

DAYLIGHT & SUNLIGHT ASSESSMENT

PROPERTY ADDRESS

3, 5 & 7 Fortess Road, Kentish Town, NW5 1AA

DATE

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PREPARED BY EAL Consult



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EXECUTIVE SUMMARY

This daylight & sunlight assessment has been prepared to support the Planning Application for the proposed development at 3, 5 & 7 Fortess Road, Kentish Town in Camden, NW5 1AA. This assessment should be consulted in conjunction with the accompanied planning drawings.

The primary purpose of this daylight, sunlight assessment is to determine the likely loss of light to adjacent buildings resulting from the construction of the commercial and residential re-development. Therefore, the proposed development can be identified as the potential source of impact.

The main objective to carry out this Daylight & Sunlight assessment is to:

 Assess the impact of the proposed development upon the current levels of sunlight/daylight being enjoyed by the existing neighbouring buildings.

The methodology set out in this report is in accordance with BRE's 'Site Layout Planning for Daylight and Sunlight' 2nd edition 2011, which is accepted as good practice by Planning Authorities.

The following assessments were carried out:

Daylight & Sunlight Assessment

- Existing dwellings
 - a. Vertical Sky Component
 - b. Annual Probability of Sunlight Hours (APSH) annual and winter calculations

A total of 5 neighbouring properties were identified, which may be impacted upon by the proposed development.

The assessment of daylight, sunlight to the surrounding residential properties indicates that the proposed development will not cause any noticeable change to existing occupants. As such the scheme is considered fully BRE compliant in terms of daylight, sunlight.

It is worth noting, that while the BRE methodology is a useful assessment for most developments in countryside and sub-urban settings, it does not however respect the lower daylight and sunlight levels found in city centres. Increased massing in cities are therefore more likely to fail these tests based on the target daylight and sunlight values set out in the BRE guidance.

The Autodesk Ecotect software was used to carry out the daylight and sunlight impact assessment. A 3-dimensional site model has been created from information supplied by the architect, drawings, including location and site plan, existing and proposed drawings.

No gardens or open spaces were identified within the site area and therefore an overshadowing assessment was not carried out.

TERMS AND DEFINITIONS

Average Daylight Factor (ADF)

The average daylight factor is the average indoor illuminance (from daylight) on the working plane within a room, expressed as a percentage of the simultaneous outdoor illuminance on a horizontal plane under an unobstructed CIE 'standard overcast sky'.

CIE Standard Overcast Sky

A completely overcast sky for which the ratio of its illuminance Ly at an angle of elevation y above the horizontal to the luminance Lz at the zenith is given by: Ly=Lz (1+2siny) /3 A CIE standard overcast sky is darkest at the horizon and brightest at the zenith (vertically overhead).

No-Sky Line

The no-sky line divides those areas of the working plane which can receive direct light from the sky, from those which cannot. It is important as it indicates how good the distribution of daylight is in a room. Areas beyond the no-sky line will generally look gloomy.

As an approximation, obstructions that are parallel to the window can be considered infinite.

Working Plane

The working plane is a notional surface, typically at about desk or table height, at which daylight factor or the 'no-sky line' is calculated or plotted.

For the purpose of assessing useful daylight, a working plane of 850mm above finished floor level is assumed. It is generally expected that ceiling heights will not fall below 2.4m.

Obstruction Angle

The angular altitude of the top of an obstruction above the horizontal, measured from a reference point in a vertical plane in a section perpendicular to the vertical plane.

Probable Sunlight Hours

The long-term average of the total number of hours during a year in which direct sunlight reaches the unobstructed ground (when clouds are taken into account).

Sky Factor

Sky Factor is the ratio of the parts of illuminance at a point on a given plane that would be received directly through unglazed openings from a sky of uniform luminance, to illuminance on a horizontal plane due to an unobstructed hemisphere of this sky. The sky factor does not include reflected light, either from outdoor or indoor surfaces.

