

Proposed Residential Development

**Alliance House, 29-30 High Holborn,
London, WC1V 6AZ.**

Noise Impact Assessment

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Doc Ref: 1037918.ad.Issue1



**Noise Impact Assessment
Proposed Mixed Use Development**

Project Address:	Alliance House, 29-30 High Holborn London WC1V 6AZ
Project Reference:	103918

Issue/Revision Record

Issue:	Date:	Remarks:	Author:
1	01/11/2019	First Issue	Andy Dodd

	Signature:	Print:	Title:	Date:
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1. INTRODUCTION

- 1.1 Acoustics Plus Ltd (APL) is an independent firm of multi-disciplinary acoustic engineers. APL is engaged by both private and public sector clients. APL is a registered member of The Association of Noise Consultants (ANC) and the author is a corporate member of The Institute of Acoustics (IOA).
- 1.2 APL has been instructed by, Westcombe Homes, to consider and advise upon the noise implications of the proposed redevelopment of the site. The development proposals will comprise the erection of a 4 storey rear extension at 2nd, 3rd, 4th and 5th floor levels to create 4 no. self-contained flats (1 no. 2-bed and 3 no. studios).
- 1.3 It is understood that the Local Planning Authority (LPA) will require more information, specifically in regard of noise. It is further understood that the noise matters are in connection with the proposed new buildings proximity to nearby highways and existing commercial premises.
- 1.4 The object of this report is to determine environmental noise levels at the site in accordance with Government planning policy guidance and Camden Council. Outline comments regarding any noise control measures will also be provided to demonstrate that the ingress of noise may be properly controlled.
- 1.5 The report will give due regard to the following documents:
 - (a) *National Planning Policy Framework February 2019 – Ministry of Housing Communities & Local Government;*
 - (b) *Noise Policy Statement for England (NPSE) March 2010 – Department for Environment, Food and Rural Affairs;*
 - (c) *ProPG: Planning and Noise May 2017 Professional Practice Guidance on Planning and Noise;*
 - (d) *BS8233:2014 “Sound insulation and noise reduction for buildings – Code of Practice”;*
 - (e) *Planning condition No.3 of Decision notice 2015/6112?P*

2. BASELINE SITUATION

- 2.1 The Application Site (the "site") is located at Alliance House, 29-30 High Holborn, London, WC1V 6AZ. The site (highlighted in red) is shown in Diagram 1.

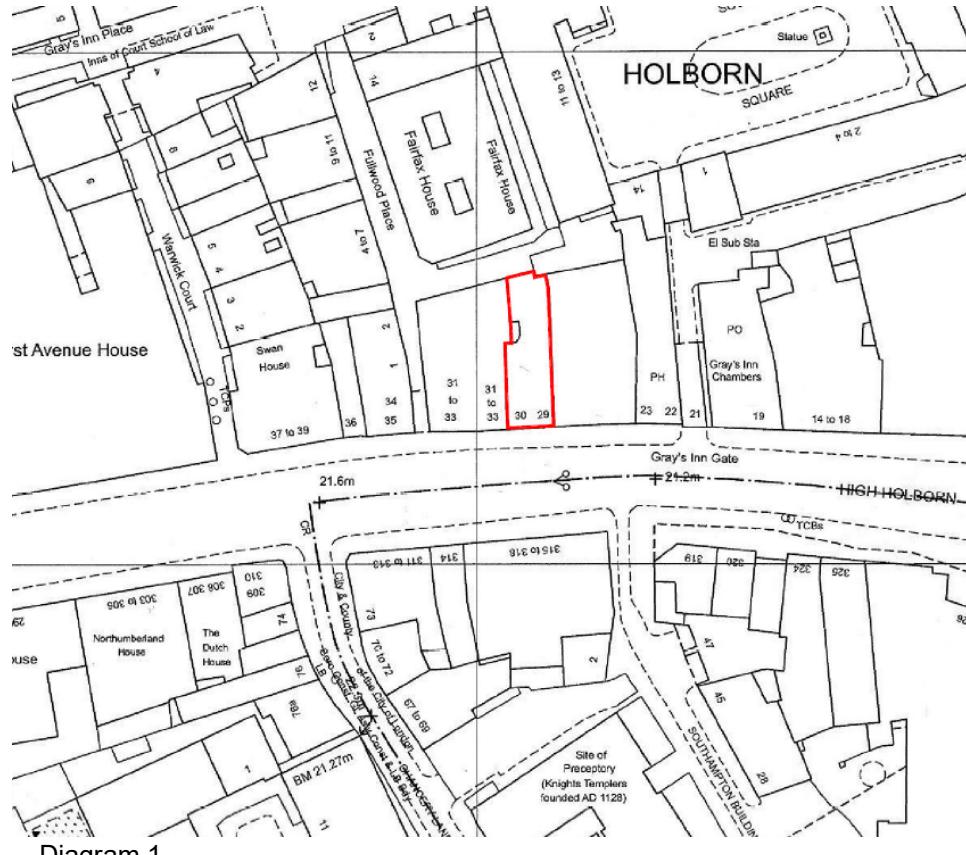


Diagram 1

- 2.2 The development proposals will comprise the erection of a 4 storey rear extension at 2nd, 3rd, 4th and 5th floor levels to create 4 no. self-contained flats (1 no. 2-bed and 3 no. studios).
- 2.3 The proposal would result in the creation of dwellings surrounded by largely commercial and office use.

3. NOISE CRITERIA

New residential accommodation

- 3.1 Camden Council have conditioned the application and Condition No.3 is reproduced below:

"The noise level in rooms at the development hereby approved shall meet the 'Good' noise standard specified in BS8233:1999 for internal rooms and external amenity areas".

Reason: To ensure that the amenity of occupiers of the development site is not adversely affected by noise in accordance with policy CS5 of the London Borough of Camden Local Development Framework Core Strategy and policy DP28 of the London Borough of Camden Local Development Framework Development Policies.

- 3.2 It is noted that BS8233:1999 is superseded by BS8233:2014 and that for the purposes of this report the newer standard guidelines will be adopted.
- 3.3 The new National Planning Policy Framework (NPPF) released in February 2019 has replaced planning policy guidance which previously covered planning and pollution control and new development in England. The purpose of the planning system is to contribute to the achievement of sustainable development. There are three dimensions to sustainable development: economic, social and environmental. The environmental role is to contribute to protecting and enhancing our natural, built and historic environment; including making effective use of land, helping to improve biodiversity, using natural resources prudently, minimising waste and pollution, and mitigating and adapting to climate change, including moving to a low carbon economy.
- 3.4 One of the core planning principles is to contribute to conserving and enhancing the natural environment and reducing pollution. Planning policies and decisions should contribute to and enhance the natural and local environment by:
- (a) *protecting and enhancing valued landscapes, sites of biodiversity or geological value and soils (in a manner commensurate with their statutory status or identified quality in the development plan);*
 - (b) *recognising the intrinsic character and beauty of the countryside, and the wider benefits from natural capital and ecosystem services – including the*

economic and other benefits of the best and most versatile agricultural land, and of trees and woodland;

- (c) *maintaining the character of the undeveloped coast, while improving public access to it where appropriate;*
- (d) *minimising impacts on and providing net gains for biodiversity, including by establishing coherent ecological networks that are more resilient to current and future pressures;*
- (e) *preventing new and existing development from contributing to, being put at unacceptable risk from, or being adversely affected by, unacceptable levels of soil, air, water or noise pollution or land instability. Development should, wherever possible, help to improve local environmental conditions such as air and water quality, taking into account relevant information such as river basin management plans; and*
- (f) *remediating and mitigating despoiled, degraded, derelict, contaminated and unstable land, where appropriate.*

