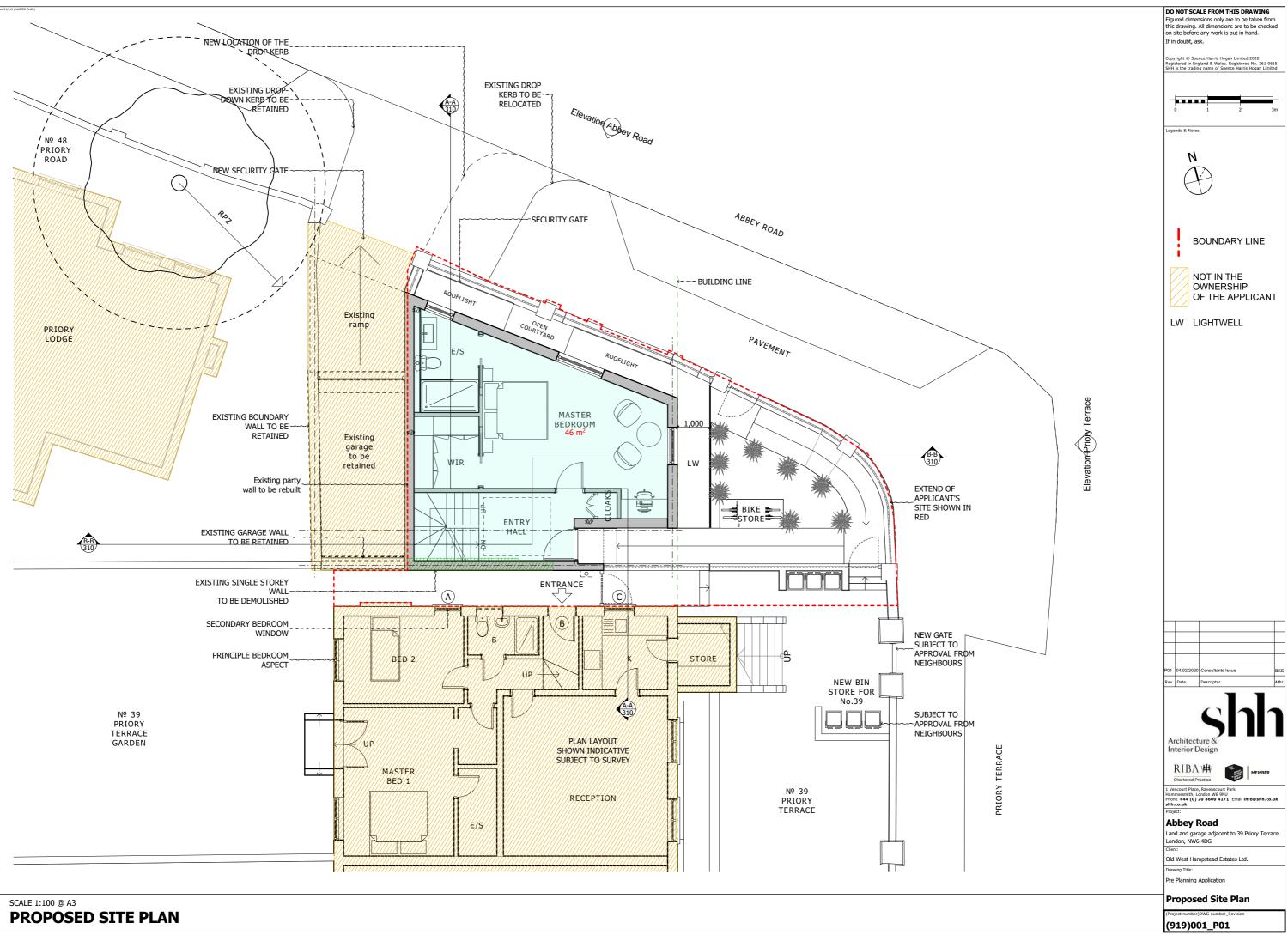


PROPOSED SECTION B-B

	DO NOT SCALE FROM THIS DRAWING Figured dimensions only are to be taken from this drawing. All dimensions are to be checked on site before any work is put in hand. If in doubt, ask. Copyright © Spence Harris Hogan Limited 2020 Registered in England & Wales. Registered No. 261 0615 SHH is the trading name of Spence Harris Hogan Limited
	Legends & Notes: BOUNDARY LINE NOT IN THE OWNERSHIP OF THE APPLICANT LW LIGHTWELL
4,607 o of Parapet 3,875 of Terrace	
0,570 Der Ground	P01 04/02/2020 Consultants Issue BKS Rev Date Descriptor Athr.
ory rrace	Architecture & Interior Design
7,720 und	RIBA W Image: Characterized Practice I Vencourt Place, Ravenscourt Park Hammersmith, London WG 9NU Phone +44 (0) Second 121 Email info@shh.co.uk Project: Abbey Road Land and garage adjacent to 39 Priory Terrace
4,870 sement	London, NW6 4DG Client: Old West Hampstead Estates Ltd. Drawing Title: Pre Planning Application
	(Project number)DWG number_Revision
	(919)310_P01







