

Appendix B Contents

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APPENDIX – PART 1B

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Excavation Method Drive-in Windowless Sampler	Dimensions	Ground Level (mOD) 85.55	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 13/01/2016	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
				85.45	0.10	Brick Paving		
				85.40	(0.15)	Made Ground (yellowish brown sand with gravel)		
				85.25	0.30	Concrete		
					(1.10)	Made Ground (brown to dark brown silty sandy clay with gravel and occasional brick fragments)		
1.20	D1			84.15	1.40	Made Ground (pale greenish grey and orange-brown slightly sandy silty clay with occasional gravel, carbonaceous material and brick fragments)		
1.50	D2				(0.70)			
1.90	D3			83.45	2.10	Made Ground (orange-brown slightly sandy silty clay with gravel; dark grey between 2.7-2.8m)		
2.25	D4				(1.00)			
2.75	D5		Slow Inflow(1) at 3.00m, not sealed.	82.45	3.10	Firm becoming stiff brown becoming brownish grey silty CLAY		∇1
3.50	D6			81.55	4.00	Terminated at 4.00m		

Remarks Groundwater monitoring standpipe installed to 3.1m Borehole completed from base of Trial Pit No 5	Scale (approx)	Logged By
	1:50	JS
	Figure No. J15315.BH1	

Excavation Method Drive-in Windowless Sampler	Dimensions	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 13/01/2016	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
0.50	D1			85.40 85.35 85.30	0.10 0.15 0.20	Brick Paving Made Ground (yellowish brown sand with gravel) Concrete Made Ground (brown, orange-brown and greenish grey silty sandy clay with gravel, rootlets and brick fragments)		
1.50	D2				(3.00)			
2.50	D3							
3.35	D4		Slow Inflow(1) at 3.00m, not sealed.	82.30 82.00 81.80	3.20 (0.30) 3.50 (0.20) 3.70	Firm greenish grey to orange-brown & dark grey slightly silty CLAY with gravel and carbonaceous material Firm mottled pale grey to bluish & orange-brown slightly silty CLAY with occasional gravel Firm becoming stiff brown becoming brownish grey silty CLAY		
4.50	D5				(1.30)			
				80.50	5.00	Terminated at 5.00m		

Remarks Groundwater monitoring standpipe installed to 4.0 m	Scale (approx)	Logged By
	1:50	JS
	Figure No. J15315.BH2	

Excavation Method Drive-in Windowless Sampler	Dimensions	Ground Level (mOD) 85.40	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 13/01/2016	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
2.00	D1			83.70	(1.70)	Made Ground (brown to dark brown sandy silty clay with gravel, ash, charcoal, rootlets and brick fragments)		
					(0.70)	Made Ground (orange-brown & grey mottled slightly silty clay with rare brick fragments)		
3.00	D2			83.00	(1.35)	Firm greenish grey and orange-brown slightly silty CLAY with carbonaceous material and gravel		
4.00-4.50	D3			81.65	(0.75)	Firm becoming stiff pale orange-brown becoming brownish grey slightly silty CLAY		
					(4.50)	Terminated at 4.50m		

Remarks Taken from base of TP6 Groundwater not encountered Groundwater monitoring standpipe installed at 3.0m	Scale (approx)	Logged By
	1:50	JS
	Figure No. J15315.BH3	

Excavation Method Opendrive lined percussive sampler	Dimensions 110mm to 1.00m	Ground Level (mOD) 85.40	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 20/01/2016	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
1.00-1.45	SPT N=7		1,2/2,1,2,2	85.35 85.28	(0.05) 0.05 (0.05) 0.10 (0.05) 0.15 (1.55)	Paving Stone Made Ground (orange-brown sand) Concrete Made Ground (brown to orange brown mottled grey silty clay with gravel, brick fragments, charcoal, ash and roots)		
2.00-2.45	SPT N=6		0,0/1,2,1,2	83.70	1.70 (0.80)	Made Ground (grey and orange-brown mottled slightly silty clay with rare brick fragments and rootlets)		
3.00-3.45 3.00	SPT N=7 D1		0,0/1,2,2,2 Slow Inflow(1) at 3.30m, not sealed.	82.90	2.50 (1.00)	Firm pale orange-brown and greenish grey silty CLAY with occasional gravel and carbonaceous material; dark grey carbonaceous layers at 2.8 m to 3.0 m and 3.3 m to 3.4 m		
4.00-4.45 4.00	SPT N=7 D2		2,1/2,1,2,2	81.90 81.70	3.50 (0.20) 3.70	Firm pale orange-brown mottled grey slightly silty CLAY Firm becoming stiff pale orange-brown becoming brownish grey slightly silty CLAY with rare selenite crystals and occasional partings of silt and sand		
4.50	D3		2,1/2,1,2,2		(1.30)			
5.00-5.45	SPT N=10		2,1/2,2,3,3	80.40	5.00	Stiff dark brownish grey slightly silty CLAY with occasional partings of silt and sand; claystone encountered at 6.5 m to 6.7 m		
5.50	D4							
6.00-6.45	SPT N=14		2,2/2,2,3,7					
6.50	D5							
7.00-7.45	SPT N=13		2,3/2,3,4,4					
7.50	D6				(5.00)			
8.00-8.45	SPT N=13		2,2/3,3,3,4					
8.50	D7							
9.00-9.45	SPT N=13		2,3/3,3,4,3					
9.50	D8							
10.00-10.45	SPT N=11		2,2/1,3,3,4	75.40	10.00			

Remarks
Groundwater monitoring standpipe installed at 5.0m.
SPT N results potentially impacted by proximity to BH3 and the potential effects of water softening in the base of the borehole, such that the results are not considered to represent the true in-situ strength.
The assessment of the strength for the natural soils is therefore based on a combination of the test results together with the field observations, which indicated a firm becoming stiff consistency, and not just the SPT 'N' results alone.

Scale (approx)	Logged By
1:50	JS
Figure No. J15315.BH4	

Excavation Method Opendrive percussive lined sampler	Dimensions 110mm to 1.00m	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 11/07/2017	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Sample / Tests	Water Depth (m)	Field Records	Level (mOD)	Depth (m) (Thickness)	Description	Legend	Water
1.00-1.45	SPT(C) N=9	DRY	0,1/2,2,2,3	85.40	0.10	Brick Paving		
				85.35	0.15	Made Ground (yellowish brown sand)		
				85.30	0.20	Concrete		
2.00-2.45	SPT(C) N=8	DRY	1,1/2,2,2,2	83.30	2.20 (0.75)	Made Ground (brown silty slightly sandy clay with occasional gravel, ash and small brick fragments)		
						Made Ground (brown silty clay with rare brick fragments)		
3.00-3.45	SPT(C) N=8	DRY	0,0/0,3,2,3	82.55	2.95 (0.45)	Made Ground (greenish brown silty clay with very rare brick fragments)		
						Made Ground (greenish brown silty clay with very rare brick fragments)		
4.00-4.45	SPT N=12	DRY	2,2/3,3,3,3	82.10	3.40 (2.05)	Firm becoming stiff brownish grey silty CLAY with relic root traces		
						Firm becoming stiff brownish grey silty CLAY with relic root traces		
5.00-5.45	SPT N=16	DRY	2,2/3,4,5,4	80.05	5.45	Complete at 5.45m		

Remarks Groundwater not encountered during drilling and borehole remained dry throughout an observation period of approximately 4 hours.	Scale (approx)	Logged By
	1:50	MP
	Figure No. j15315.BH5	

Method DPSH	Cone Dimensions	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 11/07/2017	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Blows for Depth Increment	Field Records	Level (mOD)	Depth (m)	Blows for Depth Increment																
					0	1	2	3	4	5	6	7	8	9	10						
0.10-0.20	1		85.50	0.00																	
0.20-0.30	1																				
0.30-0.40	0																				
0.40-0.50	0																				
0.50-0.60	1		85.00	0.50																	
0.60-0.70	0																				
0.70-0.80	0																				
0.80-0.90	2																				
0.90-1.00	3																				
1.00-1.10	1		84.50	1.00																	
1.10-1.20	1																				
1.20-1.30	1																				
1.30-1.40	0																				
1.40-1.50	1																				
1.50-1.60	0		84.00	1.50																	
1.60-1.70	1																				
1.70-1.80	0																				
1.80-1.90	0																				
1.90-2.00	1																				
2.00-2.10	0		83.50	2.00																	
2.10-2.20	0																				
2.20-2.30	1																				
2.30-2.40	0																				
2.40-2.50	0		83.00	2.50																	
2.50-2.60	1																				
2.60-2.70	0																				
2.70-2.80	1																				
2.80-2.90	1																				
2.90-3.00	0		82.50	3.00																	
3.00-3.10	2																				
3.10-3.20	1																				
3.20-3.30	2																				
3.30-3.40	1																				
3.40-3.50	2		82.00	3.50																	
3.50-3.60	2																				
3.60-3.70	2																				
3.70-3.80	2																				
3.80-3.90	3																				
3.90-4.00	3		81.50	4.00																	
4.00-4.10	4																				
4.10-4.20	3																				
4.20-4.30	4																				
4.30-4.40	4																				
4.40-4.50	3		81.00	4.50																	
4.50-4.60	3																				
4.60-4.70	4																				
4.70-4.80	3																				
4.80-4.90	4		80.50	5.00																	
4.90-5.00	4																				
5.00-5.10	5																				
5.10-5.20	6		80.00	5.50																	
5.20-5.30	6																				
5.30-5.40	6																				
5.40-5.50	5																				
5.50-5.60	5																				
5.60-5.70	6		79.50	6.00																	
5.70-5.80	5																				
5.80-5.90	7																				
5.90-6.00	7		79.00	6.50																	
			78.50	7.00																	
			78.00	7.50																	
			77.50	8.00																	

Remarks

Groundwater not encountered
Classification after Huntley (1990): Very Soft = <1; Soft = 1 to 2; Firm: 3 to 4; Stiff = 5 to 8; Very stiff = > 8

Scale (approx)	Logged By
1:40	MJD
Figure No.	
J15315.DP1	

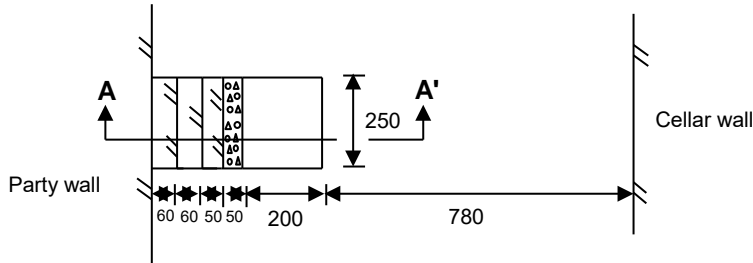
Method Super Heavy Dynamic Probe (DPSH)	Cone Dimensions	Ground Level (mOD) 85.40	Client Manuela Eleuteri	Job Number J15315
	Location	Dates 11/07/2017	Engineer Richard Tant Associates	Sheet 1/1

Depth (m)	Blows for Depth Increment	Field Records	Level (mOD)	Depth (m)	Blows for Depth Increment															
					0	1	2	3	4	5	6	7	8	9	10					
0.00-0.10	2		85.40	0.00																
0.10-0.20	3																			
0.20-0.30	2																			
0.30-0.40	1																			
0.40-0.50	1																			
0.50-0.60	1		84.90	0.50																
0.60-0.70	2																			
0.70-0.80	1																			
0.80-0.90	1																			
0.90-1.00	1																			
1.00-1.10	1		84.40	1.00																
1.10-1.20	1																			
1.20-1.30	2																			
1.30-1.40	1																			
1.40-1.50	0																			
1.50-1.60	0		83.90	1.50																
1.60-1.70	1																			
1.70-1.80	0																			
1.80-1.90	0																			
1.90-2.00	1		83.40	2.00																
2.00-2.10	0																			
2.10-2.20	0																			
2.20-2.30	1																			
2.30-2.40	0																			
2.40-2.50	0		82.90	2.50																
2.50-2.60	0																			
2.60-2.70	1																			
2.70-2.80	0																			
2.80-2.90	1		82.40	3.00																
2.90-3.00	1																			
3.00-3.10	1																			
3.10-3.20	1																			
3.20-3.30	2																			
3.30-3.40	2																			
3.40-3.50	2		81.90	3.50																
3.50-3.60	2																			
3.60-3.70	2																			
3.70-3.80	2																			
3.80-3.90	3																			
3.90-4.00	3		81.40	4.00																
4.00-4.10	3																			
4.10-4.20	4																			
4.20-4.30	4																			
4.30-4.40	4																			
4.40-4.50	3		80.90	4.50																
4.50-4.60	4																			
4.60-4.70	4																			
4.70-4.80	3																			
4.80-4.90	4		80.40	5.00																
4.90-5.00	4																			
5.00-5.10	5																			
5.10-5.20	5		79.90	5.50																
5.20-5.30	7																			
5.30-5.40	6																			
5.40-5.50	7		79.40	6.00																
5.50-5.60	7																			
5.60-5.70	7																			
5.70-5.80	7																			
5.80-5.90	7		78.90	6.50																
5.90-6.00	7																			
			78.40	7.00																
			77.90	7.50																
			77.40	8.00																

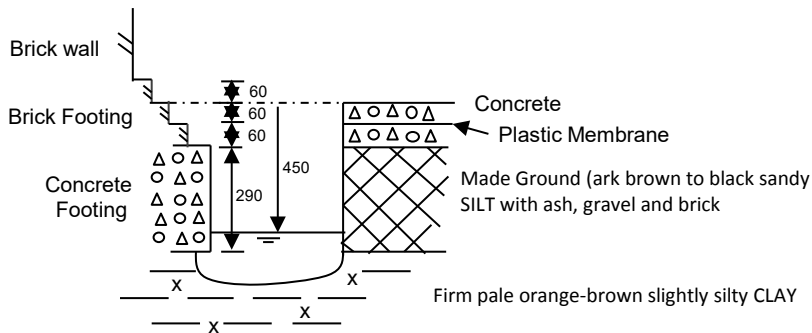
Remarks Groundwater not encountered Classification after Huntley (1990): Very Soft = <1; Soft = 1 to 2; Firm: 3 to 4; Stiff = 5 to 8; Very stiff = > 8	Scale (approx)	Logged By
	1:40	MJD
	Figure No. J15315.DP2	

Excavation Method Manual	Dimensions 250 x 420 x 500	Ground Level (mOD) 83.85	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 1/1

PLAN



SECTION A - A'

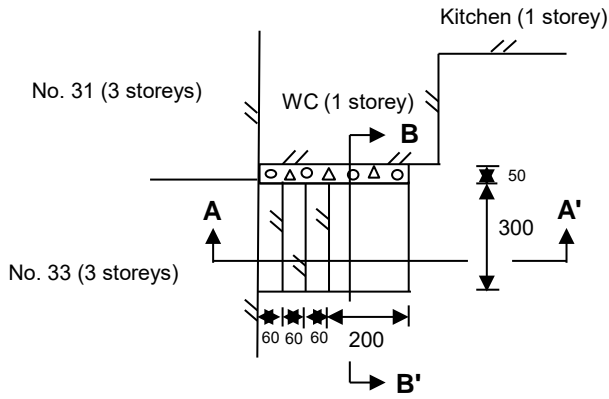


Remarks:
All dimensions in millimetres
Trial pit sides remained stable during excavation
Groundwater encountered at a depth of 0.45 m

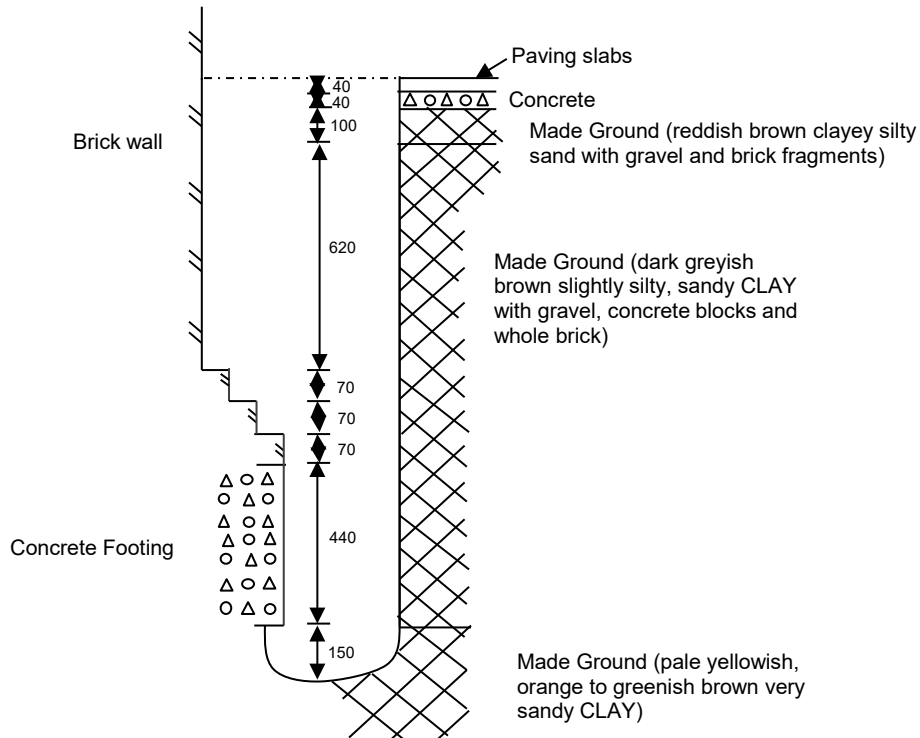
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Logged by:
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Excavation Method Manual	Dimensions 350 x 380 x 1600	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 1/2

PLAN



SECTION A - A'



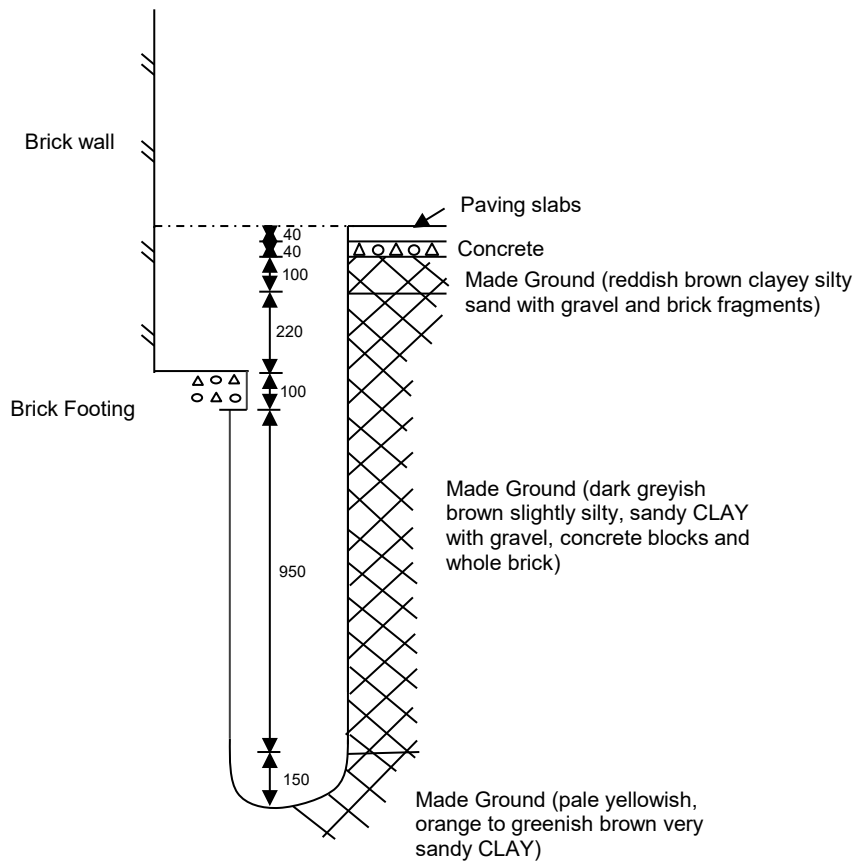
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All dimensions in millimetres
Trial pit sides remained stable during excavation
Groundwater not encountered

Scale:
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Logged by:
JS

Excavation Method Manual	Dimensions 350 x 380 x 1600	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 2/2

SECTION B - B'

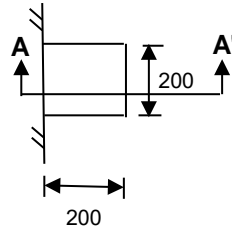


Remarks:
All dimensions in millimetres
Trial pit sides remained stable during excavation
Groundwater not encountered

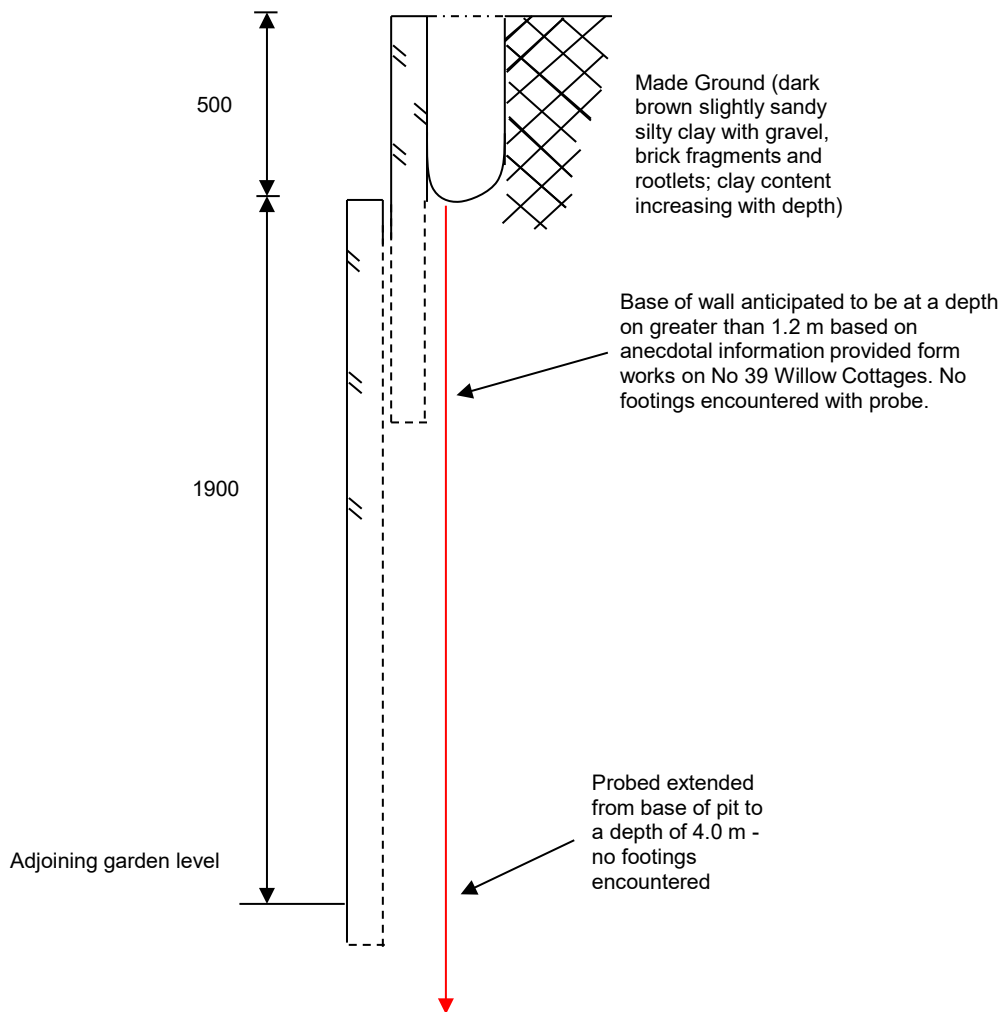
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Excavation Method Manual	Dimensions 200 x 200 x 500	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 1/1

PLAN



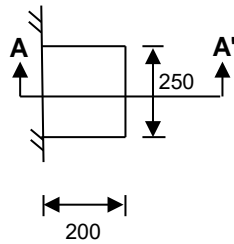
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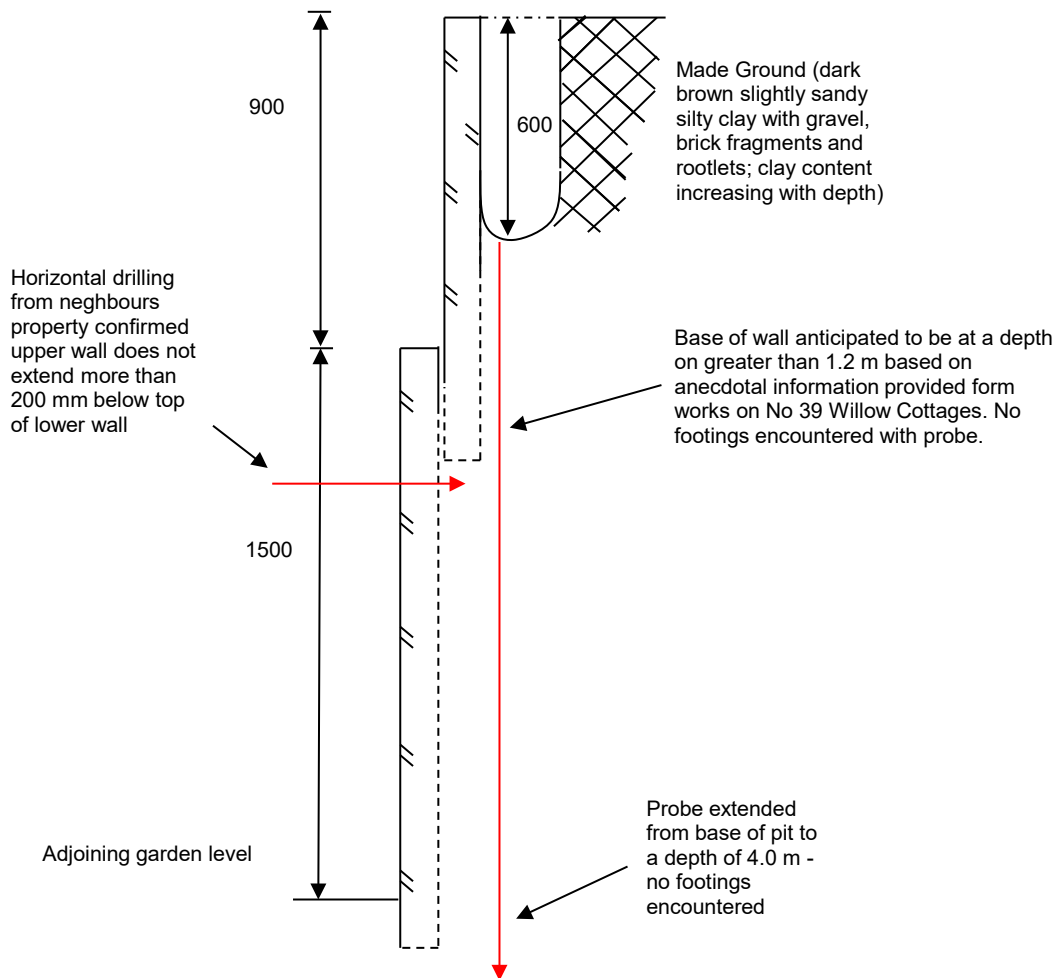
Remarks: All dimensions in millimetres Trial pit sides remained stable during excavation Groundwater not encountered	Scale: 1:20
	Logged by: JS

Excavation Method Manual	Dimensions 200 x 250 x 600	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 1/1

PLAN



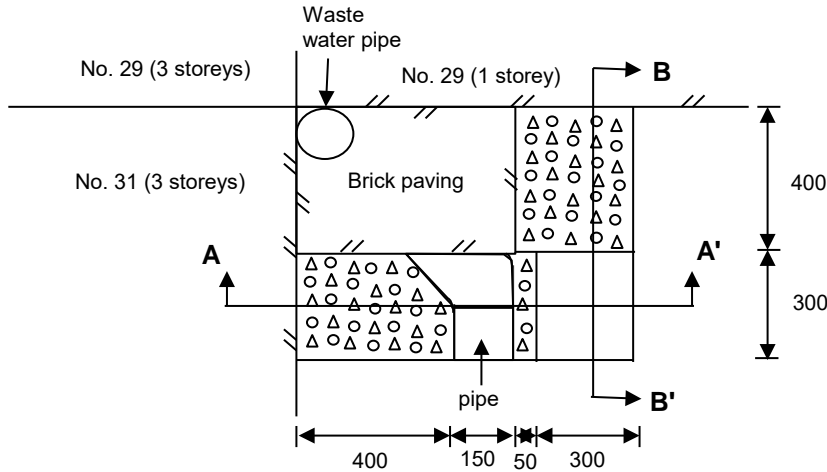
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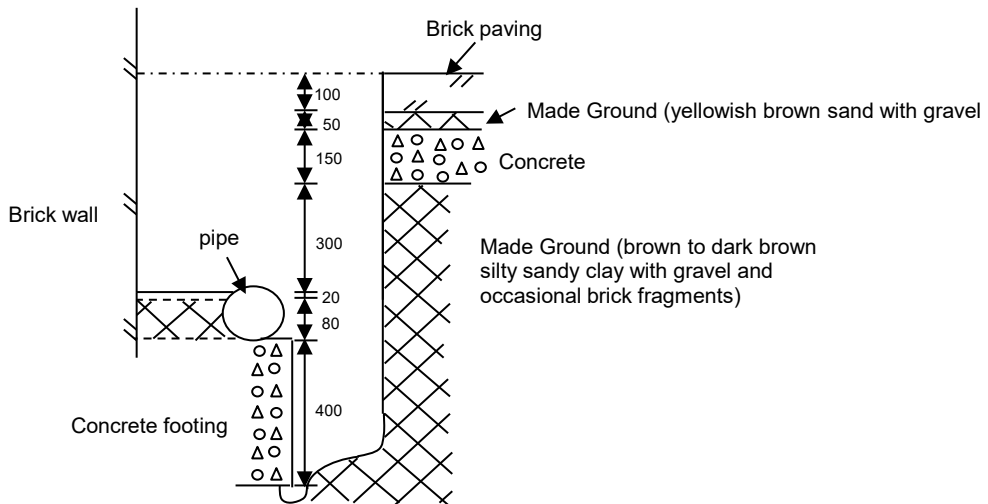
Remarks: All dimensions in millimetres Trial pit sides remained stable during excavation Groundwater not encountered	Scale: 1:20
	Logged by: JS

Excavation Method Manual	Dimensions 700 x 900 x 1200	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 1/2

PLAN



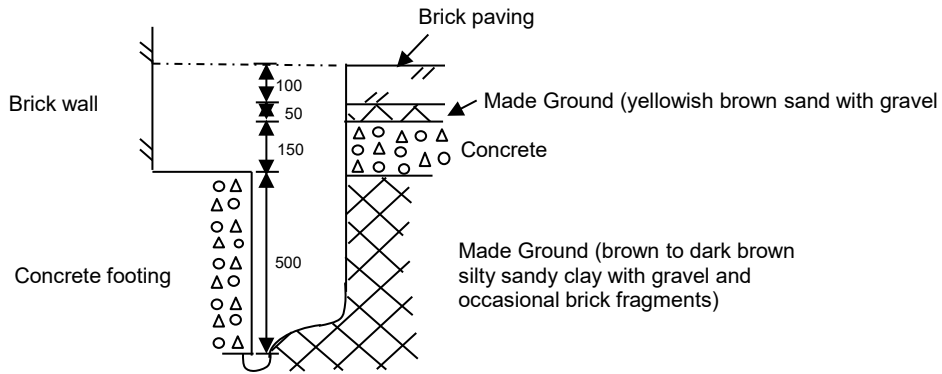
SECTION A - A'



Remarks: All dimensions in millimetres Trial pit sides remained stable during excavation Groundwater not encountered	Scale: 1:20
	Logged by: JS

Excavation Method Manual	Dimensions 700 x 900 x 1200	Ground Level (mOD) 85.50	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 2/2

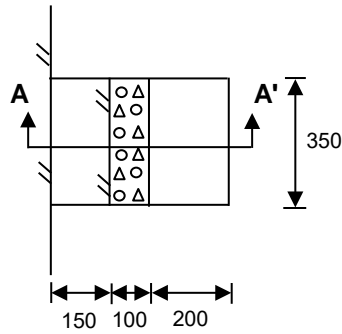
SECTION B - B'



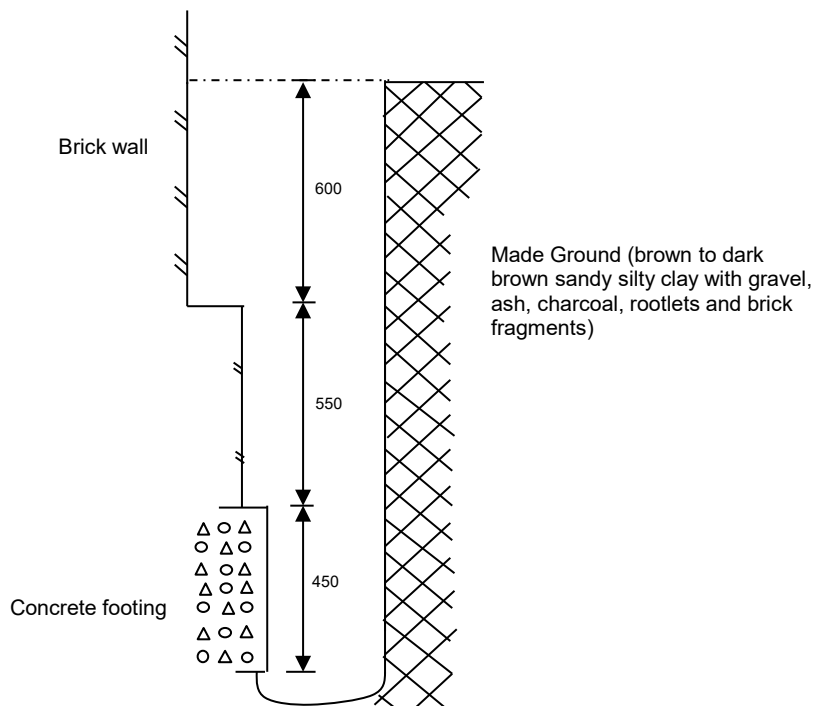
Remarks: All dimensions in millimetres Trial pit sides remained stable during excavation Groundwater not encountered	Scale: 1:20
	Logged by: JS

Excavation Method Manual	Dimensions 350 x 450 x 1800	Ground Level (mOD) 85.40	Client Manuela Eleuteri	Job Number J15315
	Location Ground Level	Dates 12/01/16 to 13/01/16	Engineer Richard Tant Associates	Sheet 1/1

PLAN



SECTION A - A'



Remarks:
All dimensions in millimetres
Trial pit sides remained stable during excavation
Groundwater not encountered

Scale:
1:20
Logged by:
JS

Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

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View of TP1 - looking southeast



View into TP1 - looking southeast

Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

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View of TP2 - looking southeast



View into TP2 - looking southeast

Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

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View of TP3 - looking northeast



View into TP3 - looking north

Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

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View of TP4 - looking northwest



Plan view of TP4 - looking northwest

Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

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View of TP5 - looking southeast



View into TP5 - looking east

Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

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View of TP6 - looking northwest



View into TP6 - looking northeast



Summary of Test Results

Job No. 20228	Project Name 31 Willoughby Road	Programme	
		Samples received	21/01/2016
Project No. J15315	Client GEA	Schedule received	21/01/2016
		Project started	22/01/2016
		Testing Started	02/02/2016

Hole No.	Sample				Soil Description	NMC %	Passing 425µm %	LL %	PL %	PI %	Remarks
	Ref	Top	Base	Type							
BH1	6	3.50		D	Brown and occasional blue grey silty CLAY	33	100	63	23	40	
BH2	5	4.50		D	Brown and occasional blue grey silty CLAY with rare fine gravel	32	99	64	26	38	
BH4	1	3.00		D	Dark grey slightly fine sandy slightly gravelly silty CLAY (gravel is fine)	30	97	48	24	24	
BH4	3	4.50		D	Brown and occasional blue grey silty CLAY with rare fine gravel	31	99	69	25	44	
BH4	5	6.50		D	Dark brown silty CLAY with rare fine gravel	32	99	70	24	46	
BH4	7	8.50		D	Dark blue grey silty CLAY with rare fine gravel	29	99	67	25	42	

	Test Methods: BS1377: Part 2: 1990: Natural Moisture Content : clause 3.2 Atterberg Limits: clause 4.3 and 5.0	Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU Tel: 01923 711 288 Email: James@k4soils.com	Checked and Approved Initials J.P Date: 03/02/2016
	Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)		MSF-5-R1(a) -Rev. 0



Unit A2
Windmill Road
Ponswood Industrial Estate
St Leonards on Sea
East Sussex
TN38 9BY
Telephone: (01424) 718618
Facsimile: (01424) 729911
info@elab-uk.co.uk

THE ENVIRONMENTAL LABORATORY LTD

Analytical Report Number: 16-05425

Issue: 1

Date of Issue: 29/01/2016

Contact: James Phaure

Customer Details: K4 Soils Laboratory Ltd
Unit 8
Watford
Hertfordshire WD18 9RU

Quotation No: Q15-00248

Order No: 20228

Customer Reference: J15315

Date Received: 27/01/2016

Date Approved: 29/01/2016

Details: 31 Willoughby Way

Approved by:

John Wilson, Operations Manager

Any comments, opinions or interpretations expressed herein are outside the scope of UKAS accreditation (Accreditation Number 2683)



Sample Summary

Report No.: 16-05425

Elab No.	Client's Ref.	Date Sampled	Date Scheduled	Description	Deviations
51816	BH4 D1 3.00	Not Provided	27/01/2016	Silty loam	a



2683

Results Summary

Report No.: 16-05425

ELAB Reference	51816
Customer Reference	D1
Sample ID	
Sample Type	SOIL
Sample Location	BH4
Sample Depth (m)	3.00
Sampling Date	

Determinand	Codes	Units	LOD	
Miscellaneous				
Soil Organic Matter	U	%	0.1	3.3



Method Summary

Report No.: 16-05425

Parameter	Codes	Analysis Undertaken On	Date Tested	Method Number	Technique
Soil					
Soil organic matter	U	Air dried sample	29/01/2016	BS1377:P3	Titrimetry



Report Information

Report No.: 16-05425

Key

U	hold UKAS accreditation
M	hold MCERTS and UKAS accreditation
N	do not currently hold UKAS accreditation
^	MCERTS accreditation not applicable for sample matrix
*	UKAS accreditation not applicable for sample matrix
S	Subcontracted to approved laboratory UKAS Accredited for the test
SM	Subcontracted to approved laboratory MCERTS/UKAS Accredited for the test
I/S	Insufficient Sample
U/S	Unsuitable sample
n/t	Not tested
<	means "less than"
>	means "greater than"

Soil sample results are expressed on an air dried basis

Comments or interpretations are beyond the scope of UKAS accreditation

The results relate only to the items tested

PCB congener results may include any coeluting PCBs

Uncertainty of measurement for the determinands tested are available upon request

Deviation Codes

-
- | | |
|---|--|
| a | No date of sampling supplied |
| b | No time of sampling supplied (Waters Only) |
| c | Sample not received in appropriate containers |
| d | Sample not received in cooled condition |
| e | The container has been incorrectly filled |
| f | Sample age exceeds stability time (sampling to receipt) |
| g | Sample age exceeds stability time (sampling to analysis) |

Where a sample has a deviation code, the applicable test result may be invalid.

Sample Retention and Disposal

All soil samples will be retained for a period of one month

All water samples will be retained for 7 days following the date of the test report

Charges may apply to extended sample storage

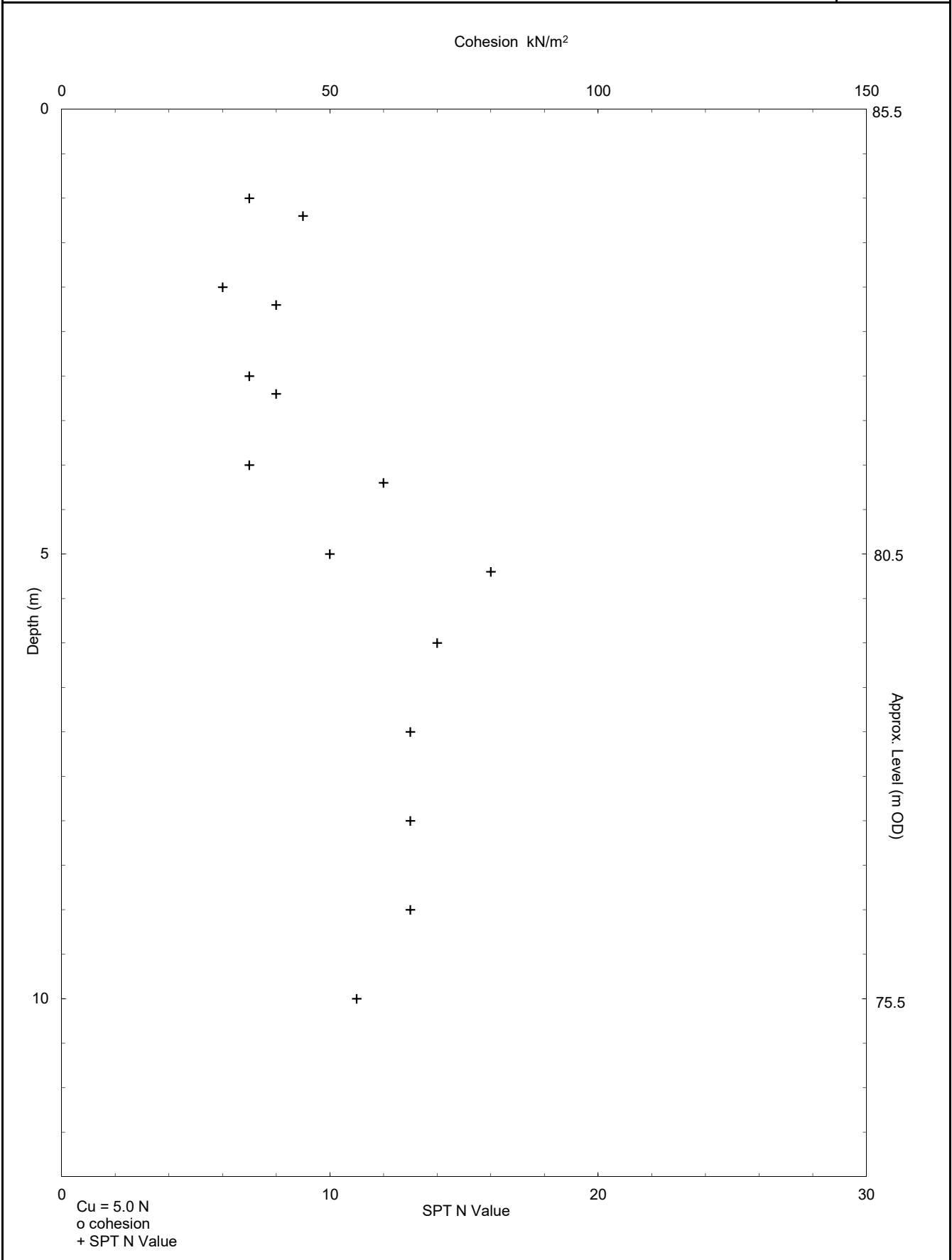
Site 31 Willoughby Road, London, NW3 1RT

Client Manuela Eleuteri

Engineer Richard Tant Associates

Job Number
J15315

Sheet
1 / 1



Project: J15315 - 31 Willoughby Road, London, NW3 1RT

Client: GEA	Chemtest Job No.:				16-00910	16-00910	16-00910	16-00910
Quotation No.:	Chemtest Sample ID.:				241134	241135	241136	241139
Order No.:	Client Sample Ref.:				BH1	BH2	TP1	TP6
	Client Sample ID.:				1	1	1	1
	Sample Type:				SOIL	SOIL	SOIL	SOIL
	Top Depth (m):				2.25	0.50	0.40	0.50
	Bottom Depth (m):							1.00
	Date Sampled:				13-Jan-2016	13-Jan-2016	13-Jan-2016	13-Jan-2016
Determinand	Accred.	SOP	Units	LOD				
Moisture	N	2030	%	0.020	23	21	27	16
Stones	N	2030	%	0.020	< 0.020	< 0.020	< 0.020	< 0.020
Soil Colour	N	2040		N/A	Brown	Brown	Brown	Brown
Other Material	N	2040		N/A	Stones	Stones	Stones	Stones, Brick
Soil Texture	N	2040		N/A	Clay	Clay	Clay	Clay
pH	M	2010		N/A	7.3	8.1	8.2	8.2
Sulphate (2:1 Water Soluble) as SO ₄	M	2120	g/l	0.010	0.058	< 0.010	0.16	0.011
Chloride (Extractable)	M	2220	g/l	0.010	0.023	< 0.010	0.019	< 0.010
Cyanide (Total)	M	2300	mg/kg	0.50	< 0.50	< 0.50	< 0.50	< 0.50
Sulphide (Easily Liberatable)	M	2325	mg/kg	0.50	2.1	1.6	6.8	1.9
Sulphate (Total)	M	2430	mg/kg	100	1300	850	3000	1100
Arsenic	M	2450	mg/kg	1.0	9.8	17	47	19
Cadmium	M	2450	mg/kg	0.10	0.10	< 0.10	< 0.10	< 0.10
Chromium	M	2450	mg/kg	1.0	39	40	52	34
Copper	M	2450	mg/kg	0.50	16	33	270	50
Mercury	M	2450	mg/kg	0.10	< 0.10	0.80	0.13	0.66
Nickel	M	2450	mg/kg	0.50	43	25	53	25
Lead	M	2450	mg/kg	0.50	37	330	670	350
Selenium	M	2450	mg/kg	0.20	0.28	< 0.20	< 0.20	< 0.20
Zinc	M	2450	mg/kg	0.50	58	81	180	120
Total Organic Carbon	M	2625	%	0.20	0.41	0.67	5.8	1.1
TPH >C5-C6	N	2670	mg/kg	1.0	< 1.0	< 1.0	< 1.0	< 1.0
TPH >C6-C7	N	2670	mg/kg	1.0	< 1.0	< 1.0	< 1.0	< 1.0
TPH >C7-C8	N	2670	mg/kg	1.0	< 1.0	< 1.0	< 1.0	< 1.0
TPH >C8-C10	N	2670	mg/kg	1.0	< 1.0	< 1.0	< 1.0	< 1.0
TPH >C10-C12	N	2670	mg/kg	1.0	< 1.0	< 1.0	< 1.0	< 1.0
TPH >C12-C16	N	2670	mg/kg	1.0	< 1.0	< 1.0	< 1.0	4.7
TPH >C16-C21	N	2670	mg/kg	1.0	< 1.0	2.7	< 1.0	31
TPH >C21-C35	N	2670	mg/kg	1.0	< 1.0	5.3	< 1.0	38
Total TPH >C5-C35	N	2670	mg/kg	10	< 10	< 10	< 10	74
Naphthalene	M	2700	mg/kg	0.10	< 0.10	< 0.10	< 0.10	2.6
Acenaphthylene	M	2700	mg/kg	0.10	< 0.10	< 0.10	< 0.10	0.20
Acenaphthene	M	2700	mg/kg	0.10	< 0.10	< 0.10	< 0.10	1.5
Fluorene	M	2700	mg/kg	0.10	< 0.10	< 0.10	< 0.10	1.5
Phenanthrene	M	2700	mg/kg	0.10	< 0.10	< 0.10	< 0.10	19
Anthracene	M	2700	mg/kg	0.10	< 0.10	< 0.10	< 0.10	2.2
Fluoranthene	M	2700	mg/kg	0.10	< 0.10	0.76	0.45	21
Pyrene	M	2700	mg/kg	0.10	< 0.10	0.71	0.47	19

Project: J15315 - 31 Willoughby Road, London, NW3 1RT

Client: GEA		Chemtest Job No.:		16-00910	16-00910	16-00910	16-00910
Quotation No.:		Chemtest Sample ID.:		241134	241135	241136	241139
Order No.:		Client Sample Ref.:		BH1	BH2	TP1	TP6
		Client Sample ID.:		1	1	1	1
		Sample Type:		SOIL	SOIL	SOIL	SOIL
		Top Depth (m):		2.25	0.50	0.40	0.50
		Bottom Depth (m):					1.00
		Date Sampled:		13-Jan-2016	13-Jan-2016	13-Jan-2016	13-Jan-2016
Determinand	Accred.	SOP	Units	LOD			
Benzo[a]anthracene	M	2700	mg/kg	0.10	< 0.10	< 0.10	9.3
Chrysene	M	2700	mg/kg	0.10	< 0.10	< 0.10	9.7
Benzo[b]fluoranthene	M	2700	mg/kg	0.10	< 0.10	< 0.10	11
Benzo[k]fluoranthene	M	2700	mg/kg	0.10	< 0.10	< 0.10	4.5
Benzo[a]pyrene	M	2700	mg/kg	0.10	< 0.10	< 0.10	7.6
Indeno(1,2,3-c,d)Pyrene	M	2700	mg/kg	0.10	< 0.10	< 0.10	5.2
Dibenz(a,h)Anthracene	M	2700	mg/kg	0.10	< 0.10	< 0.10	1.3
Benzo[g,h,i]perylene	M	2700	mg/kg	0.10	< 0.10	< 0.10	4.1
Total Of 16 PAH's	M	2700	mg/kg	2.0	< 2.0	< 2.0	120
Total Phenols	M	2920	mg/kg	0.30	< 0.30	< 0.30	< 0.30

Report Information

Key

- U UKAS accredited
- M MCERTS and UKAS accredited
- N Unaccredited
- S This analysis has been subcontracted to a UKAS accredited laboratory that is accredited for this analysis
- SN This analysis has been subcontracted to a UKAS accredited laboratory that is not accredited for this analysis
- T This analysis has been subcontracted to an unaccredited laboratory
- I/S Insufficient Sample
- U/S Unsuitable Sample
- N/E not evaluated
- < "less than"
- > "greater than"

Comments or interpretations are beyond the scope of UKAS accreditation

The results relate only to the items tested

Uncertainty of measurement for the determinands tested are available upon request

None of the results in this report have been recovery corrected

All results are expressed on a dry weight basis

The following tests were analysed on samples as received and the results subsequently corrected to a dry weight basis TPH, BTEX, VOCs, SVOCs, PCBs, Phenols

For all other tests the samples were dried at < 37°C prior to analysis

All Asbestos testing is performed at our Coventry laboratory

Issue numbers are sequential starting with 1 all subsequent reports are incremented by 1

Sample Deviation Codes

- A - Date of sampling not supplied
- B - Sample age exceeds stability time (sampling to extraction)
- C - Sample not received in appropriate containers
- D - Broken Container

Sample Retention and Disposal

All soil samples will be retained for a period of 60 days from the date of receipt

All water samples will be retained for 14 days from the date of receipt

Charges may apply to extended sample storage

If you require extended retention of samples, please email your requirements to:

customerservices@chemtest.co.uk

Site	31 Willoughby Road, London, NW3 1RT	Job Number	J15315
Client	Manuela Eleuteri	Sheet	1 / 2
Engineer	Richard Tant Associates		

Proposed End Use Residential with plant uptake

Soil pH 8

Soil Organic Matter content % 6.0

Contaminant	Screening Value mg/kg	Data Source	Contaminant	Screening Value mg/kg	Data Source
Metals			Anions		
Arsenic	37	C4SL	Soluble Sulphate	500 mg/l	Structures
Cadmium	26	C4SL	Sulphide	50	Structures
Chromium (III)	3000	LQM/CIEH	Chloride	400	Structures
Chromium (VI)	21	C4SL	Others		
Copper	2,330	LQM/CIEH	Organic Carbon (%)	6	Methanogenic potential
Lead	200	C4SL	Total Cyanide	140	WRAS
Elemental Mercury	1	SGV	Total Mono Phenols	420	SGV
Inorganic Mercury	170	SGV	PAH		
Nickel	97	LQM/CIEH	Naphthalene	12.40	C4SL exp & LQM/CIEH
Selenium	350	SGV	Acenaphthylene	850	LQM/CIEH
Zinc	3,750	LQM/CIEH	Acenaphthene	1,000	LQM/CIEH
Hydrocarbons			Fluorene	780	LQM/CIEH
Benzene	0.87	C4SL	Phenanthrene	380	LQM/CIEH
Toluene	610	SGV	Anthracene	9,200	LQM/CIEH
Ethyl Benzene	350	SGV	Fluoranthene	670	LQM/CIEH
Xylene	230	SGV	Pyrene	1,600	LQM/CIEH
Aliphatic C5-C6	110	LQM/CIEH	Benzo(a) Anthracene	8.7	C4SL exp & LQM/CIEH
Aliphatic C6-C8	370	LQM/CIEH	Chrysene	14	C4SL exp & LQM/CIEH
Aliphatic C8-C10	110	LQM/CIEH	Benzo(b) Fluoranthene	10.5	C4SL exp & LQM/CIEH
Aliphatic C10-C12	540	LQM/CIEH	Benzo(k) Fluoranthene	15.0	C4SL exp & LQM/CIEH
Aliphatic C12-C16	3000	LQM/CIEH	Benzo(a) pyrene	5.00	C4SL
Aliphatic C16-C35	76,000	LQM/CIEH	Indeno(1 2 3 cd) Pyrene	6.2	C4SL exp & LQM/CIEH
Aromatic C6-C7	See Benzene	LQM/CIEH	Dibenzo(a h) Anthracene	1.35	C4SL exp & LQM/CIEH
Aromatic C7-C8	See Toluene	LQM/CIEH	Benzo (g h i) Perylene	71	C4SL exp & LQM/CIEH
Aromatic C8-C10	151	LQM/CIEH	Screening value for PAH	71.4	B(a)P / 0.15
Aromatic C10-C12	346	LQM/CIEH	Chlorinated Solvents		
Aromatic C12-C16	593	LQM/CIEH	1,1,1 trichloroethane (TCA)	53.1	LQM/CIEH
Aromatic C16-C21	770	LQM/CIEH	tetrachloroethane (PCA)	2.4	LQM/CIEH
Aromatic C21-C35	1230	LQM/CIEH	tetrachloroethene (PCE)	4.5	LQM/CIEH
PRO (C ₅ -C ₁₀)	1352	Calc	trichloroethene (TCE)	0.598	LQM/CIEH
DRO (C ₁₂ -C ₂₈)	80,363	Calc	1,2-dichloroethane (DCA)	0.014	LQM/CIEH
Lube Oil (C ₂₈ -C ₄₄)	77,230	Calc	vinyl chloride (Chloroethene)	0.00329	LQM/CIEH
TPH	1000	Trigger for speciated testing	tetrachloromethane (Carbon tetra)	0.089	LQM/CIEH
			trichloromethane (Chloroform)	3.86	LQM/CIEH

Notes

Concentrations measured below the above values may be considered to represent 'uncontaminated conditions' which pose 'LOW' risk to human health. Concentrations measured in excess of these values indicate a potential risk which require further, site specific risk assessment.

SGV - Soil Guideline Value, derived from the CLEA model and published by Environment Agency 2009

LQM/CIEH - Generic Assessment Criteria for Human Health Risk Assessment 2nd edition (2009) derived using CLEA 1.04 model 2009

C4SL - Defra Category 4 Screening value based on Low Level of Toxicological Risk

C4SL exp & LQM/CIEH calculated using C4SL revisions to exposure assessment but LQM/CIEH health criteria values

Calc - sum of nearest available carbon range specified including BTEX for PRO fraction

B(a)P / 0.15 - GEA experience indicates that Benzo(a) pyrene (one of the most common and most carcinogenic of the PAHs) rarely exceeds 15% of the total PAH concentration, hence this Total PAH threshold is regarded as being conservative

Site	31 Willoughby Road, London, NW3 1RT	Job Number	J15315
Client	Manuela Eleuteri	Sheet	2 / 2
Engineer	Richard Tant Associates		

Proposed End Use **Residential with plant uptake**

The key generic assumptions for this end use are as follows;

- that groundwater will not be a critical risk receptor;
- that the critical receptor for human health will be a young female aged 0 to 6 years old;
- that the exposure duration will be six years;
- that the building type equates to a terraced house.
- that the critical exposure pathways will be direct soil and indoor dust ingestion, consumption of home grown produce, consumption of soil adhering to home grown produce, skin contact with soils and dust, and inhalation of dust and vapours

Where contaminant concentrations are measured at concentrations below the generic screening value it is considered that they pose an acceptable level of risk and thus further consideration of these contaminant concentrations is not required. However, where concentrations are measured in excess of the generic screening value there is considered to be a potential that they could pose an unacceptable risk and thus further action will be required which could include:

- additional testing to zone the extent of the contaminated material and thus reduce the uncertainty with regard to its potential risk;
- site specific risk assessment to refine the assessment criteria and allow an assessment to be made as to whether the concentration present would pose an unacceptable risk at this site; or
- soil remediation or risk management to mitigate the risk posed by the contaminant to a degree that it poses an acceptable risk.



Geotechnical & Environmental Associates

Widbury Barn
Widbury Hill
Ware, Herts
SG12 7QE

Site
31 Willoughby Road, London, NW3 1RT

Borehole Number
BH1

Installation Type Standpipe	Dimensions Internal Diameter of Tube [A] = 30 mm Diameter of Filter Zone = 60 mm		Client Manuela Eleuteri	Job Number J15315
	Location	Ground Level (mOD) 85.55	Engineer Richard Tant Associates	Sheet 1/1

Legend	Water	Instr (A)	Level (mOD)	Depth (m)	Description	Groundwater Strikes During Drilling										
						Date	Time	Depth Struck (m)	Casing Depth (m)	Inflow Rate	Readings				Depth Sealed (m)	
											5 min	10 min	15 min	20 min		
			84.55	1.00	Bentonite Seal	13/01/16		3.00		Slow Inflow					NOT	
						Groundwater Observations During Drilling										
						Start of Shift					End of Shift					
						Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
					Slotted Standpipe	Instrument Groundwater Observations										
						Inst. [A] Type : Slotted Standpipe										
						Instrument [A]			Remarks							
						Date	Time	Level (mOD)								
						02/02/16		2.55	83.00							
						23/02/16		2.34	83.21							
						05/07/17		2.46	83.09							
						11/07/17		3.00	82.55							
			82.45	3.10												
					General Backfill											
			81.55	4.00												

Remarks



Geotechnical & Environmental Associates

Widbury Barn
Widbury Hill
Ware, Herts
SG12 7QE

Site
31 Willoughby Road, London, NW3 1RT

Borehole Number
BH2

Installation Type Standpipe	Dimensions Internal Diameter of Tube [A] = 30 mm Diameter of Filter Zone = 60 mm		Client Manuela Eleuteri	Job Number J15315
	Location	Ground Level (mOD) 85.50	Engineer Richard Tant Associates	Sheet 1/1

Legend	Water	Instr (A)	Level (mOD)	Depth (m)	Description	Groundwater Strikes During Drilling										
						Date	Time	Depth Struck (m)	Casing Depth (m)	Inflow Rate	Readings				Depth Sealed (m)	
											5 min	10 min	15 min	20 min		
			84.50	1.00	Bentonite Seal	13/01/16		3.00		Slow Inflow					NOT	
						Groundwater Observations During Drilling										
						Date	Start of Shift					End of Shift				
							Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
					Slotted Standpipe											
						Instrument Groundwater Observations										
						Inst. [A] Type : Slotted Standpipe										
						Date	Instrument [A]			Remarks						
							Time	Depth (m)	Level (mOD)							
						02/02/16		3.00	82.50							
						23/02/16		3.04	82.46							
						05/07/17		3.17	82.33							
						11/07/17		3.20	82.30							
			81.50	4.00	General Backfill											
			80.50	5.00												

Remarks



Geotechnical &
Environmental
Associates

Widbury Barn
Widbury Hill
Ware, Herts
SG12 7QE

Site
31 Willoughby Road, London, NW3 1RT

**Borehole
Number**
BH3

Installation Type Standpipe	Dimensions Internal Diameter of Tube [A] = 30 mm Diameter of Filter Zone = 60 mm		Client Manuela Eleuteri	Job Number J15315
	Location	Ground Level (mOD) 85.40	Engineer Richard Tant Associates	Sheet 1/1

Legend	Water	Instr (A)	Level (mOD)	Depth (m)	Description	Groundwater Strikes During Drilling															
						Date	Time	Depth Struck (m)	Casing Depth (m)	Inflow Rate	Readings				Depth Sealed (m)						
			84.40	1.00	Bentonite Seal	Groundwater Observations During Drilling															
						Start of Shift					End of Shift										
						Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)					
					Slotted Standpipe	Instrument Groundwater Observations															
						Inst. [A] Type : Slotted Standpipe															
						Date	Instrument [A]			Remarks											
							Time	Depth (m)	Level (mOD)												
			82.40	3.00		02/02/16		2.75	82.65												
						23/02/16		2.70	82.70												
						14/12/16		2.75	82.65												
						05/07/17		2.85	82.55												
						11/07/17		2.80	82.60												
			80.90	4.50	General Backfill																

Remarks



Geotechnical &
Environmental
Associates

Widbury Barn
Widbury Hill
Ware, Herts
SG12 7QE

Site
31 Willoughby Road, London, NW3 1RT

**Borehole
Number**
BH4

Installation Type
Standpipe

Dimensions
Internal Diameter of Tube [A] = 30 mm
Diameter of Filter Zone = 60 mm

Client
Manuela Eleuteri

**Job
Number**
J15315

Location

Ground Level (mOD)

Engineer

Sheet

85.40

Richard Tant Associates

1/1

Legend	Water	Instr (A)	Level (mOD)	Depth (m)	Description	Groundwater Strikes During Drilling										
						Date	Time	Depth Struck (m)	Casing Depth (m)	Inflow Rate	Readings				Depth Sealed (m)	
			84.40	1.00	Bentonite Seal	20/01/16		3.30	1.00	Slow Inflow						NOT
Groundwater Observations During Drilling																
			80.40	5.00	Slotted Standpipe	Start of Shift		End of Shift								
						Date	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)	Time	Depth Hole (m)	Casing Depth (m)	Water Depth (m)	Water Level (mOD)
Instrument Groundwater Observations																
Inst. [A] Type : Slotted Standpipe																
			75.40	10.00	General Backfill	Instrument [A]			Remarks							
						Date	Time	Depth (m)				Level (mOD)				
						02/02/16		2.75	82.65							
						23/02/16		2.76	82.64							
						13/12/16		2.75	82.65							
						05/07/17		2.88	82.52							
						11/07/17		2.89	82.51							

Remarks

Site	31 Willoughby Road, London, NW3 1RT	Job Number	J15315
Client	Manuela Eleuteri	Sheet	1/1
Engineer	Richard Tant Associates		

Date: 05 July 2017

Borehole No: 1

Test No: 1

Test Data

Soakage Calculation

Before start of test:

Borehole Diameter (m) 0.0600
Borehole Area (m) 0.0028
Borehole Perimeter (m) 0.188

Standpipe depth (m): 3.28

Screen depth (m): 1.00

Water level (m): 2.46

From Plot:
D1 (m) 3.12
D2 (m) 3.10
T1 (min) 0
T2 (min) 120

Time (mins)	Depth to Water (m)	Depth of Water (m)
0.0	3.12	0.16
1.0	3.12	0.16
3.0	3.12	0.16
5.0	3.11	0.17
10.0	3.11	0.17
15.0	3.11	0.17
20.0	3.11	0.17
30.0	3.11	0.17
45.0	3.11	0.17
60.0	3.10	0.18
90.0	3.10	0.18
120.0	3.10	0.18

Soakage Volume (m³) 0.000
Soakage Area (m²) 0.43
Time (min) 120

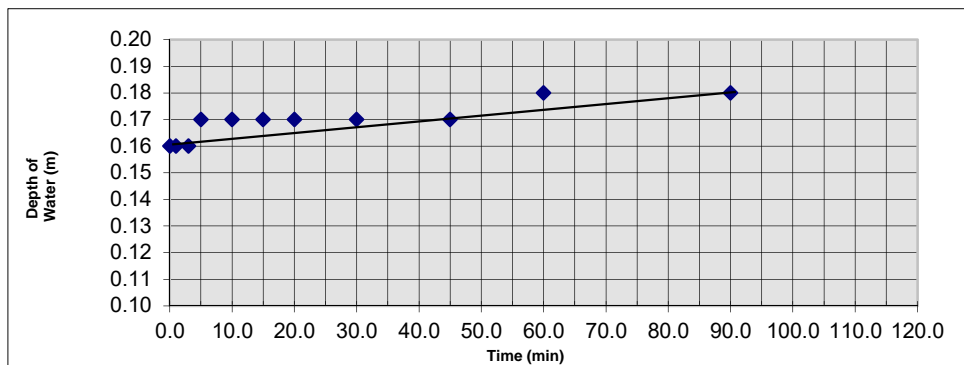
Soakage rate (m/sec)	1.81554E-08
Soakage rate (m/day)	0.001568627

At end of test:

Standpipe depth (m): 3.28

Screen depth (m): 1.00

Water level (m): 3.10



Remarks: Bailing at this position to reduce the water level, had no measureable effect on the water level in the nearby standpipe within BH2

Site	31 Willoughby Road, London, NW3 1RT	Job Number	J15315
Client	Manuela Eleuteri	Sheet	1/1
Engineer	Richard Tant Associates		

Date: 05 July 2017

Borehole No: 2

Test No: 1

Test Data

Soakage Calculation

Before start of test:

Borehole Diameter (m) 0.0600

Borehole Area (m) 0.0028

Borehole Perimeter (m) 0.188

Standpipe depth (m): 3.82

Screen depth (m): 1.00

Water level (m): 3.17

From Plot: D1 (m) 3.32

D2 (m) 3.21

T1 (min) 30

T2 (min) 120

Time (mins)	Depth to Water (m)	Depth of Water (m)
0.0	3.48	0.34
1.0	3.47	0.35
3.0	3.46	0.36
5.0	3.43	0.39
10.0	3.40	0.42
15.0	3.38	0.44
20.0	3.35	0.47
30.0	3.32	0.50
45.0	3.29	0.53
60.0	3.26	0.56
90.0	3.23	0.59
120.0	3.21	0.61

Soakage Volume (m³) 0.000

Soakage Area (m²) 0.53

Time (min) 90

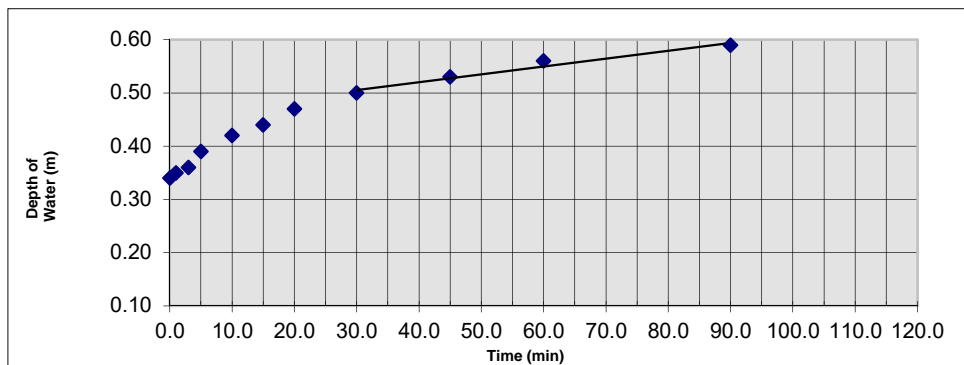
Soakage rate (m/sec)	1.0778E-07
Soakage rate (m/day)	0.009312169

At end of test:

Standpipe depth (m): 3.82

Screen depth (m): 1.00

Water level (m): 3.21



Remarks: Bailing at this position to reduce the water level, had no measureable effect on the water level in the nearby standpipe within BH1

Site	31 Willoughby Road, London, NW3 1RT	Job Number	J15315
Client	Manuela Eleuteri	Sheet	1/1
Engineer	Richard Tant Associates		

Date: 05 July 2017

Borehole No: 4

Test No: 1

Test Data

Soakage Calculation

Before start of test:

Borehole Diameter (m) 0.1000
Borehole Area (m) 0.0079
Borehole Perimeter (m) 0.314

Standpipe depth (m): 4.80

Screen depth (m): 1.00

Water level (m): 2.88

From Plot: D1 (m) 4.77
D2 (m) 4.62
T1 (min) 10
T2 (min) 120

Time (mins)	Depth to Water (m)	Depth of Water (m)
0.0	4.80	0.00
1.0	4.80	0.00
3.0	4.79	0.01
5.0	4.79	0.01
10.0	4.77	0.03
15.0	4.76	0.04
20.0	4.75	0.05
30.0	4.73	0.07
45.0	4.71	0.09
60.0	4.68	0.12
90.0	4.64	0.16
120.0	4.62	0.18

Soakage Volume (m³) 0.001
Soakage Area (m²) 1.20
Time (min) 110

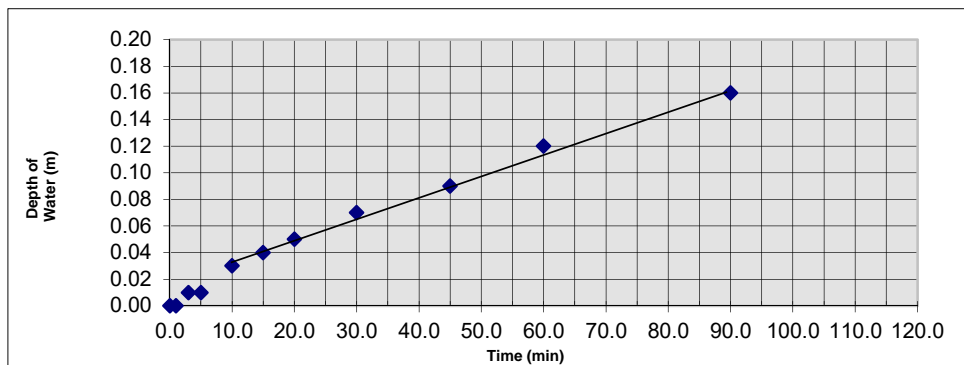
Soakage rate (m/sec)	1.48544E-07
Soakage rate (m/day)	0.012834225

At end of test:

Standpipe depth (m): 4.80

Screen depth (m): 1.00

Water level (m): 4.62



Remarks: Monitoring of the adjacent standpipe within BH3 showed no change in the observed water level (2.85 m) during bailing out of BH4 and throughout the subsequent test.