Vertical Sky Component (VSC)

Ratio of that part of illuminance, at a point on a given vertical plane, that is received directly from a CIE standard overcast sky, to illuminance on a horizontal plane due to an unobstructed hemisphere of this sky.

Usually the 'given vertical plane' is the outside of a window wall. The VSC does not include reflected light, either from the ground or from the buildings.

CURRENT POLICIES, REGULATIONS AND BENCHMARKS

Regulations

European workplace directive – Assess to daylight required

Building Regulations - No minimum daylight standards

Like UK, many other countries have some planning regulations that affect daylight but are not necessarily found as a daylighting regulation. However there is some demand from the planning authorities in these areas (e.g. City of Westminster in London) for improved guide lines, possibly based on typical daylight access in particular city zones.

Rights of Light

In UK, "Rights of Light" legally protects individuals against newly constructed neighbouring properties and extensions that may affect their daylighting. It has been defined in terms of the position of the 0.2% Sky Factor Contour.

Standards

- BS 8206-2 2008 Code of Practice for Daylighting
- Building Bulletin 87 Guidelines for Environmental Design in Schools
- Building Bulletin 90 Lighting Design for Schools
- Building Bulletin 95 Designing Schools for the future
- CIBSE LG2 Lighting for Healthcare buildings

Guides

- CIBSE SLL Daylighting and Window Design LG10 1999
- BRE Designing Buildings for Daylight
- BRE Designing with Innovative Daylighting
- 3-5 Benchmarks
- Code of Sustainable Homes
- BREEAM
- LEED

Recommendations as to daylight in domestic buildings are to be found in the British Standard BS 8206-02 (BSI, 2002) on Lighting, specifically the section on day lighting, in the publications of the CIBSE and in the publication of BRE (1,2,3).

The recommendations for internal spaces are expressed in three ways:

- A minimum average Daylight Factor (2% for Kitchen, 1.5% for Living Rooms and 1% for Bed Rooms)
- The position of the No-Sky Line at working plane height (0.85m). If the area beyond the No-Skyline is more than 50% the room will look gloomy
- Limiting Depth Criteria

To put the first recommendation in context, a room with an average daylight factor of more than 5% is regarded as well daylit, that is electric lights would be used infrequently during daylight hours, but if it is below 2% electric lights would be used frequently. The requirements are therefore minimal.

These recommendations are illumination based so orientation is not considered a factor. As the perception of how well a space is daylit may be influenced by the factors orientation, shading control and view hence the orientation factor can be used to reflect the higher levels of illuminance on the South facade.

In regard to a new building affecting an existing recommendations have an origin in solar access in the UK. The new building should not reduce the Vertical Sky Component (VSC) below 27% or if it does it should not reduce it by more than 20%. Where there is horizontally facing window/skylight VSC can be up to 40%.

In most city centres the Vertical Sky Component is already below 27% at many windows of building. Planning Authorities have tended to use the 20% reduction guideline when assessing planning permission in such areas which unfortunately has its drawbacks, leading to creeping increased heights in urban areas reducing daylight access.

METHODOLOGY

BRE Guide: Site Layout Planning for Daylight and Sunlight, 2011

This assessment would be based on the various numerical tests laid out in the Building Research Establishment (BRE) Guidelines "Site Layout Planning for Daylight and Sunlight: a good practice guide" 2011. It is important to note that BRE tests in general are based on the requirements of the BS Standards 8206 Part 2.

Following factors will be calculated for the Sunlight/Daylight Assessment:

- Sunlight/Daylight to existing windows
- Daylight to proposed habitable rooms

"The guide is intended for building designers and their clients, consultants and planning officials. The advice given here is not mandatory and the guide should not be seen as an instrument of planning policy; its aim is to help rather than constrain the designer. Although it gives numerical guidelines, these should be interpreted flexibly since natural lighting is only one of many factors in site layout design."

The first step in the methodology is to determine the key sensitive receptors, which windows may be affected by the existing buildings.