3.5 Paragraph 180 of the NPPF states Planning policies and decisions should also ensure that new development is appropriate for its location taking into account the likely effects (including cumulative effects) of pollution on health, living conditions and the natural environment, as well as the potential sensitivity of the site or the wider area to impacts that could arise from the development. In doing so they should:

- (a) *mitigate and reduce to a minimum potential adverse impacts resulting from noise from new development – and avoid noise giving rise to significant adverse impacts on health and the quality of life (see Explanatory Note to the Noise Policy Statement for England (Department for Environment, Food & Rural Affairs, 2010);*
- (b) *mitigate and reduce to a minimum potential adverse impacts resulting from noise from new development – and avoid noise giving rise to significant adverse impacts on health and the quality of life (see Explanatory Note to the Noise Policy Statement for England (Department for Environment, Food & Rural Affairs, 2010);*
- (c) *limit the impact of light pollution from artificial light on local amenity, intrinsically dark landscapes and nature conservation.*

3.6 The Noise Policy Statement for England (NPSE) was developed by DEFRA and published in March 2010. The vision of the NPSE is to ‘Promote good health and good quality of life through the effective management of noise within the context of Government policy on sustainable development.

3.7 The NPSE aims to ‘Through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy on sustainable development:

- (a) *avoid significant adverse impacts on health and quality of life;*
- (b) *mitigate and minimise adverse impacts on health and quality of life; and*
- where possible, contribute to the improvement of health and quality of life’.*

- 3.8 The Professional Practice Guidance on Planning and Noise (ProPG) has been produced to provide practitioners with guidance on a recommended approach to the management of noise within the planning system in England. The recommended ProPG internal noise level guidelines are described in Table 1. These guidelines reflect and extend current practice contained in BS8233:2014 (Sound Insulation and Noise Reduction for Buildings – Code of Practice). For clarity, blue italic font is used to highlight additions to the guidance contained in Table 4 of BS8233:2014. The dB values provided in the table for different activities are target levels. The table plus supporting notes are referred to as ProPG internal noise level guidelines.

Activity	Location	07:00-23:00hrs	23:00-07:00hrs
Resting	Living room	35dB L _{Aeq,16hr}	-
Dining	Dining room/area	40dB L _{Aeq,16hr}	-
Sleeping (daytime resting)	Bedroom	35dB L _{Aeq,16hr}	30dB L _{Aeq,8hr} 45dB L _{Amax,F}

Table 1

*NOTE 1 The Table provides recommended **internal L_{Aeq} target** levels for overall noise in the design of a building. These are the sum total of structure-borne and airborne noise sources. Ground-borne noise is assessed separately and is not included as part of these targets, as human response to ground-borne noise varies with many factors such as level, character, timing, occupant expectation and sensitivity.*

*NOTE 2 The **internal L_{Aeq} target** levels shown in the Table are based on the existing guidelines issued by the WHO and assume normal diurnal fluctuations in external noise. In cases where local conditions do not follow a typical diurnal pattern, for example on a road serving a port with high levels of traffic at certain times of the night, an appropriate alternative period, e.g. 1 hour, may be used, but the level should be selected to ensure consistency with the **internal L_{Aeq} target** levels recommended in the Table.*

*NOTE 3 These **internal L_{Aeq} target** levels are based on annual average data and do not have to be achieved in all circumstances. For example, it is normal to exclude occasional events, such as fireworks night or New Year's Eve.*

*NOTE 4 Regular individual noise events (for example, scheduled aircraft or passing trains) can cause sleep disturbance. A guideline value may be set in terms of SEL or L_{Amax,F}, depending on the character and number of events per night. Sporadic noise events could require separate values. **In most circumstances in noise sensitive rooms at night (e.g. bedrooms) good acoustic design can be used so that individual noise events do not normally exceed 45dB L_{Amax,F} more than 10 times a night.** However, where it is not reasonably practicable to achieve this guideline then the judgement of acceptability will depend not only on the maximum noise levels but also on factors such as the source, number, distribution, predictability and regularity of noise events (see Appendix A).*

NOTE 5 Designing the site layout and the dwellings so that the internal target levels can be achieved with open windows in as many properties as possible demonstrates good acoustic design. Where it is not possible to meet internal target levels with windows open, internal noise levels can be assessed with windows closed, however any façade openings used to provide whole dwelling ventilation (e.g. trickle ventilators) should be assessed in the “open” position and, in this scenario, the internal L_{Aeq} target levels should not normally be exceeded, subject to the further advice in Note 7.

NOTE 6 Attention is drawn to the requirements of the Building Regulations.

NOTE 7 Where development is considered necessary or desirable, despite external noise levels above WHO guidelines, the internal L_{Aeq} target levels may be relaxed by up to 5 dB and reasonable internal conditions still achieved. The more often internal L_{Aeq} levels start to exceed the internal L_{Aeq} target levels by more than 5 dB, the more that most people are likely to regard them as “unreasonable”. Where such exceedances are predicted, applicants should be required to show how the relevant number of rooms affected has been kept to a minimum. Once internal L_{Aeq} levels exceed the target levels by more than 10 dB, they are highly likely to be regarded as “unacceptable” by most people, particularly if such levels occur more than occasionally. Every effort should be made to avoid relevant rooms experiencing “unacceptable” noise levels at all and where such levels are likely to occur frequently, the development should be prevented in its proposed form (see Section 3.D).

4. NOISE OUTLINE

- 4.1 In order to determine the environmental noise level, consideration must be given to the noise levels on the site from the presence of urban traffic movements and nearby commercial activities.
- 4.2 Given the proposed site, measurements were obtained at second floor level at a location indicative of the proposed second floor residential accommodation that will be closest to the dominant noise source affecting the site (existing installation of mechanical plant).
- 4.3 This measurement location was chosen to represent worst case noise levels that would be experienced at the façades of the residential accommodation.
- 4.4 The particulars of the measurement exercise are recorded below:

Date: 25-28 October 2019
Start Time: 12:05 hrs
Location: Second floor level overlooking southern side of site.

- 4.5 The measurements carried out during the exercise are recorded below.

$L_{Aeq, 5mins}$ (dB re 20 μ Pa) - average equivalent sound pressure level
 $L_{Amax, 5mins}$ (dB re 20 μ Pa) - maximum sound pressure level

- 4.6 The measurements obtained during the exercise are presented in Appendix A.

5. EQUIPMENT

All measurements were obtained using the following equipment:

- Svantek Svan971 Class 1 Serial No. 51704
- Rion Calibrator Type NC-74 Class 1 Serial No. 00410215

- 5.1 The relevant equipment carries full and current traceable calibration. The equipment, where necessary, was calibrated prior to and after the measurements were carried out.

6. NOISE OUTLINE

New residential accommodation

- 6.1 Given the monitoring positions and the measurements obtained, it is possible to calculate the $L_{Aeq,T}$ values experienced during the day and night-time periods.
- 6.2 When determining an internal noise level, BS8233 specifies a design range in terms of $L_{Aeq,T}$. With regard to T, BS8233 states "*The time period should be appropriate for the activity involved (e.g. 23:00-07:00 for bedrooms)*".
- 6.3 For the purposes of this report and in line with the recommendations of the supplementary planning document and BS8233, the following time periods are considered.
 - (a) *07:00 hrs to 23:00 hrs for living, dining rooms & studios (day)*
 - (b) *23:00 hrs to 07:00 hrs for bedrooms (night)*
- 6.4 In accordance with these time periods, the appropriate average $L_{Aeq,T}$ level during the relevant period has been considered. This has been calculated based on the $L_{Aeq,5min}$ measurements obtained during the assessment.