Perspective Views









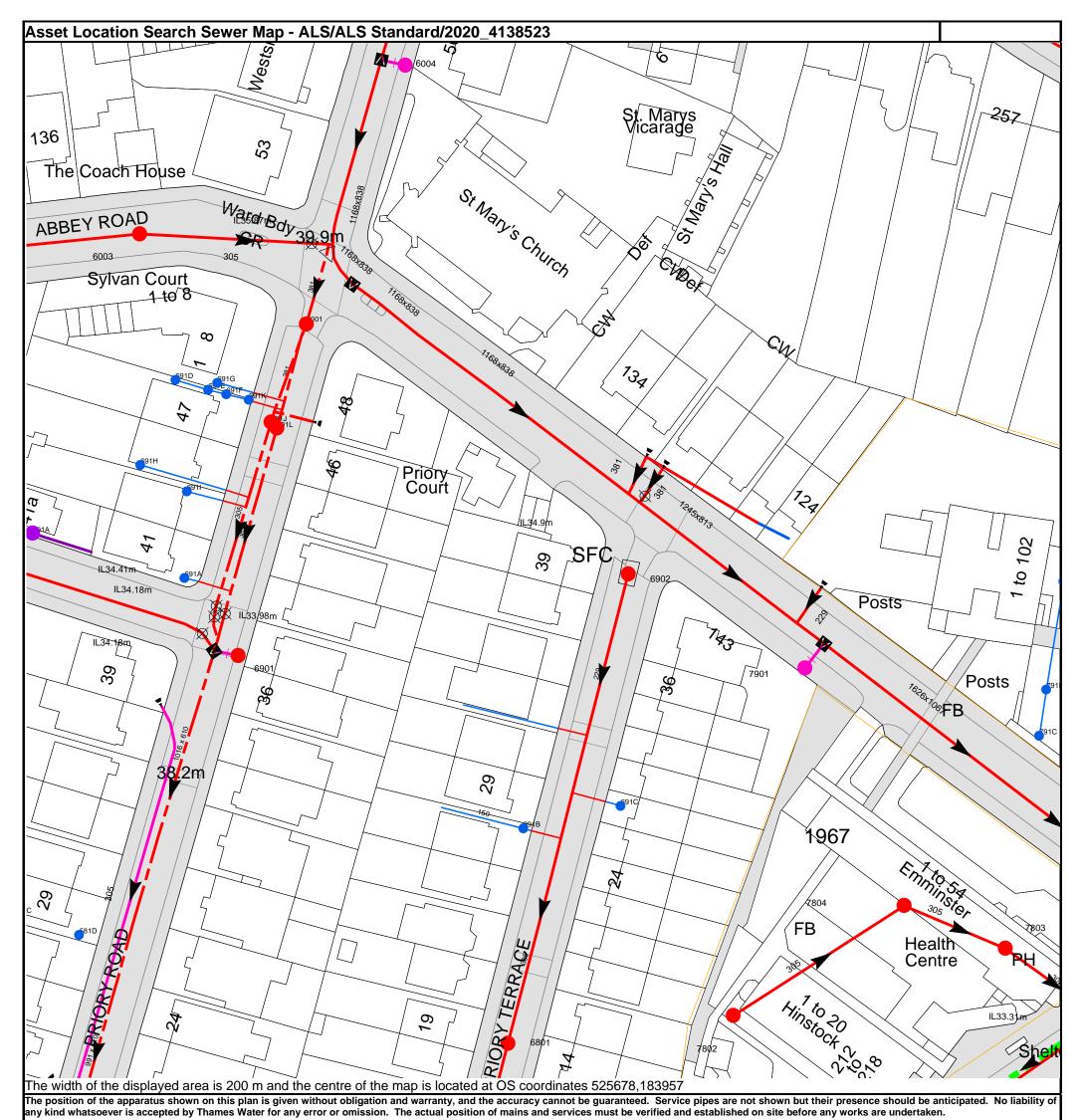
MEMBER

shh

Date: 04/02/2020 © Spence Harris Hogan 2020



Appendix B - Thames Water Sewer Records



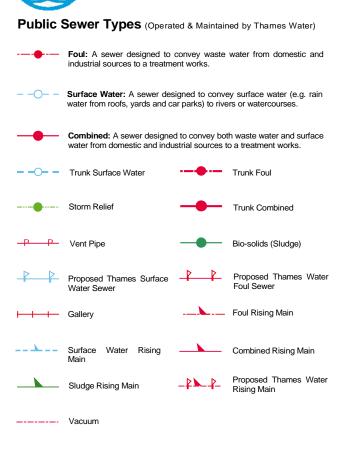
ed on the Ordnance Survey Map with the Sanction of the controller of H.M. Stationery Office, License no. 100019345 Crown Copyright Reserved

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Manhole Reference	Manhole Cover Level	Manhole Invert Level
6004	n/a	n/a
6003	40.11	n/a
691E	n/a	n/a
691G	n/a	n/a
691F	n/a	n/a
6901	n/a	n/a
691K	n/a	n/a
691J	n/a	n/a
691L	n/a	n/a
6001	39.34	35.05
6801	36.62	32.66
691B	n/a	n/a
691C	n/a	n/a
6902	38.55	34.35
7802	36.8	34.48
7901	n/a	n/a
7804	36.84	33.81
7803	37.01	33.48
791C	n/a	n/a
791B	n/a	n/a
791A	n/a	n/a
591A	n/a	n/a
581D	n/a	n/a
691H	n/a	n/a
691D	n/a	n/a
691A	n/a	n/a
6911	n/a	n/a

NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

ALS Sewer Map Key



Sewer Fittings

A feature in a sewer that does not affect the flow in the pipe. Example: a vent is a fitting as the function of a vent is to release excess gas.

- Air Valve Dam Chase Fitting
- ≥ Meter

Π

0 Vent Column

Operational Controls

A feature in a sewer that changes or diverts the flow in the sewer. Example: A hydrobrake limits the flow passing downstream.

X Control Valve Ф Drop Pipe Ξ Ancillary Weir

Outfall

Inlet

Undefined End

End Items

いし

End symbols appear at the start or end of a sewer pipe. Examples: an Undefined End at the start of a sewer indicates that Thames Water has no knowledge of the position of the sewer upstream of that symbol, Outfall on a surface water sewer indicates that the pipe discharges into a stream or river.

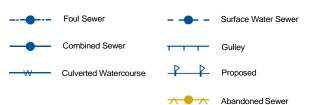
- **Other Symbols** Symbols used on maps which do not fall under other general categories
- ****/ Public/Private Pumping Station
- * Change of characteristic indicator (C.O.C.I.)
- Ø Invert Level
- < Summit

Areas

Lines denoting areas of underground surveys, etc.

Agreement **Operational Site** :::::: Chamber Tunnel Conduit Bridge

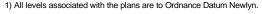
Other Sewer Types (Not Operated or Maintained by Thames Water)



