BASEMENT IMPACT ASSESSMENT

19 PARK SQUARE EAST, LONDON

FOR

19 PARK SQUARE EAST LTD





CONTENTS PAGE No.

APPROVAL & DISTRIBUTION SHEET	i
FOREWORD	ii
1. SUMMARY	1-2
2. INTRODUCTION	3-5
2.1 GENERAL INTRODUCTION	3
2.2 SOURCES OF INFORMATION	3-4
2.3 EXSISTING SITE LOCATION AND LAYOUT	4
2.4 TOPOGRAPHY	4
2.5 PROPOSED DEVELOPMENT	4-5
2.6 NEIGHBOURING PROPERTIES AND STRUCTURES	5
3. DESK STUDY	6-9
3.1 SITE HISTORY	6
3.2 GEOLOGY	6-7
3.3 HYDROGEOLOGY	7-8
3.4 HYDROLOGY	8
3.5 FLOODING	8-9
3.6 CONCEPTUAL SITE MODEL	9
4. SCREENING	10-13
4.1 SLOPE STABILITY	10-11
4.2 SUBTERRANEAN (GROUNDWATER) FLOW	11-12
4.3 SURFACE FLOW AND FLOODING	12-13
5. SITE INVESTIGATION	14-16
5.1 INTRUSIVE GROUND INVESTIGATION	14
5.2 GROUND AND GROUNDWATER CONDITIONS	14-16
5.3 SITE MODEL	16
6. SCOPING AND IMPACT ASSESSMENT	17-21
6 1 SLOPE STABILITY	17-18



6.2 SUBTERRANEAN GROUNDWATER FLOW	19-20
6.3 SURFACE WATER	20-21
7. GROUND MOVEMENT ASSESSMENT	22-26
7.1 INTRODUCTION	
7.2 PROPOSED BASEMENT LAYOUT	
7.3 GROUND CONDITIONS	
7.4 PDISP ANALYSIS	
7.5 HEAVE AND SETTLEMENT ANALYSIS	
8. DAMAGE CATEGORY ASSESSMENT	27-35
8.1 INTRODUCTION	27
8.2 CRITICAL DAMAGE CATEGORY LOCATIONS	27-28
8.3 AFFECTED WIDTHS OF CRITICAL LOCATIONS	28-29
8.4 DISPLACEMENTS ALONG ASSESSED WALLS	30-33
8.5 DAMAGE CATEGORY RATING	34-35
9. BASEMENT IMPACT ASSESSMENT CONCLUSIONS AND SUMMARY	36-40
9.1 STAGE 1: SCREENING	36-37
9.2 GROUND INVESTIGATION	37-38
9.3 SITE MODEL	38-39
9.4 SCOPING AND IMPACT ASSESSMENT	39-40
10. REFERENCES	41
FIGURES	
Figure 1: Loaded Zones Introduced to PDISP	23
Figure 2: Critical Damage Category Assessment (DCA) Locations	28
Figure 3: Predicted Displacements for Assessed Walls	31-33
Figure 4: Damage Category Ratings	34
Figure 5: Classification of Visual Damage to Wall	35
TABLES	
Table 3-1: BGS Borehole Data	7
Table 4-1: Screening- Slope Stability	10-11

Table 4-2: Screening- Subterranean (Groundwater) Flow	11-12
Table 4-3: Screening- Surface Flow and Flooding	12-13
Table 5-1: Ground Investigation Details	14
Table 5-2.1: Summary of Ground Conditions	15
Table 5-2.2: Summary of Groundwater Monitoring	16
Table 6-1: Scoping- Slope Stability Impact Assessment	17-18
Table 6-2: Scoping and Impact Assessment- Subterranean (Groundwater) Flow Impact	
Assessment	19-20
Table 6-3: Scoping and Impact Assessment- Surface Water Flow Impact Assessment	20-21
Table 7-2: Maximum Net Bearing Pressures for PDISP	23
Table 7-3: Soil Parameters for PDISP	24
Table 7-5: Summary of Predicted Ground Movements form PDISP	26
Table 8-3: Geometries, Affected Widths and Predicted Settlements of Critical Locations	29
Table 8-4.1: Displacements of Assessed Walls at Closest Point	30
Table 8-4.2: Vertical Deflections of Assessed Walls	33

APPENDICES

APPENDIX A- CET REPORT FIGURES

APPENDIX B- PROPOSED DEVELOPMENT PLANS

APPENDIX C- ENVIROCHECK REPORT

APPENDIX D- SITE INVESTIGATION LOGS

APPENDIX E- PDISP EXPORTS



APPROVAL & DISTRIBUTION SHEET

PROJECT DETAILS	
CET LEAD NO.	1038915
JOB NAME	The Diorama
CLIENT	19 Park Square East Ltd.
STATUS	Final
VERSION	V2

DISTRIBUTION			
Date:	Issued to:	Name:	No:
May 2020	19 Park Square East Ltd.	Paddy Donaghy	1
May 2020	CET Infrastructure	File	1

PREPARED BY:

James Maness BSc (Hons), FGS

Geotechnical Engineer

APPROVED BY:

Phillip West BSc, MSc, CEng, MICE

Consultancy Manager

CHECKED BY:

Tony Lappin BSc (Hons), MSc, CGeol, FGS

Geotechnical Engineer

Construction Testing Solutions Limited trading as CET Infrastructure

Northdown House

Ashford Road

Harrietsham

Kent ME17 1QW

Tel: + 44 (0) 1622 858545 Web: www.cet-testing.com



FOREWORD

This document has been prepared by CET Infrastructure with all reasonable skill, care and diligence within the terms of the contract with the Client and within the limitations of the resources devoted to it by agreement with the Client. Any interpretation included herein is outside the scope of CET Infrastructure's UKAS accreditation.

This document is confidential to the Client and CET Infrastructure accepts no responsibility whatsoever to third parties to whom this document, or any part thereof, is made known. Any such party relies upon the document at their own risk.

This document shall not be used for engineering or contractual purposes unless signed above by the author and the approver for and on behalf of CET Infrastructure and unless the document status is 'Final'.

Unless specifically assigned or transferred within the terms of the agreement, the consultant asserts and retains all Copyright, and other intellectual Property Rights in and over the Report and its contents.



1. SUMMARY

The site is located at 19 Parks Square East, NW1 4LH within the jurisdiction of the London Borough of Camden.

The site is occupied by a four/five-storey disused office building and associated courtyard areas that occupies the entire footprint of the site.

The proposed development comprises the extension of the existing basement under the site footprint and lowering of the floor levels in the 'vault' section. The proposed scheme will be implemented by a series of "hit and miss" underpinned walls.

The following assessments are presented in this report:

- Desk Study;
- Screening;
- Scoping;
- Site investigation;
- Ground movement/Damage category assessment; and
- Summary and impact assessment.

A conceptual ground model for the site is summarised as follows:

- Excavation Levels Circa 26mAOD for the bulk excavation and 25mAOD for the underpinning of the basement extension. Vault areas to be lowered by 1.2m to circa 24.9mAOD with underpinning blocks founding at circa 24.4mAOD.
- **Site Topography** Relatively flat at approximately 29mAOD.
- Surface Water Bodies 473m from the site.
- Flood Risk 0.1% annual risk from water courses and High (greater than 3.3%) from surface water.
- Ground Conditions:
 - o Made Ground penetrated from 29mAOD.
 - Langley Silt Member penetrated from 28.2 to 28.25mAOD.
 - Lynch Hill Gravel Member penetrated from 27 to 25.78mAOD.
 - o London Clay Formation proved to 7.65mAOD.
- Aquifer Secondary A Aquifer in the Lynch Hill Gravel Member.
- Groundwater Groundwater level of 23mAOD to 21.65mAOD.



The main conclusions from the screening and scoping assessment are as follows:

- The site is located above a Secondary Aquifer, the Lynch Hill Gravel Member, however a measured groundwater level of between 23 and 21.65mAOD in the installed standpipes indicates the proposed basement will not extend below the groundwater table. Therefore, on the basis of the observed groundwater levels no dewatering is likely to be required. It is also unlikely that the basement would cause any significant adverse impact on groundwater flows as there are already basements surrounding the proposed construction in all four cardinal directions. Groundwater level monitoring readings should be taken during the detailed design period and prior to construction to establish the long-term groundwater regime.
- Flooding from surface water is characterised as high for this site indicating that there is a greater than 3.3% annual risk from flooding at the development site. The development must therefore meet the requirements as set out in LBC Core Strategy Camden Development Policy 27, which state that "the scale of the scheme is such that there is no, or minimal, impact on drainage conditions". Reference should be made to the separately reported FRA for comments on mitigation measures proposed for the site.
- Construction of the basement and lowering of the vault floor level will result in lowering of the foundations compared to adjacent sites by an assumed net value of between 0.6m and 1.1m, and excavation of the basement will result in some ground movements. The effect of this has been reviewed in the ground movement and damage category assessment sections of this report. Contour plots of displacement in response to the changes in vertical pressure caused by the excavation and construction of the proposed basement are included. Based upon the maximum displacements predicted by PDISP analyses, Damage Category Assessments were undertaken for the worst-case scenarios in the adjoining properties and these combined with the ground movements alongside the basement in response to the lateral stress release are as predicted by CIRIA publication C760.
- In the assessed cases, the nearest walls of 20 Park Square East (South Wall), 20 Park Square East (Rear Wall) and 20 & 18 Park Square East Vault (Rear Walls) are classified as Category 1 'very slight', while The Diorama (South West Wall) is classified as Category 0 'negligible' (as given in CIRIA SP200). The damage category results have been plotted graphically in Figure 4. Parameters for founding depths have been assumed where not data was available, and this will require validation prior to construction. No further Damage Category Assessments have been carried out as other structures in the vicinity are further away and therefore considered lower risk. Use of best practice construction methods will be essential to ensure that the ground movements are kept in line with the above predictions. Pre-construction condition surveys of neighbouring properties are also recommended, and a system of monitoring adjoining and adjacent structures should be established before the works start.



2. INTRODUCTION

2.1 GENERAL INTRODUCTION

This report presents a Basement Impact Assessment (BIA), Ground Movement Assessment (GMA) and Damage Category Assessment (DCA) for the proposed basement extension and deepening of the 'Vault' sections at 17 Park Square East, NW1 4LH, which is within the London Borough of Camden.

This report has been carried out at the request Quartz Project Services Limited acting on behalf of the client 19 Park Square East Limited.

This BIA has been produced specifically to meet the requirements of London Borough of Camden (LBC), including Planning Guidance - Basements (Camden Planning Guidance CPG, March 2018) - and the Local Plan (A5 Basements, July 2017). The report structure follows guidance for BIAs set out in the Camden Borough CPG4 (2015). The CPG4 requires desk study, screening and scoping stages, a site investigation and interpretation and ground movement assessment, and impact assessment.

This BIA evaluates the geological, hydrogeological and hydrological conditions and assess the potential detrimental ground stability, groundwater and surface water impacts the proposed development may have on the surrounding area and neighbouring properties.

Attention is drawn to the fact that whilst every effort has been made to ensure the accuracy of the data supplied and any analysis derived from it, there is a potential for variations in ground and groundwater conditions between and beyond the specific locations investigated. No liability can be accepted for any such variations. Furthermore, any recommendations are specific to the client's requirements as detailed herein and no liability will be accepted should these be used by third parties without prior consultation with CET Infrastructure.

2.2 SOURCES OF INFORMATION

The following baseline data have been referenced to complete the BIA in relation to the proposed development:

- Site walkover conducted during a ground investigation in August 2019;
- Current/historical mapping contained in an Envirocheck report;



- The site's geological setting based on the British Geological Survey (BGS) Geological Map Sheet 270
 (South London 1: 50,000 scale solid and drift, 2006), the BGS digital geology maps that utilises most
 up to date names of geological units (www.bgs.ac.uk/data) and the Geology of London Memoir
 (Ellison et al., 2004);
- Online flood risk mapping by the Environment Agency;
- LB Camden, Strategic Flood Risk Assessment (produced by URS, 2014);
- LB Camden, Planning Guidance (CPG) Basements (March 2018);
- LB Camden, Camden Geological, Hydrogeological and Hydrological Study Guidance for Subterranean Development GHHS (produced by Arup, 2010); and
- LB Camden, Local Plan Policy A5 Basements (2017).

2.3 EXSISTING SITE LOCATION AND LAYOUT

The subject site is located at 19 Park Square East, NW1 4LH at approximate Ordnance Survey grid reference TQ 287822 (see Appendix A1).

The property comprises an existing five storey section with an existing basement. The neighbouring properties comprise similarly constructed 4-storey buildings including basements. The footprint of the building is of an irregular polygon shape approximate dimensions of which can be found as Appendix A2.

The property is located roughly within the centre of Park Square East and shares a party wall with No. 20 Park Square East to the south and No. 18 Park Square East to the north.

2.4 TOPOGRAPHY

The topographic map shown on an online topographic map source (http://en-gb.topographic-map.com) shows that the general area of the site is located on at about 30mAOD. However topographic maps provided by Form Structural Design show a street level of circa 29mAOD and as such this has been adopted in subsequent conceptual site models. The general area of the site is essentially level with no significant slopes noted as shown on Appendix A3. The map indicates a change in slope of approximately 1.5m over Park Square East.

2.5 PROPOSED DEVELOPMENT

Based on the provided drawings (Appendix B), the proposed development at 19 Park Square East includes the excavation and construction a single storey basement extension under the courtyard area with sides up to



10m in length. It has been assumed for purposes of this analysis that the footing width will be 1m. The total basement extension area is estimated to be about 40m².

The proposed SSL floor level of the basement extension will be circa 26.3mAOD with a proposed foundation level of 25mAOD, including an allowance for construction of the floor slab. The perimeter walls will comprise reinforced concrete (RC) retaining walls with a reinforced ground bearing concrete floor slab.

The Vault section of the site is to have the floor levels lowered by 1.2m below the existing floor level of circa 26.1mAOD. Underpinning blocks are assumed to extend 0.5m below the proposed excavation level i.e. 24.4mAOD.

2.6 NEIGHBOURING PROPERTIES AND STRUCTURES

The subject site is bordered to the north and south by No. 18 and No.20 Park Square East respectively. The west of the site is bordered by Park Square East, with the east of the site being bordered by the atrium of No. 18 Park Square East.

The neighbouring properties on Park Square East comprise similarly constructed four-storey properties of brick construction. The neighbouring properties were noted as having basements underneath their footprints and do not appear to be additions added after original construction.

Access to the public database (<u>tfl.maps.arcgis.com</u>) provided by TFL asset protection locates the nearest TFL rail asset zone of influence is about 50m to the south of the site.



3. DESK STUDY

Information in this section has been obtained from the sources outlined in Section 1.2. The background information has been used to undertake a screening and assessment of potential basement impacts.

3.1 SITE HISTORY

Historical maps have been obtained for the area and are presented in the Envirocheck Report in Appendix C. Notable developments are detailed below:

- 1869 to 1880: The earliest map available shows the property and those surrounding were already
 established. The property at this time was described as occupied by a "Baptist Chapel" up to 19401951.
- 1953 1954: The maps listed the building as "The Arthur Stanley Institute of Middlesex Hospital".
 There were no significant changes to the surrounding structures worth noting.
- 1966 1988: The site was shown as being the "Bedford College Annexe of the University of London".
 No significant changes to the surrounding structures was noted.
- No specific name for the building is given.

3.2 GEOLOGY

Publications of the British Geological Survey (BGS) indicate that the site is underlain by the London Clay Formation with superficial deposits of Langley Silt Member over Lynch Hill Gravel Member. The online BGS geological map extract displaying the geology is presented in Figure A4.

A BGS borehole located within approximately 70m north of the site on St Andrews Place was available for review. The depths of the geology and groundwater levels are summarised in Table 3-1.



Table 3-1: BGS Borehole Data

Borehole Reference	Ground Level	Geology	Geological Unit	Depth From (m bgl)	Depth To (m bgl)	Groundwater Strike (m)
		Tarmac & Brick	Made Ground	0	0.15	
		Clay & Stones	Made Ground	0.15	0.9	
		Brown Clay	Langley Silt Member	0.9	2.4	
TQ28SE126	29.81mAOD	Gravel and Sand	Lynch Hill Gravel Member	2.4	9.1	9.1
		Firm Brown Clay over Stiff Grey Clay	Weathered and Relatively Unweathered London Clay Formation	9.1	11.2	

The borehole records in Table 3-1 show a typical sequence of London Clay Formation, with superficial deposits of Langley Silt Member overlying Lynch Hill Gravel Member. These deposits will be locally mantled by Made Ground dependant on the current and previous use of the site. Superficial deposits were penetrated to a depth of 9.1m below ground level, with deposits of the London Clay formation being encountered thereafter. This borehole is located about 70m to the north of the site, but the geology at the site is not expected to vary significantly, only the thicknesses. The actual ground conditions have been assessed by a site specific ground investigation and are discussed later in this report.

3.3 HYDROGEOLOGY

A groundwater strike was noted as being encountered at 9.1m below ground level in the BGS borehole in Table 3-1, however a standing water level of 5.8m below ground level was also recorded. It is worth noting that while this may represent the groundwater in this geographic location at the time the borehole was drilled the groundwater table is liable to seasonal and long-term changes. Comments on the groundwater for the subject site is addressed in later chapters.

Hydrogeological information provided by the Envirocheck report is summarised below:

Aquifer Category (as defined by the Environment Agency) – The Superficial Deposits (Lynch Hill
Gravel Member) are described as Secondary A Aquifer with a medium vulnerability.



The bedrock aquifer (London Clay Formation) designation is Unproductive (non-aquifer); rock layers or drift deposits with low permeability that have negligible significance for water supply or river base flow.

The Superficial and Bedrock have a combined Medium vulnerability.

- Nearest groundwater abstraction licence There have been 18 licensed groundwater abstractions
 within 1km of the site with the closest being 354m to the west for the purpose of production of
 energy for electricity: heat pump from a ground water source.
- Source Protection Zone (SPZ) None present at the site.
- Groundwater vulnerability Medium; and,
- Groundwater flooding susceptibility Potential for groundwater flooding to occur.

3.4 HYDROLOGY

Hydrological information provided by the Envirocheck report and the Camden Geological, Hydrogeological and Hydrological Study – Guidance for Subterranean Development GHHS is summarised below:

- Surface water features Nearest surface water feature 473m from the subject site.
- Surface water abstraction licences The nearest surface water abstractions are within the Regent's
 Canal. The Regent's Canal is over 1km from the subject site.
- River and coastal Zone 2 or 3 flooding Site is not a Zone 2 or 3 floodplain and none are identified within 500m.
- Risk of flooding from rivers and seas Less than 0.1% yearly risk.
- Risk of flooding from surface water Yearly flood risk for the site identified as greater than 3.3%.
- Flood defences None identified within 500m.
- Flood storage areas None identified within 500m.

The book 'The Lost Rivers of London' (Barton, 1992) has been consulted and does not identify any former tributaries on the site. The nearest such example has been mapped in excess of 500m from the site.

3.5 FLOODING

The flood risk from rivers and seas as identified in the Environment Agency flood map for planning service, Figure A5, indicates a low risk.



The following risk ratings have been collated from the various references referred to in Section 10 of this report:

- High risk for surface water flooding (greater than 3.3%).
- No historical flood incidents recorded near the site.
- Surface water body was recorded 473m from the site, but environment agency has not identified this as a flood risk to the site.
- No sewer flooding events recorded within 250m of the site.

3.6 CONCEPTUAL SITE MODEL

A conceptual site model for the site has been developed using the information obtained from the desk study for use during the Screening stage.

The conceptual site model can be summarised as follows:-

- Excavation Levels Circa 26mAOD for the bulk excavation and 25mAOD for the underpinning of the basement extension. Vault areas to be lowered by 1.2m to circa 24.9mAOD with underpinning blocks founding at circa 24.4mAOD.
- **Site Topography** Relatively flat at 29mAOD.
- Surface Water Bodies 473m from the site.
- Flood Risk Very low risk (less than 0.1% annual risk) from water courses and high (greater than 3.3%) from surface water.

• Ground Conditions:

- o Made Ground to a minimum level of approximately 28.2mAOD.
- o Langley Silt Member to a minimum level of approximately 25.78mAOD.
- Lynch Hill Gravel Member to a minimum level of approximately 20.6mAOD.
- Weathered and relatively unweathered London Clay Formation proved to a minimum level of 7.65mAOD.
- Aquifer Superficial Deposits (Lynch Hill Gravel Member) are a Secondary A Aquifer. Bedrock (London Clay Formation) is Unproductive' stratum.
- **Groundwater** Water strike at approximately 20.7mAOD with standing water level of 24.1mAOD 70m from the site.



4. SCREENING

Screening has been carried out using the criteria outlined in CPG4 to identify any matters of concern relating to slope stability, groundwater flow and surface water flow/flooding that should be carried forward to the Scoping stage. The screening process uses the background site information provided in Section 2 and Section 3 of this report to complete flow charts provided in CPG4. The flow charts are reproduced in the tables below. Items requiring scoping, investigation and impact assessment are highlighted in yellow and are addressed in subsequent sections of this report.

4.1 SLOPE STABILITY

The slope stability screening flowchart from CPG4 is displayed in Table 4-1.

Table 4-1: Screening – Slope Stability

	Slope stability screening chart
Does the existing site include slopes, natural or manmade, greater than 7	No. The site is relatively flat with no sloping land above 7 degrees to the horizontal.
degrees? (approx. 1 in 8) 2. Will the proposed re-profiling of landscaping at site change slopes at the property boundary to more than	No. No re-profiling is planned.
7 degrees? (approx. 1 in 8) 3. Does the development neighbouring land, including railway cuttings and the like, with a slope greater than 7 degrees? (approx. 1 in 8)	No. The surrounding area slopes at less than 7 degrees.
4. Is the site within a wider hillside setting in which the general slope is greater than 7 degrees? (approx. 1 in 8)	No. The surrounding area slopes at less than 7 degrees.
5. Is the London Clay the shallowest strata at the site?	No, the shallowest stratum is Langley Silt Member.
6. Will any trees be felled as part of the proposed development and/or are any works proposed within any tree protection zones where trees are to be retained?	No, there are no trees on the property.
7. Is there a history of seasonal shrink- swell subsidence in the local area,	None recorded. Suitable heave protection to be implemented where clay soils are deemed to be desiccated. Lynch Hill Gravel Member to



Slope stability screening chart		
and/or evidence of such effects at site?	be the founding stratum is not liable to seasonal shrink swell.	
8. Is the site within 100m of a watercourse or a potential spring line?	None recorded.	
9. Is the site within an area of previously worked ground?	No. There is no evidence of any previously worked ground on the site.	
10. Is the site within an aquifer? If so, will the proposed basement extend beneath the water table such that dewatering may be required during construction?	Yes. The Envirocheck report indicates the Superficial Deposits are a Secondary A Aquifer. Based on the proposed excavation levels for the site dewatering is not likely to be required.	
11. Is the site within 50m of the Hampstead Heath Ponds	Not within 50m.	
12. Is the site within 5m of a highway or pedestrian right of way?	Yes, the excavation for the lowering of the vault section will be within will be within 5m of Park Square East.	
13. Will the proposed basement significantly increase the differential depth of foundations relative to neighbouring properties?	No, the neighbouring properties have been constructed with basements to approximately the same depth as the existing basement on this site.	
14. Is the site over (or within the exclusion zone of) any tunnels, e.g. railway lines?	No. The nearest railway tunnel exclusion zone is about 50m from the site boundary.	

4.2 SUBTERRANEAN (GROUNDWATER) FLOW

The subterranean (groundwater) flow screening flowchart from CPG4 is displayed in Table 4-2.

Table 4-2: Screening – Subterranean (Groundwater) Flow

Subterranean (groundwater) flow screening chart		
1. a) Is the site located directly above an aquifer?	Yes. The Envirocheck report indicates the Superficial Deposits are a Secondary A Aquifer.	
b) Will the proposed basement extend beneath the water table surface?	Based on BGS borehole records the excavation is unlikely to encounter groundwater. However, a ground investigation will be required to assess the conditions of the groundwater beneath the subject site. Further consideration of this will be given in light of the site specific ground investigation.	
2. Is the site within 100m of a watercourse, well (used/disused) or potential spring line?	No.	



3. Is the site within the catchment of	No.
the pond chains on Hampstead	
Heath?	
4. Will the proposed basement	Yes. Part of the existing courtyard areas are soft landscaped, with the
development result in a change in the	proposed material to be removed and basement extended beneath
proportion of hard surfaced/paved	these areas. These areas are of insignificant size in comparison to the
external areas?	site and surrounding area.
5. As part of the site drainage, will more	No, there are currently no water discharges to the ground on site or
surface water (e.g. rainfall and	proposed to be constructed. Additionally, the subject site is currently
runoff) than at present be discharged	mostly hard landscaped.
to the ground (e.g. via soakaways	
and/or SUDS)?	
6. Is the lowest point of the proposed	No. There are no ponds or spring lines identified in the vicinity of the
excavation (allowing for any drainage	site.
and foundation space under the	
basement floor) close to, or lower	
than, the mean water level in any	
local pond or spring line?	

4.3 SURFACE FLOW AND FLOODING

The surface flow and flooding screening flowchart from CPG4 is displayed in Table 4-3.

Table 4-3: Screening – Surface Flow and Flooding

Surfac	e flow and flooding screening chart
Is the site within the catchment of the pond chains on Hampstead Heath?	No.
As part of the proposed site drainage, will surface water flows (e.g. volume of rainfall and peak runoff) be materially changed from the existing route?	Courtyards to be changed from soft to hard landscaped. This will not likely rise to the level of a 'material change'.
3. Will the proposed basement development result in a change in the proportion of hard surfaced / paved external areas?	Yes. Soils in courtyard area to be excavated and basement constructed underneath. In effect this will be changed from soft to hard landscaped.
4. Will the proposed basement result in changes to the profile of the inflows (instantaneous and long term) of	No. There are no nearby watercourses.



surface water being received by adjacent properties or downstream watercourses?	
5. Will the proposed basement result in changes to the quality of surface water being received by adjacent properties or downstream watercourses?	No. There are no nearby water courses.
6. Is the site in an area identified to have surface water flood risk or is it at risk from flooding, for example because the proposed basement is below the static water level of nearby surface water feature?	Yes. The site is a high flood risk from surface water flooding. There are no nearby surface water features.



5. SITE INVESTIGATION

A site investigation stage has been undertaken to develop an understanding of the site and its immediate surroundings and for use in assessing matters of concern identified during the Screening stage. The results have been used to address the matters of concern in the Scoping and Impact Assessment stages.

5.1 INTRUSIVE GROUND INVESTIGATION

A ground investigation (GI) was completed by CET in October 2019 and comprised one 'cut-down' cable percussion borehole (BH01) and two modular windowless sampler boreholes (BH02 & BH03). Details of the GI are outlined in Table 5-1. The boreholes were undertaken within the footprint of the existing and adjacent properties.

Table 5-1: Ground Investigation Details

Type	Reference	Depth mbgl	Installation Details	
Туре		(termination)		
'Cut-down'	BH01 (Located in	20.45	7m installation with 2m	
Cable	rotunda area).		plain pipe and 2m of slotted.	
Percussion.			Bentonite seal at top and	
			bottom of installation.	
Modular	BH02 (Located in	18.45	6m installation with 1m	
Windowless	Basement of 17 Park		plain pipe and 5m of slotted.	
sampler	Square East).		Bentonite seal at top and	
			bottom of installation.	
Modular	BH03 (Located in	20	10m installation with 2m	
Windowless	Courtyard of 19 Park		plain pipe and 5m of slotted.	
sampler	Square East).		Bentonite seal at top and	
			bottom of installation.	

5.2 GROUND AND GROUNDWATER CONDITIONS

A summary of the ground and groundwater conditions encountered in the GI is presented in the table below. The borehole logs are presented in Appendix D.



Table 5-2.1: Summary of Ground Conditions

	Approximate level to	Thickness (m)	Description
Strata name	top of strata (mAOD)	THERITESS (III)	Description
Made Ground	30	0.25 to 1.9	Very clayey, slightly sandy GRAVEL of angular to rounded, fine to coarse flint and brick. Low cobble content of angular brick.
Langley Silt Member	28.2 to 28.25	1.2 to 1.75m	Firm and firm becoming stiff with depth, brown, slightly gravelly CLAY. Gravel is angular to rounded, fine and medium flint. Or Soft, brown, slightly fine sandy, silty CLAY.
Lynch Hill Gravel Member	27 to 25.78	5.18 to 5.9m	Loose to very dense, brown, very fine to coarse sandy, locally sandy and slightly sandy GRAVEL of sub-angular to rounded, fine to coarse flint.
Weathered and Relatively Unweathered London Clay Formation.	21.3 to 20.6	Not proved.	Stiff, brown mottled grey, becoming brown and grey mottled CLAY with occasional sand size selenite and silt partings. Or Stiff, grey, very closely to closely fissured CLAY with rare fine and medium sand size selenite.

A groundwater seepage was recorded in BH01 at 9.5m below ground level rising to 8m below ground level after 20 minutes of monitoring. Groundwater was likely masked in BH02 and BH03 by the continuous casing of the borehole during the drilling process. Groundwater monitoring standpipes were installed within each of the boreholes to the various depths as described in Table 5-1. Subsequent readings of the standpipes were undertaken and are presented in Table 5-2.2.



Table 5-2.2: Summary of Groundwater Monitoring

Standpipe ID	BH01		BH02		BH03	
Date of						
Monitoring	05/12/2019	12/12/2019	05/12/2019	12/12/2019	05/12/2019	12/12/2019
Visit.						
Level (mAOD)	Dry	21.65	21.72	21.74	22.42	23.0

5.3 SITE MODEL

An updated site model has been developed using the information obtained from the site investigation for use during the Scoping and Impact Assessment stages.

The updated site model can be summarised as follows:

- Excavation Levels Circa 26mAOD for the bulk excavation and 25mAOD for the underpinning of the basement extension. Vault areas to be lowered by 1.2m to circa 24.9mAOD with underpinning blocks founding at circa 24.4mAOD.
- Existing Foundation Level for Neighbouring Properties Would be anticipated to be at least 25.4mAOD due to the similarly constructed basements.
- Site Topography Relatively flat at 29mAOD
- Surface Water Bodies 473m from the site.
- Flood Risk Less than 0.1% annual risk from water courses and high (greater than 3.3%) from surface water.

Ground Conditions:

- Made Ground to a minimum level of approximately 28.2mAOD.
- o Langley Silt Member to a minimum level of approximately 25.78mAOD.
- o Lynch Hill Gravel Member to a minimum level of approximately 20.6mAOD.
- Weathered and relatively unweathered London Clay Formation proved to a minimum level of 7.65mAOD.
- Aquifer Lynch Hill Gravel Member Secondary A Aquifer.
- **Groundwater** Groundwater level of 23mAOD to 21.65mAOD



6. SCOPING AND IMPACT ASSESSMENT

The Scoping stage identifies the potential impacts of the proposed scheme that were identified by the Screening stage. Items that have been identified as having a potential impact have been taken forward into the Impact Assessment stage.

The following impact assessments are based on concerns identified previously and the CPG4 screening assessments in Section 4.

6.1 SLOPE STABILITY

The potential impacts identified in the slope stability CPG4 Stage 1 Screening Assessment, Table 4-1, have been addressed in Table 6-1.

Table 6-1: Scoping- Slope Stability Impact Assessment

	Slope stability scoping chart							
Screening	Scoping	Impact Assessment						
Question								
10. Is the site within an aquifer? If so, will the proposed basement extend beneath the water table such that dewatering may be required during construction?	"Yes. The Envirocheck report indicates the Superficial Deposits are a Secondary A Aquifer." Groundwater for the site was measured to a level of between 23mAOD and 21.65mAOD. Minimum excavation level is to be higher than the highest groundwater measured. Excavation is not likely to encounter groundwater.	No impact assessment required. Further consideration given below.						



12. Is the site
within 5m of a
highway or
pedestrian
right of way?

"Yes, the excavation for the rear basement and lowering of the vault section will be within 5m of the Albany Terrace and Park Square East respectively."

Excavation and formation of the basement could cause ground movement affecting the carriageway.

The vault design and construction will need to consider the carriageway in a similar manor to how it addresses the neighbouring properties. The impacts and potential mitigation are discussed in more detail below.

Groundwater has been monitored over a short term period. Taking in to account the water strikes during the investigation and subsequent monitoring readings groundwater has always been encountered at levels below 24mAOD. However this represents the groundwater level over the period of October to December, and further groundwater monitoring may be required to assess the seasonal variations and long term groundwater conditions.

Ground movement associated with forming the basement excavation is a potential hazard. A Damage Category Assessment (DCA) (Sections 7 and 8) has been completed to assess the effects of the excavation and construction of the proposed basement on neighbouring properties.

The excavation and construction of the proposed basement and ground floor lowering will inevitably cause some ground movement. The magnitude of movements when using underpinning techniques will primarily depend on the geology, the adequacy of temporary support to both the underpinning excavations and the partially complete underpinning prior to installation of full permanent support as well as the quality of workmanship when constructing the permanent structure.