Location	L_{Aeq}	L_{Amax}
07:00 – 23:00	58	-
23:00 – 07:00	57	71

Table 2

- 6.5 BS8233 refers to maximum levels that are "not normally exceeded". From the data collected, typical maximum levels were calculated in the spirit of BS8233 and in line with the recommendations of ProPG, the 10th highest $L_{Amax,F}$ level was chosen. ProPG states as follows:
 - "*In noise-sensitive rooms at night (e.g. bedrooms) individual noise events (from all sources) should not normally exceed 45dB $L_{Amax,F}$ more than 10 times a night as this represents a threshold below which the effects of individual noise events on sleep can be regarded as negligible.*"

Outside amenity spaces

- 6.6 When considering external noise levels and the noise levels experienced within the proposed amenity areas, BS8233:2014 “Guidance on sound insulation and noise reduction for buildings” states:

“For traditional external areas that are used for amenity space, such as gardens and patios, it is desirable that the external noise level does not exceed 50 dB LAeq,T, with an upper guideline value of 55 dB LAeq,T which would be acceptable in noisier environments. However, it is also recognized that these guideline values are not achievable in all circumstances where development might be desirable. In higher noise areas, such as city centres or urban areas adjoining the strategic transport network, a compromise between elevated noise levels and other factors, such as the convenience of living in these locations or making efficient use of land resources to ensure development needs can be met, might be warranted. In such a situation, development should be designed to achieve the lowest practicable levels in these external amenity spaces, but should not be prohibited.”

- 6.7 Further, World Health Organisation (WHO) “Guidelines on Community Noise” suggests a maximum external noise level of 55 dB(A) L_{Aeq} between 7am and 11pm.
- 6.8 Onsite noise measurements show that the first floor façade facing onto the existing installation of mechanical plant located at ground and lower ground floor levels experience average noise levels of 58dB L_{Aeq} during the daytime period, given that the proposed amenity areas are to be located at sixth floor level and set back from the building boundary and so at a greater distance away from commercial activities / plant noise and will be further afforded screening by the building envelope, this would reduce the noise level to below the upper guideline value of 55dB L_{Aeq,T}. for these external amenity spaces.

7. GLAZING RECOMMENDATIONS

- 7.1 With regard to site noise levels, the average daytime and night time noise levels recorded are detailed within Table 2, the full measurement results are presented in Appendix A.
- 7.2 It is recommended that in order to meet the LPA requirements, acoustic fenestration measures be considered in order to protect the daytime and night time amenity of future occupiers, it is understood that mechanical ventilation is to be provided to the residential units and so passive / trickle ventilation elements will not need to be considered within the calculation exercises.
- 7.3 To reduce daytime and night time noise exposure in the proposed dwellings, attention should be given to the sound insulation of the façade of the building. The windows will normally be the weakest part of any façade.
- 7.4 Based on outline information supplied, it is anticipated the proposed external wall constructions will have an insulation value of around R_w 74dB for the wall system. The proposed roof construction will have an insulation value of around R_w 58dB these performance values were obtained from proprietary prediction software 'Insul' produced by Marshall Day, a copy of the prediction outputs is contained within Appendix B of this report. The predicted outputs obtained from Insul have been corrected to account for laboratory predictions and their likely performance when installed onsite, a nominal -7-9dB correction has been assumed for the different constructions. Given the external noise levels it is recommended that the glazing performances be considered. These will provide the necessary sound insulation values to reduce the internal noise levels to an acceptable level.

- 7.5 From the calculated levels it is possible to predict the internal noise levels within habitable rooms. In order to undertake this, consideration has been given to the following formula:

$$SPL_{in} = SPL_{out} + 10 \log_{10} \left(\frac{A_0}{S} 10^{\frac{-D_{n,e}}{10}} + \frac{S_{wi}}{S} 10^{\frac{-R_{wi}}{10}} + \frac{S_{ew}}{S} 10^{\frac{-R_{ew}}{10}} + \frac{S}{A} \right) + 3$$

where:
 SPL_{in} = sound pressure level inside the room
 SPL_{out} = highest sound pressure level outside the room
 A_0 = reference absorption area of $10m^2$
 S_{wi} = area in m^2 of the windows of the room
 S_{ew} = area in m^2 of the external wall of the room
 R_{wi} = weighted sound reduction index of window ($R_w + C_{tr}$)
 R_{ew} = weighted sound reduction index of external wall
 S = area through which sound is transmitted (m^2)
 A = amount of acoustic absorption in room (m^2)
 K = a numerical factor associated with sound incidence

Equation 1

- 7.6 Room dimensions and the size of windows have been extracted from scaled drawings. For the purposes of the calculation exercises, a typical example of a room type at various levels has been considered.
- 7.7 Due to the varying methods of quantifying the sound insulation performance of building elements, the following parameters are described:
- R_w Weighted Sound Reduction Index: Single figure sound insulation value derived from the measured sound reduction index R .
 - C_{tr} Spectrum adaptation term: The correction to a sound insulation quantity (such as $D_{nT,w}$) to take account of a specific sound spectra. See BS EN ISO 717 – 1: 1997 – Noise spectrum No. 2 - noise from traffic, aircraft, factories, railways and disco's
- 7.8 To meet the criteria, Equation 1 was rearranged in terms of R_w (the sound reduction index of the window). The window specification required in order to achieve the internal noise levels as set out in BS8233 are as shown in Table 3, the rooms chosen are typical of worst case scenarios of rooms with the largest areas of glazing combined with the smallest volumes at various floor levels of the building. Details of the elements considered within the calculation exercises are contained within Appendix C of this report.

Location	Room use	Sound Reduction Index Glazing (R_w)
First floor	Master bedroom	34
First floor	Bedroom2	34
Second floor	Kitchen diner	32
Third floor	Studio	33
Fifth floor	Studio	34

Table 3

- 7.9 Suggested window specifications are detailed in Appendix D. These windows have published R_w performances. The published performance figures for these windows were obtained from laboratory measurements of the glass only. The best workmanship practices and installation guidelines should be followed to ensure that the stated performances can be obtained once installed.
- 7.10 Alternatively, it is highly recommended that the glazing is over specified to allow a 5dB workmanship tolerance (hence requirement = $R_w + 5$ dB workmanship correction, required especially at 125Hz and 250Hz frequencies) or a tested glazing system (glass and frame) with the required octave band performance levels is chosen.
- 7.11 To achieve the values of sound reduction required by the glazing, the following configurations could be utilised, these products (taken from Guardian Glass), are available on the market and would meet the performance criteria, other manufacturers are available. Details of the systems are contained within Appendix D.

Glazing configuration examples:

Guardian Glass 6mm float glass /10mm void/ 4mm float glass R_w 34dB

Guardian Glass 6mm float glass /10mm void/ 3mm float glass R_w 33dB

Guardian Glass 5mm float glass /10mm void/ 3mm float glass R_w 32dB

Purge Ventilation

7.12 Ventilation requirements for dwellings (and other buildings) are covered under the Building Regulations 'Approved Document F – Means of Ventilation, 2010 Edition1 (ADF). Unfortunately, ADF contains very little information on the potential interactions between ventilation and the acoustic design of dwellings.