Notes:

hames

Water



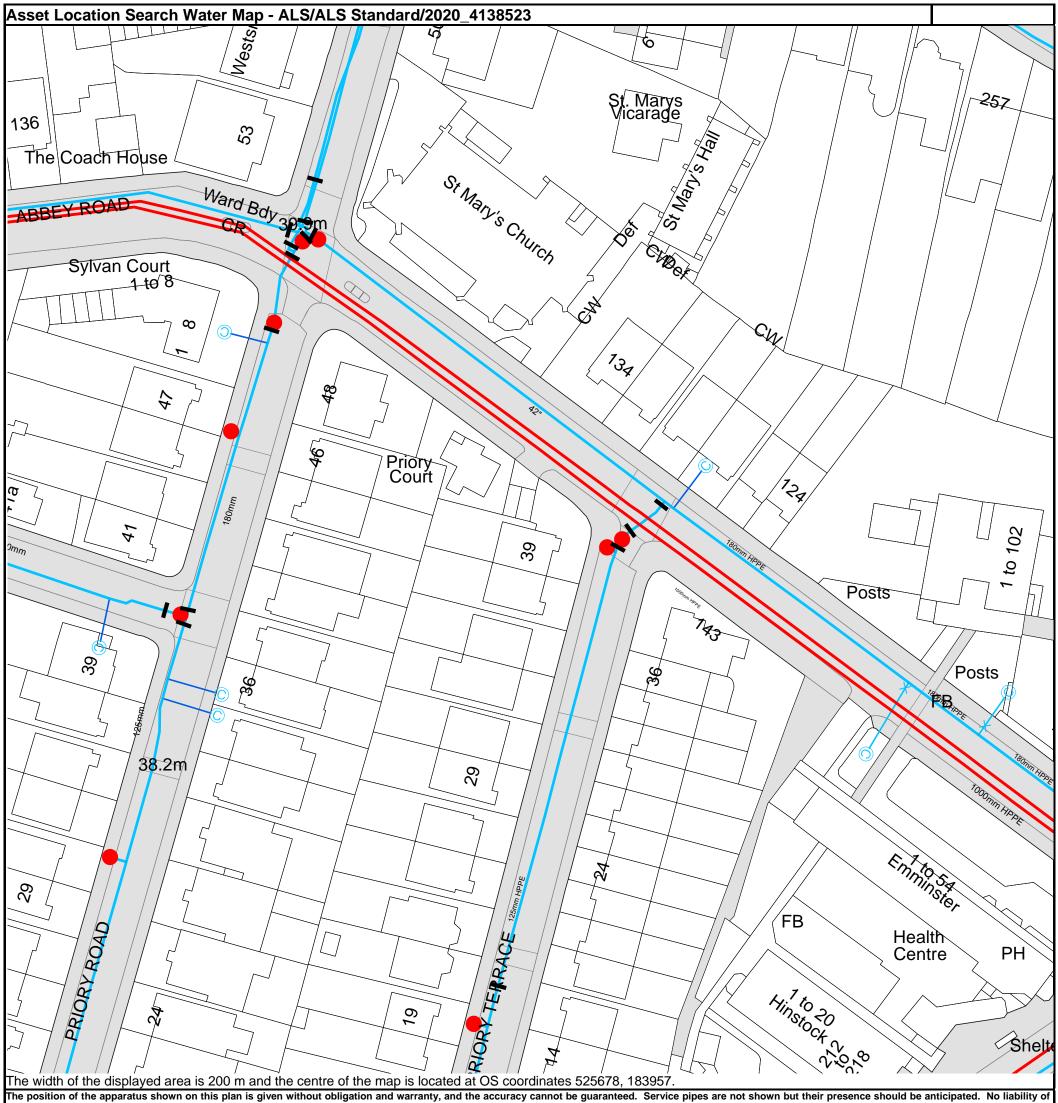
2) All measurements on the plans are metric.

- 3) Arrows (on gravity fed sewers) or flecks (on rising mains) indicate direction of flow.
- 4) Most private pipes are not shown on our plans, as in the past, this information has not been recorded.

5) 'na' or '0' on a manhole level indicates that data is unavailable.

6) The text appearing alongside a sewer line indicates the internal diameter of the pipe in milimetres. Text next to a manhole indicates the manhole reference number and should not be taken as a measurement. If you are unsure about any text or symbology present on the plan, please contact a member of Property Insight on 0845 070 9148.

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The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

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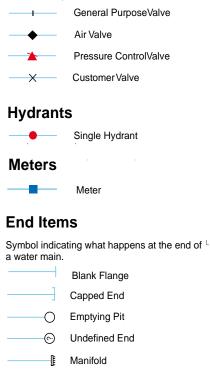
ALS Water Map Key

Water Pipes (Operated & Maintained by Thames Water)

- Distribution Main: The most common pipe shown on water maps.
 With few exceptions, domestic connections are only made to distribution mains.
- Trunk Main: A main carrying water from a source of supply to a treatment plant or reservoir, or from one treatment plant or reservoir to another. Also a main transferring water in bulk to smaller water mains used for supplying individual customers.
- **Supply Main:** A supply main indicates that the water main is used as a supply for a single property or group of properties.
- STREE
 Fire Main: Where a pipe is used as a fire supply, the word FIRE will be displayed along the pipe.
- **Metered Pipe:** A metered main indicates that the pipe in question supplies water for a single property or group of properties and that quantity of water passing through the pipe is metered even though there may be no meter symbol shown.
- Transmission Tunnel: A very large diameter water pipe. Most tunnels are buried very deep underground. These pipes are not expected to affect the structural integrity of buildings shown on the map provided.
- **Proposed Main:** A main that is still in the planning stages or in the process of being laid. More details of the proposed main and its reference number are generally included near the main.

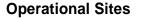
PIPE DIAMETER	DEPTH BELOW GROUND
Up to 300mm (12")	900mm (3')
300mm - 600mm (12" - 24")	1100mm (3' 8")
600mm and bigger (24" plus)	1200mm (4')

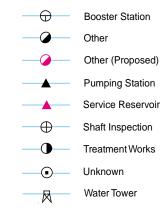
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Valves