It is crucial therefore that the use of best practice methods of temporary support and high-quality workmanship are used to control ground movements alongside the basement excavations. Prior to excavation of the underpinning works all cracks in load-bearing walls that have weakened structural integrity should be fully repaired in accordance with recommendations from the appointed structural engineer.

Under UK standard practice, the design and implementation of temporary works is the contractor's responsibility, so it is considered essential that the contractor employed for these works has successfully completed similar schemes. Therefore, it is recommended that only carefully pre-selected contractors are invited to tender for the works. The contractor's temporary works should be fully detailed in their works method statements.



6.2 SUBTERRANEAN GROUNDWATER FLOW

The potential impacts identified in the subterranean flow CPG4 Stage 1 Screening Assessment, Table 4-2, have been addressed in Table 6-2.

Table 6-2: Scoping and Impact Assessment-Subterranean (Groundwater) Flow Impact Assessment

	Subterranean (groundwater) flow scoping chart					
Screening Question	Scoping	Impact Assessment				
1. a) Is the site located directly above an aquifer?	"Yes. The Envirocheck report indicates the Superficial Deposits are a Secondary A Aquifer." The groundwater table has been recorded to a level of lower than the lowest proposed excavation level, i.e below a level of 24mAOD.	There are currently similarly constructed basements to that proposed on this site existing on adjacent sites. These surround the site in all four cardinal directions. Although, based on measured groundwater levels, groundwater is not likely to rise to the level of the proposed basement, however should this occur the existing basements will be forming obstructions to groundwater flow as it stands. The proposed construction will not increase the surface area in any of the four directions and will not extended to depths greater than exist on site and likely surrounding the site. Therefore should groundwater level rise groundwater flow is not likely to be significantly impacted by the basement extension in any direction. This hydrogeological regime (i.e. groundwater levels and pressures) will be affected by long-term climatic variations as well as seasonal fluctuations and other				
		man-induced influences, all of which must be considered by the designers when selecting a design water level for the permanent works. No long term, multiseasonal groundwater monitoring data is available, so a conservative approach will be needed, as required by current geotechnical design standards.				
b) Will the proposed basement extend beneath the water table surface?	The ground investigation and subsequent monitoring visits encountered groundwater at its shallowest to be 23mAOD. Which is 1m below the minimum proposed excavation level. Based on the above measurement the	No impact assessment required.				



	basement construction is not expected to encounter groundwater. However, this is not considering the longer term groundwater regime. Longer term monitoring should be undertaken prior to construction to confirm that this is the case.	
4. Will the proposed basement development result in a change in the proportion of hard surfaced/paved external areas?	"Yes. Part of the existing courtyard areas are soft landscaped, with the proposed material to be removed and basement extended beneath these areas."	The proposed increase in proportion of hard surfaced/paved external areas is only to be circa 40m^2 . Please refer to the FRA for mitigation measures to be put in place.

6.3 SURFACE WATER

The potential impacts identified in the subterranean flow CPG4 Stage 1 Screening Assessment, Table 4-3, have been addressed in Table 6-3.

Table 6-3: Scoping and Impact Assessment- Surface Water Flow Impact Assessment

	Surface water scoping chart					
Screening Question	Scoping	Impact Assessment				
3. Will the proposed basement development result in a change in the proportion of hard surfaced/paved external areas?	"Yes. Courtyards to be changed from soft to hard landscaped."	The proposed increase in proportion of hard surfaced/paved external areas is only to be circa 40m2. Please refer to the FRA for mitigation measures to be put in place.				
6. Is the site in an area identified to have surface	"Yes. The site is a high flood risk from surface water flooding. There are no nearby surface water features."	The site is currently situated in an area identified as a high surface water flood risk (greater than 3.3% annually) by the Environment Agency and Camden Borough Council. The development must therefore				



water flood risk	meet the requirements as set out in LBC
or is it at risk	Core Strategy Camden Development Policy
from flooding,	27, which state that "the scale of the scheme is such that there is no, or minimal,
for example	impact on drainage conditions". Reference
because the	should be made to the FRA for details on
proposed	proposed mitigation measures.
basement is	
below the static	
water level of	
nearby surface	
water feature?	



7. GROUND MOVEMENT ASSESSMENT

7.1 INTRODUCTION

Oasys PDISP software has been used to undertake the analyses of heave and settlement ground movements arising from changes in vertical stresses caused by excavation of the basement. The analysis is based on Boussinesq's theory of analysis for calculating stresses and strains in soils due to vertically applied loads with the predicted ground movements being derived by integration of vertical strains derived from Boussinesq's equations. These preliminary analyses have not modelled the horizontal forces on the retaining walls and so have simplified the stress regime significantly. In addition, consistent with Boussinesq theory, the soils are assumed to comprise a semi-infinite isotropically homogeneous elastic medium.

7.2 PROPOSED BASEMENT LAYOUT

The basement layout has been based on drawings provided by Form Structural Design (Figure 1). The layout of the extension is to be approximately 5m by 8m and to a level of circa 26.3mOAD. Line loadings on the underpinned walls have been advised as being between 320kN/m run and 19.8kN/m run.

The vault area is to have the floor level lowered by 1.2m from a current level of approximately 26.2mAOD. Underpinning blocks will be used to form the retaining structure and has been assumed to be founding at least 1m below the proposed final floor level and be cast in 1m wide bays.

Gross pressure changes across the development have been estimated based on information provided by the structural engineer. The load zones, positive and negative, used to model the proposed basement in PDISP are displayed in Figure 1. These include the excavation and loads on the retaining walls, excavation of central area from existing ground level and construction of the basement ground bearing floor slab.

It is assumed the retaining walls will be cast in 1m wide bays with a base width of about 1m. There will be no internal columns or pads and the basement will be a reinforced concrete box.

Table 7-2 presents the net changes in vertical pressure for each load zone for the four major stages in the sequence of stress changes which will result from excavation and construction of the basement as outlined below:

Stage 1: Construction of retaining walls – Short-term (undrained) condition;



- Stage 2: Bulk excavation to basement formation level Short-term (undrained) conditions;
- Stage 3: Construction of the basement Short-term (undrained) conditions; and
- Stage 4: Construction of the basement Long-term (drained) conditions.

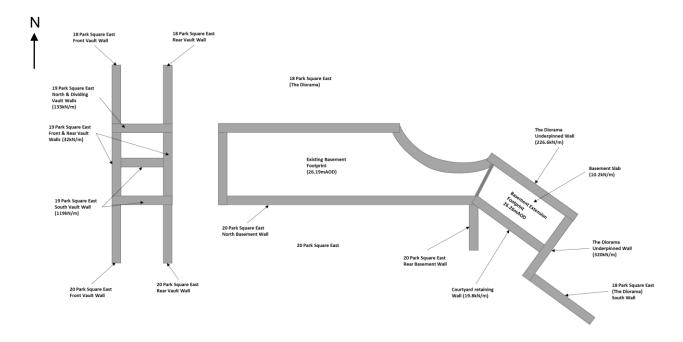


Figure 1: Loaded Zones Introduced to PDISP

Table 7-2: Maximum Net Bearing Pressures for PDISP

	Maximum Net change in vertical pressure (kN/m²)				
Zone	Stage 1 Retaining wall	Stage 2 Bulk Excavation	Stages 3 & 4 Basement construction short and long term		
Underpinned basement walls	320	320	320		
Basement slab	0	-82	-71.8		

7.3 GROUND CONDITIONS

The ground conditions used in the analysis are based on the ground conditions encountered in CET's ground investigation as shown in Table 7-2 and the logs are contained in Appendix D. In light of the ground



investigation the proposed basement will be constructed within the Lynch Hill Gravel Member with underpinning blocks founded at 25mAOD and 24.4mAOD.

The short-term and long-term geotechnical properties used in the analysis are summarised in Table 7-3. These were based on the results of the ground investigation. The Young's modulus properties for the Lynch Hill Gravel Member and London Clay Formation have been selected based on average SPT 'N' values at the foundation depth. The derivation of parameters has been made using CIRIA Special Publication 27 and CIRIA Special Publication 200.

All Made Ground and Langley Silt Member will be excavated and therefore only the change in vertical pressure, due to its excavation, is required for the PDISP analyses. Geotechnical parameters for the Made Ground are not used in the analysis. As can be seen in Table 7-3 the level to top of the Made Ground strata is elevated circa 1m from ground levels taken from street level due to the levels of strata penetrated in the boreholes sunk in the courtyards of 17 and 19 Park Square East.

A global Poisson's ratio of 0.3 has been adopted for the Lynch Hill Gravel Member and 0.5 for the London Clay Formation over their respective modelled thickness in the undrained and 0.2 for the London Clay Formation in the drained condition. This has been based on guidance provided in Thomlinson's Foundation Design and Construction and Simons and Menzies' A Short Course In Foundation Engineering.

Table 7-3: Soil Parameters for PDISP

Strata	Level to Top of Strata (mAOD)	Bulk Density (kN/m³)	Undrained Young's Modulus, Eu (MPa)	Drained Young's Modulus, E' (MPa)	Undrained Poisson's Ratio	Drained Poisson's Ratio
Made Ground	30	19	Not used	Not used	Not used	Not used
Langley Silt Member	28.2	18	Not used	Not used	Not used	Not used
Lynch Hill Gravel Member	26.5	20	60	60	0.3	N/A
London Clay Formation	21.3	19	59	35	0.5	0.2



7.4 PDISP ANALYSIS

Three dimensional analyses of vertical displacements have been undertaken using PDISP software and the basement geometry, loads/stresses and ground conditions outlined above to assess the potential magnitudes of ground movements (heave or settlement) which may result from the vertical stress changes caused by excavation of the basement. PDISP analyses have been carried out as follows:

- Stage 1: Construction of the retaining walls Short-term (undrained) condition;
- Stage 2: Bulk excavation of central area to basement formation level Short-term (undrained)
 conditions;
- Stage 3: Construction of the basement floor slab Short-term (undrained) conditions; and
- Stage 4: Construction of the basement floor slab Long-term (drained) conditions.

The results of the analyses for Stages 1, 2, 3 and 4 are presented as contour plots in Appendix E.

7.5 HEAVE SETTLEMENT ANALYSIS

Excavation of the basement and construction of the underpins will cause immediate elastic heave/settlements in response to the stress changes. The basement will be founded on granular soils that will likely have relatively small immediate effects.

The ranges of predicted short-term and long-term movements for each of the main sections of the proposed basement are presented in Table 7-5. Positive values in Table 7-5 represent settlement and negative values represent heave. All values are approximate owing to the simplification of the stress regime and include only displacements caused by stress changes in the ground beneath the basement.

All the short-term elastic displacements would have occurred before the basement slab is cast, so only the post-construction incremental heave/settlements, the difference from Stages 3, short-term, to 4, long-term, are relevant to the slab design.



Table 7-5: Summary of Predicted Ground Movements form PDISP

Location / Building Element	Stage 1 (short term) Retaining walls	Stage 2 (short term) Bulk Excavation	Stage 3 (short term) Basement slab construction	Stage 4 (long term) Basement slab construction
The Diorama South West Wall	4mm to 0mm	3.6mm to 0mm	3.6mm to 0mm	5.2mm to 0.2mm
20 Park Square East Rear Basement Wall	1.7mm to 0.8mm	0.7mm to 0.1mm	0.7mm to 0.3mm	1.7mm to 1.2mm
20 Park Square East North Basement Wall	1.7mm to Negligible	0.4mm to Negligible Heave	0.5mm to Negligible Heave	1.2mm to 0.3mm
Basement Floor Slab Area	6.7 to 1.9mm	3.9mm to -1.2mm	4.2mm to -0.7mm	6.6mm to 0.4mm
20 Park Square East Rear Vault Wall	1.8mm to 0.1mm	1.7mm to 0.1mm	1.8mm to 0.1mm	2.7mm to 0.5mm
18 Park Square East Rear Vault Wall	2mm to 0.2mm	1.9mm to 0.2mm	1.9mm to 0.2mm	2.9mm to 0.5mm
Vault Floor Slab Area	3.5mm to 2.1mm	2.9mm to 1.2mm	3.2mm to 1.6mm	4.5mm to 3.0mm
Park Square East Road	1.9mm to 0mm	1.6mm to 0mm	1.8mm to 0mm	2.9mm to 0.2mm



8. DAMAGE CATEGORY ASSESSMENT

8.1 INTRODUCTION

Behaviour of the ground will depend on the quality and methods of construction, so rigorous calculations of predicted ground movements are not practical. However, provided that the temporary support follows best practice, then industry experience has shown that the bulk movements of the ground alongside retaining walls for a single storey basement at a nominal depth 3.5m below ground level should not exceed 5mm horizontally, and effected soil is up to 4 times the depth of excavation. This figure should be adjusted pro-rata for shallower or deeper basements.

To relate these predicted ground movements to possible damage to adjacent properties, it is necessary to consider the strains and the angular distortion (as a deflection ratio) that may be generated using the method proposed by Burland (2001, in CIRIA Special Publication 200, which developed earlier work by Burland and others).

8.2 CRITICAL DAMAGE CATEGORY LOCATIONS

Evidence from site visits suggest that the neighbouring properties on Park Square East have similarly constructed basements to that which currently exist on site. There are no proposals for additional basements on the adjoining sites currently being considered by the London Borough of Camden, as confirmed by a search of their planning application portal.

As ground movements reduce with distance away from the proposed basement and the relative founding depths, the worst-case scenarios will be the rear and north walls of No. 20 Park Square East, the South West Wall of No. 18 Park Square East and the rear vault walls of number 18 and 20 Park Square East. The locations of the assessed walls are displayed in Figure 2. There will be no lateral pressure release to the south west of the basement and therefore these walls are considered to undergo inconsequential movement and have therefore not been considered.

Where current foundation details of neighbouring properties have not been available assumed parameters have been used. These values will require validation prior to construction. Should footings prove to be at higher levels than those used this will likely result in higher damage category outcomes.



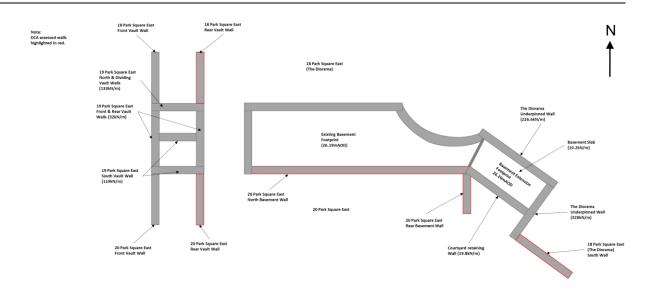


Figure 2: Critical Damage Category Assessment (DCA) Locations

8.3 AFFECTED WIDTHS OF CRITICAL LOCATIONS

The damage category assessments will consider the PDISP analyses of ground movements from vertical stress changes and ground movements alongside the proposed underpinning retaining walls caused by relaxation of the ground in response to the excavations.

CIRIA C760 (Gaba et al., 2017) details that ground movements related to the construction of retaining walls in coarse-grained soil extends up to two times the depth of excavation which at this site will be up to 2.2m laterally. A settlement of up to 0.3% of the excavation depth is predicted by CIRIA C760 which is considered appropriate for the development. However the section of underpinning for The Diorama adjacent to The Diorama North Wall has been extended by 2.5m from the bulk excavation resulting in a 2.5m offset for the assessed wall as applied in Table 8-3 and seen in Figure 2. The relevant geometries of the assessed locations have been obtained from the available drawings or approximated using maps and aerial images. The relevant geometries and affected widths and predicted settlements of the critical locations are detailed in Table 8-3.



Table 8-3: Geometries, Affected Widths and Predicted Settlements of Critical Locations

	No. 20 (Rear Basement Wall)	No. 20 (North Basement Wall)	The Diorama (South Wall)	20 Park Square East Rear Vault Wall	18 Park Square East Rear Vault Wall
Relative depth of foundations beneath ground floor	0.5m	0.5m	1.4m	0.7m (assumed)	0.7m (assumed)
Existing Approximate Floor Levels	26.1mAOD	26.1mAOD	28.5mAOD	26.1mAOD	26.1mAOD
Relative depth of excavation (below foundation level)	25.6mAOD - 25mAOD = 0.6m	25.6mAOD - 25mAOD = 0.6m	27.1mAOD - 26mAOD= 1.1m	25.4mAOD – 24.4mAOD = 1m	25.4mAOD – 24.4mAOD = 1m
Zone of influence behind basement wall (Settlement)	2 x 0.6 = 1.2m	2 x 0.6 = 1.2m	1.1 x 2= 2.2m	1m x 2 = 2m	1m x 2 = 2m
Zone of influence behind basement wall (horizontal)	4 x 0.6 = 2.4m	4 x 0.6 = 2.4m	1.1 x 4= 4.4m	1m x 4 = 4m	1m x 4 = 4m
Ground surface movement due to excavation in front of basement wall (CIRIA 760 Figure 6.16)	0.3% of max excavation depth	0.3% of max excavation depth	0.04% of max excavation depth	0.3% of max excavation depth	0.3% of max excavation depth
Distance from proposed basement	0m	0m	2.5m	0m	0m
Approximate width of assessed wall	8m	16m	11m	3m	3m
Affected width,	1.2m	1.2m	2.2m	2m	2m
Height of affected	12m (approximate	12m (approximate average height)	9m (approximate average height)	3m (approximate average height)	3m (approximate average height)



	No. 20 (Rear Basement Wall)	No. 20 (North Basement Wall)	The Diorama (South Wall)	20 Park Square East Rear Vault Wall	18 Park Square East Rear Vault Wall
building, H	average height)				
L/H	c. 0.5	c. 0.5	c. 0.5	c. 0.5	c. 0.5
CIRIA predicted settlement	1.8mm	1.8mm	0.44mm	3mm	3mm

8.4 DISPLACEMENTS ALONG ASSESSED WALLS

The predicted horizontal displacements and the relative theoretical horizontal strains beneath each wall as well as the maximum settlements produced by PDISP beneath the location of the assessed walls are displayed in Table 8-4.1.

Table 8-4.1: Displacements of Assessed Walls at Closest Point

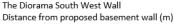
	No. 20 (Rear Basement Wall)	No. 20 (North Basement Wall)	The Diorama (South West Wall)	20 Park Square East Rear Vault Wall	18 Park Square East Rear Vault Wall
Horizontal displacement	0.9mm	0.9mm	1.6mm	1.4mm	1.4mm
Horizontal strain, ε _h	0.038%	0.038%	0.036%	0.035%	0.035%
Maximum PDISP settlement	1.7mm	1.7mm	4mm	1.8mm	2mm
CIRIA settlement	1.8mm	1.8mm	0.44mm	3mm	3mm
Combined CIRIA and PDISP settlement	3.5mm (Increased to 5mm in subsequent analysis)	3.5mm (Increased to 5mm in subsequent analysis)	4.44mm (Increased to 5mm in subsequent analysis)	4.8mm (Increased to 5mm in subsequent analysis)	5mm

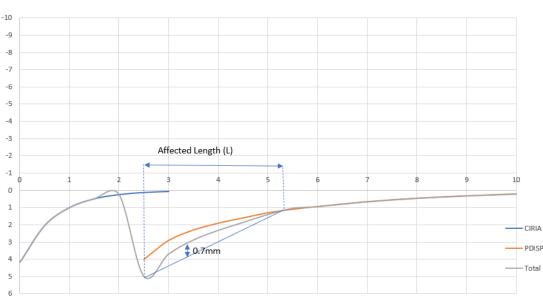
The horizontal strain is the horizontal displacement divided by the respective values in the 'Zone of influence behind basement wall (horizontal).



The settlement profile produced by PDISP along the assessed wall locations must be added to the settlement profile presented in Figure 6.16 of CIRIA Report C760, which is appropriate for the proposed construction method. The combined maximum settlements, at the closest point of the assessed walls are displayed in Table 8-4.1. Where settlement values predicted are less than 5mm these have been increased to a minimum of 5mm to reflect minimum settlement expected by Camden Council. The CIRIA settlement profiles from the basement wall to the maximum distance of affected ground are predicted to be the same for both walls and this is displayed in Figure 3.

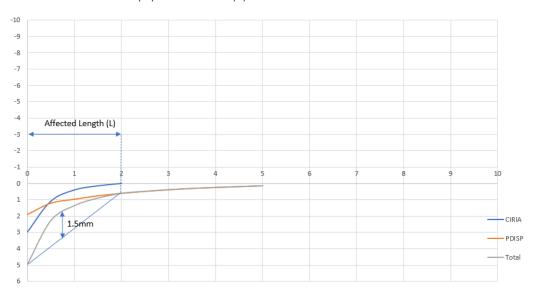
The deflection along the walls is calculated as the difference between the tangent of the relevant width of the affected walls and the total combined predicted ground surface movements curves from the CIRIA C760 and the PDISP analyses.



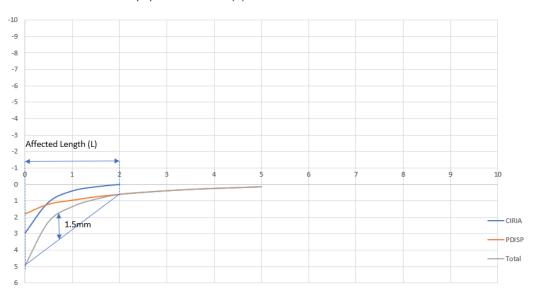




20 Park Square East Rear Vault Wall Distance from proposed basement wall (m)



18 Park Square East Rear Vault Wall Distance from proposed basement wall (m)

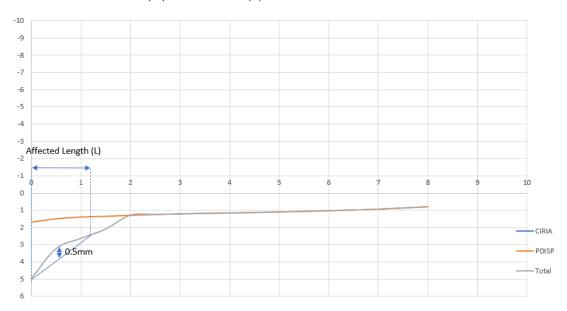




Settlement/Heave (mm)

Settlement/Heave (mm)

20 Park Square East Rear Basement Wall Distance from proposed basement wall (m)



20 Park Square East North Basement Wall Distance from proposed basement wall (m)

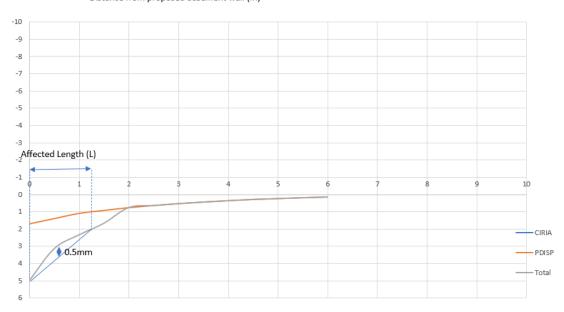


Figure 3: Predicted Displacements for Assessed Walls



The maximum vertical deflections, from the convex settlement curves for the coarse-grained soils support case and the relevant deflection ratios are displayed in Table 8-4.2.

The deflection along the wall is calculated as the difference between the tangent of the relevant width of the affected wall and the total combined predicted ground surface movements curves (from Figure 6.16 of CIRIA C760 and the PDISP analyses). Deflection ratios are measured as the above value divided by the respective 'Zone of influence behind basement wall (settlement)' row in table 8-3.

Table 8-4.2: Vertical Deflections of Assessed Walls

	No. 20 (Rear Basement Wall)	No. 20 (North Basement Wall)	The Diorama (South West Wall)	20 Park Square East Rear Vault Wall	18 Park Square East Rear Vault Wall
Vertical deflection, Δ	0.5mm	0.5mm	0.7mm	1.5mm	1.5mm
Deflection ratio, Δ/L	0.042%	0.042%	0.025%	0.075%	0.075%

8.5 DAMAGE CATEGOREY RATING

The damage category for both assessed walls are identical and are illustrated in Figure 4, using the damage category ratings and graphs given in CIRIA SP200. Figure 5 explains the damage categories.

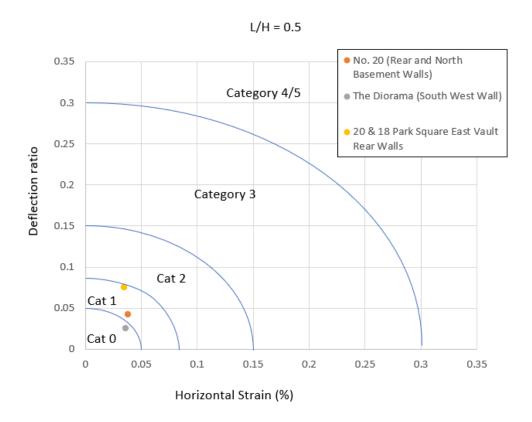


Figure 4: Damage Category Ratings

The results show the affected walls are:

- 20 Park Square East Rear Basement Wall
- 20 Park Square East North Basement Wall
- The Diorama South West Wall
- 20 & 18 Park Square East Vault Rear Walls

Any walls outside of the ones considered above are further away from proposed excavations and as such will have damage categories lower than those presented in figure 4. As such these would be expected to have damage categories of below 2 which is allowable under Camden guidance.

Use of best practice construction methods will be essential to ensure that the ground movements are kept in line with the above predictions. Pre-construction condition surveys of neighbouring properties are also recommended and a system of monitoring adjoining/adjacent structures should be established before the works start.



Category of damage	Description of typical damage (ease of repair is underlined)	Approximate crack width (mm)	Limiting tensile strain, $\varepsilon_{_{Nm}}$ (%)
0 Negligible	Hairline cracks of less than about 0.1 mm are classed as negligible	<0.1	0.0 to 0.05
1 Very slight	Fine cracks that can easily be treated during normal decoration. Perhaps isolated slight fracture in building. Cracks in external brickwork visible on inspection	<1	0.05 to 0.075
2 S l ight	Cracks easily filled. Redecoration probably required. Several slight fractures showing inside of building. Cracks are visible externally and some repointing may be required externally to ensure weathertightness. Doors and windows may stick slightly.	<5	0.075 to 0.15
3 Moderate	The cracks require some opening up and can be patched by a mason. Recurrent cracks can be masked by suitable lining. Repointing of external brickwork and possibly a small amount of brickwork to be replaced. Doors and windows sticking. Service pipes may fracture. Weathertightness often impaired.	5 to 15 or a number of cracks >3	0.15 to 0.3
4 Severe	Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows. Windows and frames distorted, floor sloping noticeably. Walls leaning or bulging noticeably, some loss of bearing in beams. Services pipes disrupted.	15 to 25, but also depends on number of cracks	>0.3
5 Very severe	This requires a major repair, involving partial or complete rebuilding. Beams lose bearings, walls lean badly and require shoring. Windows broken with distortion. Danger of instability.	Usually >25, but depends on numbers of cracks	

Notes

- 1 In assessing the degree of damage, account must be taken of its location in the building or structure.
- 2 Crack width is only one aspect of damage and should not be used on its own as a direct measure of it.

Figure 5: Classification of Visual Damage to Wall

(after Burland et al, 1977; and Boscardin and Cording, 1989; and Burland, 2001).



9. BASEMENT IMPACT ASSESSMENT AND SUMMARY

This Summary includes the principal aspects and primary findings of this assessment. The whole report should be read to obtain a full understanding of the matters considered.

Location: 19 Park Square East, W8 6JW in the London Borough of Camden.

9.1 STAGE 1: SCREENING

Items identified during a Screening stage as requiring further assessment are outlined below.

Slope Stability:

Slope stability screening chart		
10. Is the site within an aquifer? If so, will the proposed basement extend beneath the water table such that dewatering may be required during construction?	Yes. The Envirocheck report indicates the Superficial Deposits are a Secondary A Aquifer.	
12. Is the site within 5m of a highway or pedestrian right of way?	Yes, the excavation for the lowering of the vault section will be within will be within 5m of Park Square East.	

Subterranean Groundwater Flow:

Subterran	Subterranean (groundwater) flow screening chart		
1. a) Is the site located directly above an aquifer?	Yes. The Envirocheck report indicates the Superficial Deposits are a Secondary A Aquifer.		
b) Will the proposed basement extend beneath the water table surface?	Based on BGS borehole records the excavation is unlikely to encounter groundwater. However, a ground investigation will be required to assess the conditions of the groundwater beneath the subject site. Further consideration of this will be given in light of the site specific ground investigation.		
4. Will the proposed basement development result in a change in the proportion of hard surfaced/paved	Yes. Part of the existing courtyard areas are soft landscaped, with the proposed material to be removed and basement extended beneath these areas. These areas are of insignificant size in comparison to the		
external areas?	site and surrounding area.		



Surface Flow and Flooding:

Surface flow and flooding screening chart			
3. Will the proposed basement	Yes. Courtyards to be changed from soft to hard landscaped.		
development result in a change in the			
proportion of hard surfaced / paved			
external areas?			
6. Is the site in an area identified to	Yes. The site is a high flood risk from surface water flooding. There		
have surface water flood risk or is it	are no nearby surface water features.		
at risk from flooding, for example			
because the proposed basement is			
below the static water level of nearby			
surface water feature?			

9.2 GROUND INVESTIGATION

A ground investigation (GI) was completed by CET in October 2019 and comprised one 'cut-down' cable percussion borehole (BH01) and two modular windowless sampler boreholes (BH01 & BH02).

Strata name	Approximate level to top of strata (mAOD)	Thickness (m)	Description
Made Ground	30	0.25 to 1.9	Very clayey, slightly sandy GRAVEL of angular to rounded, fine to coarse flint and brick. Low cobble content of angular brick.
Langley Silt Member	28.2 to 28.25	1.2 to 1.75m	Firm and firm becoming stiff with depth, brown, slightly gravelly CLAY. Gravel is angular to rounded, fine and medium flint. Or Soft, brown, slightly fine sandy, silty CLAY.



Lynch Hill Gravel Member	27 to 25.78	5.18 to 5.9m	Loose to very dense, brown, very fine to coarse sandy, locally sandy and slightly sandy GRAVEL of sub-angular to rounded, fine to coarse flint.
Weathered and Relatively Unweathered London Clay Formation.	21.3 to 20.6	Not proved.	Stiff, brown mottled grey, becoming brown and grey mottled CLAY with occasional sand size selenite and silt partings. Or Stiff, grey, very closely to closely fissured CLAY with rare fine and medium sand size selenite.

A groundwater seepage was recorded in BH01 at 9.5m below ground level rising to 8m below ground level after 20 minutes of monitoring. Groundwater was likely masked in BH02 and BH03 by the continuous casing of the borehole during the drilling process. Groundwater monitoring standpipes were installed within each of the boreholes to the various depths as described in Table 5-1 of this report. Subsequent readings of the standpipes were undertaken with groundwater level varying between 23mAOD to 21.65mAOD.

9.3 SITE MODEL

A ground model for the site is summarised as follows:

- Excavation Levels Circa 26mAOD for the bulk excavation and 25mAOD for the underpinning of the basement extension. Vault areas to be lowered by 1.2m to circa 24.9mAOD with underpinning blocks founding at circa 24.4mAOD.
- **Site Topography** Relatively flat at approximately 29mAOD.
- Surface Water Bodies 473m from the site.
- Flood Risk 0.1% annual risk from water courses and High (greater than 3.3%) from surface water.
- Ground Conditions:
 - o Made Ground penetrated from 29mAOD.
 - Langley Silt Member penetrated from 28.2 to 28.25mAOD.
 - Lynch Hill Gravel Member penetrated from 27 to 25.78mAOD.
 - o London Clay Formation proved to 7.65mAOD.
- Aquifer Secondary A Aquifer in the Lynch Hill Gravel Member.



• **Groundwater** – Groundwater level of 23mAOD to 21.65mAOD.

9.4 SCOPING AND IMPACT ASSESSMENT

- The site is located above a Secondary Aquifer, the Lynch Hill Gravel Member, however a measured groundwater level of between 23 and 21.65mAOD in the installed standpipes indicates the proposed basement will not extend below the groundwater table. Therefore, on the basis of the observed groundwater levels no dewatering is likely to be required. It is also unlikely that the basement would cause any significant adverse impact on groundwater flows as there are already basements surrounding the proposed construction in all four cardinal directions. Groundwater level monitoring readings should be taken during the detailed design period and prior to construction to establish the long-term groundwater regime.
- Flooding from surface water is characterised as high for this site indicating that there is a greater than 3.3% annual risk from flooding at the development site. The development must therefore meet the requirements as set out in LBC Core Strategy Camden Development Policy 27, which state that "the scale of the scheme is such that there is no, or minimal, impact on drainage conditions". Reference should be made to the separately reported FRA for comments on mitigation measures proposed for the site.
- Construction of the basement and lowering of the vault floor level will result in lowering of the foundations compared to adjacent sites by an assumed net value of between 0.6m and 1.1m, and excavation of the basement will result in some ground movements. The effect of this has been reviewed in the ground movement and damage category assessment sections of this report. Contour plots of displacement in response to the changes in vertical pressure caused by the excavation and construction of the proposed basement are included. Based upon the maximum displacements predicted by PDISP analyses, Damage Category Assessments were undertaken for the worst-case scenarios in the adjoining properties and these combined with the ground movements alongside the basement in response to the lateral stress release are as predicted by CIRIA publication C760.
- In the assessed cases, the nearest walls of 20 Park Square East (South Wall), 20 Park Square East (Rear Wall) and 20 & 18 Park Square East Vault (Rear Walls) are classified as Category 1 'very slight', while The Diorama (South West Wall) is classified as Category 0 'negligible' (as given in CIRIA SP200). The damage category results have been plotted graphically in Figure 4. Parameters for founding depths have been assumed where not data was available, and this will require validation prior to construction. No further Damage Category Assessments have been carried out as other structures in the vicinity are further away and therefore considered lower risk. Use of best practice construction methods will be essential to ensure that the ground movements are kept in line with the above predictions. Pre-construction condition surveys of neighbouring properties are also recommended,



and a system of monitoring adjoining and adjacent structures should be established before the works start.