7.13 ADF requires that:

- *"There shall be adequate means of ventilation provided for people in the building"*
- *"Ventilation is simply the removal of 'stale' indoor air from a building and its replacement with 'fresh' outside air".*

7.14 Ventilation is required for one or more of the following purposes:

- a) *Provision of outside air for breathing;*
- b) *Dilution and removal of airborne pollutants, including odours;*
- c) *Control of excess humidity (arising from water vapour in the indoor air);*
- d) *Provision of air for fuel-burning appliances (which is covered under Part J of the Building Regulations).*

7.15 Ventilation may also provide a means to control thermal comfort but this is not controlled under the Building Regulations. Part L addresses minimising energy use due to the effects of solar gain in summer.'

- 7.16 ADF describes three types of ventilation provision and associated ventilation rates. The types of ventilation are summarised below:

Type of ventilation	Location / Reason for ventilation	When is this required
Whole Dwelling Ventilation	To provide fresh air to the building and to dilute and disperse residual water vapour not dealt with by extract ventilation as well as removing water vapour and other pollutants which are released throughout the building	Continuously
Extract Ventilation	From rooms where most water vapour and/or pollutants are released, e.g. due to activities such as cooking, bathing or photocopying. This is to minimise their spread to the rest of the building.	Continuous or Intermittent
Purge Ventilation	Throughout the building to aid removal of high concentrations of pollutants and water vapour released from occasional activities such as painting and decorating or accidental releases such as smoke from burnt food or spillage of water.	Occasionally

Table 4

- 7.17 It is proposed to install ‘whole dwelling ventilation’ to each residential unit.
- 7.18 In addition to the above ADF also states:
- *“Purge ventilation provisions may also be used to improve thermal comfort, although this is not controlled under the Building Regulations.”*
- 7.19 With reference to the provision of purge ventilation within habitable rooms, the approved document provides the following note. ‘There may be practical difficulties in achieving this (e.g. if unable to open a window due to excessive noise from outside).’ However, no objective guidance is provided in the Approved Document as to what constitutes “excessive noise” or how to resolve the practical difficulties.
- 7.20 Given the measured noise levels at the site and during occasions when purge ventilation is required with the windows open it should be noted that the acoustic performance of the building envelope will be reduced, typically reducing the insulation to no more than 10 to 15 dB(A). Most residents value the ability to open windows at will, for a variety of reasons but the internal target noise levels can only be practically achieved with windows closed. This is the case as this site is in an urban area adjacent to transportation noise sources.
- 7.21 It should also be noted that the internal noise level guidelines are generally not applicable under “purge ventilation” conditions as defined by Building Regulations Approved Document F, as this should only occur occasionally (e.g. to remove odour from painting and decorating or from burnt food).

8. CONCLUSION

- 8.1 Based on the foregoing, it can be concluded that:
- (a) *The average and maximum noise levels measured at the proposed development during the day and night time periods are detailed in Table 2;*
 - (b) *It has been demonstrated that the internal noise level requirements of Camden Council can be met;*
 - (c) *The minimum required glazing performances are detailed in Table 3;*
 - (d) *The required level of sound insulation needed to achieve this internal level is based on the considered building envelope make up and measured external noise levels with the windows closed.*
- 8.2 The noise level within the proposed sixth floor roof level amenity area will be below the upper guideline value of 55dB L_{Aeq, T}.