Key receptors are windows directly facing and located perpendicular - to the site.

Existing Buildings

Using simple geometry, it will be determined whether the daylight to existing buildings and amenity spaces is adversely affected and this will be done using 25 degree and 45 degree methods.

If new buildings are set out in accordance with the 25 degree method for daylight, this will be sufficient to show that the sunlight to the existing buildings will not be adversely affected.

If these two methods of assessments are satisfied, this will be sufficient in showing that the day lighting to existing buildings and their amenity spaces will not be adversely affected by the new development.

Calculation Method of Daylight to Surrounding Windows

A plane is drawn at 25 degrees from the horizontal, at the centre of an existing window. If a new development intersects with this plane, the internal daylight levels of the surrounding windows may be reduced. When an obstruction of the 25 degree plane occurs, a more detailed assessment involving the Vertical Sky Component of the affected window would need to be carried out.

Calculation Method of Vertical Sky Component (VSC)

The Vertical Sky Component is the ratio of the direct sky illuminance falling on the vertical wall at a reference point, to the simultaneous horizontal illuminance under an unobstructed sky. To maintain good levels of daylight, the Vertical Sky Component of a window needs to be 27% or greater. If the VSC is less than 27%, then a comparison of existing and proposed levels of VSC level would need to be calculated.

VSC can be determined by calculating the Obstruction angle: Obstruction Angle = tan-1 (H/D)

Where; H is the height of the obstruction above the middle of the window and D is the horizontal distance from the window to the obstruction

Good levels of daylighting can still be achieved if VSC levels are within 0.8 of their former value. Otherwise, the Average Daylight Factor of the internal rooms would need to be calculated.

Calculation Method of No-Sky Line

The no-sky line test involves the calculation of percentage of a room's area which can receive direct skylight. Diffuse daylight is likely to be adversely affected if after the development the area of a room receiving direct skylight is 0.8 times its former value.

The depth of no-sky line (d) is calculated as: d=X(H/Y)

Where; X is the distance from the outside wall to the obstruction, H is height of the window head above the working plane and Y is the height of obstruction above the window head.

From the depth of no-skyline we can calculate "The percentage of working plane that receives direct light from the sky (D)" which can be calculated as: $D = (d/rd) \times 100$

Where d is the depth of no-skyline and rd is the room depth.

Calculation Method of Average Daylight Factor (ADF)

The calculation of ADF takes into account a range of variables e.g size of the window, area of room surfaces, type of glazing, number of windows in a room and factors such as reflectivity of the internal finishes. For any receptors failing to satisfy the VSC criteria of 27%, a more detailed study based on the Average Daylight Factor (ADF) should be undertaken for comparison against the minimum daylight requirement as described in the BS 8206-02 (BSI, 2002).

BRE Formula to calculate Daylight Factor (DF): DF = (M x W x 0 x T) / [A x (1-R2)]

Where; M is correction factor for dirt, W is total glazed area of windows or roof lights, 0 is angle of visible sky, T is transmission factor of glazing, A is total area of all the room surfaces (ceiling, floor, walls and windows) and R is area weighted average reflectance of the room surfaces (walls, floor and ceiling).

Calculation Method of Limiting Depth Criteria

Where all conditions are required to be satisfied for good day-lighting in major rooms of the proposed development, once ADF calculated, Limiting Depth criteria can be determined by the ratio between the ADF in the front half of the room and the rear half. This should not exceed 3. If a significant area of the working plane lies beyond the no-skyline then the distribution of the daylight in the space will look poor.

Limiting Depth Criteria can be calculated as: L/W+L/H should be less than / equal to 2/(1-R)

Where; L is the depth of the room from the window to the back wall, W is the width of the room measured parallel to the window, H is the height of the window head above the floor level and R is area weighted average reflectance of the room surfaces (walls, floors and ceiling).

SITE

The proposed site is located in a predominantly residential and commercial area and therefore, a daylight and sunlight assessment was undertaken to determine the potential impact of the proposed development on these neighbouring areas.