10. REFFERENCES

Barton, N. 1992. The Lost Rivers of London. Historical Publications, London.

British Geological Survey (BGS) Geological Map Sheet 270 (South London 1: 50,000 scale solid and drift, 2006), the BGS digital geology maps that utilises the most up to date names of geological units (www.bgs.ac.uk/data), and the Geology of London Memoir (Ellison et al., 2004).

Burland, J.B., et al. 2001. Building response to tunnelling. Case studies from the Jubilee Line Extension, London. CIRIA Special Publication 200.

Gaba A.R., et al. 2017. Guidance on Embedded Retaining Wall Design. CIRIA Report C760.

London Borough of Camden, Local Plan Policy A5 Basements (2017).

Padfield, C.J. and Sharrock, M.J. 1983. Settlement of structures on clayey soils. CIRIA Special Publication 27.F

Tomlinson, M.J. 1986. Foundation Design and Construction.

Simons, N. and Menzies B., 1977. A Short Course in Foundation Engineering.



APPENDIX A CET REPORT FIGURES

CET		INFRASTRUCTURE Giving our all
	©	

Northdown House, Ashford Road, Harrietsham, Maidstone Kent, ME17 1QW Telephone: 01622 858545 Facsimile: 01622 858544

The Di	iorama- :	17-19	Park S	Square	East
--------	-----------	--------------	--------	--------	-------------

Lead No. **1038915**

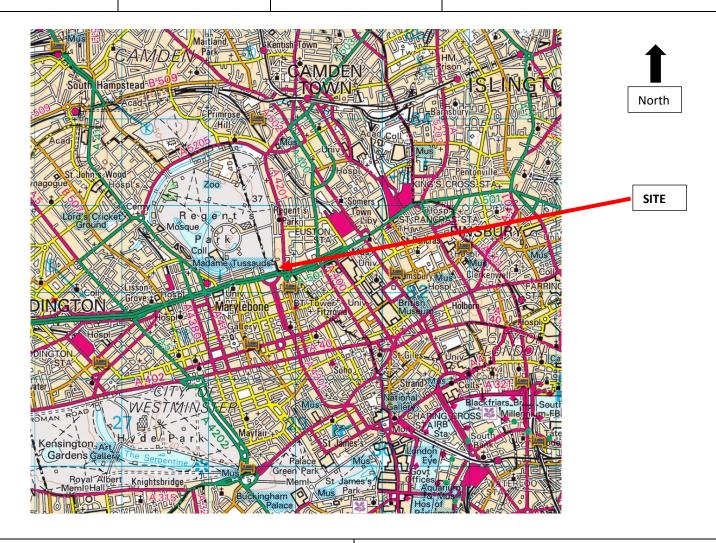
Created By: JM

Checked: PJW

Approved: PJW

Date:

November 2019



Site Location Plan

Scale: 1 square = 1km

CFT	INFRASTRUCTURE Giving our all

Northdown House, Ashford Road, Harrietsham, Maidstone Kent, ME17 1QW Telephone: 01622 858545 Facsimile: 01622 858544

The D	iorama-	17-19	Park S	Square	East
-------	---------	--------------	--------	--------	-------------

Lead No.

1038915

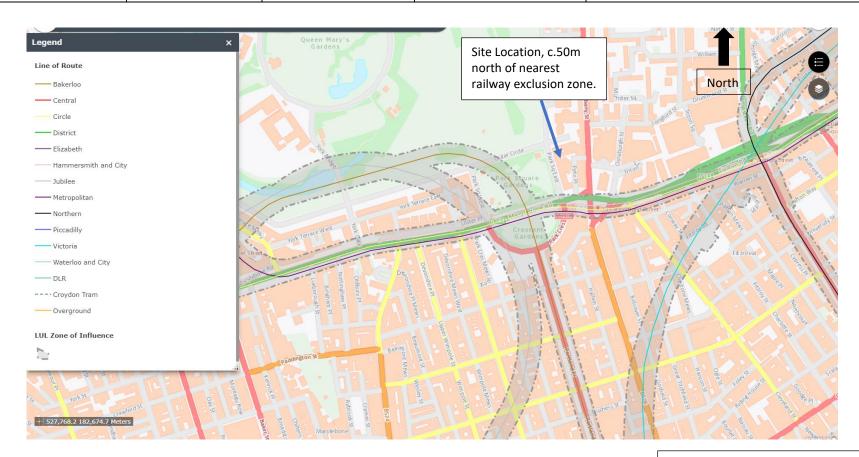
Created By: JM

Checked: PJW

Approved: PJW

Date:

November 2019



Transport for London Property Asset Manager

Tunnel Asset Locations

Scale: As shown

CET	INFRASTRUCTURE Giving our all
,	Road, Harrietsham, Maidstone

Telephone: 01622 858545 Facsimile: 01622 858544

The Diora	ıma- 17-1	L9 Park	Square	East
-----------	-----------	---------	--------	------

Lead No. **1038915**

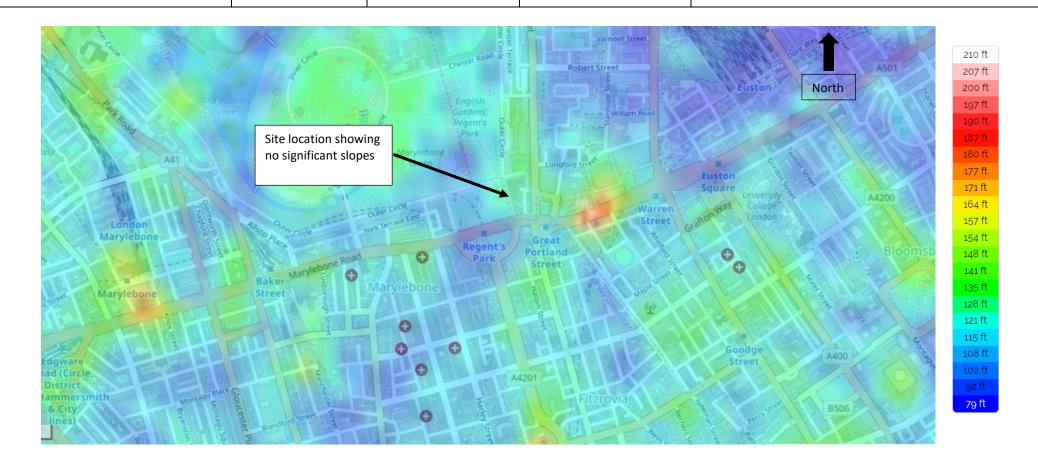
Created By: **JM**

Checked: **PJW**

Approved: PJW

November 2019

Date:



Topographic Map

Scale: NTS

CET	INFRASTRUCTURE Giving our all
· ·	Road, Harrietsham, Maidstone NE17 1QW

Telephone: 01622 858545 Facsimile: 01622 858544

The Diorama- 17-19 Park Square East

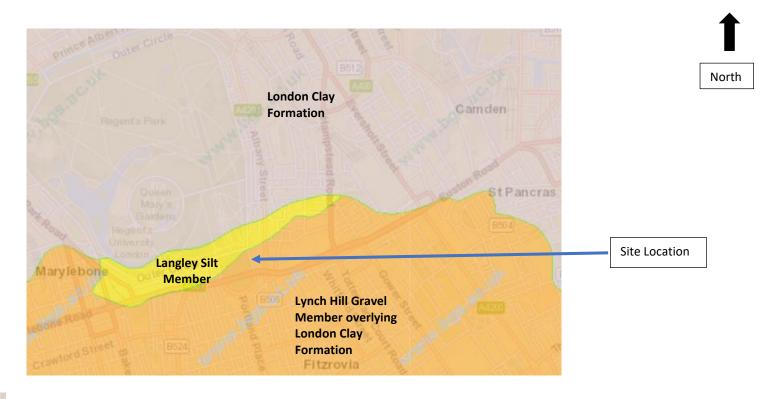
Lead No.		
	1038915	

Created By: **JM**

Checked: PJW

Approved: **PJW**

Date: November 2019





© British Geological

Geological Map

FIGURE A4

Scale: As shown

	· ·	INFRASTRUCTURE Giving our all
North day on Haysa	Ashford Dood	Harriotcham Maidstana

Northdown House, Ashford Road, Harrietsham, Maidstone Kent, ME17 1QW Telephone: 01622 858545 Facsimile: 01622 858544

T	he	D	iorama-	17	7-19	Park	Sa	uare	East
•			orania			· air	99	aarc	Last

1038915

Created By: **JM**

Checked: Approved: PJW

Date:

Site Location within

Flood Zone 1

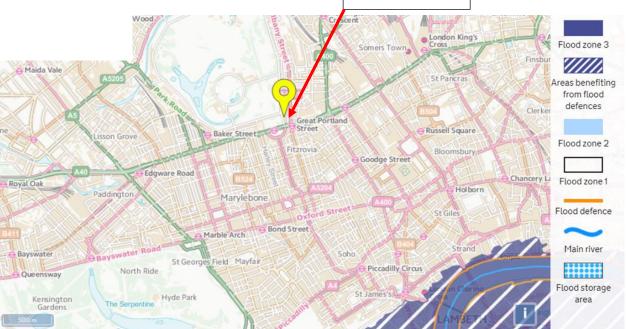
Lead No.

November 2019

FLOOD ZONE 1

Land and property in flood zone 1 have a low probability of flooding

More information about flood zones



PJW

Flood Zone Map

Scale: As shown

CFT	INFRASTRUCTURE Giving our all

The Diorama- 17-19 Park Square East

ead No.		
	1038915	

November 2019

Northdown House, Ashford Road, Harrietsham, Maidstone Kent, ME17 1QW Telephone: 01622 858545 Facsimile: 01622 858544 Created By: Checked: Approved: Date:

JM PJW PJW

Flood risk from rivers or the sea	\otimes
Very low risk means that each year this area has a chance of flooding of less than 0.1%. This takes into account the effect of any flo defences in the area. These defences reduce but do not completely stop the chance of flooding as they can be overtopped, or fail.	od North
Regent's Centre Longford Street Centre London Street Sta'(L	Hospi Statistica Mus
Sch Sch Vork Terrace East Warnin Street (LÜUE) The Portland Hospital For Women And Children A501 Marylebone Road A501 Marylebone Road A501 PW Hospi PW To Sch	itzrovia savesti di sa
University of Westminster Westminster Vestminster Notify Jace Hospi Weymouth Street Neymouth Street	Additional PW

Flood Risk (Rivers & Seas)

Scale: NTS

CE		INFRASTRUCTURE Giving our all
	o	

Northdown House, Ashford Road, Harrietsham, Maidstone Kent, ME17 1QW Telephone: 01622 858545 Facsimile: 01622 858544

The D	iorama-	17-19	Park S	Square	East
-------	---------	--------------	--------	--------	-------------

PJW

Created By: **JM**

Checked:

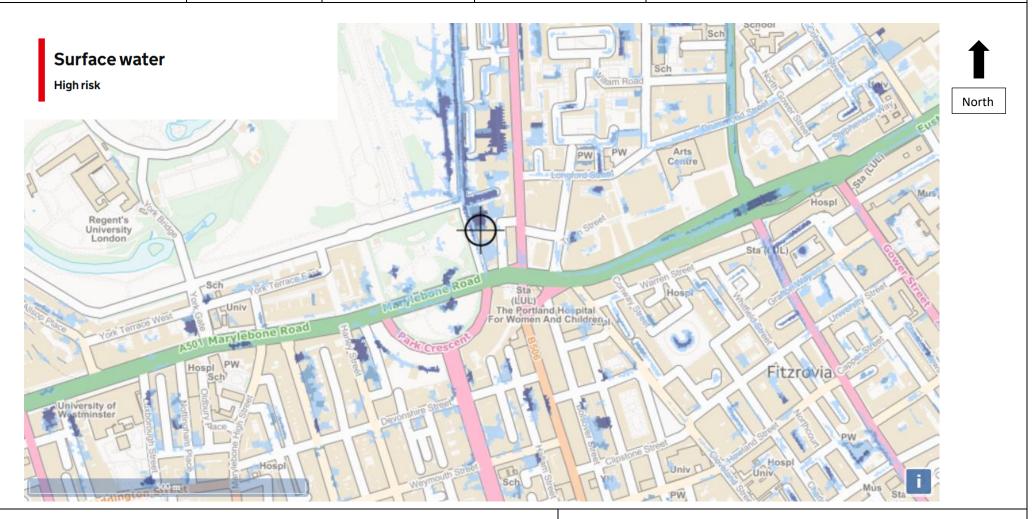
Approved: PJW

Date:

Lead No.

November 2019

1038915

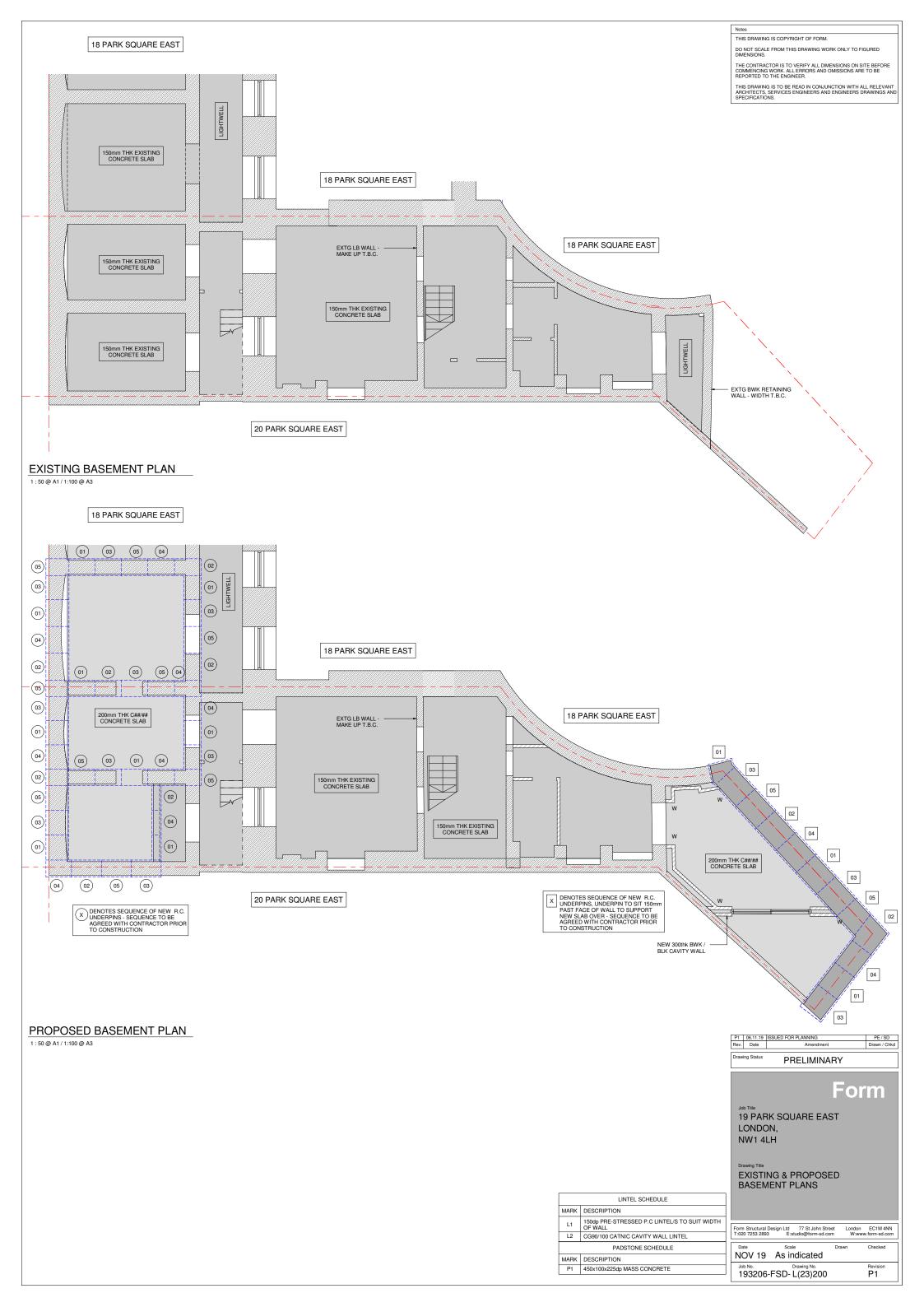


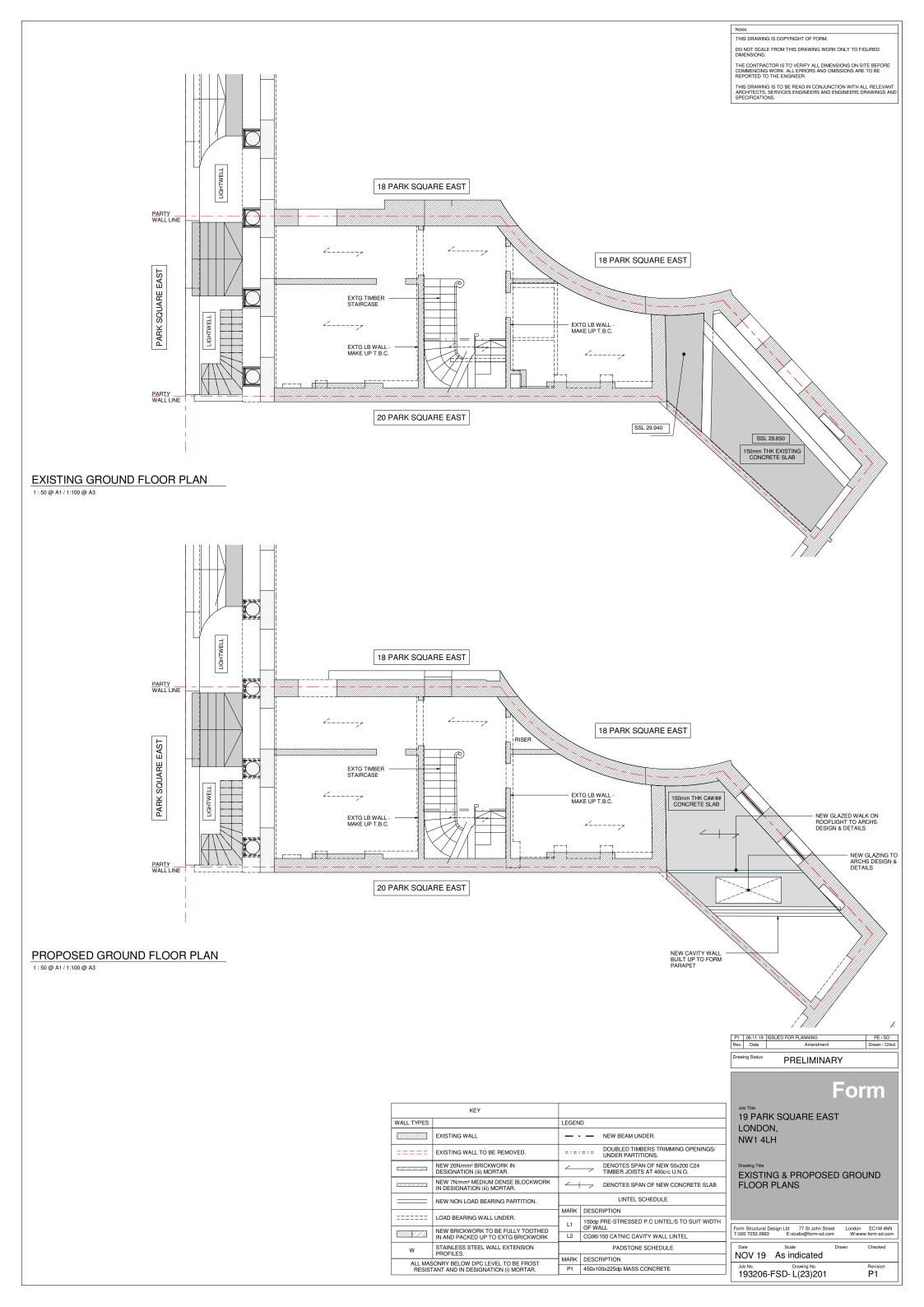
Flood Risk (Surface Water)