- Fire Supply





Other Symbols

Data Logger

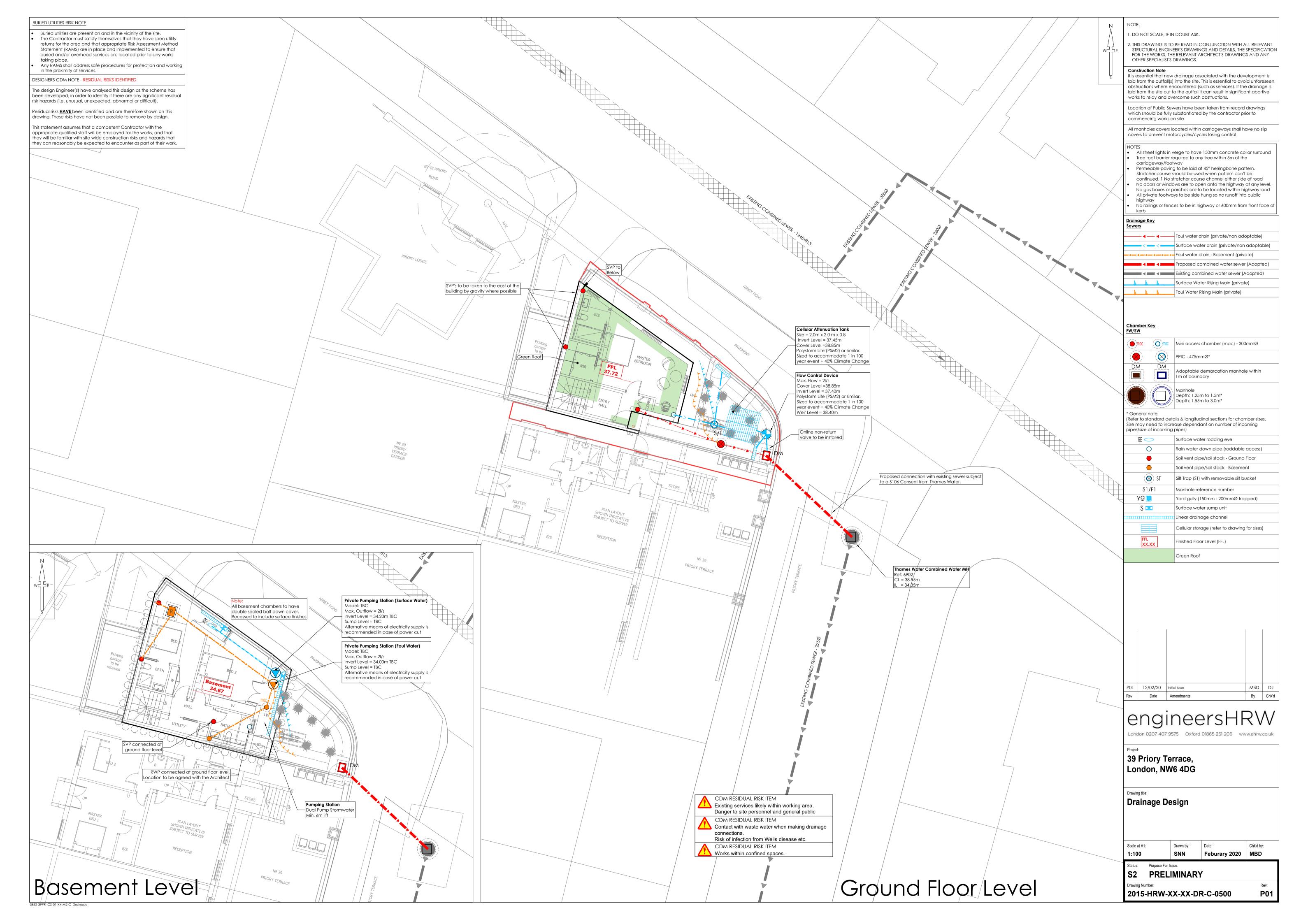
Other Water Pipes (Not Operated or Maintained by Thames Water)

Other Water Company Main: Occasionally other water company water pipes may overlap the border of our clean water coverage area. These mains are denoted in purple and in most cases have the owner of the pipe displayed along them.

Private Main: Indiates that the water main in question is not owned by Thames Water. These mains normally have text associated with them indicating the diameter and owner of the pipe.



Appendix C - Drainage Strategy





Appendix D - MicroDrainage Calculations

Infrastruct CS Ltd		Page 1
The Stables	Greenfield Runoff	
High Cogges, Witney	39 Priory Road	
Oxfordshire	London	Micro
Date 12/02/2020	Designed by MBD	Dcainago
File 3832 - GREENFIELD.SRCX	Checked by DJ	Diamaye
Innovyze	Source Control 2019.1	

ICP SUDS Mean Annual Flood

Input

Return Period (years)	100	Soil	0.450
Area (ha)	0.012	Urban	0.250
SAAR (mm)	600	Region Number	Region 6

Results 1/s

QBAR Rural 0.0 QBAR Urban 0.1 Q100 years 0.2 Q1 year 0.1 Q30 years 0.1 Q100 years 0.2