**PROPOSED BASEMENT AT
31 WILLOUGHBY ROAD,
LONDON, NW3 1RT**

FLOOD RISK ASSESSMENT

JANUARY 2016

REF: 1542/RE/12-15/01 REVISION A

Evans Rivers and Coastal Ltd

T: 07896 328220

E: Enquiries@evansriversandcoastal.co.uk

W: www.evansriversandcoastal.co.uk

CONTRACT

Evans Rivers and Coastal Ltd has been commissioned by Geotechnical and Environmental Associates to carry out a Flood Risk Assessment for a proposed basement at number 31 Willoughby Road, London, NW3 1RT.

QUALITY ASSURANCE, ENVIRONMENT AND HEALTH AND SAFETY

Evans Rivers and Coastal Ltd operates a Quality Assurance, Environmental, and Health and Safety Policy.

This project comprises various stages including data collection; hydrological and hydrogeological assessments; surface water drainage designs; and reporting. Quality will be maintained throughout the project by producing specific methodologies for each work stage. Quality will also be maintained by initiating internal quality procedures including the validation of third party deliverables; creation of an audit trail to record any changes made; and document control using a database and correspondence log file system.

To adhere to the Environmental Policy, data will be obtained and issued in electronic format and alternatively by post. Paper use will also be minimised by communicating via email or telephone where possible. Documents and drawings will be transferred in electronic format where possible and all waste paper will be recycled. Meetings away from the office of Evans Rivers and Coastal Ltd will be minimised to prevent unnecessary travel, however for those meetings deemed essential, public transport will be used in preference to car journeys.

The project will follow the commitment and objectives outlined in the Health and Safety Policy operated by Evans Rivers and Coastal Ltd. All employees will be equipped with suitable personal protective equipment prior to any site visits and a risk assessment will be completed and checked before any site visit. Other factors which have been taken into consideration are the wider safety of the public whilst operating on site, and the importance of safety when working close to a water source and highway. Any designs resulting from this project and directly created by Evans Rivers and Coastal Ltd will also take into account safety measures within a "designers risk assessment".

Report carried out by:



.....
Rupert Evans, BSc (Hons), MSc, CEnv, C.WEM, MCIWEM, AIEMA

DISCLAIMER

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DRAWINGS	BPS1195.02 4186/SM01

1. INTRODUCTION

1.1 Project Scope

1.1.1 Evans Rivers and Coastal Ltd has been commissioned by Geotechnical and Environmental Associates to carry out a Flood Risk Assessment for a proposed basement at number 31 Willoughby Road, London, NW3 1RT.

1.1.2 Specifically, this assessment intends to:

- 1) Carry out an appraisal of flood risk from all sources such as fluvial/tidal, groundwater, surface water/sewers, artificial sources in accordance with NPPF and other documents such as the SFRA and SWMP;
- 2) Recommend mitigation measures where appropriate;
- 3) Report findings and recommendations.

1.1.3 This assessment is carried out in accordance with the requirements of the National Planning Policy Framework (NPPF) dated March 2012. Other documents which have been consulted include:

- DEFRA/EA document entitled *Framework and guidance for assessing and managing flood risk for new development Phase 2 (FD2320/TR2)*, 2005;
- DEFRA/Jacobs 2006. *Groundwater flooding records collation, monitoring and risk assessment (ref HA5)*.
- National Planning Practice Guidance – Flood Risk and Coastal Change.
- London Borough of Camden Preliminary Flood Risk Assessment (PFRA) Version 0.2 dated 2011.
- London Borough of Camden Strategic Flood Risk Assessment (SFRA) dated 2014.
- London Borough of Camden Surface Water Management Plan (SWMP) Version 1 dated 2011.
- London Borough of Camden flood risk management strategy (FRMS) dated 2013.
- London Borough of Camden, Camden geological, hydrogeological and hydrological study – Guidance for subterranean development dated 2010.
- London Borough of Camden, Camden Planning Guidance – Basements and Lightwells (CPG 4) dated July 2015.
- Woods-Ballard., et al. 2015. *The SUDS Manual, Report C753*. London: CIRIA.
- National SUDS Working Group. 2004. *Interim Code of Practice for Sustainable Drainage Systems*.

2. DATA COLLECTION

2.1 To assist with this report, the data collected included:

- 1:250,000 *Soil Map of South East England* (Sheet 6) published by Cranfield University and Soil Survey of England and Wales 1983.
- 1:625,000 *Hydrogeological Map of England and Wales*, published in 1977 by the Institute of Geological Sciences (now the British Geological Survey).
- Local borehole data extracted from the *BGS Online Geology Viewer*.
- *Summary of ground investigation preliminary findings* produced by Geotechnical and Environmental Associates in January 2016 (excerpts in Appendix A).
- Information and data from:
 - London Borough of Camden Preliminary Flood Risk Assessment (PFRA) Version 0.2 dated 2011.
 - London Borough of Camden Strategic Flood Risk Assessment (SFRA) dated 2014.
 - London Borough of Camden Surface Water Management Plan (SWMP) Version 1 dated 2011.
 - London Borough of Camden Flood Risk Management Strategy (FRMS) dated 2013.
 - London Borough of Camden, Camden geological, hydrogeological and hydrological study – Guidance for subterranean development dated 2010.

2.2 All third party data used in this study has been checked and verified prior to use in accordance with Evans Rivers and Coastal Ltd Quality Assurance procedures.

3. SITE CHARACTERISTICS

3.1 Existing Site Characteristics and Location

3.1.1 The site is located at number 31 Willoughby Road, London, NW3 1RT. The approximate Ordnance Survey (OS) grid reference for the site is 526727 185854 and the location of the site is shown on Figure 1.

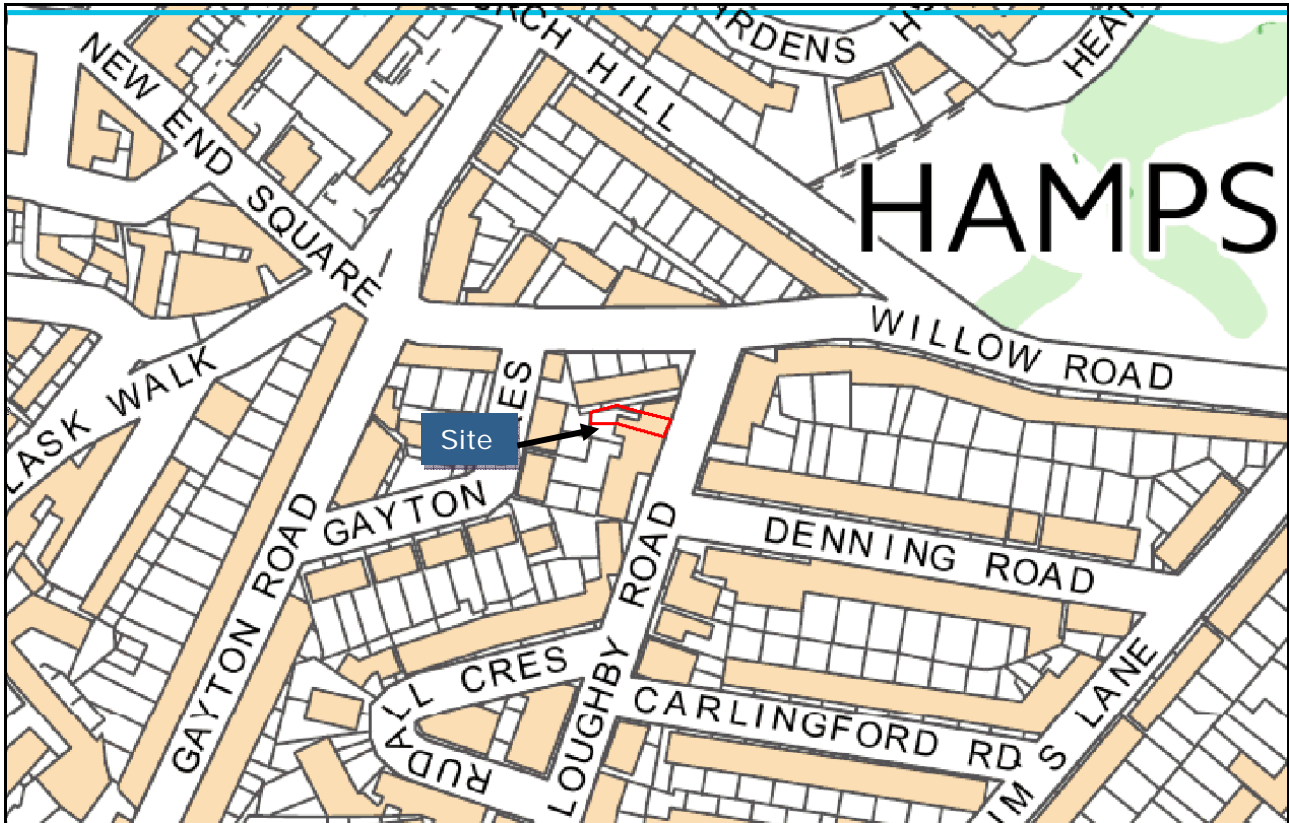


Figure 1: Site location plan (Source: Ordnance Survey, 2015)

3.1.2 The site is located within a residential area and comprises a four-storey building which is accessed from Willoughby Road adjacent to the eastern frontage of the site. There are front and rear garden areas which are largely covered by block paving apart from a small area of the front garden which remains vegetated (i.e. bedding plants).

3.1.3 The topographical survey/existing layout can be seen on Drawing Number BPS1195.02 and shows that ground levels across the site do not vary significantly and that the dwelling is set approximately 300mm higher than existing ground levels.

3.2 Site Proposals

3.2.1 It is understood that the development will comprise the construction of a single level basement beneath the existing property, which will extend beneath part of rear garden and beyond the existing front footprint to create a lightwell space. The proposed basement is understood to extend to a depth of approximately 3m, such that formation level is expected to be within the London Clay.

3.2.2 It is understood that this Flood Risk Assessment needs to assess the flood risk to the basement level only. The site proposals can be seen on Drawing Number 4186/SM01.

4. SOURCES OF FLOODING

4.1 Fluvial/Tidal

- 4.1.1 The Environment Agency Flood Map shows that the site is located within the NPPF Flood Zone 1, 'Low Probability' which comprises land as having less than a 1 in 1000 year annual probability of fluvial or tidal flooding (i.e. an event more severe than the extreme 1 in 1000 year event). NPPF states that all uses of land, including basements, are appropriate in this zone.
- 4.1.2 The SFRA also states that there has been no historical flooding within the Borough from fluvial or tidal sources. Furthermore, the SWMP confirms that the Borough does not fall within the Environment Agency's flood zones and therefore is not at significant risk from fluvial or tidal flooding.
- 4.1.3 The SFRA and SWMP states that all main rivers historically located within the Borough are now culverted and incorporated into the sewer network. The SWMP discusses the River Fleet which is one of London's "lost rivers" and which historically originates from springs on Hampstead Heath and drains to the Thames through the Borough. The Fleet is entirely incorporated within the sewer network.
- 4.1.4 The SFRA continues to discuss the Borough's historic rivers and in addition to the Fleet, the Tyburn, Kilburn and Brent were also located in the area of Hampstead Heath. All of these "lost rivers" are also now incorporated into the local sewer system maintained by Thames Water. It is for these reasons that the Borough is located entirely within Flood Zone 1.

4.2 Critical Drainage Areas (CDA)

- 4.2.1 Despite the site being located within Flood Zone 1, it is understood from Figure 6/Rev 2 of the SFRA and Figure 3.1 of the SWMP, that the site is located within the Group3-010 Critical Drainage Area (CDA).
- 4.2.2 The SWMP defines the CDA as:

"A discrete geographic area (usually a hydrological catchment) where multiple and interlinked sources of flood risk (surface water, groundwater, sewer, main river and/or tidal) cause flooding in one or more Local Flood Risk Zones during severe weather thereby affecting people, property or local infrastructure."

4.3 Groundwater Flooding

- 4.3.1 In addition to the information provided in the SFRA and SWMP, in order to assess the potential for groundwater flooding, the Jacobs/DEFRA report entitled *Strategy for Flood and Coastal Erosion Risk Management: Groundwater Flooding Scoping Study*, published in May 2004, was consulted, together with the guidance offered within the document entitled *Groundwater flooding records collation, monitoring and risk assessment (ref HA5)*, commissioned by DEFRA and carried out by Jacobs in 2006.
- 4.3.2 The *Summary of ground investigation preliminary findings* produced by Geotechnical and Environmental Associates in January 2016, indicates that the soils beneath the site comprise Made Ground (sandy clay) overlying London Clay. Groundwater seepages were encountered during the investigation and within the London Clay at 3m bgl.

- 4.3.3 Paragraphs 2.10.4 and 2.10.6 of the SFRA states that the London Clay has a low permeability but is likely to permit moderate infiltration. Paragraph 6.4.8 of the SFRA suggests that there could be perched water within sand pockets of the London Clay.
- 4.3.4 Figure 4e/Rev 1 of the SFRA shows that the site has not been affected in the past from groundwater flooding incidents and that the site is not located within an area of increased susceptibility to elevated groundwater and is therefore expected to remain at depth. Figure 4a/Rev 1 of the SFRA also shows that the site is not located across an area with superficial (and more permeable) deposits beneath the surface.
- 4.3.5 The BGS Groundwater Susceptibility Map also indicates that there is “Limited Potential for Groundwater Flooding to Occur” at the site.
- 4.3.6 The results from the intrusive testing indicate that groundwater is likely to be encountered below the site to a depth of 3m and therefore equal to or higher than the proposed basement floor.
- 4.3.7 The potential for groundwater to rise significantly is low considering the low permeable soil types, however, it is recommended that the basement is designed to achieve a Grade 3 level of waterproofing protection as outlined in BS8102:2009. A new reinforced concrete lining wall and ground-bearing concrete slab could be constructed using water resistant concrete to form the primary barrier. An internal drained cavity system will act as a secondary barrier against water ingress.
- 4.3.8 The evidence suggests that it is unlikely that the water table has the potential to breach the ground surface and flow into the building and basement via the ground floor.
- 4.3.9 The groundwater flooding risk to the property and basement is considered to be overall low and the risk reduced further by the appropriate mitigation measures stated within this section.

4.4 Surface Water Flooding and Sewer Flooding

- 4.4.1 Surface water and sewer flooding across urban areas is often a result of high intensity storm events which exceed the capacity of the sewer thus causing it to surcharge and flood. Poorly maintained sewer networks and blockages can also exacerbate the potential for sewer flooding.

Surface Water Flooding

- 4.4.2 It has been established that the site lies within the Group3-010 Critical Drainage Area. The SFRA notes that the surface water mapping indicates that the surface water flood extent broadly follows the natural topography of the borough and man-made features such as roads and rail lines. During extreme modelling scenarios, the SFRA states that there is increased ponding in areas of properties. For example, the SWMP indicates that the modelling shows deep flooding at Gospel Park, affecting Oak Village, Lamble St, Grafton Road and Kiln Place, caused by railway embankments creating a “basin” into which surface water collects.
- 4.4.3 The SFRA discusses the two large surface water flooding events in the Borough, which occurred in 1975 and 2002 and caused widespread damage. It is understood that during these events the sewers reached maximum capacity, however, Figure 3ii/Rev 1 of the SFRA shows that the site and the adjacent highway of Willoughby Road were not affected during these events.

4.4.4 Figure 3ii/Rev 1 of the SFRA (Figure 2 below) also shows that the site and the adjacent highway of Willoughby Road are not at risk from surface water flooding during events up to and including the 1 in 1000 year event. In fact, the site is located across an area with a less than 1 in 1000 year return period of surface water flooding.

4.4.5 It is considered that the site is not at risk of surface water flooding as indicated by the maps.

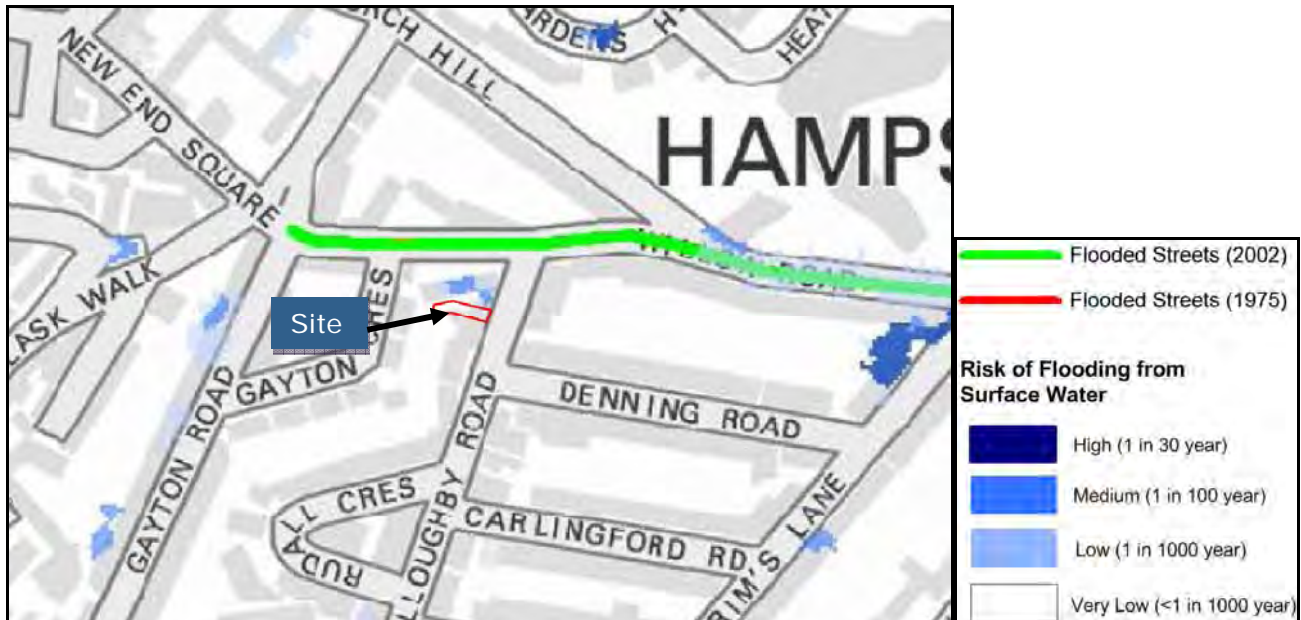


Figure 2: Location of site in relation to surface water flood extent (Source: taken from Figure 3ii/Rev 1 of the SFRA)

Sewer Flooding

4.4.6 The SFRA states that the majority of the Borough is served by a combined surface and foul water system which is designed to accommodate rainfall events of up to 1 in 30 years return period.

4.4.7 The combined sewer network outfalls into the River Thames during intense rainfall events when the sewer network reaches capacity. The evidence suggests that as the sewer capacity becomes exceeded this results in surcharging of the network prior to sufficient discharge into the Thames.

4.4.8 Figure 5a/Rev 1 of the SFRA indicates that the site is located across an area which has had 4 recorded internal sewer flooding incidents. Figure 5b/Rev 1 of the SFRA that the site is located across an area which has had 1 external sewer flooding incidents.

4.4.9 It is likely that foul water from the basement level will be drained to a submersible packaged pumping station and pumped to ground level where it will flow into the surrounding sewer system via gravity. It is understood that a non-return valve (e.g. <http://www.forgevalves.co.uk/>) will be installed so that the basement (and upper floors) will be protected further from sewer flooding.

4.4.10 This approach also complies with paragraph 5.11 of the Camden Planning Guidance CPG4 dated 2015. Therefore, if the sewer in the road becomes completely full during a heavy storm, foul water does not backflow into the property.

4.5 Reservoirs, Canals And Other Artificial Sources

- 4.5.1 The failure of man-made infrastructure such as flood defences and other structures can result in unexpected flooding. Flooding from artificial sources such as reservoirs, canals and lakes can also occur suddenly and without warning, leading to high depths and velocities of flood water which pose a safety risk to people and property.
- 4.5.2 The Environment Agency's "Risk of flooding from reservoirs" map suggests that the site is not at risk from reservoir flooding. This supported by the SFRA which also states that the risk of flooding from the Regent's Canal is low.

5. SURFACE WATER DRAINAGE

- 5.1 Policy 5.13 in Chapter 5 of the London Plan dated March 2015, requires sustainable drainage systems (SUDS) to be installed where appropriate and in line with the drainage hierarchy in order for runoff to be managed as close to its source as possible.
- 5.2 The London Plan states that SUDS should be utilised unless there are practical reasons for not doing so. The less permeable soils beneath the site are unlikely to possess sufficient infiltration capacity for the practical use of infiltration devices.
- 5.3 Despite a small increase in impermeable area at the front of the property as a result of the basement development, there is a lack of available space and little opportunity to reduce runoff rates from the site via attenuation or rainwater harvesting.
- 5.4 If an attenuation tank was included at the site, it would need to be located in the rear garden area and therefore it may be difficult to direct flows from this device through the house and into the sewer beneath Willoughby Road. It is likely that in this instance, surface water from the tank would be directed to the foul water pump at basement level in order to maintain a discharge into the sewer. There is uncertainty about the viability of this approach, especially when considering the positions of existing downpipes and the reliability of the pump to accommodate surface water flows as well as foul water flows.
- 5.5 Despite this, other SUDS measures should be considered such as rain gardens (i.e. vegetated depressions which hold back water) and pervious surfaces (i.e. possibly permeable paving which could temporarily retain surface water).

6. CONCLUSIONS

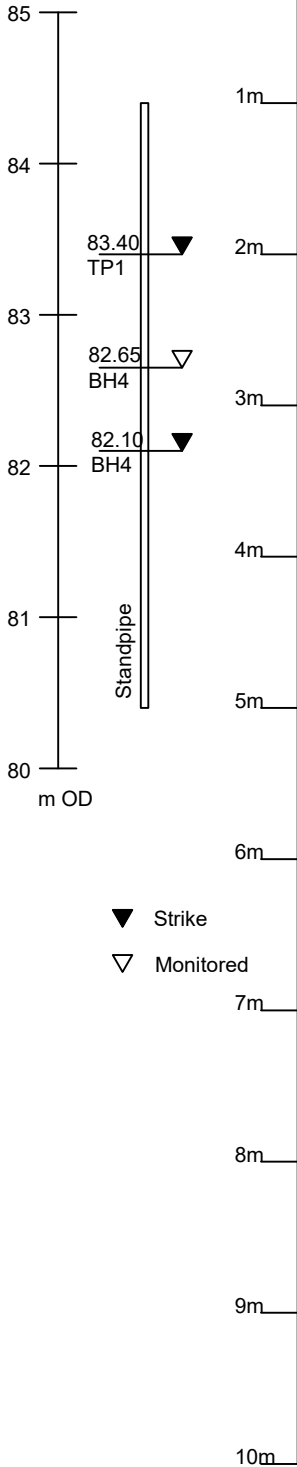
- A review of the relevant guidance documents and various types of data collected at the site has enabled a full assessment of the flood risks to be quantified.
- The site is located within the Flood Zone 1 therefore all uses of land are appropriate in this zone.
- This assessment has investigated the possibility of groundwater flooding and flooding from other sources at the site. It is considered that there will be low risk of groundwater flooding and surface water flooding across the site.
- There is a low to moderate risk of flooding from sewers, however, as a precaution; the risk from sewer flooding should be mitigated further by introducing a non-return valve to the pumped system.

7. BIBLIOGRAPHY

- i. Communities and Local Government 2012. *National Planning Policy Framework*.
- ii. DEFRA/EA 2005. *Framework and guidance for assessing and managing flood risk for new development, Phase 2, Flood and Coastal Defence R&D Programme, R&D Technical Report FD2320/TR2*. Water Research Council.
- iii. DEFRA/Jacobs 2004. *Strategy for Flood and Coastal Erosion Risk Management: Groundwater Flooding Scoping Study (LDS), Final Report, Volumes 1 and 2*.
- iv. Geological Society of London 2006. *Groundwater and Climate Change*. Geoscientist magazine, Volume 16, No 3.
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- vi. London Borough of Camden Preliminary Flood Risk Assessment (PFRA) Version 0.2 dated 2011.
- vii. London Borough of Camden 2014. *Strategic Flood Risk Assessment*.
- viii. London Borough of Camden 2013a. *CPG4 Basement and Lightwells*.
- ix. London Borough of Camden 2013b. *Flood risk management strategy*.
- x. London Borough of Camden 2011. *Surface Water Management Plan* Version 1.
- xi. London Borough of Camden 2010. *Camden geological, hydrogeological and hydrological study – Guidance for subterranean development*.
- xii. Water UK 2012. *Sewers for Adoption 7th Edition, A design and construction guide for developers*. Water Research Council.

GROUND & WATER PROFILE

GL 85.4m OD



- ▼ Strike
- ▽ Monitored

Paving

Sandy silty CLAY + gravel

Slightly silty CLAY

Silty CLAY + gravel + carbonaceous layers

Silty CLAY

Silty CLAY + silt & sand partings and selenite.

Silty CLAY + partings + claystones

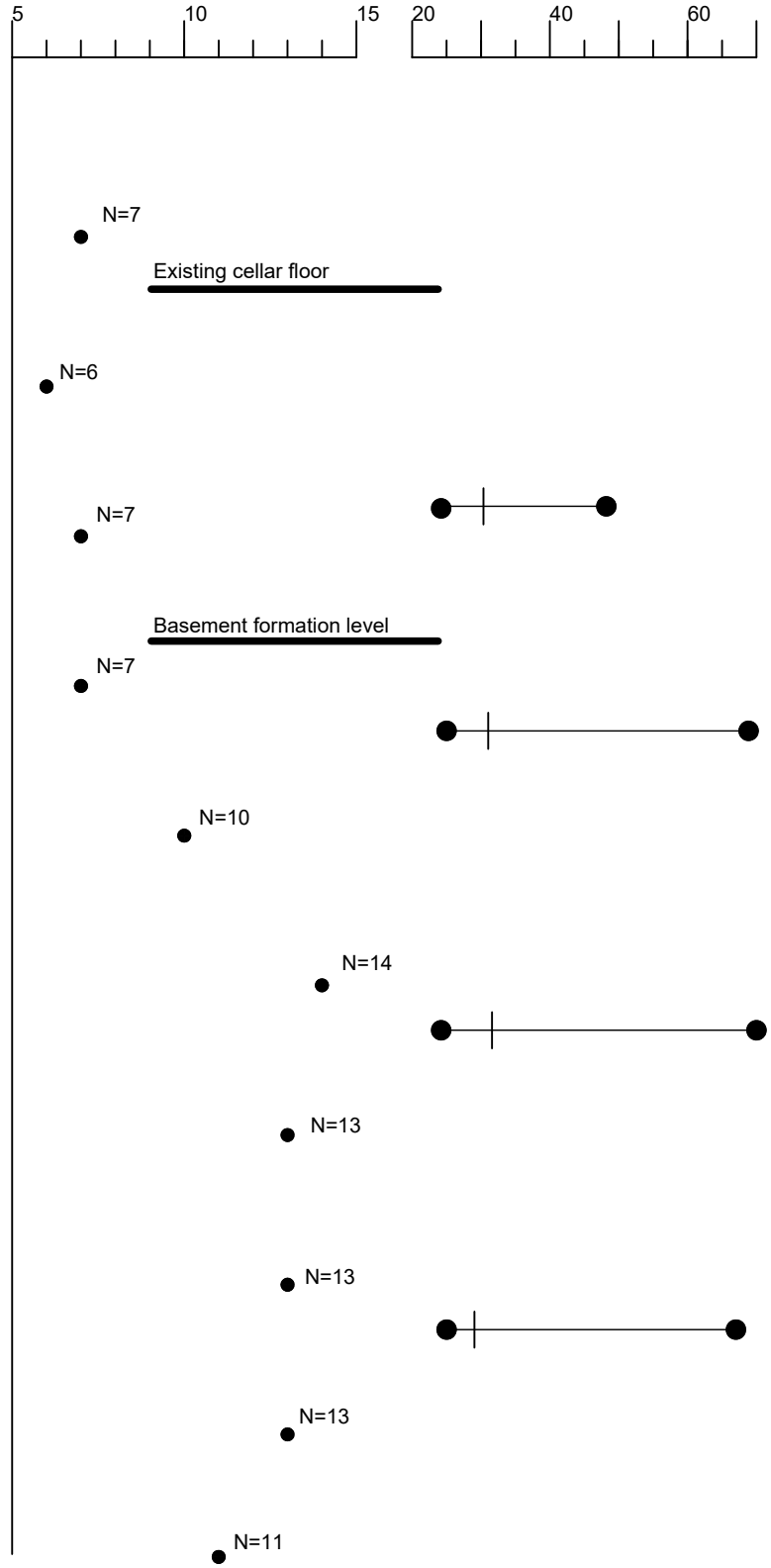
MADE GROUND

FIRM

STIFF

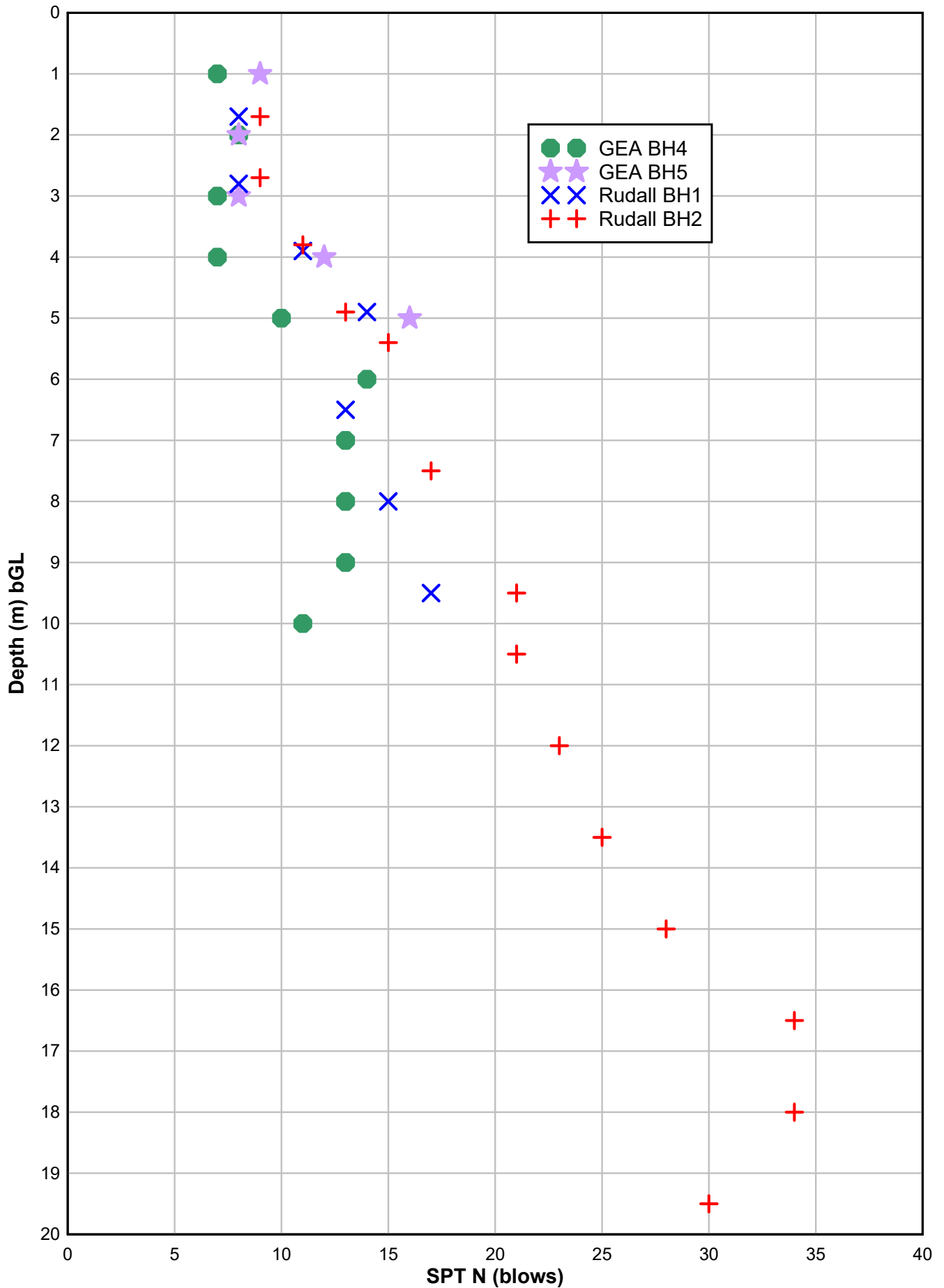
N Values

m/c %



31 WILLOUGHBY ROAD NW3 1RT
GEA BOREHOLE 4 DATA COLLATED

G1808 31 WILLOUGHBY ROADNW3 1RT - Proposed Basement SPT Profiles GEA BH4, BH5 & 37-39 Rudall Crescent BH1, BH2



Appendix C Contents

Eldreds 2018-2019 ground investigation – factual report

Figure 4 - Site plan

Borehole records

Laboratory test results

Figure 5 – Transducer arrangement

Figure 6 – Plot of particle size distribution test results

Figure 7 – Plot of Moisture content, plasticity and clay content profiles

Figure 8 – Plot of groundwater measurement August 2018 to March 2019

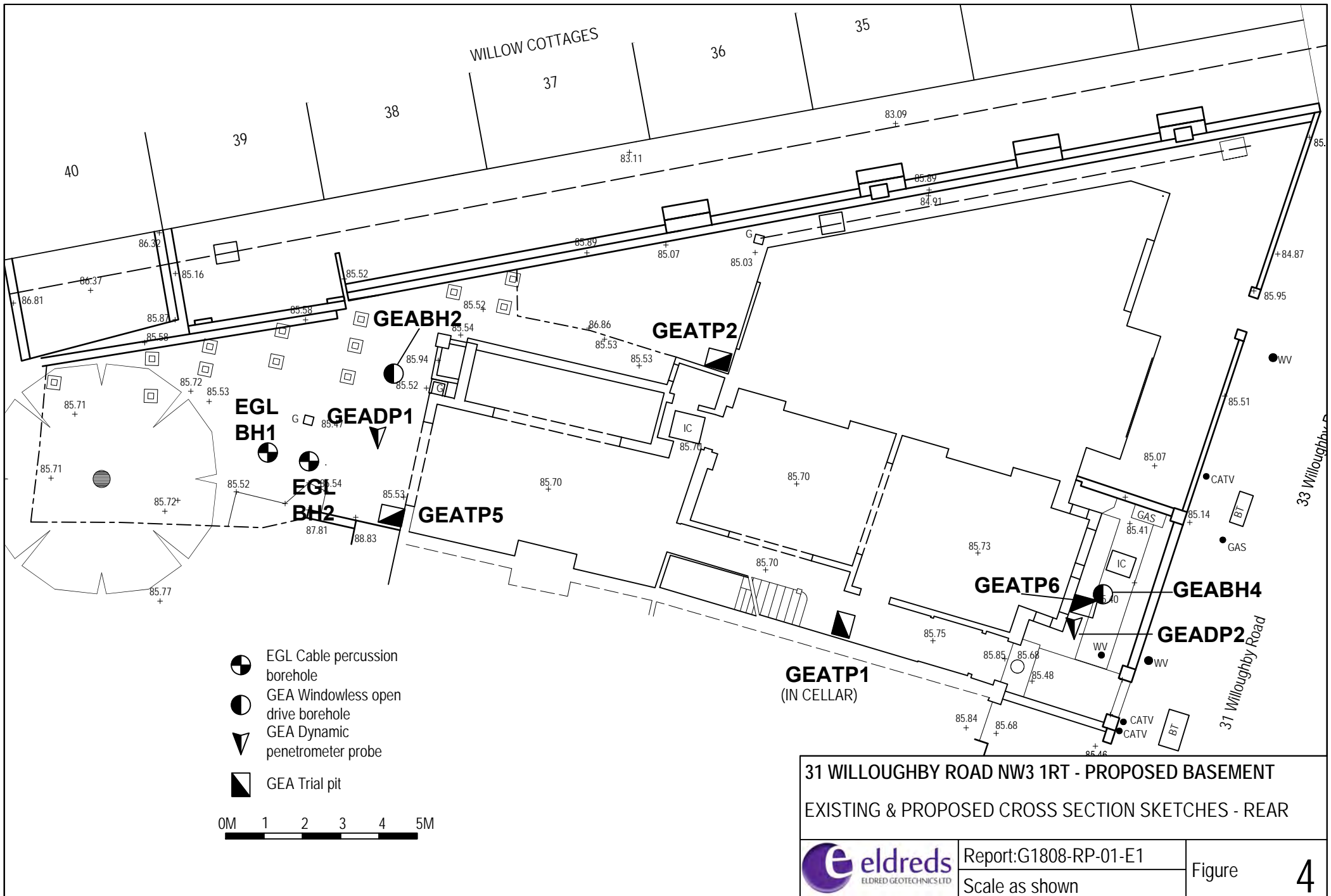
Figure 9 – Sketched long section

Figure 10 – Sketched cross section of front part of No.31

Figure 11 – Sketched cross section of rear part of No.31

Figure 12 – Plot of SPT and U100 blow count profiles

Figure 13 – Plot of SPTCu and Triaxial test undrained shear strength profiles





Project 31 WILLOUGHBY ROAD NW3 1RT - BASEMENT				BH1
Job No G1808	Date 13-08-18 14-08-18	Ground Level (m ODN) 85,50	Co-Ordinates (OSGB36) E 526.718,0 N 185.855,0	
Method Demountable cable percussion rig; borehole 200dia. to 5m, 150dia. 5m to EOB				Sheet 1 of 3

SAMPLES & TESTS			Water	EXCAVATION RECORD				
Depth	Type No	Test Result		Reduced Level	Legend	Depth (Thickness)	MATERIAL DESCRIPTION	
							Main Description	Strata Notes
0,50-0,95	B1			(1,30)		0,0- 0,2 Brick pavours on sharp sand 0,2- 0,3 Concrete 0,3- 0,5 Crushed brick 0,5- 1,3 Soft grey/green clay sand & brick; (cutting tool drove brick to 2m bGL) (MADE GROUND)		
1,00-1,95 1,00	B3 C	N7 1/2/1/2/2/2	84,20		1,30			
1,50-1,95 1,50	B4 C	N8 2/1/1/2/3/2				Soft low strength brown sandy and silty CLAY with rare rounded flint gravel and 5mm angular brick fragments (driven from above?) (MADE GROUND)		
2,00-2,45	U5	12 blows			(2,20)			
2,50 2,50	S6 SPT	N7 1/1/2/2/1/2		↓				
2,80								
3,00-3,45 3,00-3,45	U7 B8	16 blows NR						
3,50 3,50	S9 SPT	N10 1/2/2/2/3/3	82,00		3,50	Firm medium strength brown slightly sandy silty CLAY with rare m.f. rounded flint gravel. (HEAD)		
4,00-4,45	U10	25 blows	81,50		4,00			
4,50 4,50	S11 SPT	N15 1/2/3/3/4/5			(0,50)			
5,00-5,45	U12	30 blows			(2,00)	Firm becoming stiff, medium strength brown fragmented and thinly laminated silty CLAY disturbed by freeze/thaw, possibly with zones of concentrated mobilization. Occasional fine roots. (LONDON CLAY - Disturbed)		

Groundwater Observations During Drilling					Groundwater Strikes During Drilling							Chiselling		
Date & Time	Obs. (min)	Hole Depth (m)	Casing Depth (m)	Water Depth (m)	Date & Time	Obs. (min)	Strike Depth (m)	Casing Depth (m)	Inflow Rate	Rise to depth	Depth Sealed (m)	From (m)	To (m)	Time (hhmm)
13/08 00:00	Wet	2,80	2,00	2,80	13/08 00:00	30	2.8	2,00	Seep					
13/08 00:00	Dry	4,00	4,00											

All dimensions in metres Scale 1:34.375	Contractor P J Drilling Ltd	Plant Used Dando 100 modular rig.	Logged By Mdf/MLE
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Eldred Geotechnics Ltd Telephone: 01689 869406 Email: mail@eldreds-geo.co.uk
 2019_CPBH_LOG_EG_G1808_31_WILLOUGHBY ROAD NW3 1RT.GPJ ELDRED-2013.GDT 14/07/19



Project 31 WILLOUGHBY ROAD NW3 1RT - BASEMENT				BH2
Job No G1808	Date 15-08-18 15-08-18	Ground Level (m ODN) 85,50	Co-Ordinates (OSGB36) E 526.719,0 N 185.855,0	
Method Demountable cable percussion rig; borehole 200dia.				Sheet 1 of 1

SAMPLES & TESTS			Water	EXCAVATION RECORD				
Depth	Type No	Test Result		Reduced Level	Legend	Depth (Thickness)	MATERIAL DESCRIPTION	
							Main Description	Strata Notes
0,50-0,95	B1	NR	85,00	[Cross-hatch pattern]	0,50	Brick pavements on sand to 0.15m on 100mm thick concrete on soft dark grey/brown clay with brick. (MADE GROUND)	15mm layer of organic material; possibly from stream bed. circa 2.5m	
1,00-1,45	B3 SPT	N4 1/2/1/1/1/1		[Cross-hatch pattern]		Soft low strength dark grey/brown becoming brown mottled green silty sandy and slightly gravelly CLAY. Gravel is m.f rounded flint with rare crushed brick. Occasional fine roots. (MADE GROUND) .		
1,50-1,95	U4	11 blows		[Cross-hatch pattern]	(2,50)			
1,95-2,00	D5 S6			[Cross-hatch pattern]				
2,00-2,45	B7 SPT	N4 2/1/1/1/1/1		[Cross-hatch pattern]				
2,50-2,95	U8	11 blows		[Cross-hatch pattern]				
2,95-3,00	D9 S10		82,50	[Cross-hatch pattern]	3,00	Soft medium strength brown silty, slightly sandy CLAY. Occasional fine roots. (HEAD)		
3,00-3,45	B11 SPT	N7 1/1/1/2/2/2		[Cross-hatch pattern]				
3,45-3,50	D12 U11	15 blows		[Cross-hatch pattern]	(1,50)			
3,95-4,00	D12 S13			[Cross-hatch pattern]				
4,00-4,50	U14		81,00	[Cross-hatch pattern]	4,50	Firm medium strength thinly laminated brown silty CLAY. Occasional fine roots. (DISTURBED LONDON CLAY)		
4,50-4,95				[Cross-hatch pattern]	(0,50)			
4,95	D15		80,50	[Cross-hatch pattern]	5,00	Borehole ends		

Eldred Geotechnics Ltd Telephone: 01689 869406 Email: mail@eldreds-geo.co.uk 2019_CPBH_LOG_EG_G1808_31_WILLOUGHBY ROAD NW3 1RT.GPJ ELDRED-2013.GDT_14/07/19

Groundwater Observations During Drilling					Groundwater Strikes During Drilling							Chiselling		
Date & Time	Obs. (min)	Hole Depth (m)	Casing Depth (m)	Water Depth (m)	Date & Time	Obs. (min)	Strike Depth (m)	Casing Depth (m)	Inflow Rate	Rise to depth	Depth Sealed (m)	From (m)	To (m)	Time (hhmm)
		1,35		Dry										
		3,00	2,00	Dry										
		3,50	3,00	Dry										
		5,00	3,00	Dry										

All dimensions in metres Scale 1:34.375	Contractor P J Drilling Ltd	Plant Used Dando 100 modular rig.	Logged By Mdf/MLE
--	--------------------------------	--------------------------------------	----------------------

Descriptions of samples from 31 Willoughby Road recovered 13th to 15th August 2018 Logged by M.H. de Freitas

Bulk(B), SPT(S), Cutting shoe (CS) samples logged 13th-15th August

U(UUTxl) extruded & tested 15th November; logged 26th November 2018

Vocabulary of spacing:

Fissuring. Very close = 20 – 60mm. Extremely close = <20mm.

Thinly laminated = < 6mm

Loc'n	Depth	Type	Description	Geology
BH1	0.5	B		
	1.0-1.45	B		
	1.5-1.95	B		
	2.0-2.45	U	Soft brown clay @PL comprising angular fragments of clay mixed with ~ 0.5cm lenses silt which together exhibit a crude stratification, plus occasional 0.5cm angular fragment of red brick. Fine rootlets present. .	Made Ground
	2.5-2.95	S	Soft brown damp clay with possibly slightly silt/fine sand content with rounded flint fragment medium gravel size. @ PL or just wet of.	Made Ground
	3.0-3.45	B	Soft, brown, moist to almost wet clay matrix supporting isolated medium to fine (and suspect smaller) size angular fragments of brick and stone. Brown colouration in clay contains patches of different hues. Wet of PL	
	3.5-3.95	S	Firm brown damp mosaic of angular clasts ~ 7mm side length of London Clay some being litho-relics, with veins and blotches of blue. Rounded flints of medium and fine grained gravel size. @PL or just wet of	London Clay
	4.0-4.45	U	Soft to firm brown horizontally thinly laminated brown clay @ PL comprised of angular but rounded fragments of laminated clay up to 4cm across often with smooth surfaces, closely packed and mainly outlined by light brown 1mm rim of light brown clay; occasional 1mm rim of soft light blue clay. (Disturbed by freeze-thaw).	London Clay
	4.5-4.95	S	Stiff brown damp mosaic of angular lithorelics of thinly laminated London Clay ~ 7mm side length, bounded by veins of blue clay <1mm thick. @PL	London Clay

Descriptions of samples from 31 Willoughby Road recovered 13th to 15th August 2018 Logged by M.H. de Freitas

Bulk(B), SPT(S), Cutting shoe (CS) samples logged 13th-15th August

U(UUTxl) extruded & tested 15th November; logged 26th November 2018

Vocabulary of spacing:

Fissuring. Very close = 20 – 60mm. Extremely close = <20mm.

Thinly laminated = < 6mm

Loc'n	Depth	Type	Description	Geology
BH1	5.0-5.45	U	Firm grey very closely fissured clay going brown on the fissures. Fissures producing blocks 5cm -6cm across; clay in blocks @ PL. Between these blocks is soft grey clay on wet side of PL consisting of 1cm angular fragments forming a clay clast supported fabric in a soft clay matrix. Some of the boundaries between this soft clay and the blocks bounded by fissures are striated surfaces that are sub-horizontal and at 45°. Fine lace-like network of black fibrous rootlets on some planar surfaces. (Disturbed with what appear to be zones of concentrated mobilization; slope instability, valley bulge?).	London Clay
	5.5-5.95	S	Stiff brown damp mosaic of angular fragments larger than those above ~10mm+ very well thinly laminated; appears to be undisturbed. @PL.	London Clay
	6.0-6.45	U	Stiff horizontally very closely fissured grey thinly laminated clay that has a dry silty appearance, just turning brown on fissure surfaces; on dry side of PL. Horizontal fissures smooth, undulating and extremely closely spaced	London Clay
	6.5-6.95	S	Stiff grey damp very well & thinly laminated clay. @PL	London Clay
	7.0-7.45	U	Stiff grey thinly laminated clay that glistens suggesting a visible silt content. On dry side of PL. Horizontal smooth undulating fissures just discernible. Small gastropods occasionally present	London Clay
	7.5-7.95	S	Stiff grey damp very well & thinly laminated clay. @PL	London Clay
	8.0-8.45	U	Firm grey thinly laminated clay just wet of PL. Bands of broken shells 1cm thick at 40° subparallel to laminations. Weakly developed	London Clay

Descriptions of samples from 31 Willoughby Road recovered 13th to 15th August 2018 Logged by M.H. de Freitas

Bulk(B), SPT(S), Cutting shoe (CS) samples logged 13th-15th August

U(UUTxl) extruded & tested 15th November; logged 26th November 2018

Vocabulary of spacing:

Fissuring. Very close = 20 – 60mm. Extremely close = <20mm.

Thinly laminated = < 6mm

Loc'n	Depth	Type	Description	Geology
BH1			horizontal and sub-vertical fissuring. Although it looks disturbed (40° dips) no striated surfaces were found.	
	8.5-8.95	S	Stiff grey damp very well & thinly laminated clay. @PL	London Clay
	9.0-9.45	U	Stiff grey thinly laminated very closely fissured clay on dry side of PL, possibly silty. Fissures smooth and planar to undulating. No striations. (Undisturbed)	London Clay
	9.45	CS	Firm to stiff thinly laminated extremely closely fissured damp grey clay. Dry of PL	London Clay
	9.5-9.95	S	Stiff grey damp very well & thinly laminated clay. @PL	London Clay
	10.0-10.45	U		
	10.5	CS	Stiff thinly laminated extremely closely fissured damp grey clay. @ PL	London Clay
	10.5-10.95	S	Stiff grey damp very well & thinly laminated clay. @PL or just below	London Clay
	11.0-11.45	U		
	11.5-11.95	S	Stiff grey damp very well thinly laminated clay that breaks more easily and could contain more silt than above. Dry of PL	London Clay
	12.0-12.45	U	Stiff grey thinly laminated clay on dry side of PL, possibly silty. Very closely fissured.	London Clay
	12.5-12.95	S	Stiff to Very Stiff grey damp very well thinly laminated clay that breaks more easily and could contain more silt than that to 11.5m. Dry of PL	London Clay
	13.0-13.45	U		
13.5-13.95	S	Stiff to Very Stiff grey damp very well thinly laminated clay that breaks more easily and could contain more silt than that to 11.5m. Dry of PL	London Clay	

Descriptions of samples from 31 Willoughby Road recovered 13th to 15th August 2018 Logged by M.H. de Freitas

Bulk(B), SPT(S), Cutting shoe (CS) samples logged 13th-15th August

U(UUTxl) extruded & tested 15th November; logged 26th November 2018

Vocabulary of spacing:

Fissuring. Very close = 20 – 60mm. Extremely close = <20mm.

Thinly laminated = < 6mm

Loc'n	Depth	Type	Description	Geology
BH1	14.0-14.45	U	Firm grey thinly laminated very closely fissured clay with m/c close to PL; possibly silty. Occasional light brown 1mm thick bands of silt to fine sand	London Clay
	14.45	CS	Stiff thinly laminated extremely closely fissured damp grey clay. Occasional fragments of shell. More easily split than that at 190.5 and may contain more silt. Appears to be unfissured. Dry of PL	London Clay
	14.5-14.95	S	Stiff to Very Stiff grey extremely closely fissured damp thinly laminated clay that breaks more easily and could contain more silt than that to 11.5m. Fissures are fine and delicate in nature. No sign of polishing on them. Dry of PL	London Clay
BH2	0.5	B		
	1.0-1.45	B		
	1.5-1.95	U	Brown mottled green clay peds 2cm – 3cm just wet of PL, intermixed with lenticles of green silt/sand separated by a sharp horizontal boundary from structureless brown clay wet of PL with included angular fine gravel size fragments of red brick..	Made ground
	2.0	CS	Soft brown structureless clay matrix with sand and silt content supporting fragments of brick and stone fine gravel to medium sand in size. Rootlets and @ just dry of PL. Crumbles on remoulding	

Descriptions of samples from 31 Willoughby Road recovered 13th to 15th August 2018 Logged by M.H. de Freitas

Bulk(B), SPT(S), Cutting shoe (CS) samples logged 13th-15th August

U(UUTxl) extruded & tested 15th November; logged 26th November 2018

Vocabulary of spacing:

Fissuring. Very close = 20 – 60mm. Extremely close = <20mm.

Thinly laminated = < 6mm

Loc'n	Depth	Type	Description	Geology
BH2	2.0-2.45	S	Soft brown structureless clay matrix supporting fragments of brick and stone fine gravel to medium sand in size. Rootlets and @ PL or just wet of.	Made Ground
	2.5-2.95	B	Stiff light brown/orange structureless clay on wet side of PL containing rootlets and occasional rounded flint of fine/medium size gravel, and 1.5cm sub-horizontal layer of structureless black clay containing soft elongate fragments of wood (10mm long x 2mm across) and possibly peat.	Made Ground
	2.5-2.95	U	No recovery	
	2.95	CS	Soft brown clay with silt and occasional rounded flint med to coarse gravel size. Light brown 1mm peds of soil surrounded by darker mottled brown with light and dark hues clay matrix forming agglomerates ~ 1cm in diameter with an elliptical shape that has its long axis approx. sub-horizontal. Separates along the boundaries of the aggregates which often have blue veining and staining and sometimes rootlets. Overall @ PL.	Transported
	3.0-3.45	B	Soft brown clay with silt. Light brown 1mm peds of soil surrounded by darker clay matrix forming agglomerates ~ 1cm in diameter with an elliptical shape that has its long axis approx. sub-horizontal. Separates along the boundaries of the aggregates which often have blue veining and staining and sometimes rootlets. Overall @ PL.	Transported
	3.45	CS	Soft brown clay with silt. Light brown 1mm peds of soil surrounded by darker clay matrix forming agglomerates ~ 1cm in diameter with an elliptical shape that has its long axis approx. sub-horizontal. Separates along the boundaries	Transported

Descriptions of samples from 31 Willoughby Road recovered 13th to 15th August 2018 Logged by M.H. de Freitas

Bulk(B), SPT(S), Cutting shoe (CS) samples logged 13th-15th August

U(UUTxl) extruded & tested 15th November; logged 26th November 2018

Vocabulary of spacing:

Fissuring. Very close = 20 – 60mm. Extremely close = <20mm.

Thinly laminated = < 6mm

Loc'n	Depth	Type	Description	Geology
BH2			of the aggregates which often have blue veining and staining and sometimes rootlets. Overall @ PL.	
	3.5-3.95	U	Accumulation of stiff/firm brown thinly laminated clay peds at PL, clast supported but exhibiting extremely closely fissuring with green gleying 1mm on occasional sub-vertical surfaces.	Transported
	3.95	CS	Soft and highly remoulded sample on wet side of PL. Of dubious representativeness.	
	4.0-4.45	S	Soft to firm brown thinly laminated clay with blue staining on some laminae. @ PL (in situ).	London Clay
	4.5-4.95	U	Firm brown thinly laminated clay comprising of angular but rounded fragments of the clay 1cm – 2cm across at around PL, with much green gleying on sub-horizontal and 45° pervasive surfaces; no striations or polishing. 1cm thick orange brown lens of fine-medium sand that thins to nothing across the diameter of the core and containing fine network of black rootlets.	Disturbed
	4.95	CS	Firm brown thinly laminated London Clay just on dry side of PL and appears to be silty with blue staining on some laminae and blue veining on some fissures. Occasional rootlets penetrating fissures.	