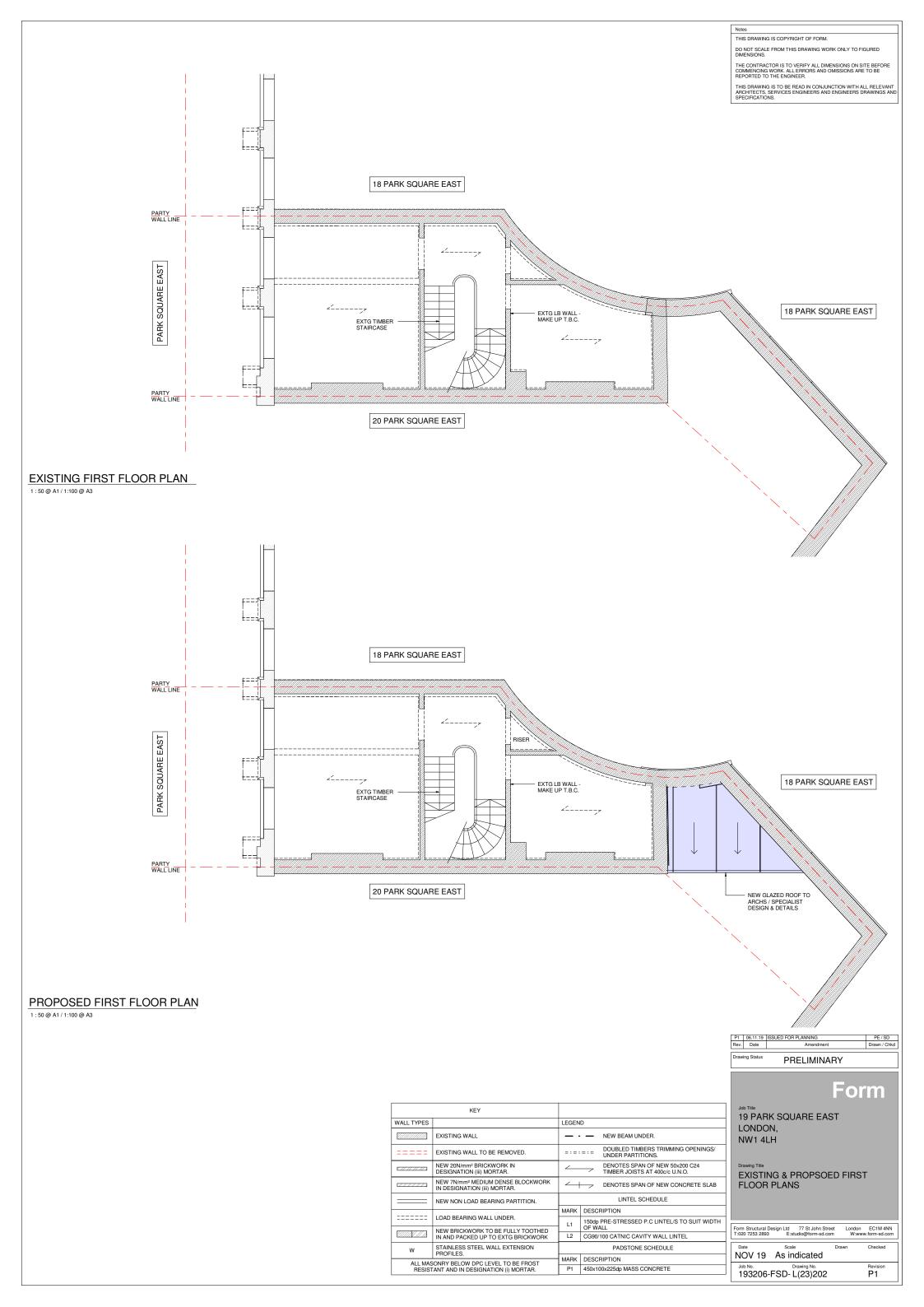
Scale: As shown

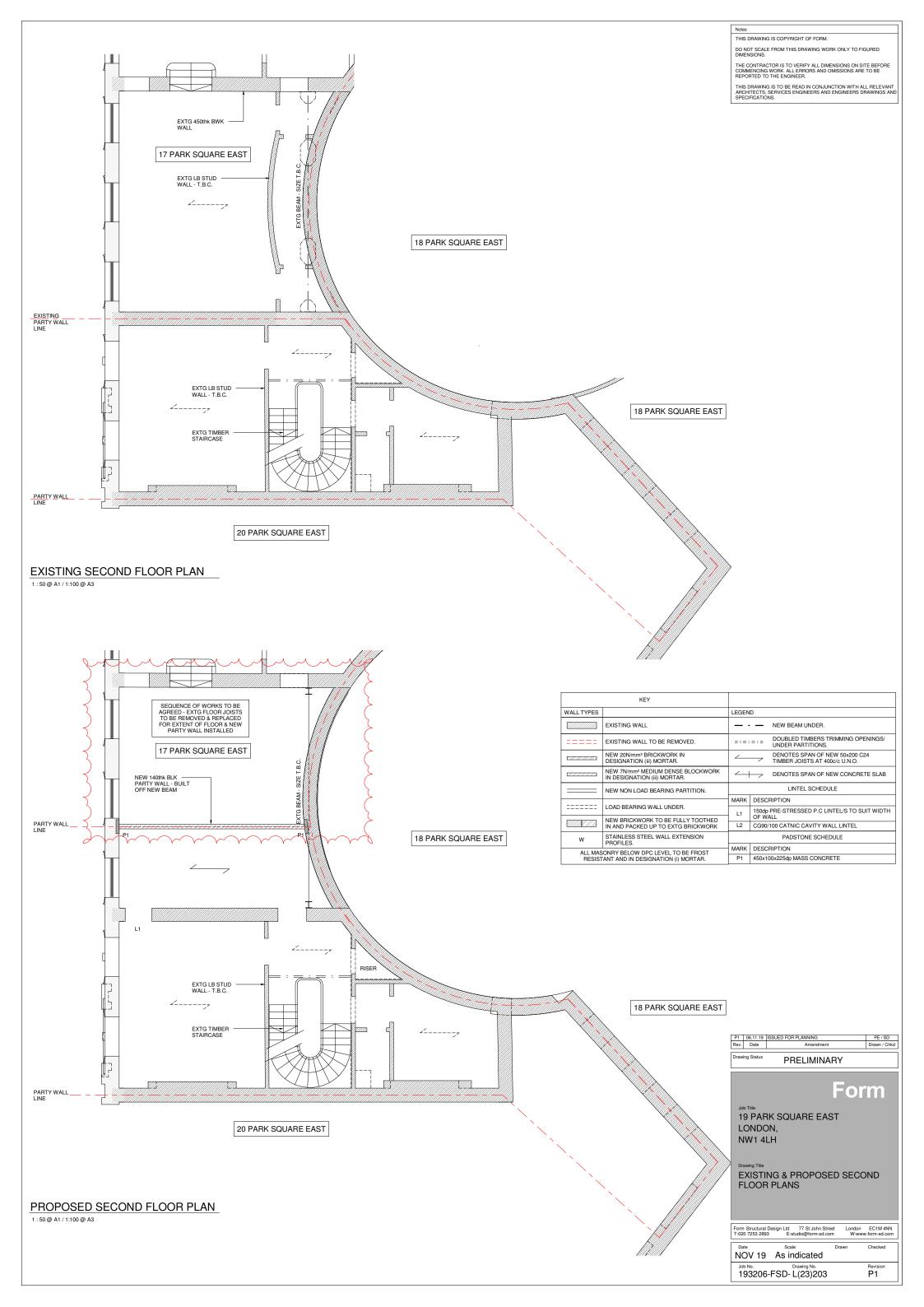


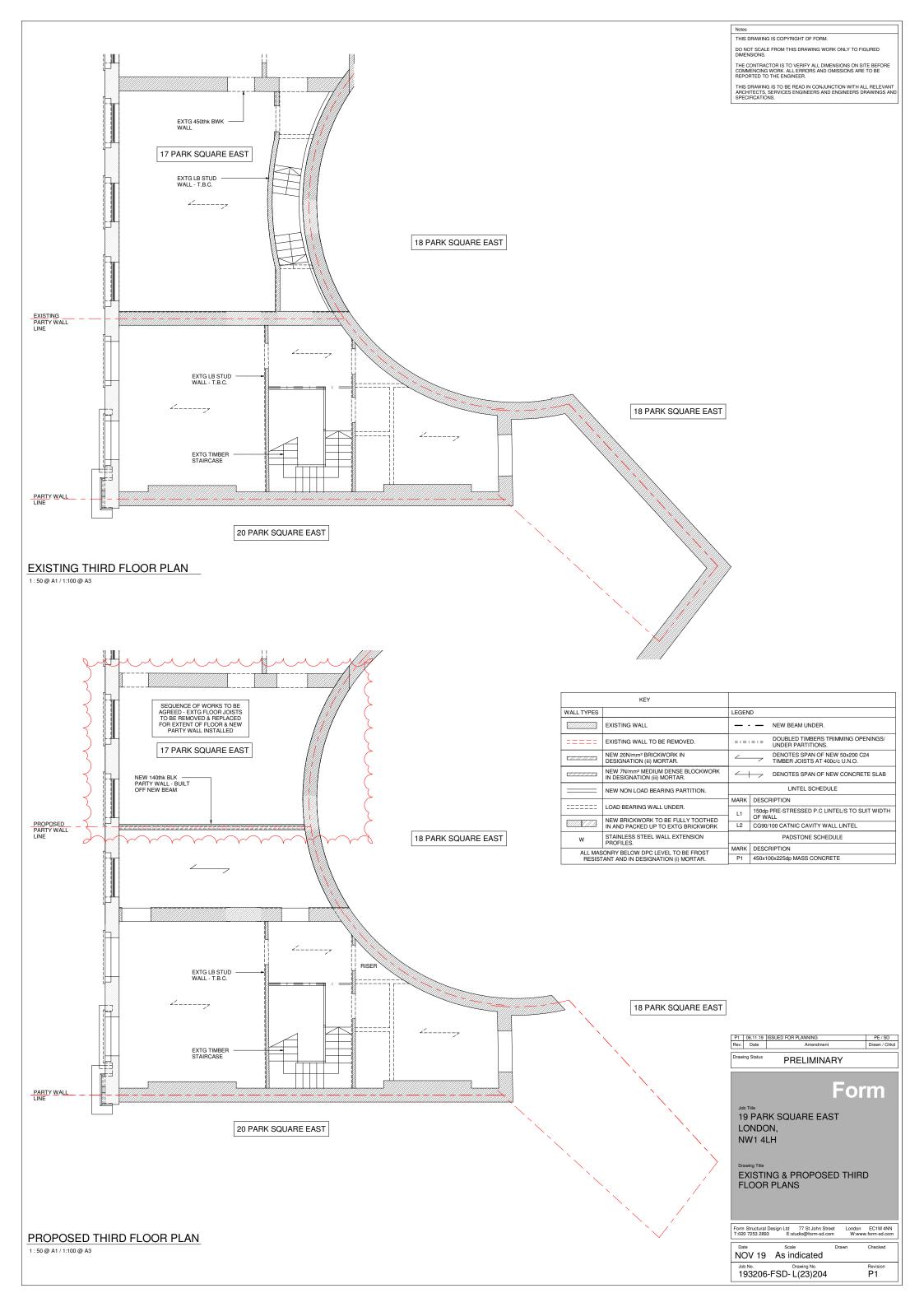
APPENDIX B PROPOSED DEVELOPMENT PLANS

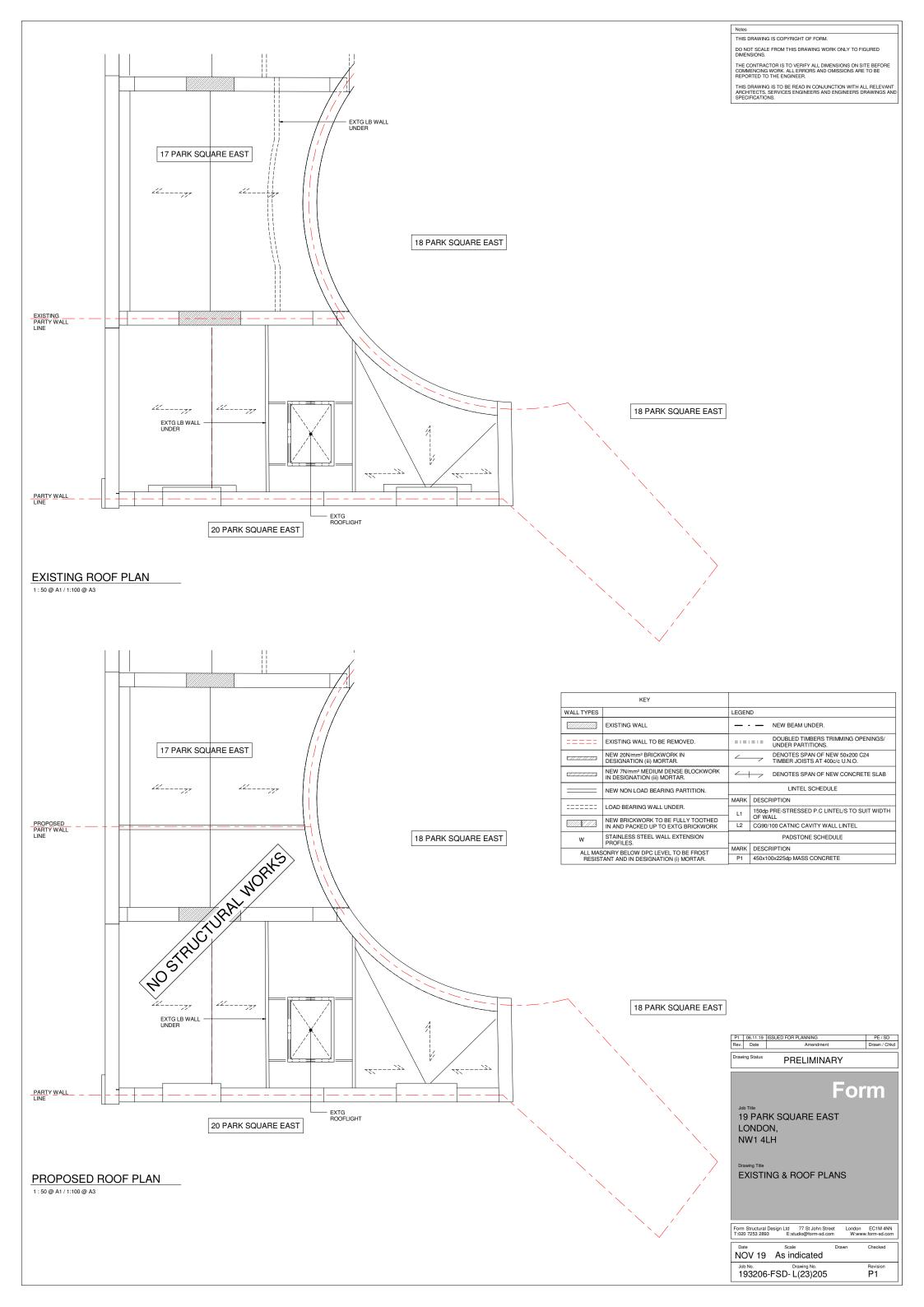














APPENDIX C ENVIROCHECK REPORT



APPENDIX D SITE INVESTIGATION LOGS

Client:	17 Parl East Lt					Square	Hole Di	ameter ((mm):	100 to 20.45	ōm	BOREHO	
Method: Cable Percussion							150 to 7.50m Casing Dia. (mm):			m	NUMBER		
Date Started: 14/10/2019 Co-ordinates					Ground Level		D.f.N.	1020015		3H01			
					1		(m	AOD)	28.50	Ref. No:	1038915	Sheet 1 o	f 3
Depth	II/Well Legend	Water Depth	Depth	iples Type	In Type	Situ Tests Results	Reduced Level (mAOD)	Depth & (Thickness) (m)		Desci	ription of Strata		Legend
(m)		(m)	(m) - 0.00 -	В	-		28.50	(0.25) -	Concrete.				
0.50			0.50	D	-		28.25	0.25		rounded,	gravelly CLAY. Go fine and medium r)		
			1.20	D	c [N = 4	25.00	(1.45)					+ + + + + + + + + + + + + + + + + + +
2.00	• •		- 1.70 - -2.00	D D	СП	N = 8	26.80	1.70 - (0.30) - 2.00	Soft, brow (Langley Si		ine sandy, silty C r)	LAY.	××
			2.50	D				- - - - -	sandy, bec	oming ver	nse, brown, sligh y sandy at 4m be angular to round	elow ground	
			-3.00 -3.00 - -4.00	D B	c	N = 8		- - - - -		t. Low cob	ble content of ro		
			3.50	D	- - -			- - - - - -					
			-4.00	D	С	N = 18		-					
			4.50	D				(5.20) -					
			-5.00 - - -	D	[c	N = 23		- - - - - - - -					
			-6.00 -6.00 - -7.00	D B	-			- - - - - -					
			6.50	D	c	N = 24		- - - - - -					
7.00	(w)		7.50	D	-		21.30	7.20	grey mottl	ed at 9m b	grey, becoming below ground lev	el, CLAY with	
		8.00	-8.00 	D	c	N = 12		- - - - - - -			Clay Formation)	pai uiigs.	
			-9.00	D	-			(2.80) -					
		9.50	9.50	D	c	N = 13		- - - - -					
	ral Ren ater str		7.5m ri	ising to	8m l	l pelow grou	ınd leve	ı after	20 minute	S.			<u> </u>
Driller:		LH				BORE	HOI F	RFCC)RD			F-4	FRUCTURE
Logged		JM				JOIL	Scale 1:					Giving or	ur all

Scale 1:50 See Key Sheet for explanation of symbols, etc.

The Diorama

FIG A1

Logged: Checked:

Appr'd:

JM

				Ltd, 19 na Esta		Square	Hole Di	ameter (mm):	100 to 20.45		BOREH		
Method: Cable Percussion							Casing	Dia. (mm	n):	150 to 7.50r	n	NUMB		
Date Started: 14/10/2019 Co-ordinates					Groun	nd Level		Τ.	400045	BH0				
Date St	arted:		2019 C	o-ordina	ites 			AOD)	28.50	Ref. No:	1038915	Sheet 2 o	of 3	
Backfil	l/Well	Water		nples	In	Situ Tests	Reduced	Depth &						
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	(Thickness) (m)			ription of Strata		Legend	
			-		-		18.50	10.00 -			y to closely fissu			
			10.50	D	-					fine and mo Clay Format	edium sand size	selenite.		
					-				(LONGON C	Sidy i Office	1011)			
			-11.00	D	c n	N = 18		-						
			11.00 - 12.00	В	-								F_=_	
								_					E- <u>-</u>	
			-		-			-						
					-]						
			-		-			-						
			12.50	D	СП	N = 19								
			-		-			-						
			-		ļ "			-					[-]	
			-		-			-					<u> </u>	
			13.50	D									E	
			-		ŀ									
			-		СП	N = 19		-						
			-		-			-						
			-		"			-						
													F_=_	
			-		-			_					E_=_	
								(10.45)						
			-		C	N = 24		-						
			-											
			-16.00 - 17.00	В										
			-		-			-						
													<u> </u>	
			-		-	N - 27		-					F=-	
					C	N = 27								
					<u> </u>			-						
			-		-								<u> </u>	
					-]					F_=_=	
			-		-								<u> </u>	
			-		c n	N = 25							<u> </u>	
			-					-					<u> </u>	
			[[[]						
			-		-			-						
			-		-									
			-		Ė			-						
			-		-]					<u> </u>	
	ral Rem							1 6	20					
1. Wa	ter stri	ike at S	∌.5m r	ising to	o 8m k	pelow grou	and leve	ei after	20 minute	es.				

Driller:	LH	BOREHOLE RECORD	INFRASTRUCTURE Giving our all
Logged:	JM	Scale 1:50 See Key Sheet for explanation of symbols, etc.	
Checked:	A	The Diorama	FIC A1
Appr'd:	Or	The Diorama	FIG A1

				Ltd, 19		Square	Hole Di	ameter (BOREHOLE				
				na Estat	e Ltd				n	NUMBER			
Method	d: Cab	le Percı	ussion				Casing	Dia. (mm):	150 to 7.50n		BH01	
Date St	arted:	14/10/2	2019 C	o-ordina	tes			nd Level AOD)	28.50	Ref. No:	1038915	Sheet 3 of	
Backfil	l/Well	Water	Sam	ples	In	Situ Tests	Reduced	Depth		<u> </u>			
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	& (Thickness) (m)		Descr	ription of Strata		Legend
20.00			-		. C	N = 28		-					
							8.05	20.45		End of E	Borehole at 20.45m		
					-								
					-]					
					[
					[]					
					[
					-								
					-								
					-								
					[
					[
					[
					[
			-										
			-		-			-					
					-								
					-			=					
			-		-								
					-			-					
								-					
					-			-					
			-		-								
					-								
					-								
			-		-			-					
					-								
					-								
			-		- -								
					- -								
					-								
					<u>-</u>								
	ral Ren ter str		9.5m ri	ising to	8m k	pelow grou	nd leve	el after	20 minute	es.			
Driller:		LH				BORE	HOLE	RECO	RD			INFRASTI Giving out	
Logged	:	JM				See Key Sheet	Scale 1:	:50				® Siving out	an

The Diorama

FIG A1

Checked:

Appr'd:

Client: 17 Park Square East Ltd, 19 Park Square East Ltd, The Diorama Estate Ltd								iameter (75mr	BOREHOLE NUMBER					
Metho	d: Win	dowles	ss Samp	oler						1		BH02		
Date St	arted:	21/10/2	2019 C	o-ordina	ites			nd Level AOD)	26.10	Ref. No:	1038915	Sheet 1 of	f 3	
Backfill/Well Water Samples In Situ 1						n Situ Tests	Reduced	Depth						
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (Thickness) (m) Description of Strata						Legend	
							26.10	(0.32)_	Concrete.					
			-				25.78	0.32	Dense to v	verv dense.	brown, very fir	ne to coarse		
0.50			-		-			-	sandy, loca	ally sandy G	GRAVEL of sub-r			
			-		-			-		fine to coar I Gravel Me				
1.00			-1.00 -	В	- s П	N = 58		-	, ,		·			
			2.00											
			-		ļ									
			-											
			-					-						
			-2.00 -	В	s n	N = 42								
			3.00		-									
			-											
			-											
			-					(-,,						
			-3.00 -	В	s n	N = 47		(5.18)						
			4.00											
								-						
								-						
			-4.00 - - 5.00	В	[s [N = 43		-						
			5.00]						
					[]									
								-						
			-5.00 - - 6.00	В	[s	N = 14								
			6.00		-]						
					ł U		20.60	5.50						
			-				20.60	(0.40)			grey CLAY with i	rare silty fine		
							20.20	5.90	sand parti (Weather	_	Clay Formation)			
6.00	- W		-6.00 - - 7.00	В	s	N = 25	20.20	3.50	Stiff, grey,	very closel	y to closely fissi	ured CLAY	<u> </u>	
			7.00					_		fine and me Clay Formati	edium sand size	selenite.		
6.50			-		ļ U			-	(,	,			
Genera	l Remark			<u> </u>	<u> </u>		1							
1. Grave	el transit	ioning t	to Clay a	at 5.0m k	oelow	ground level	, inferred	l from dr	op in SPT N v	alue.				
Driller:		AR				BORE	HOLE	RFCC)RD			INFRAST	RUCTURE	
Logged		JM	-			See Key Shee	Scale 1	:33				Giving ou	ır all	
Checke		K				See key silee						EIC A	,	
Appr'd:							ine	Diora	FIG A2					

Client:	17 Par East Lt	k Squar d, The	re East Dioran	Ltd, 19 na Estat	Park :	Square	Hole Di	iameter (r 75mm	BOREHOLE NUMBER					
Method	d: Win	ndowles	ss Samp	oler					rtuperii.o		10.75111	BH02		
Date St	arted:	21/10/2	2019 C	o-ordina	ites			Ground Level (m AOD) 26.10 Ref. No: 1038915				Sheet 2 of 3		
	ll/Well	Water	Sam	nples	In	Situ Tests	Reduced	Depth &						
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	(Thickness) (m)		Descr	ription of Strata	Legend		
												<u> </u>		
			- -7.00 -	В	- S _П	N = 24								
			- 8.00 -		-							<u> </u>		
			-											
			-		-									
			-		-							<u> </u>		
			- -8.00 -	В	s n	N = 26						<u> </u>		
			- 9.00 -		-							L		
			-					=				<u> </u>		
			-		-							<u> </u>		
					-									
			-9.00 -	В	s n	N = 24								
			10.00		-							<u> </u>		
												<u> </u>		
					-									
					-							E-E-		
			-10.00 -	В	s n	N = 29						<u> </u>		
			11.00											
			-											
					-			-				<u> </u>		
												<u> </u>		
			-11.00 - - 12.00	В	s	N = 33								
			12.00									<u> </u>		
												<u> </u>		
					-			-						
					-			-						
			-12.00 - - 13.00	В	[c	N = 38						<u> </u>		
			13.00					(12.55)				<u> </u>		
]				L		
					[]				E-E-		
					ŀ									
			-13.00 - - 14.00	В	s	N = 38								
General			<u> </u>			Tround lovel						<u> </u>		

1. Gravel transitioning to Clay at 5.0m below ground level, inferred from drop in SPT N value.

Driller:	AR	BOREHOLE RECORD	INFRASTRUCTURE Giving our all
Logged:	JM	Scale 1:33 See Key Sheet for explanation of symbols, etc.	
Checked:	A	The Diorama	FIG A2
Appr'd:	Or	The Diorama	FIG AZ

Client:				Ltd, 19 na Esta		Square	Hole Di	ameter (75mn	BOREHOLE NUMBER			
Metho	d: Win	dowles	s Samp	oler				751111	BH02			
Date Started: 21/10/2019 Co-ordinates								nd Level AOD)	26.10	Ref. No:	1038915	Sheet 3 of 3
Backfi	ll/Well	Water	Sam	ples	In	Situ Tests	Reduced	Depth		•		
Depth (m)	Legend	egend Depth (m) Depth Type Type Resul			Results	Level (mAOD)	& (Thickness) (m)		Desc	ription of Strata	Legend	
			-14.0015.0016.0017.0018.0016.0017.0018.00	В		N = 44 N = 52	7.65	18.45		End of	Borehole at 18.45m	
			-		-			_				
	l Remarl el transi		o Clay a	it 5.0m l	below (ground level,	inferred	from dro	op in SPT N v	/alue.		
Oriller:		AR				BOREI	HOLE	RECO	RD		CE	INFRASTRUCTURE Giving our all

Scale 1:33
See Key Sheet for explanation of symbols, etc.

The Diorama

FIG A2

Driller:

Logged:

Checked:

Appr'd:

JM

Or

Client: 17 Park Square East Ltd, 19 Park Square East Ltd, The Diorama Estate Ltd								ameter (BOREHOLE				
Method: Windowless Sampler								75n	o 20m	NUMBER BH03			
Date St	arted:	25/10/2	2019 C	o-ordina	ites		1	nd Level AOD)	30.10	Ref. No:	1038915	Sheet 1 of	f 4
Backfill/Well Water Samples In Situ Tests						Situ Tests	Reduced	Depth					
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	& (Thickness) (m)		ription of Strata		Legend	
	Legend			Type B B B	S	N = 4 N = 51 N = 50/160mm			slightly fin rounded, for content of (Made Grown of Made G	e gravel. k brown me to coarse fine	vith depth, brow is angular to rou	of angular to k. Low cobble vn, slightly unded, fine se sandy,	
			- -6.00 - - 7.00 - -	В	- S	N = 50		(5.90)_					
Genera	l Remark	KS:											
Drill		N 4\4/				מסחבי	וחור	DECC	NDD			INFRAST	RUCTURE
Driller: Logged		MW JM				BORE	Scale 1:	:33				Giving ou	
Checke	_	3101				See Key Sheet							
Appr'd:							The Diorama FIG A						

Client: 17 Park Square East Ltd, 19 Park Square East Ltd, The Diorama Estate Ltd				Hole Di	iameter (BOREHOLE							
Metho	d: Win	dowles	ss Samp	oler				/5n	nm tapering	with depth t	o 20m	NUMB BH03	
Date St	tarted:	25/10/2	2019 C	o-ordina	ites			nd Level AOD)	30.10	Ref. No:	1038915	Sheet 2 o	
Backfi	II/Well	Water	Sam	ples	In	Situ Tests	Reduced	Depth				1	
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	& (Thickness) (m)		Desci	ription of Strata		Legend
10.00	Remarl		-7.008.009.0010.0011.0012.0013.0014.00 -	B B B		N = 62 N = 50 N = 22 N = 25 N = 25	21.10	9.80 -	sand parti (Weathere Stiff, grey, with rare	ings. ed London very closel	grey CLAY with r Clay Formation) y to closely fissuedium sand size ion)	ured CLAY	
Jenera	. nemun												
Driller:		MW				BORE			DRD			INFRAST Giving or	TRUCTURE ur all
Logged: JM See Key Sheet						See Key Shee	Scale 1		ols, etc.			Siving of	un
Checked:						•	The Diorama					FIG A3	
Appr'd:							The Diorama					FIG A	3

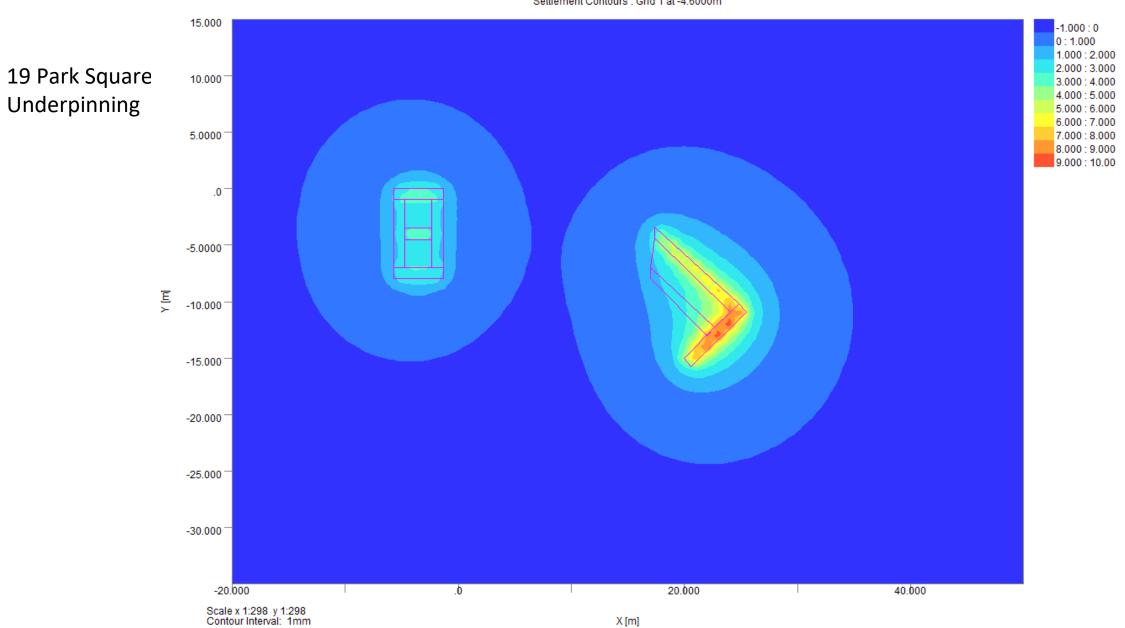
Client:	East Ltd, The Diorama Estate Ltd						Hole Diameter (mm): 75mm tapering with depth to 20m					BOREHOLE NUMBER		
Metho	d: Win	idowles	s Samp	oler				, 51111			20111	BH03	.11	
Date St	arted:	25/10/2	2019 C	o-ordina	ites			nd Level AOD)	30.10	Ref. No:	1038915	Sheet 3 of	4	
Backfi	ll/Well	Water	San	nples	In	Situ Tests	Reduced	Depth						
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	& (Thickness) (m)		Descr	iption of Strata		Legend	
			[["			-						
					-									
			-		_									
			-14.00 -	В	s _[N = 42								
			- 15.00 -											
			-											
			-		"									
					-									
			-		-			(10.20)						
			-15.00 -	В	[s []	N =50/95mm		(10.20)						
			16.00											
			-		-			-						
			-		-								<u></u>	
			-		-									
			-16.00 -	В	-								<u></u>	
			17.00		_									
			-											
			-		-								<u></u>	
			-		-								<u></u>	
			-		-									
			- -17.00 -	В	- 5 -	N = 21								
			18.00			N = 21								
					-									
			_		ł U									
			-		-									
					-									
			18.00	В	-									
			-18.00 - - 19.00	В	-			1 7						
					-									
			-					+						
								-						
			-		-								<u></u>	
			10.00			N 22		-						
			-19.00 - - 20.00	В	S	N = 33								
			-		- [
			-											
			-		-									
Genera	l Remari	ks:												
Driller:		MW				BORE		RECO	RD			INFRASTE Giving our		
Logged: JM See Key Sheet f						See Kev Shee	Scale 1		s, etc.			s Siving our		
Checked:										FIC AS				
Appr'd:							ıne	Diorar		FIG A3	•			

Client: 17 Park Square East Ltd, 19 Park Square East Ltd, The Diorama Estate Ltd						Square	Hole Di	iameter (n	BOREHOLE					
	d: Win						75mm tapering with depth to 20m					NUMBER		
Date St	arted:	25/10/2	2019 C	o-ordina	ites			nd Level AOD)	30.10	Ref. No:	1038915	BH03 Sheet 4 of	4	
Backfi	ll/Well	Water	Sam	nples	In	Situ Tests	Reduced	Depth						
Depth (m)	Legend	Depth (m)	Depth (m)	Туре	Туре	Results	Level (mAOD)	& (Thickness) (m)		Descr	ription of Strata		Legend	
					-		10.10	20.00						
			-		-		10.10	20.00		End of E	Borehole at 20.00m			
			-											
			-		-									
			-											
			-											
			-		-									
			-											
			_		-			-						
			_		[
			-		-									
			-		-									
			-											
			-		-									
			-											
			-											
			-											
			-											
			-											
			-											
					ŀ									
			-]						
			_		-									
			-											
			-											
			-		-									
					ŀ									
			-		-									
					[7					ļ	
			-		-									
			-		ļ									
			-		<u> </u>									
			-		}									
			-		-			-						
					[
Com	l D - · · · · ·	<u> </u>					1							
Genera	l Remarl	(5]												
Driller:		MW				BORE		RECOF	RD		CE	INFRAST Giving ou		
Logged		JM				See Key Shee	Scale 1 t for explana	:33 tion of symbols	s, etc.			© ®		
Checke		W					The	Diorar	ma			FIG A3	3	
Appr'd:		Or											-	

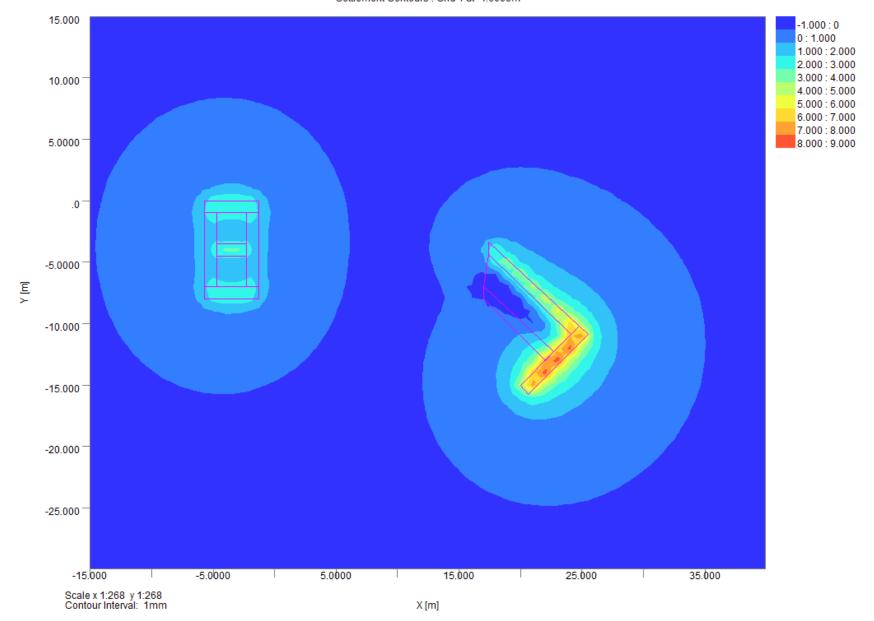


APPENDIX E PDISP EXPORTS

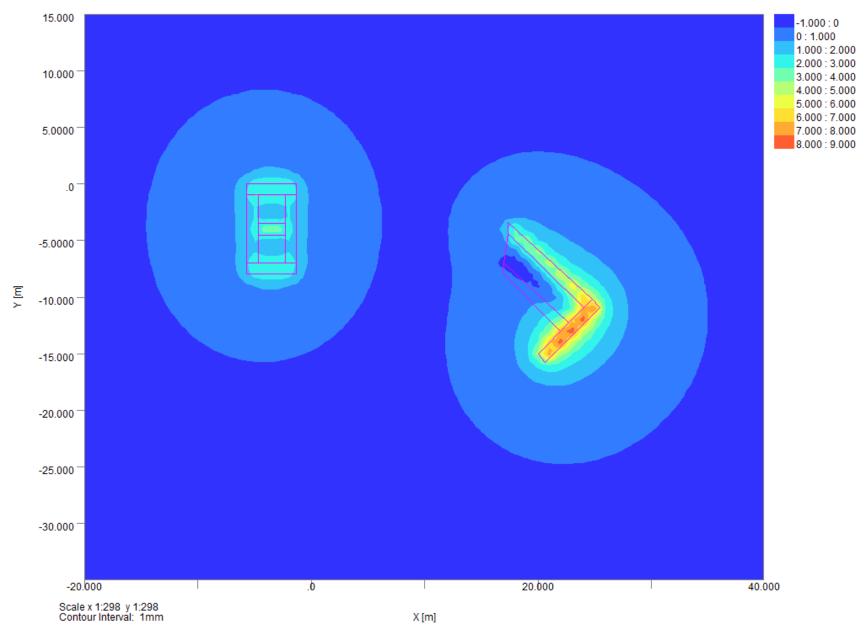
Settlement Contours: Grid 1 at -4.6000m



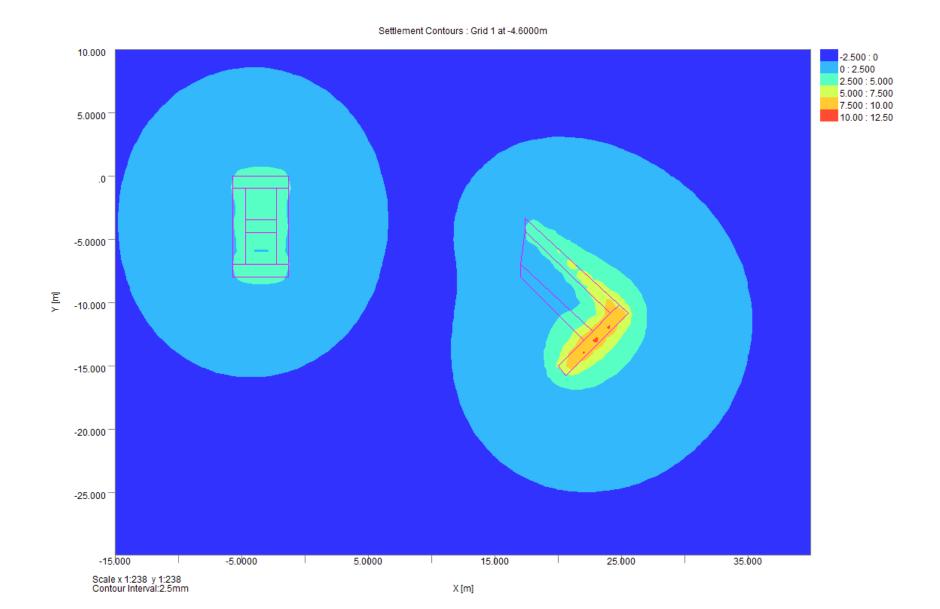




19 Park Square Basement Slab



19 Park Square Total Settlement (inc. Long Term)



Oasys Ltd.

The Diorama

19 Park Square East Stage 1

File PDisp 19 Park Square East Stage 1.pdd

Exported 06/05/20 21:36:35

PDisp 20.0.0.12 64bit Copyright © Oasys 1997-2019

Titles

START_TABLE

Job No.: 1038915

The

Job Title: Diorama

19 Park

Sub-title: Square East

Calculation

Heading: Stage 1 Initials:

Checker:

Date Saved:

Date Checked:

Notes:

PDisp 19 Park Square East Stage

File Name:

1.pdd

G:\Projects\ Projects 2019\10389 15 - The Diorama, London (LON)\Repo rts\BIA\No.