The proposal includes the re-development of three 2storey buildings with commercial use on the ground floor and residential use on the upper floors. The proposal includes the construction of a 3storey building with an approximate height of 7m. Five neighbouring properties were identified that could possibly be affected from this proposed extension.

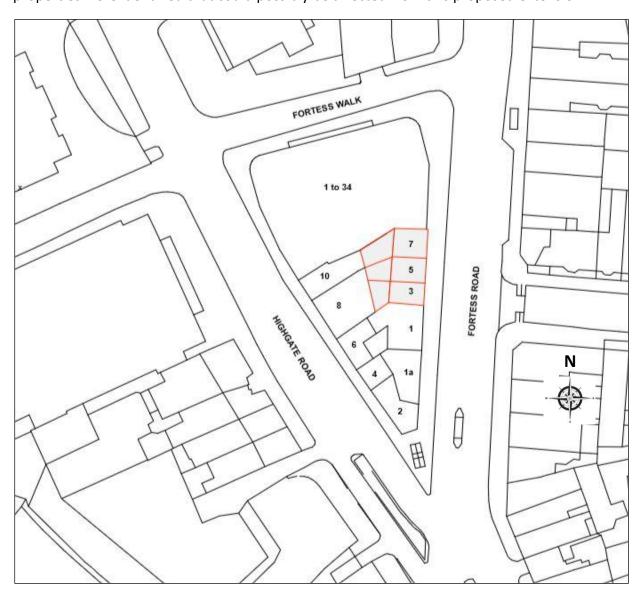


Figure 1 - Site Location



Figure 2 – Possibly Affected Neighbouring Properties

Possibly affected properties:

- 1. No 12 Fortess Road
- 2. No 1 Fortess Road
- 3. No 8 Highgate Road
- 4. No 10 Highgate Road
- 5. No 1-34 Fortess Road

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Vertical Sky Component (VSC)

VSC analysis of each window was carried out. The results are listed in the following pages. If the VSC is greater than 27%, then enough skylight should still be reaching the window and the levels of daylight experienced in the space should not be seriously affected.

Vertical Sky Component Assessment

Table 1 – Vertical Sky Component for the existing properties, Post Development

Vertical Sky Comp	onent	Post development	VSC after Proposal
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - GF	25.0	No
	Win02 - FF	28.1	Yes
	Win03 - FF	28.1	Yes
No 12 Fortess Road	Win 04 - FF	28.0	Yes
	Win 05 - SF	29.4	Yes
	Win 06 - SF	29.4	Yes
	Win 07 - SF	29.3	Yes

Results show that the Vertical Sky Component is less than the recommended value of 27% only for one window. Further calculations will demonstrate the difference in light levels at predevelopment.

Table 2 – Vertical Sky Component for the existing properties, Pre Development

Vertical Sky Component		Pre development	VSC
Assessed neighbouring property:	Window no.	BRE VSC %	>27
No 12 Fortess Road	Win01 – GF	25.6	No

Further calculations demonstrate that the Vertical Sky Component for the specific windows is the same before the construction of the new development. Therefore, there will be no loss of light for this neighbouring property.

Table 3 – Vertical Sky Component for the existing properties, Post Development

Vertical Sky Component		Post development	VSC after Proposal
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	12.3	No
	Win02 - FF	11.8	No
No 1 Fortess Road	Win03 - SF	14.5	No
NO 1 FOILESS ROAU	Win04 - SF	14.1	No
	Win05 - TF	19.1	No
	Win06 - TF	19.0	No

Results show that the Vertical Sky Component is less than the recommended value of 27% for all the windows. Further calculations will demonstrate the difference in light levels at predevelopment.