Summary of Natural Moisture Content, Liquid Limit and Plastic Limit Results

Job No. 25366	Project Name 31 Willoughby Road, London NW3 1RT	Programme	
		Samples received	17/08/2018
Project No. G1808	Client Eldred Geotechnics Ltd	Schedule received	22/10/2018
		Project started	23/10/2018
		Testing Started	01/11/2018

Hole No.	Sample				Soil Description	NMC	Passing 425µm	LL	PL	PI	Remarks
	Ref	Top m	Base m	Type							
BH1	4	1.50	1.95	B	Green silty clayey SAND with numerous brown slightly sandy silty clay lumps and rare fm sub-angular to sub-rounded gravel	21	91	43	17	26	
BH1	5	2.00	2.45	U	High strength brown mottled orangish brown clayey gravelly silty SAND with rare fine brick fragments (gravel is fmc and rounded to sub-angular)	17	80	41	17	24	
BH1	8	3.00	3.45	B	Brown and occasional greenish grey slightly gravelly sandy silty CLAY (gravel is fm and sub-angular to sub-rounded)	28	94	42	18	24	
BH1	10	4.00	4.45	U	Medium strength brown slightly mottled grey silty CLAY with rare pockets of orange fine sand / silt and traces of selenite crystals and rootlets	33	99	66	23	43	
BH1	12	5.00	5.45	U	High strength brown silty CLAY with rare pockets of orange fine sand / silt	32	100	68	27	41	
BH1	14	6.00	6.45	U	High strength dark brown slightly mottled orangish brown silty CLAY with occasional pockets of fine sand / silt	28	99	67	25	42	
BH1	16	7.00	7.45	U	High strength dark grey silty CLAY with rare pockets of fine sand	28	100	68	24	44	
BH1	18	8.00	8.45	U	High strength dark grey silty CLAY	29	100	66	25	41	
BH2	3	1.00	1.45	B	Greenish grey and occasional dark grey gravelly clayey very silty SAND with rare cobbles (gravel is fmc and sub-angular to sub-rounded)	20	87	36	18	18	
BH2	4	1.50	1.95	U	High strength brown and orangish brown mottled slightly gravelly sandy silty CLAY with rare brick fragments and traces of carbonaceous deposits (gravel is fm and sub-angular)	21	87	33	15	18	
BH2	8	2.50	2.95	U	Medium strength grey, brown and orangish brown mottled slightly gravelly sandy silty CLAY (gravel is fm and rounded to sub-angular)	27	74	42	20	22	
BH2	11	3.00	3.45	B	Brown slightly mottled grey slightly sandy silty CLAY	33	99	62	22	40	

 2519	Test Methods: BS1377: Part 2: 1990: Natural Moisture Content : clause 3.2 Atterberg Limits: clause 4.3, 4.4 and 5.0	Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU Tel: 01923 711 288 Email: James@k4soils.com	Checked and Approved Initials J.P Date: 06/11/2018
	Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)		MSF-5-R1



Summary of Natural Moisture Content, Liquid Limit and Plastic Limit Results

Job No. 25366	Project Name 31 Willoughby Road, London NW3 1RT	Programme	
		Samples received	17/08/2018
Project No. G1808	Client Eldred Geotechnics Ltd	Schedule received	22/10/2018
		Project started	23/10/2018
		Testing Started	01/11/2018

Hole No.	Sample				Soil Description	NMC	Passing 425µm	LL	PL	PI	Remarks
	Ref	Top m	Base m	Type							
BH2	11	3.50	3.95	U	High strength brown and orangish brown mottled silty CLAY with occasional pockets of fine sand and rare fine gravel	31	99	68	24	44	
BH2	14	4.50	4.95	U	High strength slightly mottled orangish brown and grey silty CLAY with occasional pockets of fine sand	34	100	72	24	48	

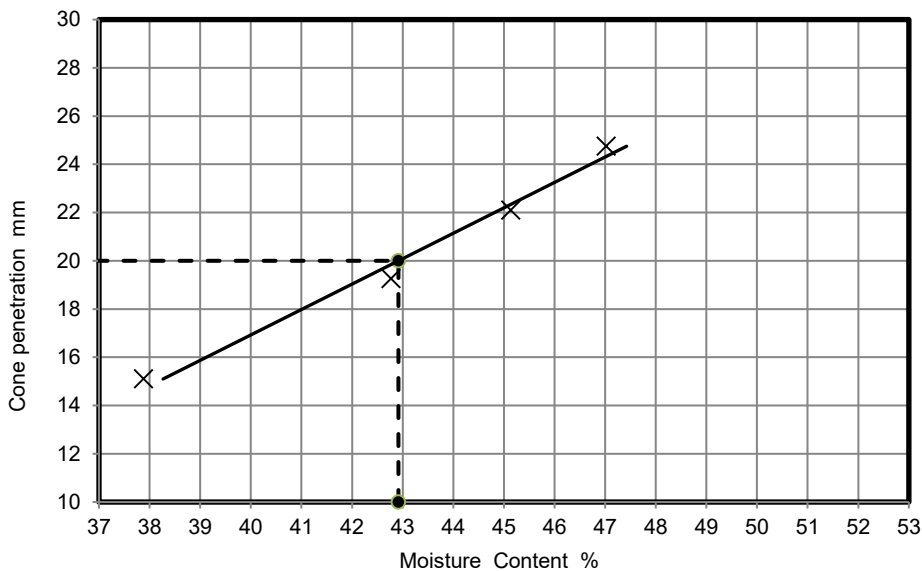
<p>Test Methods: BS1377: Part 2: 1990: Natural Moisture Content : clause 3.2 Atterberg Limits: clause 4.3, 4.4 and 5.0</p>	<p>Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU</p> <p>Tel: 01923 711 288 Email: James@k4soils.com</p>	<p>Checked and Approved</p> <p>Initials J.P</p> <p>Date: 06/11/2018</p>
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LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	4
Depth Top	1.50 m
Depth Base	1.95 m
Sample Type	B
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

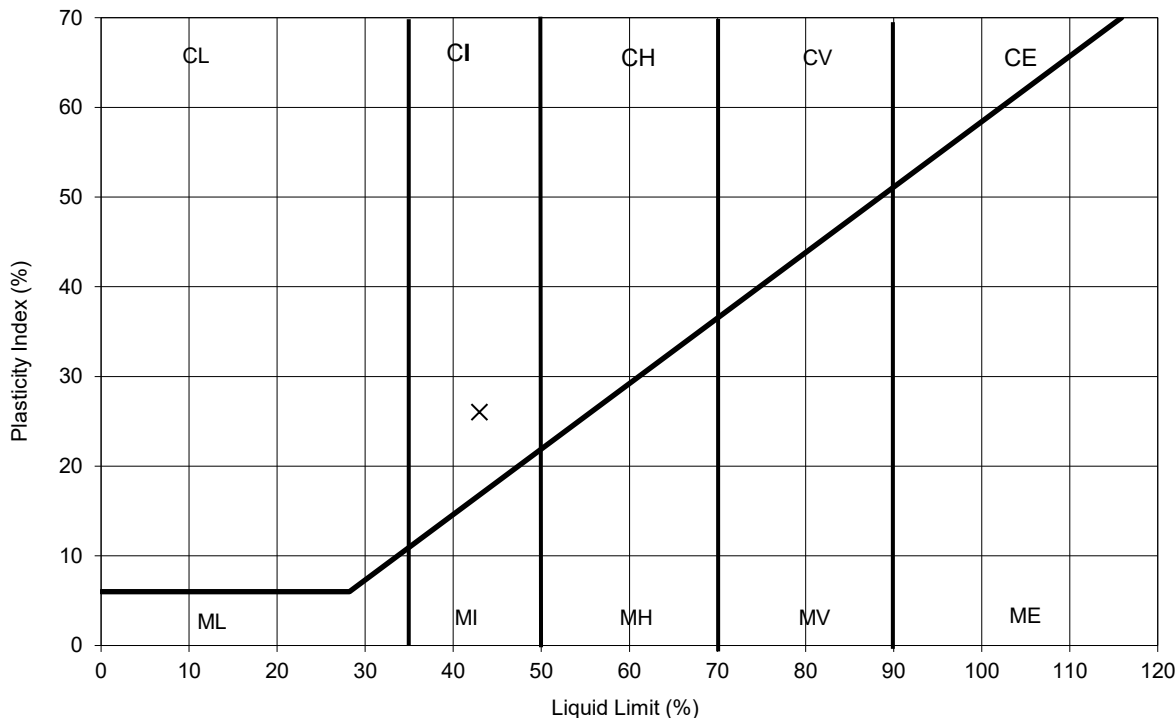
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Green silty clayey SAND with numerous brown slightly sandy silty clay lumps and rare fm sub-angular to sub-rounded gravel		



NATURAL MOISTURE CONTENT	21	%
% PASSING 425µm SIEVE	91	%
LIQUID LIMIT	43	%
PLASTIC LIMIT	17	%
PLASTICITY INDEX	26	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

Initials: J.P
 Date: 06/11/2018



2519

Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

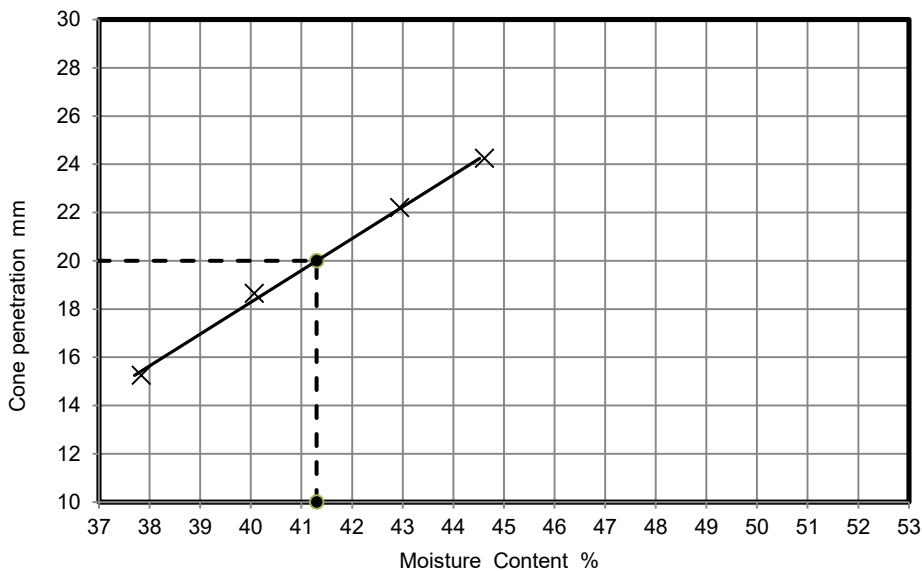
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	5
Depth Top	2.00 m
Depth Base	2.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

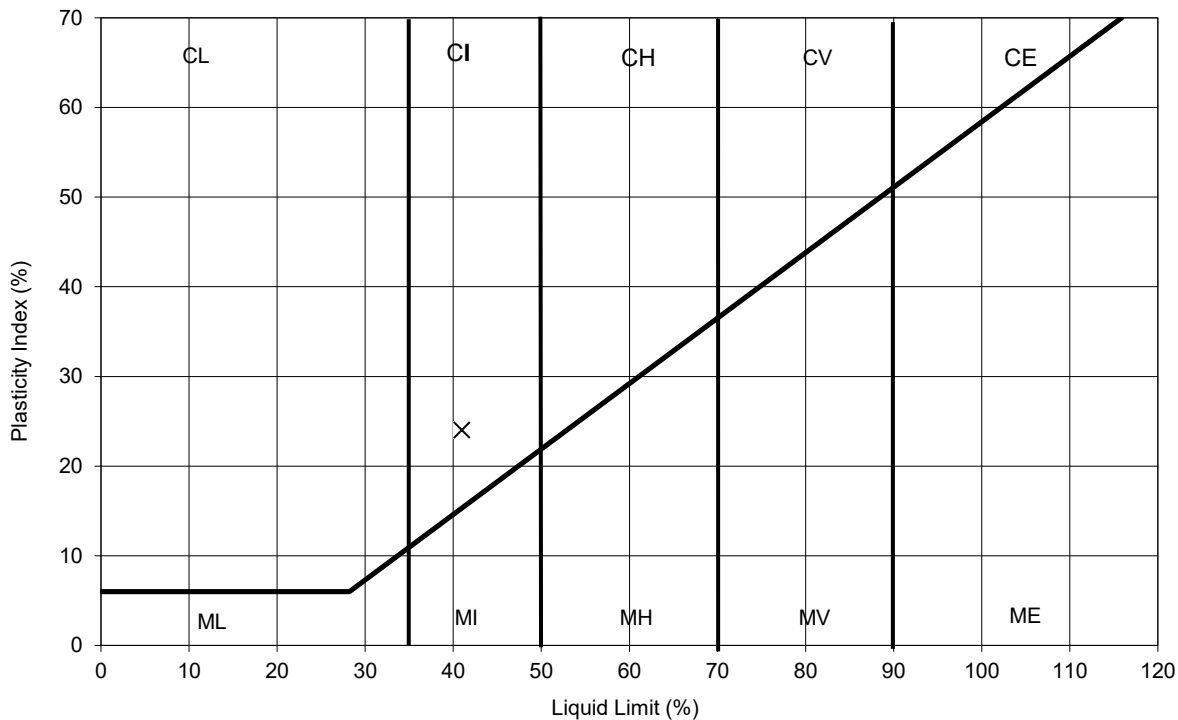
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength brown mottled orangish brown clayey gravelly silty SAND with rare fine brick fragments (gravel is fmc and rounded to sub-angular)		



NATURAL MOISTURE CONTENT	17	%
% PASSING 425µm SIEVE	80	%
LIQUID LIMIT	41	%
PLASTIC LIMIT	17	%
PLASTICITY INDEX	24	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
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Checked and Approved

Initials: J.P
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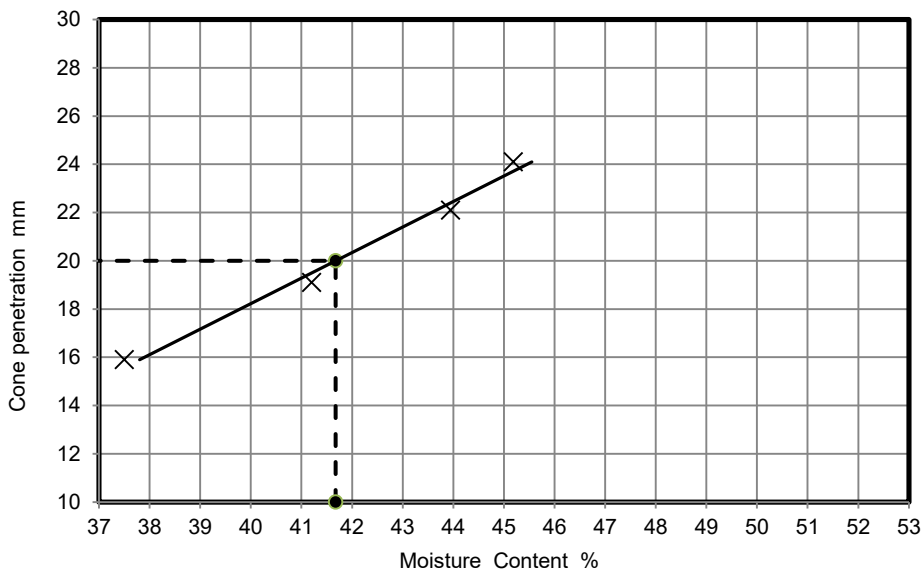
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	8
Depth Top	3.00 m
Depth Base	3.45 m
Sample Type	B
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

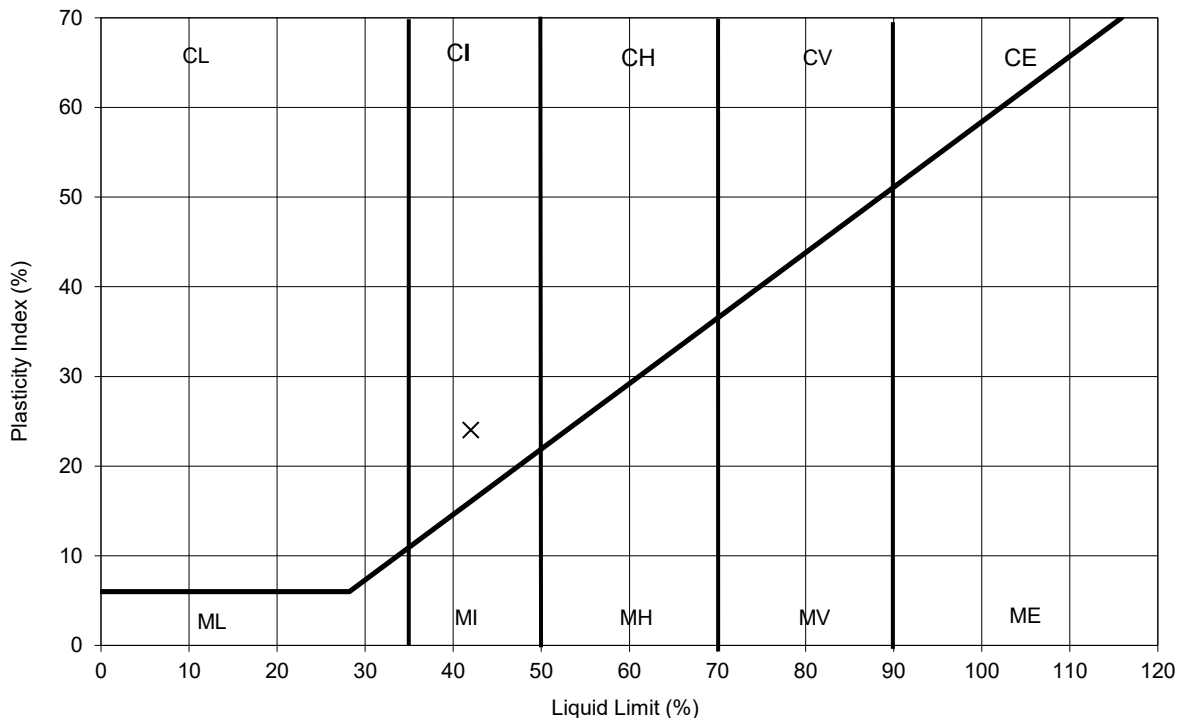
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Brown and occasional greenish grey slightly gravelly sandy silty CLAY (gravel is fm and sub-angular to sub-rounded)		



NATURAL MOISTURE CONTENT	28	%
% PASSING 425µm SIEVE	94	%
LIQUID LIMIT	42	%
PLASTIC LIMIT	18	%
PLASTICITY INDEX	24	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

Initials: J.P
 Date: 06/11/2018



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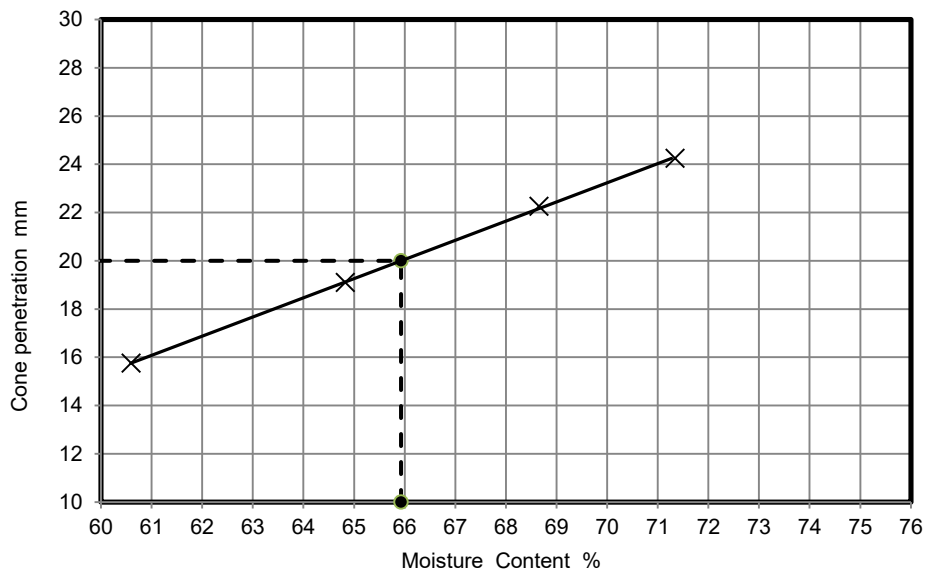
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	10
Depth Top	4.00 m
Depth Base	4.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

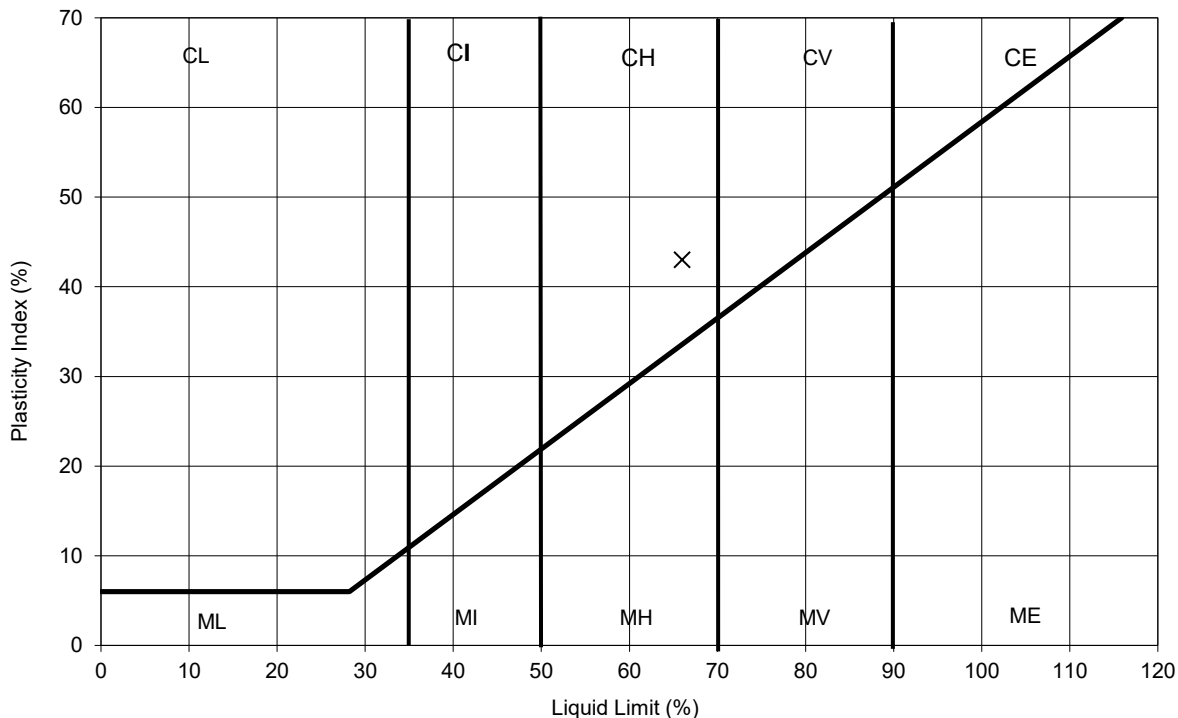
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Medium strength brown slightly mottled grey silty CLAY with rare pockets of orange fine sand / silt and traces of selenite crystals and rootlets		



NATURAL MOISTURE CONTENT	33	%
% PASSING 425µm SIEVE	99	%
LIQUID LIMIT	66	%
PLASTIC LIMIT	23	%
PLASTICITY INDEX	43	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990:Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
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2519

Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

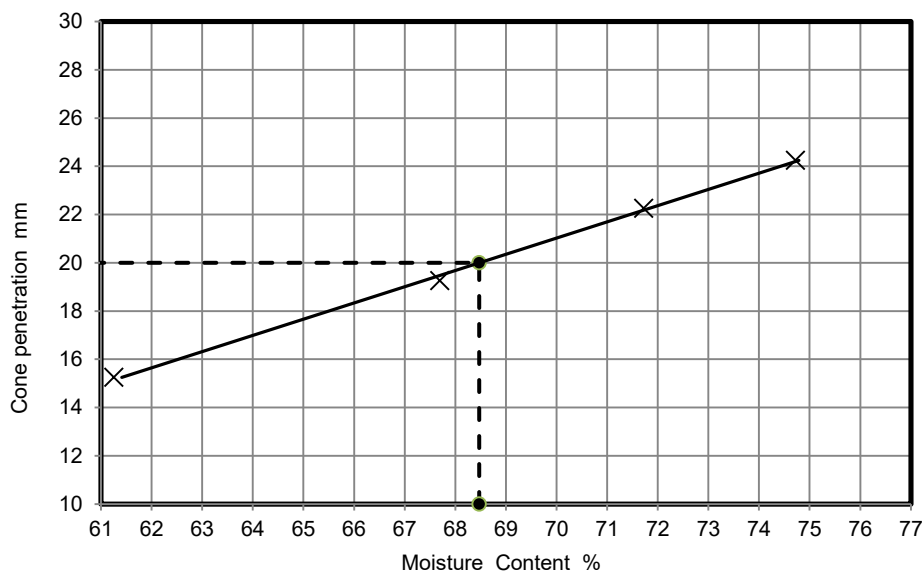
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	12
Depth Top	5.00 m
Depth Base	5.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

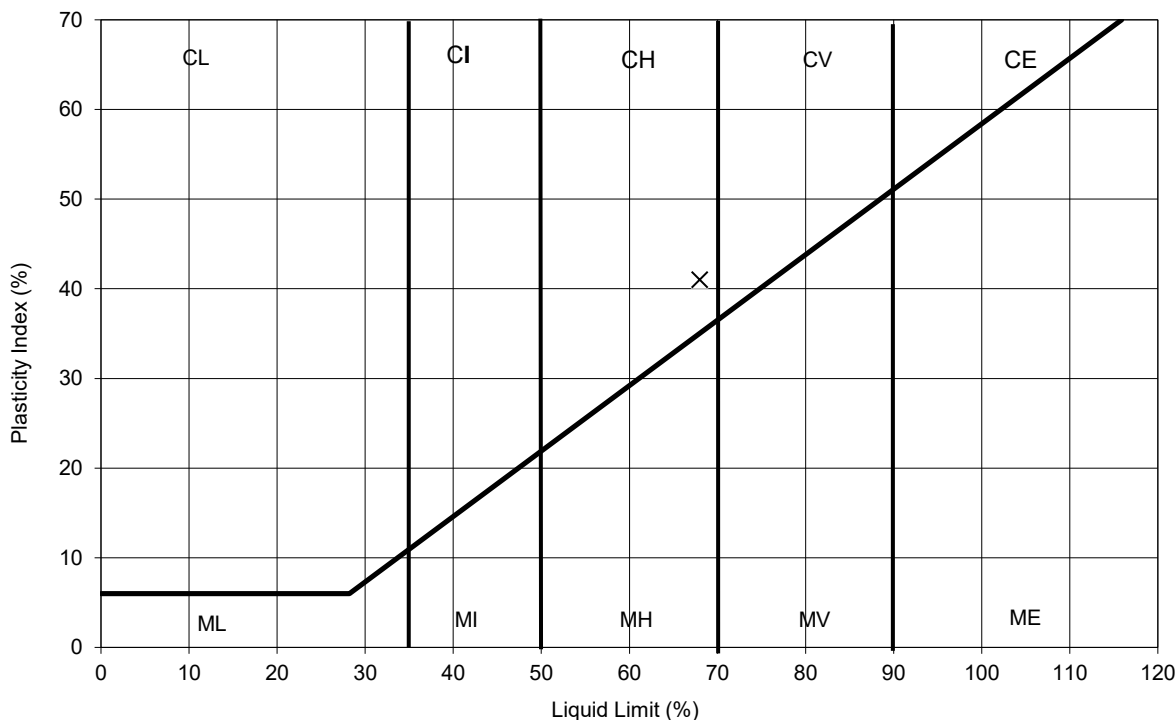
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength brown silty CLAY with rare pockets of orange fine sand / silt		



NATURAL MOISTURE CONTENT	32	%
% PASSING 425µm SIEVE	100	%
LIQUID LIMIT	68	%
PLASTIC LIMIT	27	%
PLASTICITY INDEX	41	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990:Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

Initials: J.P
Date: 06/11/2018



2519

Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

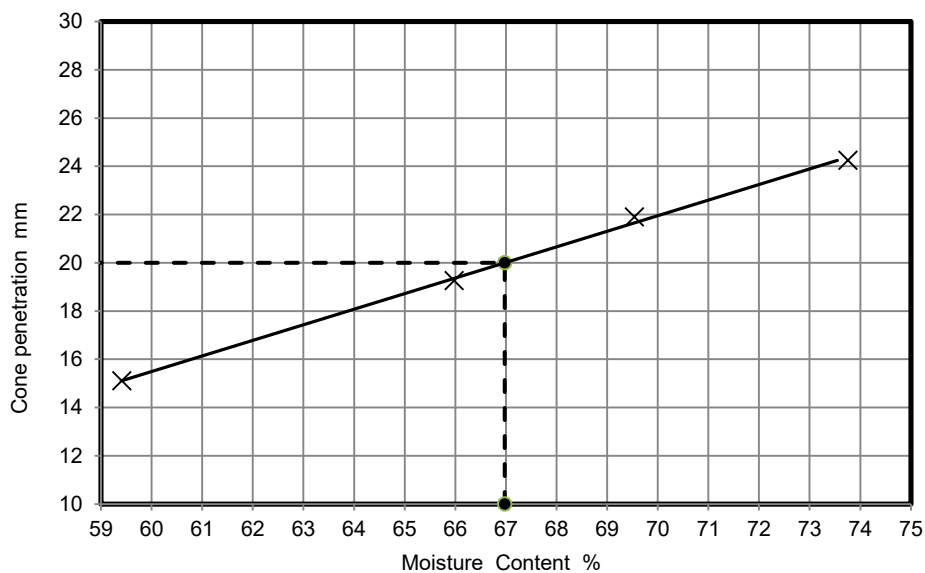
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	14
Depth Top	6.00 m
Depth Base	6.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

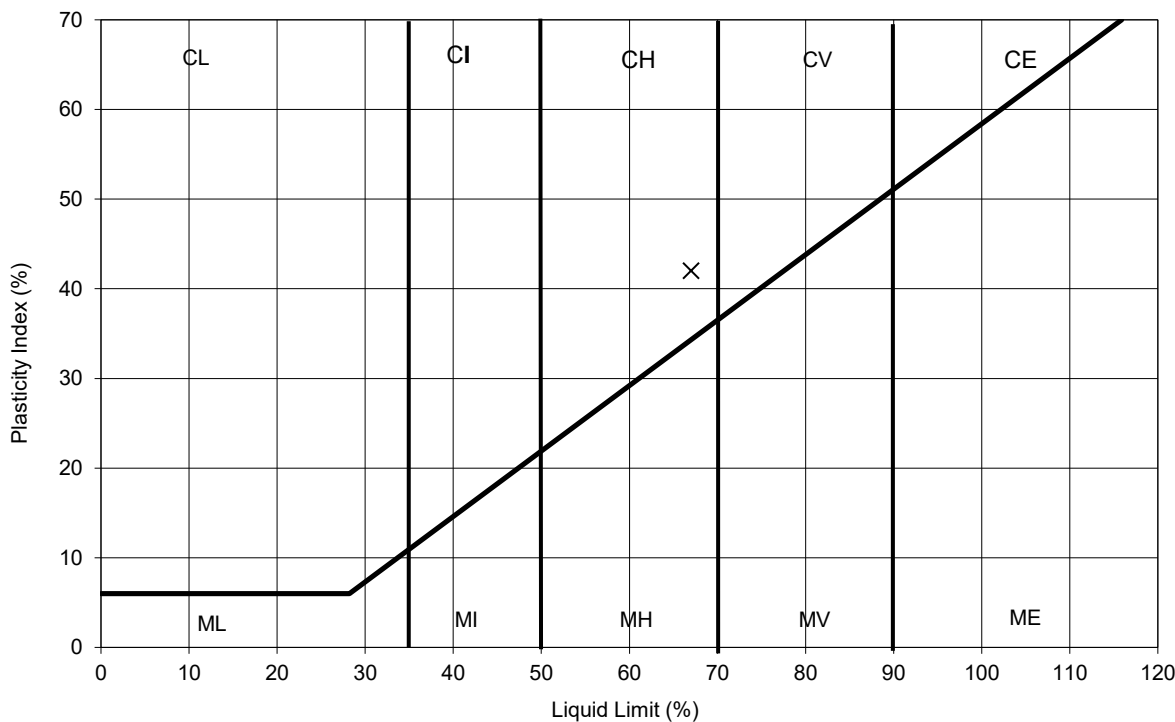
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength dark brown slightly mottled orangish brown silty CLAY with occasional pockets of fine sand / silt		



NATURAL MOISTURE CONTENT	28	%
% PASSING 425µm SIEVE	99	%
LIQUID LIMIT	67	%
PLASTIC LIMIT	25	%
PLASTICITY INDEX	42	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

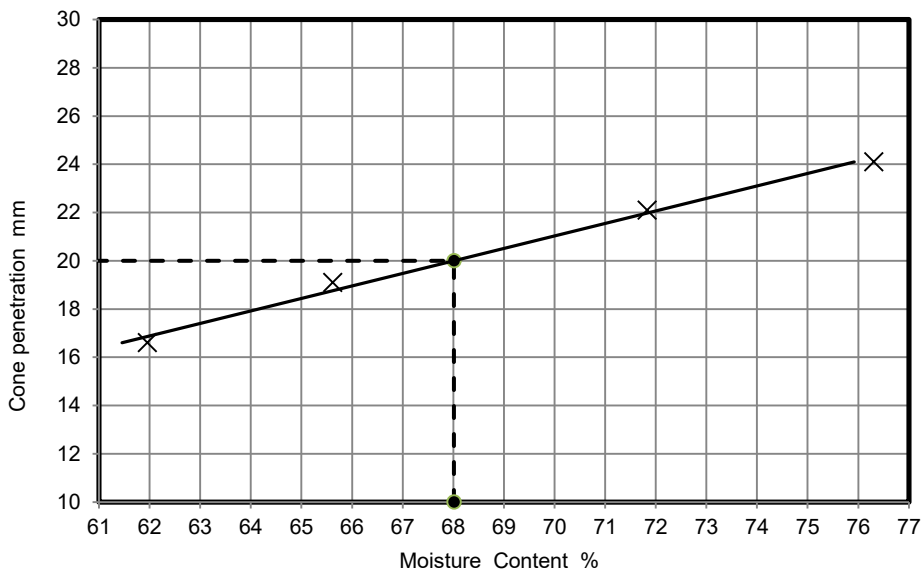
Initials: J.P
 Date: 06/11/2018



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	16
Depth Top	7.00 m
Depth Base	7.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

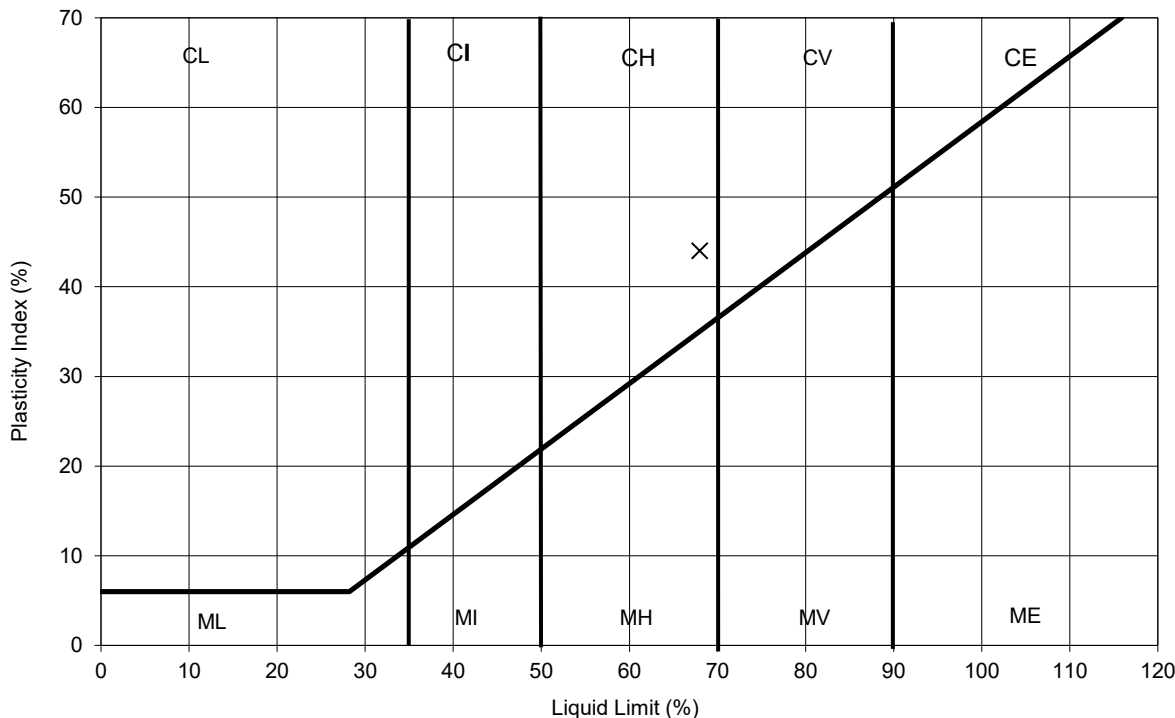
Site Name: 31 Willoughby Road, London NW3 1RT
 Project No.: G1808 Client: Eldred Geotechnics Ltd
 Soil Description: High strength dark grey silty CLAY with rare pockets of fine sand



NATURAL MOISTURE CONTENT	28	%
% PASSING 425µm SIEVE	100	%
LIQUID LIMIT	68	%
PLASTIC LIMIT	24	%
PLASTICITY INDEX	44	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990:Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

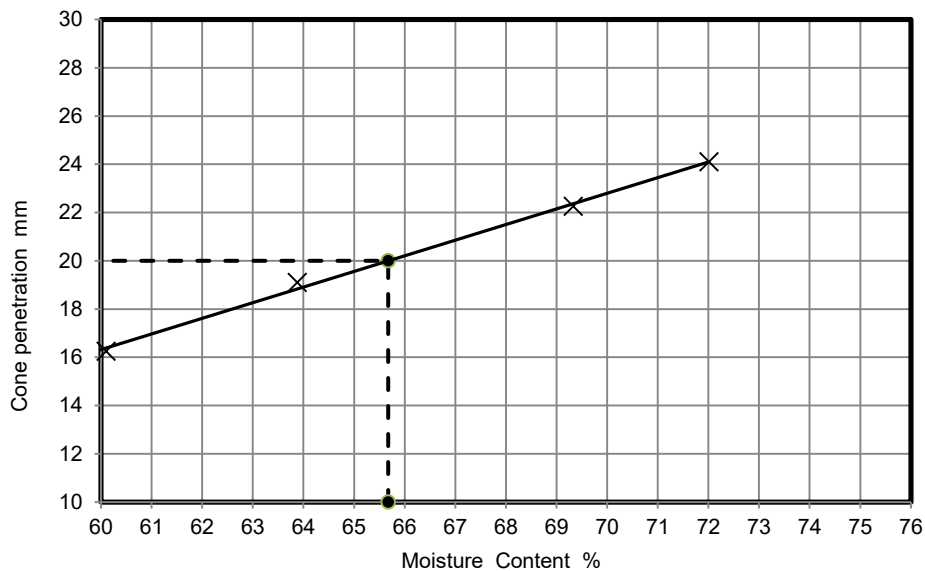
Initials: J.P
Date: 06/11/2018



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH1
Sample No.	18
Depth Top	8.00 m
Depth Base	8.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

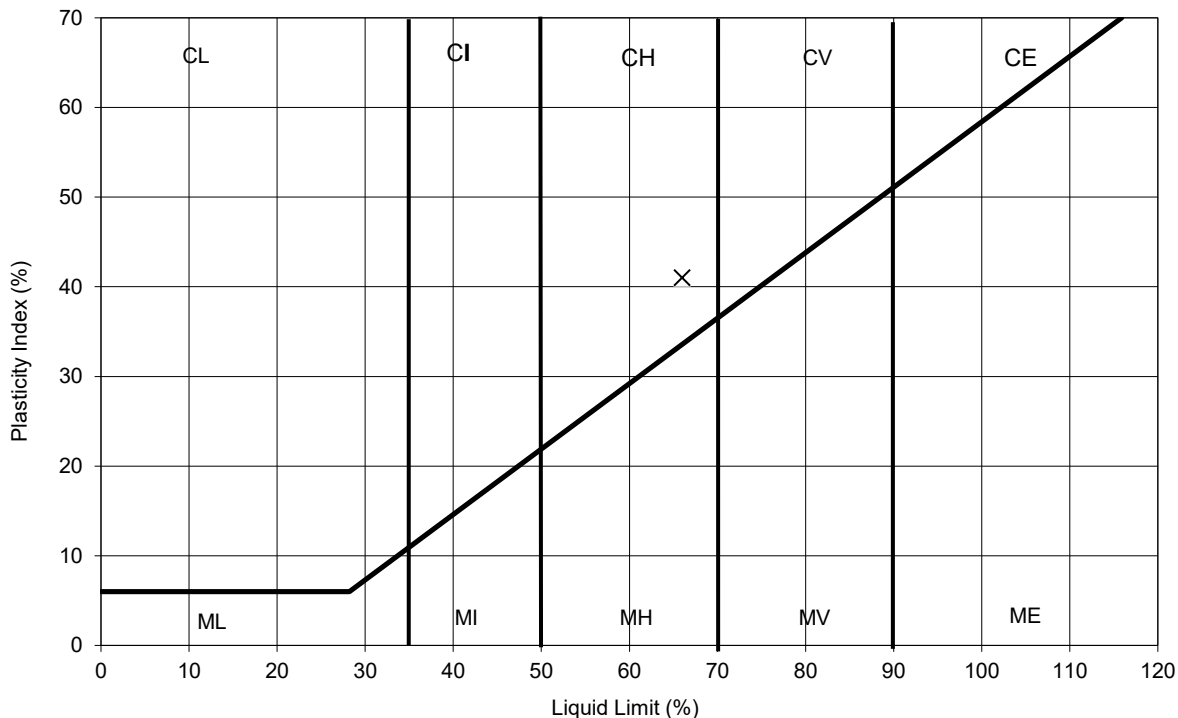
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength dark grey silty CLAY		



NATURAL MOISTURE CONTENT	29	%
% PASSING 425µm SIEVE	100	%
LIQUID LIMIT	66	%
PLASTIC LIMIT	25	%
PLASTICITY INDEX	41	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

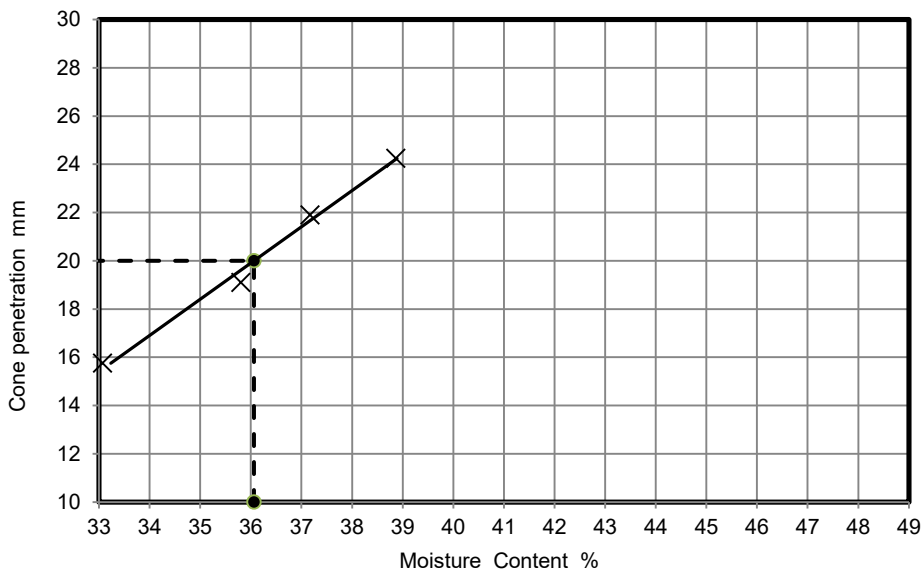
Initials: J.P
 Date: 06/11/2018



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH2
Sample No.	3
Depth Top	1.00 m
Depth Base	1.45 m
Sample Type	B
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

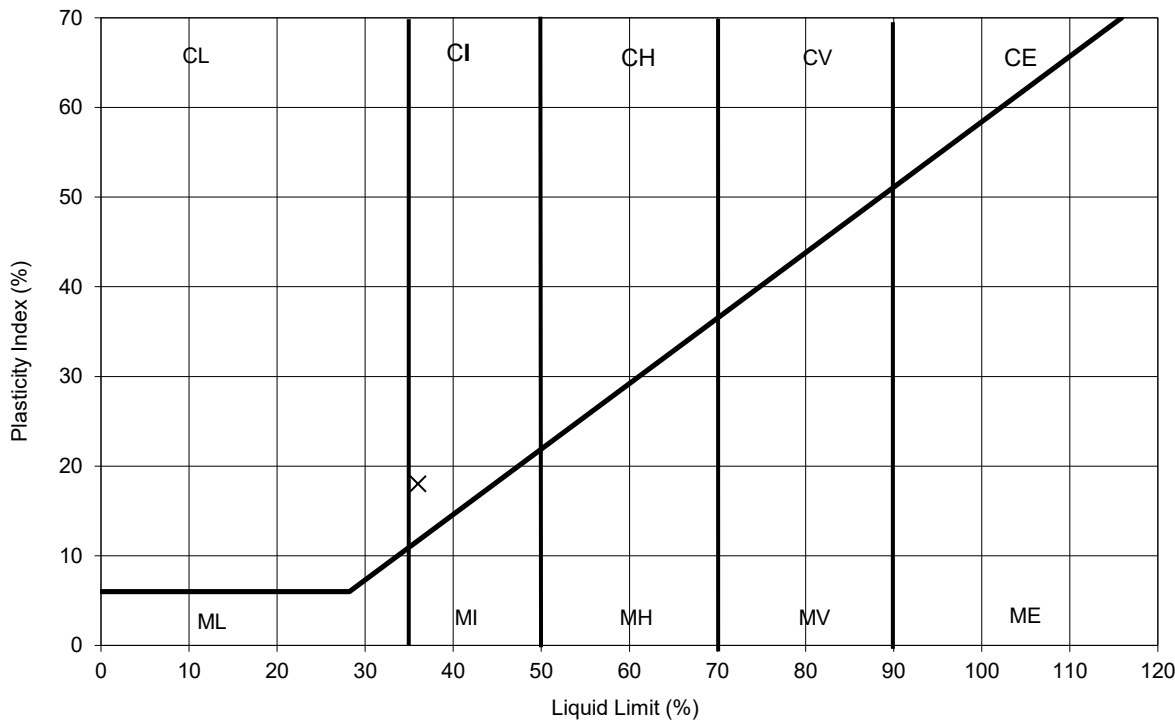
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Greenish grey and occasional dark grey gravelly clayey very silty SAND with rare cobbles (gravel is fmc and sub-angular to sub-rounded)		



NATURAL MOISTURE CONTENT	20	%
% PASSING 425µm SIEVE	87	%
LIQUID LIMIT	36	%
PLASTIC LIMIT	18	%
PLASTICITY INDEX	18	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990:Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

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Initials: J.P
Date: 06/11/2018



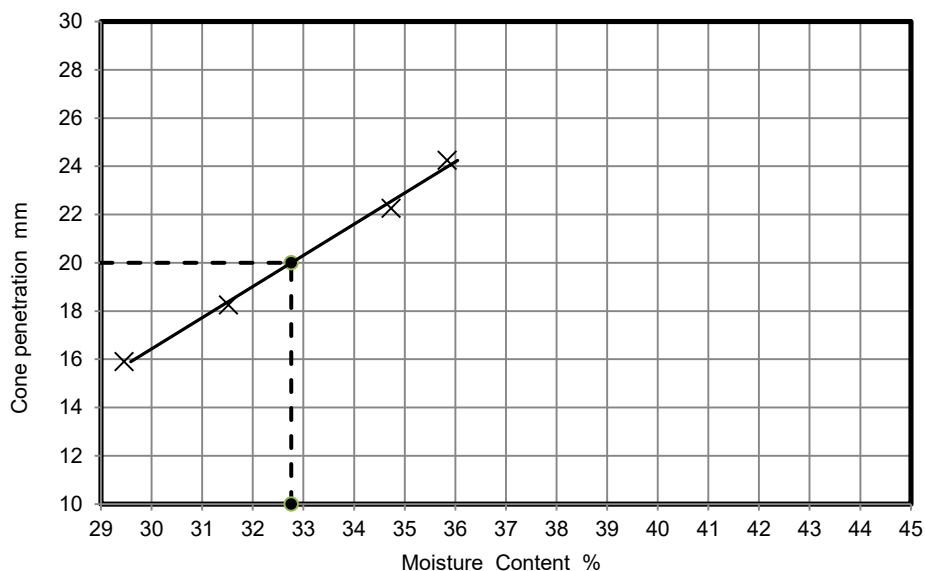
LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH2
Sample No.	4
Depth Top	1.50 m
Depth Base	1.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

Site Name: 31 Willoughby Road, London NW3 1RT

Project No.: G1808 Client: Eldred Geotechnics Ltd

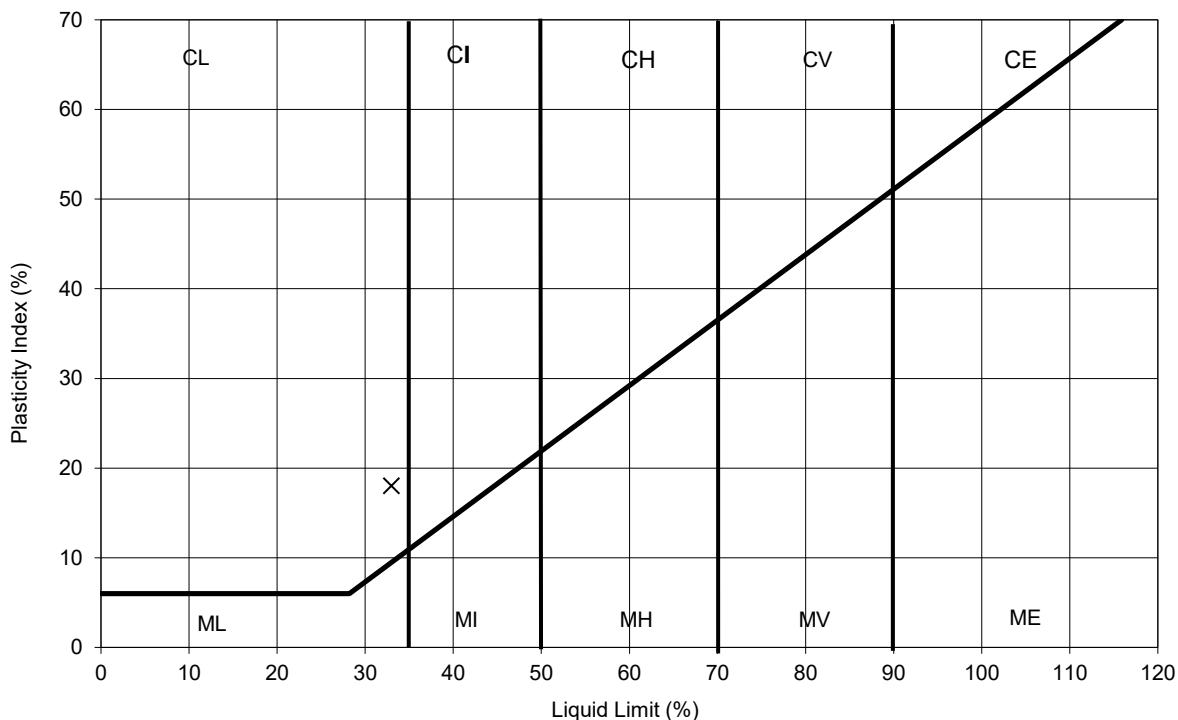
Soil Description: High strength brown and orangish brown mottled slightly gravelly sandy silty CLAY with rare brick fragments and traces of carbonaceous deposits (gravel is fm and sub-angular)



NATURAL MOISTURE CONTENT	21	%
% PASSING 425µm SIEVE	87	%
LIQUID LIMIT	33	%
PLASTIC LIMIT	15	%
PLASTICITY INDEX	18	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
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Checked and Approved

Initials: J.P
 Date: 06/11/2018



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Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

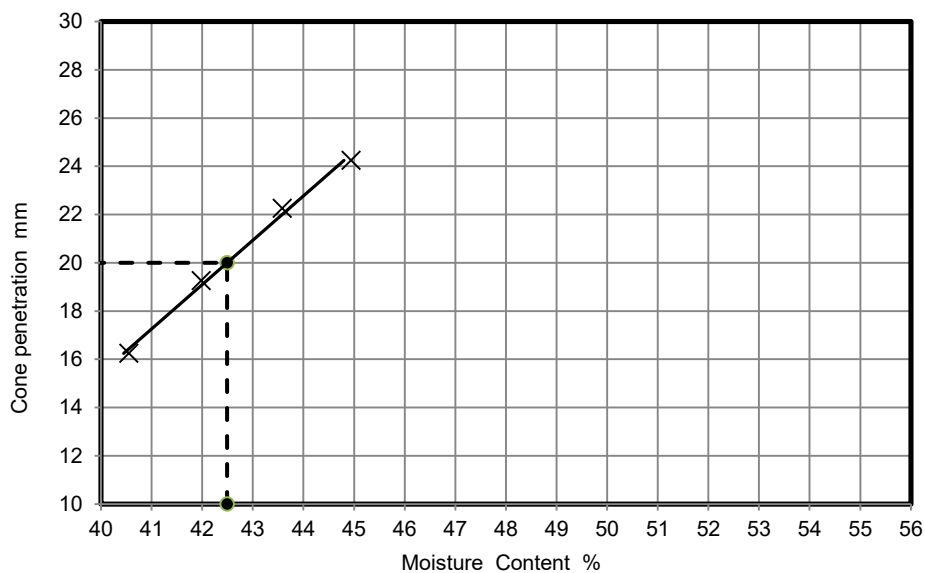
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH2
Sample No.	8
Depth Top	2.50 m
Depth Base	2.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

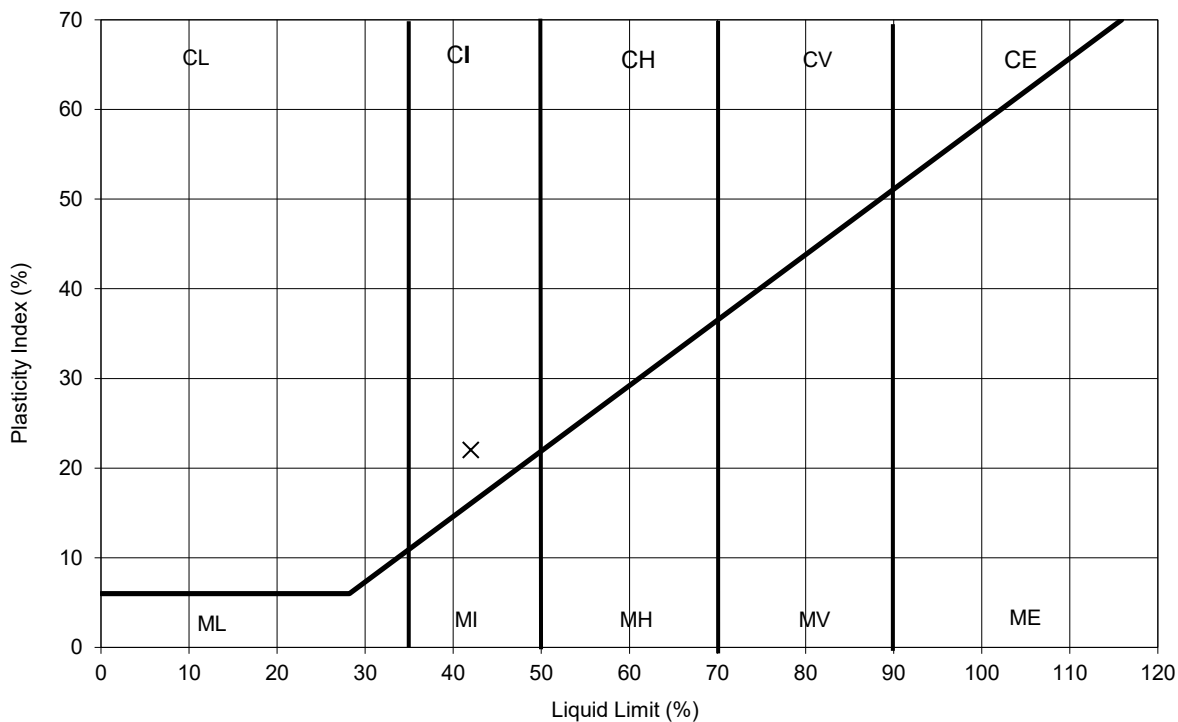
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Medium strength grey, brown and orangish brown mottled slightly gravelly sandy silty CLAY (gravel is fm and rounded to sub-angular)		



NATURAL MOISTURE CONTENT	27	%
% PASSING 425µm SIEVE	74	%
LIQUID LIMIT	42	%
PLASTIC LIMIT	20	%
PLASTICITY INDEX	22	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

Initials: J.P
Date: 06/11/2018



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Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

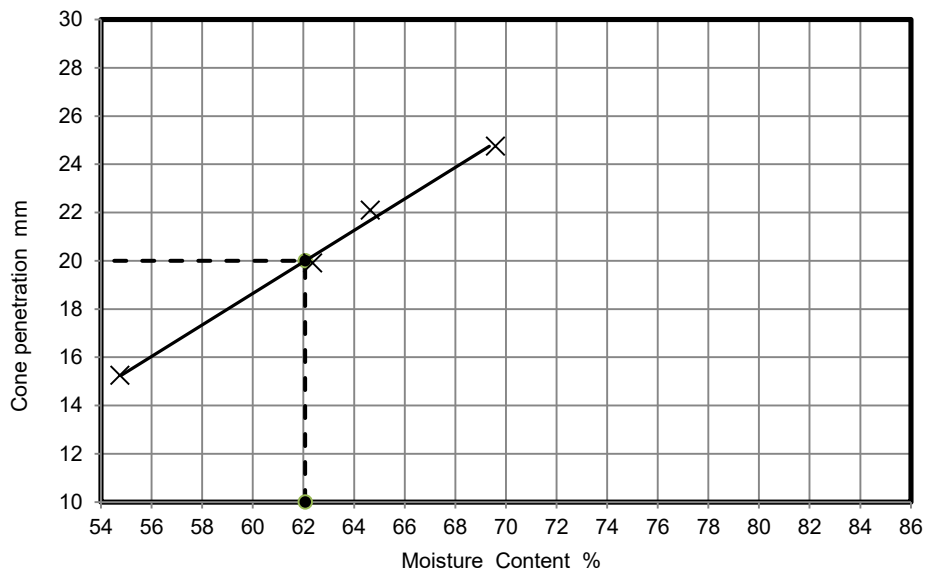
MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH2
Sample No.	11
Depth Top	3.00 m
Depth Base	3.45 m
Sample Type	B
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

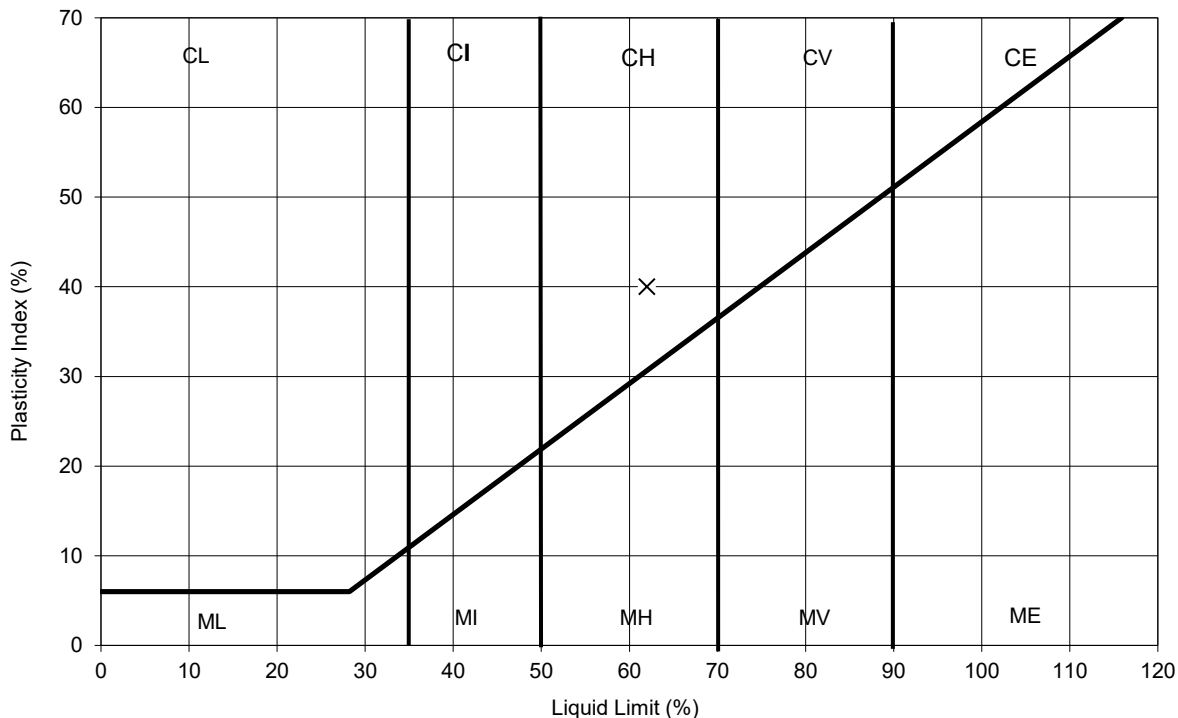
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Brown slightly mottled grey slightly sandy silty CLAY		



NATURAL MOISTURE CONTENT	33	%
% PASSING 425µm SIEVE	99	%
LIQUID LIMIT	62	%
PLASTIC LIMIT	22	%
PLASTICITY INDEX	40	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990:Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

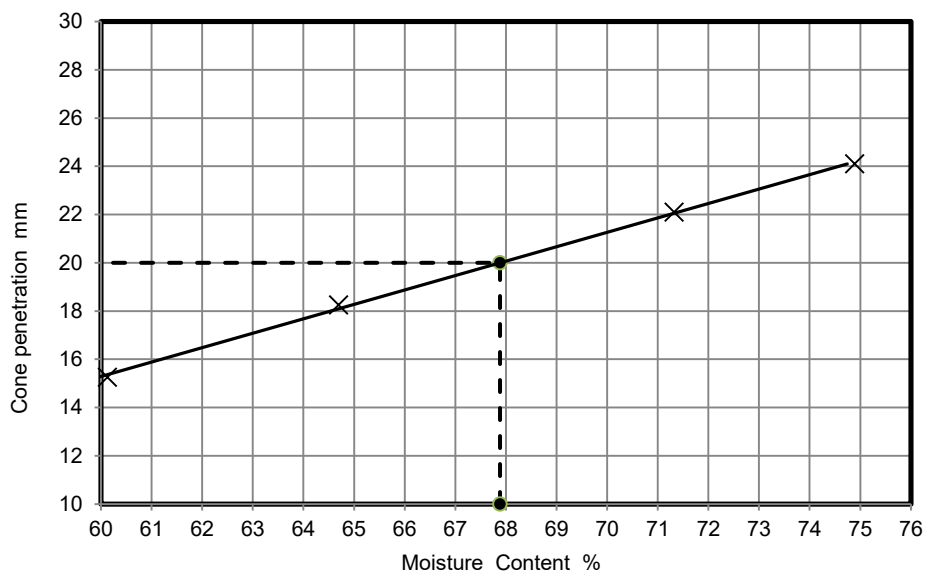
Initials: J.P
 Date: 06/11/2018



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH2
Sample No.	11
Depth Top	3.50 m
Depth Base	3.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

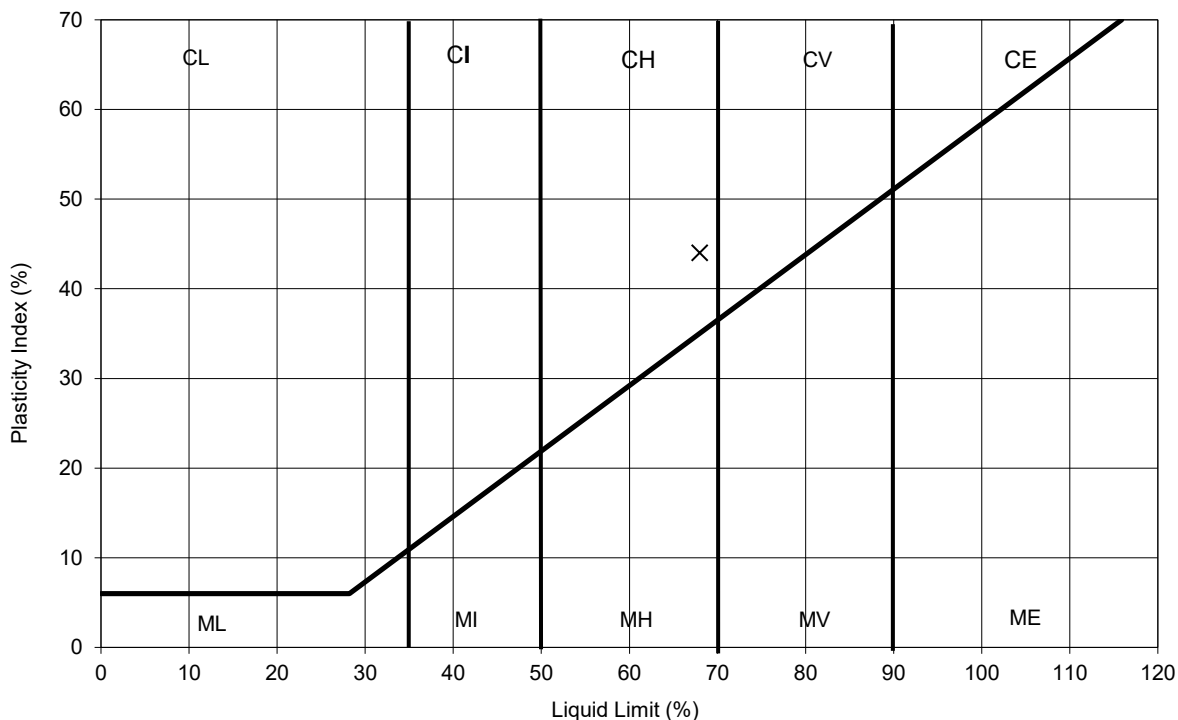
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength brown and orangish brown mottled silty CLAY with occasional pockets of fine sand and rare fine gravel		



NATURAL MOISTURE CONTENT	31	%
% PASSING 425µm SIEVE	99	%
LIQUID LIMIT	68	%
PLASTIC LIMIT	24	%
PLASTICITY INDEX	44	%

Remarks

PLASTICITY INDEX



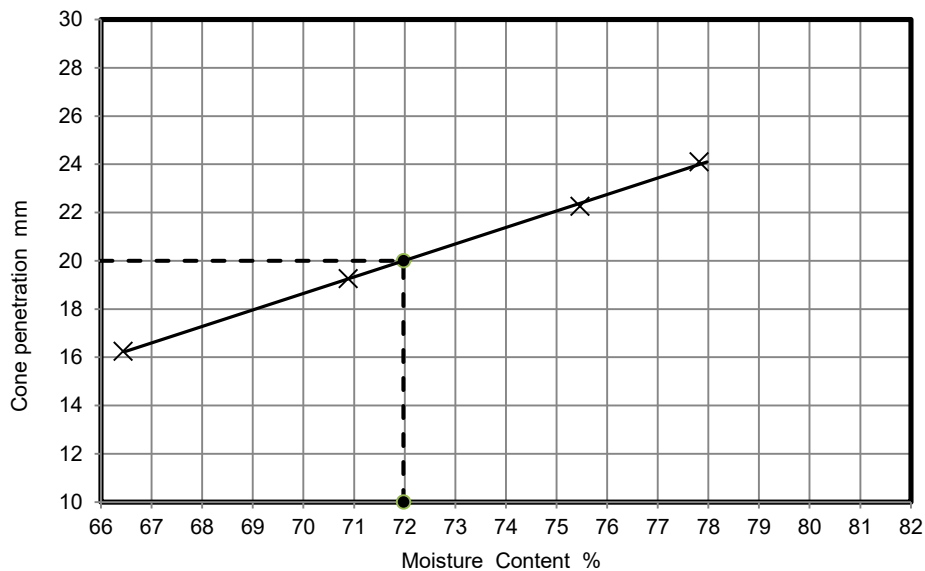
TEST METHOD BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index BS1377: Part 2 :Clause 3.2 : 1990:Determination of the moisture content by the oven drying Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU Tel: 01923 711 288 Email: James@k4soils.com	Checked and Approved
	Initials: J.P
	Date: 06/11/2018
	MSF-5 R2