Figures

Alliance House, 29-30 High Holborn, WC1V 6AZ and surrounding area



Figure 1



Figure 2



Figure 3



Figure 3



Figure 4



Figure 5



Figure 6



Figure 7



Figure 8



Figure 9

Appendix A

No.	Date & time	LAFmax	LAeq	Leq 125 Hz	Leq 250 Hz	Leq 500 Hz	Leq 1000 Hz	Leq 2000 Hz	Leq 4000 Hz	Lzmax125 Hz	Lzmax250 Hz	Lzmax500 Hz	Lzmax1000 Hz	Lzmax2000 Hz	Lzmax 4000 Hz
370	26/10/2019 18:50:00	57	54	58	58	53	48	43	36	63	62	56	54	48	42
371	26/10/2019 18:55:00	56	53	57	56	52	48	42	35	62	60	57	50	47	43
372	26/10/2019 19:00:00	56	54	57	56	53	48	42	35	62	61	57	51	48	43
373	26/10/2019 19:05:00	57	55	57	60	53	49	43	36	62	64	58	51	46	45
374	26/10/2019 19:10:00	57	55	57	58	54	49	43	37	61	61	59	54	50	44
375	26/10/2019 19:15:00	62	55	57	57	53	49	44	36	65	61	61	60	55	43
376	26/10/2019 19:20:00	63	55	58	58	54	49	44	36	68	65	63	59	51	44
377	26/10/2019 19:25:00	56	54	57	57	53	48	43	36	61	60	58	51	48	45
378	26/10/2019 19:30:00	56	54	57	56	52	48	42	35	61	60	57	52	49	45
379	26/10/2019 19:35:00	56	53	57	56	52	48	42	35	62	60	57	52	50	45
380	26/10/2019 19:40:00	56	53	57	56	52	48	42	35	62	60	58	50	48	45
381	26/10/2019 19:45:00	56	54	57	58	53	49	43	36	62	61	58	51	46	45
382	26/10/2019 19:50:00	56	54	57	57	53	49	43	36	62	61	58	51	46	45
383	26/10/2019 19:55:00	56	53	57	56	52	48	42	35	62	61	57	51	46	47
384	26/10/2019 20:00:00	56	54	57	56	53	48	42	35	61	60	57	51	44	41
385	26/10/2019 20:05:00	58	53	57	56	52	48	42	35	63	61	57	56	51	43
386	26/10/2019 20:10:00	56	54	57	56	52	48	42	35	62	60	56	52	47	45
387	26/10/2019 20:15:00	58	54	58	58	53	48	42	35	64	65	57	51	46	42
388	26/10/2019 20:20:00	56	54	58	57	53	49	43	35	61	61	57	52	46	40
389	26/10/2019 20:25:00	57	54	57	56	52	48	42	40	62	60	56	50	48	52
390	26/10/2019 20:30:00	56	53	57	56	52	48	42	35	62	61	57	51	47	41
391	26/10/2019 20:35:00	56	53	57	56	52	48	42	35	63	60	56	51	45	43
392	26/10/2019 20:40:00	55	53	57	56	52	48	42	35	62	60	55	51	47	45
393	26/10/2019 20:45:00	56	54	57	57	53	48	43	36	62	61	58	51	46	42
394	26/10/2019 20:50:00	57	54	57	57	53	49	43	35	63	62	57	55	46	38
395	26/10/2019 20:55:00	62	54	57	56	53	49	43	35	63	62	63	59	51	43
396	26/10/2019 21:00:00	59	54	58	56	52	48	42	35	67	65	58	51	43	46
397	26/10/2019 21:05:00	57	54	57	56	53	48	42	35	62	62	57	51	44	40
398	26/10/2019 21:10:00	58	53	57	56	52	48	42	35	63	66	55	51	47	47
399	26/10/2019 21:15:00	56	54	57	57	53	49	42	35	64	63	58	51	44	42
400	26/10/2019 21:20:00	57	54	58	57	52	49	43	35	62	62	57	51	45	40
401	26/10/2019 21:25:00	56	53	57	56	52	48	42	35	62	62	58	52	47	40
402	26/10/2019 21:30:00	56	53	57	56	52	48	42	35	62	60	57	50	44	40
403	26/10/2019 21:35:00	55	53	57	56	52	48	42	35	62	61	57	51	46	40
404	26/10/2019 21:40:00	56	54	57	56	53	48	42	35	68	62	57	53	46	44
405	26/10/2019 21:45:00	56	54	58	57	53	48	42	35	63	62	57	53	45	43
406	26/10/2019 21:50:00	56	54	57	57	53	49	43	35	62	63	56	51	45	37
407	26/10/2019 21:55:00	56	54	57	56	52	48	42	35	62	61	57	51	46	40
408	26/10/2019 22:00:00	56	53	57	56	52	48	42	35	62	61	58	51	43	42
409	26/10/2019 22:05:00	56	53	57	56	52	48	42	35	61	60	58	50	44	39
410	26/10/2019 22:10:00	56	53	57	56	52	48	42	35	63	61	58	50	43	36
411	26/10/2019 22:15:00	56	54	58	57	52	48	42	35	61	62	57	51	48	45
412	26/10/2019 22:20:00	56	54	58	57	53	48	43	36	63	61	58	51	46	38
413	26/10/2019 22:25:00	56	54	57	56	53	48	43	35	62	60	57	51	47	38
414	26/10/2019 22:30:00	55	53	57	56	52	48	42	35	62	60	55	51	44	38
415	26/10/2019 22:35:00	56	53	57	56	52	48	42	34	63	61	58	51	43	36
416	26/10/2019 22:40:00	57	53	57	56	52	48	42	35	62	60	57	51	43	36
417	26/10/2019 22:45:00	57	53	57	56	52	48	42	35	61	60	56	54	48	40
418	26/10/2019 22:50:00	56	54	58	57	53	48	42	35	63	61	58	51	45	40
419	26/10/2019 22:55:00	56	53	57	56	52	48	42	35	62	60	56	51	44	38
420	26/10/2019 23:00:00	57	55	58	59	53	49	42	36	63	63	56	52	45	41
421	26/10/2019 23:05:00	56	55	58	58	53	49	43	36	62	61	57	52	46	37
422	26/10/2019 23:10:00	55	53	57	56	52	48	42	35	62	61	56	50	45	39
423	26/10/2019 23:15:00	55	53	57	56	52	48	42	35	63	60	56	50	46	38
424	26/10/2019 23:20:00	55	53	57	56	52	48	42	34	61	61	56	50	43	36
425	26/10/2019 23:25:00	56	53	58	56	52	48	42	35	62	61	57	50	46	41
426	26/10/2019 23:30:00	55	53	57	56	52	48	42	35	61	60	57	52	45	40
427	26/10/2019 23:35:00	56	54	57	58	53	49	43	36	62	61	57	51	45	39
428	26/10/2019 23:40:00	56	54	57	57	53	48	43	35	62	61	58	51	45	38
429	26/10/2019 23:45:00	55	53	57	56	52	48	42	35	63	61	55	51	44	38
430	26/10/2019 23:50:00	57	54	58	56	52	48	42	35	65	62	58	50	43	39
431	26/10/2019 23:55:00	55	53	57	56	52	48	42	35	62	60	55	50	45	37
432	27/10/2019 00:00:00	55	53	57	56	52	48	42	34	62	61	59	56	50	43
433	27/10/2019 00:05:00	59	54	57	57	52	48	42	35	61	61	57	55	50	45
434	27/10/2019 00:10:00	56	54	57	57	53	48	43	36	62	61	57	51	45	38
435	27/10/2019 00:15:00	56	53	57	56	52	48	42	35	61	61	58	51	45	39
436	27/10/2019 00:20:00	56	53	57	56	52	48	42	34	62	61	56	50	48	39
437	27/10/2019 00:25:00	57	53	57	56	52	48	42	35	62	60	55	53	49	46
438	27/10/2019 00:30:00	56	53	57	56	52	48	42	34	62	60	57	51	44	36
439	27/10/2019 00:35:00	57	53	57	56	52	48	42	35	62	60	54	55	51	37
440	27/10/2019 00:40:00	61	54	58	57	53	48	42	35	62	62	56	55	53	44
441	27/10/2019 00:45:00	55	54	58	57	52	48	42	35	62	61	56	51	45	38
442	27/10/2019 00:50:00	55	53	57	56	52	48	42	35	63	62	57	50	46	37
443	27/10/2019 00:55:00	55	53	57	56	52	48	42	34	62	61	55	50	45	36
444	27/10/2019 01:00:00	55	53	57	56	52	48	42	35	62	60	57	50	45	38
445	27/10/2019 01:05:00	55	53	57	56	52	48	42	34	62	60	55	51	43	37
446	27/10/2019 01:10:00	56	54	57	56	52	48	42	35	62	61	59	51	46	39
447	27/10/2019 01:15:00	55	54	58	57	53	48	43	35	66	63	62	60	50	44
448	27/10/2019 01:20:00	56	54	57	56	53	48	42	35	6					

No.	Date & time	LAFmax	LAeq	Leq 125 Hz	Leq 250 Hz	Leq 500 Hz	Leq 1000 Hz	Leq 2000 Hz	Leq 4000 Hz	Lzmax125 Hz	Lzmax250 Hz	Lzmax500 Hz	Lzmax1000 Hz	Lzmax 2000 Hz	Lzmax 4000 Hz
862	28/10/2019 11:50:00	66	58	64	60	56	52	47	42	70	67	65	65	64	56
863	28/10/2019 11:55:00	74	63	64	62	58	58	53	56	73	70	67	73	63	68
864	28/10/2019 12:00:00	69	60	64	65	57	53	47	41	69	68	66	58	69	61
865	28/10/2019 12:05:00	63	60	64	65	57	53	47	40	68	67	62	59	52	53
866	28/10/2019 12:10:00	74	63	64	61	59	58	53	54	71	68	69	73	64	65
867	28/10/2019 12:15:00	65	57	63	60	56	52	46	40	69	64	60	57	64	57
868	28/10/2019 12:20:00	64	58	63	60	56	52	46	40	68	63	62	57	59	58

LAeq	Leq 125 Hz	Leq 250 Hz	Leq 500 Hz	Leq 1000 Hz	Leq 2000 Hz	Leq 4000 Hz
25th Oct day	58	62	59	56	52	48
25th Oct night	55	62	58	54	50	44
26th Oct day	55	57	57	53	49	44
26th Oct night	54	57	56	52	48	42
27th Oct day	55	59	58	54	50	44
27th Oct night	57	62	59	56	53	46
28th Oct day	59	64	61	57	54	48

25th and 28th day combined	58	63	60	56	53	48	44
LAFmax	Lzmax125 Hz	Lzmax250 Hz	Lzmax500 Hz	Lzmax1000 Hz	Lzmax 2000 Hz	Lzmax 4000 Hz	
71	71	73	75	67	53	39	

Appendix B

Sound Insulation Prediction (v9.0.8)

Program copyright Marshall Day Acoustics 2017

margin of error is generally within $R_w \pm 3$ dB

- Key No. 2501

Job Name:

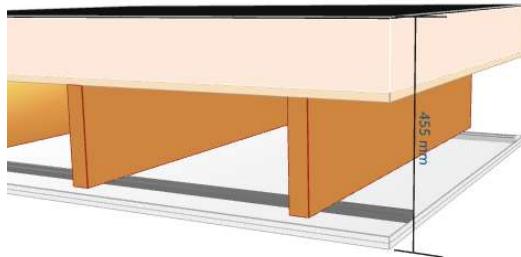
Job No.:

Date: 18/10/2019

File Name: Insu'

Initials: AD

Notes: Roof construction



R_w 58 dB
C -1 dB
Ctr -6 dB

Mass-air-mass resonant frequency = ~32 Hz

Panel Size = 2.7 m x 4.0 m

Partition surface mass = 50.6 kg/m²

System description

Panel 1 : 1 x 4 mm Nuraply waterproof membrane
+ 1 x 18 mm Plywood

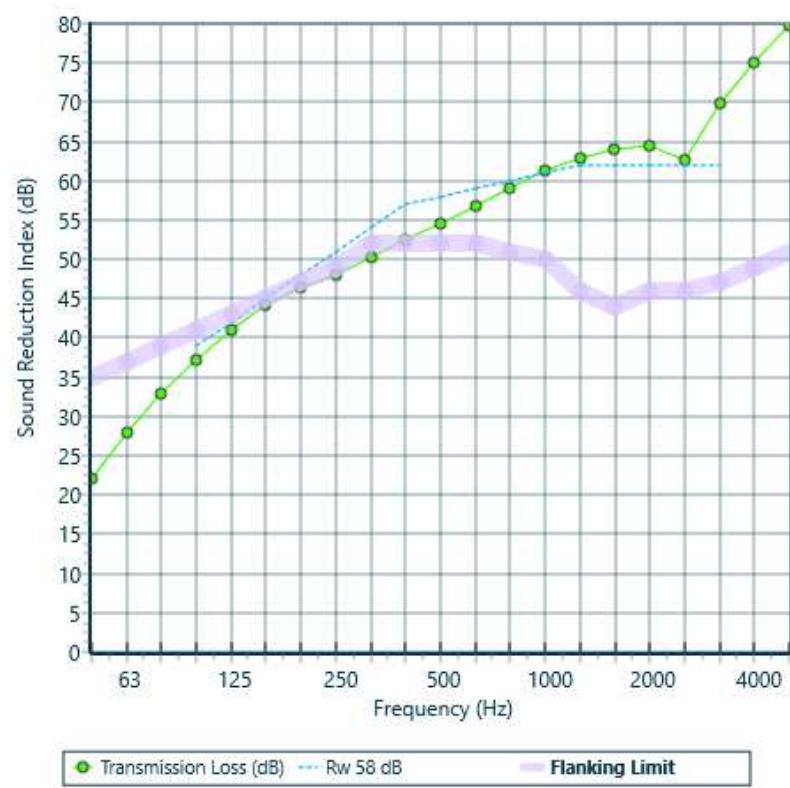
+ 1 x 139.9 mm Kingspan KS 1000AWP 120/140mm

Frame: Solid Joist with resilient rail; Cavity Width 268 mm

Panel 2 + 2 x 12.5 mm Gyproc SoundBloc 12.5mm

Floor Cover: Thickness 0.02 mm

freq.(Hz)	TL(dB)	TL(dB)
50	22	
63	28	26
80	33	
100	37	
125	41	40
160	44	
200	46	
250	48	48
315	50	
400	52	
500	55	54
630	57	
800	59	
1000	61	61
1250	63	
1600	64	
2000	64	64
2500	63	
3150	70	
4000	75	73
5000	80	



Sound Insulation Prediction (v9.0.8)

Program copyright Marshall Day Acoustics 2017

margin of error is generally within $R_w \pm 3$ dB

- Key No. 2501

Job Name:

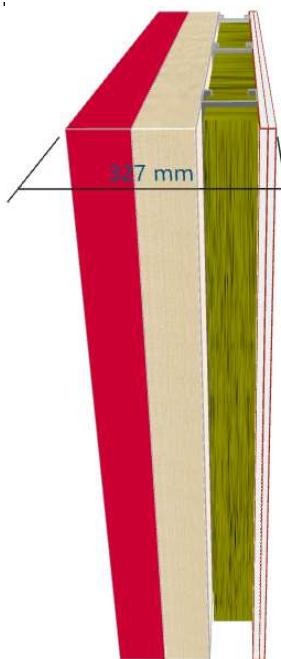
Job No.:

Date.:18/10/2019

File Name:Insu'

Initials:AD

Notes:Wall construction



R_w 74 dB
C -3 dB
Ctr -9 dB

Mass-air-mass resonant frequency = =43 Hz

Panel Size = 2.7 m x 4.0 m

Partition surface mass = 193 kg/m²

System description

Panel 1 : 1 x 102.5 mm Brick

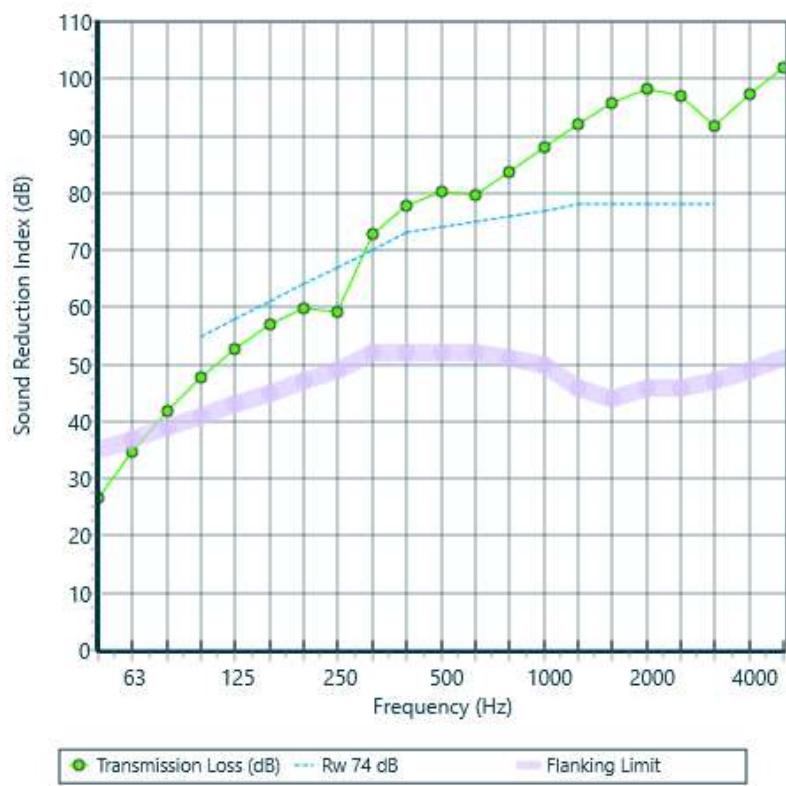
+ 1 x 99.9 mm Kingspan KS 1000LS 100/140mm

Frame: Right steel stud + air gap; Cavity Width 100 mm ,Stud spacing 600 mm , 1 x Fibreglass (10kg/m3) Thickness 100 mm

Panel 2 + 2 x 12.5 mm Gyproc Wallboard 12.5mm

Floor Cover: Thickness 0.02 mm

freq.(Hz)	TL(dB)	TL(dB)
50	27	
63	35	31
80	42	
100	48	
125	53	51
160	57	
200	60	
250	59	61
315	73	
400	78	
500	80	79
630	79	
800	84	
1000	88	87
1250	92	
1600	96	
2000	98	97
2500	97	
3150	92	
4000	97	95
5000	102	