Table 4 – Vertical Sky Component for the existing properties, Pre Development

Vertical Sky Comp	onent	Pre development	VSC
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	12.4	No
	Win02 - FF	12.0	No
No 1 Fortess Road	Win03 - SF	14.5	No
NO 1 FOILESS ROAU	Win04 - SF	14.1	No
	Win05 - TF	19.1	No
	Win06 - TF	19.0	No

Results show that the VSC for all the windows is still less than 27% at pre construction phase. Therefore, the proposal is considered appropriate for the specific site.

Table 5 – Vertical Sky Component for the existing properties, Post Development

Vertical Sky Comp	onent	Post development	VSC after Proposal
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	9.4	No
	Win02 - FF	9.6	No
	Win03 - FF	9.6	No
No 8 Highgate Road	Win 04 - SF	15.3	No
	Win05 – SF	15.6	No
	Win06 – SF	15.8	No
	Win07 – SF	15.2	No

Results show that the Vertical Sky Component is less than the recommended value of 27%. Further calculations will demonstrate the difference in light levels at pre-development.

Table 6 – Vertical Sky Component for the existing properties, Pre Development

Vertical Sky Comp	onent	Pre development	VSC
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	10.5	No
	Win02 - FF	10.9	No
	Win03 - FF	11.0	No
No 8 Highgate Road	Win 04 - SF	17.9	No
	Win05 – SF	17.8	No
	Win06 – SF	17.9	No
	Win07 – SF	17.9	No

Results show that the VSC for all the windows is still less than 27% at pre construction phase. There is a small impact on the light levels that may be noticeable to the existing neighbouring property users, however, their location (windows) and use of the neighbouring rooms facing the proposed site has not been verified and therefore, the proposal is still considered appropriate for the specific site if these windows are located to non habitable rooms.

Table 7 – Vertical Sky Component for the existing properties, Post Development

Vertical Sky Component		Post development	VSC after Proposal
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	8.4	No
No 10 Highgate Road	Win02 – FF mezzanine	8.5	No
	Win03 - SF	15.2	No

Results show that the Vertical Sky Component is less than the recommended value of 27%. Further calculations will demonstrate the difference in light levels at pre-development.

Table 8 – Vertical Sky Component for the existing properties, Pre Development

Vertical Sky Component		Pre development	VSC
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	10.3	No
No 10 Highgate Road	Win02 – FF mezzanine	10.2	No
	Win03 - SF	17.1	No

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Results show that the VSC for all the windows is still less than 27% at pre construction phase. There is a small impact on the light levels that may be noticeable to the existing neighbouring property users, however, if these windows are located to non habitable rooms the proposal is still considered appropriate for the specific site.

Table 9 – Vertical Sky Component for the existing properties, Post Development

Vertical Sky Comp	onent	Post development	VSC after Proposal
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	10.4	No
	Win02 – FF	10.2	No
	Win03 - FF	10.2	No
	Win04 - FF	9.1	No
	Win05 - FF	10.8	No
	Win06 - SF	15.7	No
	Win07 – SF	15.5	No
No 1-34 Fortess Road	Win08 – SF	15.5	No
	Win09 – SF	14.2	No
	Win010 – SF	15.9	No
	Win011 – TF	19.3	No
	Win012 – TF	19.3	No
	Win013 – TF	19.1	No
	Win014 – TF	18.5	No
	Win015 – TF	20.0	No

Results show that the Vertical Sky Component is less than the recommended value of 27%. Further calculations will demonstrate the difference in light levels at pre-development.

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Table 10 – Vertical Sky Component for the existing properties, Pre Development

Vertical Sky Component		Pre development	vsc
Assessed neighbouring property:	Window no.	BRE VSC %	>27
	Win01 - FF	10.4	No
	Win02 – FF	10.2	No
	Win03 - FF	10.2	No
	Win04 - FF	9.1	No
	Win05 - FF	10.8	No
	Win06 - SF	15.7	No
	Win07 – SF	15.5	No
No 1-34 Fortess Road	Win08 – SF	15.5	No
	Win09 – SF	14.2	No
	Win010 – SF	15.9	No
	Win011 – TF	19.3	No
	Win012 – TF	19.3	No
	Win013 – TF	19.1	No
	Win014 – TF	18.5	No
	Win015 – TF	20.0	No

Results show that the VSC for all the windows is the same at pre and post construction phase. Please note that additional existing obstructions located in front of the existing neighbouring properties have not been modelled for this assessment. The assessment does not take into account temporary obstructions that can be removed and that do not include any habitable spaces.