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

Job No.	25366
Borehole/Pit No.	BH2
Sample No.	14
Depth Top	4.50 m
Depth Base	4.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project Started	23/10/2018
Date Tested	01/11/2018

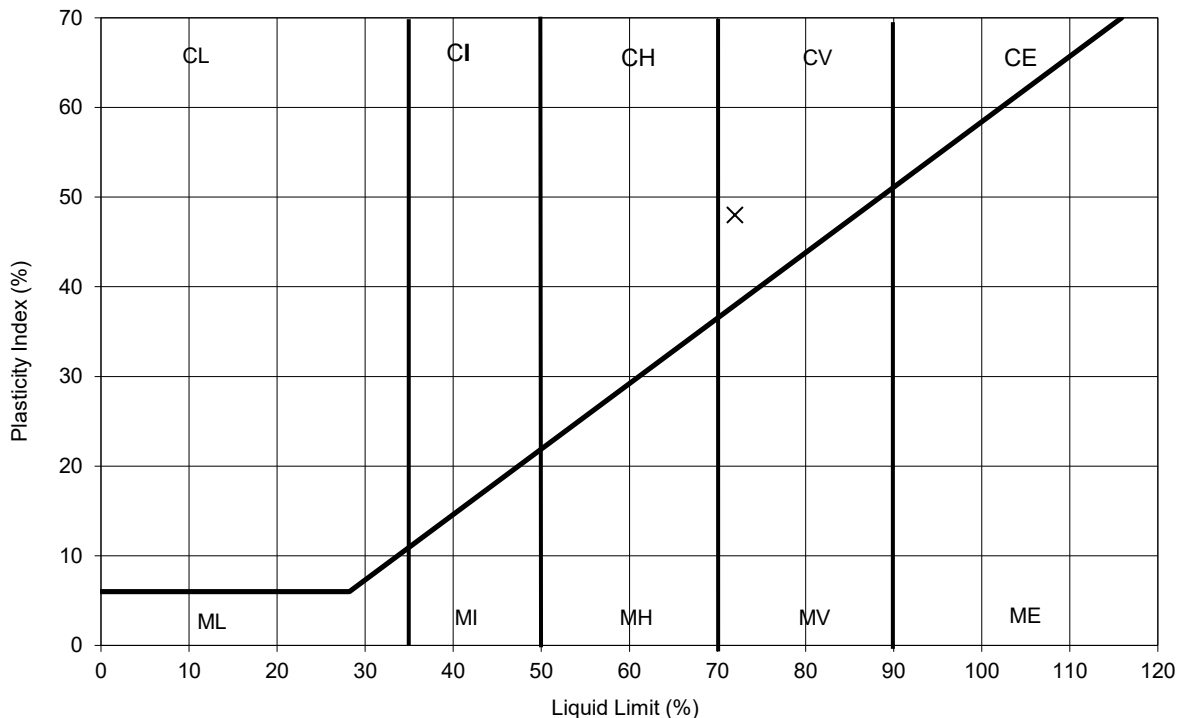
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength slightly mottled orangish brown and grey silty CLAY with occasional pockets of fine sand		



NATURAL MOISTURE CONTENT	34	%
% PASSING 425µm SIEVE	100	%
LIQUID LIMIT	72	%
PLASTIC LIMIT	24	%
PLASTICITY INDEX	48	%

Remarks

PLASTICITY INDEX



TEST METHOD

BS1377: Part 2 :Clause 4.4 : 1990 Determination of the liquid limit by the cone penetrometer method
 BS1377: Part 2 :Clause 5.0 : 1990: Determination of the plastic limit and plasticity index
 BS1377: Part 2 :Clause 3.2 : 1990: Determination of the moisture content by the oven drying
 Test Report by K4 SOILS LABORATORY Unit 8 Olds Close Olds Approach Watford Herts WD18 9RU
 Tel: 01923 711 288 Email: James@k4soils.com

Checked and Approved

Initials: J.P
 Date: 06/11/2018



2519

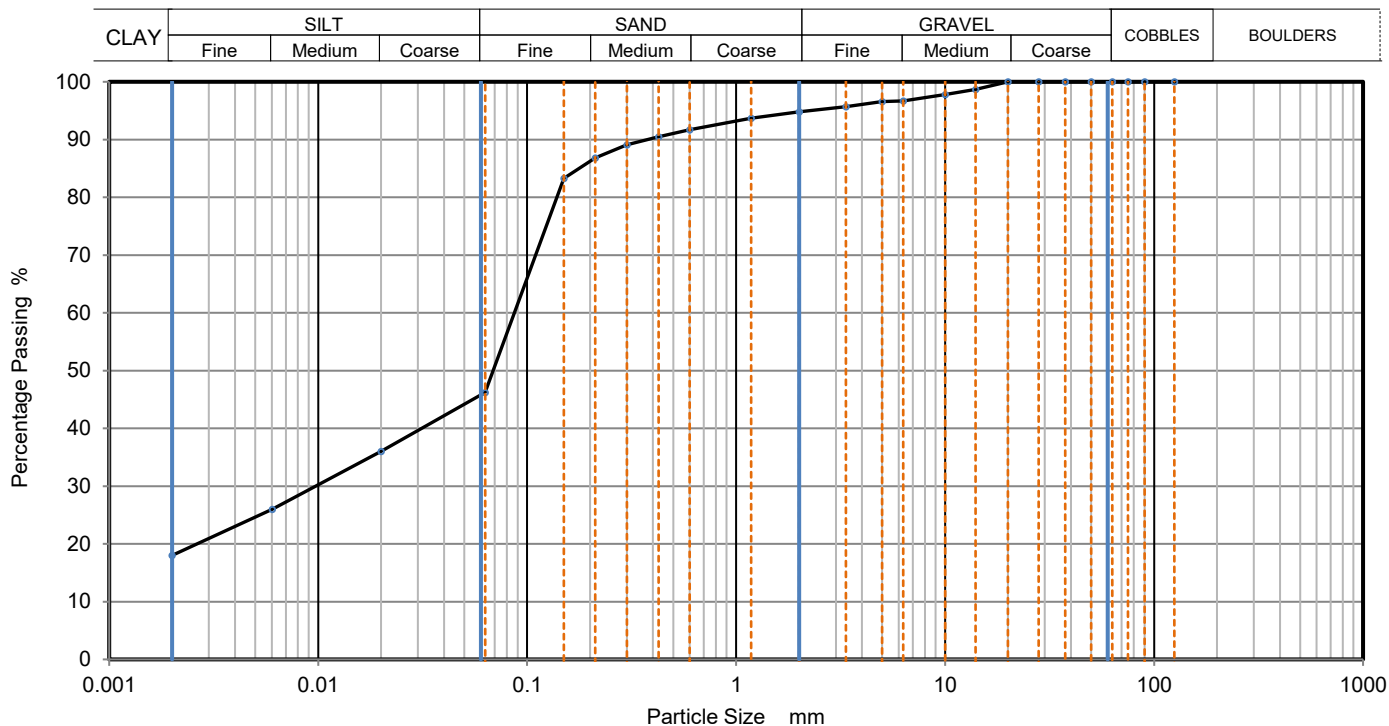
Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

MSF-5 R2



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366			
		Borehole/Pit No.	BH1			
Site Name		31 Willoughby Road, London NW3 1RT		Sample No.	4	
Project No.	G1808	Client	Eldred Geotechnics Ltd		Depth Top	1.50 m
Soil Description	Green silty clayey SAND with numerous brown slightly sandy silty clay lumps and rare fm sub-angular to sub-rounded gravel			Depth Base	1.95 m	
				Sample Type	B	
				Samples received	17/08/2018	
				Schedules received	22/10/2018	
Test Method		BS1377:Part 2: 1990, clause 9.0		Project started	23/10/2018	
				Date tested	01/11/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	36
90	100	0.0060	26
75	100	0.0020	18
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	99		
10	98		
6.3	97		
5	97		
3.35	96		
2	95		
1.18	94		
0.6	92	Particle density (assumed) 2.70 Mg/m ³	
0.425	91		
0.3	89		
0.212	87		
0.15	83		
0.063	46		

Dry Mass of sample, g 333

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	5.2
Sand	48.5
Silt	27.9
Clay	18.4

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks
Preparation and testing in accordance with BS1377 unless noted below



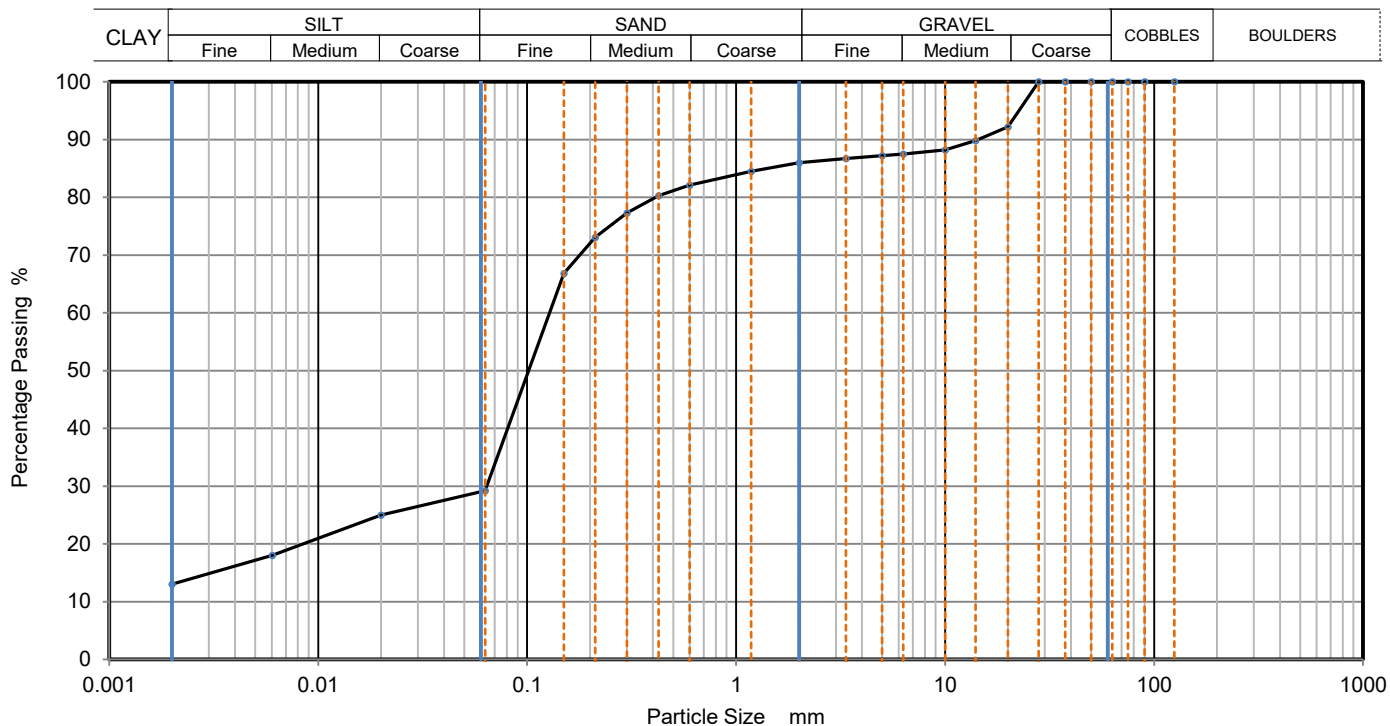
K4 Soils Laboratory
 Unit 8, Olds Close, Watford, Herts, WD18 9RU
 Email: james@k4soils.com
 Tel: 01923 711288

Checked and Approved
 Initials: J.P
 Date: 06/11/2018



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366			
		Borehole/Pit No.	BH1			
Site Name		31 Willoughby Road, London NW3 1RT		Sample No.	5	
Project No.	G1808	Client	Eldred Geotechnics Ltd		Depth Top	2.00 m
Soil Description	High strength brown mottled orangish brown clayey gravelly silty SAND with rare fine brick fragments (gravel is fmc and rounded to sub-angular)			Depth Base	2.45 m	
				Sample Type	U	
				Samples received	17/08/2018	
				Schedules received	22/10/2018	
Test Method		BS1377:Part 2: 1990, clause 9.0		Project started	23/10/2018	
				Date tested	31/10/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	25
90	100	0.0060	18
75	100	0.0020	13
63	100		
50	100		
37.5	100		
28	100		
20	92		
14	90		
10	88		
6.3	88		
5	87		
3.35	87		
2	86		
1.18	85		
0.6	82	Particle density (assumed) 2.70 Mg/m ³	
0.425	80		
0.3	77		
0.212	73		
0.15	67		
0.063	29		

Dry Mass of sample, g

189

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	14.0
Sand	56.8
Silt	16.5
Clay	12.7

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks

Preparation and testing in accordance with BS1377 unless noted below



K4 Soils Laboratory
 Unit 8, Olds Close, Watford, Herts, WD18 9RU
 Email: james@k4soils.com
 Tel: 01923 711288

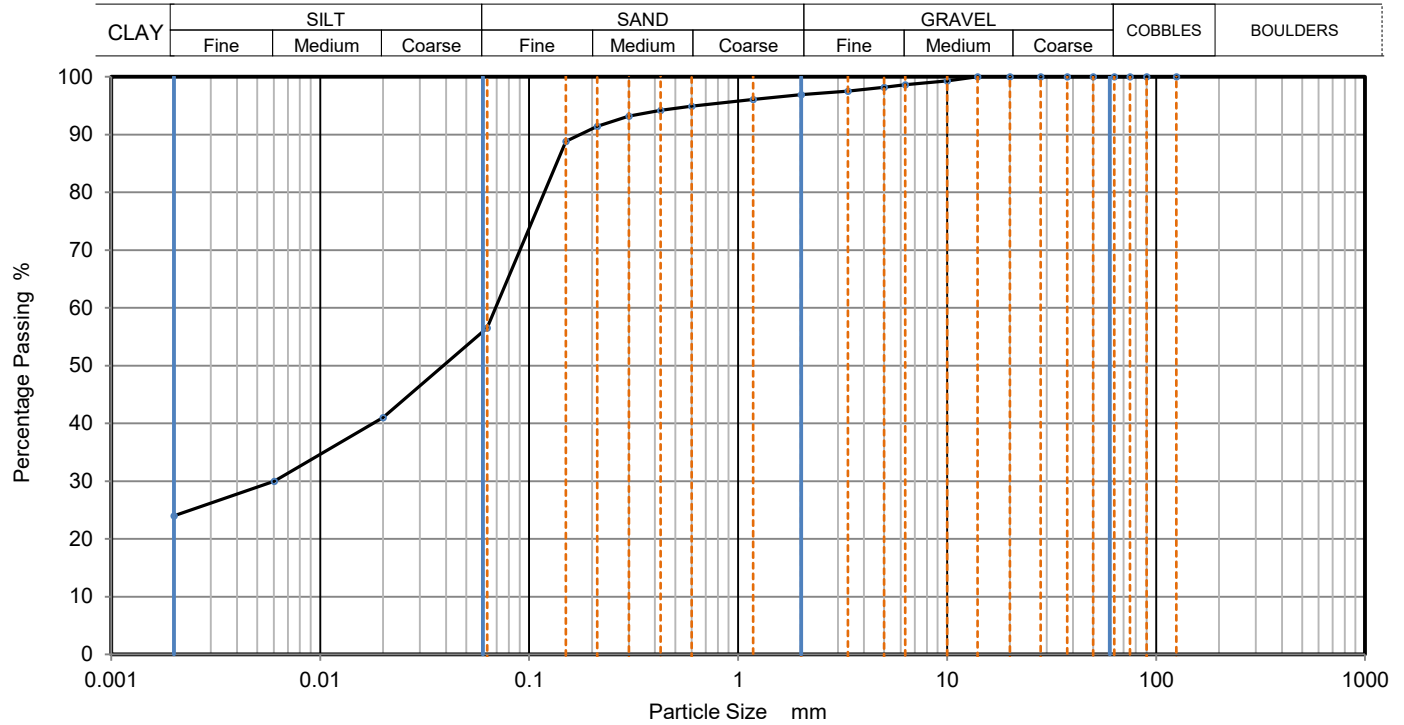
Checked and Approved

Initials: **J.P**
 Date: 06/11/2018



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366			
		Borehole/Pit No.	BH1			
Site Name		31 Willoughby Road, London NW3 1RT		Sample No.	8	
Project No.	G1808	Client	Eldred Geotechnics Ltd		Depth Top	3.00 m
Soil Description	Brown and occasional greenish grey slightly gravelly sandy silty CLAY (gravel is fm and sub-angular to sub-rounded)			Depth Base	3.45 m	
				Sample Type	B	
				Samples received	17/08/2018	
				Schedules received	22/10/2018	
Test Method	BS1377:Part 2: 1990, clause 9.0			Project started	23/10/2018	
				Date tested	01/11/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	41
90	100	0.0060	30
75	100	0.0020	24
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	99		
5	98		
3.35	98		
2	97		
1.18	96		
0.6	95	Particle density (assumed) 2.70 Mg/m ³	
0.425	94		
0.3	93		
0.212	91		
0.15	89		
0.063	57		

Dry Mass of sample, g

349

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	3.1
Sand	40.4
Silt	32.7
Clay	23.8

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks

Preparation and testing in accordance with BS1377 unless noted below



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 Email: james@k4soils.com
 Tel: 01923 711288

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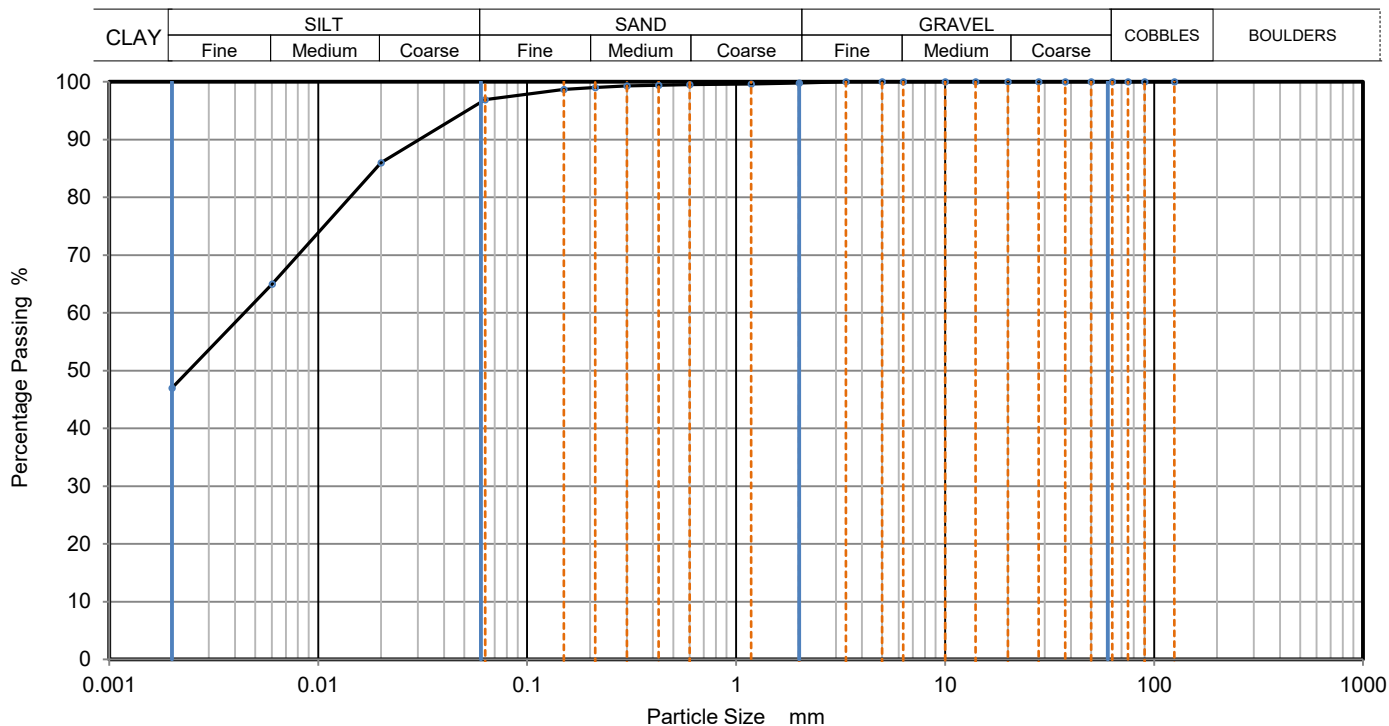
Initials: J.P

Date: 06/11/2018



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366		
		Borehole/Pit No.	BH1		
Site Name	31 Willoughby Road, London NW3 1RT		Sample No.	10	
Project No.	G1808	Client	Eldred Geotechnics Ltd	Depth Top	4.00 m
Soil Description	Medium strength brown slightly mottled grey silty CLAY with rare pockets of orange fine sand / silt and traces of selenite crystals and rootlets			Depth Base	4.45 m
				Sample Type	U
				Samples received	17/08/2018
				Schedules received	22/10/2018
Test Method	BS1377:Part 2: 1990, clause 9.0		Project started	23/10/2018	
			Date tested	31/10/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	86
90	100	0.0060	65
75	100	0.0020	47
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	100		
0.6	100	Particle density (assumed) 2.70 Mg/m ³	
0.425	99		
0.3	99		
0.212	99		
0.15	99		
0.063	97		

Dry Mass of sample, g 4

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.2
Sand	2.9
Silt	50.0
Clay	46.9

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks
Preparation and testing in accordance with BS1377 unless noted below



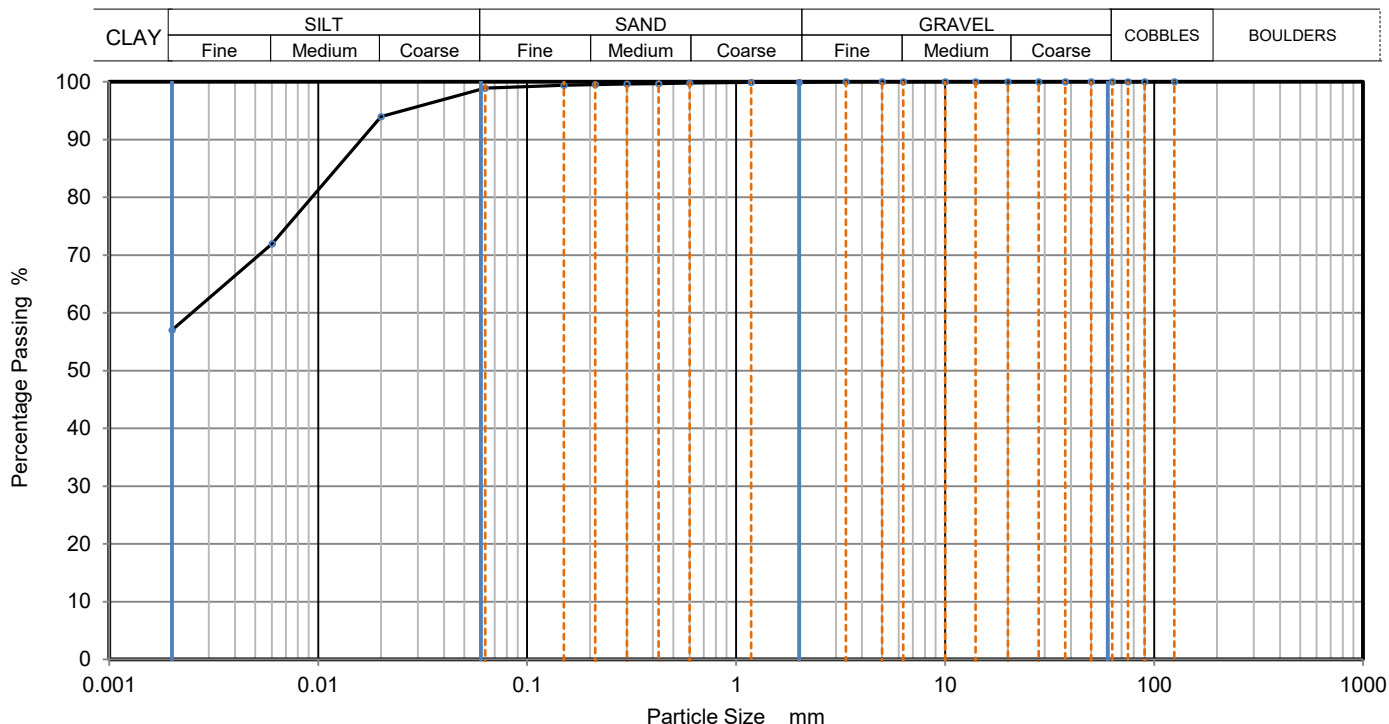
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Date: 06/11/2018



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366		
		Borehole/Pit No.	BH1		
Site Name		31 Willoughby Road, London NW3 1RT			
Project No.	G1808	Client	Eldred Geotechnics Ltd		
Soil Description	High strength brown silty CLAY with rare pockets of orange fine sand / silt			Depth Top	5.00 m
				Depth Base	5.45 m
				Sample Type	U
				Samples received	17/08/2018
Test Method		BS1377:Part 2: 1990, clause 9.0		Project started	23/10/2018
				Date tested	31/10/2018



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	94
90	100	0.0060	72
75	100	0.0020	57
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	100		
0.6	100	Particle density (assumed)	
0.425	100	2.70	Mg/m ³
0.3	100		
0.212	100		
0.15	99		
0.063	99		

Dry Mass of sample, g 3

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.1
Sand	1.1
Silt	42.2
Clay	56.6

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks
Preparation and testing in accordance with BS1377 unless noted below



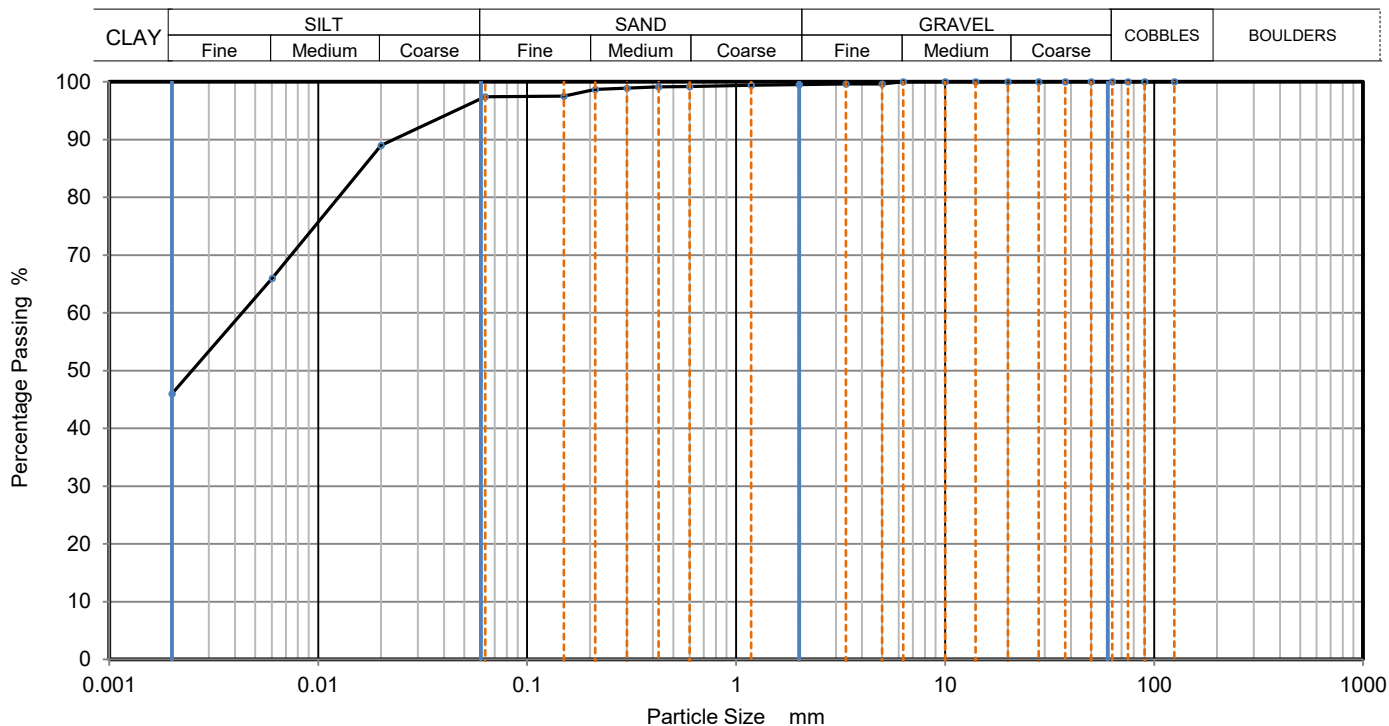
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PARTICLE SIZE DISTRIBUTION

		Job Ref	25366			
		Borehole/Pit No.	BH1			
Site Name		31 Willoughby Road, London NW3 1RT		Sample No.	14	
Project No.	G1808	Client	Eldred Geotechnics Ltd		Depth Top	6.00 m
Soil Description	High strength dark brown slightly mottled orangish brown silty CLAY with occasional pockets of fine sand / silt			Depth Base	6.45 m	
				Sample Type	U	
				Samples received	17/08/2018	
				Schedules received	22/10/2018	
Test Method		BS1377:Part 2: 1990, clause 9.0		Project started	23/10/2018	
				Date tested	31/10/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	89
90	100	0.0060	66
75	100	0.0020	46
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	99		
0.6	99	Particle density (assumed) 2.70 Mg/m ³	
0.425	99		
0.3	99		
0.212	99		
0.15	98		
0.063	97		

Dry Mass of sample, g

4

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.5
Sand	2.1
Silt	51.6
Clay	45.8

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks

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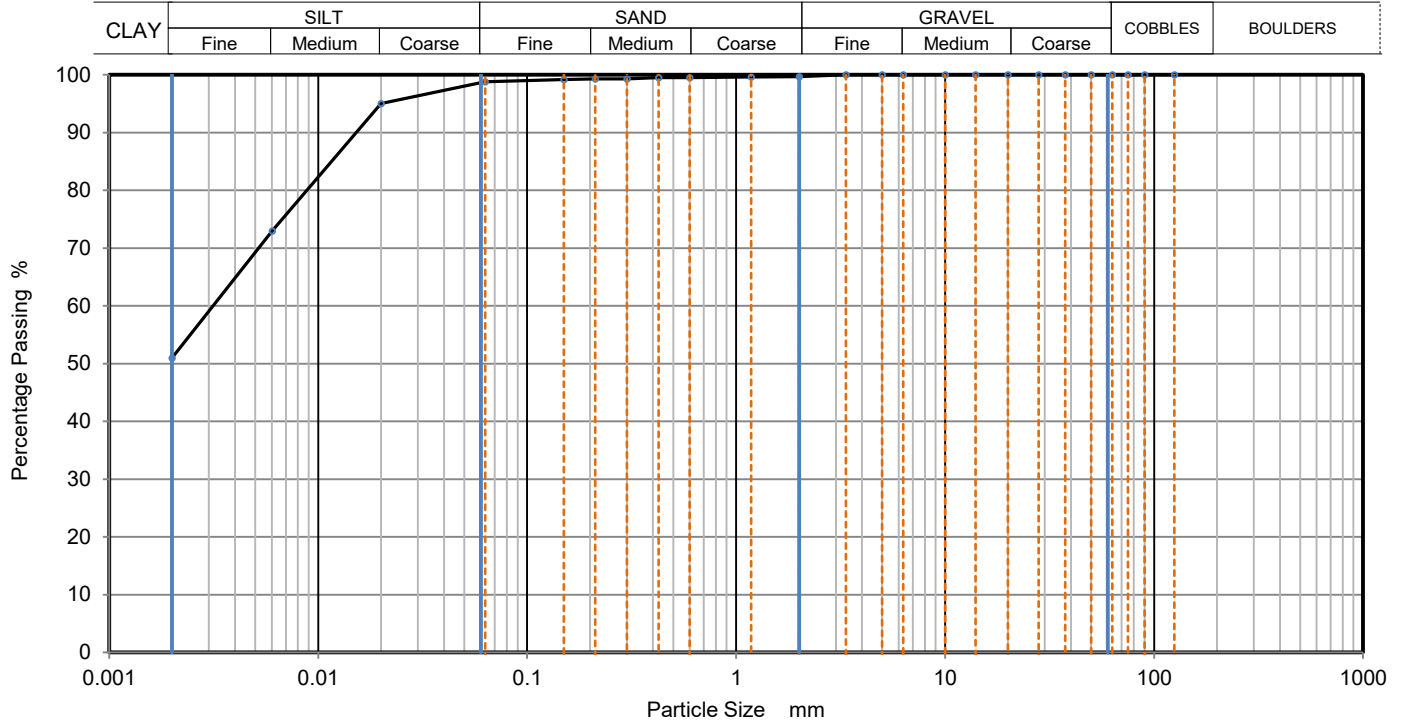
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PARTICLE SIZE DISTRIBUTION

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	16
Depth Top	7.00 m
Depth Base	7.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project started	23/10/2018
Date tested	31/10/2018

Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	High strength dark grey silty CLAY with rare pockets of fine sand		
Test Method	BS1377:Part 2: 1990, clause 9.0		



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	95
90	100	0.0060	73
75	100	0.0020	51
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	100		
0.6	100	Particle density (assumed)	
0.425	100	2.70	Mg/m ³
0.3	99		
0.212	99		
0.15	99		
0.063	99		

Dry Mass of sample, g 1

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.3
Sand	1.0
Silt	47.3
Clay	51.4

Grading Analysis		
D100	mm	
D60	mm	0.00312
D30	mm	
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

Remarks
Preparation and testing in accordance with BS1377 unless noted below



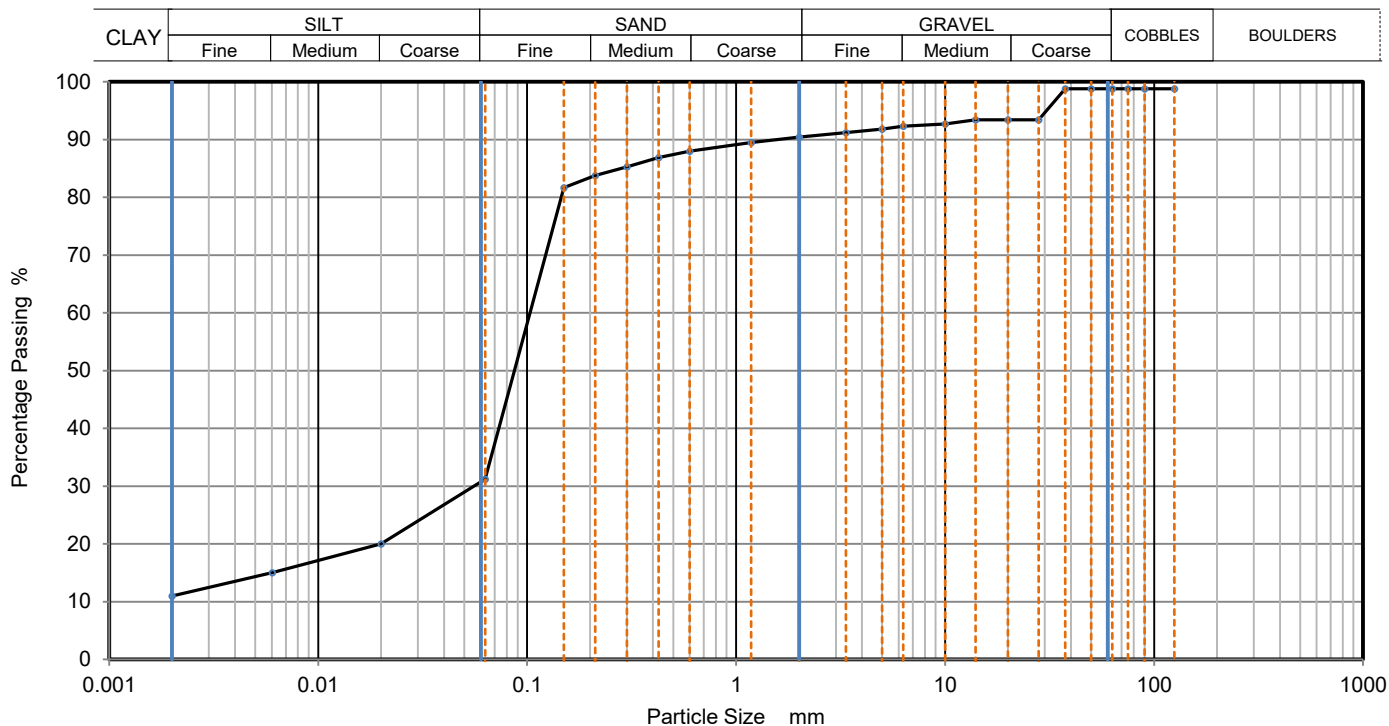
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PARTICLE SIZE DISTRIBUTION

		Job Ref	25366			
		Borehole/Pit No.	BH2			
Site Name		31 Willoughby Road, London NW3 1RT		Sample No.	3	
Project No.	G1808	Client	Eldred Geotechnics Ltd		Depth Top	1.00 m
Soil Description	Greenish grey and occasional dark grey gravelly clayey very silty SAND with rare cobbles (gravel is fmc and sub-angular to sub-rounded)			Depth Base	1.45 m	
				Sample Type	B	
				Samples received	17/08/2018	
				Schedules received	22/10/2018	
Test Method	BS1377:Part 2: 1990, clause 9.0			Project started	23/10/2018	
				Date tested	01/11/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	99	0.0200	20
90	99	0.0060	15
75	99	0.0020	11
63	99		
50	99		
37.5	99		
28	93		
20	93		
14	93		
10	93		
6.3	92		
5	92		
3.35	91		
2	90		
1.18	90		
0.6	88	Particle density (assumed) 2.70 Mg/m ³	
0.425	87		
0.3	85		
0.212	84		
0.15	82		
0.063	31		

Dry Mass of sample, g 601

Sample Proportions	% dry mass
Very coarse	1.2
Gravel	8.4
Sand	59.2
Silt	20.1
Clay	11.1

Grading Analysis		
D100	mm	
D60	mm	0.103
D30	mm	0.0557
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

Remarks
Preparation and testing in accordance with BS1377 unless noted below



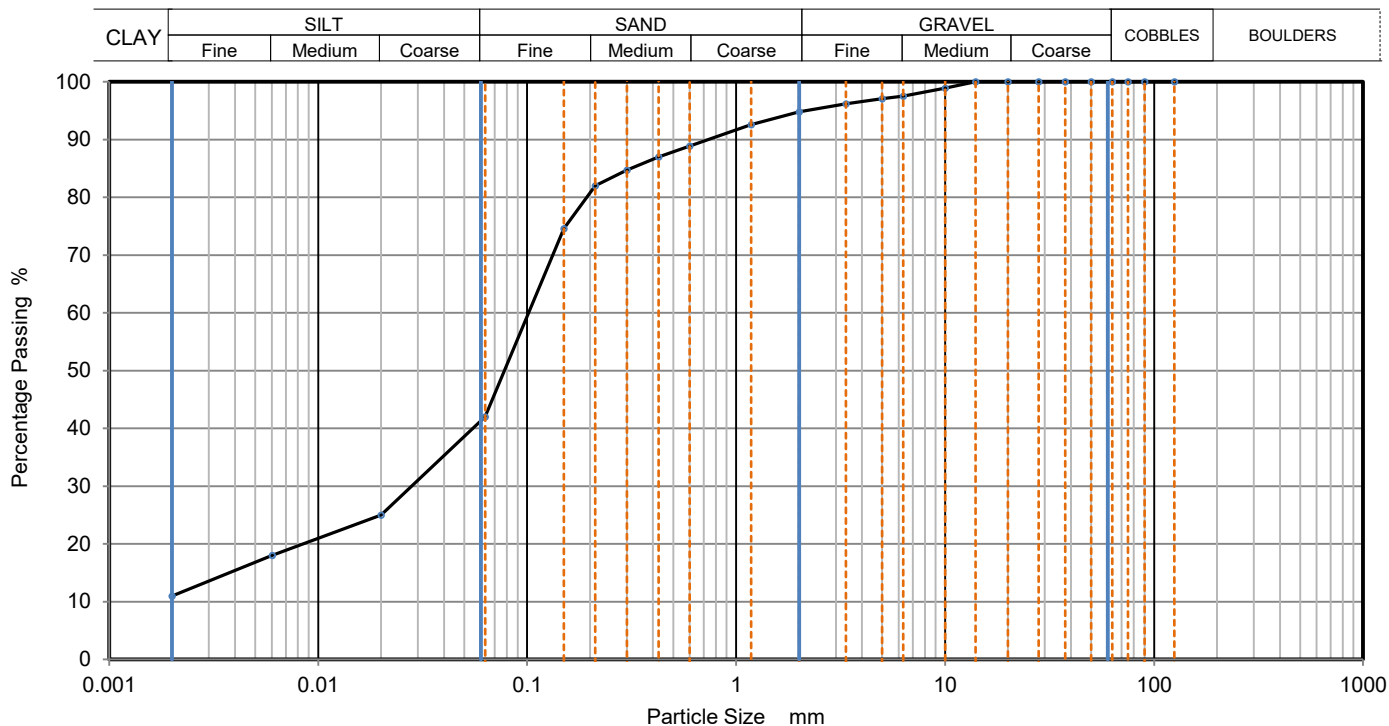
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PARTICLE SIZE DISTRIBUTION

			Job Ref	25366	
			Borehole/Pit No.	BH2	
Site Name			31 Willoughby Road, London NW3 1RT	Sample No.	4
Project No.	G1808	Client	Eldred Geotechnics Ltd	Depth Top	1.50 m
Soil Description	High strength brown and orangish brown mottled slightly gravelly sandy silty CLAY with rare brick fragments and traces of carbonaceous deposits (gravel is fm and sub-angular)			Depth Base	1.95 m
				Sample Type	U
				Samples received	17/08/2018
				Schedules received	22/10/2018
Test Method			BS1377:Part 2: 1990, clause 9.0	Project started	23/10/2018
				Date tested	31/10/2018



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	25
90	100	0.0060	18
75	100	0.0020	11
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	99		
6.3	98		
5	97		
3.35	96		
2	95		
1.18	93		
0.6	89	Particle density (assumed) 2.70 Mg/m ³	
0.425	87		
0.3	85		
0.212	82		
0.15	75		
0.063	42		

Dry Mass of sample, g 312

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	5.2
Sand	52.8
Silt	30.7
Clay	11.3

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks
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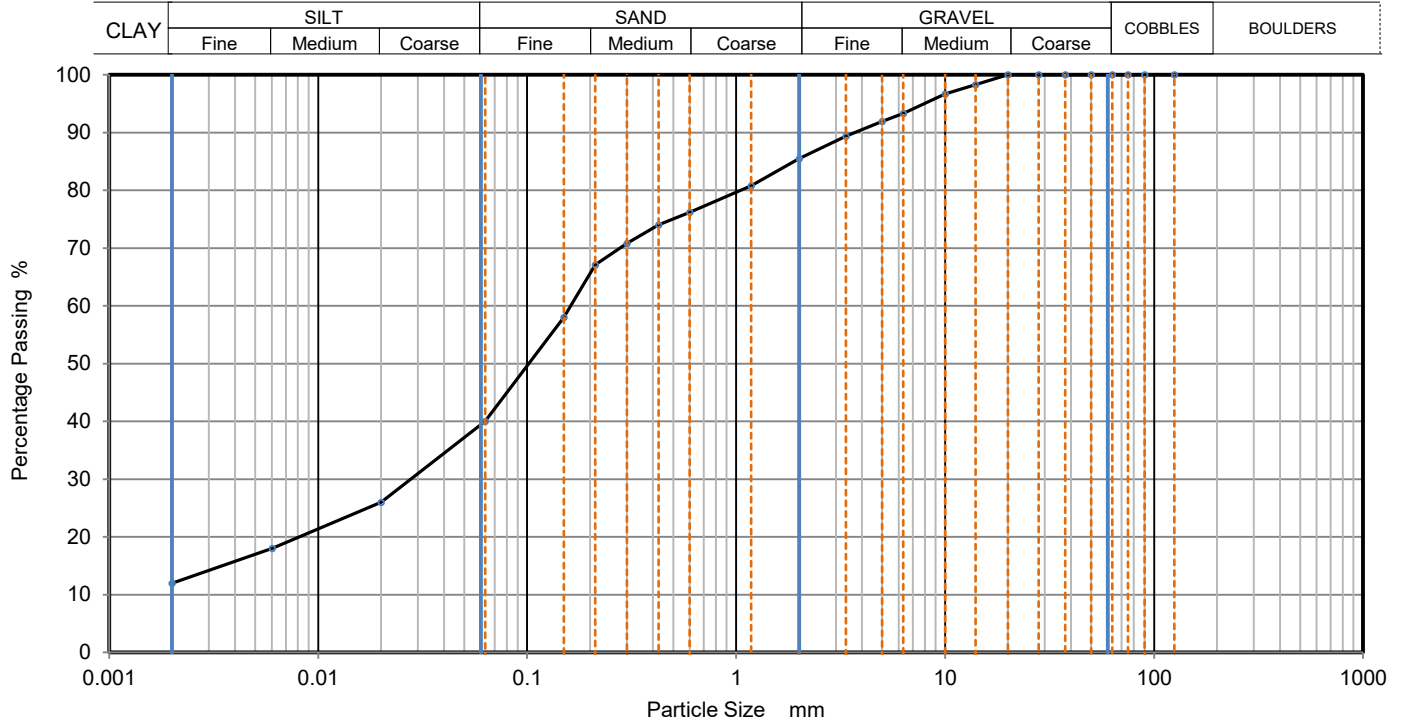
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PARTICLE SIZE DISTRIBUTION

Job Ref	25366
Borehole/Pit No.	BH2
Sample No.	8
Depth Top	2.50 m
Depth Base	2.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Project started	23/10/2018
Date tested	31/10/2018

Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldred Geotechnics Ltd
Soil Description	Medium strength grey, brown and orangish brown mottled slightly gravelly sandy silty CLAY (gravel is fm and rounded to sub-angular)		



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	26
90	100	0.0060	18
75	100	0.0020	12
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	98		
10	97		
6.3	93		
5	92		
3.35	89		
2	86		
1.18	81		
0.6	76	Particle density (assumed) 2.70 Mg/m ³	
0.425	74		
0.3	71		
0.212	67		
0.15	58		
0.063	40		

Dry Mass of sample, g

188

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	14.5
Sand	45.5
Silt	27.5
Clay	12.5

Grading Analysis		
D100	mm	
D60	mm	0.162
D30	mm	0.0275
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

Remarks

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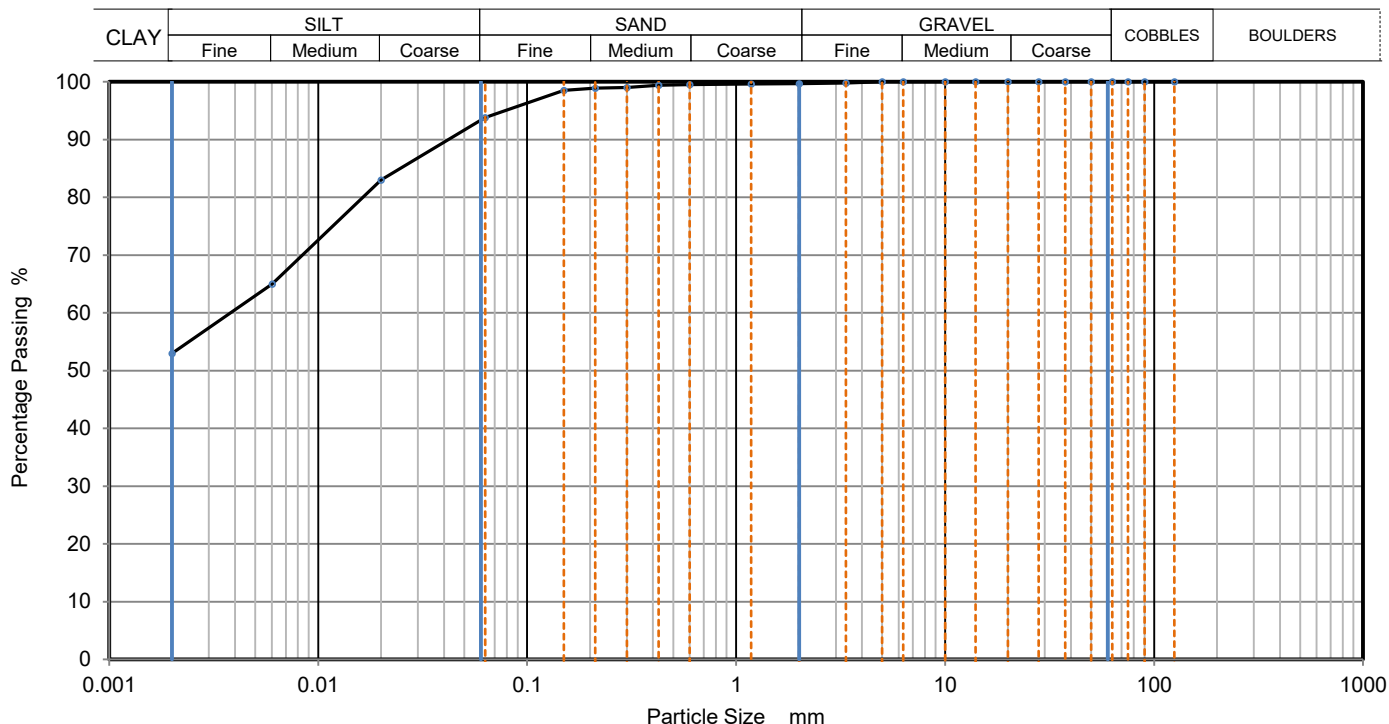
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PARTICLE SIZE DISTRIBUTION

		Job Ref	25366		
		Borehole/Pit No.	BH2		
Site Name	31 Willoughby Road, London NW3 1RT			Sample No.	11
Project No.	G1808	Client	Eldred Geotechnics Ltd	Depth Top	3.00 m
Soil Description	Brown slightly mottled grey slightly sandy silty CLAY			Depth Base	3.45 m
				Sample Type	B
				Samples received	17/08/2018
				Schedules received	22/10/2018
Test Method	BS1377:Part 2: 1990, clause 9.0			Project started	23/10/2018
				Date tested	01/11/2018



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	83
90	100	0.0060	65
75	100	0.0020	53
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	100		
0.6	100	Particle density (assumed)	
0.425	99	2.70	Mg/m ³
0.3	99		
0.212	99		
0.15	99		
0.063	94		

Dry Mass of sample, g 14

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.3
Sand	5.9
Silt	40.8
Clay	53.0

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks
Preparation and testing in accordance with BS1377 unless noted below



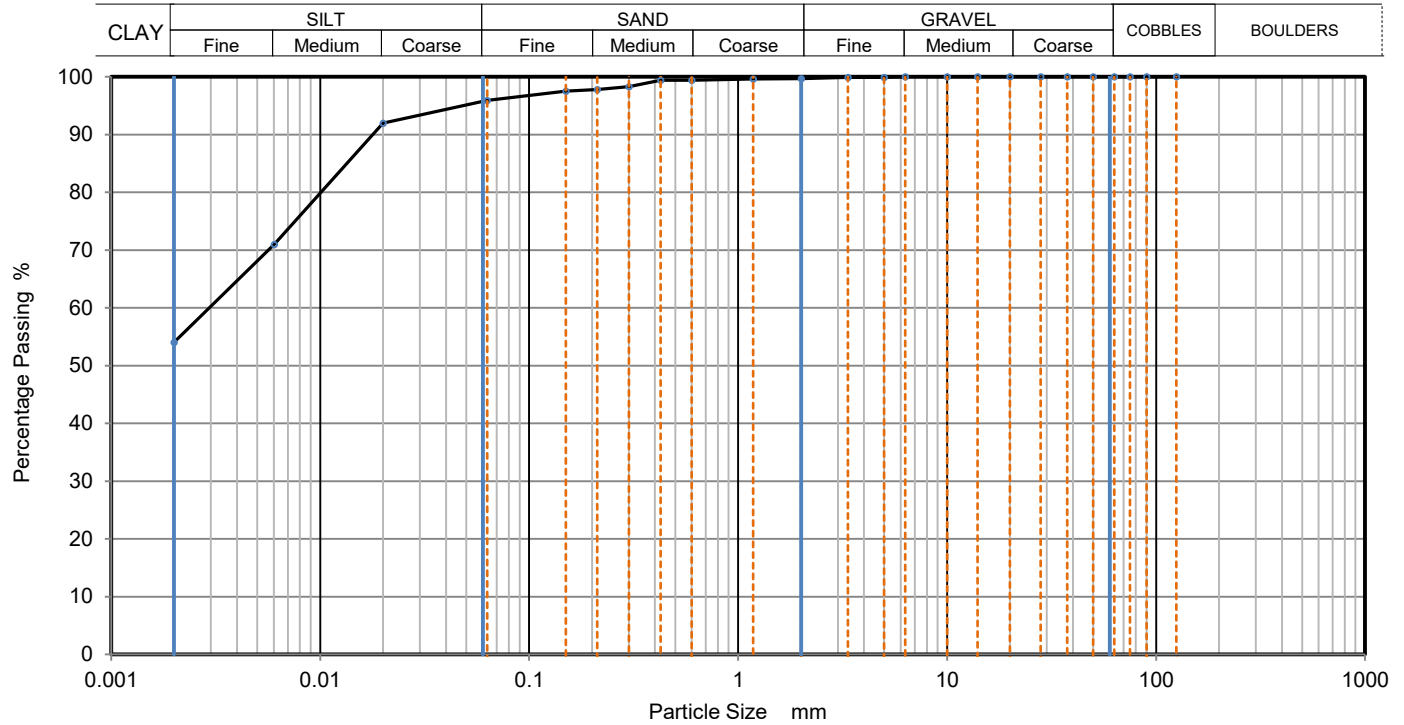
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 Date: 06/11/2018



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366		
		Borehole/Pit No.	BH2		
Site Name	31 Willoughby Road, London NW3 1RT			Sample No.	11
Project No.	G1808	Client	Eldred Geotechnics Ltd	Depth Top	3.50 m
Soil Description	High strength brown and orangish brown mottled silty CLAY with occasional pockets of fine sand and rare fine gravel			Depth Base	3.95 m
				Sample Type	U
				Samples received	17/08/2018
				Schedules received	22/10/2018
Test Method	BS1377:Part 2: 1990, clause 9.0			Project started	23/10/2018
				Date tested	31/10/2018



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	92
90	100	0.0060	71
75	100	0.0020	54
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	100		
0.6	99	Particle density (assumed) 2.70 Mg/m ³	
0.425	99		
0.3	98		
0.212	98		
0.15	98		
0.063	96		

Dry Mass of sample, g

4

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.3
Sand	3.8
Silt	41.9
Clay	54.0

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks

Preparation and testing in accordance with BS1377 unless noted below



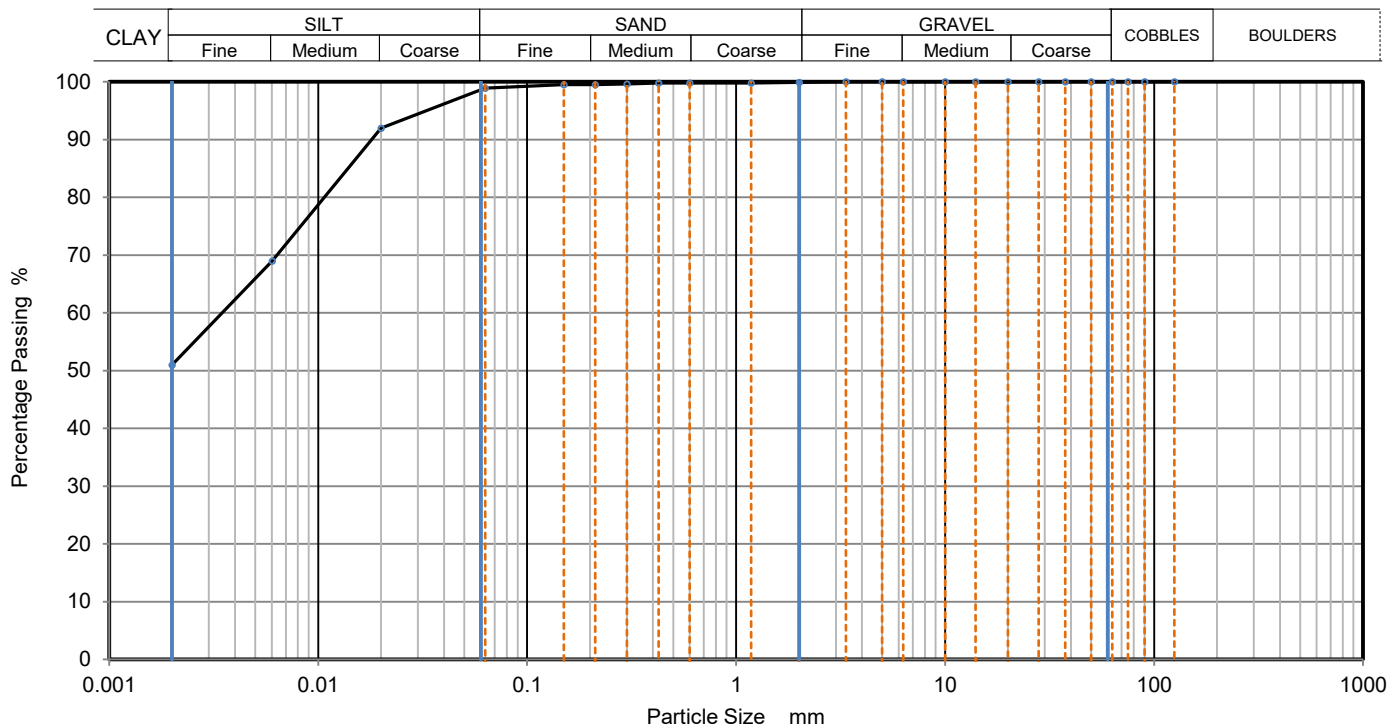
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 Initials: J.P
 Date: 06/11/2018
 MSF-5-R3



PARTICLE SIZE DISTRIBUTION

		Job Ref	25366			
		Borehole/Pit No.	BH2			
Site Name		31 Willoughby Road, London NW3 1RT		Sample No.	14	
Project No.	G1808	Client	Eldred Geotechnics Ltd		Depth Top	4.50 m
Soil Description	High strength slightly mottled orangish brown and grey silty CLAY with occasional pockets of fine sand			Depth Base	4.95 m	
				Sample Type	U	
				Samples received	17/08/2018	
				Schedules received	22/10/2018	
Test Method		BS1377:Part 2: 1990, clause 9.0		Project started	23/10/2018	
				Date tested	31/10/2018	



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	0.0200	92
90	100	0.0060	69
75	100	0.0020	51
63	100		
50	100		
37.5	100		
28	100		
20	100		
14	100		
10	100		
6.3	100		
5	100		
3.35	100		
2	100		
1.18	100		
0.6	100	Particle density (assumed) 2.70 Mg/m ³	
0.425	100		
0.3	100		
0.212	100		
0.15	100		
0.063	99		

Dry Mass of sample, g 2

Sample Proportions	% dry mass
Very coarse	0.0
Gravel	0.1
Sand	1.0
Silt	47.8
Clay	51.1

Grading Analysis	
D100	mm
D60	mm
D30	mm
D10	mm
Uniformity Coefficient	
Curvature Coefficient	

Remarks
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Unconsolidated Undrained Triaxial Compression tests without measurement of pore pressure Summary of Results

Tests carried out in accordance with BS1377:Part 7 : 1990 clause 8 or 9 as appropriate to test

Job No. 25366	Project Name 31 Willoughby Road, London NW3 1RT	Programme	
		Samples received	17/08/2018
		Schedule received	22/10/2018
Project No. G1808	Client Eldreds	Project started	23/10/2018
		Testing Started	29/10/2018

Hole No.	Sample				Soil Description	Test Type	Density		w	Length	Diameter	σ_3	At failure				Remarks
	Ref	Top m	Base m	Type			bulk Mg/m ³	dry					Axial strain %	$\sigma_1 - \sigma_3$ kPa	cu kPa	Mode	
BH1	5	2.00	2.45	U	High strength brown mottled orangish brown clayey gravelly silty SAND with rare fine brick fragments (gravel is fmc and rounded to sub-angular)	UU	1.83	1.48	23	198	102	50	5.6	170	85	B	
BH1	10	4.00	4.45	U	Medium strength brown slightly mottled grey silty CLAY with rare pockets of orange fine sand / silt and traces of selenite crystals and rootlets	UU	1.93	1.45	33	198	102	70	7.1	140	70	B	
BH1	12	5.00	5.45	U	High strength brown silty CLAY with rare pockets of orange fine sand / silt	UU	1.88	1.42	33	198	102	100	7.6	202	101	B	
BH1	14	6.00	6.45	U	High strength dark brown slightly mottled orangish brown silty CLAY with occasional pockets of fine sand / silt	UU	1.94	1.50	29	198	102	120	5.1	255	127	B	
BH1	16	7.00	7.45	U	High strength dark grey silty CLAY with rare pockets of fine sand	UU	1.99	1.52	30	198	102	140	7.6	204	102	B	
BH1	18	8.00	8.45	U	High strength dark grey silty CLAY	UU	2.03	1.57	29	198	102	160	11	190	95	C	
BH1	23	10.00	10.45	U	Very high strength dark grey silty CLAY with occasional pockets of fine sand	UU	2.03	1.59	28	198	102	200	5.1	360	180	B	
BH1	29	12.00	12.45	U	Very high strength dark grey silty CLAY with occasional pockets of fine sand	UU	2.02	1.63	24	198	102	240	2.5	340	170	B	Disturbed
BH1	35	14.00	14.45	U	Very high strength dark grey silty CLAY with frequent pockets of fine sand and rare decayed shell deposits	UU	2.11	1.69	25	198	102	280	19	335	168	C	
BH2	4	1.50	1.95	U	High strength brown and orangish brown mottled slightly gravelly sandy silty CLAY with rare brick fragments and traces of carbonaceous deposits (gravel is fm and sub-angular)	UU	2.05	1.62	27	198	102	50	17	172	86	C	
BH2	8	2.50	2.95	U	Medium strength grey, brown and orangish brown mottled slightly gravelly sandy silty CLAY (gravel is fm and rounded to sub-angular)	UU	2.04	1.66	23	198	102	50	20	83	41	P	
BH2	11	3.50	3.95	U	High strength brown and orangish brown mottled silty CLAY with occasional pockets of fine sand and rare fine gravel	UU	1.99	1.50	33	198	102	60	6.1	175	87	B	
BH2	14	4.50	4.95	U	High strength slightly mottled orangish brown and grey silty CLAY with occasional pockets of fine sand	UU	2.01	1.51	33	198	102	75	8.1	171	86	C	

Legend UU - single stage test (single and multiple specimens) σ_3 Cell pressure Mode of failure ; B - Brittle
 UUM - Multistage test on a single specimen $\sigma_1 - \sigma_3$ Maximum corrected deviator stress P - Plastic
 suffix R - remoulded or recompacted cu Undrained shear strength, $\frac{1}{2}(\sigma_1 - \sigma_3)$ C - Compound



Test Report by K4 SOILS LABORATORY
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Checked and Approved

Initials: J.P

Date: 15/11/2018



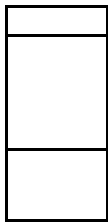
**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	5
Depth Top	2.00 m
Depth Base	2.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength brown mottled orangish brown clayey gravelly silty SAND with rare fine brick fragments (gravel is fmc and rounded to sub-angular)		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