File Path: 19

END_TABLE

History

START_TABLE

Time Date Ву Notes

18-Dec-19	12:29 jmaness	New
18-Dec-19	16:02 jmaness	
18-Dec-19	16:32 jmaness	
18-Dec-19	16:46 jmaness	
15-Jan-20	17:21 jmaness	
15-Jan-20	17:52 jmaness	
15-Jan-20	18:04 jmaness	
16-Jan-20	10:57 jmaness	
16-Jan-20	21:11 jmaness	
20-Jan-20	18:05 jmaness	
13-Feb-20	16:08 jmaness	
13-Feb-20	16:17 jmaness	
13-Feb-20	17:52 jmaness	
25-May-20	12:19 jmaness	
27-May-20	13:49 jmaness	
27-May-20	13:55 jmaness	
29-May-20	14:56 jmaness	
05-Jun-20	21:35 jmaness	

Analysis Options

General

Global Poisson's ratio: 0.50

Maximum allowable ratio between values of E: 1.5

Horizontal rigid boundary level: 7.65 [m OD]

Displacements at load centroids: Yes

GSA piled raft data

: No

Elastic

Elastic : Yes

Analysis: Boussinesq

Consolidation

Consolidation : No

Soil ProfilesSoil Profile 1

Number intermedi

Youngs Youngs

Level at displacem Modulus : Modulus : Poissons Non-linear Layer ref. Name top ent levels Top Btm. . [mOD] [kN/m²] [kN/m²] Langley Silt 1 Member 29 3 9600 9600 0.2 None Lynch Hill Gravel 2 Member 26.5 10 60000 60000 0.3 None London Clay

27

59000

59000

0.5 None

21.3

END_TABLE

Non-linear Curve Coordinates - Nonlinear Curve 1

START_TABLE

Point Strain [%] Factor

3 Formation

END_TABLE

Soil Zones

START_TABLE

Profile Zone Name X min X max Y min Y max [m]

[m] [m] [m]

Soil

1 Soil Zone 1 -100 100 -100 100 Profile 1

END_TABLE

Polygonal Load

START_TABLE

Position : Position: Polygon: No. of

Value :

Position: Polygon: Rect. Rectangle Normal Load ref. Name Level Coords. tolerance s (local z) [%] [kN/m²]

[m] [m] (17,-8) (17,-7) (22.7,-12.3) (22,-

1 A 6 19.8

25 13) 10 (20, -15)(20.6,-15.8) (25.5,-10.9) (24.8,-10.2) (24.1,-10.9) (22.7,-

2 B 25 12.3) 10 320

	(24.1,- 10.9)			
	(24.8,-			
	10.2)			
	(17.4,-3.4)			
3 C	25 (17.4,-4.4)	10	6	226.6
3 0	(17.4,-4.4)	10	Ü	220.0
	(17,-7)			
	(22.7,-			
	12.3)			
	(24.1,-			
4 D	26 10.9)	10	6	0
	(-1.33,-8)			
	(-5.73,-8)			
Vault South	(-5.73,-7)			
5 Wall	24.4 (-1.33,-7)	10	1	119
	(-1.33,-7)			
	(-2.33,-7)			
Vault East	(-2.33,-1)			
6 Wall	24.4 (-1.33,-1)	10	1	32
	(-5.73,-7)			
	(-4.73,-7)			
Vault West	(-4.73,-1)			
7 Wall	24.4 (-5.73,-1)	10	1	32
	(-1.33,-1)			
	(-1.33,-0)			
Vault North	(-5.73,-0)			
8 Wall	24.4 (-5.73,-1)	10	1	133
	(-2.33,-			
	4.5) (-			
Marile.	2.33,-3.5)			
Vault	(-4.73,-			
Dividing 9 Wall	3.5) (-	10	1	119
9 wan	24.4 4.73,-4.5) (-2.33,-	10	1	119
	(-2.53,- 4.5) (-			
Vault	4.3) (- 2.33,-7) (-			
Excavation	4.73,-7) (-			
10 (North)	25 4.73,-4.5)	10	1	0
10 (1401111)	(-2.33,-	10	-	O
	3.5) (-			
Vault	2.33,-1) (-			
Excavation	4.73,-1) (-			
11 (South)	25 4.73,-3.5)	10	1	0
	. ,			

Polygonal Loads' Rectangles

START_TABLE

Angle of local x from

No. Centre : x Centre : y global X Width x Depth y [m] [m] [Degrees] [m] [m]

Load 1 : A

(Edge 2 optimal)

19.6 -10.1 45 0.70711 7.4246 20 -10 45 0.056569 7.0004 2 20.6 -10.5 45 0.056569 5.4447 3 45 0.056569 21.2 3.8891 4 -11 5 21.8 -11.5 45 0.056569 2.3335 22.4 -12 45 0.056569 0.77782

Load 2 : B

(Edge 3 optimal)

1 22.7 -13 135 0.98995 6.8589

Load	2	\boldsymbol{c}

(Edge 2 optimal)						
(Luge 2 openius)	1 2 3 4 5 6	21 17.6 17.6 17.5 17.5	-7.3 -4.1 -3.9 -3.8 -3.6 -3.5	137.42 137.42 137.42 137.42 137.42 137.42	9.3315 0.13533 0.13533 0.13533 0.13533 0.13533	0.8627 0.66269 0.51543 0.36816 0.2209 0.073633
Load 4 : D						
(Edge 4 optimal)	1 2 3 4 5 6	20.6 17.7 17.6 17.6 17.5	-8.9 -6 -5.7 -5.3 -4.9	135.87 135.87 135.87 135.87 135.87	7.7816 0.30466 0.30466 0.30466 0.30466 0.30466	2.0622 1.9302 1.5013 1.0723 0.64339 0.21446
Load 5 : Vault South Wall						
(Edge 2 optimal)	1	-3.5	-7.5	-180	4.4	1
Load 6 : Vault Ea Wall	est					
(Edge 2 optimal)	1	-1.8	-4	-180	1	6
Load 7 : Vault West Wall						
(Edge 1 optimal)	1	-5.2	-4	0	1	6
Load 8 : Vault North Wall						
(Edge 1 optimal)	1	-3.5	-0.5	90	1	4.4
Load 9 : Vault Dividing Wall						
(Edge 1 optimal)	1	-3.5	-4	90	1	2.4
Load 10 : Vault Excavation (Nort	th)					
(Edge 2 optimal)	1	-3.5	-5.8	-90	2.5	2.4
Load 11 : Vault Excavation (Sout	th)					
(Edge 1 optimal)	1	-3.5	-2.3	90	2.5	2.4
END_TABLE						
Displacement						

Displacement Lines

START_TABLE									Detailed
Name	X1 [m]	Y1 [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]		Intervals Calculate [No.]	Results
20 Park Square East Rear		17	-8	25.6	17	-16	25.6	16 Yes	Yes
20 Park Square East South		17	-8	25.6	1	-8	25.6	32 Yes	Yes
The Diorama South West		20.6	-15.8	27.1	28.4	-23.6	27.1	22 Yes	Yes
Floor Slab		17	-6	26	23	-11.6	26	16 Yes	Yes

East Rear -1.3 -8 25.4 -1.3 -13 25.4 10 Yes Yes 18 PSE Front -5.7 0 25.4 -5.7 5 25.4 10 Yes Yes 18 PSE Rear -1.3 0 25.4 -1.3 5 25.4 10 Yes Yes 0 18 PSE South 0 25.6 17 0 25.6 34 Yes Yes Vault Area -3.5 -1 25 -3.5 -7 25 12 Yes Yes

-5.7

-13

-4

25.4

29

10 Yes

20 Yes

Stress:

Yes

Yes

25.4

Park Square East

-15.7

29

END_TABLE

Road

20 Park Square

East Front Wall

20 Park Square

-5.7

-5.7

-8

-4

Displacement Grids

START_TABLE

										Ext	rusion:	
	Extrusion:							Inter	als Extrusio	n: Inte	ervals	Detailed
Name	Direction	X1	Y1	Z1	X2	Y2	Z2	Alon	Line Distance	e Alo	ng Calculat	e Results
		[m]	[m]	[m]	[m]	[m]	[m]	[No.]	[m]	[No	0.]	
Grid 1	Global X		-50	-50	25.3 -		50	25.3	100	100	100 No	No

END_TABLE

Results : Immediate : Load Centres : Polygonal

START_TABLE

Stress: Stress: Sum Ref. Name z dz Calc. Level Vertical Princ. Vert. Strain [m] [mOD] [mm] [mOD] $[kN/m^2]$ [kN/m²] [19.8 -10.2 25 1 A 3 24.769 18.896 47.841 1.70E-04

2 B		22.7	-13	25	10.3	24.769	309.33	695.08	0.0032268
3 C		21.1	-7.4	25	7.2	24.769	215.68	467.44	0.0023359
4 D		20.3	-8.6	26	3.5	25.765	0	0	0
Vai	ult South								
5 Wa	all ult East	-3.5	-7.5	24.4	3.8	24.142	113.78	248.7	0.0012217
6 Wa	all	-1.8	-4	24.4	2.5	24.142	32.508	89.377	2.57E-04
Vai	ult West								
7 Wa	all	-5.2	-4	24.4	2.5	24.142	32.508	89.338	2.58E-04
Vai	ult North								
8 Wa		-3.5	-0.5	24.4	4.2	24.142	127.16	277.57	0.0013673
Div	riding								
9 Wa Vai		-3.5	-4	24.4	4	24.142	113.68	247.12	0.0012276
Exc	cavation								
10 (No Vai		-3.5	-5.8	25	2.1	24.769	2.36E-06	0.027612	-1.38E-07
Exc	cavation								
11 (So	outh)	-3.5	-2.3	25	2.2	24.769	2.09E-06	0.025468	-1.27E-07

Results:
Consolidation:
Load Centres:
Polygonal

None

Results : Total : Load Centres : Polygonal

None

Results: Immediate: Displacement Data: Lines

o.,							•		Character	Stress:		
Ref.	Name	x [m]	y [m]	z [mOD]	dz [mm]	С	alc. Level	Stress: Vertical [kN/m²]	Sum Princ. [kN/m²]	Vert. Strai	n
	20 Park Square East											
	1 Rear 20 Park Square East		17	-8	25.6	=	1.7	25.361		0	0	0
	1 Rear 20 Park Square East		17	-8.5	25.6	:	1.5	25.361		0	0	0
	1 Rear 20 Park Square East		17	-9	25.6	:	1.4	25.361		0	0	0
	1 Rear 20 Park Square East		17	-9.5	25.6	:	1.4	25.361		0	0	0
	1 Rear		17	-10	25.6	:	1.3	25.361		0	0	0

20.5								
20 Park Square East								
1 Rear	17	-10.5	25.6	1.3	25.361	0	0	0
20 Park								
Square East								
1 Rear	17	-11	25.6	1.2	25.361	0	0	0
20 Park								
Square East								
1 Rear	17	-11.5	25.6	1.2	25.361	0	0	0
20 Park								
Square East	17	12	25.6	1.2	25.261	0	^	0
1 Rear 20 Park	17	-12	25.6	1.2	25.361	0	0	0
Square East								
1 Rear	17	-12.5	25.6	1.1	25.361	0	0	0
20 Park	-/	12.5	23.0		25.501	Ü	Ü	Ü
Square East								
1 Rear	17	-13	25.6	1.1	25.361	0	0	0
20 Park								
Square East								
1 Rear	17	-13.5	25.6	1.1	25.361	0	0	0
20 Park								
Square East								
1 Rear	17	-14	25.6	1	25.361	0	0	0
20 Park								
Square East	47	445	25.6		25.264	0	•	
1 Rear 20 Park	17	-14.5	25.6	1	25.361	0	0	0
Square East								
1 Rear	17	-15	25.6	0.9	25.361	0	0	0
20 Park	-/	13	23.0	0.5	25.501	Ü	Ü	Ü
Square East								
1 Rear	17	-15.5	25.6	0.9	25.361	0	0	0
20 Park								
Square East								
1 Rear	17	-16	25.6	0.8	25.361	0	0	0
20 Park								
Square East	4-		25.6	4.7	25.264	•		
2 South	17	-8	25.6	1.7	25.361	0	0	0
20 Park								
Square East								
2 South	16.5	-8	25.6	1.3	25.361	0	0	0
2 334	10.0	Ü	25.0	1.0	25.502	· ·	Ü	·
20 Park								
Square East								
2 South	16	-8	25.6	1.1	25.361	0	0	0
20 Park								
Square East								
2 South	15.5	-8	25.6	0.9	25.361	0	0	0
20 Park								
Square East 2 South	15	-8	25.6	0.8	25.361	0	0	0
2 300111	13	-0	23.0	0.6	23.301	U	U	U
20 Park								
Square East								
2 South	14.5	-8	25.6	0.6	25.361	0	0	0
20 Park								
Square East								
2 South	14	-8	25.6	0.5	25.361	0	0	0
20 Park								
Square East								
2 South	13.5	-8	25.6	0.4	25.361	0	0	0
20 Da -1								
20 Park								
Square East	12	_0	25 F	0.4	25 261	0	0	0
2 South	13	-8	25.6	0.4	25.361	0	0	0

20 Park Square East 2 South 12.5 -8 25.6 0.3 25.361 0 0 0 20 Park Square East 2 South 12 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 0 20 Park Square East 2 South 8 25.6 0 25.361 0 0 0 0 20 Park Square East 2 South 8 25.6 0 25.361 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
2 South 12.5 -8 25.6 0.3 25.361 0 0 0 20 Park Square East 2 South 12 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0	
20 Park Square East 2 South 12 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
Square East 2 South 12 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
Square East 2 South 12 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
2 South 12 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
20 Park Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2	
Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	0 0
Square East 2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	0 0
2 South 11.5 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0	0 0
20 Park Square East 2 South 11 -8 25.6 0.2 25.361 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	0 0
Square East 2 South 11 -8 25.6 0.2 25.361 0 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	0 0
2 South 11 -8 25.6 0.2 25.361 0 0 20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	0 0
20 Park Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	0 0
Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	0 0
Square East 2 South 10.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	0 0
2 South 10.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	0 0
20 Park Square East 2 South 10 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	0 0
Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
Square East 2 South 10 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
2 South 10 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
20 Park Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
Square East 2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
2 South 9.5 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 2 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	0 0
Square East 2 South 9 -8 25.6 0.1 25.361 0 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 2 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 0	
2 South 9 -8 25.6 0.1 25.361 0 0 20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
20 Park Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	0 0
Square East 2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
2 South 8.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
20 Park Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0	
Square East 2 South 8 -8 25.6 0 25.361 0 0 2 20 Park Square East 2 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East 2 2 South 7.5 -8 25.6 0 25.361 0 0	0
Square East 2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East	
2 South 8 -8 25.6 0 25.361 0 0 20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East	
20 Park Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East	0 0
Square East 2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East	
2 South 7.5 -8 25.6 0 25.361 0 0 20 Park Square East	
20 Park Square East	
Square East	0 0
Square East	
2 South 7 -8 25.6 0 25.361 0 0	0
20 Park	
20 Park Square East	
2 South 6.5 -8 25.6 0 25.361 0 0	0 0
_ 555 5.5 6 £5.0 6 £5.301 0 U	, 0
20 Park	
Square East	
2 South 6 -8 25.6 0.1 25.361 0 0	0 0
20 Park	
Square East	
2 South 5.5 -8 25.6 0.1 25.361 0 0	0 0
20 Park	
20 Park Square East	
2 South 5 -8 25.6 0.1 25.361 0 0	
2 350ddii) 0
20 Park	0 0
Square East) 0
2 South 4.5 -8 25.6 0.1 25.361 0 0) 0
•	
20 Park	
Square East	
2 South 4 -8 25.6 0.1 25.361 0 0	0 0
	0 0

20 Park Square East								
2 South	3.5	-8	25.6	0.2	25.361	0	0	0
20 Park Square East								
2 South	3	-8	25.6	0.2	25.361	0	0	0
20 Park Square East								
2 South	2.5	-8	25.6	0.3	25.361	0	0	0
20 Park								
Square East 2 South	2	-8	25.6	0.3	25.361	0	0	0
20 Park								
Square East 2 South	1.5	-8	25.6	0.4	25.361	0	0	0
20 Park								
Square East 2 South	1	-8	25.6	0.5	25.361	0	0	0
The	_	J	25.0	0.5	25.502	· ·	Ü	· ·
Diorama 3 South West	20.6	-15.8	27.1	4	26.8	0	0	0
	20.6	-13.6	27.1	4	20.0	U	U	U
The Diorama								
3 South West	21	-16.2	27.1	2.9	26.8	0	0	0
The Diorama								
3 South West	21.3	-16.5	27.1	2.3	26.8	0	0	0
The Diorama								
3 South West	21.7	-16.9	27.1	1.9	26.8	0	0	0
The Diorama								
3 South West	22	-17.2	27.1	1.6	26.8	0	0	0
The Diorama								
3 South West	22.4	-17.6	27.1	1.3	26.8	0	0	0
The Diorama								
3 South West	22.7	-17.9	27.1	1.1	26.8	0	0	0
The Diorama								
3 South West	23.1	-18.3	27.1	0.9	26.8	0	0	0
The Diorama								
3 South West	23.4	-18.6	27.1	0.8	26.8	0	0	0
The								
Diorama 3 South West	23.8	-19	27.1	0.7	26.8	0	0	0
The								
Diorama 3 South West	24.1	-19.3	27.1	0.6	26.8	0	0	0
The								
Diorama 3 South West	24.5	-19.7	27.1	0.5	26.8	0	0	0
5 Journ West	24.3	-15./	27.1	0.5	20.0	U	U	U

The Diorama 3 South West	24.9	-20.1	27.1	0.4	26.8	0	0	0
The Diorama 3 South West	25.2	-20.4	27.1	0.3	26.8	0	0	0
The Diorama	25.6	20.0	27.1	0.2	26.8	0	0	0
3 South West The Diorama	25.6	-20.8	27.1	0.3	26.8	0	0	0
3 South West	25.9	-21.1	27.1	0.2	26.8	0	0	0
Diorama 3 South West	26.3	-21.5	27.1	0.2	26.8	0	0	0
The Diorama 3 South West	26.6	-21.8	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	27	-22.2	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	27.3	-22.5	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	27.7	-22.9	27.1	0	26.8	0	0	0
The Diorama 3 South West	28	-23.2	27.1	0	26.8	0	0	0
The Diorama 3 South West	28.4	-23.6	27.1	0	26.8	0	0	0
4 Floor Slab	17	-6	26	1.9	25.765	0	0	0
4 Floor Slab	17.4	-6.3	26	2.1	25.765	0	0	0
4 Floor Slab	17.8	-6.7	26	2.3	25.765	0	0	0
4 Floor Slab	18.1	-7	26	2.5	25.765	0	0	0
4 Floor Slab	18.5	-7.4	26	2.6	25.765	0	0	0
4 Floor Slab	18.9	-7.8	26	2.8	25.765	0	0	0
4 Floor Slab	19.3	-8.1	26	2.9	25.765	0	0	0
		-0.1						
4 Floor Slab	19.6	-8.4	26	3.1	25.765	0	0	0
4 Floor Slab 4 Floor Slab				3.1	25.765 25.765	0	0	0
	19.6	-8.4	26					
4 Floor Slab	19.6 20	-8.4 -8.8	26 26	3.2	25.765	0	0	0
4 Floor Slab	19.6 20 20.4	-8.4 -8.8 -9.2	26 26 26	3.2 3.4	25.765 25.765	0	0	0
4 Floor Slab 4 Floor Slab 4 Floor Slab	19.6 20 20.4 20.8	-8.4 -8.8 -9.2 -9.5	26 26 26 26	3.2 3.4 3.5	25.765 25.765 25.765	0 0 0	0 0 0	0 0 0
4 Floor Slab 4 Floor Slab 4 Floor Slab 4 Floor Slab	19.6 20 20.4 20.8 21.1	-8.4 -8.8 -9.2 -9.5	26 26 26 26 26	3.2 3.4 3.5 3.7	25.765 25.765 25.765 25.765	0 0 0	0 0 0	0 0 0
4 Floor Slab	19.6 20 20.4 20.8 21.1 21.5	-8.4 -8.8 -9.2 -9.5 -9.8	26 26 26 26 26 26	3.2 3.4 3.5 3.7	25.765 25.765 25.765 25.765 25.765	0 0 0 0	0 0 0 0 0	0 0 0 0

4 Floor Slab	22.6	-11.3	26	5.5	25.765	0	0	0	
							_	_	
4 Floor Slab	23	-11.6	26	6.8	25.765	0	0	0	
20 Park									
Square East									
5 Front Wall	-5.7	-8	25.4	1.9	25.144	0	0	0	
20 Park									
Square East									
5 Front Wall	-5.7	-8.5	25.4	1.3	25.144	0	0	0	
20.5									
20 Park Square East									
5 Front Wall	-5.7	-9	25.4	1	25.144	0	0	0	
		-		_		-	-	-	
20 Park									
Square East		0.5	25.4	0.0	25 4 4 4	•	•	2	
5 Front Wall	-5.7	-9.5	25.4	0.8	25.144	0	0	0	
20 Park									
Square East									
5 Front Wall	-5.7	-10	25.4	0.6	25.144	0	0	0	
20 Park									
Square East									
5 Front Wall	-5.7	-10.5	25.4	0.5	25.144	0	0	0	
20 Paul									
20 Park Square East									
5 Front Wall	-5.7	-11	25.4	0.4	25.144	0	0	0	
20 Park									
Square East 5 Front Wall	-5.7	-11.5	25.4	0.3	25.144	0	0	0	
5 FIOHE Wall	-5.7	-11.5	25.4	0.5	25.144	U	U	U	
20 Park									
Square East									
5 Front Wall	-5.7	-12	25.4	0.2	25.144	0	0	0	
20 Park									
Square East									
5 Front Wall	-5.7	-12.5	25.4	0.2	25.144	0	0	0	
20 Park									
Square East									
5 Front Wall	-5.7	-13	25.4	0.2	25.144	0	0	0	
20 Park									
Square East									
6 Rear	-1.3	-8	25.4	1.8	25.144	0	0	0	
20 Park Square East									
6 Rear	-1.3	-8.5	25.4	1.2	25.144	0	0	0	
20 Park	2.5	0.5				Ü	-	Ü	
Square East									
6 Rear	-1.3	-9	25.4	1	25.144	0	0	0	
20 Park									
Square East 6 Rear	-1.3	-9.5	25.4	0.8	25.144	0	0	0	
20 Park	-1.5	-3.3	23.4	0.6	ZJ.144	U	U	J	
Square East									
6 Rear	-1.3	-10	25.4	0.6	25.144	0	0	0	

0 0 0
0
0
0
0
0
0
0
0
0
0
0
0
0
0
U
0
0
0
U
0
0
0
O
0
0
0
0
_
0
0
0
0 0 0
0 0 0
0 0 0
0 0 0
0 0 0 0 0
0 0 0 0 0 0 0
0 0 0 0 0
0 0 0 0 0 0 0
0 0 0 0 0 0 0 0

10 DCE								
18 PSE 9 South	3	0	25.6	0.2	25.361	0	0	0
18 PSE	2.5		25.6		25.264	•		
9 South 18 PSE	3.5	0	25.6	0.2	25.361	0	0	0
9 South	4	0	25.6	0.1	25.361	0	0	0
18 PSE 9 South	4.5	0	25.6	0.1	25.361	0	0	0
18 PSE	4.5	O	25.0	0.1	25.501	O	Ü	Ü
9 South	5	0	25.6	0.1	25.361	0	0	0
18 PSE 9 South	5.5	0	25.6	0.1	25.361	0	0	0
18 PSE								
9 South 18 PSE	6	0	25.6	0	25.361	0	0	0
9 South	6.5	0	25.6	0	25.361	0	0	0
18 PSE 9 South	7	0	25.6	0	25.361	0	0	0
18 PSE	,	O	25.0	O	25.501	O	Ü	Ü
9 South	7.5	0	25.6	0	25.361	0	0	0
18 PSE 9 South	8	0	25.6	0	25.361	0	0	0
18 PSE								
9 South 18 PSE	8.5	0	25.6	0	25.361	0	0	0
9 South	9	0	25.6	0	25.361	0	0	0
18 PSE 9 South	9.5	0	25.6	0	25.361	0	0	0
18 PSE	9.5	O	23.0	O	25.501	U	O	O
9 South	10	0	25.6	0	25.361	0	0	0
18 PSE 9 South	10.5	0	25.6	0	25.361	0	0	0
18 PSE								
9 South 18 PSE	11	0	25.6	0	25.361	0	0	0
9 South	11.5	0	25.6	0	25.361	0	0	0
18 PSE 9 South	12	0	25.6	0.1	25.361	0	0	0
18 PSE	12	U	23.0	0.1	23.301	U	U	U
9 South	12.5	0	25.6	0.1	25.361	0	0	0
18 PSE 9 South	13	0	25.6	0.1	25.361	0	0	0
18 PSE								
9 South 18 PSE	13.5	0	25.6	0.1	25.361	0	0	0
9 South	14	0	25.6	0.2	25.361	0	0	0
18 PSE 9 South	14.5	0	25.6	0.2	25.361	0	0	0
18 PSE	14.5	Ü	25.0	0.2	25.501	Ü	Ü	ŭ
9 South 18 PSE	15	0	25.6	0.2	25.361	0	0	0
9 South	15.5	0	25.6	0.2	25.361	0	0	0
18 PSE	4.5	0	25.6	0.2	25.264	0		0
9 South 18 PSE	16	0	25.6	0.3	25.361	0	0	0
9 South	16.5	0	25.6	0.3	25.361	0	0	0
18 PSE 9 South	17	0	25.6	0.3	25.361	0	0	0
10 Vault Area	-3.5	-1	25	3.5	24.769	1.97E-06	0.02454	-1.23E-07
10 Vault Area	-3.5	-1.5	25	2.5	24.769	2.02E-06	0.024957	-1.25E-07
10 Vault Area	-3.5	-2	25	2.2	24.769	2 07F-06	0.025359	-1.27E-07
10 Vault Alea	-3.3	-2	23	2.2	24.703	2.07L-00	0.023333	-1.27L-07
10 Vault Area	-3.5	-2.5	25	2.2	24.769	2.12E-06	0.025744	-1.29E-07
10 Vault Area	-3.5	-3	25	2.4	24.769	2.17E-06	0.026109	-1.31E-07
10 Vault Area	-3.5	-3.5	25	3.4	24.769	2.21E-06	0.026453	-1.32E-07
10 Vault Area	-3.5	-4	25	4.1	24.769	2.26E-06	0.026775	-1.34E-07
10 Vault Area	-3.5	-4.5	25	3.3	24.769	2.29F-06	0.027074	-1.35E-07
10 Vault Alea	3.3	+.J	23	3.3	-7.703	2.23L-00	5.527074	1.33L-07

10 Vault Area	-3.5	-5	25	2.4	24.769	2.33E-06	0.027347	-1.37E-07	
10 Vault Area	-3.5	-5.5	25	2.2	24.769	2.36E-06	0.027595	-1.38E-07	
10 Vault Area	-3.5	-6	25	2.1	24.769	2.39E-06	0.027816	-1.39E-07	
10 Vault Area	-3.5	-6.5	25	2.3	24.769	2.41E-06	0.028008	-1.40E-07	
10 Vault Area	-3.5	-7	25	3.2	24.769	2.43E-06	0.028172	-1.41E-07	
Park Square 11 East Road	-5.7	-4	29	1.9	28.688	0	0	0	
Park Square 11 East Road	-6.2	-4	29	1.4	28.688	0	0	0	
Park Square 11 East Road	-6.7	-4	29	1.2	28.688	0	0	0	
Park Square 11 East Road	-7.2	-4	29	0.9	28.688	0	0	0	
Park Square 11 East Road	-7.7	-4	29	0.8	28.688	0	0	0	
Park Square 11 East Road	-8.2	-4	29	0.6	28.688	0	0	0	
Park Square 11 East Road	-8.7	-4	29	0.5	28.688	0	0	0	
Park Square 11 East Road	-9.2	-4	29	0.4	28.688	0	0	0	

Park Square 11 East Road	-9.7	-4	29	0.4	28.688	0	0	0
Park Square 11 East Road	-10.2	-4	29	0.3	28.688	0	0	0
Park Square 11 East Road	-10.7	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-11.2	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-11.7	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-12.2	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-12.7	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-13.2	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-13.7	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-14.2	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-14.7	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-15.2	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-15.7	-4	29	0	28.688	0	0	0

Results : Consolidation : Displacement Data : Lines

None

Results : Total : Displacement Data

: Lines

None

Oasys Ltd.

The Diorama

19 Park Square East Stage 2

File PDisp 19 Park Square East Stage 2.pdd Exported 06/05/20 21:45:09

PDisp 20.0.0.12 64-bit Copyright © Oasys 1997-2019

Titles

START_TABLE

Job No.: 1038915

Job Title: The Diorama

19 Park

Sub-title: Square East

Calculation

Heading: Stage 2 Initials: JM

Checker:

Date Saved:

Date Checked:

Notes:

File Name:

PDisp 19 Park Square East Stage 2.pdd

> G:\Projects\P rojects 2019\103891 5 - The Diorama, London (LON)\Report

File Path: s\BIA\No.19

END_TABLE

History

 ${\sf START_TABLE}$

Date Time By Notes

18-Dec-19	12:29 jmaness	Nev
18-Dec-19	16:02 jmaness	
18-Dec-19	16:32 jmaness	
18-Dec-19	16:46 jmaness	
15-Jan-20	17:21 jmaness	
15-Jan-20	17:52 jmaness	
15-Jan-20	18:04 jmaness	
16-Jan-20	10:57 jmaness	
16-Jan-20	21:11 jmaness	
20-Jan-20	18:05 jmaness	
13-Feb-20	16:08 jmaness	
13-Feb-20	16:17 jmaness	
13-Feb-20	17:52 jmaness	
25-May-20	12:19 jmaness	
25-May-20	12:30 jmaness	
27-May-20	15:00 jmaness	
29-May-20	14:53 jmaness	
05-Jun-20	21:39 jmaness	

Analysis Options

General

Global Poisson's ratio: 0.50

Maximum allowable ratio between values of E: 1.5

Horizontal rigid boundary level: 7.65 [m OD]

Displacements at load centroids: Yes

GSA piled raft data : No

Elastic

Elastic : Yes

Analysis: Boussinesq

Consolidation

Consolidation : No

Soil ProfilesSoil Profile 1

Number intermedi

ate	Youngs	Youngs
-----	--------	--------

Layer ref.	Name	Level at top [mOD]	ate displacem ent levels	Youngs Modulus : Top [kN/m²]	Youngs Modulus : Btm. [kN/m²]	Poissons ratio	Non-linear curve
	Langley Silt 1 Member Lynch Hill Gravel	29	3	9600	9600	0.2	None
	2 Member	26.5	10	60000	60000	0.3	None
	London Clay 3 Formation	21.3	27	59000	59000	0.5	None

END_TABLE

Non-linear Curve Coordinates -Non-linear Curve 1

START_TABLE

Point Strain [%] Factor

END_TABLE

Soil Zones

START_TABLE

X min X max Y min Y max Profile Zone Name [m] [m] [m] [m] Soil

1 Soil Zone 1 -100 100 -100 100 Profile 1

END_TABLE

Polygonal Load

START_TABLE

Position :

Position: Polygon: No. of Value : Position : Polygon : Rect. Rectangle Normal Load ref. Coords. (local z) Name Level tolerance s [m] [m] [%] [kN/m²] (17,-8) (17,-7) (22.7,-12.3) (22,-1 A 25 13) 10 19.8 (20,-15) (20.6,-15.8) (25.5,-10.9) (24.8,-10.2) (24.1,-10.9) (22.7,-2 B 25 12.3) 10 1 320

	(24.1,- 10.9) (24.8,- 10.2)			
3 C	(17.4,-3.4) 25 (17.4,-4.4) (17.4,-4.4) (17,-7) (22.7,-	10	6	226.6
4 D	12.3) (24.1,- 26 10.9)	10	6	-82
Vault South	(-1.33,-8) (-5.73,-8)	10	ŭ	02
5 Wall	(-5.73,-7) 24.4 (-1.33,-7) (-1.33,-7)	10	1	119
Vault East 6 Wall	(-2.33,-7) (-2.33,-1) 24.4 (-1.33,-1)	10	1	32
Vault West	(-5.73,-7) (-4.73,-7) (-4.73,-1)			
7 Wall	24.4 (-5.73,-1) (-1.33,-1) (-1.33,-0)	10	1	32
Vault North 8 Wall	(-5.73,-0) 24.4 (-5.73,-1) (-2.33,-	10	1	133
	4.5) (- 2.33,-3.5) (-4.73,-			
Vault 9 Dividing Wall	3.5) (- 24.4 4.73,-4.5) (-2.33,-	10	1	119
Vault Excavation	4.5) (- 2.33,-7) (- 4.73,-7) (-			
10 (North)	25 4.73,-4.5) (-2.33,- 3.5) (-	10	1	-23
Vault Excavation 11 (South)	2.33,-1) (- 4.73,-1) (- 25 4.73,-3.5)	10	1	-23
(/			_	_5

Polygonal Loads' Rectangles

START_TABLE

Angle of local x from

No. $\begin{array}{cccc} \text{Centre}: x & \text{Centre}: y & \text{global X} & \text{Width x} & \text{Depth y} \\ [m] & [m] & [\text{Degrees}] & [m] & [m] \end{array}$

Load 1: A

(Edge 2 optimal)

19.6 -10.1 45 0.70711 7.4246 20 7.0004 2 -10 45 0.056569 3 20.6 -10.5 45 0.056569 5.4447 4 21.2 45 0.056569 3.8891 -11 5 21.8 -11.5 45 0.056569 2.3335 6 22.4 -12 45 0.056569 0.77782

Load 2 : B

(Edge 3 optimal)

1 22.7 -13 135 0.98995 6.8589

Load	2	r

(Edge 2 optimal)	21	-7.3	137.42	9.3315	0.8627
2 3 4 5	17.6 17.6 17.5 17.5	-4.1 -3.9 -3.8 -3.6 -3.5	137.42 137.42 137.42 137.42 137.42	0.13533 0.13533 0.13533 0.13533	0.66269 0.51543 0.36816 0.2209 0.073633
Load 4 : D	17.4	3.3	137.42	0.13333	0.073033
(Edge 4 optimal) 1 2 3 4 5	20.6 17.7 17.6 17.6 17.5	-8.9 -6 -5.7 -5.3 -4.9	135.87 135.87 135.87 135.87 135.87 135.87	7.7816 0.30466 0.30466 0.30466 0.30466 0.30466	2.0622 1.9302 1.5013 1.0723 0.64339 0.21446
Load 5 : Vault South Wall					
(Edge 2 optimal)	-3.5	-7.5	-180	4.4	1
Load 6 : Vault East Wall					
(Edge 2 optimal)	-1.8	-4	-180	1	6
Load 7 : Vault West Wall					
(Edge 1 optimal)	-5.2	-4	0	1	6
Load 8 : Vault North Wall					
(Edge 1 optimal)	-3.5	-0.5	90	1	4.4
Load 9 : Vault Dividing Wall					
(Edge 1 optimal)	-3.5	-4	90	1	2.4
Load 10 : Vault Excavation (North)					
(Edge 2 optimal)	-3.5	-5.8	-90	2.5	2.4
Load 11 : Vault Excavation (South)					
(Edge 1 optimal)	-3.5	-2.3	90	2.5	2.4
END_TABLE					

Displacement Lines

START_TABLE Name	X1 [m]	Y1 [m]	Z1] [m]	X2 [m]	Y2 [m]	Z2 [m]	Intervals [No.]	Calculate	Detailed Results
20 Park Square East Rear		17	-8	25.6	17	-16	25.6	16 Yes	Yes
20 Park Square East South		17	-8	25.6	1	-8	25.6	32 Yes	Yes
The Diorama South West		20.6	-15.8	27.1	28.4	-23.6	27.1	22 Yes	Yes
Floor Slab		17	-6	26	23	-11.6	26	16 Yes	Yes
20 Park Square East Front Wall		-5.7	-8	25.4	-5.7	-13	25.4	10 Yes	Yes
20 Park Square East Rear		-1.3	-8	25.4	-1.3	-13	25.4	10 Yes	Yes
18 PSE Front		-5.7	0	25.4	-5.7	5	25.4	10 Yes	Yes
18 PSE Rear		-1.3	0	25.4	-1.3	5	25.4	10 Yes	Yes
18 PSE South		0	0	25.6	17	0	25.6	34 Yes	Yes
Vault Area		-3.5	-1	25	-3.5	-7	25	12 Yes	Yes
Park Square Eas Road	t	-5.7	-4	29	-15.7	-4	29	20 Yes	Yes
END_TABLE									
Displacement Grids									
START_TABLE									
Name	Extrusio Directio		Y1] [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]		Extrusion: Extrusion: Intervals Detailed e Distance Along Calculate Results [m] [No.]
Grid 1	Global X	(-50	-50	25.3 -		50	25.3 100	0 100 100 No No
END_TABLE									

Load Centres : Polygonal START_TABLE Stress: | Stress: | Sum | Sum | Sum | Stress: | Sum | Su Ref. Name

Results : Immediate :