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Sunlight Assessment – Annual Probable Sunlight Hours

Annual probable sunlight hours (APSH) is a measure of sunlight that a given window may expect over a year period. The BRE guidance recognises that sunlight is less important than daylight in the amenity of a room and is heavily influenced by orientation. North facing windows may receive sunlight on only a handful of occasions in a year, and windows facing eastwards or westwards will only receive sunlight for some of the day. Therefore, **BRE** guidance states that only windows with an orientation within 90 degrees of south need be assessed. Therefore, the surrounding properties located within the 90 degrees of south have been assessed.

For sunlight studies the APSH (annual probable hours) test calculates the percentage of statistically probable hours of sunlight received by each window in both the summer and winter months. From March 21st to September 21st – Summer period and from the 21st September to 21st of March – Winter period.

Sunlight is measured using a sun indicator which contains 100 spots, each representing 1% of APSH. Therefore, where no obstruction exists the total annual probable sunlight hours would amount to 1486 and therefore each spot equates to 14.86 hours of the total annual sunlight hours.

Following are the recommended Sunlight hours for London. Total recommended sunlight hours:

- = 25% of APSH for London
- = 25% of 1468hrs
- $= (25/100) \times 1486$
- = 371.5hrs/yr

Recommended sunlight hours for winter

- = 5% of APSH for London
- = 5% of 1486hrs
- $= (5/100) \times 1486$
- = 74.3hrs/yr

Table 11 – Annual Probable Sunlight Hours for existing properties, after the proposed development

Annual Probable Sun	Post development	
Assessed neighbouring property:	Window no.	>371.5hrs
	Win01 - GF	Yes
	Win02 - FF	Yes
	Win03 - FF	Yes
No 12 Fortess Road	Win 04 - FF	Yes
	Win 05 - SF	Yes
	Win 06 - SF	Yes
	Win 07 - SF	Yes

Table 12 – Winter Probable Sunlight Hours for existing properties, after the proposed development

Winter Probable Sunl	Post development	
Assessed neighbouring property: Window no.		>74.3hrs
	Win01 - GF	Yes
	Win02 - FF	Yes
	Win03 - FF	Yes
No 12 Fortess Road	Win 04 - FF	Yes
	Win 05 - SF	Yes
	Win 06 - SF	Yes
	Win 07 - SF	Yes

Table 13 – Annual Probable Sunlight Hours for existing properties, after the proposed development

Annual Probable Sun	Post development	
Assessed neighbouring property: Window no.		>371.5hrs
	Win01 - FF	Yes
	Win02 - FF	Yes
No 1 Fortess Road	Win03 - SF	Yes
NO 1 FOILESS ROAU	Win04 - SF	Yes
	Win05 - TF	Yes
	Win06 - TF	Yes

Table 14 – Winter Probable Sunlight Hours for existing properties, after the proposed development

Winter Probable Sun	Post development	
Assessed neighbouring property: Window no.		>74.3hrs
	Win01 - FF	Yes
	Win02 - FF	Yes
No 1 Fortoss Bood	Win03 - SF	Yes
No 1 Fortess Road	Win04 - SF	Yes
	Win05 - TF	Yes
	Win06 - TF	Yes

Table 15 – Annual Probable Sunlight Hours for existing properties, after the proposed development

Annual Probable Sun	Post development	
Assessed neighbouring property:	>371.5hrs	
	Win01 - FF	Yes
	Win02 - FF	Yes
	Win03 - FF	Yes
No 8 Highgate Road	Win 04 - SF	Yes
	Win05 – SF	Yes
	Win06 – SF	Yes
	Win07 – SF	Yes