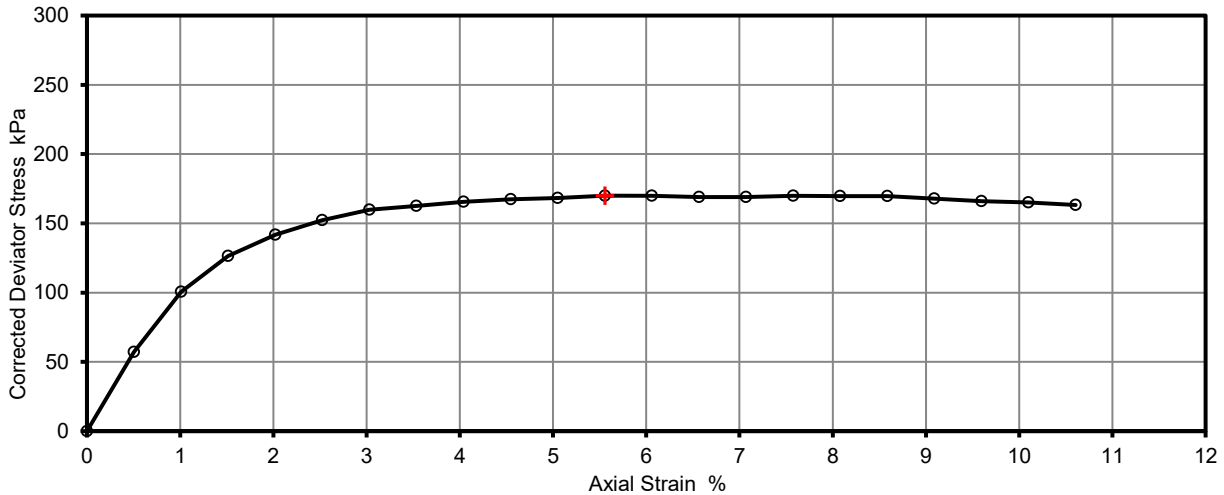
Remarks

Position within sample

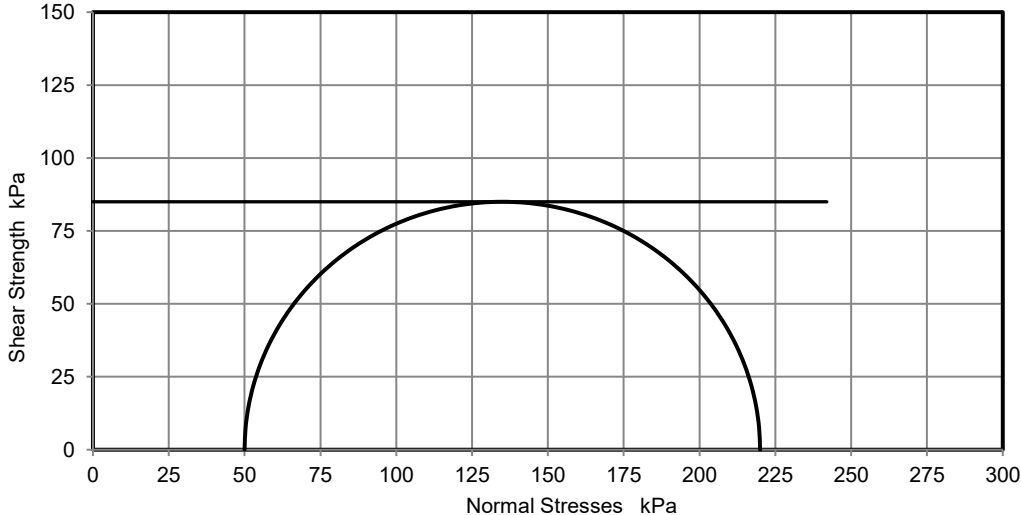


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	1.83	Mg/m ³
Moisture Content	23	%
Dry Density	1.48	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	50	kPa
Axial Strain	5.6	%
Deviator Stress, (σ ₁ - σ ₃) _f	170	kPa
Undrained Shear Strength, c _u	85	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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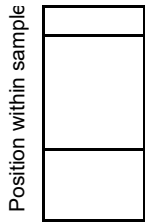


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	10
Depth Top	4.00 m
Depth Base	4.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	28/10/2018

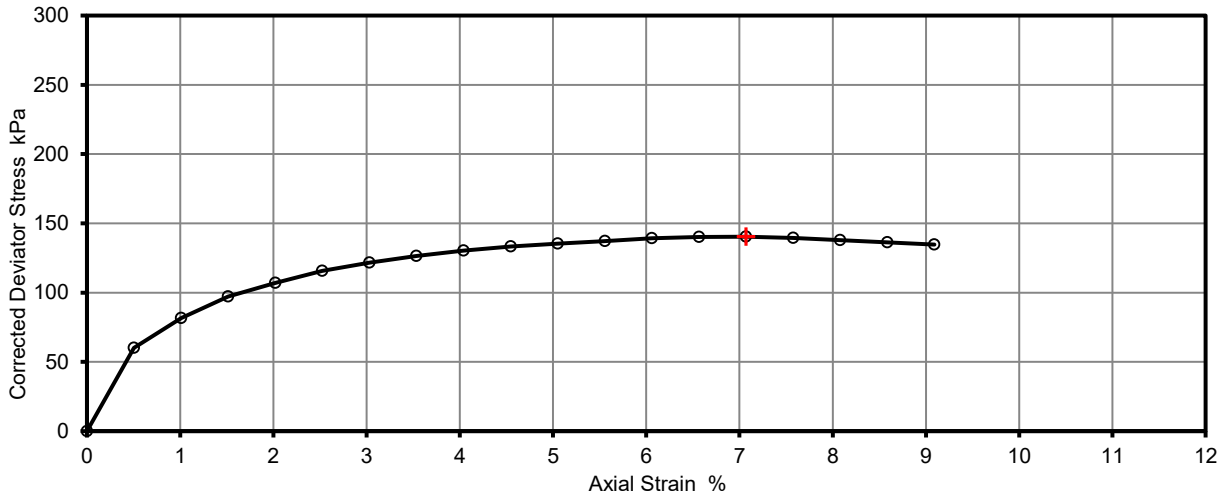
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	Medium strength brown slightly mottled grey silty CLAY with rare pockets of orange fine sand / silt and traces of selenite crystals and rootlets		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

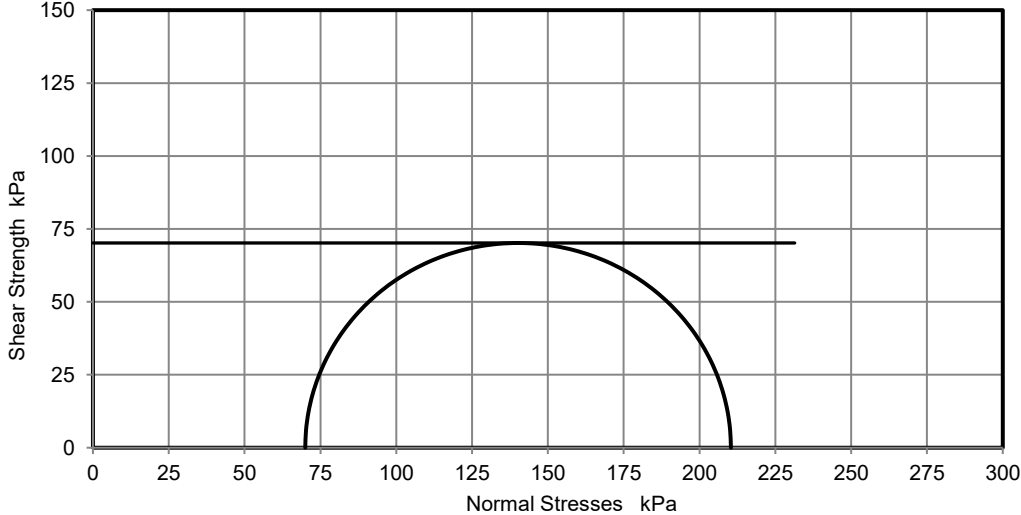


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	1.93	Mg/m ³
Moisture Content	33	%
Dry Density	1.45	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	70	kPa
Axial Strain	7.1	%
Deviator Stress, (σ ₁ - σ ₃) _f	140	kPa
Undrained Shear Strength, c _u	70	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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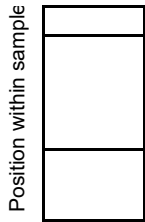


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	12
Depth Top	5.00 m
Depth Base	5.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

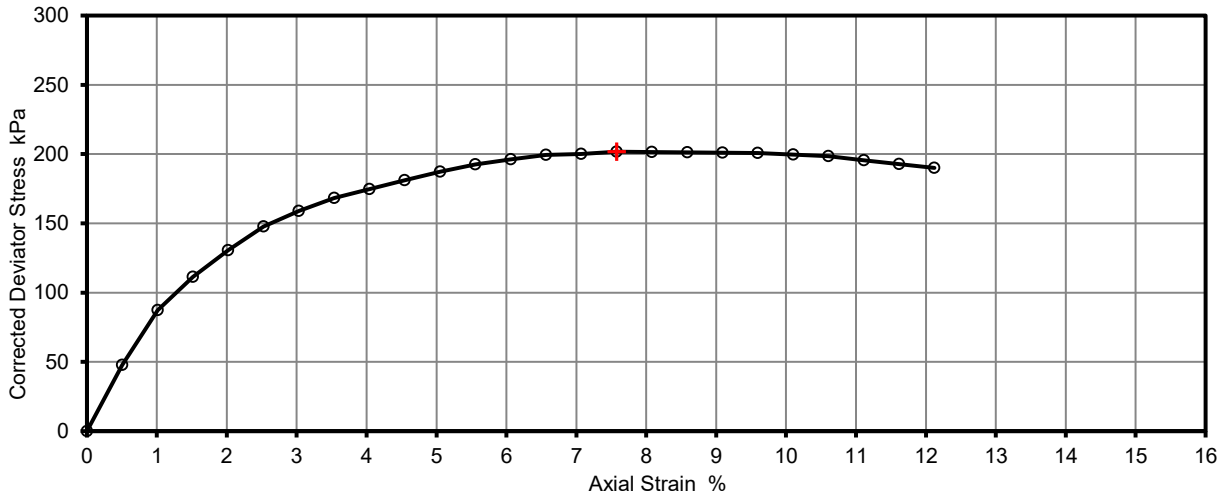
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength brown silty CLAY with rare pockets of orange fine sand / silt		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

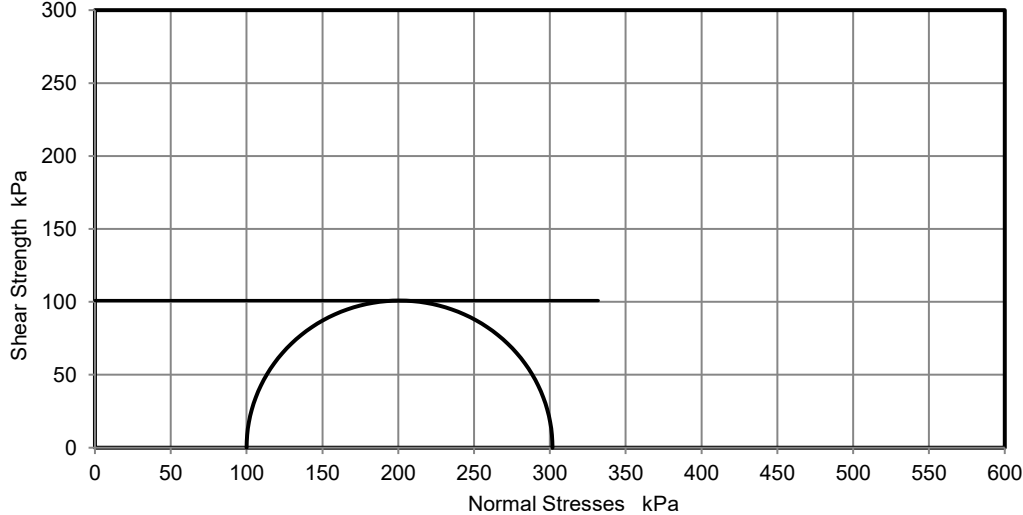


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	1.88	Mg/m ³
Moisture Content	33	%
Dry Density	1.42	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	100	kPa
Axial Strain	7.6	%
Deviator Stress, (σ ₁ - σ ₃) _f	202	kPa
Undrained Shear Strength, c _u	101	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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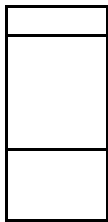
**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	14
Depth Top	6.00 m
Depth Base	6.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength dark brown slightly mottled orangish brown silty CLAY with occasional pockets of fine sand / silt		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

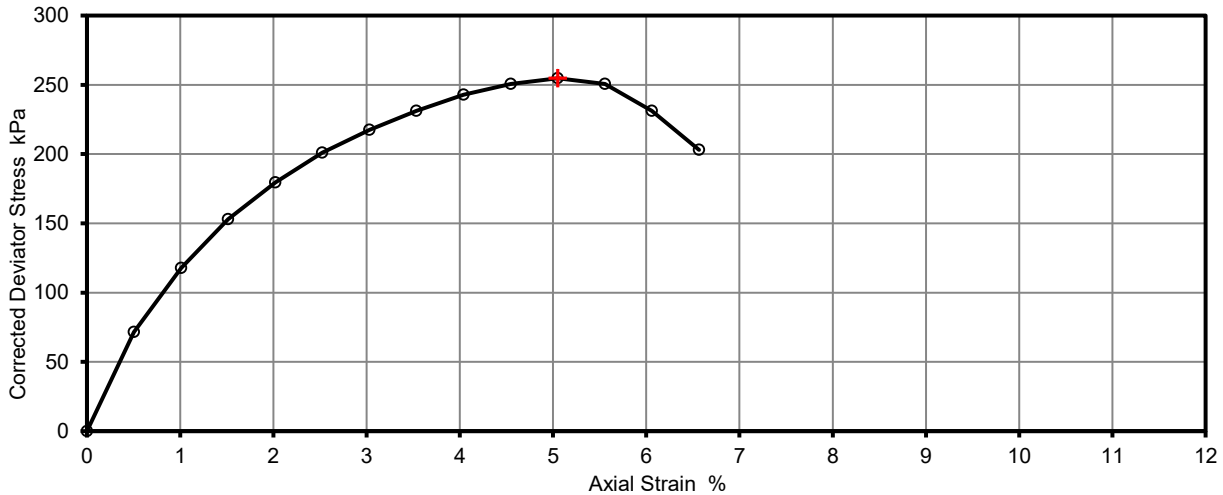
Remarks

Position within sample

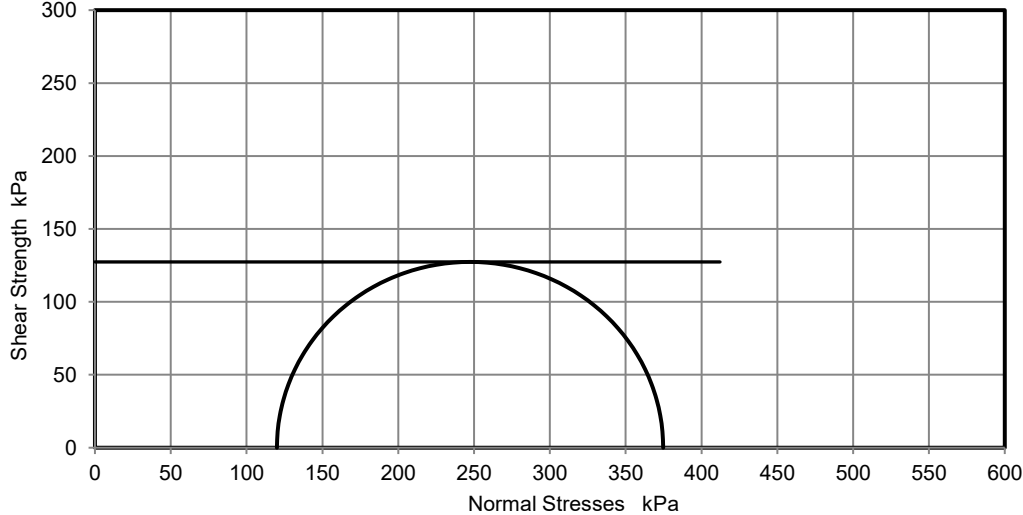


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	1.94	Mg/m ³
Moisture Content	29	%
Dry Density	1.50	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	120	kPa
Axial Strain	5.1	%
Deviator Stress, (σ ₁ - σ ₃) _f	255	kPa
Undrained Shear Strength, c _u	127	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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Email: James@k4soils.com

Checked and Approved

Initials: J.P

Date 15/11/2018

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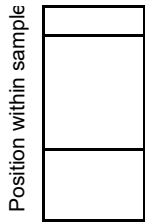


Unconsolidated Undrained Triaxial Compression Test without measurement of pore pressure - single specimen

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	16
Depth Top	7.00 m
Depth Base	7.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

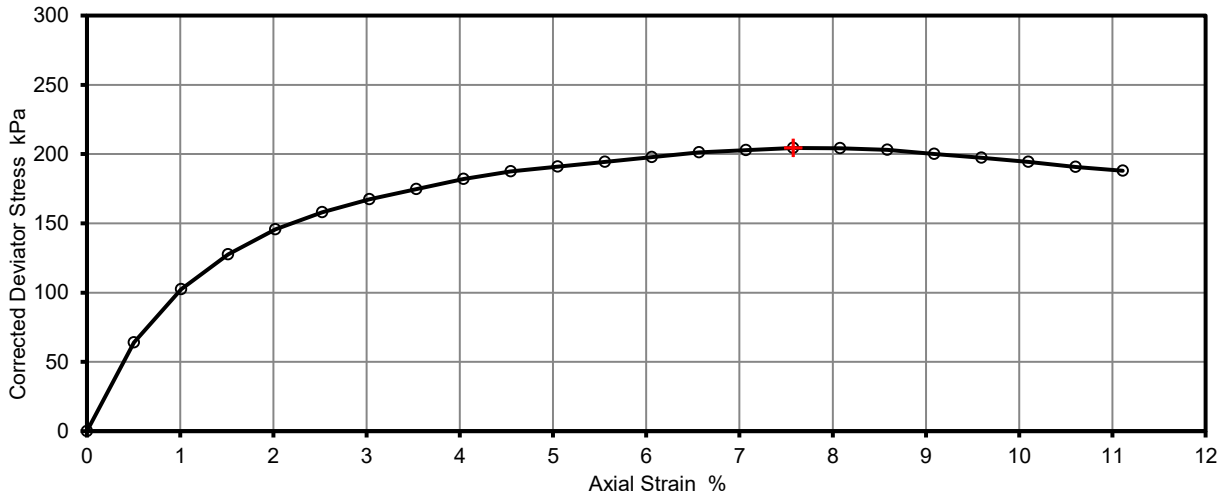
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength dark grey silty CLAY with rare pockets of fine sand		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

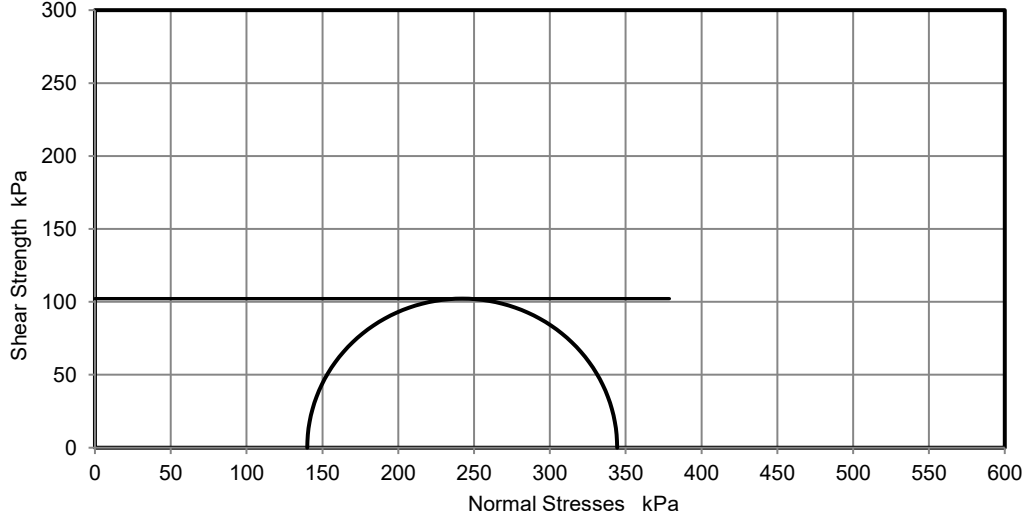


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	1.99	Mg/m3
Moisture Content	30	%
Dry Density	1.52	Mg/m3
Rate of Strain	2.0	%/min
Cell Pressure	140	kPa
Axial Strain	7.6	%
Deviator Stress, (σ ₁ - σ ₃) _f	204	kPa
Undrained Shear Strength, c _u	102	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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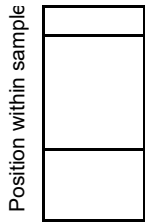


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	18
Depth Top	8.00 m
Depth Base	8.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

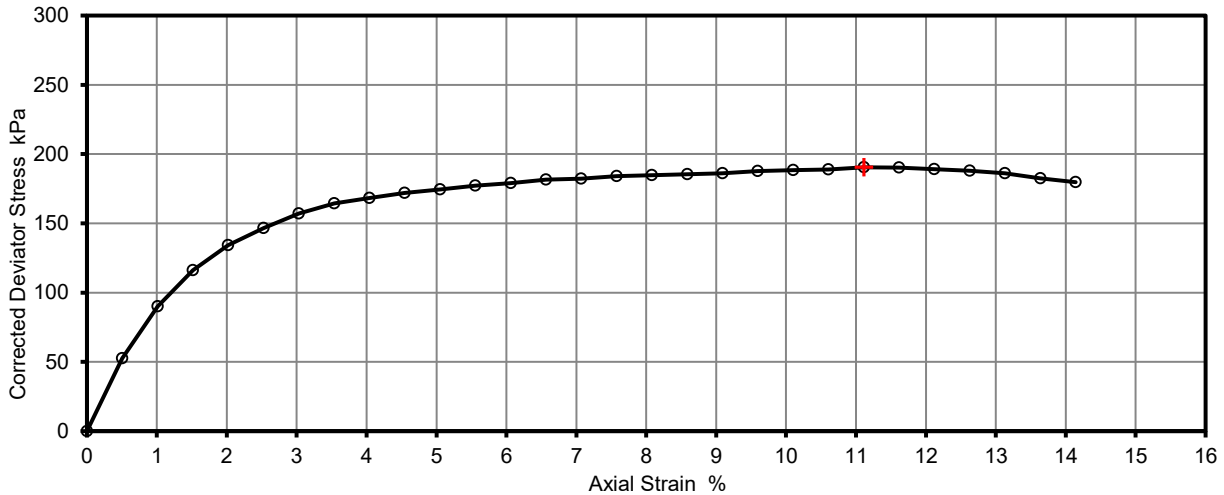
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength dark grey silty CLAY		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

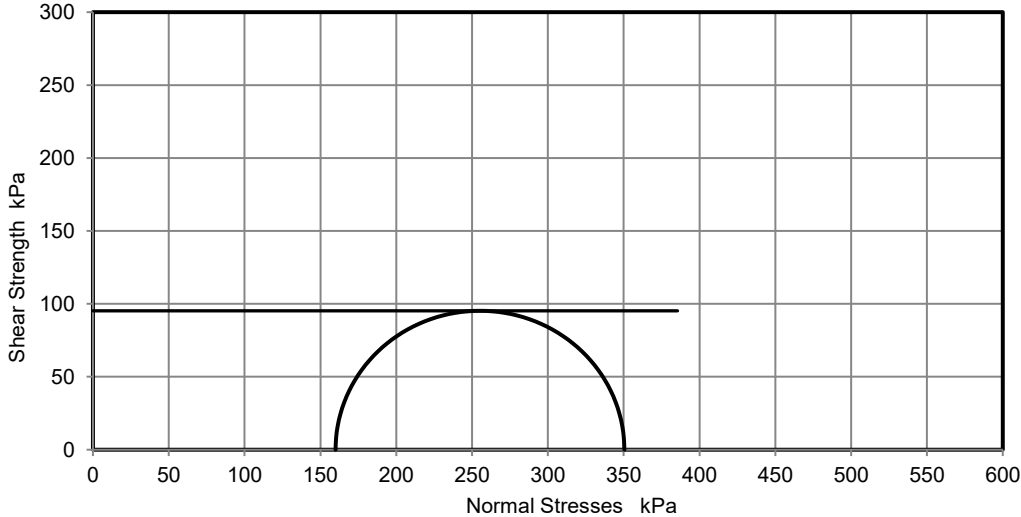


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.03	Mg/m ³
Moisture Content	29	%
Dry Density	1.57	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	160	kPa
Axial Strain	11	%
Deviator Stress, (σ ₁ - σ ₃) _f	190	kPa
Undrained Shear Strength, c _u	95	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Compound	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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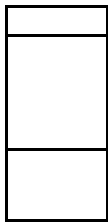
**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	23
Depth Top	10.00 m
Depth Base	10.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	13/11/2018

Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	Very high strength dark grey silty CLAY with occasional pockets of fine sand		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

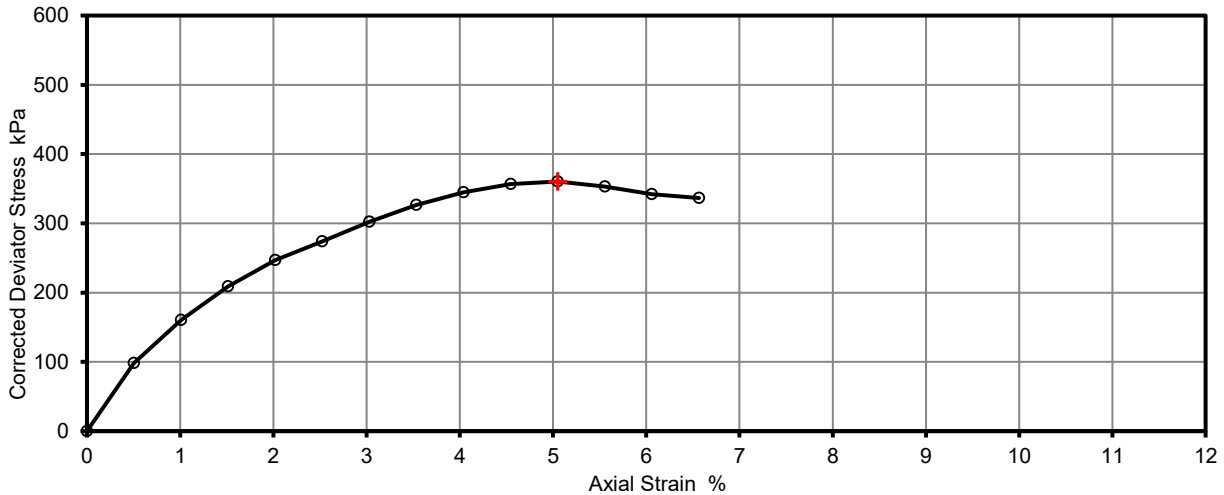
Remarks

Position within sample

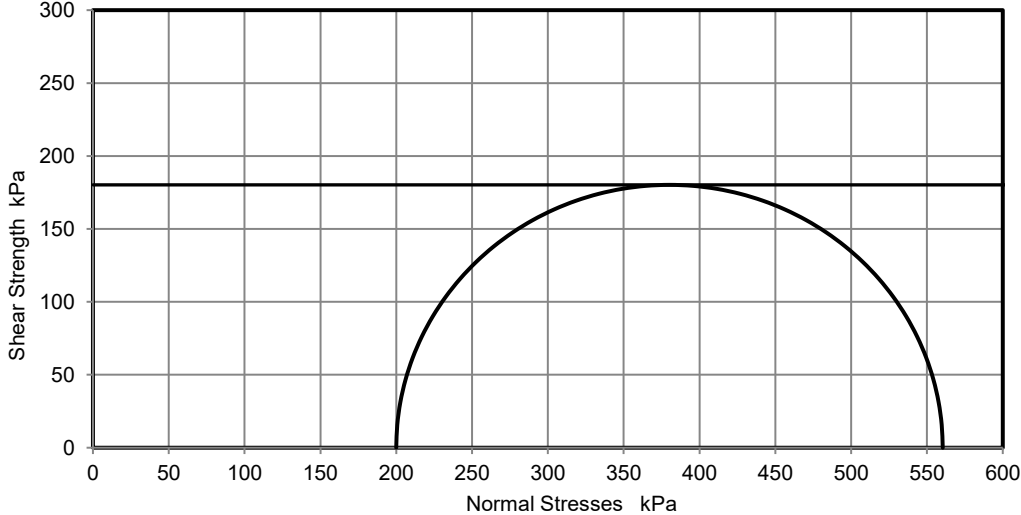


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.03	Mg/m ³
Moisture Content	28	%
Dry Density	1.59	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	200	kPa
Axial Strain	5.1	%
Deviator Stress, (σ ₁ - σ ₃) _f	360	kPa
Undrained Shear Strength, c _u	180	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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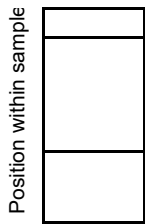
**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	29
Depth Top	12.00 m
Depth Base	12.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	13/11/2018

Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	Very high strength dark grey silty CLAY with occasional pockets of fine sand		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

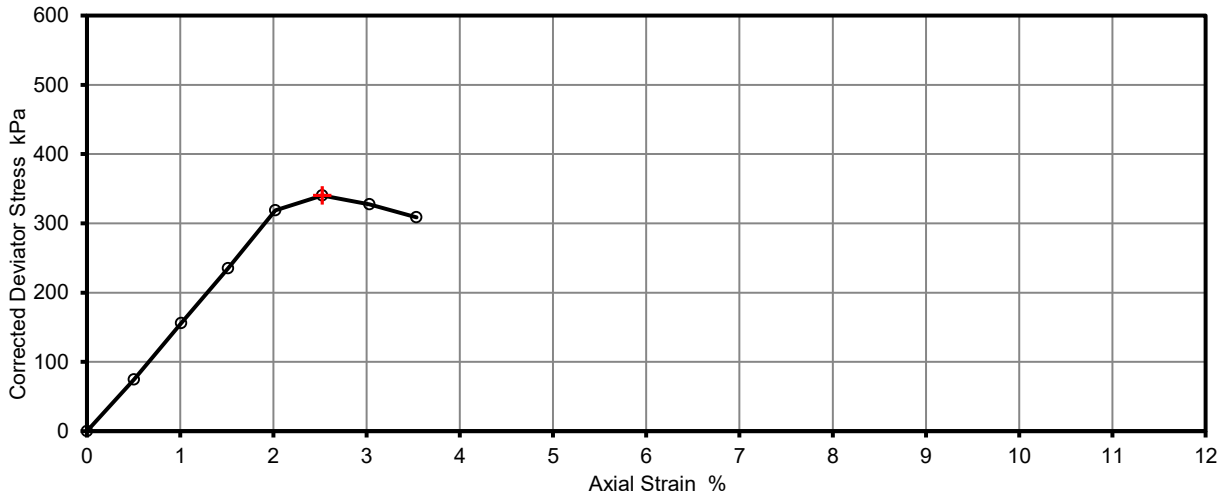
Remarks

Disturbed

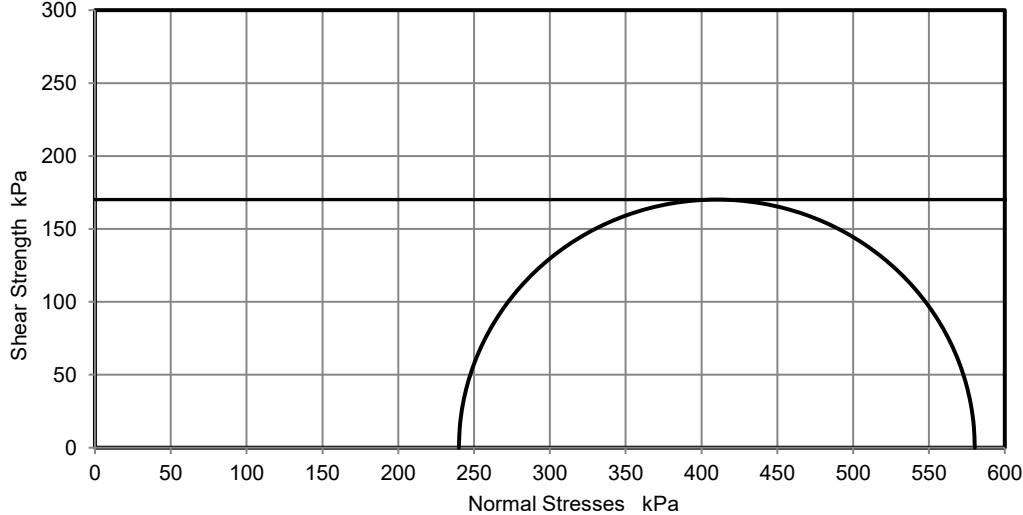


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.02	Mg/m ³
Moisture Content	24	%
Dry Density	1.63	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	240	kPa
Axial Strain	2.5	%
Deviator Stress, (σ ₁ - σ ₃) _f	340	kPa
Undrained Shear Strength, c _u	170	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



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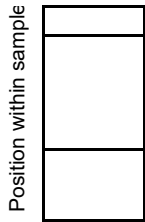


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH1
Sample No.	35
Depth Top	14.00 m
Depth Base	14.45 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	13/11/2018

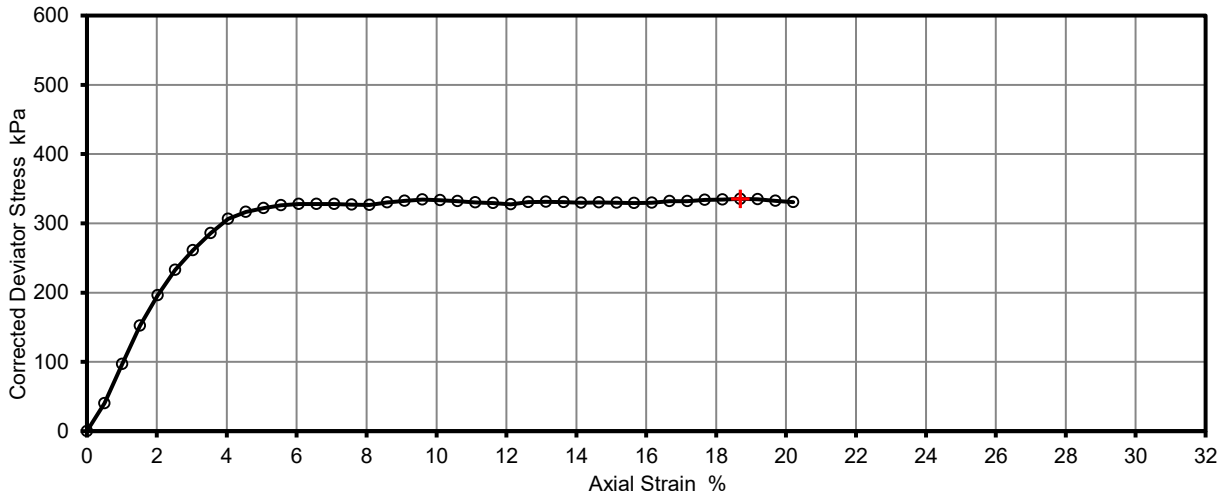
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	Very high strength dark grey silty CLAY with frequent pockets of fine sand and rare decayed shell deposits		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

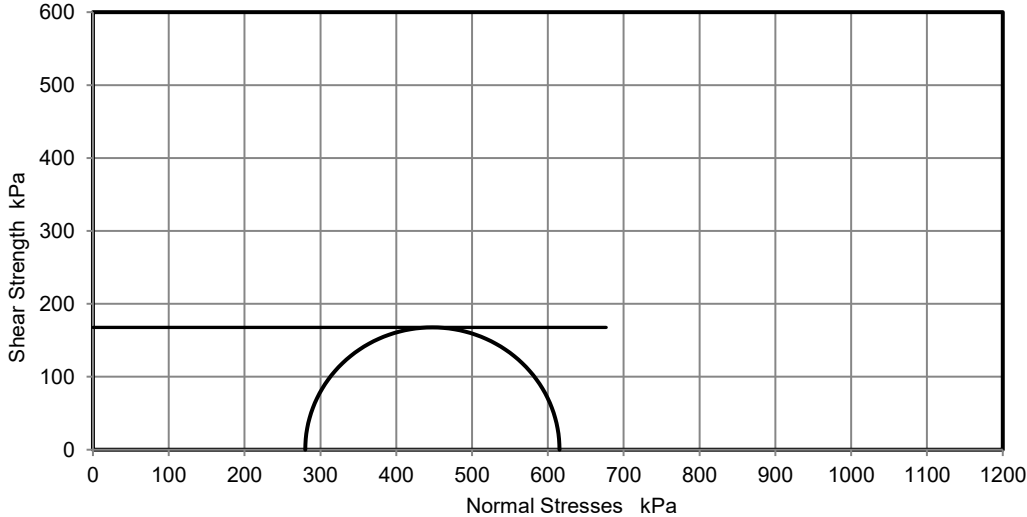


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.11	Mg/m3
Moisture Content	25	%
Dry Density	1.69	Mg/m3
Rate of Strain	2.0	%/min
Cell Pressure	280	kPa
Axial Strain	19	%
Deviator Stress, ($\sigma_1 - \sigma_3$)f	335	kPa
Undrained Shear Strength, c_u	168	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)$ f
Mode of Failure	Compound	

Deviator Stress v Axial Strain



Mohr Circles



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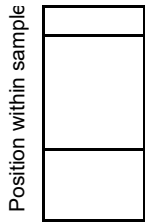


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH2
Sample No.	4
Depth Top	1.50 m
Depth Base	1.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

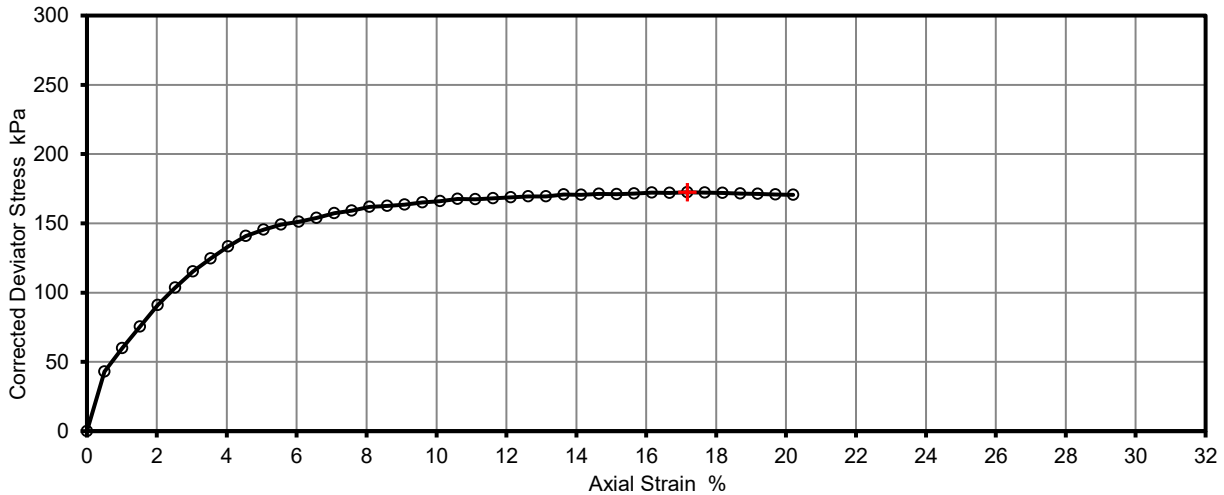
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength brown and orangish brown mottled slightly gravelly sandy silty CLAY with rare brick fragments and traces of carbonaceous deposits (gravel is fm and sub-angular)		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

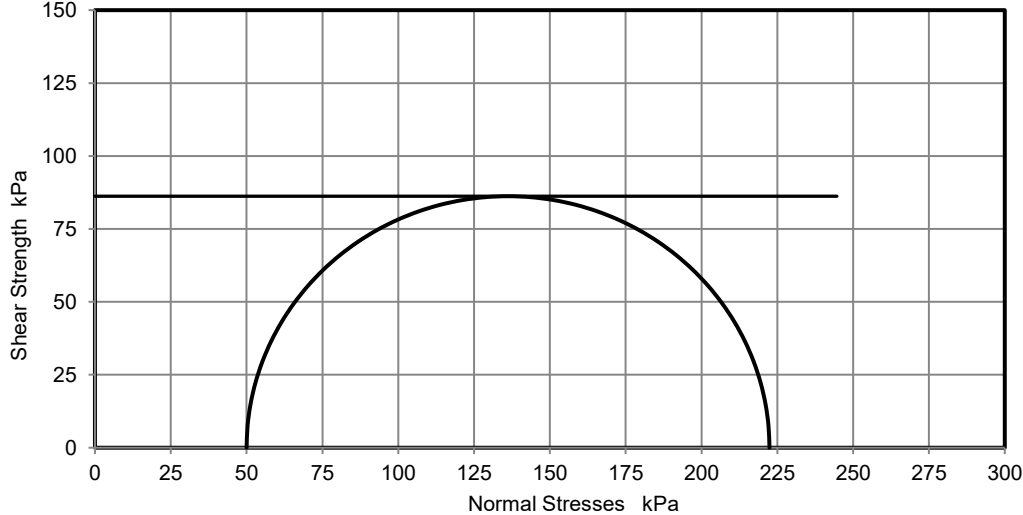


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.05	Mg/m3
Moisture Content	27	%
Dry Density	1.62	Mg/m3
Rate of Strain	2.0	%/min
Cell Pressure	50	kPa
Axial Strain	17	%
Deviator Stress, ($\sigma_1 - \sigma_3$)f	172	kPa
Undrained Shear Strength, cu	86	kPa $\frac{1}{2}(\sigma_1 - \sigma_3)$ f
Mode of Failure	Compound	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

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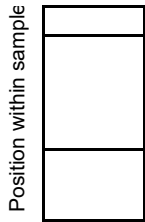


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH2
Sample No.	8
Depth Top	2.50 m
Depth Base	2.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

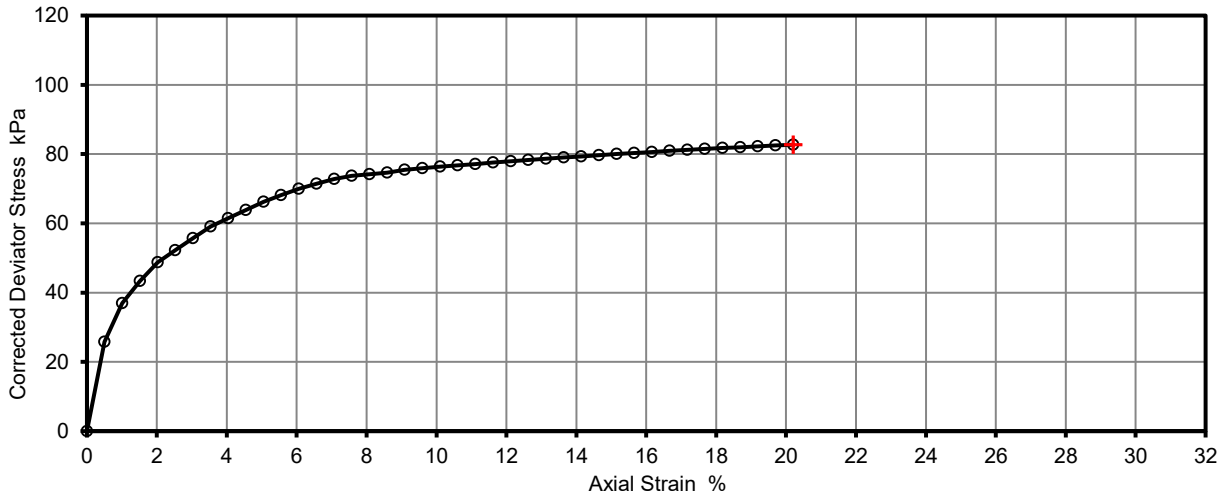
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	Medium strength grey, brown and orangish brown mottled slightly gravelly sandy silty CLAY (gravel is fm and rounded to sub-angular)		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

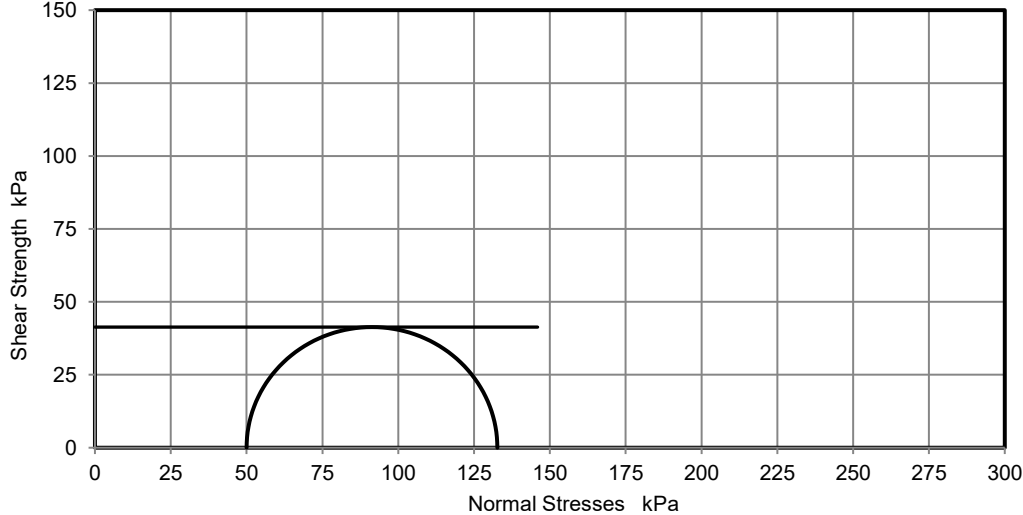


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.04	Mg/m3
Moisture Content	23	%
Dry Density	1.66	Mg/m3
Rate of Strain	2.0	%/min
Cell Pressure	50	kPa
Axial Strain	20	%
Deviator Stress, (σ ₁ - σ ₃) _f	83	kPa
Undrained Shear Strength, c _u	41	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Plastic	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.



2519

Approved Signatories: K.Phaure (Tech.Mgr) J.Phaure (Lab.Mgr)

Test Report by K4 SOILS LABORATORY
Unit 8 Olds Close Olds Approach
Watford Herts WD18 9RU
Tel: 01923 711 288
Email: James@k4soils.com

Checked and Approved
Initials: J.P
Date 15/11/2018

MSF-5 R7

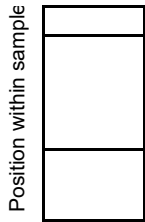


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH2
Sample No.	11
Depth Top	3.50 m
Depth Base	3.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

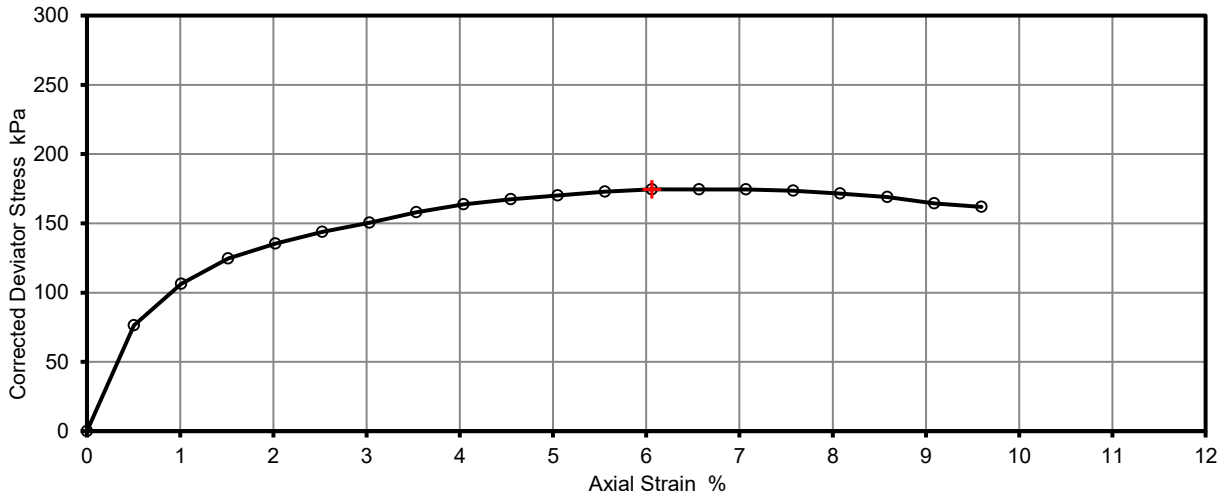
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength brown and orangish brown mottled silty CLAY with occasional pockets of fine sand and rare fine gravel		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

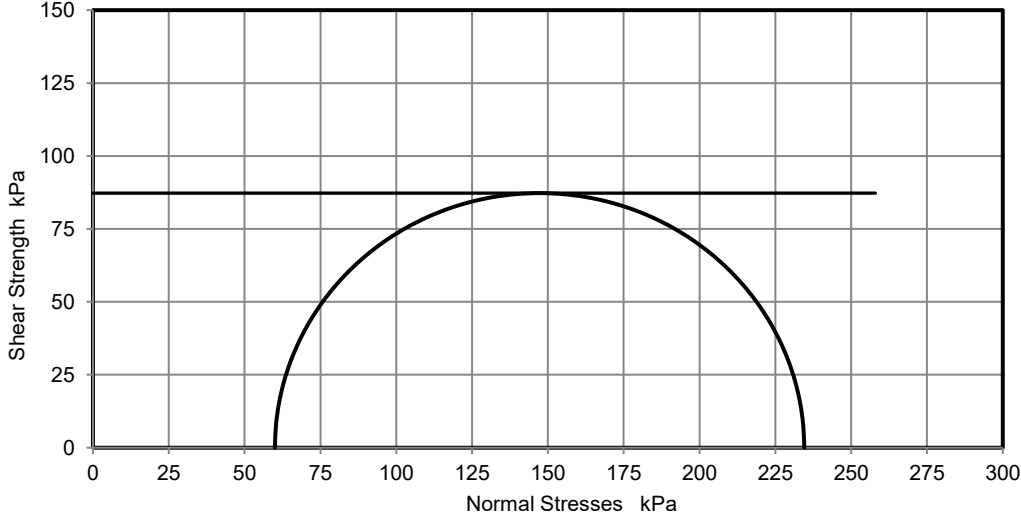


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	1.99	Mg/m ³
Moisture Content	32	%
Dry Density	1.50	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	60	kPa
Axial Strain	6.1	%
Deviator Stress, (σ ₁ - σ ₃) _f	175	kPa
Undrained Shear Strength, c _u	87	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Brittle	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.



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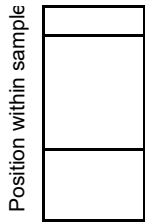


**Unconsolidated Undrained Triaxial
Compression Test without measurement of
pore pressure - single specimen**

Job Ref	25366
Borehole/Pit No.	BH2
Sample No.	14
Depth Top	4.50 m
Depth Base	4.95 m
Sample Type	U
Samples received	17/08/2018
Schedules received	22/10/2018
Date of test	29/10/2018

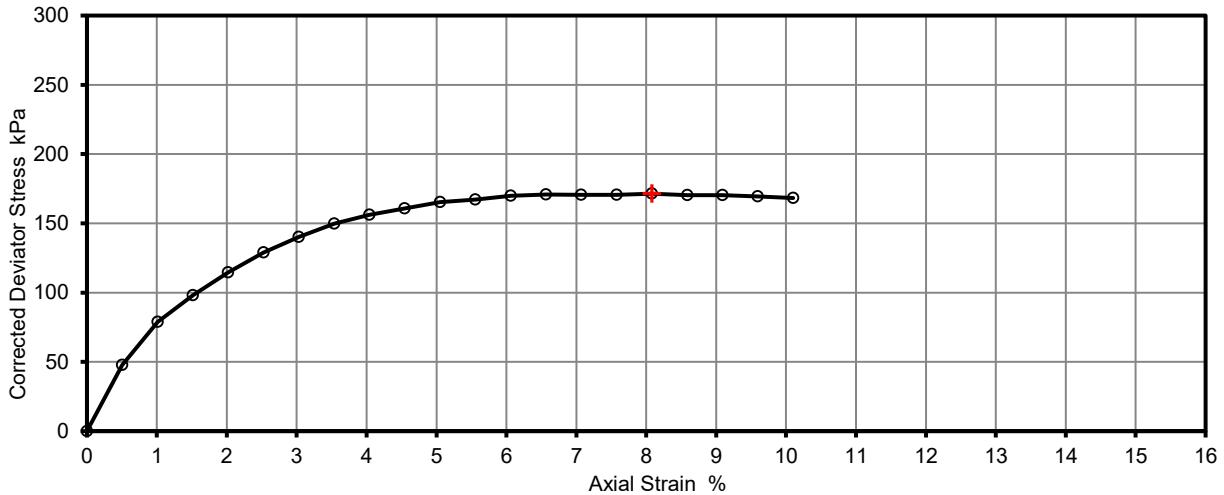
Site Name	31 Willoughby Road, London NW3 1RT		
Project No.	G1808	Client	Eldreds
Soil Description	High strength slightly mottled orangish brown and grey silty CLAY with occasional pockets of fine sand		
Test Method	BS1377 : Part 7 : 1990, clause 8, single specimen		

Remarks

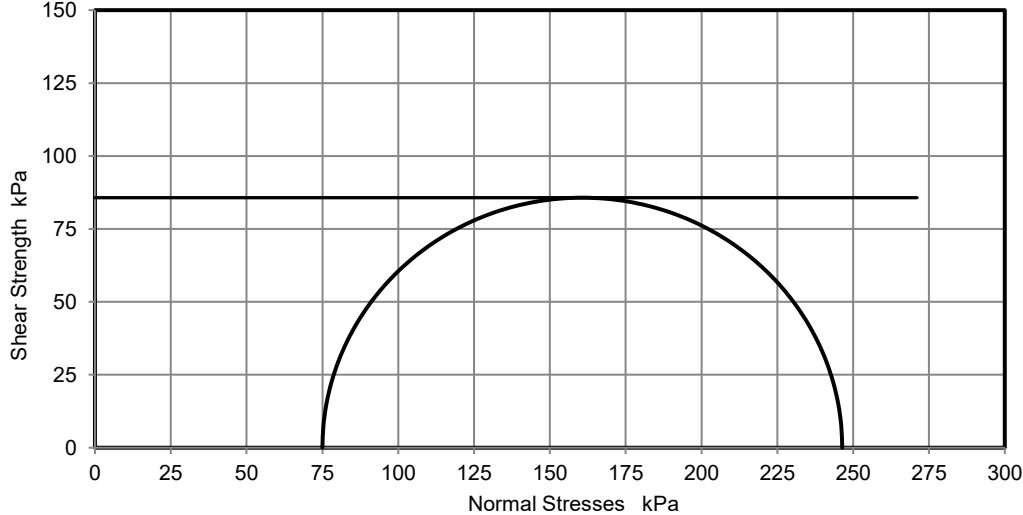


Test Number	1	
Length	198.0	mm
Diameter	102.0	mm
Bulk Density	2.01	Mg/m ³
Moisture Content	33	%
Dry Density	1.51	Mg/m ³
Rate of Strain	2.0	%/min
Cell Pressure	75	kPa
Axial Strain	8.1	%
Deviator Stress, (σ ₁ - σ ₃) _f	171	kPa
Undrained Shear Strength, c _u	86	kPa ½(σ ₁ - σ ₃) _f
Mode of Failure	Compound	

Deviator Stress v Axial Strain



Mohr Circles



Deviator stress corrected for area change and membrane effects

Mohr circles and their interpretation is not covered by BS1377. This is provided for information only.



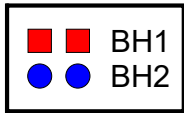
Test Report by K4 SOILS LABORATORY
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Initials: J.P
Date 15/11/2018

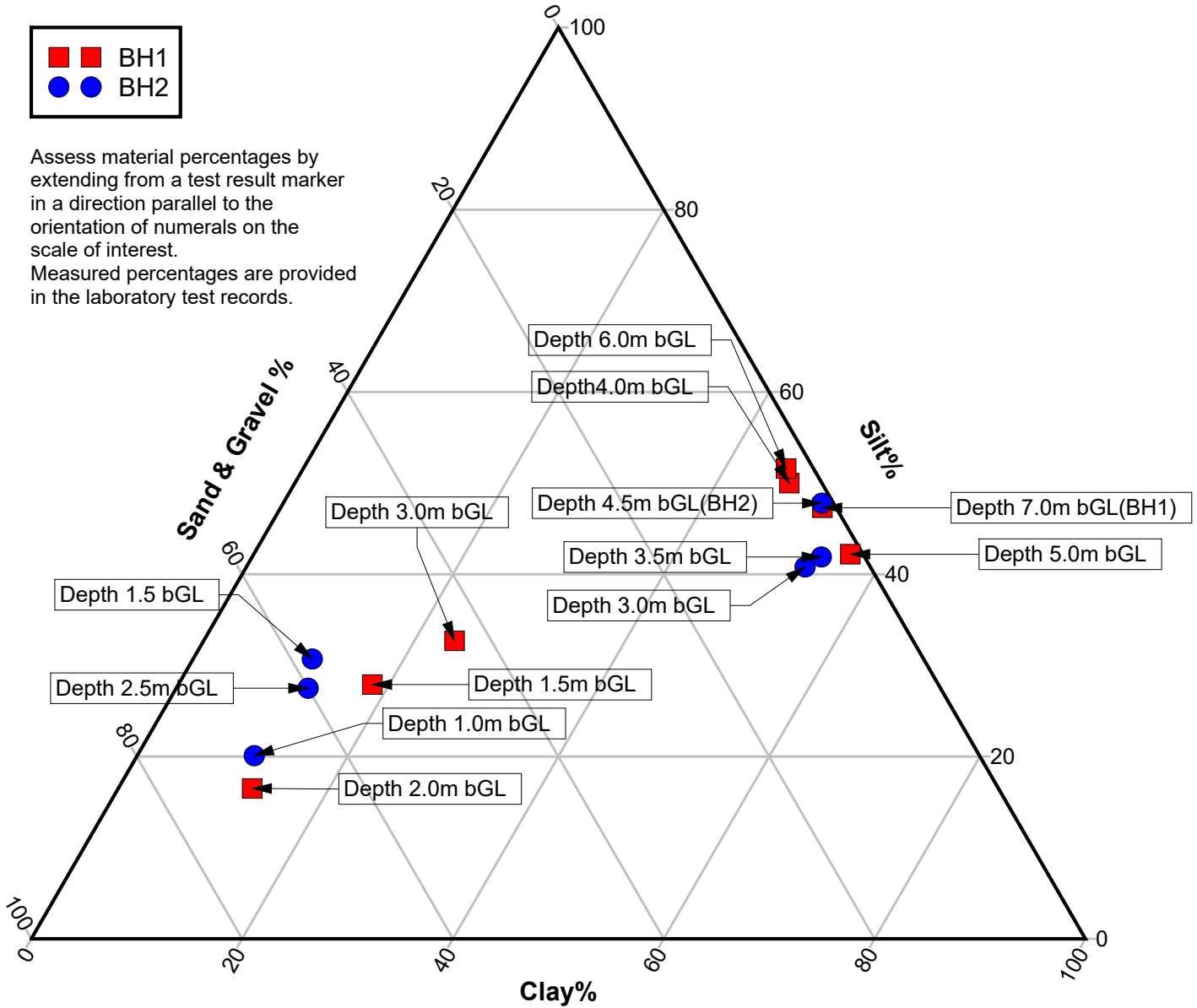
Groundwater instrumentation

Borehole	GEA BH2 (rear)	GEA BH4 (front)	EGL BH1 W1	EGL BH1 W2	EGL BH2 W1	EGL BH2 W2
Transducerr ref.	B12690	B12691	B12692	B12701	B12703	B12698
Well depth mbGL	3.75	4.00	7.79	4.00	5.10	3.16
Ground level mOD	85.50	85.40	85.50	85.50	85.50	85.50
Datum level mOD	85.50	85.40	85.61	85.70	85.65	85.64
Well base level mOD	81.75	81.40	77.71	81.50	80.40	82.34
Depth Datum to transducer m.	3.50	3.52	7.50	4.15	5.10	2.80
Transducer level mOD	82.00	81.88	78.11	81.55	80.55	82.84
Slots top level mOD	84.50	84.40	78.71	82.50	81.40	83.34
Slots btm level mOD	81.50	81.40	77.71	81.50	80.40	82.34
Filter top level mOD	84.50	84.40	78.71	82.50	81.40	83.34
Filter base level mOD	81.50	81.40	77.71	81.50	80.40	82.34
BH dia. at filter mm.	60	60	150	200	200	200
Well ID mm	30	30	50	50	50	50
Well OD mm	36	36	60	60	60	60

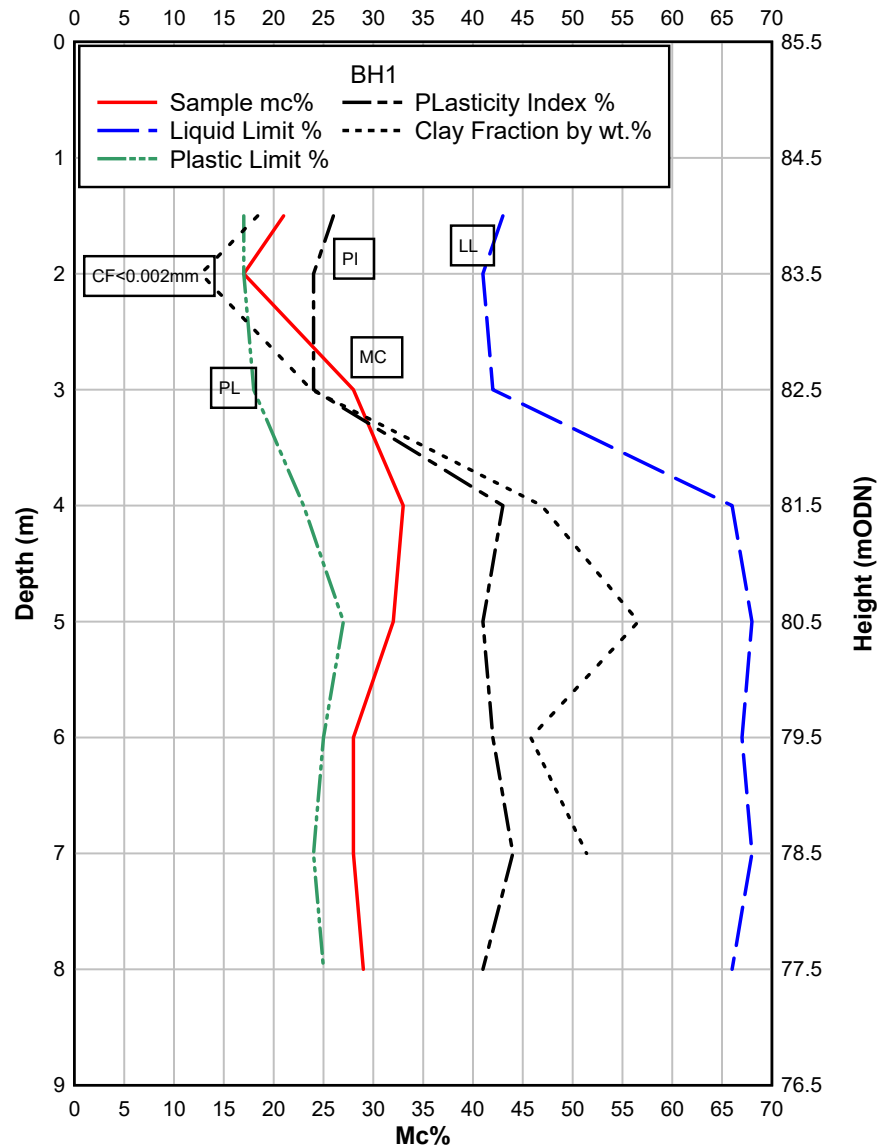
G1808 31 Willoughby Road NW3 1RT - Proposed Basement Sample Depths and Results of Particle Size Distribution Tests



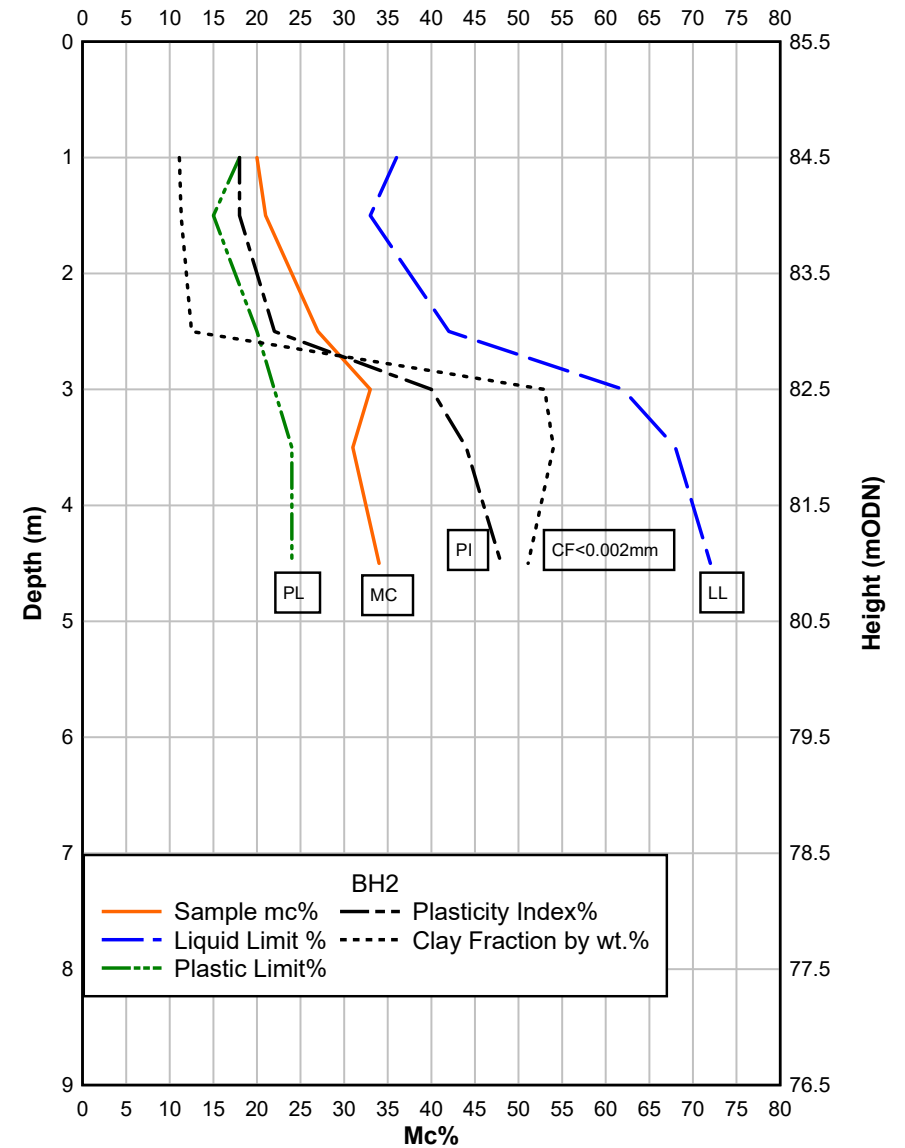
Assess material percentages by extending from a test result marker in a direction parallel to the orientation of numerals on the scale of interest. Measured percentages are provided in the laboratory test records.