INITASLIUCT	CS Ltd								Page 1
The Stables				Atte	enuatio	n Tank	5		
High Cogges	, Witney			39 E	Priory	Terrac	ce		The second
Oxfordshire	· -			Lond	-				Mierco
Date 12/02/					gned b	V MRD			Micro
File 3832 -			N NTT2		-	-			Drainago
	AIIENUAII	LON 14	ANK		cked by				
Innovyze				Sour	ce Con	trol 2	2019.1		
	<u>Summary c</u>	of Res	sults	for 10	<u>)0 year</u>	Retu	rn Per	iod (+40%)
		Storm		Max	Max	Max	Max	Status	
		Event		Level (m)	Depth C (m)	ontrol (1/s)	(m ³)		
				(111)	(111)	(1/5)	(111)		
	15	min S	ummer	38.073	0.623	2.0	2.5	O K	
	30	min S	ummer	38.123	0.673	2.0	2.7	O K	
				38.083		2.0	2.5		
				37.955		1.8	2.0		
				37.852		1.6	1.6		
				37.773		1.4	1.3		
				37.668		1.2	0.9		
				37.604		1.0	0.6		
				37.562		0.9	0.4		
				37.532 37.496		0.8 0.7	0.3		
				37.496		0.7	0.2		
				37.450		0.3	0.0		
				37.450		0.3	0.0	0 K	
				37.450		0.2	0.0	0 K	
				37.450		0.2	0.0		
	7200	min S	ummer	37.450	0.000	0.1	0.0	ОК	
	8640	min S	ummer	37.450	0.000	0.1	0.0	ОК	
	10080	min S	ummer	37.450	0.000	0.1	0.0	O K	
	15	min W	inter	38.073	0.623	2.0	2.5	0 K	
	30	min W	inter	38.111	0.661	2.0	2.6	O K	
		~ .		_ ·					
				Rain					
		Storm					-	me-Peak	
		Storm Event			Volume	Volu	ime	me-Peak (mins)	
							ime		
	15	Event min Sı		(mm/hr)	Volume (m ³)	Volu (m ³	ume) 3.7	(mins) 14	
	15 30	Event min Su min Su	ummer	(mm/hr) 147.288 95.147	Volume (m ³) 0.0	Volu (m ³	3.7 4.8	(mins) 14 23	
	15 30 60	Event min Su min Su min Su	ummer ummer	(mm/hr) 147.288 95.147 58.456	Volume (m ³) 0.0 0.0	Volu (m ³	3.7 4.8 5.8	(mins) 14 23 40	
	15 30 60 120	Event min Su min Su min Su min Su	ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696	Volume (m ³) 0.0 0.0 0.0	Volu (m ³	3.7 4.8 5.8 6.9	(mins) 14 23 40 72	
	15 30 60 120 180	Event min Su min Su min Su min Su min Su	ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247	Volume (m ³) 0.0 0.0 0.0 0.0	Volu (m ³)	3.7 4.8 5.8 6.9 7.6	(mins) 14 23 40 72 104	
	15 30 60 120 180 240	Event min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0	(mins) 14 23 40 72 104 134	
	15 30 60 120 180 240 360	Event min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	Volu (m ³	3.7 4.8 5.8 6.9 7.6 8.0 8.7	(mins) 14 23 40 72 104 134 194	
	15 30 60 120 180 240 360 480	Event min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1	(mins) 14 23 40 72 104 134 194 254	
	15 30 60 120 180 240 360 480 600	Event min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5	(mins) 14 23 40 72 104 134 194 254 314	
	15 30 60 120 180 240 360 480 600 720	Event min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544 8.227	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5 9.9	(mins) 14 23 40 72 104 134 194 254 314 372	
	15 30 60 120 180 240 360 480 600 720 960	Event min Su min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5	(mins) 14 23 40 72 104 134 194 254 314	
	15 30 60 120 180 240 360 480 600 720 960 1440	Event min Su min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544 8.227 6.505	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5 9.9 10.4	(mins) 14 23 40 72 104 134 194 254 314 372 492	
	15 30 60 120 180 240 360 480 600 720 960 1440 2160	Event min Su min Su min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544 8.227 6.505 4.665	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5 9.9 10.4 11.2	(mins) 14 23 40 72 104 134 194 254 314 372 492 734	
	15 30 60 120 180 240 360 480 600 720 960 1440 2160 2880	Event min Su min Su min Su min Su min Su min Su min Su min Su min Su min Su	ummer ummer ummer ummer ummer ummer ummer ummer ummer ummer ummer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544 8.227 6.505 4.665 3.341	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5 9.9 10.4 11.2 12.0	(mins) 14 23 40 72 104 134 194 254 314 372 492 734 0	
	15 30 60 120 180 240 360 480 600 720 960 1440 2160 2880 4320	Event min Su min Su	Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544 8.227 6.505 4.665 3.341 2.635	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5 9.9 10.4 11.2 12.0 12.6	(mins) 14 23 40 72 104 134 194 254 314 372 492 734 0 0 0	
	15 30 60 120 180 240 360 480 600 720 960 1440 2160 2880 4320 5760	Event min Su min Su	Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer Jimmer	(mm/hr) 147.288 95.147 58.456 34.696 25.247 20.040 14.437 11.439 9.544 8.227 6.505 4.665 3.341 2.635 1.883	Volume (m ³) 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Volu (m ³)	3.7 4.8 5.8 6.9 7.6 8.0 8.7 9.1 9.5 9.9 10.4 11.2 12.0 12.6 13.6	(mins) 14 23 40 72 104 134 194 254 314 372 492 734 0 0 0 0	
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TANK Results f	39 E Lond Desi Chec	Priory don igned k cked by	-			Micro
	Lond Desi Chec	lon Igned k cked by	by MBD	:e		Micro
	Desi Chec	lgned k cked by	-			- Micro
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			Z D.T			Deain
Results f	Sour		200			Digiti
Results f		cce Cor	ntrol 2	019.1		
<u>Results f</u>						
	<u>for 1(</u>	<u>00 yea</u>	r Retur	n Per	iod (+40%)	
	Max	Max Donth (Max	Max	Status	
nt I	(m)	(m)	Control (1/s)	(m ³)		
	(111)	()	(1/3)	(
Winter 3			1.9	2.4		
Winter 3			1.6	1.7		
Winter 3			1.4	1.2		
Winter 3			1.2	0.9		
Winter 3			0.9	0.5		
Winter 3 Winter 3			0.8 0.7	0.3		
Winter 3 Winter 3			0.7	0.2		
Winter 3			0.8	0.1		
Winter 3			0.3	0.0		
Winter 3			0.2	0.0		
Winter 3	7.450	0.000	0.2	0.0	ОК	
winter 3	7.450	0.000	0.1	0.0	O K	
winter 3			0.1	0.0		
Winter 3			0.1	0.0		
1 Winter 3 1 Winter 3			0.1	0.0		
	Rain mm/hr)	Floode Volume	d Discha 9 Volu	-	.me-Peak (mins)	
		(m³)	(m³)		
Winter 5	58.456	Ο.	0	5.8	42	
	34.696			6.9	76	
Winter 2	25.247	0.	0	7.6	108	
	20.040			8.0	138	
Winter 1				8.7	196	
Winter 1				9.1	256	
Winter Winter	9.544			9.5	314	
Winter Winter	8.227			9.9 10.4	374 492	
Winter	4.665			10.4	492	
Winter	3.341			12.0	0	
Winter	2.635			12.6	0	
Winter	1.883			13.6	0	
Winter	1.482			14.2	0	
Winter					0	
Winter						
winter	0.929	υ.	U _	13.0	U	
Wi Wi	nter	nter 1.230 nter 1.057	nter 1.230 0. nter 1.057 0.	nter 1.230 0.0 2 nter 1.057 0.0 2	nter 1.230 0.0 14.8 nter 1.057 0.0 15.2	nter 1.230 0.0 14.8 0 nter 1.057 0.0 15.2 0

Infrastruct CS Ltd		Page 3
The Stables	Attenuation Tank	
High Cogges, Witney	39 Priory Terrace	
Oxfordshire	London	Micco
Date 12/02/2020	Designed by MBD	Micro
	Checked by DJ	Drainage
	Source Control 2019.1	
Rai	infall Details	
Rainfall Model	FSR Winter Storms Y	les
Return Period (years)	100 Cv (Summer) 1.0	
Region Engla M5-60 (mm)	nd and Wales Cv (Winter) 1.0 20.600 Shortest Storm (mins)	
Ratio R	0.438 Longest Storm (mins) 100	
Summer Storms	Yes Climate Change % +	
Tim	<u>e Area Diagram</u>	
	l Area (ha) 0.010	
	me (mins) Area	
Fro	om: To: (ha)	
	0 4 0.010	
<u>Tim</u>	<u>e Area Diagram</u>	
	l Area (ha) 0.000	
	me (mins) Area om: To: (ha)	
	0 4 0.000	
 @1 ΩΩ	2-2019 Innovyze	