1 A

2 B	22.7	-13	25	9.2	24.769	302.59	673.12	0.0031906
3 C	21.1	-7.4	25	4.9	24.769	193.56	411.68	0.0021354
4 D	20.3	-8.6	26	-0.6	25.765	-81.609	-209.85	-7.19E-04
Vault South								
5 Wall Vault East	-3.5	-7.5	24.4	3.4	24.142	110.04	237.74	0.0011956
6 Wall	-1.8	-4	24.4	2.1	24.142	30.512	80.031	2.61E-04
Vault West								
7 Wall	-5.2	-4	24.4	2.1	24.142	30.513	80.032	2.61E-04
Vault North								
8 Wall	-3.5	-0.5	24.4	3.8	24.142	123.43	266.62	0.0013411
Vault								
9 Dividing Wall Vault	-3.5	-4	24.4	3.4	24.142	106.24	226.12	0.0011712
Excavation								
10 (North) Vault	-3.5	-5.8	25	1.2	24.769	-22.891	-57.9	-2.06E-04
Excavation								
11 (South)	-3.5	-2.3	25	1.3	24.769	-22.891	-57.897	-2.07E-04

Results:
Consolidation:
Load Centres:
Polygonal

None

Results : Total : Load Centres : Polygonal

None

Results : Immediate : Displacement Data : Lines

517.II.1_17.IBEE								Stress:		Stress: Sum	
Ref.	Name	x	у		z	dz		Calc. Level	Stress: Vertical	Princ.	Vert. Strain
		[m]	[m]		[mOD]	[mm]		[mOD]	[kN/m²]	$[kN/m^2]$	[
	20 Park Square East										
	1 Rear 20 Park		17	-8	25.6		0.1	25.361	-4.1754	-27.984	4.95E-05
	Square East 1 Rear 20 Park Square East		17	-8.5	25.6		0.1	25.361	-1.8035	-19.12	5.65E-05
	1 Rear 20 Park Square East		17	-9	25.6		0.2	25.361	-0.88784	-13.714	4.93E-05
	1 Rear 20 Park Square East		17	-9.5	25.6		0.2	25.361	-0.4852	-10.23	4.06E-05
	1 Rear		17	-10	25.6		0.3	25.361	-0.2869	-7.8594	3.31E-05

20 Park									
Square East									
1 Rear	17	-10.5	25.6	0.4	25.361	-0.18004	-6.1737	2.70E-05	
20 Park Square East									
1 Rear	17	-11	25.6	0.4	25.361	-0.1182	-4.9311	2.21E-05	
20 Park									
Square East									
1 Rear	17	-11.5	25.6	0.5	25.361	-0.080329	-3.9888	1.82E-05	
20 Park									
Square East 1 Rear	17	-12	25.6	0.5	25.361	-0.056064	-3.2583	1.51E-05	
20 Park	17	-12	23.0	0.5	25.501	-0.030004	-3.2363	1.511-05	
Square East									
1 Rear	17	-12.5	25.6	0.6	25.361	-0.039943	-2.6823	1.25E-05	
20 Park									
Square East									
1 Rear 20 Park	17	-13	25.6	0.6	25.361	-0.028921	-2.2225	1.05E-05	
Square East									
1 Rear	17	-13.5	25.6	0.7	25.361	-0.021215	-1.8518	8.80E-06	
20 Park									
Square East									
1 Rear	17	-14	25.6	0.7	25.361	-0.015732	-1.5509	7.41E-06	
20 Park									
Square East 1 Rear	17	-14.5	25.6	0.7	25.361	-0.011778	-1.3053	6.27E-06	
20 Park	1,	14.5	23.0	0.7	23.301	0.011770	1.3033	0.272 00	
Square East									
1 Rear	17	-15	25.6	0.7	25.361	-0.0088952	-1.1039	5.33E-06	
20 Park									
Square East	4-	45.5	25.6	2.5	25.264	0.0057744		4.545.06	
1 Rear 20 Park	17	-15.5	25.6	0.6	25.361	-0.0067741	-0.93814	4.54E-06	
Square East									
1 Rear	17	-16	25.6	0.6	25.361	-0.0052008	-0.80116	3.89E-06	
20 Park									
Square East									
		_							
2 South	17	-8	25.6	0.1	25.361	-4.1754	-27.984	4.95E-05	
	17	-8	25.6	0.1	25.361	-4.1754	-27.984	4.95E-05	
2 South 20 Park Square East	17	-8	25.6	0.1	25.361	-4.1754	-27.984	4.95E-05	
20 Park	17 16.5	-8	25.6 25.6	0.1	25.361 25.361	-4.1754 -1.541	-27.984 -16.569	4.95E-05 4.95E-05	
20 Park Square East									
20 Park Square East 2 South 20 Park									
20 Park Square East 2 South 20 Park Square East	16.5	-8	25.6	0.1	25.361	-1.541	-16.569	4.95E-05	
20 Park Square East 2 South 20 Park									
20 Park Square East 2 South 20 Park Square East 2 South	16.5	-8	25.6	0.1	25.361	-1.541	-16.569	4.95E-05	
20 Park Square East 2 South 20 Park Square East	16.5	-8	25.6	0.1	25.361	-1.541	-16.569	4.95E-05	
20 Park Square East 2 South 20 Park Square East 2 South 20 Park	16.5	-8	25.6	0.1	25.361	-1.541	-16.569	4.95E-05	
20 Park Square East 2 South	16.5 16	-8 -8	25.6 25.6	0.1	25.361 25.361	-1.541 -0.62393	-16.569 -10.298	4.95E-05 3.80E-05	
20 Park Square East 2 South	16.5 16	-8 -8	25.6 25.6	0.1	25.361 25.361	-1.541 -0.62393	-16.569 -10.298	4.95E-05 3.80E-05	
20 Park Square East 2 South	16.5 16 15.5	-8 -8	25.6 25.6 25.6	0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05	
20 Park Square East 2 South	16.5 16	-8 -8	25.6 25.6	0.1	25.361 25.361	-1.541 -0.62393	-16.569 -10.298	4.95E-05 3.80E-05	
20 Park Square East 2 South	16.5 16 15.5	-8 -8	25.6 25.6 25.6	0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05	
20 Park Square East 2 South	16.5 16 15.5	-8 -8 -8	25.6 25.6 25.6	0.1 0.1 0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05	
20 Park Square East 2 South 20 Park Square East	16.5 16 15.5	-8 -8	25.6 25.6 25.6	0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05	
20 Park Square East 2 South	16.5 16 15.5	-8 -8 -8	25.6 25.6 25.6	0.1 0.1 0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05 2.02E-05	
20 Park Square East 2 South	16.5 16 15.5	-8 -8 -8	25.6 25.6 25.6	0.1 0.1 0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05 2.02E-05	
20 Park Square East 2 South	16.5 16 15.5	-8 -8 -8	25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007 -0.075812	-16.569 -10.298 -6.7515 -4.6453	4.95E-05 3.80E-05 2.77E-05 2.02E-05	
20 Park Square East 2 South	16.5 16 15.5 15	-8 -8 -8	25.6 25.6 25.6	0.1 0.1 0.1	25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007	-16.569 -10.298 -6.7515	4.95E-05 3.80E-05 2.77E-05 2.02E-05	
20 Park Square East 2 South	16.5 16 15.5 15	-8 -8 -8	25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007 -0.075812	-16.569 -10.298 -6.7515 -4.6453	4.95E-05 3.80E-05 2.77E-05 2.02E-05	
20 Park Square East 2 South	16.5 16 15.5 15 14.5	-8 -8 -8 -8	25.6 25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361 25.361	-0.62393 -0.28128 -0.14007 -0.075812 -0.043907	-16.569 -10.298 -6.7515 -4.6453 -3.329	4.95E-05 3.80E-05 2.77E-05 2.02E-05 1.50E-05	
20 Park Square East 2 South	16.5 16 15.5 15	-8 -8 -8	25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361	-1.541 -0.62393 -0.28128 -0.14007 -0.075812	-16.569 -10.298 -6.7515 -4.6453	4.95E-05 3.80E-05 2.77E-05 2.02E-05	
20 Park Square East 2 South	16.5 16 15.5 15 14.5	-8 -8 -8 -8	25.6 25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361 25.361	-0.62393 -0.28128 -0.14007 -0.075812 -0.043907	-16.569 -10.298 -6.7515 -4.6453 -3.329	4.95E-05 3.80E-05 2.77E-05 2.02E-05 1.50E-05	
20 Park Square East 2 South	16.5 16 15.5 15 14.5	-8 -8 -8 -8	25.6 25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361 25.361	-0.62393 -0.28128 -0.14007 -0.075812 -0.043907	-16.569 -10.298 -6.7515 -4.6453 -3.329	4.95E-05 3.80E-05 2.77E-05 2.02E-05 1.50E-05	
20 Park Square East 2 South	16.5 16 15.5 15 14.5	-8 -8 -8 -8	25.6 25.6 25.6 25.6 25.6	0.1 0.1 0.1 0.1 0.1	25.361 25.361 25.361 25.361 25.361	-0.62393 -0.28128 -0.14007 -0.075812 -0.043907	-16.569 -10.298 -6.7515 -4.6453 -3.329	4.95E-05 3.80E-05 2.77E-05 2.02E-05 1.50E-05	

20 Dark									
20 Park Square East 2 South	12.5	-8	25.6	0	25.361	-0.011456	-1.1683	5.59E-06	
20 Park Square East 2 South	12	-8	25.6	0	25.361	-0.0078735	-0.94588	4.56E-06	
20 Park Square East 2 South	11.5	-8	25.6	0	25.361	-0.0055628	-0.77707	3.76E-06	
20 Park Square East 2 South	11	-8	25.6	0	25.361	-0.0040253	-0.64658	3.15E-06	
20 Park Square East 2 South	10.5	-8	25.6	0	25.361	-0.0029741	-0.54406	2.66E-06	
20 Park Square East 2 South	10	-8	25.6	0	25.361	-0.002238	-0.46234	2.26E-06	
20 Park Square East 2 South	9.5	-8	25.6	0	25.361	-0.0017117	-0.39637	1.94E-06	
20 Park									
Square East 2 South	9	-8	25.6	0	25.361	-0.0013282	-0.34251	1.68E-06	
20 Park Square East 2 South	8.5	-8	25.6	0	25.361	-0.0010441	-0.29808	1.47E-06	
20 Park Square East 2 South	8	-8	25.6	0	25.361	-8.30E-04	-0.26109	1.29E-06	
20 Park Square East 2 South	7.5	-8	25.6	0	25.361	-6.68E-04	-0.23003	1.14E-06	
20 Park Square East 2 South	7	-8	25.6	0	25.361	-5.42E-04	-0.20375	1.01E-06	
20 Park Square East 2 South	6.5	-8	25.6	0	25.361	-4.44E-04	-0.18136	8.97E-07	
20 Park Square East 2 South	6	-8	25.6	0	25.361	-3.66E-04	-0.16216	8.03E-07	
20 Park Square East 2 South	5.5	-8	25.6	0	25.361	-3.05E-04	-0.1456	7.21E-07	
20 Park Square East									
2 South	5	-8	25.6	0.1	25.361	-2.55E-04	-0.13124	6.51E-07	
20 Park Square East 2 South	4.5	-8	25.6	0.1	25.361	-2.15E-04	-0.11872	5.89E-07	
20 Park Square East 2 South	4	-8	25.6	0.1	25.361	-1.82E-04	-0.10775	5.35E-07	

20 Park								
Square East 2 South	3.5	-8	25.6	0.1	25.361	-1.55E-04	-0.09811	4.87E-07
20 Park Square East 2 South	3	-8	25.6	0.2	25.361	-1.33E-04	-0.08959	4.45E-07
20 Park Square East	2.5	o	25.6	0.2	25.361	1 155 04	0.00202	4 00E 07
2 South	2.5	-8	25.6	0.2	25.361	-1.15E-04	-0.08203	4.08E-07
20 Park Square East 2 South	2	-8	25.6	0.3	25.361	-9.91E-05	-0.0753	3.74E-07
20 Park Square East 2 South	1.5	-8	25.6	0.3	25.361	-8.60E-05	-0.0693	3.45E-07
20 Park Square East 2 South	1	-8	25.6	0.4	25.361	-7.50E-05	-0.06392	3.18E-07
The Diorama 3 South West	20.6	-15.8	27.1	3.7	26.8	0	0	0
The Diorama 3 South West	21	-16.2	27.1	2.6	26.8	0	0	0
The Diorama 3 South West	21.3	-16.5	27.1	2.1	26.8	0	0	0
The Diorama 3 South West	21.7	-16.9	27.1	1.7	26.8	0	0	0
The Diorama 3 South West	22	-17.2	27.1	1.4	26.8	0	0	0
The Diorama 3 South West	22.4	-17.6	27.1	1.1	26.8	0	0	0
The Diorama 3 South West	22.7	-17.9	27.1	1	26.8	0	0	0
The Diorama 3 South West	23.1	-18.3	27.1	0.8	26.8	0	0	0
The Diorama 3 South West	23.4	-18.6	27.1	0.7	26.8	0	0	0
The Diorama 3 South West	23.8	-19	27.1	0.6	26.8	0	0	0
The Diorama 3 South West	24.1	-19.3	27.1	0.5	26.8	0	0	0
The Diorama 3 South West	24.5	-19.7	27.1	0.4	26.8	0	0	0

The Diorama 3 South West	24.9	-20.1	27.1	0.3	26.8	0	0	0
The Diorama 3 South West	25.2	-20.4	27.1	0.3	26.8	0	0	0
The Diorama 3 South West	25.6	-20.8	27.1	0.2	26.8	0	0	0
The Diorama 3 South West	25.9	-21.1	27.1	0.2	26.8	0	0	0
The Diorama 3 South West	26.3	-21.5	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	26.6	-21.8	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	27	-22.2	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	27.3	-22.5	27.1	0.1	26.8	0	0	0
The Diorama 3 South West	27.7	-22.9	27.1	0	26.8	0	0	0
The Diorama 3 South West	28	-23.2	27.1	0	26.8	0	0	0
The Diorama 3 South West	28.4	-23.6	27.1	0	26.8	0	0	0
4 Floor Slab	17	-6	26	-0.1	25.765	-17.604	-66.567	-4.86E-05
4 Floor Slab	17.4	-6.3	26	-0.9	25.765	-74.513	-169.1	-7.69E-04
4 Floor Slab	17.8	-6.7	26	-1.1	25.765	-80.848	-196.43	-7.70E-04
4 Floor Slab	18.1	-7	26	-1.2	25.765	-81.193	-202.15	-7.48E-04
4 Floor Slab	18.5	-7.4	26	-1.2	25.765	-81.261	-204.19	-7.40E-04
4 Floor Slab	18.9	-7.8	26	-1.2	25.765	-81.295	-205.21	-7.35E-04
4 Floor Slab	19.3	-8.1	26	-1.1	25.765	-81.32	-205.84	-7.33E-04
4 Floor Slab	19.6	-8.4	26	-1	25.765	-81.342	-206.27	-7.31E-04
4 Floor Slab	20	-8.8	26	-0.9	25.765	-81.362	-206.57	-7.30E-04
4 Floor Slab	20.4	-9.2	26	-0.7	25.765	-81.381	-206.77	-7.29E-04
4 Floor Slab	20.8	-9.5	26	-0.5	25.765	-81.398	-206.86	-7.29E-04
4 Floor Slab	21.1	-9.8	26	-0.3	25.765	-81.412	-206.81	-7.30E-04
4 Floor Slab	21.5	-10.2	26	0.1	25.765	-81.424	-206.53	-7.32E-04
4 Floor Slab	21.9	-10.6	26	0.5	25.765	-81.427	-205.77	-7.35E-04
4 Floor Slab	22.3	-10.9	26	1.2	25.765	-81.395	-203.83	-7.44E-04

4 Floor Slab	22.6	-11.3	26	2.2	25.765	-81.126	-197.94	-7.68E-04
4 Floor Slab	23	-11.6	26	3.9	25.765	-75.977	-169.07	-8.01E-04
20 Park Square East 5 Front Wall	-5.7	-8	25.4	1.7	25.144	-3.85E-05	-0.03429	1.71E-07
20 Park Square East 5 Front Wall	-5.7	-8.5	25.4	1.1	25.144	-3.85E-05	-0.03428	1.71E-07
20 Park Square East 5 Front Wall	-5.7	-9	25.4	0.9	25.144	-3.83E-05	-0.03423	1.70E-07
20 Park Square East 5 Front Wall	-5.7	-9.5	25.4	0.7	25.144	-3.81E-05	-0.03413	1.70E-07
20 Park Square East 5 Front Wall	-5.7	-10	25.4	0.5	25.144	-3.79E-05	-0.034	1.69E-07
20 Park Square East 5 Front Wall	-5.7	-10.5	25.4	0.4	25.144	-3.75E-05	-0.03384	1.68E-07
20 Park Square East 5 Front Wall	-5.7	-11	25.4	0.3	25.144	-3.71E-05	-0.03364	1.67E-07
20 Park Square East 5 Front Wall	-5.7	-11.5	25.4	0.3	25.144	-3.67E-05	-0.0334	1.66E-07
20 Park Square East 5 Front Wall	-5.7	-12	25.4	0.2	25.144	-3.61E-05	-0.03313	1.65E-07
20 Park Square East 5 Front Wall	-5.7	-12.5	25.4	0.2	25.144	-3.56E-05	-0.03283	1.63E-07
20 Park Square East 5 Front Wall 20 Park Square East	-5.7	-13	25.4	0.1	25.144	-3.49E-05	-0.0325	1.62E-07
6 Rear 20 Park	-1.3	-8	25.4	1.7	25.144	-9.98E-05	-0.06032	2.99E-07
Square East 6 Rear 20 Park	-1.3	-8.5	25.4	1.1	25.144	-9.95E-05	-0.06025	2.99E-07
Square East 6 Rear 20 Park	-1.3	-9	25.4	0.9	25.144	-9.89E-05	-0.0601	2.98E-07
Square East 6 Rear 20 Park	-1.3	-9.5	25.4	0.7	25.144	-9.80E-05	-0.05984	2.97E-07
Square East 6 Rear	-1.3	-10	25.4	0.5	25.144	-9.70E-05	-0.05949	2.95E-07

20 Park								
Square East 6 Rear 20 Park	-1.3	-10.5	25.4	0.4	25.144	-9.56E-05	-0.05905	2.93E-07
Square East 6 Rear 20 Park	-1.3	-11	25.4	0.3	25.144	-9.41E-05	-0.05853	2.91E-07
Square East 6 Rear 20 Park	-1.3	-11.5	25.4	0.3	25.144	-9.23E-05	-0.05792	2.88E-07
Square East 6 Rear 20 Park	-1.3	-12	25.4	0.2	25.144	-9.04E-05	-0.05723	2.84E-07
Square East 6 Rear 20 Park	-1.3	-12.5	25.4	0.2	25.144	-8.83E-05	-0.05647	2.80E-07
Square East 6 Rear	-1.3	-13	25.4	0.1	25.144	-8.60E-05	-0.05565	2.76E-07
7 18 PSE Front	-5.7	0	25.4	1.9	25.144	-3.08E-05	-0.02981	1.48E-07
7 18 PSE Front	-5.7	0.5	25.4	1.2	25.144	-2.99E-05	-0.0293	1.46E-07
7 18 PSE Front	-5.7	1	25.4	0.9	25.144	-2.90E-05	-0.02878	1.43E-07
7 18 PSE Front	-5.7	1.5	25.4	0.7	25.144	-2.81E-05	-0.02824	1.41E-07
7 18 PSE Front	-5.7	2	25.4	0.6	25.144	-2.72E-05	-0.0277	1.38E-07
7 18 PSE Front	-5.7	2.5	25.4	0.5	25.144	-2.63E-05	-0.02714	1.35E-07
7 18 PSE Front	-5.7	3	25.4	0.4	25.144	-2.54E-05	-0.02657	1.32E-07
7 18 PSE Front	-5.7	3.5	25.4	0.3	25.144	-2.45E-05	-0.02601	1.29E-07
7 18 PSE Front	-5.7	4	25.4	0.3	25.144	-2.36E-05	-0.02543	1.27E-07
7 18 PSE Front	-5.7	4.5	25.4	0.2	25.144	-2.27E-05	-0.02486	1.24E-07
7 18 PSE Front	-5.7	5	25.4	0.2	25.144	-2.19E-05	-0.02428	1.21E-07
8 18 PSE Rear	-1.3	0	25.4	1.9	25.144	-7.29E-05	-0.04955	2.46E-07
8 18 PSE Rear	-1.3	0.5	25.4	1.2	25.144	-7.00E-05	-0.04838	2.40E-07
8 18 PSE Rear	-1.3	1	25.4	0.9	25.144	-6.71E-05	-0.04718	2.34E-07
8 18 PSE Rear	-1.3	1.5	25.4	0.7	25.144	-6.43E-05	-0.04597	2.28E-07
8 18 PSE Rear	-1.3	2	25.4	0.6	25.144	-6.14E-05	-0.04475	2.22E-07
8 18 PSE Rear	-1.3	2.5	25.4	0.5	25.144	-5.86E-05	-0.04352	2.16E-07
8 18 PSE Rear	-1.3	3	25.4	0.4	25.144	-5.59E-05	-0.04228	2.10E-07
8 18 PSE Rear	-1.3	3.5	25.4	0.3	25.144	-5.32E-05	-0.04105	2.04E-07
8 18 PSE Rear	-1.3	4	25.4	0.2	25.144	-5.05E-05	-0.03983	1.98E-07
8 18 PSE Rear	-1.3	4.5	25.4	0.2	25.144	-4.80E-05	-0.03862	1.92E-07
8 18 PSE Rear	-1.3	5	25.4	0.2	25.144	-4.55E-05	-0.03742	1.86E-07
9 18 PSE South	0	0	25.6	0.7	25.361	-4.05E-05	-0.0439	2.19E-07
9 18 PSE South	0.5	0	25.6	0.6	25.361	-4.54E-05	-0.04691	2.34E-07
9 18 PSE South	1	0	25.6	0.5	25.361	-5.10E-05	-0.0502	2.50E-07
9 18 PSE South	1.5	0	25.6	0.4	25.361	-5.74E-05	-0.0538	2.68E-07
9 18 PSE South	2	0	25.6	0.3	25.361	-6.48E-05	-0.05774	2.87E-07
9 18 PSE South	2.5	0	25.6	0.2	25.361	-7.34E-05	-0.06206	3.09E-07

9 18 PSE South	3	0	25.6	0.2	25.361	-8.33E-05	-0.0668	3.32E-07	
9 18 PSE South	3.5	0	25.6	0.2	25.361	-9.48E-05	-0.07202	3.58E-07	
9 18 PSE South	4	0	25.6	0.1	25.361	-1.08E-04	-0.07778	3.87E-07	
9 18 PSE South	4.5	0	25.6	0.1	25.361	-1.24E-04	-0.08413	4.18E-07	
9 18 PSE South	5	0	25.6	0.1	25.361	-1.42E-04	-0.09117	4.53E-07	
9 18 PSE South	5.5	0	25.6	0	25.361	-1.64E-04	-0.09897	4.91E-07	
9 18 PSE South	6	0	25.6	0	25.361	-1.90E-04	-0.10763	5.34E-07	
9 18 PSE South	6.5	0	25.6	0	25.361	-2.21E-04	-0.11727	5.82E-07	
9 18 PSE South	7	0	25.6	0	25.361	-2.57E-04	-0.12802	6.35E-07	
9 18 PSE South	7.5	0	25.6	0	25.361	-3.01E-04	-0.14003	6.94E-07	
9 18 PSE South	8	0	25.6	0	25.361	-3.53E-04	-0.15346	7.60E-07	
9 18 PSE South	8.5	0	25.6	0	25.361	-4.17E-04	-0.16852	8.34E-07	
9 18 PSE South	9	0	25.6	0	25.361	-4.93E-04	-0.1854	9.16E-07	
9 18 PSE South	9.5	0	25.6	0	25.361	-5.86E-04	-0.20437	1.01E-06	
9 18 PSE South	10	0	25.6	0	25.361	-6.99E-04	-0.22568	1.11E-06	
9 18 PSE South	10.5	0	25.6	0	25.361	-8.37E-04	-0.24964	1.23E-06	
9 18 PSE South	11	0	25.6	0	25.361	-0.0010049	-0.27653	1.36E-06	
9 18 PSE South	11.5	0	25.6	0	25.361	-0.0012101	-0.3067	1.51E-06	
9 18 PSE South	12	0	25.6	0	25.361	-0.0014603	-0.34042	1.67E-06	
9 18 PSE South	12.5	0	25.6	0	25.361	-0.0017643	-0.37797	1.85E-06	
9 18 PSE South	13	0	25.6	0	25.361	-0.0021311	-0.41951	2.05E-06	
9 18 PSE South	13.5	0	25.6	0	25.361	-0.0025695	-0.46503	2.27E-06	
9 18 PSE South	14	0	25.6	0	25.361	-0.0030854	-0.51431	2.50E-06	
9 18 PSE South	14.5	0	25.6	0	25.361	-0.0036798	-0.56674	2.75E-06	
9 18 PSE South	15	0	25.6	0.1	25.361	-0.0043444	-0.62129	3.01E-06	
9 18 PSE South	15.5	0	25.6	0.1	25.361	-0.0050573	-0.67635	3.27E-06	
9 18 PSE South	16	0	25.6	0.1	25.361	-0.0057808	-0.72978	3.52E-06	
9 18 PSE South	16.5	0	25.6	0.1	25.361	-0.0064609	-0.77899	3.75E-06	
9 18 PSE South	17	0	25.6	0.1	25.361	-0.0070349	-0.8212	3.95E-06	
10 Vault Area	-3.5	-1	25	2.9	24.769	-11.465	-30.046	-9.82E-05	
10 Vault Area	-3.5	-1.5	25	1.7	24.769	-22.567	-54.037	-2.19E-04	
10 Vault Area	-3.5	-2	25	1.3	24.769	-22.876	-57.53	-2.08E-04	
10 Vault Area	-3.5	-2.5	25	1.3	24.769	-22.879	-57.74	-2.07E-04	
10 Vault Area	-3.5	-3	25	1.5	24.769	-22.578	-54.797	-2.15E-04	
10 Vault Area	-3.5	-3.5	25	2.6	24.769	-11.511	-31.957	-8.96E-05	
10 Vault Area	-3.5	-4	25	3.5	24.769	-0.72397	-11.7	4.28E-05	
10 Vault Area	-3.5	-4.5	25	2.6	24.769	-11.511	-31.957	-8.96E-05	

10 Vault Area	-3.5	-5	25	1.5	24.769	-22.578	-54.798	-2.15E-04
10 Vault Area	-3.5	-5.5	25	1.2	24.769	-22.879	-57.742	-2.07E-04
10 Vault Area	-3.5	-6	25	1.2	24.769	-22.876	-57.532	-2.08E-04
10 Vault Area	-3.5	-6.5	25	1.5	24.769	-22.567	-54.04	-2.19E-04
10 Vault Area	-3.5	-7	25	2.6	24.769	-11.465	-30.05	-9.82E-05
Park Square 11 East Road	-5.7	-4	29	1.6	28.688	0	0	0
Park Square 11 East Road	-6.2	-4	29	1.2	28.688	0	0	0
Park Square 11 East Road	-6.7	-4	29	1	28.688	0	0	0
Park Square 11 East Road	-7.2	-4	29	0.8	28.688	0	0	0
Park Square 11 East Road	-7.7	-4	29	0.6	28.688	0	0	0
Park Square 11 East Road	-8.2	-4	29	0.5	28.688	0	0	0
Park Square 11 East Road	-8.7	-4	29	0.4	28.688	0	0	0
Park Square 11 East Road	-9.2	-4	29	0.4	28.688	0	0	0
Park Square 11 East Road	-9.7	-4	29	0.3	28.688	0	0	0
Park Square 11 East Road	-10.2	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-10.7	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-11.2	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-11.7	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-12.2	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-12.7	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-13.2	-4	29	0.1	28.688	0	0	0

Park Square 11 East Road	-13.7	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-14.2	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-14.7	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-15.2	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-15.7	-4	29	0	28.688	0	0	0

Results : Consolidation : Displacement Data : Lines

None

Results : Total : Displacement Data : Lines

None

Oasys Ltd.

The Diorama

19 Park Square East
Stage 3

File PDisp 19 Park Square East Stage 3.pdd

Exported 06/03/20 11:55:43

PDisp 20.0.0.12 64bit Copyright © Oasys 1997-2019

Titles

START_TABLE

Job No.: 1038915

Job Title: The Diorama

19 Park
Sub-title: Square East

Calculation

Heading: Stage 3 Initials: JM

Checker:

Date Saved:

Date Checked: Notes:

File Name:

PDisp 19 Park Square East Stage 3.pdd

> G:\Projects\P rojects 2019\103891 5 - The Diorama, London (LON)\Report

File Path: s\BIA\No.19

END_TABLE

History

 ${\sf START_TABLE}$

Date Time By Notes

18-Dec-19	12:29 jmaness	New
18-Dec-19	16:02 jmaness	
18-Dec-19	16:32 jmaness	
18-Dec-19	16:46 jmaness	
15-Jan-20	17:21 jmaness	
15-Jan-20	17:52 jmaness	
15-Jan-20	18:04 jmaness	
16-Jan-20	10:57 jmaness	
16-Jan-20	21:11 jmaness	
20-Jan-20	18:05 jmaness	
13-Feb-20	16:08 jmaness	
13-Feb-20	16:17 jmaness	
13-Feb-20	17:52 jmaness	
25-May-20	12:19 jmaness	
25-May-20	12:30 jmaness	
25-May-20	12:33 jmaness	
27-May-20	16:00 jmaness	
29-May-20	14:51 jmaness	
03-Jun-20	11:54 jmaness	

Analysis Options

General

Global Poisson's ratio: 0.50

Maximum allowable ratio between values of E: 1.5

Horizontal rigid boundary level: 7.65 [m OD]

Displacements at load centroids: Yes

GSA piled raft data :

No

Elastic

Elastic : Yes

Analysis: Boussinesq

Stiffness for horizontal displacement calculations: Weighted average Using legacy heave correction factor:

Consolidation

Consolidation : No

Soil ProfilesSoil Profile 1

START_TABLE

Number of intermedi

Youngs Youngs ate Level at displacem Modulus: Modulus: Poissons Non-linear Layer ref. Name ent levels Top Btm. curve top ratio [mOD] [kN/m²] $[kN/m^2]$ Langley Silt 1 Member 29 9600 9600 0.2 None Lynch Hill Gravel 2 Member 26.5 60000 60000 0.3 None 10

London Clay
3 Formation 21.3 27 59000 59000 0.5 None

END_TABLE

Non-linear Curve Coordinates - Nonlinear Curve 1

START_TABLE

Point Strain [%] Factor

END_TABLE

Soil Zones

START_TABLE

Zone Name X min X max Y min Y max Profile

[m] [m] [m]

Soil
1 Soil Zone 1 -100 100 -100 100 Profile 1

END_TABLE

Polygonal Load Data

Name

START_TABLE

Load ref.