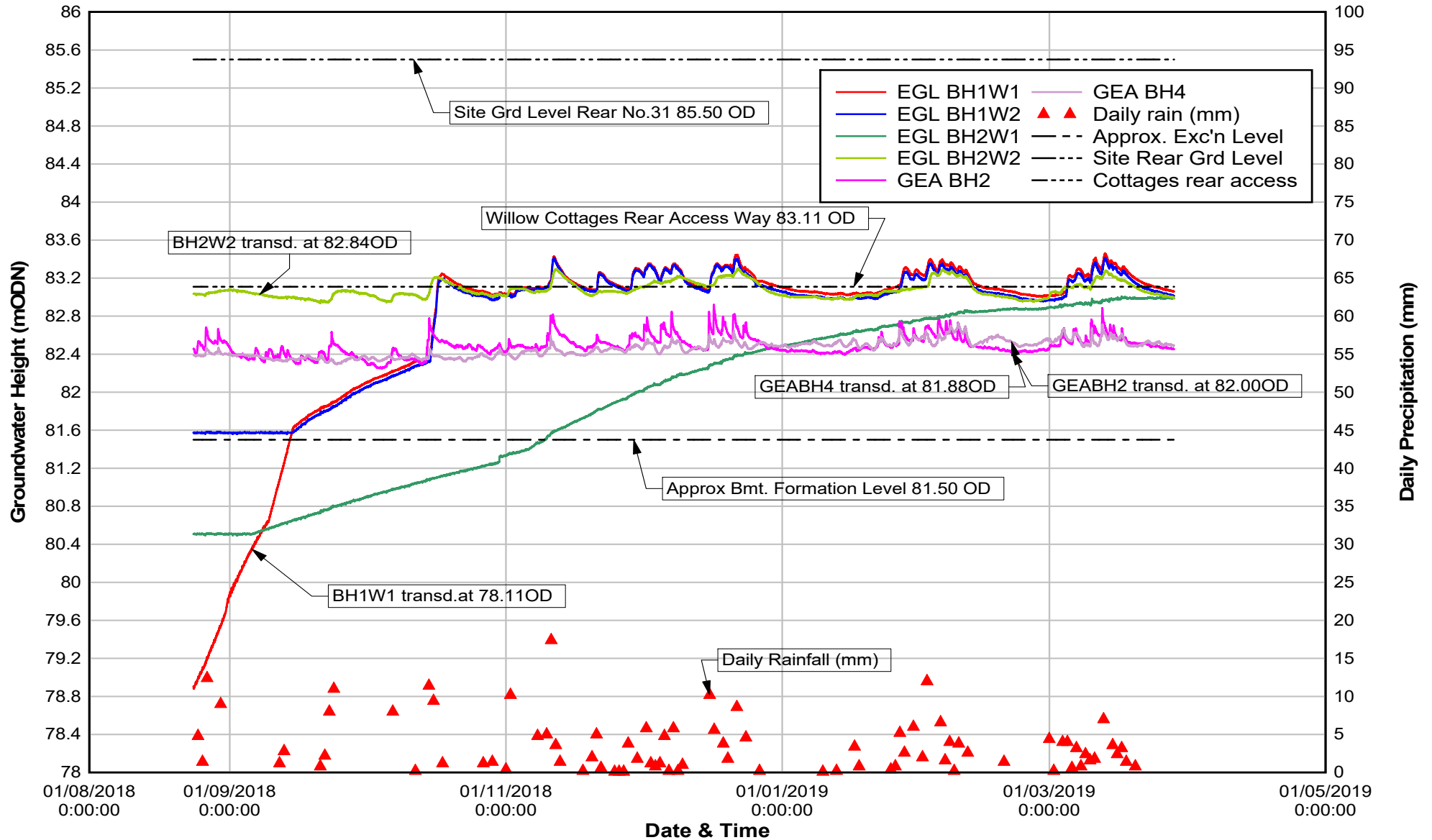
G1808 31 Willoughby Road NW3 1RT - Proposed Basement
BH1 Moisture Content & Atterberg Limits vs Depth & ODN Height



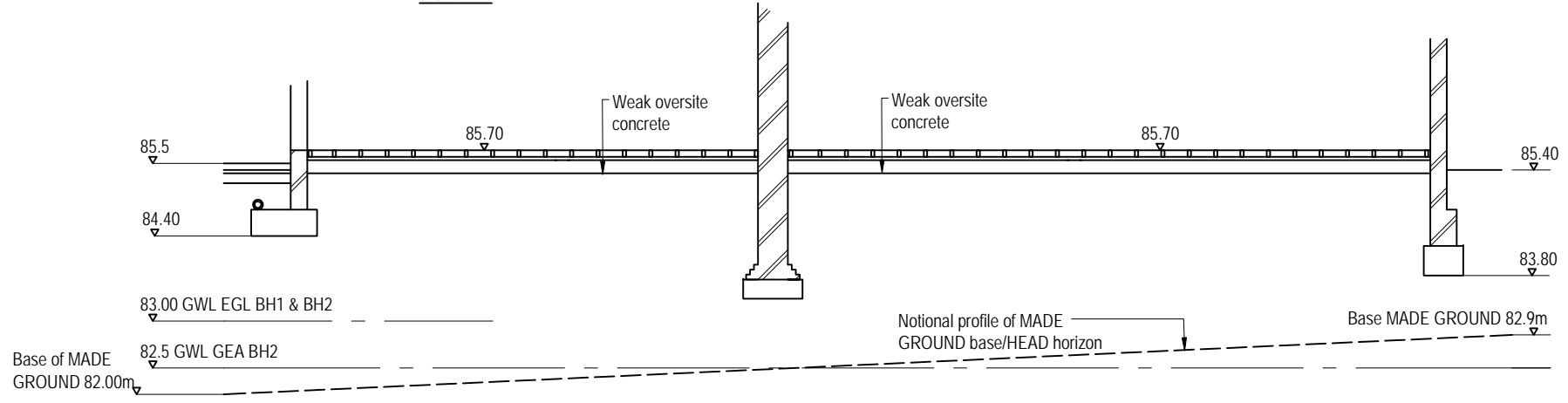
G1808 31 Willoughby Road NW3 1RT - Proposed Basement
BH2 Moisture Content & Atterberg Limits vs Depth & ODN Height



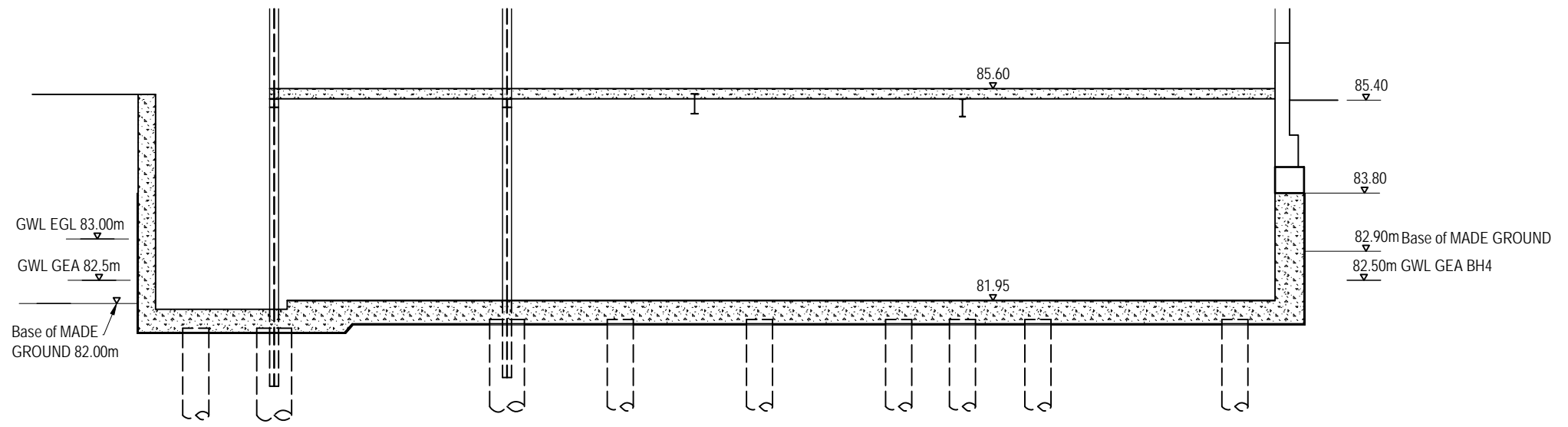
G1808 31 Willoughby Road NW3 1RT - Proposed Basement Groundwater Height (mODN) in Borehole Piezometers & Daily Rainfall



SECTION A-A



LONG SECTION EXISTING



LONG SECTION PROPOSED

31 WILLOUGHBY ROAD NW3 1RT - PROPOSED BASEMENT

EXISTING & PROPOSED LONG SECTION SKETCHES

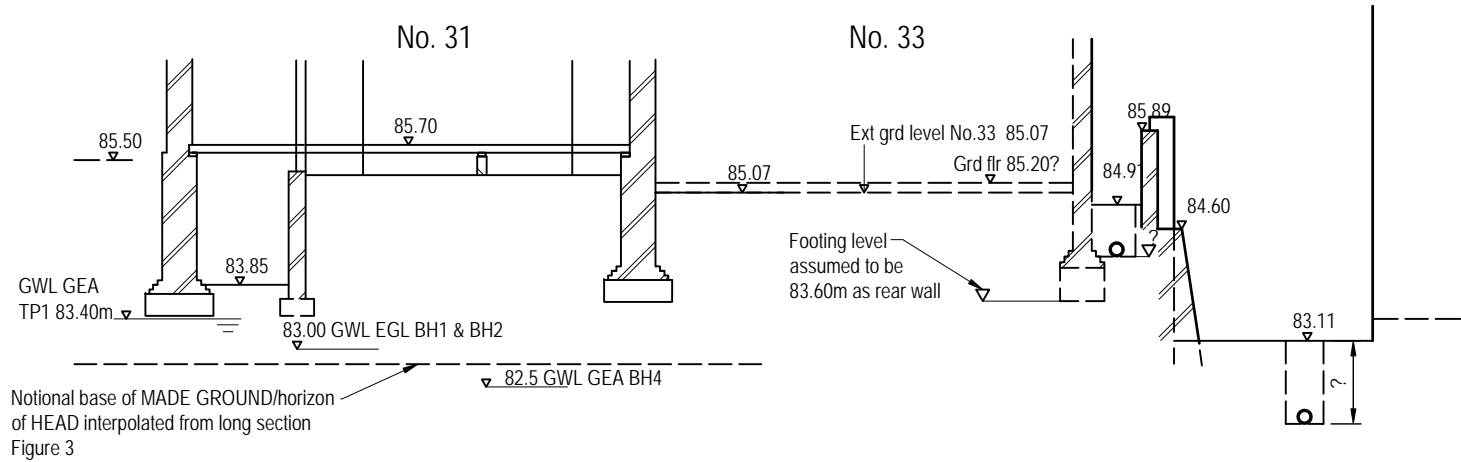


Report:G1808-RP-01-E1

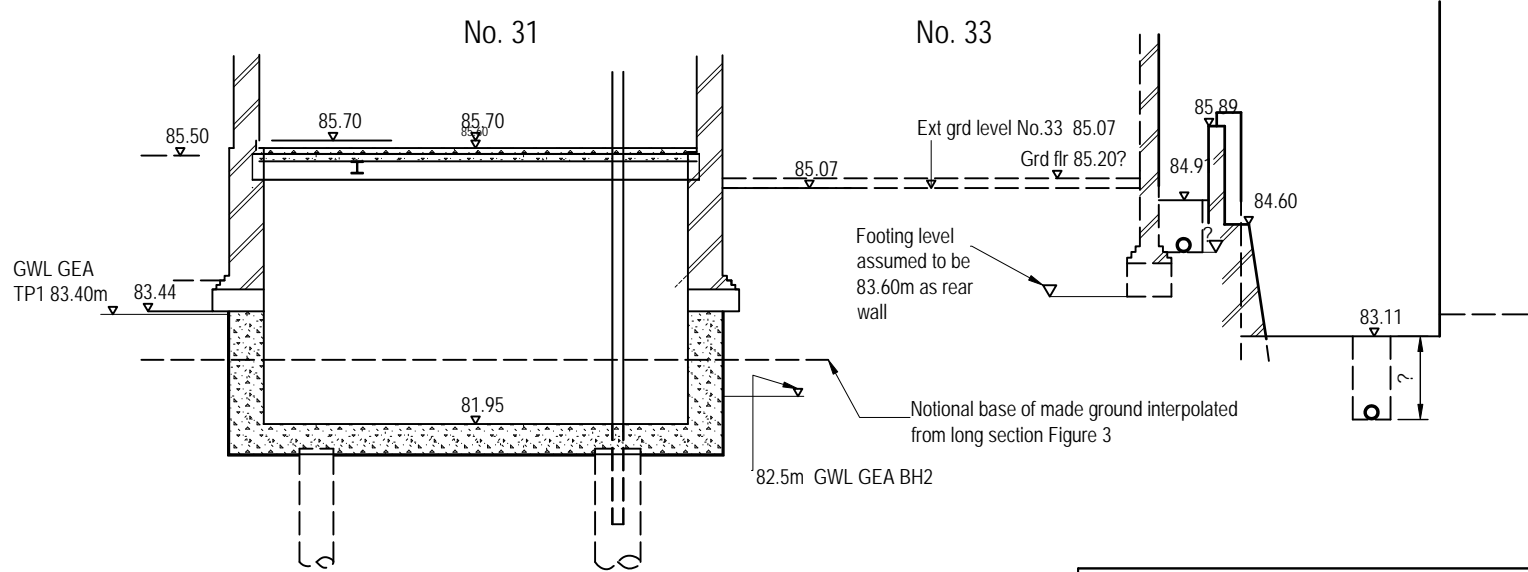
Scale as shown

Figure

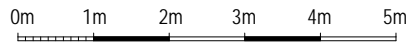
9.




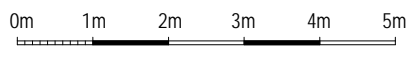
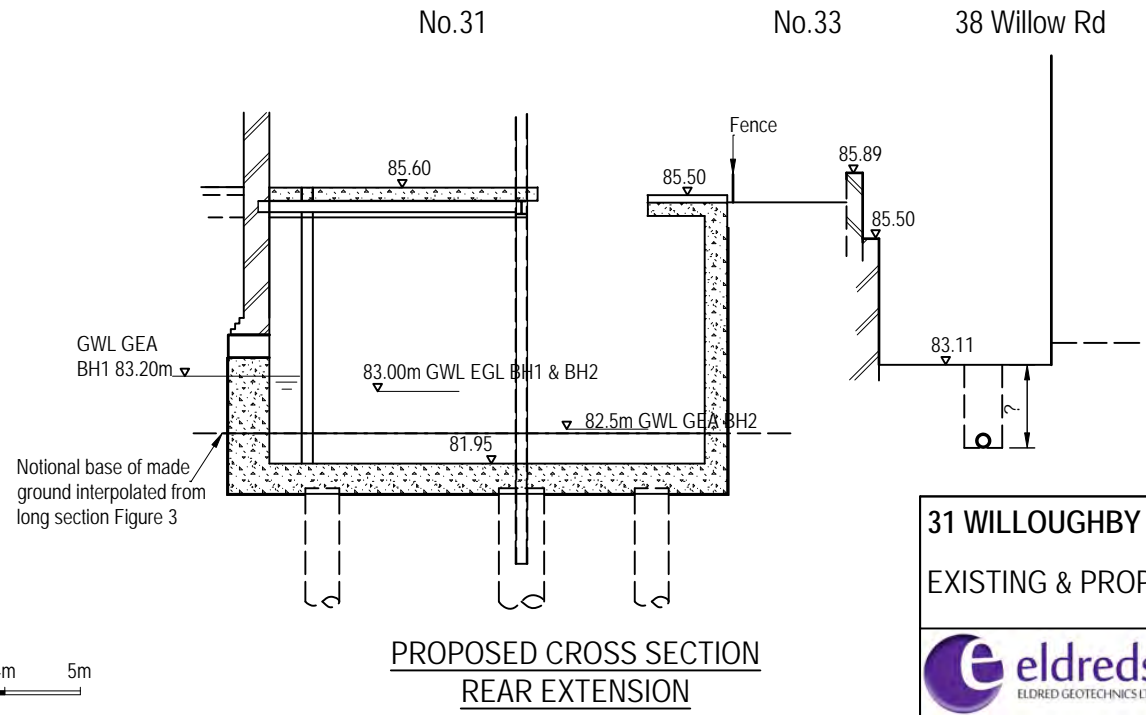
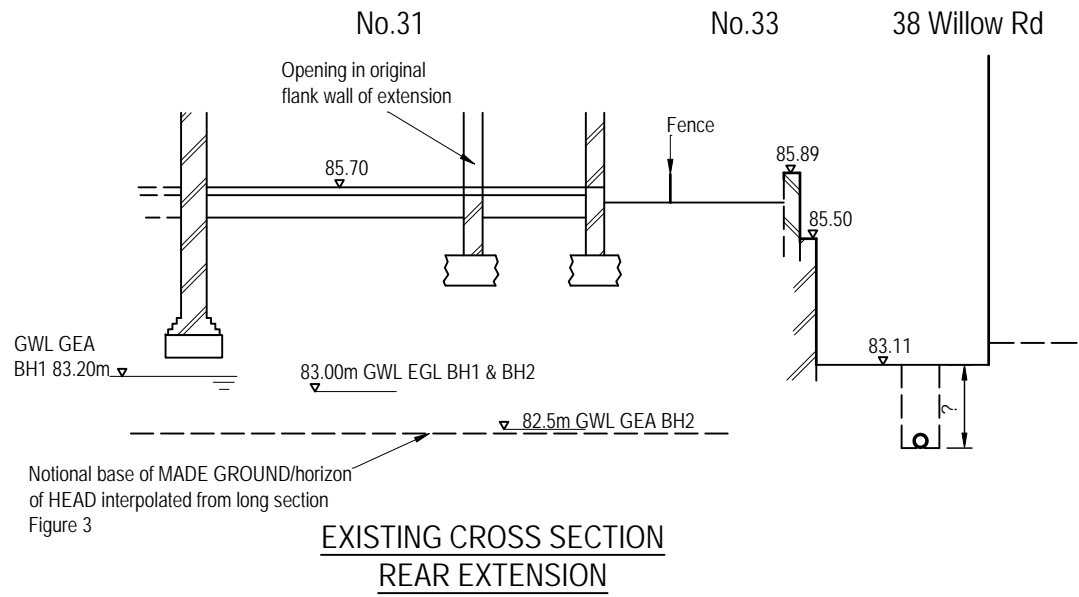
**EXISTING CROSS SECTION
REAR EXTENSION**



**PROPOSED CROSS SECTION
FRONT OF HOUSE**



31 WILLOUGHBY ROAD NW3 1RT - PROPOSED BASEMENT		
EXISTING & PROPOSED CROSS SECTION SKETCHES - FRONT		
 <small>ELDRÉD GEOTECHNICS LTD</small>	Report: G1808-RP-01-E1	Figure 10
	Scale as shown	

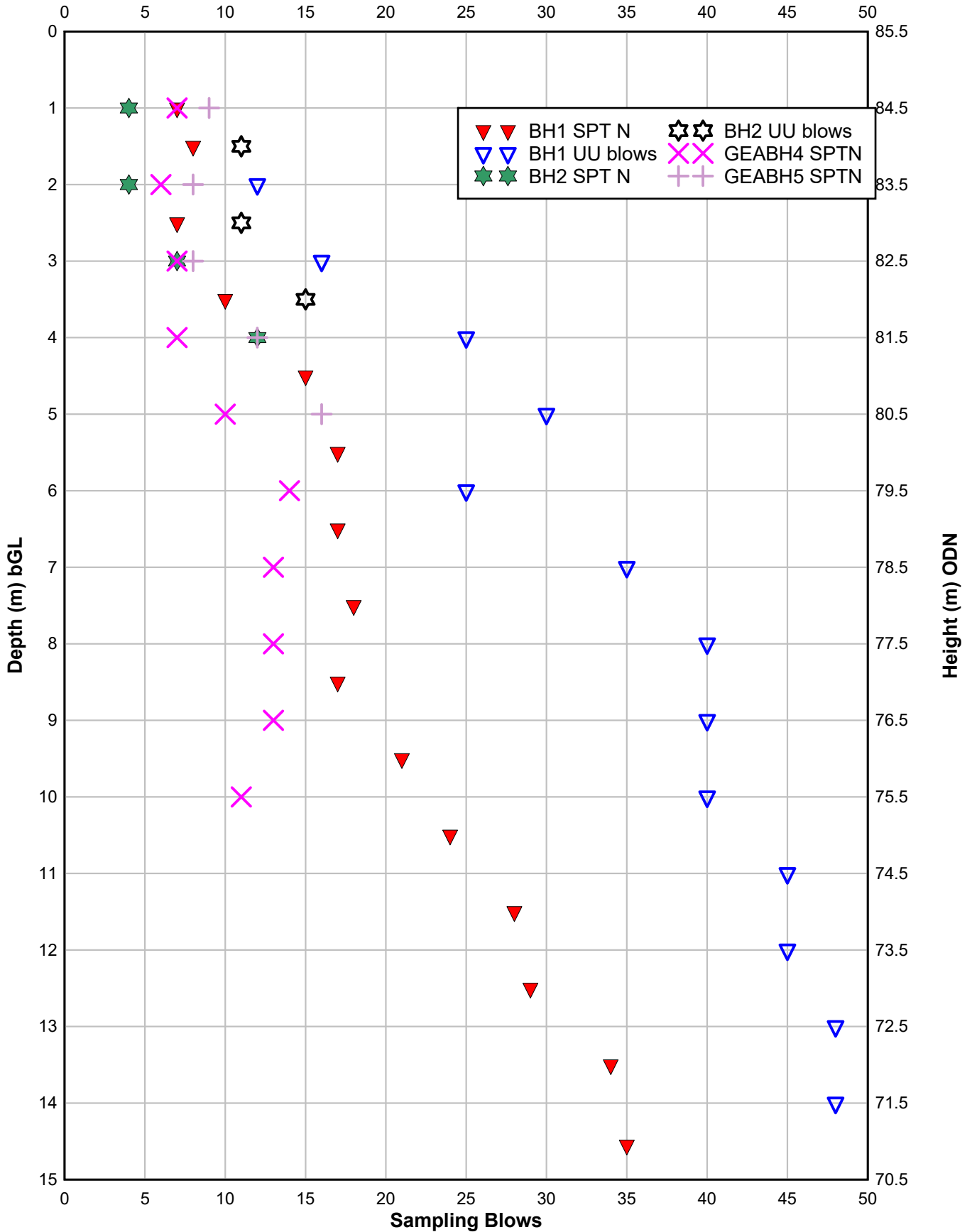


31 WILLOUGHBY ROAD NW3 1RT - PROPOSED BASEMENT
EXISTING & PROPOSED CROSS SECTION SKETCHES - REAR

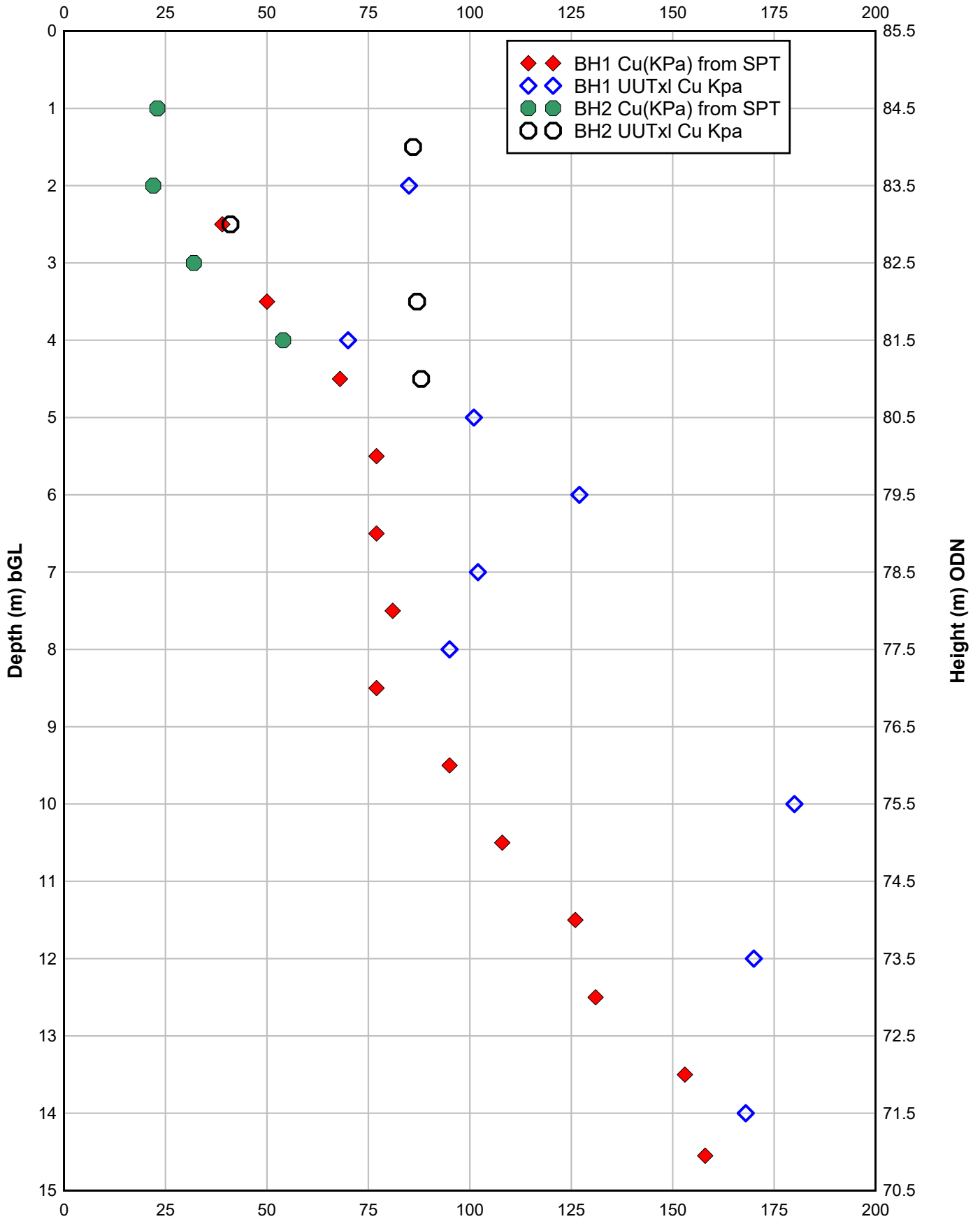


Report: G1808-RP-01-E1
Scale as shown

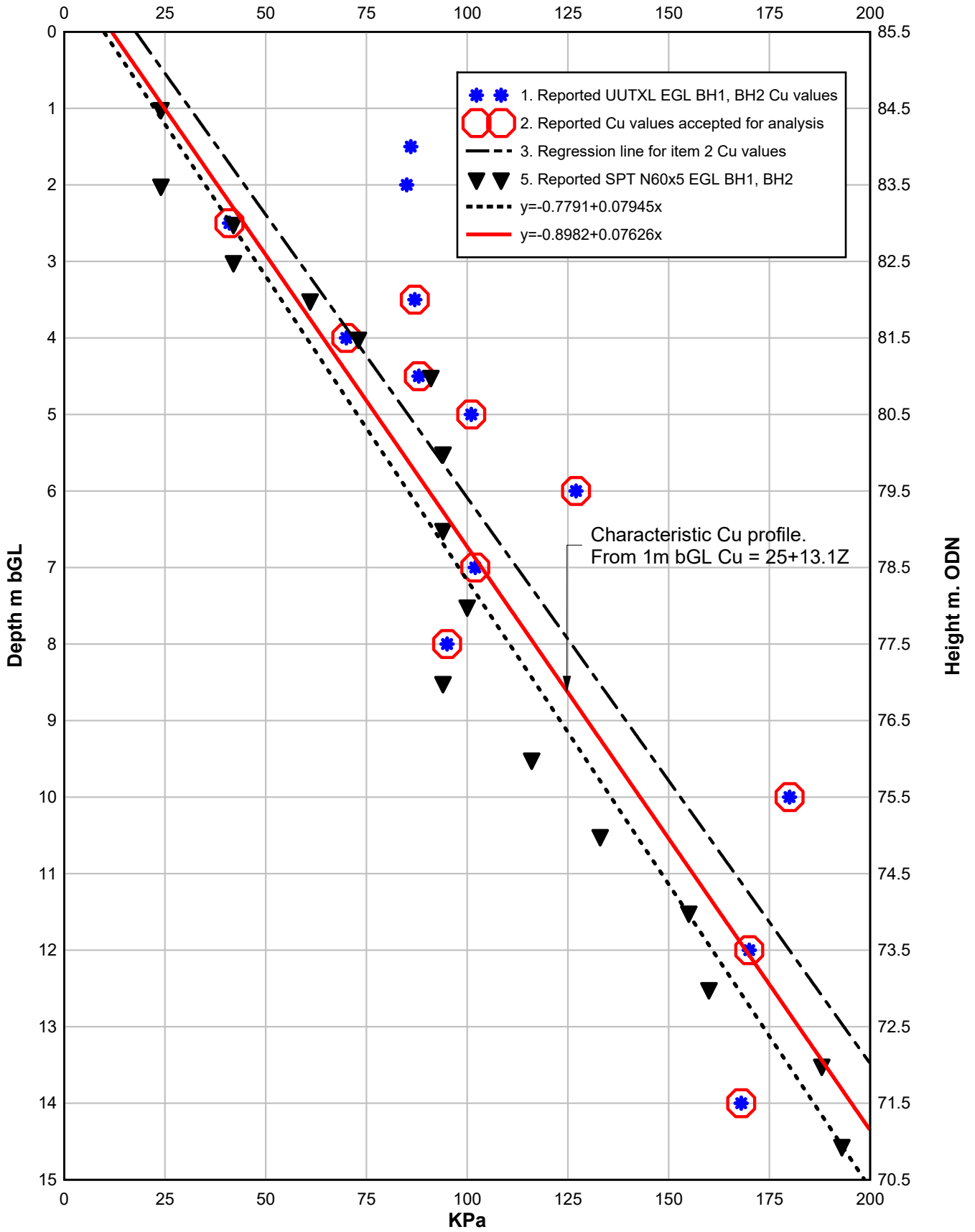
G1808 31 Willoughby Road NW3 1RT - Proposed Basement Sampling Blow Counts vs Depth & ODN Height



G1808 31 Willoughby Road NW3 1RT - Proposed Basement Undrained Shear Strength vs Depth & ODN Height



G1808 31 Willoughby Road NW3 1RT - Proposed Basement Assessed Characteristic Profile of Undrained Shear strength vs Depth



Appendix D Contents

Preliminary structural design report

Drawings of existing structure

G1808-PA-001 -E1 Existing site plan and sections

G1808-PA-002-E1 Existing sub-ground floor plan and sections

G1808-PA-003-E1 Existing ground floor plan showing first floor structure above

G1808-PA-004-E1 Existing first floor plan showing second floor structure above

G1808-PA-005-E1 Existing second floor plan showing study structure above

G1808-PA-006-E1 Existing third floor plan showing roof structure above

G1808-PA-007-E1 Existing sections

Drawings of proposed structure

G1808-PA-101 -E1 Proposed relationship of rear basement to boundary walls

G1808-PA-102-E1 Proposed basement plan and sections

G1808-PA-103-E1 Proposed ground floor plans showing ground & first floor structure

G1808-PA-104-E1 Proposed general section A-A

G1808-PA-005-E1 Proposed general cross sections

Outline structural design report G1808-ST-01-E1 for basement extension of 31 Willoughby Road NW3 1RT

1 Criteria references

1. BS EN 1990 Basis of structural design
2. BS EN 1991 Actions on structures
3. BS EN 1992 Design of concrete structures
4. BS EN 1993 Design of steel structures
5. BS EN 1995 Design of timber structures
6. BS EN 1996 Design of masonry structures

2 Overview

7. Structural alterations are required as part of a scheme to provide a single storey basement below the property. The structural proposal is for a steel framed solution which will be inserted as work proceeds to provide maximum working space for the basement and ground floor works. Refer to the engineering design illustrated by Eldreds' accompanying drawings and method statement.

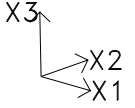
3 Software

8. STRAP (STRuctural Analysis Programs) 2018 version by Atir Engineering Software Ltd has been used for analysis of the structure. At this preliminary stage no attempt has been made to model staged construction sequences or stress reversals that installation and removal of temporary supports will cause as the frame develops: the analysis allows for what are judged to be the worst conditions likely to occur.

4 Frame arrangement

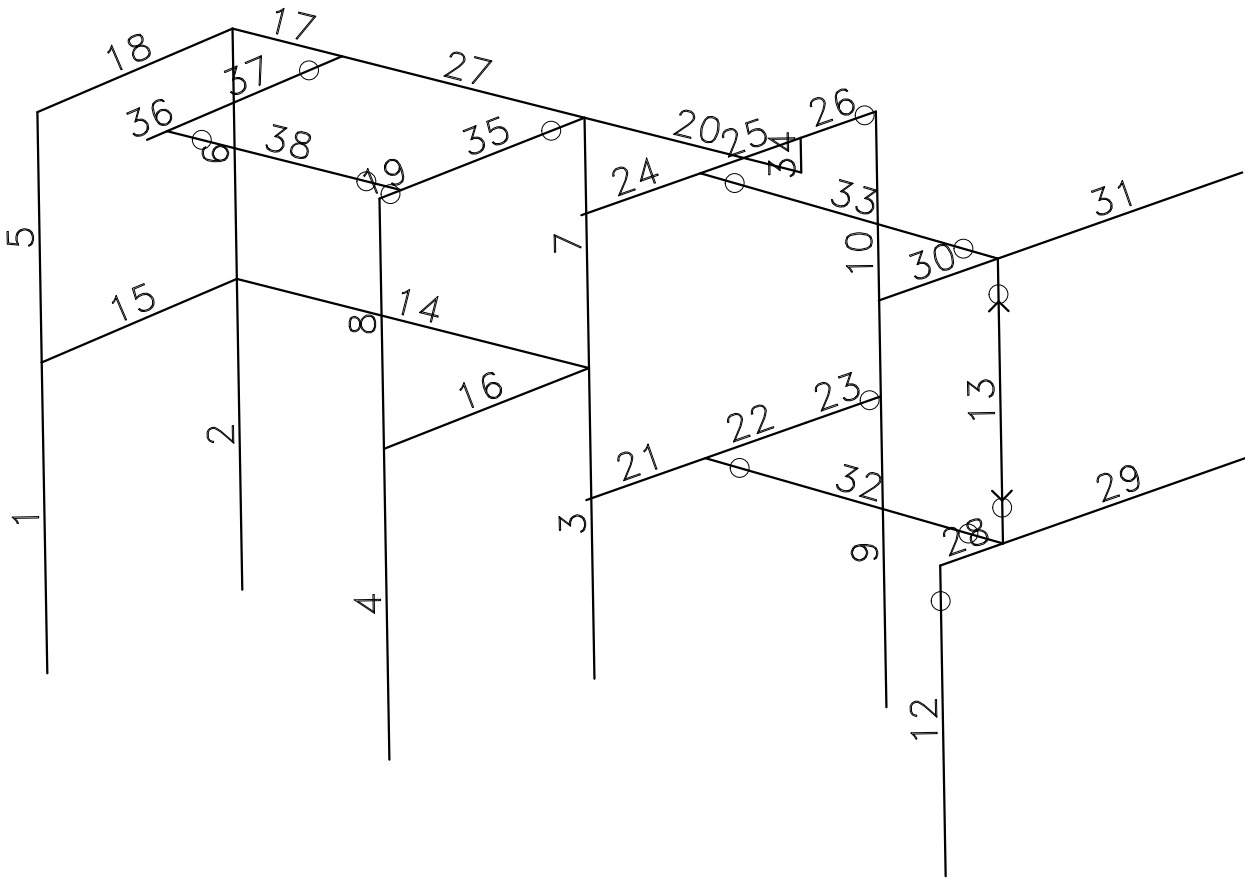
31 WILLOUGHBY ROAD NW3 1RT – BASEMENT

Steel frame isometric – STRAP beam Nos.



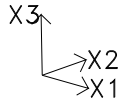
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DATE:14/07/19



31 WILLOUGHBY ROAD NW3 1RT – BASEMENT

Steel frame isometric rendered



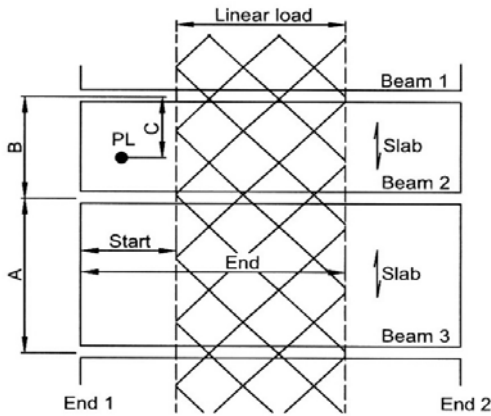
DATE:14/07/19



5 Loads

PROJECT	SUBJECT	DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension	Key to Excel tables used to calculate actions on structure	4/19	G1808	1	

Item	Table Column	Description
1	Member	Element of construction identified as receiving load
2	Action source	Element of construction or externally applied action causing load upon the member
3	Type	Load type: U = uniformly distributed (KN/m ²); L = linearly distributed over a certain distance (KN/m); P = point load (KN)
4	Unit action	Characteristic force (KN), force/unit length or area (KN/m or KN/m ²), or material density (KN/m ³)
5	Factor	Factor converting the source action to the corresponding effective action upon the member; e.g. in the simplest case, if the member spreads a source point load to cause a uniformly distributed load of length X at the level considered, the effect at that level is given by a factor of 1/X. The converse, situation would require a factor of X.
6	Width or Ht.	Refer to diagram. Considering load on Beam 2, the width of the slab load and of the linear load is A+B. For the point load, the width is entered as 1 to preserve the calculation logic. Height is entered for vertical elements such as walls, when unit loads are given /unit area on elevation.. To preserve calculation logic, height is given as 1 for unit loads /m run.
7	Proportion	Proportion of load width or height attracted to the member considered. If slabs in the diagram are simply supported, the proportion of the slab and linear loads on Beam 2 is 0.5 and the proportion of the point load is C/B.
8	Perm. & Var.	End values of permanent and variable actions are the product of items 3, 4, 5 and 6



PROJECT	SUBJECT	DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension	Construction notes and Characteristic Unit Loads	4/19	G1808	3	
EXISTING BUILDINGS: Refer to current editions of drawings G1808-GA-001 to 007					
Pitched roofs Nos 29 & 31					
Permanent	Slate			0.25	
	Battens			0.04	
	Rafters			0.10	
	Ceiling (P/Bd & skim)			0.17	
	Total			0.56 Kpa	
	30 deg. Pitch factor			1.15	
	Total on plan			0.64 KPa	
Variable				0.60 KPa	
Floors Nos 29-33					
Permanent	12mm HW overlay			0.09	
	Boards Joists, ceiling			0.50	
				0.59 Kpa	
Variable	No 31 upper			0.90 Kpa	
	All floors occupied			1.50 Kpa	
Patio roofs					
	Concrete tiles			0.38	
	50mm screed			1.15	
	Asphalt			0.42	
	Boards Joists, ceiling			0.50	
				2.45 Kpa	
Variable				1.50 KPa	

PROJECT	SUBJECT			DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension	Construction notes and Characteristic Unit Loads			4/19	G1808	4	
<p>EXISTING BUILDINGS: Refer to current editions of drawings G1808-GA-001 to 007</p>							
<p>Flat roof No.33</p>							
Permanent	Lead, code 5, underlay, paper			0.30			
	Boards Joists, ceiling			<u>0.50</u>			
				<u>0.80</u> Kpa			
Variable				<u>0.60</u> KPa			
<p>Tiled roof No.33</p>							
Permanent	Clay tiles plain			0.65			
	Battens			0.04			
	Rafters			0.10			
	Ceiling (P/Bd & skim)			<u>0.17</u>			
	Total			0.96	Kpa		
	30 deg. Pitch factor			<u>1.15</u>			
	Total on plan			<u>1.10</u>	KPa		
Variable				<u>0.60</u>	KPa		
<p>Walls</p>							
Permanent	Brick medium dense	21.53	KN.m3				
	Thickness (mm)	450		<u>9.69</u>	Kpa		
		340		<u>7.32</u>	Kpa		
		225		<u>4.84</u>	Kpa		
		112		<u>2.41</u>	KPa		
	Plaster/render per side			<u>0.25</u>	KPa		

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	6	
Member/Case	Action source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End	
					Start	End		Start	End	Start	End
<u>Ridge Beam No.31. No.29 beam similar</u>											
Permanent	Pitched roof	U	0.64	1.00	9.00	9.00	0.50	2.90	2.90		
Variable		U	0.60	1.00	9.00	9.00	0.50	2.70	2.70		
<u>Party Wall Nos 29/31 Front Section</u>											
<u>Roof to Grd</u>											
Permanent	Ridge beams 225 Wall roof to 3rd (ave 340 wall 3rd- 1st 450 wall 1st- grd 2nd-grd stair well strips Total at grd (KN/m)	U	2.90	0.22	6.00	6.00	0.50	1.93	1.93		
		U	5.34	1.00	1.75	1.75	1.00	9.35	9.35		
		U	7.82	1.00	6.20	6.20	1.00	48.49	48.49		
		U	10.19	1.00	3.35	3.35	1.00	34.13	34.13		
		U	0.59	6.00	2.00	2.00	0.50	3.54	3.54		
								97.44	97.44		
Variable	Ridge beams 2nd-grd stair well strips Total at grd (KN/m)	U	0.60	0.22	6.00	6.00	0.50	0.40	0.40		
		U	1.50	6.00	2.00	2.00	0.50	9.00	9.00		
									9.40	9.40	
<u>450mm Party wall Grd-Ftg.</u>											
Permanent	Wall	U	9.69	1.00	2.00	2.00	1.00	19.38	19.38		
		U	21.53	0.23	0.63	0.63	1.00	3.03	3.03		
		U	23.00	0.30	0.90	0.90	1.00	6.21	6.21		
									28.61	28.61	

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	7	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End 1	
					Start	End		Start	End	Start	End
Party/Ext Wall Nos 31/33											
Front & back sections 2.5m long, Roof- Grd											
Permanent	Ridge beam No.31	U	2.90	0.11	6.00	6.00	0.50	0.97	0.97		
	225 Wall roof - 3rd (ave ht) Stack 0.3m2 net	U	5.34	1.00	1.75	1.75	1.00	9.35	9.35	Stack 50% void	
	340 wall 3rd-1st	U	21.53	0.06	3.75	3.75	1.00	4.84	4.84		
	450 wall 1st-grd Stack 0.5m2 net	U	7.82	1.00	6.20	6.20	1.00	48.49	48.49		
		U	10.19	1.00	3.35	3.35	1.00	34.13	34.13	Stack 50% void	
		U	21.53	0.10	9.55	9.55	1.00	20.56	20.56		
	No.33 flat roof	U	0.80	1.00	3.50	3.50	0.50	1.40	1.40		
	No.33 1st & 2nd flrs Total at Grd (KN/m)	U	0.59	1.00	4.00	4.00	0.50	1.18	1.18		
								120.92	120.92		
Variable	Ridge beam No.31	U	2.70	0.11	6.00	6.00	0.50	0.90	0.90		
	No.33 flat roof	U	0.60	1.00	3.50	3.50	0.50	1.05	1.05		
	No.33 1st & 2nd flrs Total at Grd (KN/m)	U	1.50	1.00	4.00	4.00	0.50	3.00	3.00		
								4.95	4.95		
Middle section 4.5m long, Roof- Grd											
Permanent	Ridge beam No.31	U	2.90	0.11	6.00	6.00	0.50	0.97	0.97		
	225 Wall roof - 3rd (ave ht) Stack 0.3m2 net	U	5.34	1.00	1.75	1.75	1.00	9.35	9.35	Stack 50% void	
	340 wall 3rd-1st	U	21.53	0.07	3.75	3.75	1.00	5.38	5.38		
	450 wall 1st-grd Stack 0.5m2 net	U	7.82	1.00	6.20	6.20	1.00	48.49	48.49		
		U	10.19	1.00	3.35	3.35	1.00	34.13	34.13	Stack 50% void	
		U	21.53	0.11	9.55	9.55	1.00	22.85	22.85		
	No.33 flat roof	U	0.80	1.00	3.50	3.50	0.50	1.40	1.40		
	No.33 1st & 2nd flrs Total at Grd (KN/m)	U	0.59	1.00	4.00	4.00	0.50	1.18	1.18		
								123.74	123.74		

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	8	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End 1	
					Start	End		Start	End	Start	End
Party/Ext Wall Nos 31/33 Contd											
<u>Middle section 4.5m long, Roof- Grd Contd</u>											
Variable	Ridge beam No.31	U	2.70	0.11	6.00	6.00	0.50	0.90	0.90		
	No.33 flat roof	U	0.60	1.00	3.50	3.50	0.50	1.05	1.05		
	No.33 1st &2nd flrs	U	1.50	1.00	4.00	4.00	0.50	3.00	3.00		
	Total at Grd (KN/m)							4.95	4.95		
<u>450mm Party wall Grd-Ftg. (2.5m deep)</u>											
Permanent	Wall	U	9.69	1.00	2.00	2.00	1.00	19.38	19.38		
	Ftg spread	U	3.03	1.00	1.00	1.00	1.00	3.03	3.03		
	Concrete	U	6.90	1.00	0.90	0.90	1.00	6.21	6.21		
	Total							28.61	28.61		
Party Wall Nos 29/31 Rear Section											
<u>Roof to Grd Flr.</u>											
Permanent	Patio roof	U	2.45	2.00	3.50	3.50	0.50	8.58	8.58		
	Stack above r'f 0.4m2 net	U	21.53	0.07	4.00	4.00	1.00	5.74	5.74		
	225 wall roof- 1st	U	5.34	1.00	3.25	3.25	1.00	17.37	17.37		
	Stack r'f-grd 0.6m2 net	U	21.53	0.10	5.80	5.80	1.00	12.49	12.49		
	340 wall 1st- grd	U	7.82	1.00	2.84	2.84	1.00	22.21	22.21		
	1st flr Total at Grd (KN/m)	U	0.59	2.00	3.50	3.50	0.50	2.07	2.07		
								68.45	68.45		
Variable	Patio roof	U	1.50	2.00	3.50	3.50	0.50	5.25	5.25		
	1st Flr. Total at Grd (KN/m)	U	1.50	2.00	3.50	3.50	0.50	5.25	5.25		
								10.50	10.50		

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	9	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End 1	
					Start	End		Start	End	Start	End
Party Wall Nos 29/31 Rear Section Contd											
<u>340mm Party wall Grd-Ftg (1.5m deep)</u>											
Permanent	Wall	U	7.32	1.00	1.00	1.00	1.00	7.32	7.32		
	Stack 1.2m2	U	21.53	0.30	1.00	1.00	1.00	6.46	6.46		
	Ftg spread	U	21.53	0.23	0.63	0.63	1.00	3.03	3.03		
	Concrete	U	23.00	0.30	0.90	0.90	1.00	<u>6.21</u>	<u>6.21</u>		
	Total (KN/m)							<u>23.02</u>	<u>23.02</u>		
Front Bay wall											
<u>Roof-grd</u>											
Permanent	Tiled roof	U	1.10	1.00	1.00	1.00	0.50	0.55	0.55		
	1st flr	U	0.59	1.00	1.00	1.00	0.50	0.30	0.30		
	225 brick omit net of fenest'n 7m2	U	5.09	1.00	6.80	6.80	1.00	34.64	34.64		
		U	-4.54	7.00	0.29	0.29	1.00	<u>-9.07</u>	<u>-9.07</u>		
	Total (KN/m)							<u>26.42</u>	<u>26.42</u>		
Variable	Tiled roof	U	0.60	1.00	1.00	1.00	0.50	0.30	0.30		
	1st flr	U	1.50	1.00	1.00	1.00	0.50	<u>0.75</u>	<u>0.75</u>		
	Total (KN/m)							<u>1.05</u>	<u>1.05</u>		
<u>Grd-Ftg</u>											
Permanent	225mm brick	U	4.84	1.00	1.00	1.00	1.00	4.84	4.84		
	340mm brick	U	7.32	1.00	1.00	1.00	1.00	7.32	7.32		
	Concrete	U	5.52	1.00	1.00	1.00	1.00	<u>5.52</u>	<u>5.52</u>		
	Total (KN/m)							<u>17.68</u>	<u>17.68</u>		

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	11	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End	
					Start	End		Start	End	Start	End
Main front wall											
<u>1m wide left section bearing on 29/31 party wall above entrance</u>											
Permanent	Roof	U	0.64	1.00	1.50		0.50	0.48			
	Eaves partns	U	2.67	1.00	1.00		0.67	1.78			
	3rd flr	U	0.59	1.00	4.50		0.50	1.33			
	2nd flr	U	0.59	1.00	4.50		0.50	1.33			
	1st flr	U	0.59	1.00	4.50		0.50	1.33			
	Wall roof-2nd Ddt windows 0.8m2	U	5.09	1.00	2.90		1.00	14.77			
		U	-4.79	0.80	1.00		1.00	-3.84			
	Wall 2nd-1st Ddt windows 1.8m2	U	7.57	1.00	3.30		1.00	24.98			
		U	-7.27	1.00	1.00		1.00	-7.27			
	Total (KN/m)							34.89			
Variable	Roof	U	0.60	1.00	1.50		0.50	0.45			
	Eaves partns	U	1.35	1.00	1.00		0.67	0.90			
	3rd-1st floors	U	1.50	3.00	4.50		0.50	10.13			
	Total (KN/m)							11.48			
<u>340mm wall Grd-Ftg (2.5m deep)</u>											
Permanent	Wall	U	7.32	1.00	2.00	2.00	1.00	14.64	14.64		
	Ftg spread	U	21.53	0.23	0.63	0.63	1.00	3.03	3.03		
	Concrete	U	23.00	0.30	0.90	0.90	1.00	6.21	6.21		
	Total (KN/m)							23.88	23.88		

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	13	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End 1	
					Start	End		Start	End	Start	End
<u>Main front wall Contd.</u>											
<u>Right (No.33) side of bay, 0.8m long at Grd Flr Contd</u>											
Variable	Roof	U	0.60	3.13	1.50	1.50	0.50	1.41	1.41		
	Eaves partns	U	1.35	3.13	1.00	1.00	1.00	4.22	4.22		
	3rd-1st floors	U	1.50	9.38	4.50	4.50	0.50	31.64	31.64		
	Total (KN/m)							37.27	37.27		
<u>Main rear wall</u>											
<u>Left(No.33) side of bay, 0.7m long at Grd Flr</u>											
Permanent	Roof	U	0.64	1.79	1.50	1.50	0.50	0.86	0.86		
	Eaves partns	U	2.67	1.79	1.00	1.00	1.00	14.30	14.30		
	3rd-1st floors	U	0.59	5.36	4.50	4.50	0.50	7.11	7.11		
	Wall 3rd-2nd Ddt windows 0.8m2	U	5.09	1.79	2.90	2.90	1.00	26.38	26.38		
		U	-4.79	1.14	1.00	1.00	1.00	-5.48	-5.48		
	Wall 2nd-1st Ddt windows 1m2	U	7.57	1.79	3.30	3.30	1.00	44.61	44.61		
		U	-7.27	1.43	1.00	1.00	1.00	-10.39	-10.39		
	Wall 1st-Grd	U	7.57	1.43	3.35	3.35	1.00	36.23	36.23		
	Total (KN/m)							113.63	113.63		
Variable	Roof	U	0.60	1.79	1.50	1.50	0.50	0.80	0.80		
	Eaves partns	U	1.35	1.79	1.00	1.00	1.00	2.41	2.41		
	3rd-1st floors	U	1.50	5.36	4.50	4.50	0.50	18.08	18.08		
	Total (KN/m)							21.29	21.29		
<u>Left(No.33) side of bay, 0.7m long at soffit 1st Flr</u>											
Permanent	As above							113.63	113.63		
	Deduct wall 1st							-36.23	-36.23		
	Total (KN/m)							77.40	77.40		

31 WILLOUGHBY ROAD NW3 1RT - BASEMENT

Prepared by: MLE

Units: kN meter

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PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	14	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End 1	
					Start	End		Start	End	Start	End
<u>Main rear wall Contd</u>											
<u>Mid section of wall 2m long at Grd Flr</u>											
Permanent	Roof	U	0.56	1.75	1.50	1.50	0.50	0.74	0.74		
	Eaves partns	U	2.67	1.75	1.00	1.00	1.00	4.67	4.67		
	3rd-1st	U	0.59	5.25	4.50	4.50	0.50	6.97	6.97		
	Wall 3rd-2nd	U	5.09	1.75	2.90	2.90	1.00	25.85	25.85		
	Ddt windows 2m2	U	-4.79	1.00	1.00	1.00	1.00	-4.79	-4.79		
	Wall 2nd-Grd	U	7.57	1.25	6.35	6.35	1.00	60.09	60.09		
	Ddt windows 2.25m2	U	-7.27	1.13	1.00	1.00	1.00	-8.18	-8.18		
	Total (KN/m)							85.34	85.34		
	Total at 1st flr soffit(KN/m)							65.31	65.31		
Variable	Roof	U	0.60	1.75	1.50	1.50	0.50	0.79	0.79		
	Eaves partns	U	1.35	1.75	1.00	1.00	1.00	2.36	2.36		
	3rd-1st floors	U	1.50	5.25	4.50	4.50	0.50	17.72	17.72		
	Total (KN/m)							20.87	20.87		
<u>Right(No.29) side, 1m long supported at 2nd flr.</u>											
Permanent	Roof	U	0.56	1.00	1.50	1.50	0.50	0.42	0.42		
	Eaves partns	U	2.67	1.00	1.00	1.00	1.00	2.67	2.67		
	3rd-2nd flrs	U	0.59	1.00	4.50	4.50	0.50	1.33	1.33		
	Wall 3rd-2nd	U	5.09	1.00	3.70	3.70	1.00	18.85	18.85		
	Ddt windows 1.25m2	U	-4.79	1.25	1.00	1.00	1.00	-5.99	-5.99		
	Total(KN/m) on beam							17.27	17.27		
Variable	Roof	U	0.60	1.75	1.50	1.50	0.50	0.79	0.79		
	Eaves partns	U	1.35	1.75	1.00	1.00	1.00	2.36	2.36		
	3rd-1st floors	U	1.50	5.25	4.50	4.50	0.50	17.72	17.72		
	Total(KN/m) on beam							20.87	20.87		

PROJECT			SUBJECT					DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension			Characteristic Member Actions					4/19	G1808	15	
Member/Case	Load source	Type	Unit load	Factor	Width/height		Prop'n	Value		(m) from End 1	
					Start	End		Start	End	Start	End
Rear extension flank & rear walls											
<u>Flank wall at 1st floor</u>											
Permanent	Patio roof	U	2.45	1.00	3.50	3.50	0.50	4.29	4.29		
	1st Floor	U	0.59	1.00	3.50	3.50	0.50	1.03	1.03		
	Wall roof-1st	U	5.09	1.00	3.75	3.75	1.00	19.10	19.10		
	Total (KN/m)							<u>24.42</u>	<u>24.42</u>		
Variable	Roof	U	1.50	1.75	3.50	3.50	0.50	4.59	4.59		
	1st Floor	U	1.50	1.75	3.50	3.50	0.50	4.59	4.59		
	Total (KN/m)							<u>9.19</u>	<u>9.19</u>		
<u>Rear wall at 1st floor</u>											
Permanent	Wall roof-1st	U	5.09	1.00	3.75	3.75	1.00	<u>19.10</u>	<u>19.10</u>		
<u>Longitudinal wall adj stair</u>											
<u>3rd-1st flr</u>											
Permanent	Stud wall	U	1.22	1.00	7.70	7.70	1.00	9.39	9.39		
	Floors	U	0.59	3.00	2.00	2.00	0.50	<u>1.77</u>	<u>1.77</u>		
	Total (KN/m)							<u>11.16</u>	<u>11.16</u>		
Variable	Floors	U	1.50	3.00	2.00	2.00	0.50	<u>4.50</u>	<u>4.50</u>		
<u>1st-Grd floor</u>	brick 2.4m	U	2.91	1.88	3.35	3.35	1.00	<u>18.29</u>	<u>18.29</u>		

PROJECT	SUBJECT				DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension	Load Summaries				4/19	G1808	16	
EXISTING BUILDINGS: Refer to current editions of drawings G1808-GA-001 to 007								
					<u>Main rear wall</u>			
<u>Front Bay</u>	Perm.	Var.		Page	<u>adj PW33</u>	Perm.	Var.	Page
Total to Grd	26.42	1.05		B4	Total-Grd	113.63	21.29	KN/m B8
Grd-Ftg	17.68			B4	Grd-Ftg	23.88		B4
Total to Ftg	44.11	1.05	KN/m		Total at Ftg	137.51	21.29	KN/m
					<u>Main rear wall</u>			
					<u>mid section</u>			
					Perm.	Var.		Page
					Total-Grd	85.34	20.87	B9
					Grd-Ftg	23.88		B4
					Total at Ftg	109.22	20.87	KN/m
<u>Front Wall</u>	Perm.	Var.		Page				
<u>adj PW 29</u>					Total-Grd	34.89	11.48	B6
Grd-Ftg	23.88			B4				
Total at Ftg	58.77	11.48	KN/m					
					<u>Main rear wall</u>			
					<u>adj PW29</u>			
					Perm.	Var.		Page
Total at Ftg	58.77	11.48	KN/m		Total on beam	17.27	20.87	KN/m B9
					<u>Front Wall</u>			
					<u>LHS Bay</u>			
					Perm.	Var.		Page
Total at Grd	98.83	29.81		B7	Total at 1st	19.10		KN/m B10
Grd-Ftg	23.88			B4				
	122.70	29.81	KN/m					
					<u>Flank wal</u>			
					<u>back extn</u>			
					Perm.	Var.		Page
					Total on			
					beam at 1st	24.42	9.19	KN/m B10
<u>Front Wall</u>	Perm.	Var.		Page				
<u>adj PW33</u>					Total at Grd	84.22	37.27	B7/8
Grd-Ftg	23.88			B4				
	108.09	37.27	KN/m					
					<u>Party Wall 33</u>			
					Perm.	Var.		Page
Total at Grd	84.22	37.27		B7/8	Total at Grd	123.74	4.95	B2/3
Grd-Ftg	23.88			B4				
	108.09	37.27	KN/m		Grd-Ftg	28.61		B3
						152.36	4.95	KN/m
					<u>Internal cross</u>			
					<u>wall</u>			
					Perm.	Var.		Page
					UDL			
					in	52.17	54.77	KN/m B5

PROJECT	SUBJECT			DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension	Load Summaries			4/19	G1808	17	
<p><u>EXISTING BUILDINGS:</u> Refer to current editions of drawings G1808-GA-001 to 007</p>							
<u>Wall adj stair to grd</u>	Perm.	Var.		Page			
Total to 1st	11.16	4.50		B10			
1st-grd brick 2.4m long	18.29			B10			
Total to Grd	29.45	4.50	KN/m				
<u>PW 29 front</u>	Perm.	Var.		Page			
Total to grd	97.44	9.40		B1			
Grd-ftg	28.61			B1			
Toptal to Ftg	126.06	9.40	KN/m				
<u>PW 29 rear</u>	Perm.	Var.		Page			
Total to grd	68.45	10.50		B3			
Grd-ftg	23.02			B4			
Toptal to Ftg	91.46	10.50	KN/m				

PROJECT	SUBJECT				DATE	JOB REF.	SHEET	REVISION
31 Willoughby Road NW3 1RT Proposed Basement Extension	Load Summaries				4/19	G1808	18	
EXISTING BUILDINGS: Refer to current editions of drawings G1808-GA-001 to 007								
Total existing footing loads								
	<u>Wall</u>	<u>Perm.</u>	<u>Var.</u>	<u>Length</u>	<u>Total Perm.</u>	<u>Total Var.</u>		
	Front Bay	44.11	1.05	5.00	220.53	5.25		
	<u>Front Wall</u>							
	adj PW 29	58.77	11.48	2.00	117.54	22.96		
	<u>Front Wall</u>							
	LHS Bay	122.70	29.81	1.00	122.70	29.81		
	<u>Front Wall</u>							
	adj PW33	108.09	37.27	1.00	108.09	37.27		
	<u>Internal cross</u>							
	wall	52.17	54.77	5.50	286.94	301.24		
	<u>Main rear wall</u>							
	adj PW33	137.51	21.29	1.00	137.51	21.29		
	<u>Main rear wall</u>							
	mid section	109.22	20.87	2.00	218.44	41.74		
	<u>Main rear wall</u>							
	adj PW29	17.27	20.87	1.70	29.36	35.48		
	<u>Rear wall</u>							
	back extn	19.10		3.50	66.86	0.00		
	<u>Flank wal</u>							
	back extn	24.42	9.19	7.50	183.18	68.91		
	<u>Party Wall 33</u>							
	Wall adj stair	152.36	4.95	9.50	1447.40	47.03		
	<u>to grd</u>							
		29.45	4.50	4.50	132.53	20.25		
	<u>PW 29 front</u>							
		126.06	9.40	9.50	1197.53	89.30		
	<u>PW 29 rear</u>							
		91.46	10.50	7.00	640.25	73.50		
					4908.87	794.02		

STRAP LOADS INPUT

Load no. 1: Permanent SLS (units - kN meter)

/ BEAM LOADS

SELF X3 -1. B 1 TO 10 12 TO 35

DIST GL FX3 -20.39 B 31 30

/ BEAM LOADS

DIST GL FX3 -19.1 B 18

DIST GL FX3 -24.42 B 17 20 27

DIST GL FX3 -11.16 B 33

DIST GL FX3 -18.29 B 32

DIST GL FX3 -63.88 B 25

DIST GL FX3 -7.08 B 15 14

DIST GL FX3 -18.76 B 16

DIST GL FX3 -20.36 B 21 TO 23

DIST GL FX3 -24.43 B 28 29

/ BEAM LOADS

SELF X3 -1. B 38 37 36

DIST GL FX3 -10.98 B 38

/ END

FORCE SUMMATION

FX1=0. kN

FX2=0. kN

FX3=-1029.2 kN

*** PDELTA EFFECT WILL BE COMPUTED ***

Load no. 2: Variable SLS (units - kN meter)

/ BEAM LOADS

DIST GL FX3 -21.3 B 31 30

DIST GL FX3 -4.5 B 33

DIST GL FX3 -20.87 B 25

DIST GL FX3 -20.87 B 24

DIST GL FX3 -20.87 B 26

DIST GL FX3 -9.19 B 17 20 27

DIST GL FX3 -1.8 B 15 14

DIST GL FX3 -4.8 B 16

DIST GL FX3 -5.17 B 21 TO 23

DIST GL FX3 -6.2 B 28 29

/ END

FORCE SUMMATION

FX1=0. kN

FX2=0. kN

FX3=-403.75 kN

*** PDELTA EFFECT WILL BE COMPUTED ***

Load no. 3: Wind +X2 (units - kN meter)

/ GLOBAL LOADS

* WIND NAME Panel no. 1

* WIND PARAM EC1BS HEI X3 0. DIR +X2 TABLE 3

* WIND VAL B 30. CT 1. QREF 308.17 SEA 100. TOWN 1.