	Page 4
Attenuation Tank	
39 Priory Terrace	
London	Micco
Designed by MBD	Desinado
Checked by DJ	Diamage
Source Control 2019.1	1
	39 Priory Terrace London Designed by MBD Checked by DJ

Model Details

Storage is Online Cover Level (m) 38.850

Tank or Pond Structure

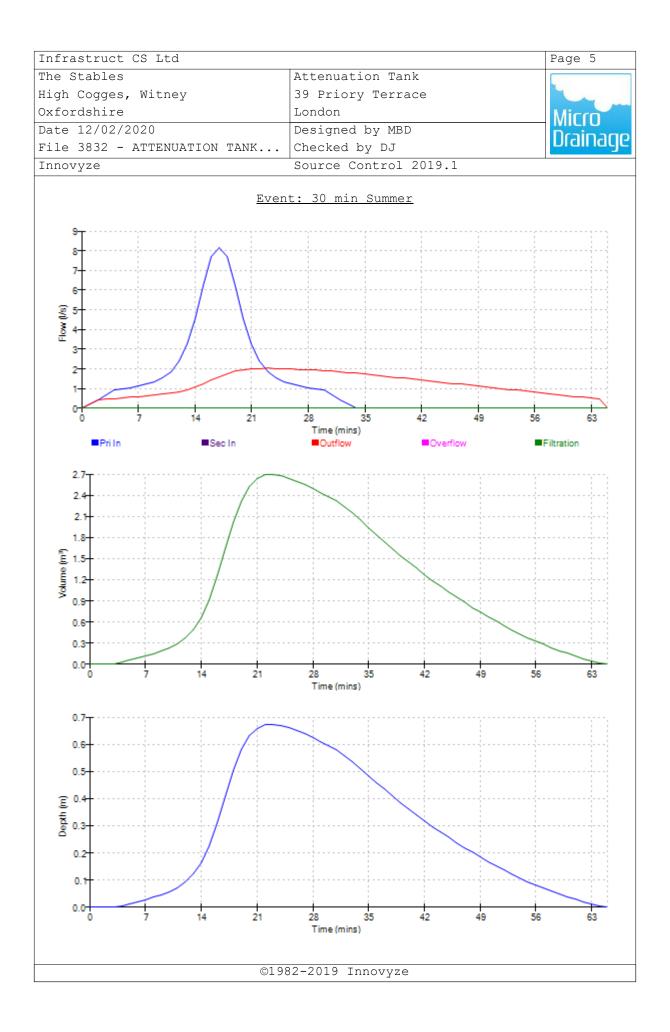
Invert Level (m) 37.450

Depth (m) Area (m²) Depth (m) Area (m²) Depth (m) Area (m²)