Table 16 – Winter Probable Sunlight Hours for existing properties, after the proposed development

Winter Probable Sun	Post development	
Assessed neighbouring property:	>74.3hrs	
	Win01 - FF	Yes
	Win02 - FF	Yes
	Win03 - FF	Yes
No 8 Highgate Road	Win 04 - SF	Yes
	Win05 – SF	Yes
	Win06 – SF	Yes
	Win07 – SF	Yes

Table 17 – Annual Probable Sunlight Hours for existing properties, after the proposed development

Annual Probable Sunl	Post development	
Assessed neighbouring property:	>371.5hrs	
	Win01 - FF	Yes
No 10 Highgato Poad	Win02 – FF	Yes
No 10 Highgate Road	mezzanine	163
	Win03 - SF	Yes

Table 18 – Winter Probable Sunlight Hours for existing properties, after the proposed development

Winter Probable Sunl	Post development	
Assessed neighbouring property:	>74.3hrs	
No 10 Highgate Road	Win01 - FF	Yes
	Win02 – FF	Yes
	mezzanine	163
	Win03 - SF	Yes

Table 19 – Annual Probable Sunlight Hours for existing properties, after the proposed development

Annual Probable Sunl	Post development	
Assessed neighbouring property: Window no.		>371.5hrs
	Win01 - FF	Yes
	Win02 – FF	Yes
	Win03 - FF	Yes
	Win04 - FF	Yes
	Win05 - FF	Yes
	Win06 - SF	Yes
	Win07 – SF	Yes
No 1-34 Fortess Road	Win08 – SF	Yes
	Win09 – SF	Yes
	Win010 – SF	Yes
	Win011 – TF	Yes
	Win012 – TF	Yes
	Win013 – TF	Yes
	Win014 – TF	Yes
	Win015 – TF	Yes

Table 20 – Winter Probable Sunlight Hours for existing properties, after the proposed development

Winter Probable Sunl	Post development	
Assessed neighbouring property: Window no.		>74.3hrs
	Win01 - FF	Yes
	Win02 – FF	Yes
	Win03 - FF	Yes
	Win04 - FF	Yes
	Win05 - FF	Yes
	Win06 - SF	Yes
	Win07 – SF	Yes
No 1-34 Fortess Road	Win08 – SF	Yes
	Win09 – SF	Yes
	Win010 – SF	Yes
	Win011 – TF	Yes
	Win012 – TF	Yes
	Win013 – TF	Yes
	Win014 – TF	Yes
	Win015 – TF	Yes

CONCLUSION

The proposed development has been designed with care so that it has minimum visual impact on its surroundings, achieving as much sunlight hours as possible despite un-avoidable site constraints and limitations.

From initial assessment three existing neighbouring properties could be slightly affected from the proposed development at 3, 5 and 7 Fortess Road. Calculations confirmed that the existing properties will receive in most cases the same amount of daylight as the pre and post construction calculations demonstrate. Two properties may notice a difference in light levels, however, the use of the rooms (habitable – non habitable) facing the proposed site has not been confirmed and therefore, the proposal is considered appropriate for the specific site.

No open spaces/gardens were identified within the area and therefore, an overshadowing assessment was not carried out.

Overall, the assessment of daylight and sunlight to the surrounding properties indicates that the proposal will not cause a noticeable change to existing occupants as the difference in the results has been kept to a minimum. As such the scheme is considered fully BRE complaint in terms of daylight and sunlight and should be considered acceptable.

The sunlight results indicate that none of the existing windows will see an annual noticeable loss in sunlight levels.

 All windows achieve in all cases (APSH and winter) the BRE requirement, with the percentage of sunlight hours exceeding the APSH 25% and 5% for winter period.

Please note that the No Sky Line¹ calculations have not been carried out for this assessment as the layout of the neighbouring properties is unknown. Therefore, an assessment would be based on room assumptions.

¹ The no-sky line test involves the calculation of percentage of a room's area which can receive direct skylight.