Appendix C

Description	Term	Weighted rating	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	63	60	56	53	48	44	44
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	$Rw,34dB$	27	26	28	37	36	36	36
External Wall	R_{ew}	$R_w,74dB$	44	54	72	80	90	88	88
Roof Construction	R_{rr}	$R_w,N/A\ dB$	100	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.5	7	9	11	11	10	10	10

Derivation	Term	Value
Façade area (including window)	S_f	14
Window area	S_{wi}	4.6
$S_f - S_{wi}$	S_{ew}	9
Area of ceiling	S_{rr}	14
$S_f + S_{rr}$	S	28
Reference absorption area	A_0	10
Room volume	V	35

Description	Term from Equation	Reference letter	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	A	63	60	56	53	48	44	44
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100	100
	$(A_0/S) * 10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	27	26	28	37	36	36	36	36
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00033	0.00042	0.00026	0.00003	0.00004	0.00004	0.00004
External Wall Construction	R_{ew}	44	54	72	80	90	90	90	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00001	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Roof Construction	R_{rr}	100	100	100	100	100	100	100	100
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-35	-34	-36	-45	-44	-44	-44
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10	10	10
	$10\log(S/A)$	G	5.7	4.7	3.9	3.9	4.3	4.3	4.3
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	36.7	33.6	27.3	15.0	11.6	11.6	7.9

RESULTANT INTERNAL NOISE LEVEL**28.7**

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	62	59	56	53	46	41
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	R_w 34dB	27	26	28	37	36	36
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88
Roof Construction	R_{tr}	R_w N/A dB	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.5	7	9	11	11	10	10

Derivation	Term	Value
Façade area (including window)	S_f	14
Window area	S_{wi}	4.6
$S_f - S_{wi}$	S_{ew}	9
Area of ceiling	S_{tr}	14
$S_f + S_{tr}$	S	28
Reference absorption area	A_0	10
Room volume	V	35

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	62	59	56	53	46	41
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S) * 10^{(A_0 - D_{ne,w})/10}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	27	26	28	37	36	36	36
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00033	0.00042	0.00026	0.00003	0.00004	0.00004
External Wall Construction	R_{ew}	44	54	72	80	90	88	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00001	0.00000	0.00000	0.00000	0.00000	0.00000
Roof Construction	R_{tr}		100	100	100	100	100	100
	$(S_{tr}/S) * 10^{(-R_{tr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-35	-34	-36	-45	-44	-44
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10	10
	$10\log(S/A)$	G	5.7	4.7	3.9	3.9	4.3	4.3
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	36.1	33.1	26.7	14.8	9.2	4.3

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{max,ff}$	74dBA	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	$R_w 34dB$	27	26	28	37	36	36
External Wall	R_{ew}	$R_w 74dB$	44	54	72	80	90	88
Roof Construction	R_{tr}	$R_w N/A dB$	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.5	7	9	11	11	10	10

Derivation	Term	Value
Façade area (including window)	S_f	14
Window area	S_{wi}	4.6
$S_f - S_{wi}$	S_{ew}	9
Area of ceiling	S_{tr}	14
$S_f + S_{tr}$	S	28
Reference absorption area	A_0	10
Room volume	V	35

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S) * 10^{(A_0 - D_{ne,w})/10}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}		27	26	28	37	36	36
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00033	0.00042	0.00026	0.00003	0.00004	0.00004
External Wall Construction	R_{ew}		44	54	72	80	90	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00001	0.00000	0.00000	0.00000	0.00000	0.00000
Roof Construction	R_{tr}		100	100	100	100	100	100
	$(S_{tr}/S) * 10^{(-R_{tr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-35	-34	-36	-45	-44	-44
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10	10
	$10\log(S/A)$	G	5.7	4.7	3.9	3.9	4.3	4.3
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	45.5	47.2	46.0	29.3	16.2	2.9

RESULTANT INTERNAL NOISE LEVEL 44.5

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	63	56	53	48	44	
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	$Rw,34dB$	27	26	28	37	36	36
External Wall	R_{ew}	$R_w,74dB$	44	54	72	80	90	88
Roof Construction	R_{rr}	$R_w,N/A\ dB$	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.5	3	5	7	7	6	6

Derivation	Term	Value
Façade area (including window)	S_f	7
Window area	S_{wi}	1.9
$S_f - S_{wi}$	S_{ew}	5
Area of ceiling	S_{rr}	8
$S_f + S_{rr}$	S	15
Reference absorption area	A_0	10
Room volume	V	20

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	63	60	56	53	48	44
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S)*10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	C	0.00025	0.00032	0.00020	0.00003	0.00003	0.00003
External Wall Construction	R_{ew}	D	0.00001	0.00000	0.00000	0.00000	0.00000	0.00000
Roof Construction	R_{rr}	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-36	-35	-37	-46	-45	-45
Total Absorption Area of Receiver Room	A (furnished)		3	5	7	7	6	6
	$10\log(S/A)$	G	7.7	5.1	3.5	3.5	4.3	4.3
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	37.5	32.9	25.8	13.5	10.4	6.7

RESULTANT INTERNAL NOISE LEVEL 28.0

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	62	59	56	53	46	41
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	R_w 34dB	27	26	28	37	36	36
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88
Roof Construction	R_{rr}	R_w N/A dB	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.5	3	5	7	7	6	6

Derivation	Term	Value
Façade area (including window)	S_f	7
Window area	S_{wi}	1.9
$S_f - S_{wi}$	S_{ew}	5
Area of ceiling	S_{tr}	8
$S_f + S_{tr}$	S	15
Reference absorption area	A_0	10
Room volume	V	20

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	62	59	56	53	46	41
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S) * 10^{(A_0 - D_{ne,w})/10}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	27	26	28	37	36	36	36
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.000025	0.000032	0.000020	0.000003	0.000003	0.000003
External Wall Construction	R_{ew}	44	54	72	80	90	88	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.000001	0.000000	0.000000	0.000000	0.000000	0.000000
Roof Construction	R_{rr}	100	100	100	100	100	100	100
	$(S_{tr}/S) * 10^{(-R_{tr}/10)}$	E	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-36	-35	-37	-46	-45	-45
Total Absorption Area of Receiver Room	A (furnished)	3	5	7	7	6	6	6
	$10\log(S/A)$	G	7.7	5.1	3.5	4.3	4.3	4.3
Total Internal Sound Pressure Level, Leg	Leg,2	A+F+G+3	36.9	32.3	25.2	13.3	8.1	3.2

RESULTANT INTERNAL NOISE LEVEL 27.4

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{max,ff}$	74dBA	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	$R_w 34dB$	27	26	28	37	36	36
External Wall	R_{ew}	$R_w 74dB$	44	54	72	80	90	88
Roof Construction	R_{rr}	$R_w N/A dB$	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.5	3	5	7	7	6	6

Derivation	Term	Value
Façade area (including window)	S_f	7
Window area	S_{wi}	1.9
$S_f - S_{wi}$	S_{ew}	5
Area of ceiling	S_{ir}	8
$S_f + S_{rr}$	S	15
Reference absorption area	A_0	10
Room volume	V	20

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S) * 10^{(A_0 - D_{ne,w})/10}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}		27	26	28	37	36	36
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.000025	0.000032	0.000020	0.000003	0.000003	0.000003
External Wall Construction	R_{ew}		44	54	72	80	90	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.000001	0.000000	0.000000	0.000000	0.000000	0.000000
Roof Construction	R_{rr}		100	100	100	100	100	100
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-36	-35	-37	-46	-45	-45
Total Absorption Area of Receiver Room	A (furnished)		3	5	7	7	6	6
	$10\log(S/A)$	G	7.7	5.1	3.5	3.5	4.3	4.3
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	46.3	46.5	44.5	27.8	15.0	1.8