0.000 4.0 0.800 4.0 0.801 0.0

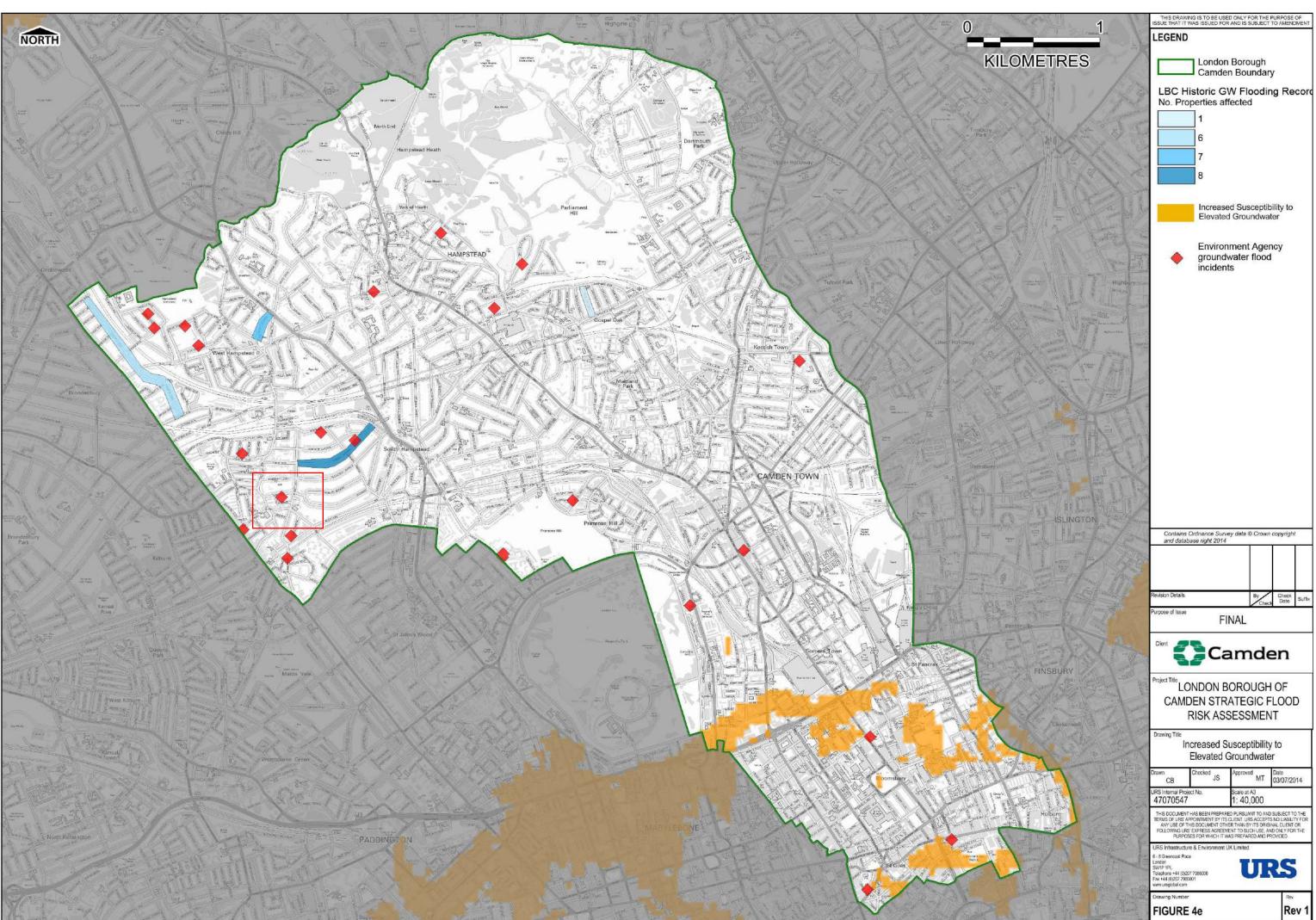
Orifice Outflow Control

Diameter (m) 0.034 Discharge Coefficient 0.600 Invert Level (m) 37.400





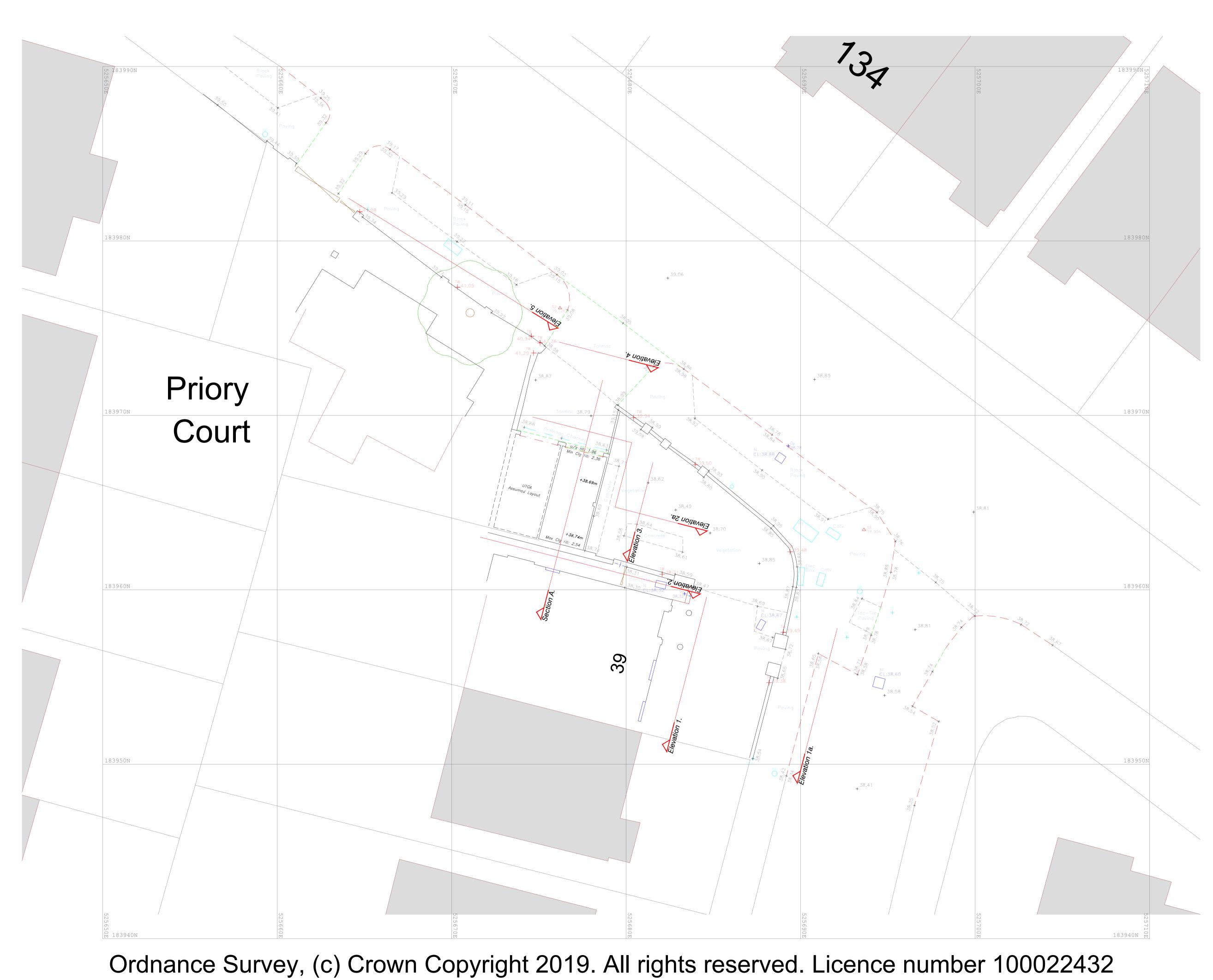
Appendix E - L.B. of Camden - Susceptibility to Elevated Groundwater Map



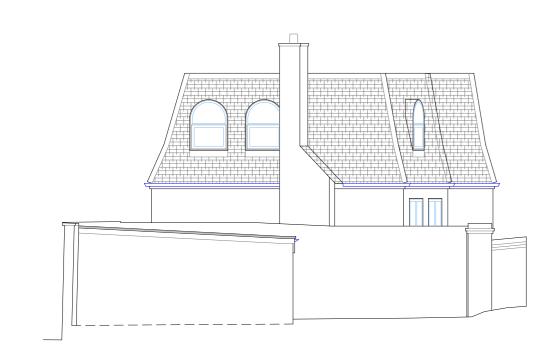
ar/Current Projects/47070547 Camden SFRA Update (ghost)/0700 WIP/0705 GIS_Data(01-WIP/01_03-Project_Files/I