APPENDIX A

Table 21 – Vertical Sky Component for the existing properties, Pre & Post Development

Vertical Sky Comp	onent	Pre development	Post development	Difference	Difference %
Assessed neighbouring property:	Window no.	BRE VSC %	BRE VSC %	Billerence	Difference //
	Win01 - GF	25.6	25.0	0.6	2.3
	Win02 - FF	28.3	28.1	0.2	0.7
	Win03 - FF	28.3	28.1	0.2	0.7
No 12 Fortess Road	Win 04 - FF	28.1	28.0	0.1	0.3
	Win 05 - SF	29.4	29.4	0.0	0.0
	Win 06 - SF	29.4	29.4	0.0	0.0
	Win 07 - SF	29.3	29.3	0.0	0.0

Table 22 – Vertical Sky Component for the existing properties, Pre & Post Development

Vertical Sky Comp	onent	Pre development	Post development	Difference	Difference %
Assessed neighbouring property:	Window no.	BRE VSC %	BRE VSC %	Difference	Difference /o
	Win01 - FF	12.4	12.3	0.1	0.8
	Win02 - FF	12.0	11.8	0.2	1.6
No 1 Fortoss Bood	Win03 - SF	14.5	14.5	0.0	0.0
No 1 Fortess Road	Win04 - SF	14.1	14.1	0.0	0.0
	Win05 - TF	19.1	19.1	0.0	0.0
	Win06 - TF	19.0	19.0	0.0	0.0

Table 23 – Vertical Sky Component for the existing properties, Pre & Post Development

Vertical Sky Comp	onent	Pre development	Post development	Difference	Difference %
Assessed neighbouring property:	Window no.	BRE VSC %	BRE VSC %	Difference	Difference //
	Win01 - FF	10.5	9.4	1.1	10.4
	Win02 - FF	10.9	9.6	1.3	11.9
	Win03 - FF	11.0	9.6	1.4	12.7
No 8 Highgate Road	Win 04 - SF	17.9	15.3	2.6	14.5
	Win05 – SF	17.8	15.6	2.2	12.3
	Win06 – SF	17.9	15.8	2.1	11.7
	Win07 – SF	17.9	15.2	2.7	15.0

Table 24 – Vertical Sky Component for the existing properties, Pre & Post Development

Vertical Sky Component		Pre development	Post development	Difference	Difference %
Assessed neighbouring property:	Window no.	BRE VSC %	BRE VSC %		31131311 66 /2
No 10 Highgate Road	Win01 - FF	10.3	8.4	1.9	18.4
	Win02 – FF mezzanine	10.2	8.5	1.7	16.6
	Win03 - SF	17.1	15.2	1.9	18.4

Table 25 – Vertical Sky Component for the existing properties, Pre & Post Development

Vertical Sky Component		Pre development	Post development	Difference	Difference %
Assessed neighbouring property:	Window no.	BRE VSC %	BRE VSC %	Difference	Zirici chice /u
No 1-34 Fortess Road	Win01 - FF	10.4	10.4	0.0	0.0
	Win02 – FF	10.2	10.2	0.0	0.0
	Win03 - FF	10.2	10.2	0.0	0.0
	Win04 - FF	9.1	9.1	0.0	0.0
	Win05 - FF	10.8	10.8	0.0	0.0
	Win06 - SF	15.7	15.7	0.0	0.0
	Win07 – SF	15.5	15.5	0.0	0.0
	Win08 – SF	15.5	15.5	0.0	0.0
	Win09 – SF	14.2	14.2	0.0	0.0
	Win010 – SF	15.9	15.9	0.0	0.0
	Win011 – TF	19.3	19.3	0.0	0.0
	Win012 – TF	19.3	19.3	0.0	0.0
	Win013 – TF	19.1	19.1	0.0	0.0
	Win014 – TF	18.5	18.5	0.0	0.0
	Win015 – TF	20.0	20.0	0.0	0.0