* WIND CP 1.15 ALL

* WIND ON BEAM -8.15 3.02 6.5 -3.105 3.317 6.5 -3.105 3.317 3.6 0. C

* WIND ON 2.9 E

DIST 0.6336 PLANE -8.15 3.02 6.5 -3.105 3.317 6.5 -3.105 3.317

3.6 P 0. 2.9 BEAMS

* WIND END

* WIND NAME Panel no. 2

* WIND PARAM EC1BS HEI X3 0. DIR +X2 TABLE 3

* WIND VAL B 30. CT 1. QREF 308.17 SEA 100. TOWN 1.

* WIND CP -1. ALL

* WIND ON BEAM -7.8 -0.46 3.6 -7.8 -0.46 6.5 -8.15 3.02 6.5 0. 3.4976 E

31 WILLOUGHBY ROAD NW3 1RT - BASEMENT

Prepared by: MLE

Units: kN meter

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Date: 14/07/19

Load no. 3: Wind +X2 (units - kN meter)

DIST 0.551 PLANE -7.8 -0.46 3.6 -7.8 -0.46 6.5 -8.15 3.02 6.5

P 0. 3.4976 BEAMS

* WIND END

/ END STATIC

FORCE SUMMATION

FX1=-6.1064 kN

FX2=8.7107 kN

FX3=0. kN

*** PDELTA EFFECT WILL BE COMPUTED ***

6 Steel Member check

6.1 Member references: STRAP correlated to Eldreds drawings

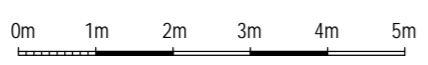
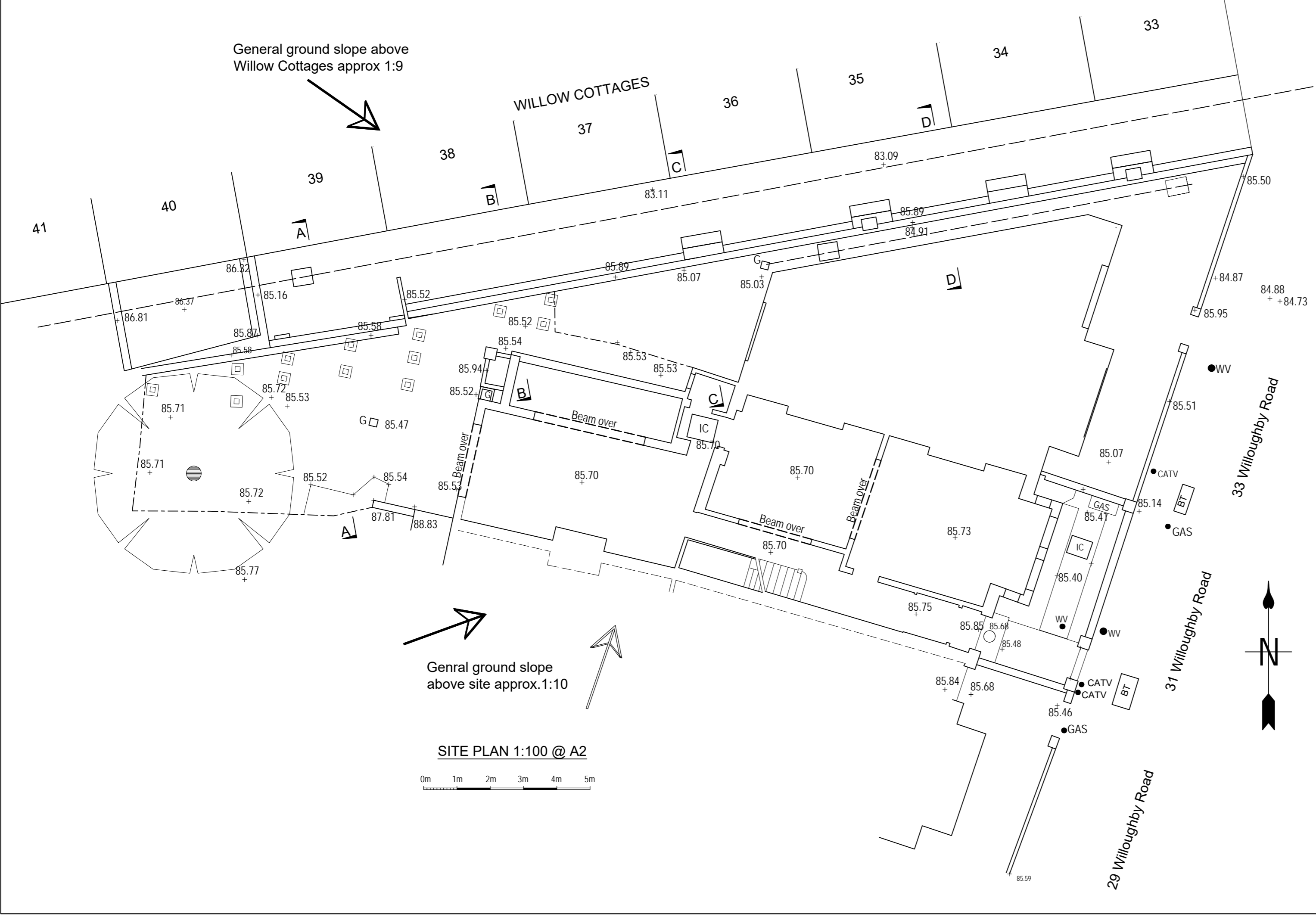
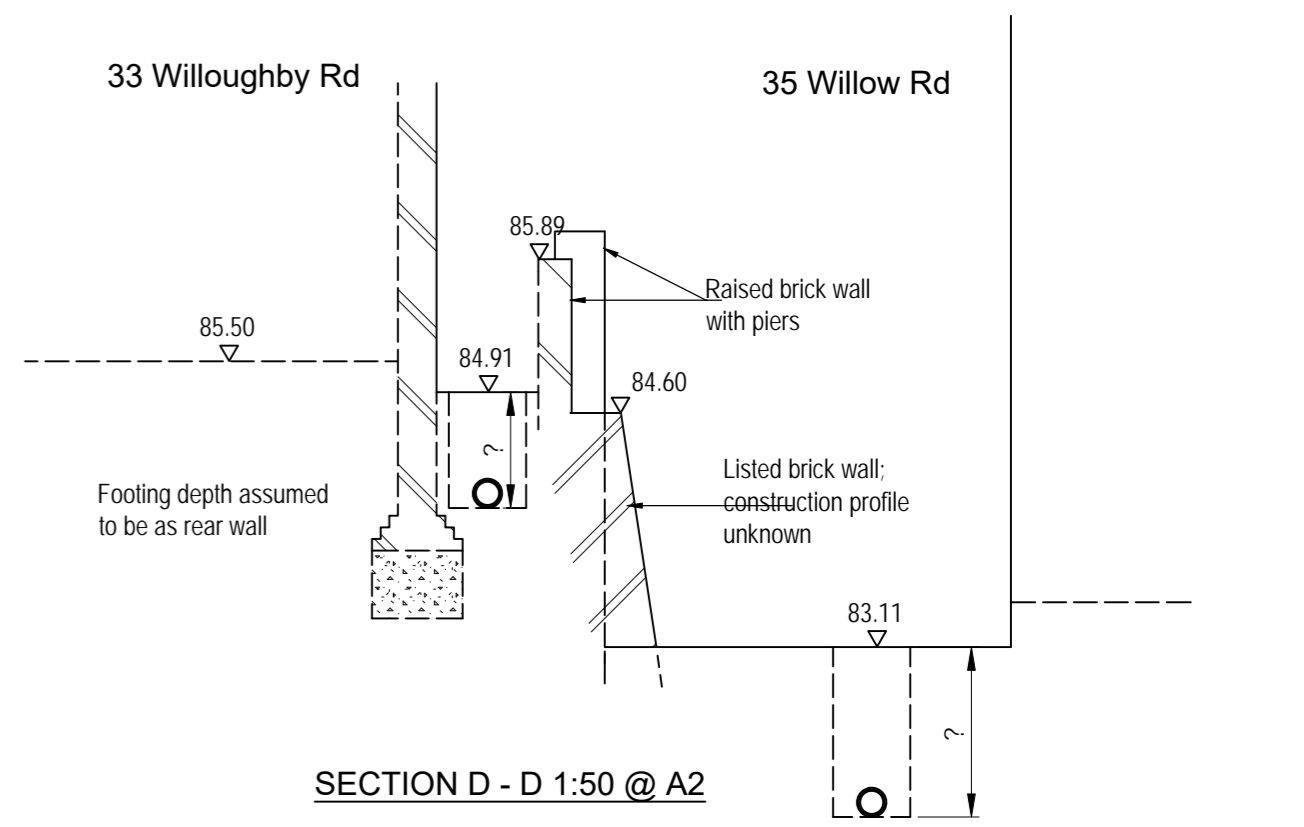
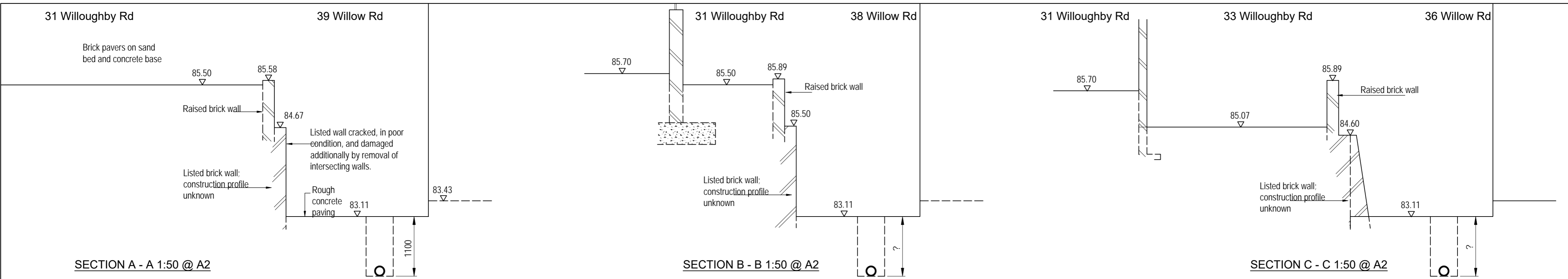
EGL	STRAP	EGL	STRAP	EGL	STRAP
B1	30,31	B10	21,22,23	C6	1
B2	24,25,26	B11	16	C7	13
B3	33	B12	15	C8	10
B4	17,27,20	B13	14	C9	7
B5	18	C1	12	C10	6
B6	37	C2	9	C11	8
B7	35	C3	3	C12	5
B8	38	C4	4		
B9	28,29	C5	2		

Results Summary Table

Beam	Section	Com	Defl L/	Slen	Nsd	Dir	Vsd	M	M	Combined Axial+Mom	
					----- Npl		----	----	----	Loc.	Over.
1	UC 152x152x23	1	9999	97	-0.14	MJ	0.00	0.02	0.02	0.09	0.16
2	UC 152x152x23	1	1861	97	-0.38	MJ	0.01	0.13	0.13	0.34	0.53
3	UC 152x152x23	1	876	97	-0.63	MI	0.00	0.03	0.00	0.60	0.88
						MJ	0.00	0.01	0.01		
4	UC 152x152x23	1	1204	97	-0.17	MJ	0.02	0.21	0.21	0.29	0.37
						MI	0.00	0.02	0.00		
5	UC 152x152x23	1	1687	78	-0.08	MJ	0.05	0.35	0.35	0.42	0.43
						MI	0.00	0.02	0.00		
6	UC 152x152x30	1	987	76	-0.17	MJ	0.07	0.37	0.37	0.39	0.62
						MI	0.01	0.26	0.00		
7	UC 152x152x30	1	932	76	-0.27	MJ	0.07	0.26	0.26	0.36	0.68
						MI	0.01	0.28	0.00		
8	UC 152x152x23	1	1210	78	-0.04	MJ	0.03	0.26	0.26	0.28	0.29
9	UC 152x152x23	1	9999	97	-0.59	MI	0.00	0.00	0.00	0.28	0.60
10	UC 152x152x23	1	9999	89	-0.35	MI	0.00	0.00	0.00	0.19	0.35
12	UC 152x152x23	1	9999	97	-0.29	MI	0.00	0.00	0.00	0.14	0.29
13	UC 152x152x23	1	9999	89	0.00	MI	0.00	0.00	0.00	0.00	0.00
14	UB 178x102x19	1	507	0	0.02	MJ	0.15	0.38	0.00	0.29	0.00
						MI	0.01	0.15	0.00		
15	UC 152x152x23	1	1825	0	0.01	MJ	0.11	0.22	0.00	0.32	0.00
						MI	0.00	0.09	0.00		

Results Summary Table

Beam	Section	Com	Defl L/	Slen	Nsd ----- Npl	Dir	Vsd ---- Vpl	M ---- Mc	M ---- Mb	Combined Axial+Mom	
										Loc.	Over.
16	UC 152x152x23	1	428	0	0.00	MJ	0.28	0.47	0.00	0.59	0.00
						MI	0.00	0.11	0.00		
17	UB 305x102x28	1	811	167	-0.05	MJ	0.32	0.80	0.95	0.69	0.98
						MI	0.01	0.05	0.00		
18	UC 152x152x23	1	493	94	-0.01	MJ	0.23	0.38	0.39	0.43	0.44
						MI	0.00	0.05	0.00		
19	UC 152x152x23	1	1558	84	0.00	MJ	0.11	0.14	0.14	0.14	0.14
21	UB 356x127x33	1	396	0	0.00	MJ	0.23	0.78	0.00	0.60	0.00
23	UB 305x102x25	1	1490	0	0.00	MJ	0.26	0.79	0.00	0.63	0.00
24]]CHANNELS381x10	1	608	33	0.00	MJ	0.12	0.41	0.41	0.41	0.41
						MI	0.00	0.01	0.00		
28	UB 406x140x39	1	436	0	0.00	MJ	0.25	0.58	0.00	0.33	0.00
30	UB 457x152x60	1	407	121	0.00	MJ	0.23	0.60	0.71	0.36	0.71
32	UB 305x102x25	1	425	0	0.00	MJ	0.14	0.50	0.00	0.25	0.00
33	UC 203x203x46	1	504	88	0.00	MJ	0.13	0.30	0.32	0.09	0.32
34	UC 152x152x23	1	9999	11	0.04	MJ	0.01	0.01	0.01	0.06	0.01
						MI	0.00	0.01	0.00		
36	UC 152x152x23	1	1584	85	0.00	MJ	0.11	0.14	0.14	0.14	0.14
38	UC 152x152x23	1	478	91	0.00	MJ	0.12	0.35	0.37	0.35	0.37



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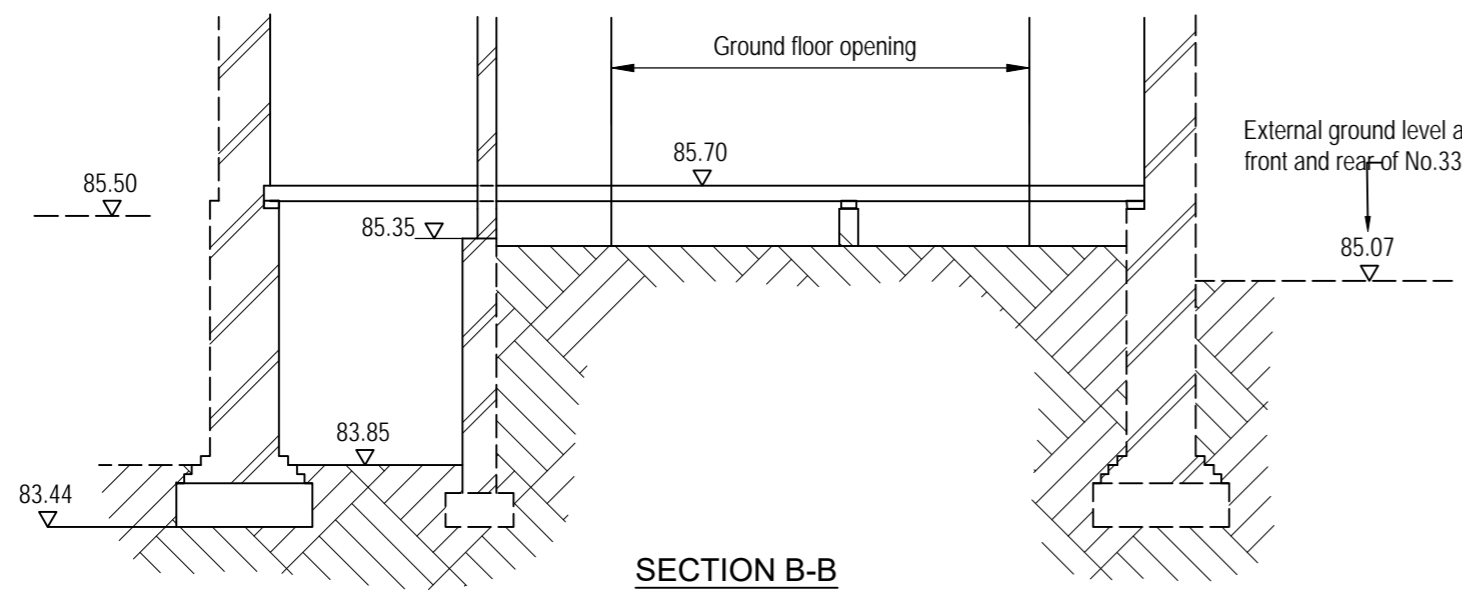
31 WILLOUGHBY ROAD LONDON NW3 1RT
 PROPOSED BASEMENT EXTENSION

EXISTING SITE PLAN AND SECTIONS

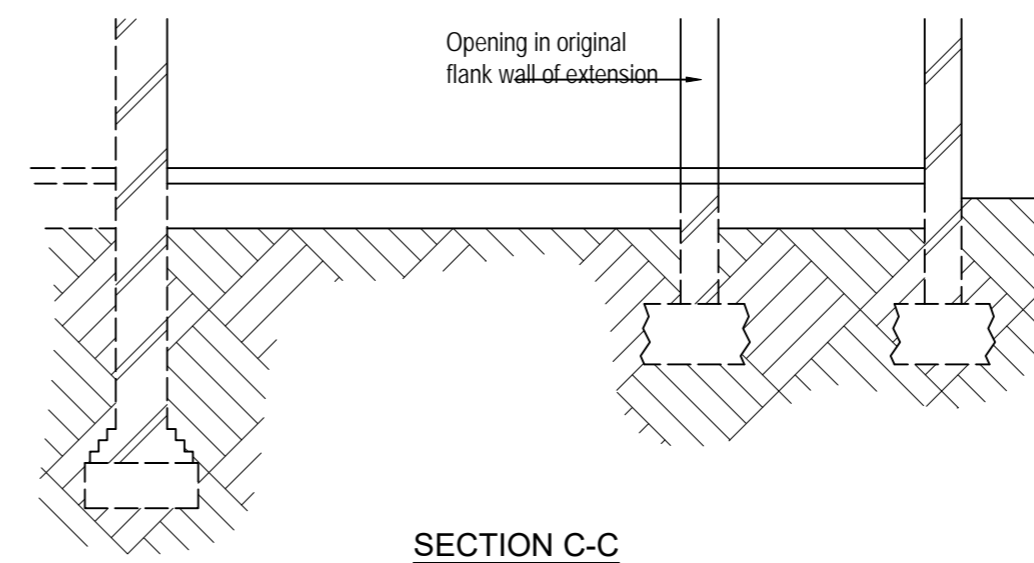
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GENERAL NOTES

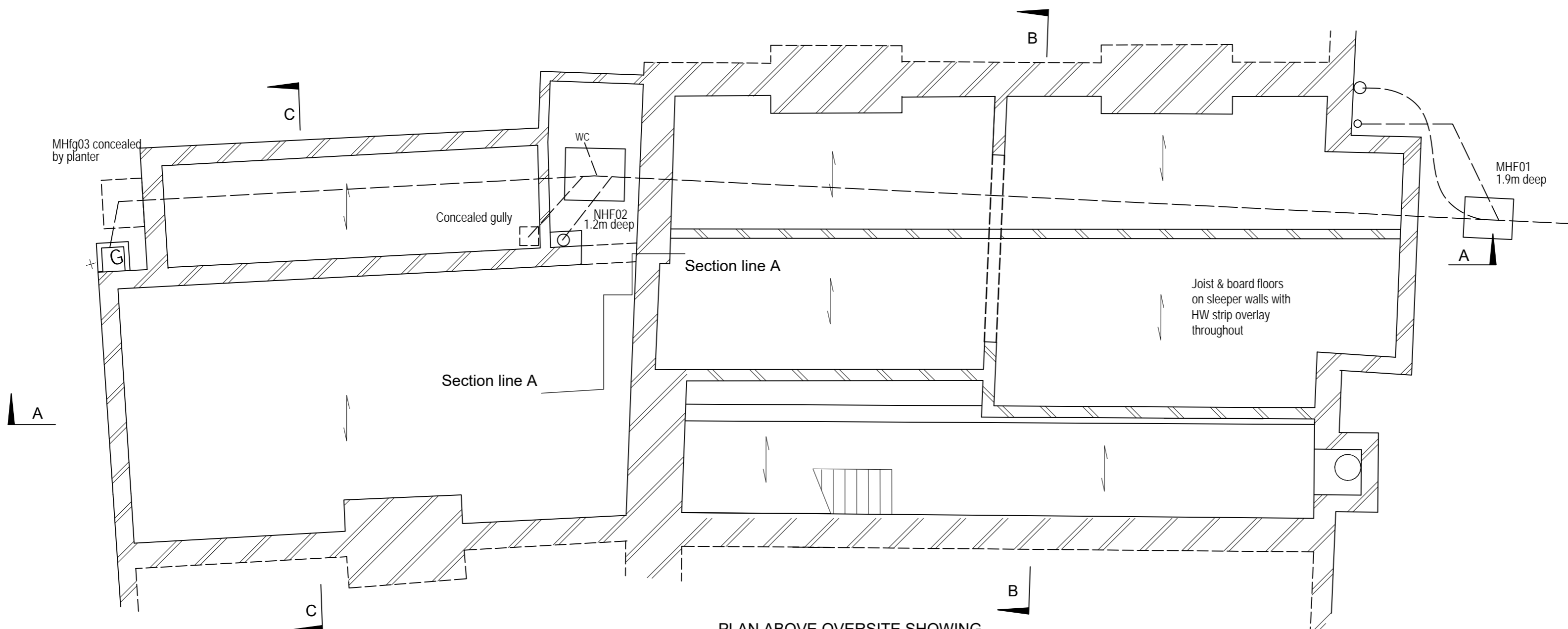
- 1 This drawing is based upon a topographical survey made by Blueprint Surveys Ltd in 2014 and referenced BPS1195, and site inspection. Broken lines indicate what are considered to be the probable outlines of construction features not visible during survey or inspection.
- 2 Foundation depths have been taken from trial pit records or have been assessed provisionally by reference to the geotechnical investigation records. Where the party wall and external wall thicknesses are not evident from the survey or currently measurable they, together with dimensions of spread footings, have been determined by reference to the 1894 London Building Act.



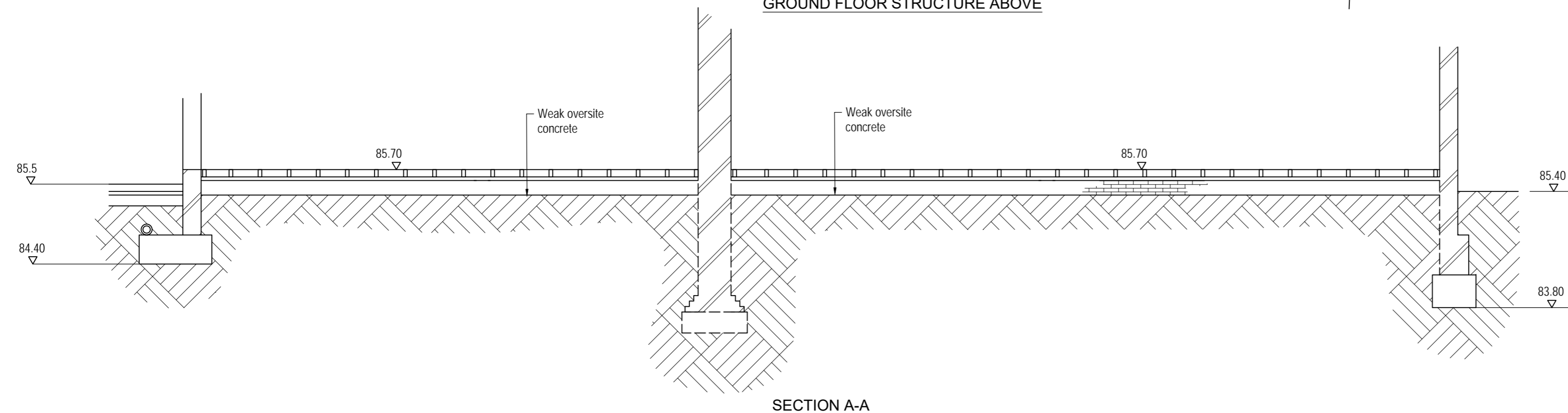
SECTION B-B



SECTION C-C



PLAN ABOVE OVERSITE SHOWING GROUND FLOOR STRUCTURE ABOVE

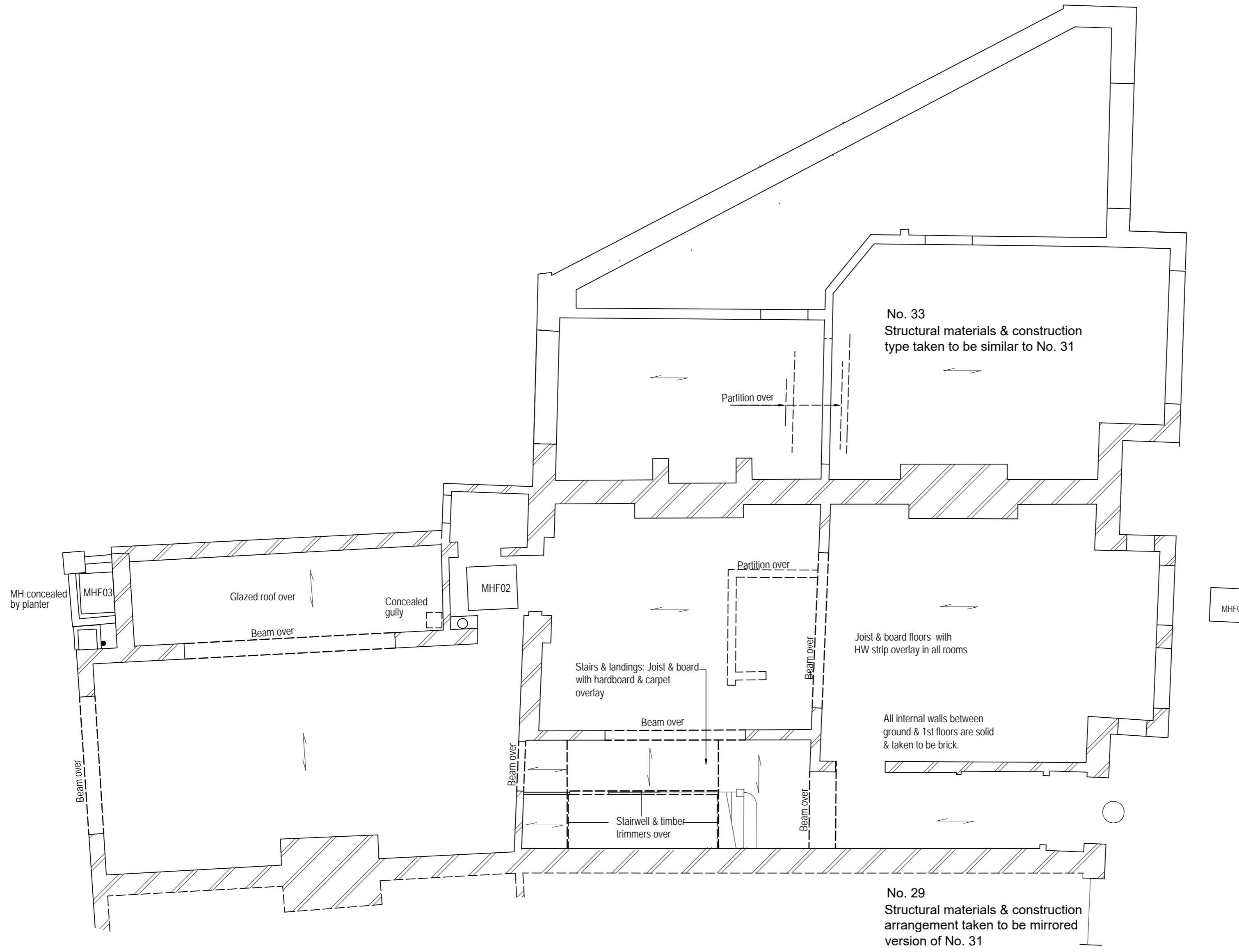


SECTION A-A

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31 WILLOUGHBY ROAD LONDON NW3 1RT PROPOSED BASEMENT EXTENSION		
EXISTING SUB GROUND FLOOR PLAN AND SECTIONS		
Scale:	Date:	Drawing ref.:
1:50	03/19	G1808-PA-002-E1
Scale refers to paper size:	A2	

GENERAL NOTES

- This drawing is based upon a topographical survey made by Blueprint Surveys Ltd in 2014 and referenced BPS1195 and site inspection. Broken lines indicate what are considered to be the probable outlines of construction features not visible during survey or inspection.



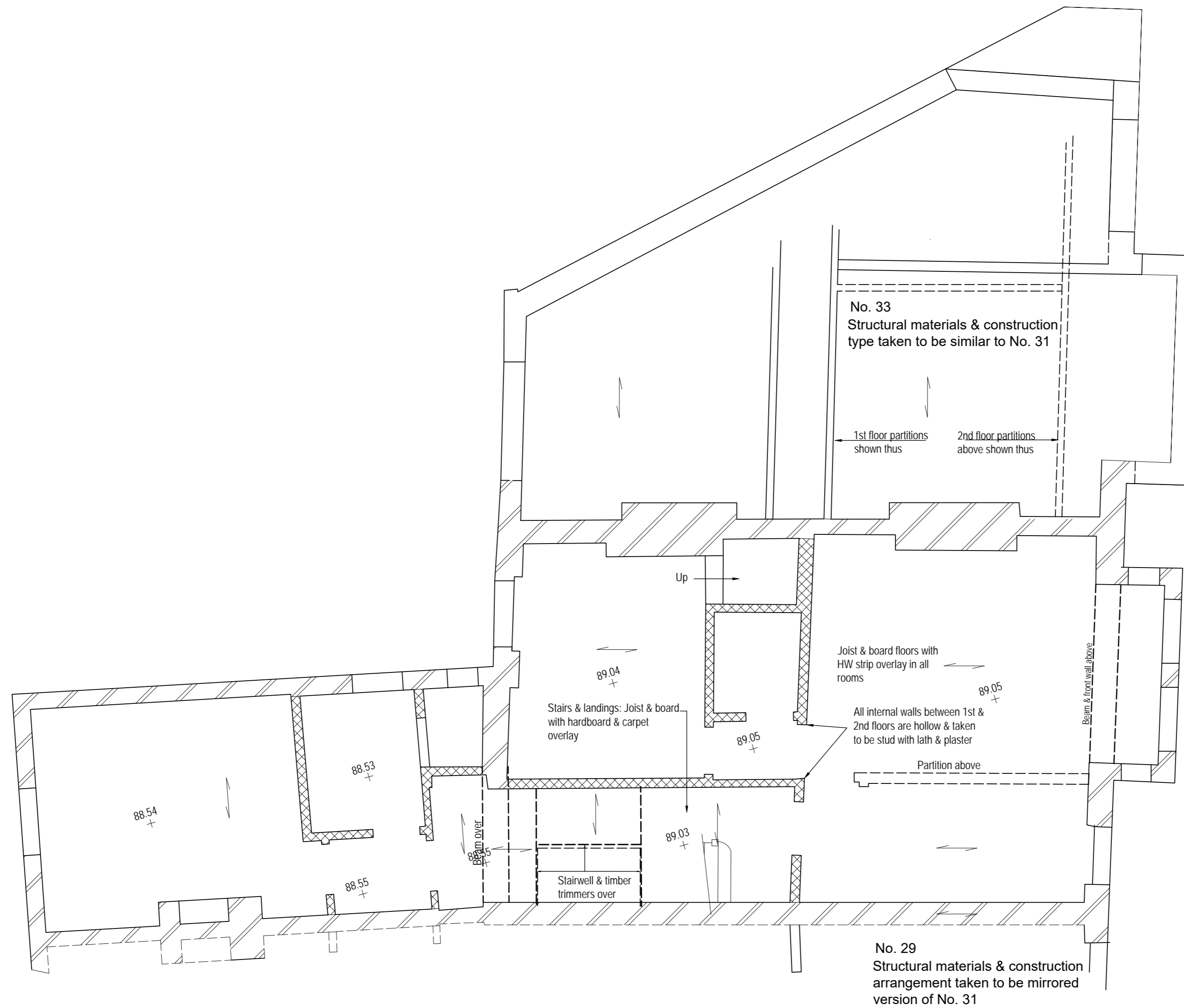
GROUND FLOOR PLAN SHOWING
FIRST FLOOR STRUCTURE ABOVE



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31 WILLOUGHBY ROAD LONDON NW3 1RT PROPOSED BASEMENT EXTENSION		
EXISTING GROUND FLOOR PLAN SHOWING FIRST FLOOR STRUCTURE ABOVE		
Scale:	Date:	Drawing ref.:
1:50	03/19	G1808-PA-003-E1
Scale refers to paper size:	A2	

GENERAL NOTES

1 This drawing is based upon a topographical survey made by Blueprint Surveys Ltd in 2014 and referenced BPS1195 and site inspection. Broken lines indicate what are considered to be the probable outlines of construction features not visible during survey or inspection.



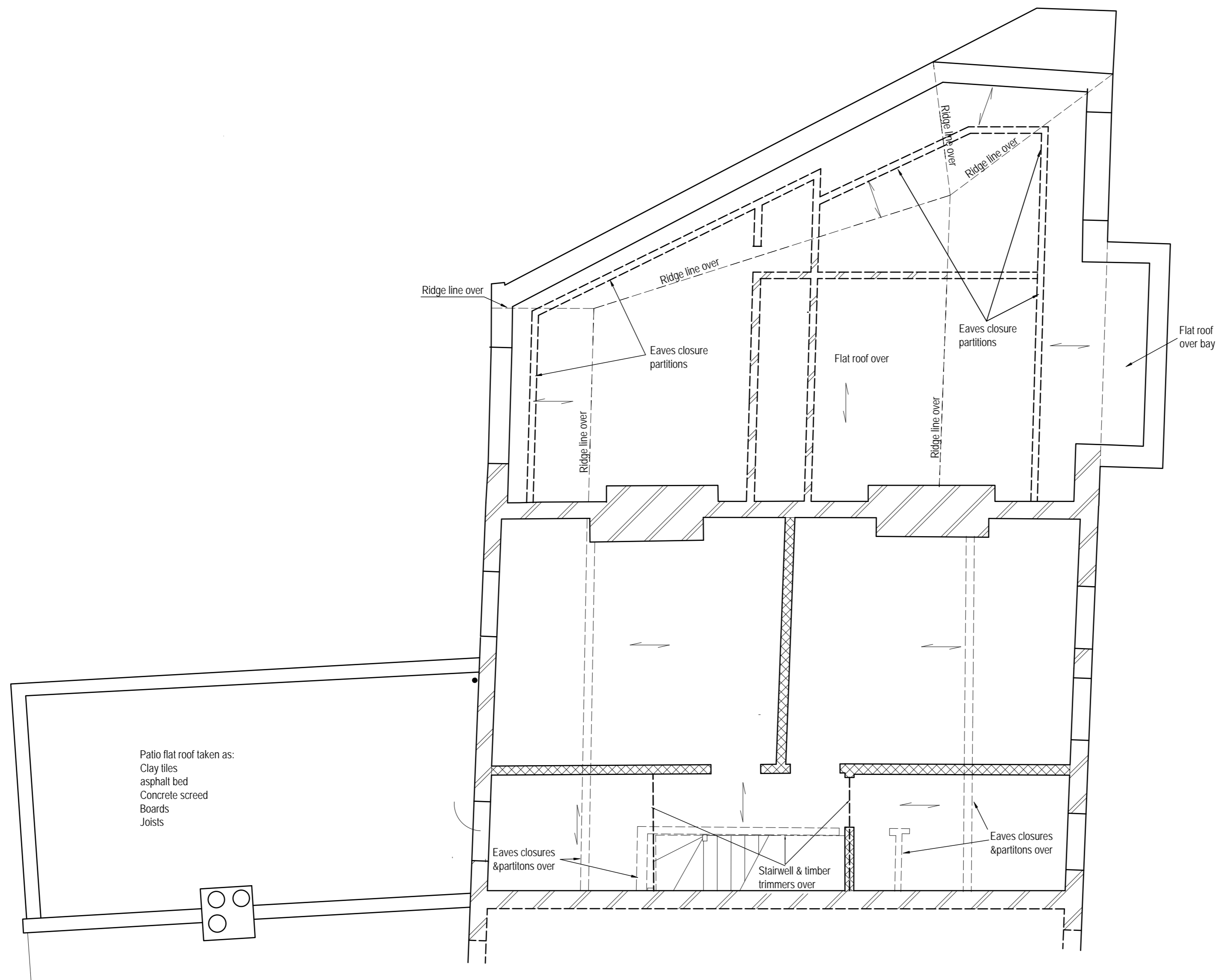
FIRST FLOOR PLAN SHOWING
SECOND FLOOR STRUCTURE ABOVE



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31 WILLOUGHBY ROAD LONDON NW3 1RT PROPOSED BASEMENT EXTENSION		
EXISTING FIRST FLOOR PLAN SHOWING SECOND FLOOR STRUCTURE ABOVE		
Scale. 1:100, 1:50	Date 03/19	Drawing ref. G1808-PA-004-E1
Scale refers to paper size: A2		

GENERAL NOTES

1 This drawing is based upon a topographical survey made by Blueprint Surveys Ltd in 2014 and referenced BPS1195 and site inspection. Broken lines indicate what are considered to be the probable outlines of construction features not visible during survey or inspection.



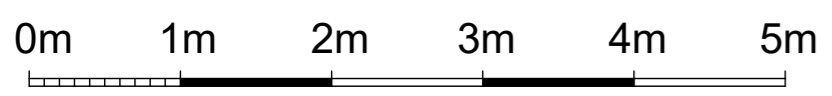
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31 WILLOUGHBY ROAD LONDON NW3 1RT
 PROPOSED BASEMENT EXTENSION

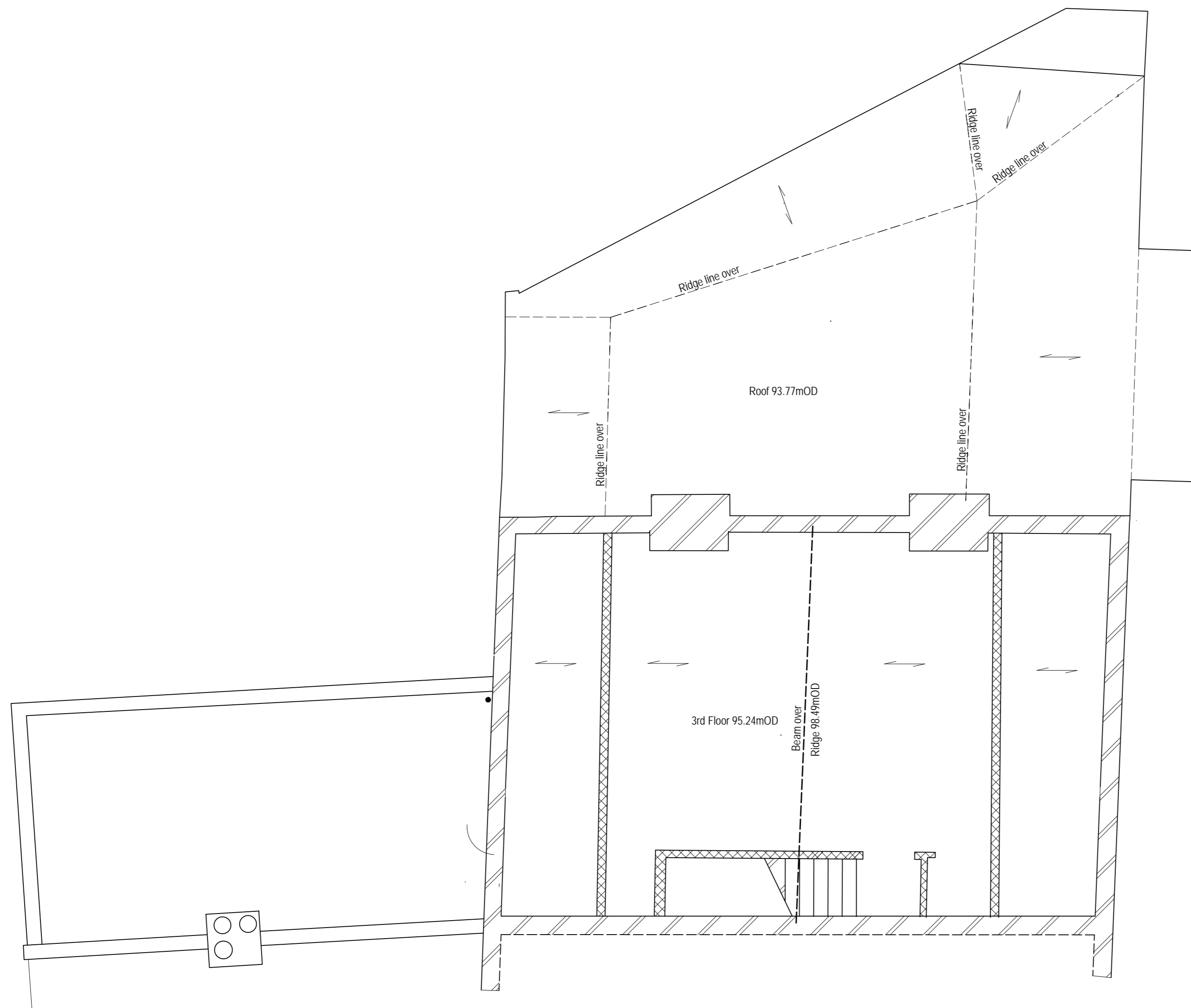
EXISTING SECOND FLOOR PLAN SHOWING
 STUDY FLOOR STRUCTURE ABOVE

Scale. 1:100, 1:50 Scale refers to paper size:	Date 03/19	Drawing ref. G1808-PA-005-E1
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GENERAL NOTES

1 This drawing is based upon a topographical survey made by Blueprint Surveys Ltd in 2014 and referenced BPS1195 and site inspection. Broken lines indicate what are considered to be the probable outlines of construction features not visible during survey or inspection.



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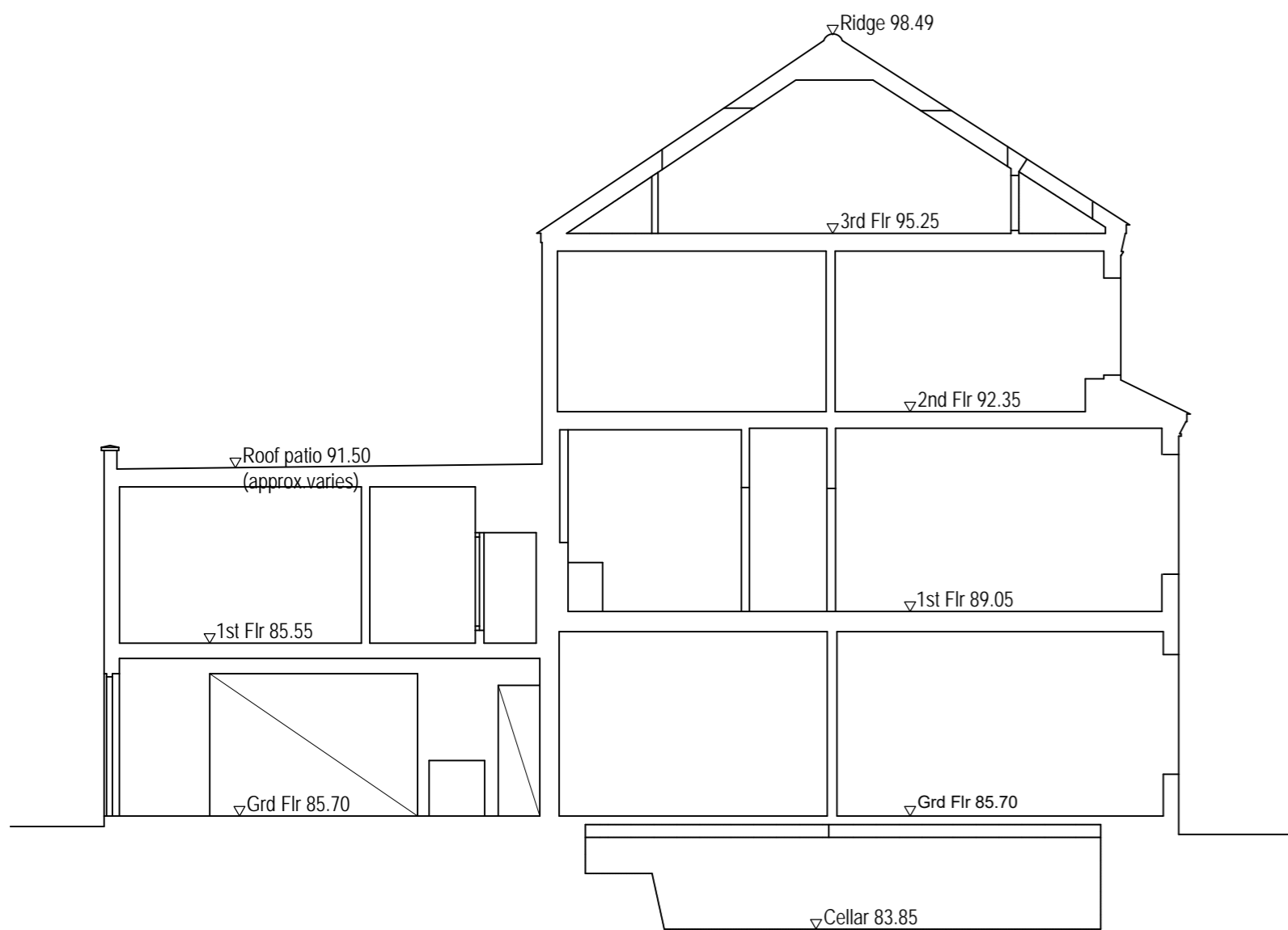
31 WILLOUGHBY ROAD LONDON NW3 1RT
 PROPOSED BASEMENT EXTENSION

EXISTING THIRD FLOOR PLAN SHOWING ROOF
 STRUCTURE ABOVE

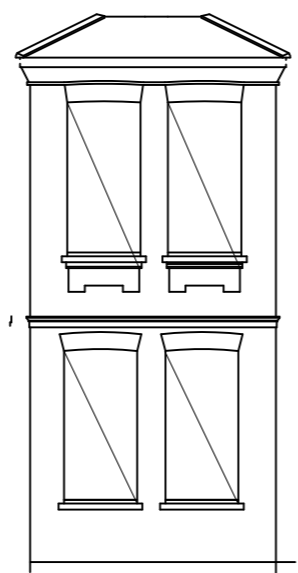
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Scale refers to paper size: A2		

GENERAL NOTES

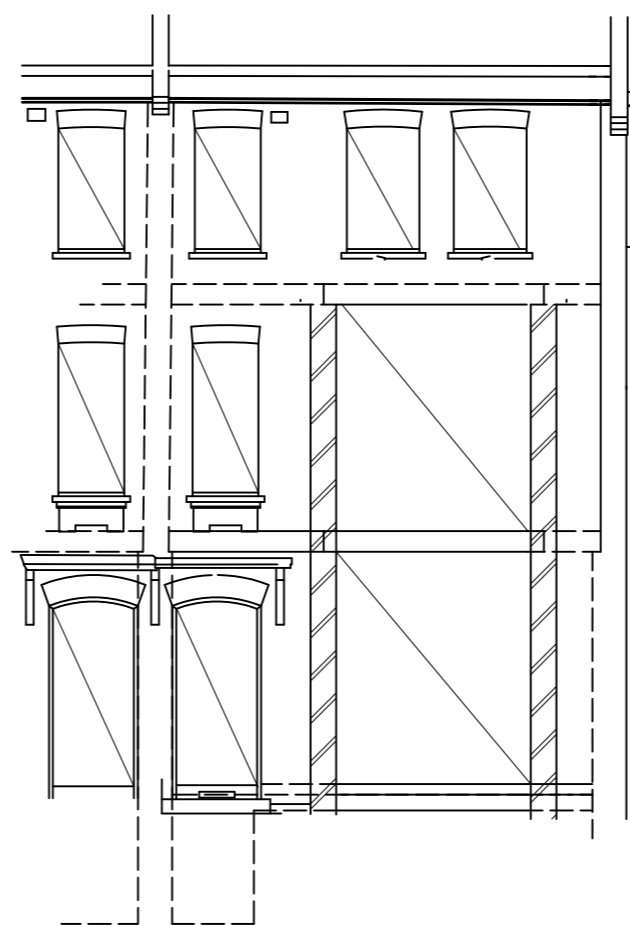
1 This drawing is based upon a topographical survey made by Blueprint Surveys Ltd in 2014 and referenced BPS1195 and site inspection.



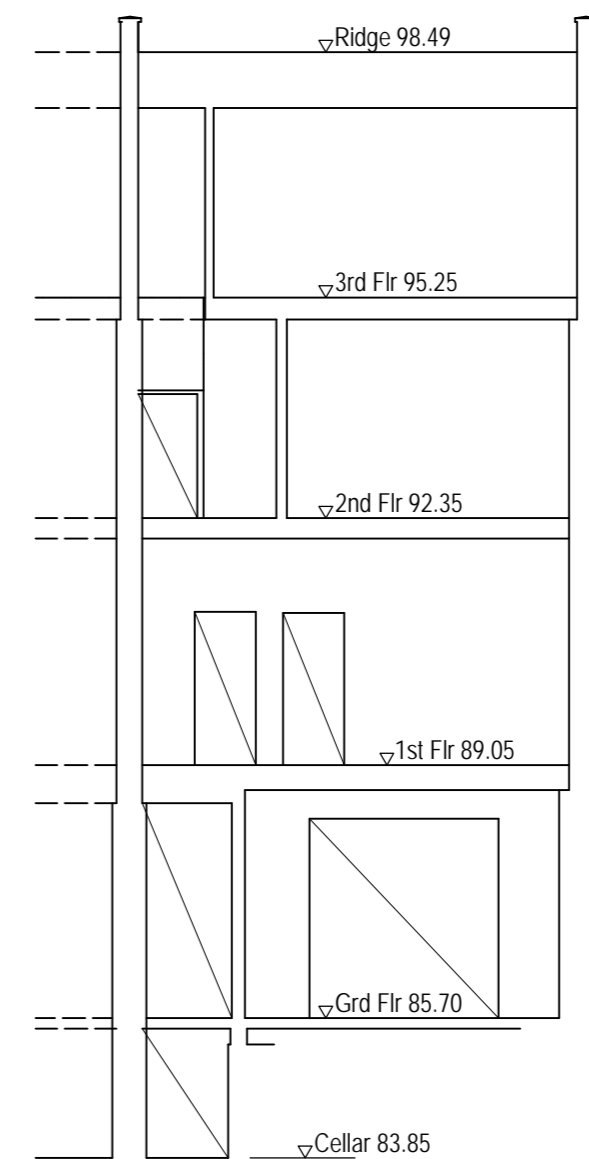
SECTION 1 - 1
1:100



ELEVATION 2 - 2
1:100

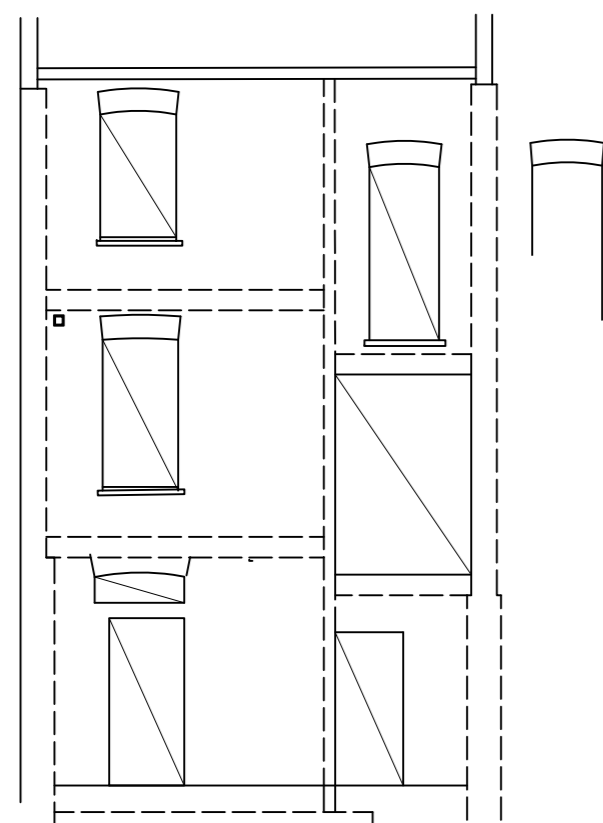


SECTION 3 - 3
1:100

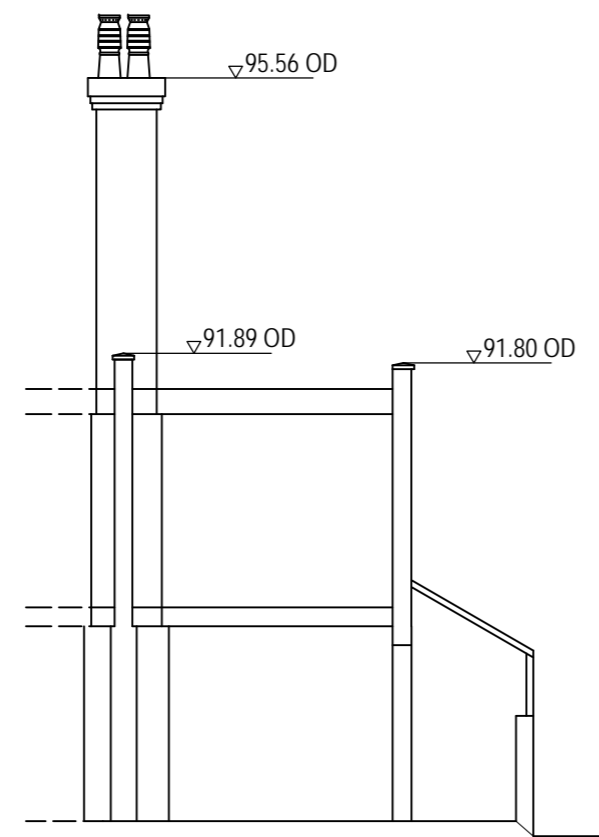


SECTION 4 - 4
1:100

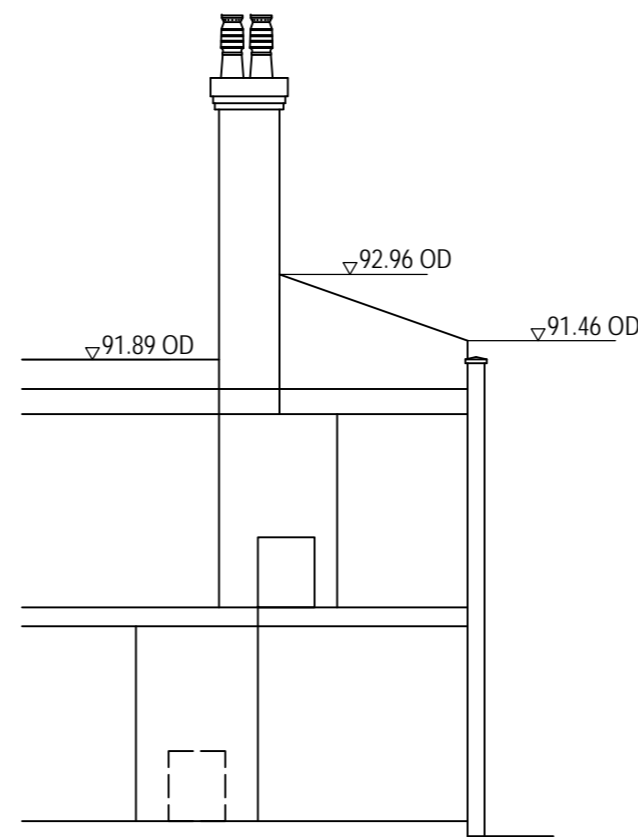
No 33 approx Flat Roof
No 33 approx 2nd. Flr.
No 33 approx 1st. Flr.
No 33 approx Grd. Flr.



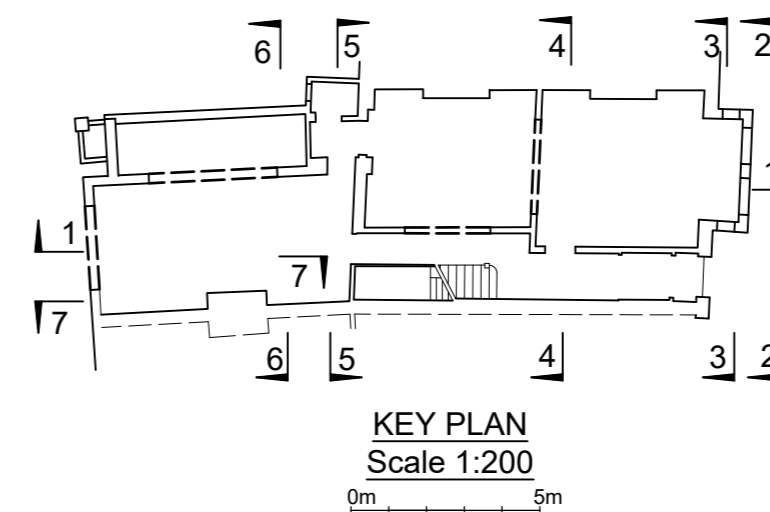
SECTION 5 - 5
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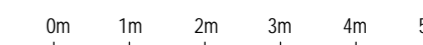
SECTION 6 - 6
1:100



SECTION 7 - 7
1:100



KEY PLAN
Scale 1:200



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31 WILLOUGHBY ROAD LONDON NW3 1RT
PROPOSED BASEMENT EXTENSION

EXISTING BUILDING SECTIONS & ELEVATIONS

Scale. 1:100 & 1:200	Date 03/19	Drawing ref. G1808-PA-007-E1
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Scale refers to paper size: A2

31 Willoughby Rd

Brick pavers on sand bed and concrete base

39 Willow Rd

31 Willoughby Rd

38 Willow Rd

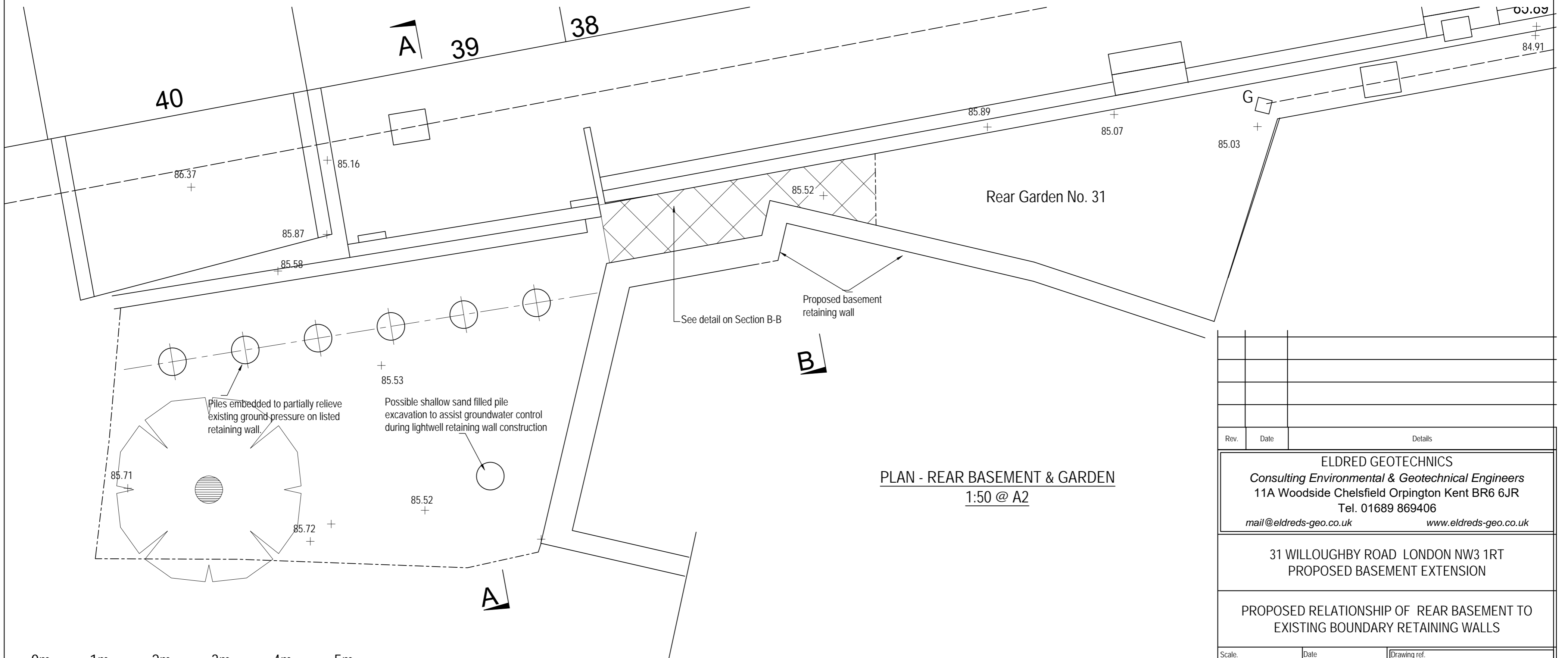
Temporary struts and walings to resist prop force of 40kN/m run of wall until basement slab constructed

BEFORE CONSTRUCTION: A trial pit is to be hand excavated to determine the existing wall profile and footing details.