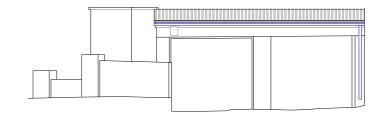


Appendix F - Topographic Survey



	•
Station Inform	nation:
Station Easting (m S1 525693.620	
S2 525676.204	
OS Note: The Ordnance Survey tile OS Buildings	e is to be used as a guide only. Surveyed Buildings
This survey has been orie. (O.S) National Grid OSGB	entated to the Ordnance Survey B36(15) via Global Navigational
A true OSGB36 coordinat) and the O.S. Active Network (OS Net). Ite has been established near to the mation using the OSTN15GB & tion models.
	related to this point and a further one ints established to create a true O.S. tion.
coordinates shown are an which have a scale factor	
of the on-site grid.	tation Table to enable establishment
SHt 1.00 HHt 2.12	Sill Height from FFL. Head Height from FFL.
SL 51.03m HL 52.82m Susp CHt: 2.00	Sill Level from defined datum. Head Level from defined datum. Suspended Ceiling Height from FFL.
Struct CHt: 3.00 Susp Ceil: 30.00m Struct Ceil: 31.00m	Structural Ceiling Height from FFL. Suspended Ceiling Level from datum.
IFL: 100.00m +100.00m	Internal Floor Level (General). Internal Floor Level (Specific).
- Insertion Point	Insertion Point for overlay drawings of other floors or details.
Elec	al Survey Legend:
Buildings Overhead Cable	IC Inspection chamber Boll Bollard Pinv Pipe invert IB Illuminated bollard
Kerb line Tarmac edge Line marking Grass verge Drop kerb Canopy/Overhang Centre line Verge	Gy Gully Bin Rubbish bin Bg Back gully Vp Vent pipe Dp Down pipe Grl Ground light Pipe Pipe above ground Lbox Letter box
▲ 1 Station and Name 100.000 Station Level	MH Manhole Ldr Ladder WL Water level Sty Stile FI Flood light IFL Internal floor level
Area of Undergrowth	Tp Telegraph post Sp Sign post
R: Ridge Level E: Eaves Level F: Flat Roof Level	Bus Bus stop ELC Electric Sv Stop valve BT British Telecom St Stop tap C'box Control box
Gate Fence types:	Er Earth rod TT Tactile Wm Water meter BP Brick paved Gas Gas valve CPS Concrete paving slabs Av Air valve CVR Cover
WM Wire Mesh	No National Construction Occurrence ICU Undentified inspection IC Inspection chamber Wo Wash out R/wall Retaining wall Re Rodding eye UTL Unable to lift
CIL Chain Link WIP Wooden Panels CIP Concrete Panels	BB Belisha beacon TCL Tree canopy level CTV Cable tv G: Girth Mkr Marker post MG Multi girth Gmkr Gas marker post Stmp Tree Stump
SIP Steel Palisade	So Soffit CL: Cover level IL: Invert level
Rev Date D	Description Drawn Q. Ref.
greer	nhatch "
Topographical Surveys Site Engineering	
 Utility / CCTV Surveys Bathymetric Surveys 	s 🗆 3D Revit & BIM Models 🗇 Area, Lease & Fire Plans
Duf	wan House iffield Road ittle Eaton
Tel (01332) 830044	Derby DE21 5DR Fax (01332) 830055 reenhatch-group.co.uk
St Albans News	vcastle Central London
St Albans Nev Hertfordshire Ne AL4 0LA	Amethyst Road Regents Park ewcastle Bus. Park ewcastle-U-Tyne NW1 5LL NE4 7YL
CLIENT	(01912) 736391 t. (0207) 2241806
5111	Architects
PROJECT	& Garages
No. 39 P	Priory Terrace W6 4DG
TITLE	Existing
Si	ite Plan
A1@ 1: 100	14.06.19 <i>QUALITY REF</i>
SP	GH5270
Grid orientation Se	ee OS notes above
Drawing No.	Rev.
Comments	<u>01_P</u> 0
This plan should only be u	roup accepts no responsibility
All dimensions should be to design and construction Some services may have b	on. been omitted due to parked vehicles.
Drainage information (whi visually inspected from thi should be treated as appr Notes:	
NOICES:	18





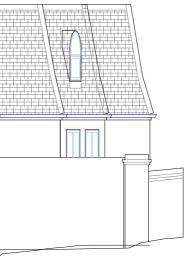
Datum: 37.00m. Elevation 3. Datum: 37.00m. Elevation 4.



Datum: 37.00m. Section A.



Datum: 37.00m. Elevation 5.



OS Note:		
The Ordnance Survey tile OS Buildings	is to be used as a Surveyed Buildir	
This survey has been orie (O.S) National Grid OSGB Satellite Systems (GNSS)	36(15) via Global	Navigational
A true OSGB36 coordinat site centre via a transform OSGM15GB transformation	nation using the O	
The survey has been corr or more OSGB36(15) poir bearing for angle orientati	elated to this poin nts established to	t and a further or create a true O.S
No scale factor has been coordinates shown are an	applied to the sur bitrary & not true (
which have a scale factor Please refer to Survey Sta of the on-site grid.		ble establishmen
Building Surv	ey Legen	d:
SHt 1.00 HHt 2.12	Sill Height from F Head Height from	FFL.
SL 51.03m HL 52.82m	Sill Level from de Head Level from	defined datum.
Susp CHt: 2.00 Struct CHt: 3.00 Susp Ceil: 30.00m	Suspended Ceilin Structural Ceiling	Height from FFL.
Susp Ceil: 30.00m Struct Ceil: 31.00m IFL: 100.00m	Suspended Ceilir Structural Ceiling	Level from datur
+100.00m	Internal Floor Lev Insertion Point for	vel (Specific).
Point	of other floors or	
[<u>Elec</u>]	<u>Gas</u>	Water
Buildings Overhead Cable	I Survey	r Boll Bollard
Wall Concrete edge Kerb line Tarmac edge Line marking Grass verge	Pinv Pipe invert Gy Gully Bg Back gully	IB Illuminated bol Bin Rubbish bin Vp Vent pipe
Drop kerb Canopy/Overhang Centre line Verge	Dp Down pipe Pipe Pipe above ground MH Manhole	Grl Ground light
▲ 1 Station and Name 100.000 Station Level	WL Water level	Sty Stile
Area of Undergrowth	Tp Telegraph post Ep Electricity post	Sp Sign post TH Trialhole
R: Ridge Level E: Eaves Level	TI Traffic light Bus Bus stop Sv Stop valve	BH Borehole ELC Electric BT British Telecon
F: Flat Roof Level Gate Fence types:	St Stop tap Er Earth rod Wm Water meter	C'box Control box TT Tactile BP Brick paved
INR Interwoven	Gas Gas valve Av Air valve ICU Undentified inspect	CPS Concrete pavir CVR Cover
PIR Post & Rail	Wo Wash out Re Rodding eye BB Belisha beacon	R/wall Retaining wall UTL Unable to lift TCL Tree canopy le
CIL Chain Link WIP Wooden Panels CIP Concrete Panels	CTV Cable tv Mkr Marker post	G: Girth MG Multi girth
SIP Steel Palisade	Gmkr Gas marker post	Store To To
	So Soffit	Stmp Tree Stump CL: Cover level IL: Invert level
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	So some	CL: Cover level L: Invert level Drawn Q, I
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site Engineering Utility / CCTV Surveys Bathymetric Surveys Bathymetric Surveys Tel (01332) 830044 D Tel (01332) 830044	Description Description Description Description Measure a Measure a Mea	CL Covertivel EL tweetlevel Drawn Q. I Drawn Q. I CCh C CCh C CCH CCH CCH CCH CCH CCH CCH C
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