Position :

 Position:
 Polygon:
 No. of
 Value:

 Position:
 Polygon:
 Rect.
 Rectangle
 Normal

 Level
 Coords.
 tolerance
 s
 (local z)

 [m]
 [m]
 [%]
 [kN/m²]

1 A	(17,-8) (17,-7) (22.7,- 12.3) (22,- 25 13) (20,-15) (20.6,- 15.8) (25.5,- 10.9) (24.8,- 10.2)	10	6	19.8
2 B	(24.1,- 10.9) (22.7,- 25 12.3)	10	1	320
3 C	(24.1,- 10.9) (24.8,- 10.2) (17.4,-3.4) 25 (17.4,-4.4) (17.4,-4.4) (17,-7) (22.7,- 13.2)	10	6	226.6
4 D	12.3) (24.1,- 26 10.9) (-1.33,-8)	10	6	-71.8
Vault South 5 Wall	(-5.73,-8) (-5.73,-7) 24 (-1.33,-7) (-1.33,-7)	10	1	119
Vault East 6 Wall	(-2.33,-7) (-2.33,-1) 24 (-1.33,-1) (-5.73,-7)	10	1	32
Vault West 7 Wall	(-4.73,-7) (-4.73,-1) 24 (-5.73,-1) (-1.33,-1)	10	1	32
Vault North 8 Wall	(-1.33,-0) (-5.73,-0) 24 (-5.73,-1) (-2.33,- 4.5) (- 2.33,-3.5) (-4.73,-	10	1	133
Vault Dividing 9 Wall	3.5) (- 24 4.73,-4.5) (-2.33,- 4.5) (-	10	1	119
Vault Excavation 10 (North)	2.33,-7) (- 4.73,-7) (- 25 4.73,-4.5) (-2.33,- 3.5) (-	10	1	-12.8
Vault Excavation 11 (South)	2.33,-1) (- 4.73,-1) (- 25 4.73,-3.5)	10	1	-12.8

Polygonal Loads' Rectangles

START_TABLE

Angle of local x from

No. Centre : x Centre : y global X Width x Depth y

	[m]	[m]]	[Degrees]	[m]	[m]
Load 1 : A						
(Edge 2 optimal)						
	1	19.6	-10.1	45		7.4246
	2	20	-10	45		7.0004
	3 4	20.6 21.2	-10.5 -11	45 45		5.4447 3.8891
	5	21.2	-11.5	45		2.3335
	6	22.4	-12	45		0.77782
Load 2 : B						
(Edge 3 optimal)						
(Luge 3 optimal)	1	22.7	-13	135	0.98995	6.8589
	_					
Load 3 : C						
(Edge 2 optimal)						
(101 171 17	1	21	-7.3	137.42	9.3315	0.8627
	2	17.6	-4.1	137.42	0.13533	0.66269
	3	17.6	-3.9	137.42	0.13533	0.51543
	4	17.5	-3.8	137.42	0.13533	0.36816
	5	17.5	-3.6	137.42	0.13533	0.2209
	6	17.4	-3.5	137.42	0.13533	0.073633
Load 4 : D						
(Edge 4 optimal)						
(Luge 4 optimal)	1	20.6	-8.9	135.87	7.7816	2.0622
	2	17.7	-6	135.87		1.9302
	3	17.6	-5.7			1.5013
	4	17.6	-5.3	135.87		1.0723
	5	17.5	-4.9			0.64339
	6	17.4	-4.6	135.87	0.30466	0.21446
Load 5 : Vault Sou Wall	ıth					
(Edge 2 optimal)						
(Edge 2 optimal)	1	-3.5	-7.5	-180	4.4	1
	_					_
Load 6 : Vault Eas Wall	t					
(Edge 2 optimal)						
	1	-1.8	-4	-180	1	6
Load 7 : Vault We Wall	est					
(Edge 1 optimal)						
(Luge 1 optimal)	1	-5.2	-4	0	1	6
	•	5.2	7	O	•	Ü
Load 8 : Vault No	rth					

(Edge 1 optimal)						
(2080 2 000000)	1	-3.5	-0.5	90	1	4.4
	-	0	0.5	30	-	•••
Load 9 : Vault						
Dividing Wall						
. 3						
(Edge 1 optimal)						
,	1	-3.5	-4	90	1	2.4
Load 10 : Vault						

Load 10 : Vault Excavation (North)

(Edge 2 optimal)	1	-3.5	-5.8	-90	2.5	2.4			
Load 11 : Vault Excavation (South)									
(Edge 1 optimal)	1	-3.5	-2.3	90	2.5	2.4			
END_TABLE									
Displacement Lines									
START_TABLE									
Name	X1 [m]	Y1 [m]	Z1 [m]	X2 [m]	Y2 [m]	Z2 [m]	Interva [No.]	ls Calculate	Detailed Results
20 Park Square East Rear	t	17	-8	25.8	17	-16	25.8	16 Yes	Yes
20 Park Square East South	t	17	-8	25.8	1	-8	25.8	32 Yes	Yes
The Diorama South West		20.6	-15.8	28.1	28.4	-23.6	28.1	22 Yes	Yes
Floor Slab		17	-6	26	23	-11.6	26	16 Yes	Yes
20 Park Square East Front Wall	t	-5.7	-8	25.3	-5.7	-13	25.3	10 Yes	Yes
20 Park Square East Rear	t	-1.3	-8	25.3	-1.3	-13	25.3	10 Yes	Yes
18 PSE Front		-5.7	0	25.3	-5.7	5	25.3	10 Yes	Yes
18 PSE Rear		-1.3	0	25.3	-1.3	5	25.3	10 Yes	Yes
18 PSE South		0	0	25.8	17	0	25.8	34 Yes	Yes
Vault Area		-3.5	-1	25	-3.5	-7	25	12 Yes	Yes
Park Square East Road		-5.7	-4	29	-15.7	-4	29	20 Yes	Yes
END_TABLE									
Displacement Grids									
START_TABLE									

Extrusion:
Intervals Extrusion: Intervals
Along Line Distance Along Calculate Results Extrusion: Ifine ve...
Along Line Distance
[No.] [m] Y1 Z1 X2 Y2 Z2 Direction X1 Name [m] [m] [m] [m] [m] [m] [No.] 50 25.3 100 100 100 No Grid 1 Global X -50 -50 25.3 -No

Results : Immediate : Load Centres : Polygonal

START_TABLE

JIANI_IADEL											
									_	Stress:	
								Stress:	Stress:	Sum	
Ref.	Name	Х	У		Z	dz		Calc. Level			Vert. Strain
		[m]	[m]	[mOD]	[mm]		[mOD]	[kN/m²]	[kN/m²]	[
	1 A		19.8	-10.2	25	5	1	24.769	-0.94855	-1.376	-1.37E-05
	2 B		22.7	-13	25	5	9.3	24.769	303.43	675.85	0.0031951
	3 C		21.1	-7.4	25	5	5.2	24.769	196.31	418.61	0.0021603
	4 D		20.3	-8.6	26	5	-0.1	25.765	-71.458	-183.74	-6.30E-04
	Vault South										
	5 Wall		-3.5	-7.5	24	ı	3.6	23.775	112.79	255.28	0.0011674
	Vault East		-3.5	-7.5	2-		3.0	23.773	112.73	233.20	0.0011074
	6 Wall		-1.8	-4	24	ı	2.2	23.775	30.614	84.826	2.39E-04
	o wan		-1.0	-4	2-		2.2	23.773	30.014	04.020	2.331-04
	Vault West										
	7 Wall		-5.2	-4	24	l	2.2	23.775	30.614	84.812	2.39E-04
	Vault North										
	8 Wall		-3.5	-0.5	24	ı	3.9	23.775	126.35	285.64	0.0013095
	Vault Dividing										
	9 Wall		-3.5	-4	24		3.6	23.775	110.23	248.84	0.001144
	Vault		-3.5	-4	24	•	5.0	23.773	110.23	240.04	0.001144
	Excavation										
			2.5	г о	21		1.0	24.700	12.74	22.22	1 155 04
	10 (North)		-3.5	-5.8	25	•	1.6	24.769	-12.74	-32.23	-1.15E-04
	Vault										
	Excavation		2.5	2.2			4 -	24760	42.74	22.222	4.455.01
	11 (South)		-3.5	-2.3	25)	1.7	24.769	-12.74	-32.229	-1.15E-04

END_TABLE

Results: Consolidation: Load Centres: Polygonal

None

Results : Total : Load Centres : Polygonal

None

Results : Immediate : Displacement Data

: Lines

START_TABLE

Stress: Stress: Sum

Ref.	Name		y [m]	z [mOD]	dz [mm]	Stress Calc. I [mOD	Level	Stress: Vertical [kN/m²]	Sum Princ. [kN/m²]	Vert. Strain
	20 Park									
	Square East		_	25.5	_			4 7000	40 50-	C 005 05
	1 Rear 20 Park	17	-8	25.8	C).3 2	25.55	-1.7063	-19.505	6.06E-05
	Square East									
	1 Rear	17	-8.5	25.8	C).3 2	25.55	-0.6521	-12.706	4.94E-05
	20 Park									
	Square East									
	1 Rear	17	-9	25.8	C	0.3 2	25.55	-0.30243	-8.8946	3.79E-05
	20 Park									
	Square East 1 Rear	17	-9.5	25.8).4 2	25.55	-0.15998	-6.5437	2.93E-05
	20 Park	17	-9.5	25.0		7.4 2		-0.13336	-0.5437	2.931-03
	Square East									
	1 Rear	17	-10	25.8	C).4 2	25.55	-0.092771	-4.9846	2.29E-05
	20 Park									
	Square East									
	1 Rear	17	-10.5	25.8	C).5 2	25.55	-0.057489	-3.8933	1.82E-05
	20 Park Square East									
	1 Rear	17	-11	25.8	r).5 2	25.55	-0.037422	-3.0972	1.47E-05
	20 Park	-/		25.0					2.33.2	2 33
	Square East									
	1 Rear	17	-11.5	25.8	C).6 2	25.55	-0.025278	-2.498	1.19E-05
	20 Park									
	Square East 1 Rear	17	-12	25.8	,).6 2) 5 5 5	-0.017564	-2.0359	9.80E-06
	1 Rear 20 Park	1/	-12	25.8		u 2	در.ر.	-0.01/304	-2.0339	J.0UE-UD
	Square East									
	1 Rear	17	-12.5	25.8	C).7 2	25.55	-0.01247	-1.6731	8.10E-06
	20 Park									
	Square East					_				
	1 Rear	17	-13	25.8	C).7 2	25.55	-0.009005	-1.3843	6.73E-06
	20 Park									
	Square East 1 Rear	17	-13.5	25.8	r).7 2	25.55	-0.006591	-1.152	5.62E-06
	20 Park	1/	15.5	25.0		4		5.555551	1.132	J.JZL 00
	Square East									
	1 Rear	17	-14	25.8	C).7 2	25.55	-0.004879	-0.96386	4.71E-06
	20 Park									
	Square East	47	445	35.0	_	17 7) [[[0.002647	0.01053	2 075 00
	1 Rear 20 Park	17	-14.5	25.8	C).7 2	23.55	-0.003647	-0.81053	3.97E-06
	Square East									
	1 Rear	17	-15	25.8	C).7 2	25.55	-0.002751	-0.68498	3.37E-06
	20 Park									
	Square East					_				
	1 Rear	17	-15.5	25.8	C).7 2	25.55	-0.002093	-0.58176	2.86E-06
	20 Park Square East									
	1 Rear	17	-16	25.8	C).6 2	25.55	-0.001605	-0.49654	2.45E-06
			_0	_5.0		-			,	J- 30
	20 Park									
	Square East									
	2 South	17	-8	25.8	C).3 2	25.55	-1.7063	-19.505	6.06E-05
	20 Park									
	Square East									
	2 South	16.5	-8	25.8	C).2 2	25.55	-0.55822	-11	4.29E-05
	20 Park									
	Square East					_				
	2 South	16	-8	25.8	C).2 2	25.55	-0.21186	-6.6576	2.87E-05
	20 Park									
	Square East									
	2 South	15.5	-8	25.8	C).2 2	25.55	-0.092149	-4.2995	1.95E-05
	20 Park									
	Square East	4-	_	25.5	_			0 0 1 1 5 -	2.004	4 275 55
	2 South	15	-8	25.8	C).2 2	25.55	-0.04495	-2.9318	1.37E-05

20 Park									
Square East									
2 South	14.5	-8	25.8	0.2	25.55	-0.024021	-2.0891	9.92E-06	
20 Park									
Square East									
2 South	14	-8	25.8	0.1	25.55	-0.013798	-1.5426	7.41E-06	
20 Park									
Square East									
2 South	13.5	-8	25.8	0.1	25.55	-0.008398	-1.1727	5.68E-06	
20 Park									
Square East									
2 South	13	-8	25.8	0.1	25.55	-0.005358	-0.91332	4.45E-06	
20 Park									
Square East									
2 South	12.5	-8	25.8	0.1	25.55	-0.003555	-0.72592	3.55E-06	
20 Park									
Square East									
2 South	12	-8	25.8	0	25.55	-0.002438	-0.58705	2.88E-06	
20.5									
20 Park									
Square East	44.5		25.0		25.55	0.004740	0.40405	2 275 26	
2 South	11.5	-8	25.8	0	25.55	-0.001719	-0.48185	2.37E-06	
20 Park									
Square East									
2 South	11	-8	25.8	0	25.55	-0.001242	-0.40065	1.98E-06	
20 Park									
Square East	40.5		25.0		25.55	0.475.04	0.00000	4 665 06	
2 South	10.5	-8	25.8	0	25.55	-9.17E-04	-0.33693	1.66E-06	
20.5									
20 Park									
Square East	40	0	25.0	•	25.55	C 005 04	0.20640	4 425 06	
2 South	10	-8	25.8	0	25.55	-6.89E-04	-0.28619	1.42E-06	
20.0									
20 Park									
Square East	0.5	0	25.0	0	25.55	F 27F 04	0.24526	1 215 00	
2 South	9.5	-8	25.8	0	25.55	-5.27E-04	-0.24526	1.21E-06	
20 D									
20 Park									
Square East	0	0	25.0	•	25.55	4 005 04	0.21100	1.055.00	
2 South	9	-8	25.8	0	25.55	-4.09E-04	-0.21186	1.05E-06	
20 Davil									
20 Park									
Square East	0.5	0	25.0	•	25.55	2 245 04	0.10422	0.455.07	
2 South	8.5	-8	25.8	0	25.55	-3.21E-04	-0.18432	9.15E-07	
20 Davil									
20 Park Square East									
2 South	8	-8	25.8	0	25.55	-2.55E-04	0 16141	8.02E-07	
2 30utii	0	-0	23.0	U	23.33	-2.33E-04	-0.10141	8.02E-07	
20 Park									
Square East									
2 South	7.5	-8	25.8	0	25.55	-2.05E-04	-0.1/218	7.06E-07	
2 300011	7.5	-0	23.0	U	23.33	-2.03L-04	-0.14216	7.00L-07	
20 Park									
Square East									
2 South	7	-8	25.8	0	25 55	-1.66E-04	-0 125 0 1	6.26E-07	
2 Jouin	,	-0	٥.٠	J	دد.دے	1.001-04	0.12331	0.20L-U/	
20 Park									
Square East									
2 South	6.5	-8	25.8	0	25 55	-1.36E-04	-0 11206	5.57E-07	
2 JUUIII	0.5	-0	23.0	U	23.33	-1.30E-04	-0.11200	J.J/E-U/	
20 Park									
Square East									
2 South	6	-8	25.8	0	25.55	-1.12E-04	-0.10018	4.98E-07	
_ 504411	Ū	J	25.0	J	25.55	1.122 04	0.10010	4.552 07	

20 Park								
Square East 2 South	5.5	-8	25.8	0	25.55	-9.34E-05	-0.08994	4.48E-07
20 Park Square East 2 South	5	-8	25.8	0.1	25.55	-7.82E-05	-0.08106	4.04E-07
20 Park Square East 2 South	4.5	0	25.8	0.1	25 55	6 E0E 0E	0.07222	2 655 07
2 South	4.5	-8	25.8	0.1	25.55	-6.59E-05	-0.07332	3.65E-07
20 Park Square East 2 South	4	-8	25.8	0.1	25.55	-5.59E-05	-0.06654	3.31E-07
20 Park Square East 2 South	3.5	-8	25.8	0.1	25.55	-4.76E-05	-0.06058	3.02E-07
20 Park Square East 2 South	3	-8	25.8	0.2	25.55	-4.08E-05	-0.05531	2.76E-07
20 Park Square East 2 South	2.5	-8	25.8	0.2	25.55	-3.51E-05	-0.05064	2.52E-07
20 Park Square East 2 South	2	-8	25.8	0.3	25.55	-3.04E-05	-0.04649	2.32E-07
20 Park Square East 2 South	1.5	-8	25.8	0.4	25.55	-2.64E-05	-0.04278	2.13E-07
20 Park Square East 2 South	1	-8	25.8	0.4	25.55	-2.30E-05	-0.03946	1.97E-07
The Diorama 3 South West	20.6	-15.8	28.1	3.7	27.7	0	0	0
The Diorama 3 South West	21	-16.2	28.1	2.7	27.7	0	0	0
The Diorama 3 South West	21.3	-16.5	28.1	2.1	27.7	0	0	0
The Diorama 3 South West	21.7	-16.9	28.1	1.7	27.7	0	0	0
The Diorama 3 South West	22	-17.2	28.1	1.4	27.7	0	0	0
The Diorama 3 South West	22.4	-17.6	28.1	1.2	27.7	0	0	0
The Diorama 3 South West	22.7	-17.9	28.1	1	27.7	0	0	0
The Diorama 3 South West	23.1	-18.3	28.1	0.8	27.7	0	0	0

The Diorama 3 South West	23.4	-18.6	28.1	0.7	27.7	0	0	0
The Diorama 3 South West	23.8	-19	28.1	0.6	27.7	0	0	0
The Diorama 3 South West	24.1	-19.3	28.1	0.5	27.7	0	0	0
The Diorama 3 South West	24.5	-19.7	28.1	0.4	27.7	0	0	0
The Diorama 3 South West	24.9	-20.1	28.1	0.3	27.7	0	0	0
The Diorama 3 South West	25.2	-20.4	28.1	0.3	27.7	0	0	0
The Diorama 3 South West	25.6	-20.8	28.1	0.2	27.7	0	0	0
The Diorama 3 South West	25.9	-21.1	28.1	0.2	27.7	0	0	0
The Diorama 3 South West	26.3	-21.5	28.1	0.1	27.7	0	0	0
The Diorama 3 South West	26.6	-21.8	28.1	0.1	27.7	0	0	0
The Diorama 3 South West	27	-22.2	28.1	0.1	27.7	0	0	0
The Diorama 3 South West	27.3	-22.5	28.1	0.1	27.7	0	0	0
The Diorama 3 South West	27.7	-22.9	28.1	0	27.7	0	0	0
The Diorama 3 South West	28	-23.2	28.1	0	27.7	0	0	0
The Diorama 3 South West	28.4	-23.6	28.1	0	27.7	0	0	0
4 Floor Slab	17	-6	26	0.1	25.765	-15.414	-58.287	-4.25E-05
4 Floor Slab	17.4	-6.3	26	-0.5	25.765	-65.244	-148.07	-6.73E-04
4 Floor Slab	17.8	-6.7	26	-0.7	25.765	-70.791	-172	-6.74E-04
4 Floor Slab	18.1	-7	26	-0.7	25.765	-71.093	-177	-6.55E-04
4 Floor Slab	18.5	-7.4	26	-0.7	25.765	-71.153	-178.79	-6.48E-04
4 Floor Slab	18.9	-7.8	26	-0.7	25.765	-71.183	-179.69	-6.44E-04
4 Floor Slab	19.3	-8.1	26	-0.6	25.765	-71.205	-180.24	-6.42E-04

4 Floor Slab	19.6	-8.4	26	-0.5	25.765	-71.224	-180.61	-6.40E-04	
4 Floor Slab	20	-8.8	26	-0.4	25.765	-71.242	-180.87	-6.39E-04	
4 Floor Slab	20.4	-9.2	26	-0.2	25.765	-71.258	-181.05	-6.39E-04	
4 Floor Slab	20.8	-9.5	26	0	25.765	-71.273	-181.13	-6.39E-04	
4 Floor Slab	21.1	-9.8	26	0.2	25.765	-71.286	-181.09	-6.39E-04	
4 Floor Slab	21.5	-10.2	26	0.6	25.765	-71.296	-180.84	-6.41E-04	
4 Floor Slab	21.9	-10.6	26	1	25.765	-71.298	-180.18	-6.44E-04	
4 Floor Slab	22.3	-10.9	26	1.6	25.765	-71.27	-178.48	-6.52E-04	
4 Floor Slab	22.6	-11.3	26	2.6	25.765	-71.035	-173.32	-6.72E-04	
4 Floor Slab	23	-11.6	26	4.3	25.765	-66.526	-148.04	-7.01E-04	
20 Park									
Square East 5 Front Wall	-5.7	-8	25.3	1.7	25.05	-4.60E-05	-0.0333	1.66E-07	
20 Park Square East									
5 Front Wall	-5.7	-8.5	25.3	1.2	25.05	-4.60E-05	-0.03329	1.65E-07	
20 Park									
Square East 5 Front Wall	-5.7	-9	25.3	0.9	25.05	-4.58E-05	-0.03324	1.65E-07	
20 Park Square East		2.5	25.0	2.7	25.25		0.00045	1 655 07	
5 Front Wall	-5.7	-9.5	25.3	0.7	25.05	-4.56E-05	-0.03315	1.65E-07	
20 Park Square East									
5 Front Wall	-5.7	-10	25.3	0.6	25.05	-4.52E-05	-0.03302	1.64E-07	
20 Park									
Square East 5 Front Wall	-5.7	-10.5	25.3	0.4	25.05	-4.48E-05	-0.03286	1.63E-07	
5 1 1 Gille 11 Gill	5	10.0	23.3	0	23.03	02 03	0.00200	1.001 07	
20 Park Square East									
5 Front Wall	-5.7	-11	25.3	0.4	25.05	-4.44E-05	-0.03267	1.62E-07	
20 Park									
Square East 5 Front Wall	-5.7	-11.5	25.3	0.3	25.05	-4.38E-05	-0.03244	1.61E-07	
20 Park Square East									
5 Front Wall	-5.7	-12	25.3	0.2	25.05	-4.32E-05	-0.03218	1.60E-07	
20 Park									
Square East 5 Front Wall	-5.7	-12.5	25.3	0.2	25.05	-4.25E-05	-0.03189	1.59E-07	
20 Park Square East			a				0.65		
5 Front Wall	-5.7	-13	25.3	0.1	25.05	-4.18E-05	-0.03156	1.57E-07	

20 Park								
Square East 6 Rear 20 Park	-1.3	-8	25.3	1.7	25.05	-1.19E-04	-0.05856	2.90E-07
Square East 6 Rear	-1.3	-8.5	25.3	1.2	25.05	-1.19E-04	-0.0585	2.90E-07
20 Park Square East 6 Rear	-1.3	-9	25.3	0.9	25.05	-1.18E-04	-0.05835	2.89E-07
20 Park Square East 6 Rear	-1.3	-9.5	25.3	0.7	25.05	-1.17E-04	-0.0581	2.88E-07
20 Park Square East 6 Rear	-1.3	-10	25.3	0.5	25.05	-1.16E-04	-0.05776	2.86E-07
20 Park Square East 6 Rear	-1.3	-10.5	25.3	0.4	25.05	-1.14E-04	-0.05734	2.84E-07
20 Park Square East 6 Rear	-1.3	-11	25.3	0.3	25.05	-1.12E-04	-0.05683	2.82E-07
20 Park Square East 6 Rear	-1.3	-11.5	25.3	0.3	25.05	-1.10E-04	-0.05624	2.79E-07
20 Park Square East 6 Rear 20 Park	-1.3	-12	25.3	0.2	25.05	-1.08E-04	-0.05557	2.76E-07
Square East 6 Rear 20 Park	-1.3	-12.5	25.3	0.2	25.05	-1.05E-04	-0.05483	2.72E-07
Square East 6 Rear	-1.3	-13	25.3	0.1	25.05	-1.03E-04	-0.05403	2.68E-07
7 18 PSE Front	-5.7	0	25.3	1.9	25.05	-3.68E-05	-0.02895	1.44E-07
7 18 PSE Front	-5.7	0.5	25.3	1.3	25.05	-3.57E-05	-0.02845	1.42E-07
7 18 PSE Front	-5.7	1	25.3	1	25.05	-3.47E-05	-0.02795	1.39E-07
7 18 PSE Front	-5.7	1.5	25.3	0.8	25.05	-3.36E-05	-0.02743	1.36E-07
7 18 PSE Front	-5.7	2	25.3	0.6	25.05	-3.25E-05	-0.0269	1.34E-07
7 18 PSE Front	-5.7	2.5	25.3	0.5	25.05	-3.15E-05	-0.02636	1.31E-07
7 18 PSE Front	-5.7	3	25.3	0.4	25.05	-3.04E-05	-0.02581	1.28E-07
7 18 PSE Front	-5.7	3.5	25.3	0.3	25.05	-2.93E-05	-0.02526	1.26E-07
7 18 PSE Front	-5.7	4	25.3	0.3	25.05	-2.82E-05	-0.0247	1.23E-07
7 18 PSE Front	-5.7	4.5	25.3	0.2	25.05	-2.72E-05	-0.02414	1.20E-07
7 18 PSE Front	-5.7	5	25.3	0.2	25.05	-2.61E-05	-0.02358	1.17E-07
8 18 PSE Rear	-1.3	0	25.3	1.9	25.05	-8.70E-05	-0.04811	2.39E-07
8 18 PSE Rear	-1.3	0.5	25.3	1.3	25.05	-8.36E-05	-0.04698	2.33E-07
8 18 PSE Rear	-1.3	1	25.3	1	25.05	-8.02E-05	-0.04582	2.27E-07
8 18 PSE Rear	-1.3	1.5	25.3	0.8	25.05	-7.68E-05	-0.04464	2.22E-07
8 18 PSE Rear	-1.3	2	25.3	0.6	25.05	-7.34E-05	-0.04345	2.16E-07
8 18 PSE Rear	-1.3	2.5	25.3	0.5	25.05	-7.01E-05	-0.04225	2.10E-07
8 18 PSE Rear	-1.3	3	25.3	0.4	25.05	-6.68E-05	-0.04106	2.04E-07
8 18 PSE Rear	-1.3	3.5	25.3	0.3	25.05	-6.36E-05	-0.03987	1.98E-07
8 18 PSE Rear	-1.3	4	25.3	0.2	25.05	-6.04E-05	-0.03868	1.92E-07
8 18 PSE Rear	-1.3	4.5	25.3	0.2	25.05	-5.73E-05	-0.0375	1.86E-07

8 18 PSE Rear	-1.3	5	25.3	0.2	25.05	-5.44E-05	-0.03634	1.81E-07	
9 18 PSE South	0	0	25.8	0.8	25.55	-1.24E-05	-0.02709	1.35E-07	
9 18 PSE South	0.5	0	25.8	0.6	25.55	-1.39E-05	-0.02895	1.44E-07	
9 18 PSE South	1	0	25.8	0.5	25.55	-1.56E-05	-0.03099	1.55E-07	
9 18 PSE South	1.5	0	25.8	0.4	25.55	-1.76E-05	-0.03321	1.66E-07	
9 18 PSE South	2	0	25.8	0.3	25.55	-1.99E-05	-0.03564	1.78E-07	
9 18 PSE South	2.5	0	25.8	0.2	25.55	-2.25E-05	-0.03831	1.91E-07	
9 18 PSE South	3	0	25.8	0.2	25.55	-2.55E-05	-0.04124	2.06E-07	
9 18 PSE South	3.5	0	25.8	0.2	25.55	-2.90E-05	-0.04446	2.22E-07	
9 18 PSE South	4	0	25.8	0.1	25.55	-3.32E-05	-0.04802	2.39E-07	
9 18 PSE South	4.5	0	25.8	0.1	25.55	-3.80E-05	-0.05195	2.59E-07	
9 18 PSE South	5	0	25.8	0.1	25.55	-4.37E-05	-0.05629	2.81E-07	
9 18 PSE South	5.5	0	25.8	0	25.55	-5.04E-05	-0.06111	3.04E-07	
9 18 PSE South	6	0	25.8	0	25.55	-5.83E-05	-0.06647	3.31E-07	
9 18 PSE South	6.5	0	25.8	0	25.55	-6.77E-05	-0.07243	3.61E-07	
9 18 PSE South	7	0	25.8	0	25.55	-7.89E-05	-0.07908	3.94E-07	
9 18 PSE South	7.5	0	25.8	0	25.55	-9.23E-05	-0.0865	4.31E-07	
9 18 PSE South	8	0	25.8	0	25.55	-1.08E-04	-0.09481	4.72E-07	
9 18 PSE South	8.5	0	25.8	0	25.55	-1.28E-04	-0.10412	5.18E-07	
9 18 PSE South	9	0	25.8	0	25.55	-1.51E-04	-0.11458	5.70E-07	
9 18 PSE South	9.5	0	25.8	0	25.55	-1.80E-04	-0.12632	6.28E-07	
9 18 PSE South	10	0	25.8	0	25.55	-2.15E-04	-0.13951	6.93E-07	
9 18 PSE South	10.5	0	25.8	0	25.55	-2.57E-04	-0.15435	7.66E-07	
9 18 PSE South	11	0	25.8	0	25.55	-3.09E-04	-0.17102	8.48E-07	
9 18 PSE South	11.5	0	25.8	0	25.55	-3.72E-04	-0.18972	9.41E-07	
9 18 PSE South	12	0	25.8	0	25.55	-4.50E-04	-0.21063	1.04E-06	
9 18 PSE South	12.5	0	25.8	0	25.55	-5.44E-04	-0.23393	1.16E-06	
9 18 PSE South	13	0	25.8	0	25.55	-6.57E-04	-0.25972	1.28E-06	
9 18 PSE South	13.5	0	25.8	0	25.55	-7.93E-04	-0.288	1.42E-06	
9 18 PSE South	14	0	25.8	0	25.55	-9.53E-04	-0.31864	1.57E-06	
9 18 PSE South	14.5	0	25.8	0.1	25.55	-0.001137	-0.35125	1.73E-06	
9 18 PSE South	15	0	25.8	0.1	25.55	-0.001344	-0.38521	1.90E-06	
9 18 PSE South	15.5	0	25.8	0.1	25.55	-0.001565	-0.4195	2.06E-06	
9 18 PSE South	16	0	25.8	0.1	25.55	-0.001791	-0.45279	2.23E-06	
9 18 PSE South	16.5	0	25.8	0.1	25.55	-0.002002	-0.48346	2.37E-06	
9 18 PSE South	17	0	25.8	0.2	25.55	-0.002181	-0.50976	2.50E-06	
10 Vault Area	-3.5	-1	25	3.1	24.769	-6.3807	-16.729	-5.46E-05	

10 Vault Area	-3.5	-1.5	25	2	24.769	-12.559	-30.08	-1.22E-04	
10 Vault Area	-3.5	-2	25	1.7	24.769	-12.731	-32.024	-1.16E-04	
10 Vault Area	-3.5	-2.5	25	1.7	24.769	-12.733	-32.141	-1.15E-04	
10 Vault Area	-3.5	-3	25	1.9	24.769	-12.565	-30.503	-1.20E-04	
10 Vault Area	-3.5	-3.5	25	2.9	24.769	-6.406	-17.792	-4.98E-05	
10 Vault Area	-3.5	-4	25	3.7	24.769	-0.40296	-6.5189	2.39E-05	
10 Vault Area	-3.5	-4.5	25	2.9	24.769	-6.406	-17.793	-4.98E-05	
10 Vault Area	-3.5	-5	25	1.9	24.769	-12.565	-30.504	-1.20E-04	
10 Vault Area	-3.5	-5.5	25	1.6	24.769	-12.733	-32.143	-1.15E-04	
10 Vault Area	-3.5	-6	25	1.6	24.769	-12.731	-32.026	-1.16E-04	
10 Vault Area	-3.5	-6.5	25	1.9	24.769	-12.559	-30.083	-1.22E-04	
10 Vault Area	-3.5	-7	25	2.8	24.769	-6.3807	-16.732	-5.46E-05	
Park Square									
11 East Road	-5.7	-4	29	1.7	28.688	0	0	0	
Park Square									
11 East Road	-6.2	-4	29	1.3	28.688	0	0	0	
Park Square									
11 East Road	-6.7	-4	29	1	28.688	0	0	0	
Park Square									
11 East Road	-7.2	-4	29	0.8	28.688	0	0	0	
Park Square									
11 East Road	-7.7	-4	29	0.7	28.688	0	0	0	
Park Square									
11 East Road	-8.2	-4	29	0.6	28.688	0	0	0	
Park Square									
11 East Road	-8.7	-4	29	0.5	28.688	0	0	0	
Park Square									
11 East Road	-9.2	-4	29	0.4	28.688	0	0	0	

Park Square 11 East Road	-9.7	-4	29	0.3	28.688	0	0	0
Park Square 11 East Road	-10.2	-4	29	0.3	28.688	0	0	0
Park Square 11 East Road	-10.7	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-11.2	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-11.7	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-12.2	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-12.7	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-13.2	-4	29	0.1	28.688	0	0	0
Park Square 11 East Road	-13.7	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-14.2	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-14.7	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-15.2	-4	29	0	28.688	0	0	0
Park Square 11 East Road	-15.7	-4	29	0	28.688	0	0	0

Results : Consolidation : Displacement Data : Lines

None

Results : Total : Displacement Data : Lines

None

Oasys Ltd.