CONSTRUCTION: Brace and excavate behind existing wall in short lengths, retain ground below wall footing with permeable no-fines concrete. Construct new wall & backfill with lightly compacted clay in 150mm layers.

SECTION A - A 1:50 @ A2

SECTION B - B 1:50 @ A2



PLAN - REAR BASEMENT & GARDEN
1:50 @ A2

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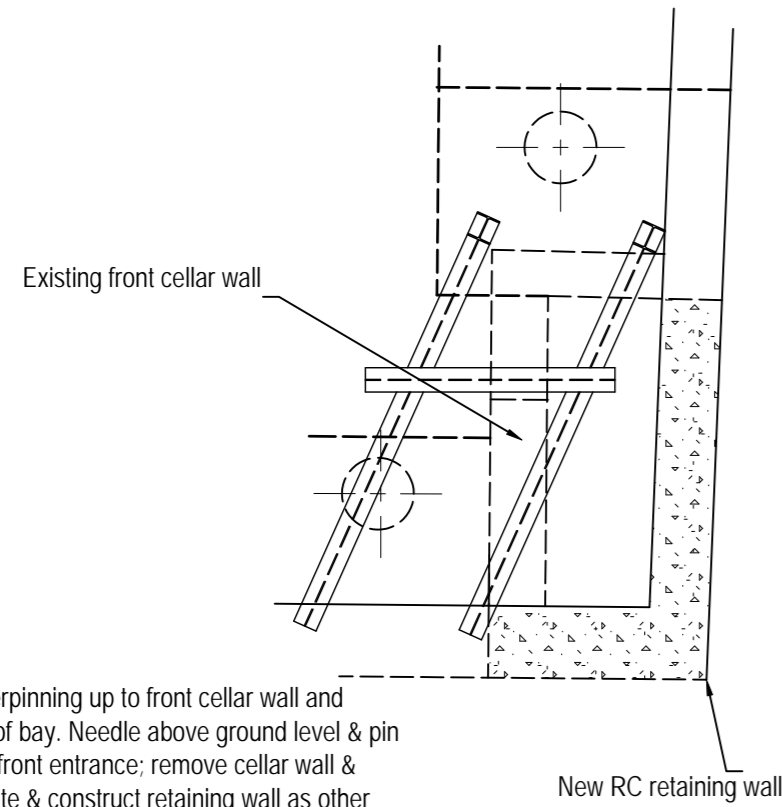
31 WILLOUGHBY ROAD LONDON NW3 1RT
 PROPOSED BASEMENT EXTENSION

PROPOSED RELATIONSHIP OF REAR BASEMENT TO
 EXISTING BOUNDARY RETAINING WALLS

Scale: 1:50	Date: 03/19	Drawing ref.: G1808-PA-101-E1
Scale refers to paper size: A2		

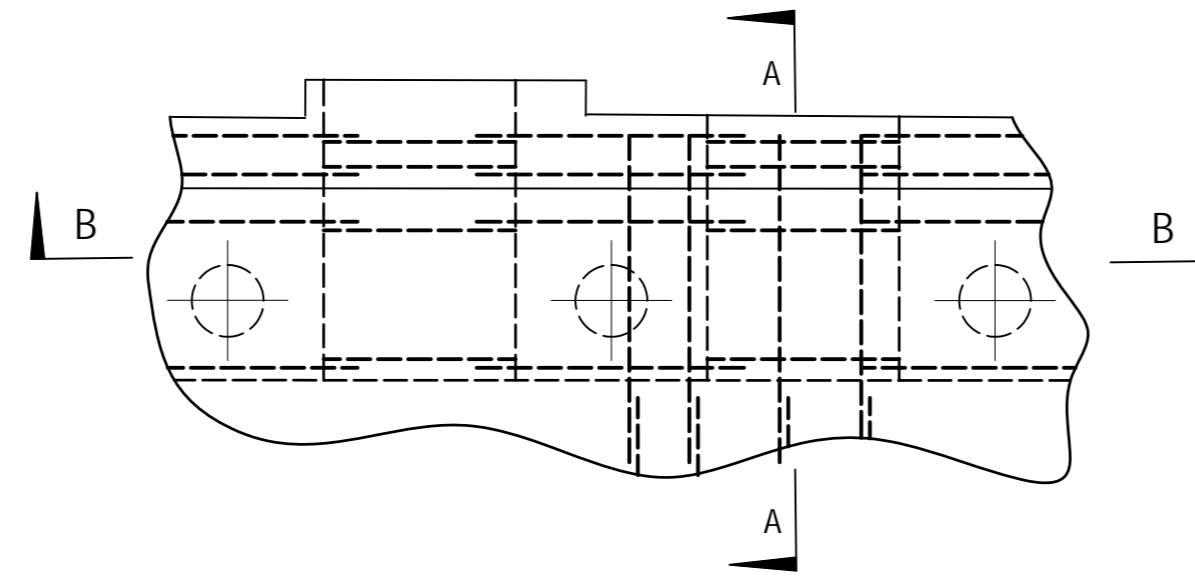
PILE INSTALLATION

- 1 All piles to be installed from mat at ground floor level: cut off level for all piles to be 0.5m minimum above soffit of basement floor slab. Steel plunge columns to be installed with guide frame, to terminate 200mm above pile mat level and to be protected.
- 2 All piles to be tested for integrity after installation and open bores to be backfilled with granular material.
- 3 Following completion of underpinning and excavation of dumping, pile heads to be cut down using non-vibratory method.



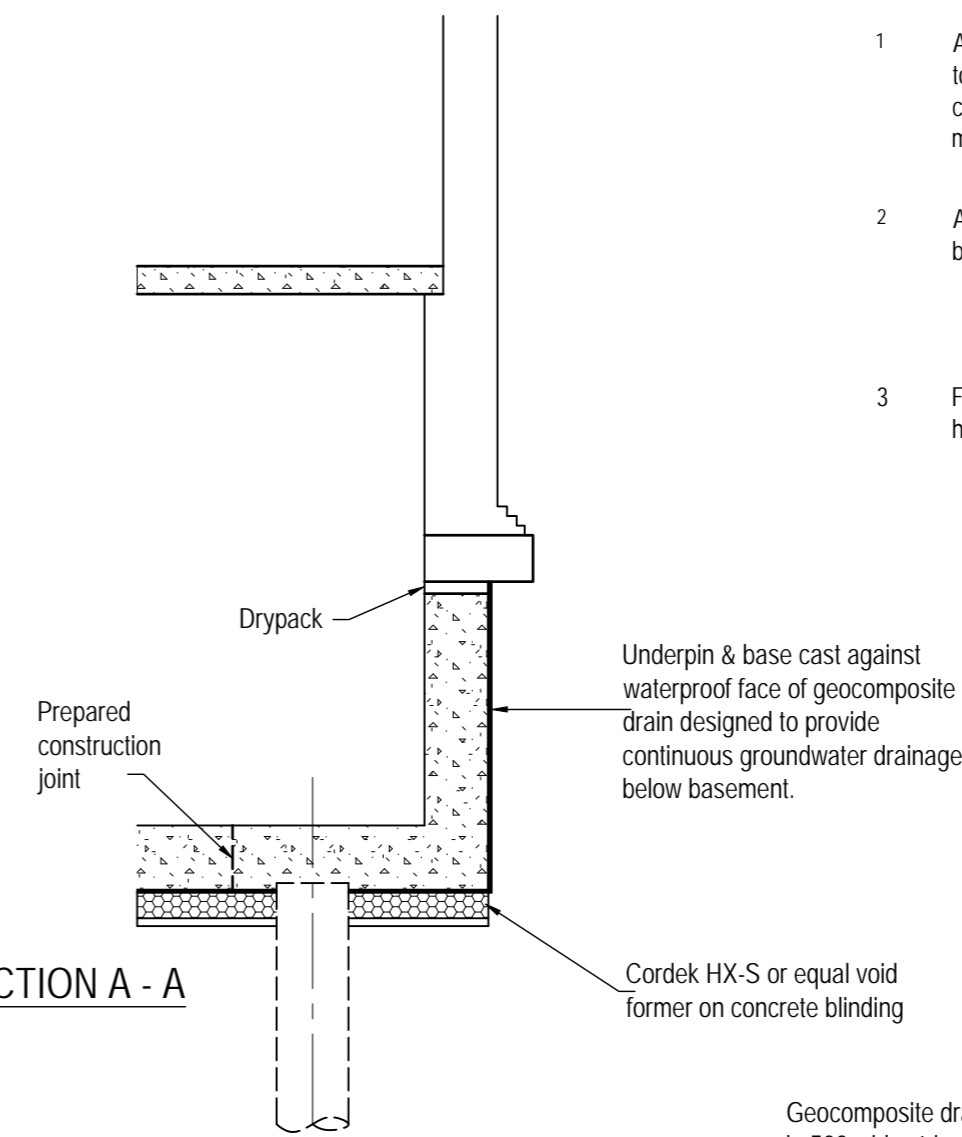
Complete underpinning up to front cellar wall and below side wall of bay. Needle above ground level & pin up wall beside front entrance; remove cellar wall & footing; excavate & construct retaining wall as other underpins. Permanent support of front entrance and side wall to be by ground floor slab.

DETAIL 1

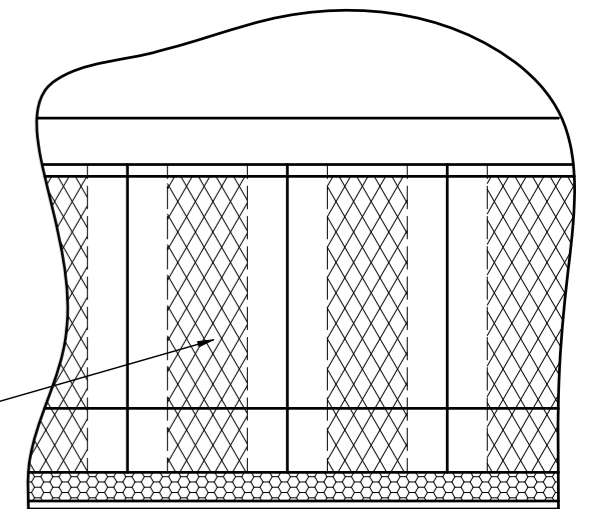


Underpinning to be carried out in 1m lengths. Type 1 pins with bases supported by piles are to be constructed first (note requirement for pile heads to be cut down without vibration) and intervening Type 2 pins are to be cast against prepared Type 1 faces. Reinforcing bars are to be lapped or to be fitted with connectors to provide a structurally continuous wall and basement floor.

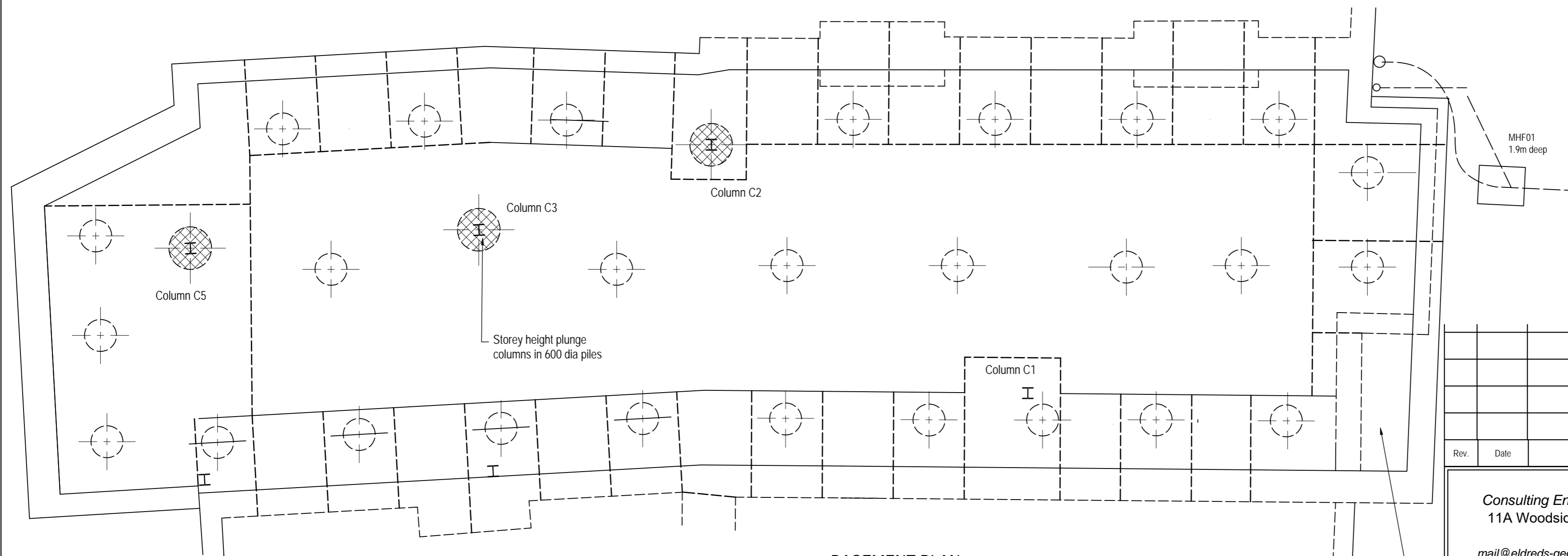
SECTION A - A



Geocomposite drains fixed in 500 wide strips and clear of construction joints



SECTION B - B



BASEMENT PLAN
Refer to drgs. G1808-PA-104 &105 for Sections A to C

Rev.	Date	Details

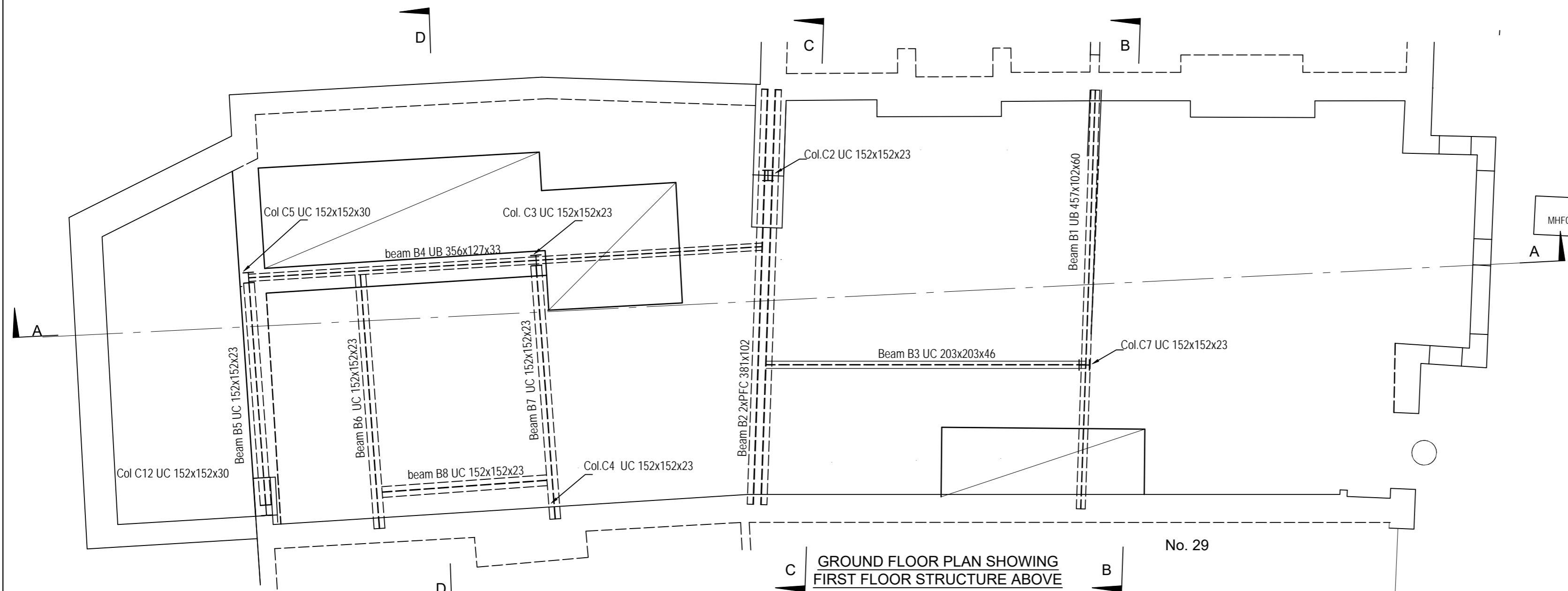
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31 WILLOUGHBY ROAD LONDON NW3 1RT
PROPOSED BASEMENT EXTENSION

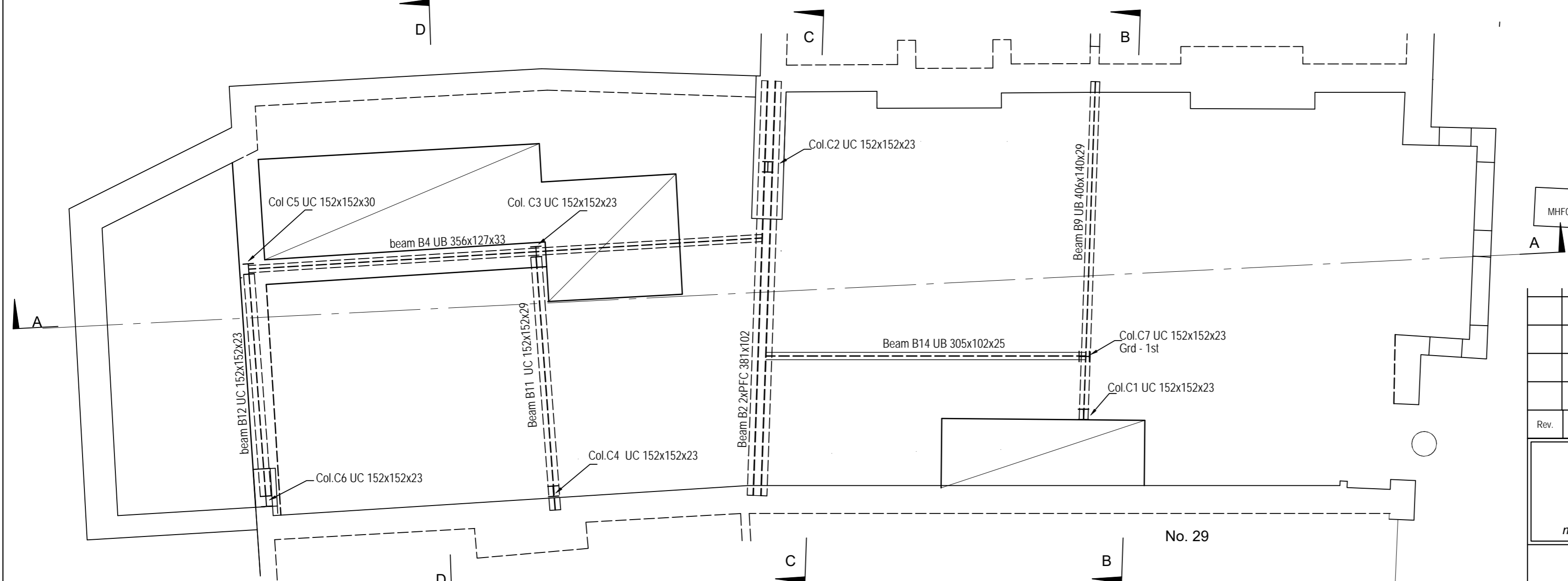
PROPOSED BASEMENT PLAN AND SECTIONS



Scale:	Date:	Drawing ref.:
1:50	03/19	G1808-PA-102-E1
Scale refers to paper size:	A2	



GROUND FLOOR PLAN SHOWING FIRST FLOOR STRUCTURE ABOVE



GROUND FLOOR PLAN SHOWING GROUND FLOOR STEEL BELOW



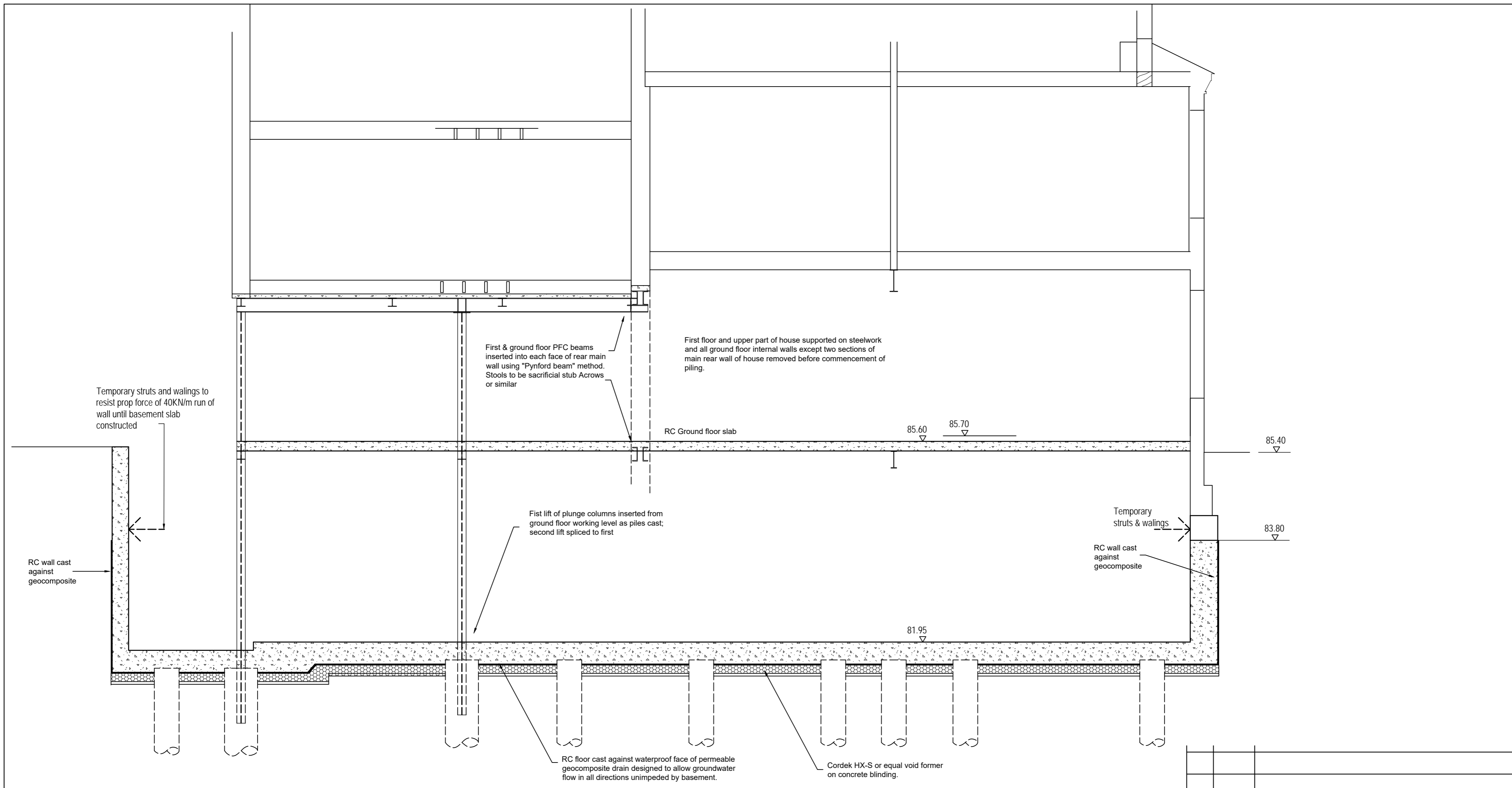
Rev.	Date	Details

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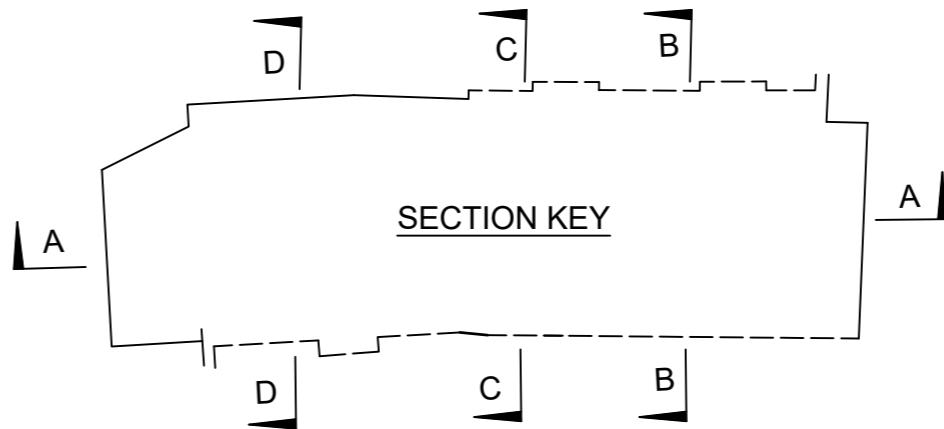
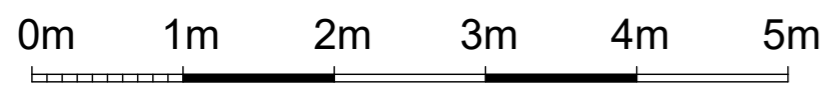
31 WILLOUGHBY ROAD LONDON NW3 1RT
 PROPOSED BASEMENT EXTENSION

GROUND FLOOR PLANS
 SHOWING GROUND AND FIRST FLOOR STRUCTURE

Scale: 1:100, 1:50	Date: 03/19	Drawing ref. G1808-PA-103-E1
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SECTION A-A



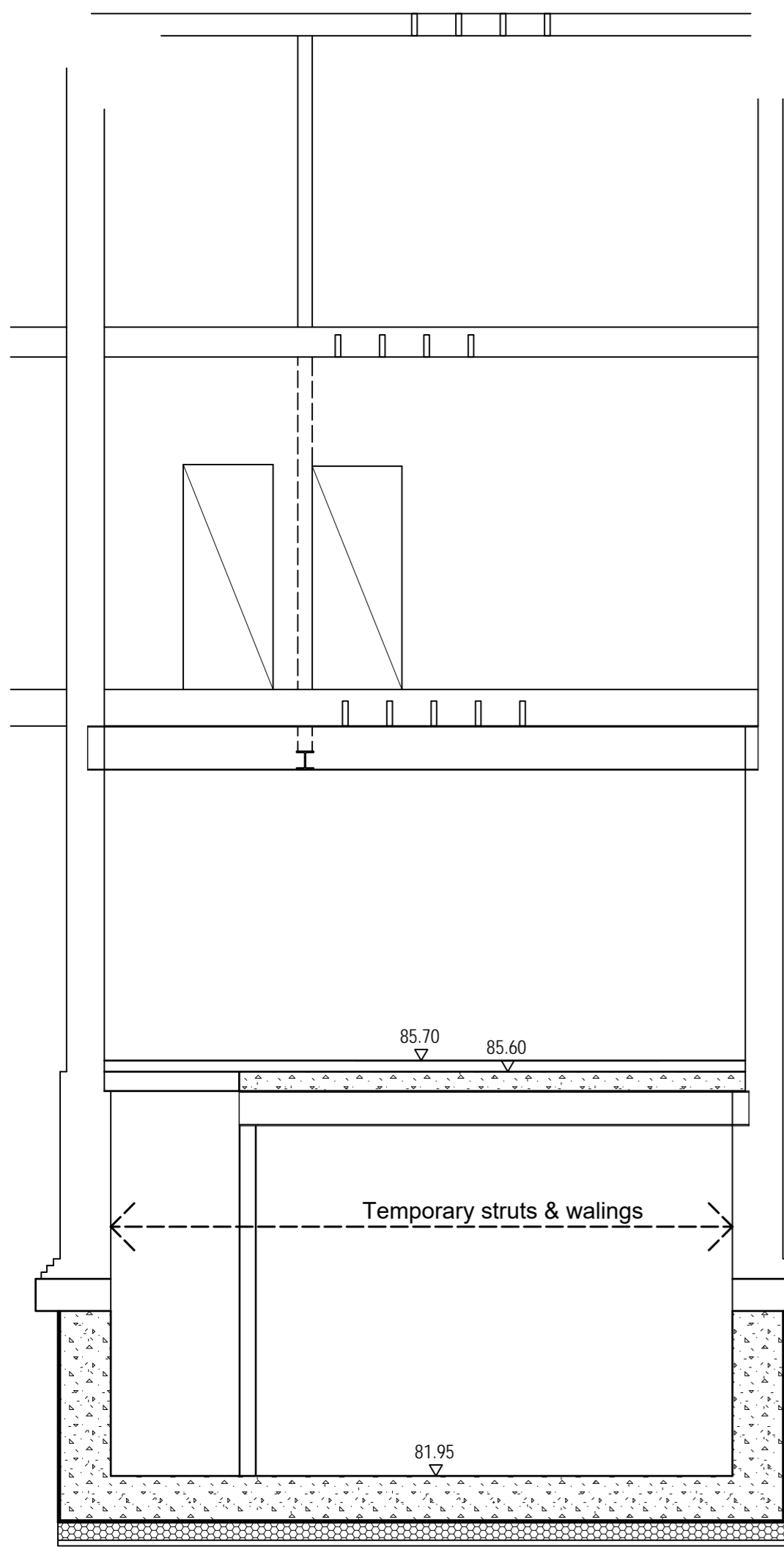
Rev.	Date	Details

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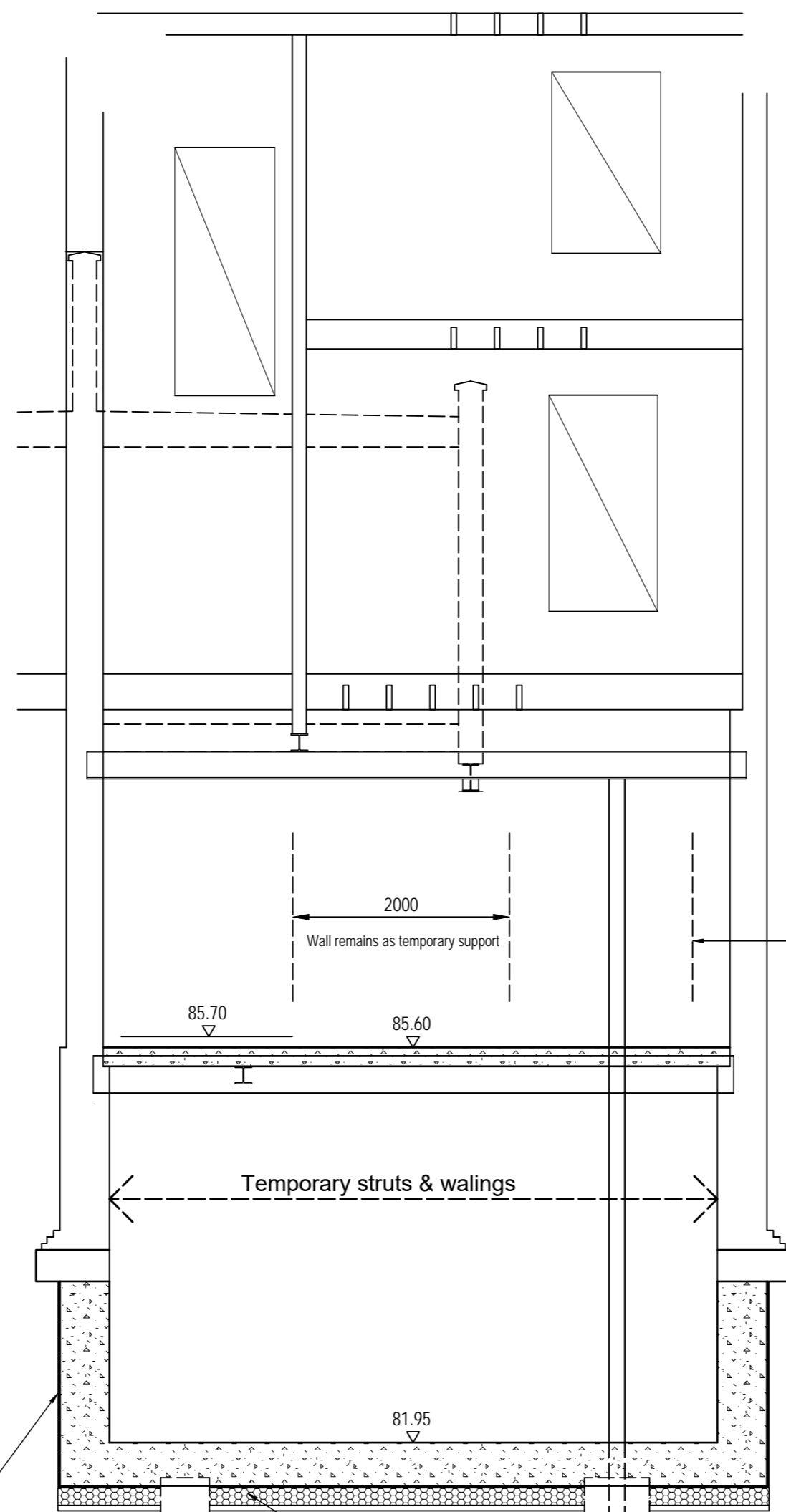
31 WILLOUGHBY ROAD LONDON NW3 1RT
 PROPOSED BASEMENT EXTENSION

PROPOSED GENERAL SECTION A - A

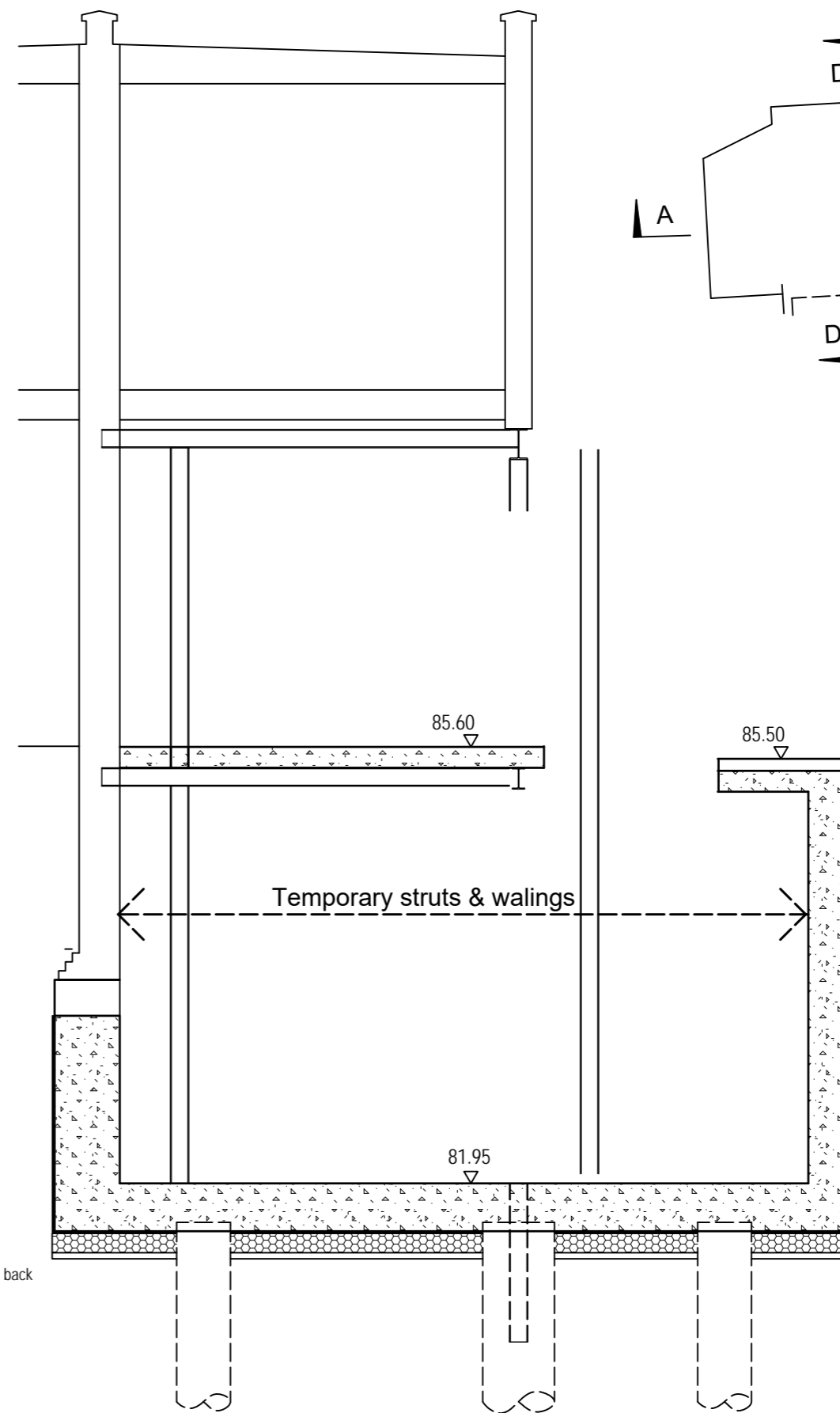
Scale. 1:50	Date 03/19	Drawing ref. G1808-PA-104-E1
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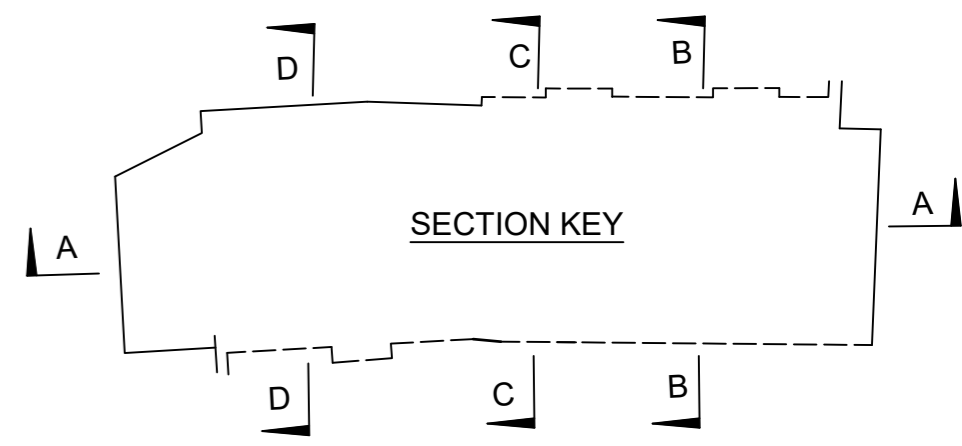
SECTION B-B



SECTION C-C



SECTION D - D



External ground level at front and rear of No.33

85.50

85.07

Temporary struts & walings

RC walls cast against waterproof face of permeable geocomposite drain designed to allow groundwater flow unimpeded by basement.

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31 WILLOUGHBY ROAD LONDON NW3 1RT
PROPOSED BASEMENT EXTENSION

PROPOSED GENERAL CROSS SECTIONS



Scale:	Date:	Drawing ref.:
1:50	03/19	G1808-PA-105-E1
Scale refers to paper size:	A2	

Appendix E Contents

Preliminary geotechnical design report

Figure 14 – Plot of derived shear strengths and characteristic profile

Figure 15 – Temporary drawdown effect of construction dewatering

Figure 16 – FLAC model geometry

Figure 17 – FLAC analysis lateral displacement undrained

Figure 18 – FLAC analysis lateral displacement drained

Figure 19 – FLAC analysis vertical displacement undrained

Figure 20 – FLAC analysis vertical displacement drained

Figure 21 – FLAC analysis lateral total stress undrained

Figure 22 – FLAC analysis lateral total stress drained

Figure 23 – FLAC analysis vertical total stress undrained

Figure 24 – FLAC analysis vertical total stress drained

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PROPOSED BUILDINGS: Refer to current editions of drawings G1808-GA-102 to 105

Front part of basement: preliminary estimate of unfactored loads imposed at basement floor soffit level (81.50 OD)

<u>Item</u>	<u>Permanent</u>	<u>Variable</u>
Existing: No.29 party wall	126.06	9.40
Existing: No.33 party wall	152.36	4.95
New; 2 No.300 RC party walls 1.5m high	21.60	
New; 450mm basement floor slab 6.5m wide	70.20	
New; basement floor finish	8.85	
New; basement floor variable		8.85
New 175mm ground floor slab	24.78	
New; ground floor finish	8.85	
New; ground floor variable		8.85
Total unfactored loads/m length of basement	412.69	32.05 KN/m
For preliminary purposes assume all load carried by piles close to external walls; piles @ 2m c/c		
SLS Loads/pile	412.69	32.05 KN/m
DA1 Comb A1	<u>557.14</u>	<u>48.08</u> KN/m
DA1 Comb A2	<u>412.69</u>	<u>41.67</u> KN/m

Rear part of basement: unfactored loads imposed at basement floor soffit level (81.50 OD)

<u>Item</u>	<u>Permanent</u>	<u>Variable</u>
Existing: No.29 party wall	91.46	10.50 KN/m
Other loads as front/2	<u>67.14</u>	<u>8.85</u> KN/m
Total unfactored loads/m length of basement	158.60	19.35 KN/m
For preliminary purposes assume all load carried by piles close to external walls; piles @ 2m c/c		
SLS Loads/pile	158.60	19.35 KN/m
DA1 Comb A1	<u>214.11</u>	<u>29.03</u> KN/m
DA1 Comb A2	<u>158.60</u>	<u>25.16</u> KN/m

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Preliminary assessment of Pile Capacity

11m pile below basement soffit. 450 dia. Front. Refer to Cu profile Figure 14

Load	DA1 Comb. 2 =	Comp	454 KN	Tension	247 KN				
	Pile dia m.	Perimeter m.	α	Section length m	Cu	γ_{Cu}	Resistance		
Shaft	0.45	1.41	0.50	11.00	129.00	1.40	716.54	KN	
End	CSA	0.16	9.00		196.00	1.40	201.60	KN	
							Total	918.14	KN
Resistance factors	R4 Comp	2.02	R4 Tens	2.90	>2 Adequate				

	DA1 Comb. 1 =		605 KN	Tension	333 KN				
	Pile dia m.	Perimeter m.	α	Section length m	Cu	γ_{Cu}	Resistance		
Shaft	0.45	1.41	0.50	11.00	129.00	1.00	1003.16	KN	
End	CSA	0.16	9.00		196.00	1.00	282.24	KN	
								1285.40	KN
Resistance factors	R1 Comp	2.12	R1 Tens	3.01	>1 Adequate				

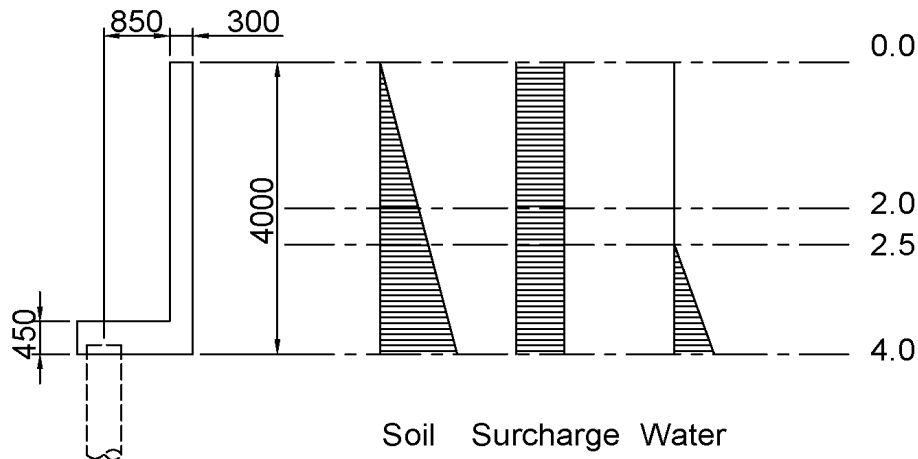
11m pile below basement soffit. 300 dia. Rear. Refer to Cu profile Figure 14

	DA1 Comb. 2 =		184 KN	Tension	247 KN				
	Pile dia m.	Perimeter m.	α	Section length m	Cu	γ_{Cu}	Resistance		
Shaft	0.30	0.94	0.50	11.00	129.00	1.40	477.70	KN	
End	CSA	0.07	9.00		196.00	1.40	88.20	KN	
								565.90	KN
Resistance factors	R4 Comp	3.08	R4 Tens	1.93	>=2 Adequate				

	DA1 Comb. 1 =		243 KN	Tension	333 KN				
	Pile dia m.	Perimeter m.	α	Section length m	Cu	γ_{Cu}	Resistance		
Shaft	0.30	0.94	0.50	11.00	129.00	1.00	668.77	KN	
End	CSA	0.07	9.00		196.00	1.00	123.48	KN	
								792.25	KN
Resistance factors	R1 Comp	3.26	R1 Tens	2.01	>1 Adequate				

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Preliminary check on stability of cantilever retaining wall in rear extension - short term condition



Soil	γ_{sat}	18.00 KN/m ³
Conc.	γ	24.00 KN/m ³

< int. friction	ϕ'	25.00 deg.
Cohes.	c'	0.00 Kpa

Ka	0.41 frac'n
----	-------------

DA1	Char.	A1	A2		A1	A2	A1	A2
Action	Pv	Pah	Pah	Arm	M O/T	M O/T	MR	MR
Soil	72.00	40	30	1.33	53	39		
Surch	10.00	25	21	2.00	49	43		
Water	7.50	10	8	0.50	5	4		
Stem	28.80			1.00			28.80	28.80
Base	9.18			0.43			3.90	3.90
					107.27	85.65	32.70	32.70

Resistance factors R1/A1 0.30 R1/A2 0.38 Inadequate.

Provide struts 1.5m from top of wall ULS force/m run = (107.27-32.7)/2.5 = 29.83 KN/m

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Preliminary assessment of impact of dewatering for reconstruction

Settlement due to construction dewatering. Refer to Figure 14

The computed estimate of ground movement has been made at this stage by a "dry" analysis using the undrained and drained bulk moduli to avoid the need of a coupled analysis. This prevents inclusion of the effect of pore water tension in the calculation.

Dewatering for a limited period will cause the phreatic surface to recede from the excavation face. Walls of adjoining buildings are approximately 5m from the excavation and the potential for excessive differential settlement is examined for the zone above insitu London Clay. For this zone:

$E_u = 4500$; $E_{u \text{ ave}} = 20350$ Kpa. Void ratio $e = 0.6$ (lab tests); $D_{10} = 0.002$ mm (labtests); range of Terzaghi & Peck [6] C constant 0.1 to 0.5.

Capillary pwp tension capacity in range of $-(0.1 \text{ to } 0.5)/(0.6 \cdot 0.002) = -100 \text{ to } -400$ KPa

	Depth m	Height ODN	pwp Kpa		
			Exist'g	Const'n	Change
Ground level	0.00	85.50			
Assumed top of capillary fringe	1.50	84.00	-10	-30	-20.00
Phreatic surface	2.50	83.00	0	-20	-20.00
Reduced to zero at drain depth	4.50	81.00	20	0	-20.00
London Clay horizon	6.00	79.50	35	15	-20.00

Increased negative pwp of -20KPa between 1.5m & 6m causes settlement of;

$$(20 \cdot 4500)/(20350) = 4.42 \text{ mm}$$

Since the pwp tension capacity (air entry value) is not exceeded by the change in pwp, equilibration will occur as indicated by mechanical consolidation rather than drainage. It may be estimated that the time required for this to occur in the material above London Clay would be approximately 3 weeks. Negative pwp would continue to exist above the phreatic surface. (In case of the London Clay, the estimated period for establishment of drained conditions over the 30m depth of influence considered would be approximately 5 years.)

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FLAC Analysis - notes and input: Figure 16 shows model geometry, figures 17 to 24 illustrate results

Units are Mg - m - sec. Stress is expressed in Kpa.

For soils, FLAC does not accept input in terms of Youngs Modulus, which is replaced by drained bulk modulus K' of the solid matrix and shear modulus G . $E' = 3K'(1-2\nu') = 2G(1+\nu')$. The undrained bulk modulus is $K = K' + K_w/n$: K_w is the bulk modulus of water ($2E+9$ GPa), n is porosity.

The permeability k used is not the hydraulic conductivity (m/sec) but the mobility coefficient ($m^2/KPa.sec$). The numerical conversion is $k(m^2/KPa.sec) = k(m/s)/10$.

Properties of structural members are input in conventional form.

Soil Properties:	Density	Bulk K_u	Bulk K'	Shear G	C_u	C'	ϕ'
	Mg/m ³	Kpa	Kpa	Kpa	Kpa	Kpa	Deg.
Soil 1 0 - 4m bGL	1.8	3.34E+06	1.16E+04	8.66E+03	37.0	2.0	25.0
Soil 2 4 - 6m bGL	1.9	3.35E+06	1.81E+04	1.36E+04	76.0	2.0	25.0
Soil 3 6 - 8m bGL	2.0	3.36E+06	2.33E+04	1.75E+04	104.0	2.0	25.0
Soil 4 8 - 14m bGL	2.0	3.37E+06	3.38E+04	2.54E+04	156.0	2.0	25.0
Soil 5 14 - 22m bGL	2.0	3.39E+06	5.22E+04	3.91E+04	247.0	2.0	25.0
Soil 6 22 - 30m bGL	2.0	3.41E+06	7.31E+04	5.48E+04	353.0	2.0	25.0

Structural elements	Density	Dia or Thickn'	E	Rot'n stiffness KNm ²	Pitch m
Concrete piles 10m long	2.4	0.45	2.80E+07	5.00E+04	2.00
Concrete walls	2.4	0.40	2.80E+07	1.48E+05	Cont.
CHS 355.6x8x68.6 prop	8.00		2.10E+08	2.77E+04	3.00
Floor slabs	2.4	2.40	2.80E+07	6.30E+04	Cont.

Interfaces	Normal spring stiffness Kpa/m	Shear spring stiffness Kpa/m	Cohesion Kpa	Friction Deg.
Piles	6.80E+04	1.80E+04	65.00	0.0
Walls	2.20E+04	4.60E+03		
Wall bases	4.64E+04	6.80E+03		

Procedure:

1. Establishment of "Greenfield" equilibrium, displacements and velocity zeroed,
2. Excavation and installation of piles, walls, temporary struts and existing structure loads; solve undrained.
3. Change properties, remove strut, install floors (basement slab high to allow heave); solve drained.

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Results of analysis with respect to risk of damage to neighbouring property

The movement of grid points at ground level extending 8m to either side of the excavation was monitored during the undrained and drained analyses. They provide the following information. (+ up or towards excn)

Ground movement (mm) 29 Willoughby Road.						Ground movement (mm) 33 Willoughby Road.					
Dist. from exc'n (m)		0.0	1.0	4.0	8.0	Dist. from exc'n (m)		0.0	1.0	4.0	8.0
Undrained	Lateral	1.7	1.6	1.5	1.1	Undrained	Lateral	0.6	0.9	1.0	0.7
	Vertical	-2.3	-1.6	-1.0	-0.5		Vertical	-2.1	-1.4	-0.8	-0.5
Drained	Lateral	2.5	1.4	1.9	1.7	Drained	Lateral	0.9	1.8	1.9	1.5
	Vertical	-4.5	-3.6	-2.2	-1.0		Vertical	-5.0	-3.5	-2.0	-1.0

Maximum input values required for reference [7] and Burland including 4.5mm inward tilt due undrained dewatering:

Undrained (29):	Lateral strain	7.50E-05	Tilt gradient B	8.10E-04	Burland Δ/L	0.006%
Drained (29)	Lateral strain	1.00E-04	Tilt gradient B	4.40E-04	Burland Δ/L	0.009%

Damage risk assessment - Nos 29 & 33 Willoughby Road

Criteria for categories of damage risk proposed by Burland and Cording et al [7] differ: Burland assumes ground and building curvature with deflection ratio based on segment height divided by baseline length whereas [7] considers the tilt gradient caused by shear distortion.

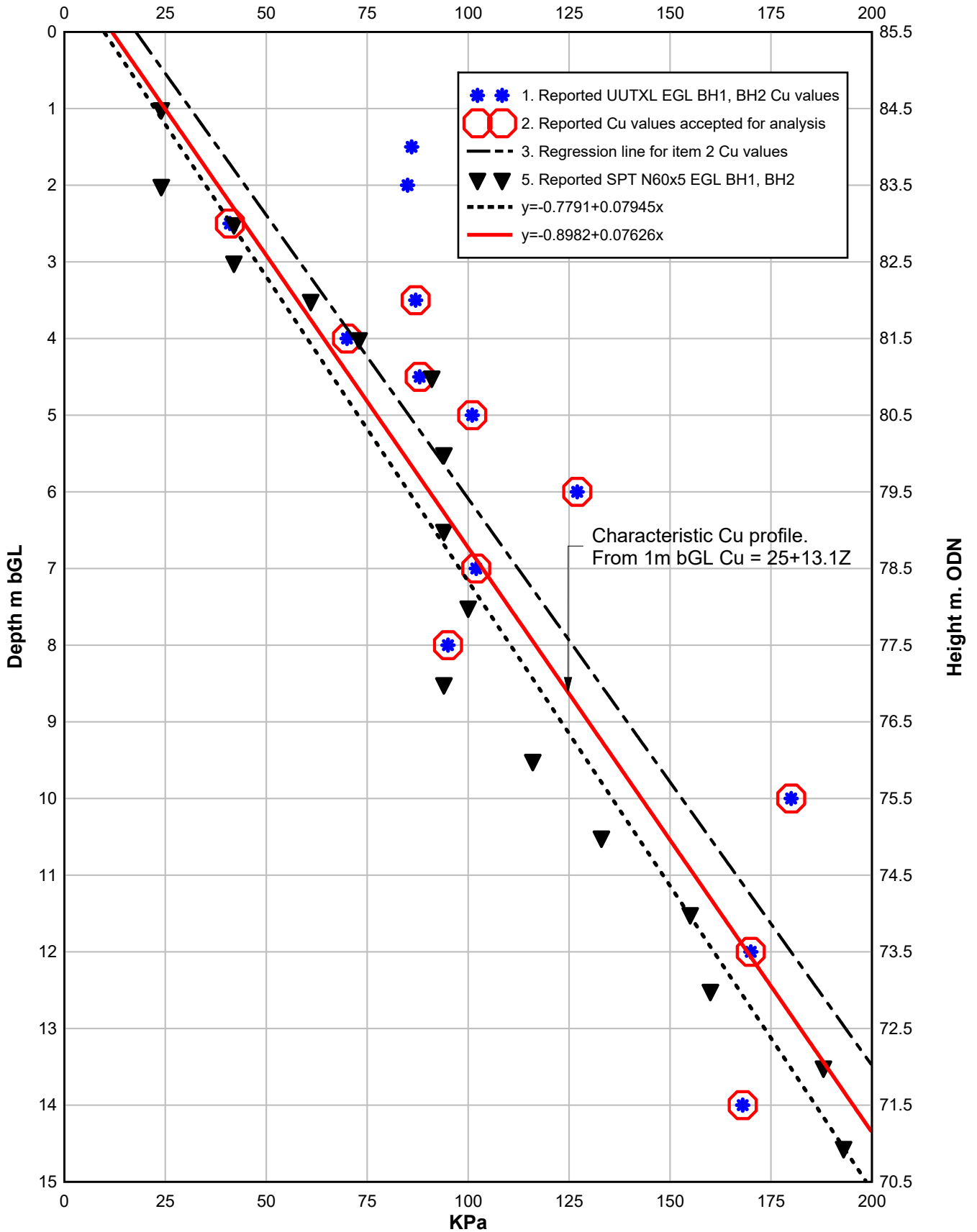
At No.33, lateral strain is compressive due to wall rotation under party wall loads: for the small tilt/angular deflections, damage will be negligible.

At No. 29, the Burland damage risk is category 0

At No. 29, the reference 7 damage risk is category 0

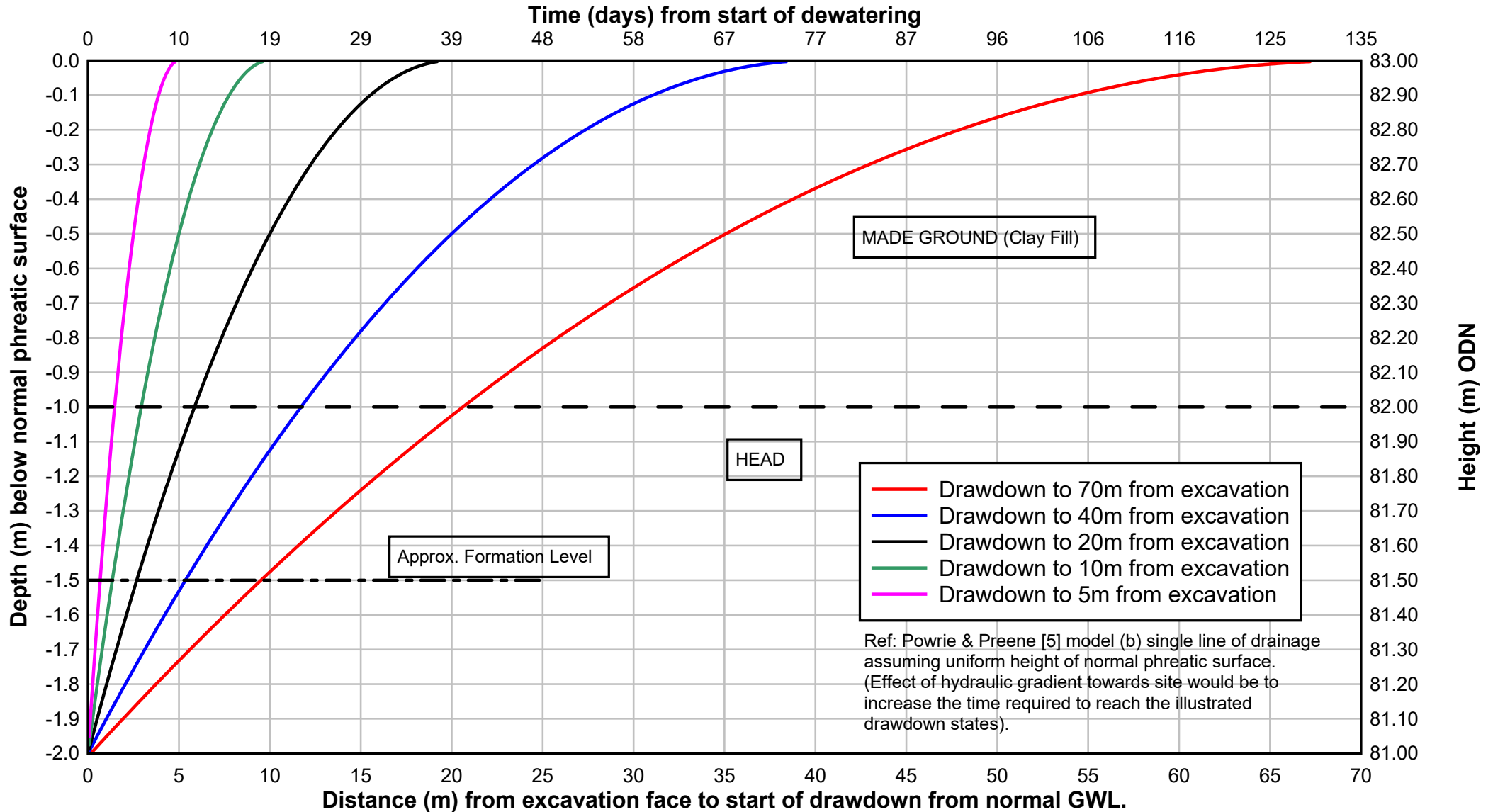
Notwithstanding the approximations made for ground conditions and model geometry, and those inherent to numerical analysis, it is considered that the margins remaining within the determined categories make this assessment robust.

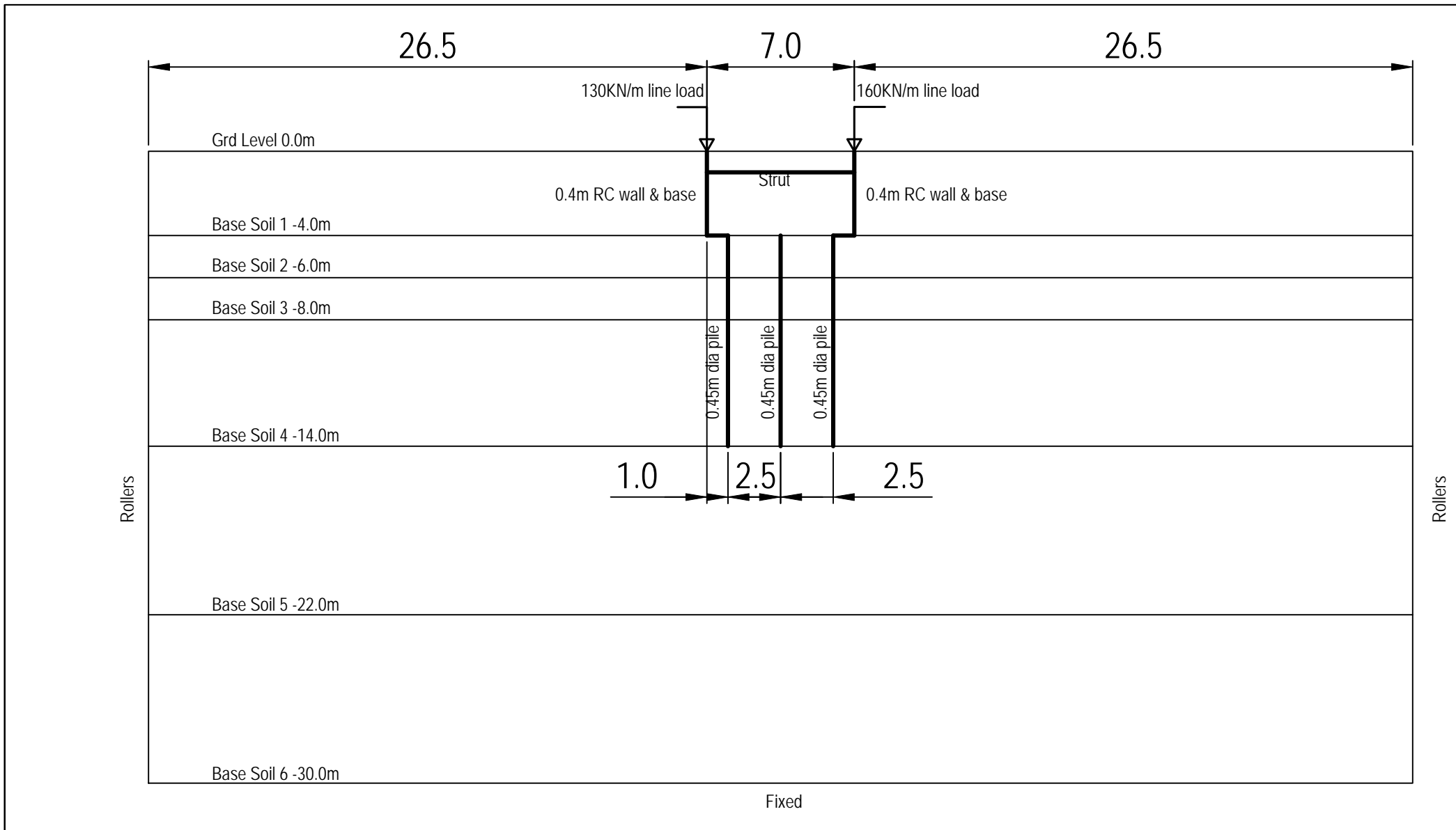
G1808 31 Willoughby Road NW3 1RT - Proposed Basement Assessed Characteristic Profile of Undrained Shear strength vs Depth



G1808 31 Willoughby Road NW3 1RT - Proposed Basement


Estimated temporary drawdown effect of construction dewatering





31 WILLOUGHBY ROAD NW3 1RT

FLAC MODEL ARRANGEMENT

	Report:	Figure 16
	Scale as shown	