The Diorama

19 Park Square East Stage 4

File PDisp 19 Park Square East Stage 4.pdd

Exported 06/06/20 00:39:03

PDisp 20.0.0.12 64bit Copyright © Oasys 1997-2019

Titles

START_TABLE

Job No.: 1038915

The Diorama Job Title:

19 Park

Sub-title: Square East

Calculation Heading: Stage 4 Initials: JM

Checker:

Date Saved:

Date Checked:

Notes:

PDisp 19 Park Square East Stage

File Name: 4.pdd

> G:\Projects\P rojects 2019\103891 5 - The Diorama, London (LON)\Repor

File Path: ts\BIA\No.19

END_TABLE

History

 ${\sf START_TABLE}$

Date Ву Notes 18-Dec-19 12:29 jmaness New 18-Dec-19 16:02 jmaness 18-Dec-19 16:32 jmaness

18-Dec-19	16:46 jmaness	
15-Jan-20	17:21 jmaness	
15-Jan-20	17:52 jmaness	
15-Jan-20	18:04 jmaness	
16-Jan-20	10:57 jmaness	
16-Jan-20	21:11 jmaness	
20-Jan-20	18:05 jmaness	
13-Feb-20	16:08 jmaness	
13-Feb-20	16:17 jmaness	
13-Feb-20	17:52 jmaness	
25-May-20	12:19 jmaness	
25-May-20	12:30 jmaness	
25-May-20	12:33 jmaness	
25-May-20	12:36 jmaness	
28-May-20	08:47 jmaness	
29-May-20	14:47 jmaness	
05-Jun-20	22:05 jmaness	
06-Jun-20	00:38 jmaness	Open

Analysis Options

General

Global Poisson's ratio: 0.50

Maximum allowable ratio between values of E: 1.5

Horizontal rigid boundary level: 7.65 [m OD]

Displacements at load centroids: Yes

GSA piled raft data :

No

Elastic

Elastic : Yes

Analysis: Boussinesq

Stiffness for horizontal displacement calculations: Weighted average

Using legacy heave correction factor:

Consolidation

Soil ProfilesSoil Profile 1

START TABLE

Number

intermedi

Youngs Youngs ate

Level at displacem Modulus: Modulus: Poissons Non-linear ent levels Top Layer ref. Name Btm. ratio top curve

[mOD] [kN/m²] [kN/m²]

21.3

Langley Silt

3 Formation

1 Member 29 9600 9600 0.2 None 3 Lynch Hill Gravel 2 Member 26.5 60000 60000 0.3 None 10

London Clay 27

35000

35000

0.2 None

END_TABLE

Non-linear Curve Coordinates - Nonlinear Curve 1

START_TABLE

Strain [%] Point Factor

END_TABLE

Soil Zones

START_TABLE

X min X max Y min Y max Profile Zone Name

[m] [m] [m] [m]

Soil 1 Soil Zone 1 -100 100 -100 100 Profile 1

END_TABLE

Polygonal Load Data

START_TABLE

Position : Position: Polygon: No. of

[%]

Value:

[kN/m²]

Position: Polygon: Rect. Rectangle Normal Load ref. Name Level Coords. tolerance s (local z)

[m] [m] (17,-8) (17,-7) (22.7,-12.3) (22,-

25 13) 1 A 10 19.8

	(20,-15)			
	(20.6,-			
	15.8)			
	(25.5,-			
	10.9)			
	(24.8,- 10.2)			
	(24.1,-			
	10.9)			
	(22.7,-			
2 B	25 12.3)	10	1	320
	(24.1,-			
	10.9)			
	(24.8,-			
	10.2)			
	(17.4,- 3.4) (17.4,-			
3 C	25 4.4)	10	6	226.6
	(17.4,-		ŭ	220.0
	4.4) (17,-			
	7) (22.7,-			
	12.3)			
	(24.1,-			
4 D	26 10.9)	10	6	-71.8
	(-1.33,-8)			
Vault South	(-5.73,-8) (-5.73,-7)			
5 Wall	24.4 (-1.33,-7)	10	1	119
	(-1.33,-7)			
	(-2.33,-7)			
Vault East	(-2.33,-1)			
6 Wall	24.4 (-1.33,-1)	10	1	32
	(-5.73,-7)			
Vault Wast	(-4.73,-7)			
Vault West 7 Wall	(-4.73,-1) 24.4 (-5.73,-1)	10	1	32
,	(-1.33,-1)	10	-	32
	(-1.33,-0)			
Vault North	(-5.73,-0)			
8 Wall	24.4 (-5.73,-1)	10	1	133
	(-2.33,-			
	4.5) (-			
	2.33,-3.5)			
Vault	(-4.73,- 3.5) (-			
9 Dividing Wall	24.4 4.73,-4.5)	10	1	119
5	(-2.33,-		_	
	4.5) (-			
Vault	2.33,-7) (-			
Excavation	4.73,-7) (-			
10 (North)	25 4.73,-4.5)	10	1	-12.8
	(-2.33,-			
Vault	3.5) (-			
Excavation	2.33,-1) (- 4.73,-1) (-			
11 (South)	25 4.73,-3.5)	10	1	-12.8
· · · · · · · · · · · · · · · · · · ·	,,		_	

Polygonal Loads' Rectangles

START_TABLE

Angle of local x from

No. Centre: x Centre: y global X Width x Depth y [m] [m] [Degrees] [m] [m]

Load 1 : A

(Edge 2 optimal)

1 19.6 -10.1 45 0.70711 7.4246 2 20 -10 45 0.056569 7.0004 3 20.6 -10.5 45 0.056569 5.4447

	4	21.2	-11	45	0.056569	3.8891
	5	21.8	-11.5		0.056569	2.3335
	6	22.4	-12	45	0.056569	0.77782
Load 2 : B						
(Edge 3 optimal)		22.7	42	425	0.00005	6.0500
	1	22.7	-13	135	0.98995	6.8589
Load 3 : C						
(Edge 2 optimal)						
	1 2	21 17.6	-7.3 -4.1	137.42 137.42	9.3315 0.13533	0.8627 0.66269
	3	17.6	-3.9	137.42	0.13533	0.51543
	4	17.5	-3.8	137.42	0.13533	0.36816
	5	17.5	-3.6	137.42	0.13533	0.2209
	6	17.4	-3.5	137.42	0.13533	0.073633
Load 4 : D						
LOau 4 . D						
(Edge 4 optimal)						
	1	20.6	-8.9	135.87	7.7816	2.0622
	2	17.7	-6	135.87	0.30466	1.9302
	3	17.6	-5.7 -5.2	135.87 135.87	0.30466	1.5013
	4 5	17.6 17.5	-5.3 -4.9	135.87	0.30466 0.30466	1.0723 0.64339
	6	17.4	-4.6	135.87	0.30466	0.21446
Load 5 : Vault Sou Wall	th					
(Edge 2 optimal)						
- , ,	1	-3.5	-7.5	-180	4.4	1
Load 6 : Vault Eas Wall	t					
(Edge 2 optimal)						
(==8===+,	1	-1.8	-4	-180	1	6
Load 7 : Vault We Wall	st					
(Edge 1 optimal)						
(1	-5.2	-4	0	1	6
Load 8 : Vault Nor Wall	th					
(Edge 1 optimal)						
	1	-3.5	-0.5	90	1	4.4
Load 9 : Vault Dividing Wall						
/Edgo 1 ontine 1						
(Edge 1 optimal)	1	-3.5	-4	90	1	2.4
	1	5.5	-	50	1	2.4
Load 10 : Vault						
Excavation (North	1)					
(Edge 2 optimal)						
(0 = 0 p (1	-3.5	-5.8	-90	2.5	2.4
1						
Load 11 : Vault Excavation (South	.)					
LXCAVALIOII (SOUTH	')					
(Edge 1 optimal)						
	1	-3.5	-2.3	90	2.5	2.4
END TABLE						
END_TABLE						

Displacement Lines

STA	RT	TA	BLE

Name	X1 [m]	Y1 [m]	Z1 [m]		X2 [m]	Y2 [m]	Z2 [m]	Intervals [No.]	Calculate	Detailed Results
20 Park Square East Rear		17	-8	25.6	17	-16	5 25.6	5 1	16 Yes	Yes
20 Park Square East South		17	-8	25.6	1	-8	25.6	5 3	32 Yes	Yes
The Diorama South West		20.6	-15.8	27.1	28.4	-23.6	i 27.:	1 2	22 Yes	Yes
Floor Slab		17	-6	26	23	-11.6	j 26	5 1	16 Yes	Yes
20 Park Square East Front Wall		-5.7	-8	25.4	-5.7	-13	25.4	4 1	10 Yes	Yes
20 Park Square East Rear		-1.3	-8	25.4	-1.3	-13	25.4	4 1	10 Yes	Yes
18 PSE Front		-5.7	0	25.4	-5.7	5	25.4	4 1	10 Yes	Yes
18 PSE Rear		-1.3	0	25.4	-1.3	5	25.4	4 1	10 Yes	Yes
18 PSE South		0	0	25.6	17	0	25.0	5 3	34 Yes	Yes
Vault Area		-3.5	-1	25	-3.5	-7	2!	5 1	12 Yes	Yes
Park Square East Road END_TABLE		-5.7	-4	29	-15.7	-4	. 29	9 2	20 Yes	Yes

Displacement Grids

START_TABLE

Name	Extrusion: Direction	X1	Y1	Z1	X2	Y2	Z2	Intervals Along Line	Extrusion: Distance	Extrusion Intervals Along	: Calculate	Detailed Results
		[m]	[m]	[m]	[m]	[m]	[m]	[No.]	[m]	[No.]		
Grid 1	Global X		-50	-50	25.3 -		50	25.3 10	00 10	00 100) No	No

END_TABLE

Results : Immediate : Load Centres : Polygonal

START_TABLE

						Stress:		Stress:	
						Calc.	Stress:	Sum	
Ref.	Name	Х	У	Z	dz	Level	Vertical	Princ.	Vert. Strain

	[m]		[m]	[mOD]	[mm]	[mOD]	$[kN/m^2]$	$[kN/m^2]$	[
1 A		19.8	-10.2	25	2.5	24.769	-0.94855	-1.376	-1.37E-05
2 B		22.7	-13	25	11.7	24.769	303.43	675.85	0.0031951
3 C		21.1	-7.4	25	6.8	24.769	196.31	418.61	0.0021603
4 D		20.3	-8.6	26	1.4	25.765	-71.458	-183.74	-6.30E-04
Vault South									
5 Wall		-3.5	-7.5	24.4	4.8	24.142	111.7	242.57	0.0012073
Vault East									
6 Wall		-1.8	-4	24.4	3.5	24.142	31.397	84.139	2.60E-04
N. 11. N. 1.									
Vault West									
7 Wall		-5.2	-4	24.4	3.5	24.142	31.397	84.135	2.60E-04
Vault North									
8 Wall		-3.5	-0.5	24.4	5.2	24.142	125.08	271.45	0.0013529
o wan		3.3	0.5	2-11	3.2	24.142	123.00	271.43	0.0013323
Vault									
9 Dividing Wall		-3.5	-4	24.4	5	24.142	109.54	235.4	0.0011963
Vault									
Excavation									
10 (North)		-3.5	-5.8	25	2.9	24.769	-12.74	-32.23	-1.15E-04
Vault									
Excavation									
11 (South)		-3.5	-2.3	25	3.1	24.769	-12.74	-32.229	-1.15E-04
		-3.5	-2.3	25	3.1	24.769	-12.74	-32.229	-1.15E-04

Results : Consolidation: Load Centres: Polygonal

None

Results : Total : Load Centres : Polygonal

None

Results : Immediate : Displacement Data : Lines

START_TABLE

Ref.	Name	x	у	z		dz		Stress: Calc. Level	Stress: Vertical	Stress: Sum Princ.	Vert. Strain
	20 Park Square East	[m]	[m]	[m	iOD]	[mm]		[mOD]	[kN/m²]	[kN/m²]	[
	1 Rear 20 Park		17	-8	25.6		1.2	25.361	-3.6561	-24.503	4.33E-05
	Square East 1 Rear 20 Park		17	-8.5	25.6		1.2	25.361	-1.5792	-16.742	4.95E-05
	Square East 1 Rear 20 Park		17	-9	25.6		1.2	25.361	-0.7774	-12.008	4.32E-05
	Square East 1 Rear 20 Park		17	-9.5	25.6		1.3	25.361	-0.42484	-8.9571	3.56E-05
	Square East 1 Rear		17	-10	25.6		1.3	25.361	-0.25122	-6.8817	2.90E-05

20 Park								
Square East								
1 Rear	17	-10.5	25.6	1.4	25.361	-0.15764	-5.4057	2.36E-05
20 Park Square East								
1 Rear	17	-11	25.6	1.4	25.361	-0.10349	-4.3177	1.93E-05
20 Park Square East								
1 Rear	17	-11.5	25.6	1.5	25.361	-0.070336	-3.4926	1.59E-05
20 Park								
Square East 1 Rear	17	-12	25.6	1.6	25.361	-0.04909	-2.853	1.32E-05
20 Park	1,	12	25.0	1.0	23.301	0.04303	2.033	1.322 03
Square East	47	42.5	25.6	4.5	25.264	0.024074	2 2 4 0 7	4 405 05
1 Rear 20 Park	17	-12.5	25.6	1.6	25.361	-0.034974	-2.3487	1.10E-05
Square East								
1 Rear	17	-13	25.6	1.6	25.361	-0.025323	-1.946	9.18E-06
20 Park Square East								
1 Rear	17	-13.5	25.6	1.7	25.361	-0.018576	-1.6214	7.70E-06
20 Park								
Square East 1 Rear	17	-14	25.6	1.7	25.361	-0.013775	-1.358	6.49E-06
20 Park	1,	14	25.0	1.,	25.501	0.013773	1.550	0.432 00
Square East								
1 Rear 20 Park	17	-14.5	25.6	1.6	25.361	-0.010313	-1.1429	5.49E-06
Square East								
1 Rear	17	-15	25.6	1.6	25.361	-0.0077887	-0.96659	4.66E-06
20 Park								
Square East 1 Rear	17	-15.5	25.6	1.5	25.361	-0.0059315	-0.82145	3.98E-06
20 Park								
Square East	17	16	25.6	1 5	25 261	0.0045530	0.7015	2 415 06
1 Rear	17	-16	25.6	1.5	25.361	-0.0045539	-0.7015	3.41E-06
20 Park								
Square East	47		25.6	4.2	25.264	2.0504	24 502	4 225 05
2 South	17	-8	25.6	1.2	25.361	-3.6561	-24.503	4.33E-05
20 Park								
Square East	46.5		0.5					
2 South	16.5	-8	25.6	1	25.361	-1.3493	-14.508	4.33E-05
20 Park								
Square East	4.5		05.6			0.54500		
2 South	16	-8	25.6	1	25.361	-0.54632	-9.0172	3.32E-05
20 Park								
Square East		_						
2 South	15.5	-8	25.6	0.9	25.361	-0.24629	-5.9117	2.42E-05
20 Park								
Square East								
2 South	15	-8	25.6	0.8	25.361	-0.12265	-4.0675	1.77E-05
20 Park								
Square East								
2 South	14.5	-8	25.6	0.7	25.361	-0.066381	-2.9149	1.31E-05
20 Park								
Square East								
2 South	14	-8	25.6	0.6	25.361	-0.038445	-2.1606	9.97E-06
20 Park								
Square East								
2 South	13.5	-8	25.6	0.6	25.361	-0.023531	-1.647	7.72E-06
20 Park								
Square East								
2 South	13	-8	25.6	0.5	25.361	-0.015073	-1.2852	6.10E-06
20 Park								
Square East								
2 South	12.5	-8	25.6	0.5	25.361	-0.010031	-1.023	4.90E-06

20 Park								
Square East								
2 South	12	-8	25.6	0.4	25.361	-0.0068941	-0.82822	3.99E-06
20 Park								
Square East 2 South	11.5	-8	25.6	0.4	25.361	-0.0048709	-0.68041	3.30E-06
2 304	11.0	Ü	23.0	0	25.501	0.00 .0703	0.000.1	5.502 00
20 Park Square East								
2 South	11	-8	25.6	0.4	25.361	-0.0035246	-0.56615	2.75E-06
20 DI-								
20 Park Square East								
2 South	10.5	-8	25.6	0.3	25.361	-0.0026041	-0.47638	2.33E-06
20 Park								
Square East								
2 South	10	-8	25.6	0.3	25.361	-0.0019596	-0.40483	1.98E-06
20 Park								
Square East 2 South	0.5	0	25.6	0.2	25 261	0.0014099	0.24707	1 705 06
2 30utii	9.5	-8	25.6	0.3	25.361	-0.0014988	-0.34707	1.70E-06
20 Park								
Square East 2 South	9	-8	25.6	0.3	25.361	-0.001163	-0.29991	1.47E-06
20 Park Square East								
2 South	8.5	-8	25.6	0.3	25.361	-9.14E-04	-0.261	1.29E-06
20 Park								
Square East								
2 South	8	-8	25.6	0.3	25.361	-7.27E-04	-0.22861	1.13E-06
20 Park								
Square East								
2 South	7.5	-8	25.6	0.3	25.361	-5.85E-04	-0.20141	9.94E-07
20 Park								
Square East 2 South	7	0	25.6	0.2	25 261	4 745 04	0.1794	0 025 07
2 300111	7	-8	25.6	0.3	25.361	-4.74E-04	-0.1784	8.82E-07
20 Park								
Square East 2 South	6.5	-8	25.6	0.3	25.361	-3.88E-04	-0.1588	7.86E-07
20 Park Square East								
2 South	6	-8	25.6	0.4	25.361	-3.21E-04	-0.14199	7.03E-07
20 Park								
Square East								
2 South	5.5	-8	25.6	0.4	25.361	-2.67E-04	-0.12749	6.32E-07
20 Park								
Square East								
2 South	5	-8	25.6	0.4	25.361	-2.23E-04	-0.11492	5.70E-07
20 Park								
Square East 2 South	4.5	-8	25.6	0.5	25.361	-1 88F-04	-0.10395	5.16E-07
_ 500011	4.5	J	23.0	5.5	25.501	1.301 04	0.10333	J.10L 07
20 Park								
Square East 2 South	4	-8	25.6	0.5	25.361	-1.60E-04	-0.09435	4.68E-07
20 Park Square East								
2 South	3.5	-8	25.6	0.6	25.361	-1.36E-04	-0.0859	4.27E-07
20 Park								
Square East								
2 South	3	-8	25.6	0.7	25.361	-1.17E-04	-0.07844	3.90E-07

20 Park Square East 2 South	2.5	-8	25.6	0.7	25.361	-1.00E-04	-0.07183	3.57E-07	
20 Park Square East 2 South	2	-8	25.6	0.8	25.361	-8.67E-05	-0.06594	3.28E-07	
20 Park Square East 2 South	1.5	-8	25.6	1	25.361	-7.53E-05	-0.06068	3.02E-07	
20 Park Square East 2 South	1	-8	25.6	1.1	25.361	-6.57E-05	-0.05597	2.78E-07	
The Diorama 3 South West	20.6	-15.8	27.1	5.3	26.8	0	0	0	
The Diorama 3 South West	21	-16.2	27.1	4.2	26.8	0	0	0	
The Diorama 3 South West	21.3	-16.5	27.1	3.6	26.8	0	0	0	
The Diorama 3 South West	21.7	-16.9	27.1	3.1	26.8	0	0	0	
The Diorama 3 South West	22	-17.2	27.1	2.7	26.8	0	0	0	
The Diorama 3 South West	22.4	-17.6	27.1	2.3	26.8	0	0	0	
The Diorama 3 South West	22.7	-17.9	27.1	2	26.8	0	0	0	
The Diorama 3 South West	23.1	-18.3	27.1	1.8	26.8	0	0	0	
The Diorama 3 South West	23.4	-18.6	27.1	1.6	26.8	0	0	0	
The Diorama 3 South West	23.8	-19	27.1	1.4	26.8	0	0	0	
The Diorama 3 South West	24.1	-19.3	27.1	1.2	26.8	0	0	0	
The Diorama 3 South West	24.5	-19.7	27.1	1	26.8	0	0	0	
The Diorama 3 South West	24.9	-20.1	27.1	0.9	26.8	0	0	0	
The Diorama 3 South West	25.2	-20.4	27.1	0.8	26.8	0	0	0	
The Diorama 3 South West	25.6	-20.8	27.1	0.7	26.8	0	0	0	

The Diorama 3 South West	25.9	-21.1	27.1	0.6	26.8	0	0	0
The Diorama 3 South West	26.3	-21.5	27.1	0.5	26.8	0	0	0
The Diorama 3 South West	26.6	-21.8	27.1	0.5	26.8	0	0	0
The Diorama 3 South West	27	-22.2	27.1	0.4	26.8	0	0	0
The Diorama 3 South West	27.3	-22.5	27.1	0.4	26.8	0	0	0
The Diorama 3 South West	27.7	-22.9	27.1	0.3	26.8	0	0	0
The Diorama 3 South West	28	-23.2	27.1	0.3	26.8	0	0	0
The Diorama 3 South West	28.4	-23.6	27.1	0.2	26.8	0	0	0
4 Floor Slab	17	-6	26	1.1	25.765	-15.414	-58.287	-4.25E-05
4 Floor Slab	17.4	-6.3	26	0.5	25.765	-65.244	-148.07	-6.73E-04
4 Floor Slab	17.8	-6.7	26	0.4	25.765	-70.791	-172	-6.74E-04
4 Floor Slab	18.1	-7	26	0.4	25.765	-71.093	-177	-6.55E-04
4 Floor Slab	18.5	-7.4	26	0.5	25.765	-71.153	-178.79	-6.48E-04
4 Floor Slab	18.9	-7.8	26	0.6	25.765	-71.183	-179.69	-6.44E-04
4 Floor Slab	19.3	-8.1	26	0.7	25.765	-71.205	-180.24	-6.42E-04
4 Floor Slab	19.6	-8.4	26	0.9	25.765	-71.224	-180.61	-6.40E-04
4 Floor Slab	20	-8.8	26	1.1	25.765	-71.242	-180.87	-6.39E-04
4 Floor Slab	20.4	-9.2	26	1.4	25.765	-71.258	-181.05	-6.39E-04
4 Floor Slab	20.8	-9.5	26	1.7	25.765	-71.273	-181.13	-6.39E-04
4 Floor Slab	21.1	-9.8	26	2.1	25.765	-71.286	-181.09	-6.39E-04
4 Floor Slab	21.5	-10.2	26	2.5	25.765	-71.296	-180.84	-6.41E-04
4 Floor Slab	21.9	-10.6	26	3.1	25.765	-71.298	-180.18	-6.44E-04
4 Floor Slab	22.3	-10.9	26	3.8	25.765	-71.27	-178.48	-6.52E-04
4 Floor Slab	22.6	-11.3	26	4.9	25.765	-71.035	-173.32	-6.72E-04
4 Floor Slab	23	-11.6	26	6.6	25.765	-66.526	-148.04	-7.01E-04
20 Park Square East 5 Front Wall	-5.7	-8	25.4	2.7	25.144	-3.37E-05	-0.03003	1.49E-07
20 Park Square East 5 Front Wall	-5.7	-8.5	25.4	2.1	25.144	-3.37E-05	-0.03002	1.49E-07

20 Park Square East 5 Front Wall	-5.7	-13	25.4	0.5	25.144	-3.06E-05	-0.02846	1.42E-07
5 Front Wall 20 Park Square East								
5 Front Wall 20 Park	-5.7 -1.3	-13 -8	25.4 25.4	2.7	25.144 25.144	-3.06E-05 -8.74E-05		1.42E-07 2.62E-07
5 Front Wall 20 Park	-5.7	-13	25.4	0.5	25.144	-3.06E-05	-0.02846	1.42E-07
Square East	-5.7	-13	25.4	0.5	25.144	-3.06E-05	-0.02846	1.42E-07
20 Park Square East 5 Front Wall	-5.7	-12.5	25.4	0.6	25.144	-3.11E-05	-0.02875	1.43E-07
Square East 5 Front Wall	-5.7	-12	25.4	0.7	25.144	-3.16E-05	-0.02901	1.44E-07
Square East 5 Front Wall 20 Park	-5.7	-11.5	25.4	0.8	25.144	-3.21E-05	-0.02925	1.46E-07
5 Front Wall 20 Park	-5.7	-11	25.4	0.9	25.144	-3.25E-05	-0.02945	1.47E-07
5 Front Wall 20 Park Square East	-5.7	-10.5	25.4	1.1	25.144	-3.29E-05		1.47E-07
5 Front Wall 20 Park Square East	-5.7	-10	25.4	1.2	25.144	-3.32E-05	-0.02977	1.48E-07
5 Front Wall 20 Park Square East	-5.7	-9.5	25.4	1.5	25.144	-3.34E-05	-0.02989	1.49E-07
20 Park Square East	-5.7	-9	25.4		25.144	3.302 03	-0.02997	1.49E-07

7 18 PSE Front	-5.7	0	25.4	2.9	25.144	-2.69E-05	-0.0261	1.30E-07
7 18 PSE Front	-5.7	0.5	25.4	2.2	25.144	-2.62E-05	-0.02566	1.28E-07
7 18 PSE Front	-5.7	1	25.4	1.8	25.144	-2.54E-05	-0.0252	1.25E-07
7 18 PSE Front	-5.7	1.5	25.4	1.6	25.144	-2.46E-05	-0.02473	1.23E-07
7 18 PSE Front	-5.7	2	25.4	1.3	25.144	-2.38E-05	-0.02425	1.21E-07
7 18 PSE Front	-5.7	2.5	25.4	1.1	25.144	-2.30E-05	-0.02376	1.18E-07
7 18 PSE Front	-5.7	3	25.4	1	25.144	-2.23E-05	-0.02327	1.16E-07
7 18 PSE Front	-5.7	3.5	25.4	0.8	25.144	-2.15E-05	-0.02277	1.13E-07
7 18 PSE Front	-5.7	4	25.4	0.7	25.144	-2.07E-05	-0.02227	1.11E-07
7 18 PSE Front	-5.7	4.5	25.4	0.6	25.144	-1.99E-05	-0.02176	1.08E-07
7 18 PSE Front	-5.7	5	25.4	0.5	25.144	-1.91E-05	-0.02126	1.06E-07
8 18 PSE Rear	-1.3	0	25.4	2.9	25.144	-6.38E-05	-0.04339	2.16E-07
8 18 PSE Rear	-1.3	0.5	25.4	2.2	25.144	-6.13E-05	-0.04236	2.10E-07
8 18 PSE Rear	-1.3	1	25.4	1.8	25.144	-5.88E-05	-0.04131	2.05E-07
8 18 PSE Rear	-1.3	1.5	25.4	1.6	25.144	-5.63E-05	-0.04025	2.00E-07
8 18 PSE Rear	-1.3	2	25.4	1.3	25.144	-5.38E-05	-0.03918	1.95E-07
8 18 PSE Rear	-1.3	2.5	25.4	1.1	25.144	-5.13E-05	-0.0381	1.89E-07
8 18 PSE Rear	-1.3	3	25.4	1	25.144	-4.89E-05	-0.03702	1.84E-07
8 18 PSE Rear	-1.3	3.5	25.4	0.8	25.144	-4.66E-05	-0.03595	1.79E-07
8 18 PSE Rear	-1.3	4	25.4	0.7	25.144	-4.43E-05	-0.03488	1.73E-07
8 18 PSE Rear	-1.3	4.5	25.4	0.6	25.144	-4.20E-05	-0.03382	1.68E-07
8 18 PSE Rear	-1.3	5	25.4	0.5	25.144	-3.98E-05	-0.03277	1.63E-07
9 18 PSE South	0	0	25.6	1.6	25.361	-3.55E-05	-0.03844	1.91E-07
9 18 PSE South	0.5	0	25.6	1.3	25.361	-3.98E-05	-0.04108	2.05E-07
9 18 PSE South	1	0	25.6	1.2	25.361	-4.47E-05	-0.04396	2.19E-07
9 18 PSE South	1.5	0	25.6	1	25.361	-5.03E-05	-0.04711	2.34E-07
9 18 PSE South	2	0	25.6	0.9	25.361	-5.67E-05	-0.05056	2.52E-07
9 18 PSE South	2.5	0	25.6	0.8	25.361	-6.42E-05	-0.05434	2.70E-07
9 18 PSE South	3	0	25.6	0.7	25.361	-7.29E-05	-0.05849	2.91E-07
9 18 PSE South	3.5	0	25.6	0.6	25.361	-8.30E-05	-0.06306	3.14E-07
9 18 PSE South	4	0	25.6	0.5	25.361	-9.47E-05	-0.0681	3.38E-07
9 18 PSE South	4.5	0	25.6	0.5	25.361	-1.09E-04	-0.07367	3.66E-07
9 18 PSE South	5	0	25.6	0.4	25.361	-1.25E-04	-0.07983	3.96E-07
9 18 PSE South	5.5	0	25.6	0.4	25.361	-1.44E-04	-0.08666	4.30E-07
9 18 PSE South	6	0	25.6	0.3	25.361	-1.66E-04	-0.09424	4.68E-07
9 18 PSE South	6.5	0	25.6	0.3	25.361	-1.93E-04	-0.10268	5.09E-07
9 18 PSE South	7	0	25.6	0.3	25.361	-2.25E-04	-0.1121	5.56E-07
9 18 PSE South	7.5	0	25.6	0.3	25.361	-2.63E-04	-0.12261	6.07E-07
9 18 PSE South	8	0	25.6	0.2	25.361	-3.09E-04	-0.13437	6.65E-07

9 18 PSE South	8.5	0	25.6	0.2	25.361	-3.65E-04	-0.14755	7.30E-07
9 18 PSE South	9	0	25.6	0.2	25.361	-4.32E-04	-0.16234	8.02E-07
9 18 PSE South	9.5	0	25.6	0.2	25.361	-5.13E-04	-0.17895	8.84E-07
9 18 PSE South	10	0	25.6	0.2	25.361	-6.12E-04	-0.19761	9.75E-07
9 18 PSE South	10.5	0	25.6	0.2	25.361	-7.33E-04	-0.21858	1.08E-06
9 18 PSE South	11	0	25.6	0.2	25.361	-8.80E-04	-0.24214	1.19E-06
9 18 PSE South	11.5	0	25.6	0.3	25.361	-0.0010596	-0.26855	1.32E-06
9 18 PSE South	12	0	25.6	0.3	25.361	-0.0012787	-0.29808	1.46E-06
9 18 PSE South	12.5	0	25.6	0.3	25.361	-0.0015448	-0.33096	1.62E-06
9 18 PSE South	13	0	25.6	0.3	25.361	-0.001866	-0.36732	1.80E-06
9 18 PSE South	13.5	0	25.6	0.3	25.361	-0.0022498	-0.40718	1.99E-06
9 18 PSE South	14	0	25.6	0.4	25.361	-0.0027016	-0.45033	2.19E-06
9 18 PSE South	14.5	0	25.6	0.4	25.361	-0.0032221	-0.49625	2.41E-06
9 18 PSE South	15	0	25.6	0.4	25.361	-0.003804	-0.54401	2.64E-06
9 18 PSE South	15.5	0	25.6	0.5	25.361	-0.0044283	-0.59222	2.87E-06
9 18 PSE South	16	0	25.6	0.5	25.361	-0.0050617	-0.639	3.09E-06
9 18 PSE South	16.5	0	25.6	0.6	25.361	-0.0056572	-0.68209	3.29E-06
9 18 PSE South	17	0	25.6	0.6	25.361	-0.0061598	-0.71905	3.46E-06
10 Vault Area	-3.5	-1	25	4.5	24.769	-6.3807	-16.729	-5.46E-05
10 Vault Area	-3.5	-1.5	25	3.4	24.769	-12.559	-30.08	-1.22E-04
10 Vault Area	-3.5	-2	25	3.1	24.769	-12.731	-32.024	-1.16E-04
10 Vault Area	-3.5	-2.5	25	3.1	24.769	-12.733	-32.141	-1.15E-04
10 Vault Area	-3.5	-3	25	3.3	24.769	-12.565	-30.503	-1.20E-04
10 Vault Area	-3.5	-3.5	25	4.3	24.769	-6.406	-17.792	-4.98E-05
10 Vault Area	-3.5	-4	25	5.1	24.769	-0.40296	-6.5189	2.39E-05
10 Vault Area	-3.5	-4.5	25	4.3	24.769	-6.406	-17.793	-4.98E-05
10 Vault Area	-3.5	-5	25	3.3	24.769	-12.565	-30.504	-1.20E-04
10 Vault Area	-3.5	-5.5	25	3	24.769	-12.733	-32.143	-1.15E-04
10 Vault Area	-3.5	-6	25	3	24.769	-12.731	-32.026	-1.16E-04
10 Vault Area	-3.5	-6.5	25	3.2	24.769	-12.559	-30.083	-1.22E-04
10 Vault Area	-3.5	-7	25	4.2	24.769	-6.3807	-16.732	-5.46E-05
Davida Carrana								
Park Square 11 East Road	-5.7	-4	29	2.9	28.688	0	0	0
Park Square								
11 East Road	-6.2	-4	29	2.4	28.688	0	0	0
Park Square								
11 East Road	-6.7	-4	29	2	28.688	0	0	0
Park Square								
11 East Road	-7.2	-4	29	1.7	28.688	0	0	0

Park Square 11 East Road	-7.7	-4	29	1.5	28.688	0	0	0
Park Square 11 East Road	-8.2	-4	29	1.3	28.688	0	0	0
Park Square 11 East Road	-8.7	-4	29	1.1	28.688	0	0	0
Park Square 11 East Road	-9.2	-4	29	1	28.688	0	0	0
Park Square 11 East Road	-9.7	-4	29	0.8	28.688	0	0	0
Park Square 11 East Road	-10.2	-4	29	0.7	28.688	0	0	0
Park Square 11 East Road	-10.7	-4	29	0.6	28.688	0	0	0
Park Square 11 East Road	-11.2	-4	29	0.5	28.688	0	0	0
Park Square 11 East Road	-11.7	-4	29	0.5	28.688	0	0	0
Park Square 11 East Road	-12.2	-4	29	0.4	28.688	0	0	0
Park Square 11 East Road	-12.7	-4	29	0.4	28.688	0	0	0
Park Square 11 East Road	-13.2	-4	29	0.3	28.688	0	0	0
Park Square 11 East Road	-13.7	-4	29	0.3	28.688	0	0	0
Park Square 11 East Road	-14.2	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-14.7	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-15.2	-4	29	0.2	28.688	0	0	0
Park Square 11 East Road	-15.7	-4	29	0.2	28.688	0	0	0

Results : Consolidation : Displacement Data :

Lines

Results : Total : Displacement Data :

Lines

None