RESULTANT INTERNAL NOISE LEVEL 43.3

Description	Term	Weighted rating	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	63	60	56	53	48	44	44
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100	100
Glazing 5mm float / 10mm / 3mm float	R_w	Rw 32dB	21	25	27	34	39	25	
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88	
Roof Construction	R_{rr}	R_w N/A dB	100	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.75	18	20	22	22	21	21	21

Derivation	Term	Value
Façade area (including window)	S_f	39
Window area	S_{wi}	8.0
$S_f - S_{wi}$	S_{ew}	31
Area of ceiling	S_{rr}	40
$S_f + S_{rr}$	S	79
Reference absorption area	A_0	10
Room volume	V	99

Description	Term from Equation	Reference letter	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	A	63	60	56	53	48	44	44
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100	100
	$(A_0/S) * 10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}		21	25	27	34	39	25	25
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00081	0.00032	0.00020	0.00004	0.00001	0.000032	
External Wall Construction	R_{ew}		44	54	72	80	90	88	
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00002	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Roof Construction	R_{rr}		100	100	100	100	100	100	100
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-31	-35	-37	-44	-49	-35	
Total Absorption Area of Receiver Room	A (furnished)		18	20	22	22	21	21	21
	$10\log(S/A)$	G	6.5	6.1	5.6	5.6	5.8	5.8	
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	41.2	33.8	27.9	17.7	8.0	18.3	

RESULTANT INTERNAL NOISE LEVEL**30.4**

Description	Term	Weighted rating	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	63	60	56	53	48	44	
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100	100
Glazing 6mm float / 10mm / 3mm float	R_w	Rw 33dB	22	25	28	35	36	27	
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88	
Roof Construction	R_{rr}	R_w N/A dB	100	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.75	12	14	16	16	15	15	15

Derivation	Term	Value
Façade area (including window)	S_f	34
Window area	S_{wi}	6.3
$S_f - S_{wi}$	S_{ew}	27
Area of ceiling	S_{rr}	30
$S_f + S_{rr}$	S	64
Reference absorption area	A_0	10
Room volume	V	75

Description	Term from Equation	Reference letter	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	A	63	60	56	53	48	44	
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100	100
	$(A_0/S) * 10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	22	25	28	35	36	36	27	
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00063	0.00031	0.00016	0.00003	0.00003	0.000020	
External Wall Construction	R_{ew}	44	54	72	80	90	90	88	
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00002	0.00000	0.00000	0.00000	0.00000	0.000000	0.000000
Roof Construction	R_{rr}	100	100	100	100	100	100	100	100
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.000000	0.000000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-32	-35	-38	-45	-46	-37	
Total Absorption Area of Receiver Room	A (furnished)		12	14	16	16	15	15	
	$10\log(S/A)$	G	7.1	6.5	5.9	5.9	6.2	6.2	
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	40.8	34.2	27.1	16.8	11.3	16.5	

RESULTANT INTERNAL NOISE LEVEL 30.0

Description	Term	Weighted rating	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	62	59	56	53	46	41	
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100	
Glazing 6mm float / 10mm / 3mm float	R_w	Rw 33dB	22	25	28	35	36	27	
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88	
Roof Construction	R_{rr}	R_w N/A dB	100	100	100	100	100	100	
Total room absorption (based on RT)	RT_{60}	0.75	12	14	16	16	15	15	

Derivation	Term	Value
Façade area (including window)	S_f	34
Window area	S_{wi}	6.3
$S_f - S_{wi}$	S_{ew}	27
Area of ceiling	S_{rr}	30
$S_f + S_{rr}$	S	64
Reference absorption area	A_0	10
Room volume	V	75

Description	Term from Equation	Reference letter	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	A	62	59	56	53	46	41	
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100	
	$(A_0/S) * 10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	
Double Glazed Windows	R_{wi}		22	25	28	35	36	27	
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00063	0.00031	0.00016	0.00003	0.00003	0.000020	
External Wall Construction	R_{ew}		44	54	72	80	90	88	
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00002	0.00000	0.00000	0.00000	0.00000	0.000000	
Roof Construction	R_{rr}		100	100	100	100	100	100	
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000	0.000000	
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-32	-35	-38	-45	-46	-37	
Total Absorption Area of Receiver Room	A (furnished)		12	14	16	16	15	15	
	$10\log(S/A)$	G	7.1	6.5	5.9	5.9	6.2	6.2	
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	40.2	33.6	26.5	16.6	8.9	13.0	

RESULTANT INTERNAL NOISE LEVEL 29.4

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{max,ff}$	74dBA	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 3mm float	R_w	$R_w 33dB$	22	25	28	35	36	27
External Wall	R_{ew}	$R_w 74dB$	44	54	72	80	90	88
Roof Construction	R_{rr}	$R_w N/A dB$	100	100	100	100	100	100
Total room absorption (based on RT)	RT_{60}	0.75	12	14	16	16	15	15

Derivation	Term	Value
Façade area (including window)	S_f	34
Window area	S_{wi}	6.3
$S_f - S_{wi}$	S_{ew}	27
Area of ceiling	S_{tr}	30
$S_f + S_{tr}$	S	64
Reference absorption area	A_0	10
Room volume	V	75

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S) * 10^{(A_0 - D_{ne,w})/10}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}		22	25	28	35	36	27
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.000063	0.000031	0.000016	0.000003	0.000003	0.000020
External Wall Construction	R_{ew}		44	54	72	80	90	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.000002	0.000000	0.000000	0.000000	0.000000	0.000000
Roof Construction	R_{rr}		100	100	100	100	100	100
	$(S_{tr}/S) * 10^{(-R_{tr}/10)}$	E	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-32	-35	-38	-45	-46	-37
Total Absorption Area of Receiver Room	A (furnished)		12	14	16	16	15	15
	$10\log(S/A)$	G	7.1	6.5	5.9	5.9	6.2	6.2
Total Internal Sound Pressure Level, Leg	Leg,2	A+F+G+3	49.6	47.7	45.8	31.1	15.9	11.6

RESULTANT INTERNAL NOISE LEVEL 44.8

Description	Term	Weighted rating	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	63	60	56	53	48	44	
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	R_w 34dB	27	26	28	37	36	36	
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88	
Roof Construction	R_{rr}	R_w 58 dB	31	39	45	52	55	64	
Total room absorption (based on RT)	$R_{T_{60}}$	0.75	12	14	16	16	15	15	15

Derivation	Term	Value
Façade area (including window)	S_f	34
Window area	S_{wi}	6.3
$S_f - S_{wi}$	S_{ew}	27
Area of ceiling	S_{rr}	30
$S_f + S_{rr}$	S	64
Reference absorption area	A_0	10
Room volume	V	75

Description	Term from Equation	Reference letter	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	A	63	60	56	53	48	44	
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100	100
	$(A_0/S) * 10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	27	26	28	37	36	36		
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00020	0.00025	0.00016	0.00002	0.00003	0.00003	
External Wall Construction	R_{ew}	44	54	72	80	90	90		
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00002	0.00000	0.00000	0.00000	0.00000	0.00000	
Roof Construction	R_{rr}	31	39	45	52	55	55		
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.00038	0.00006	0.00001	0.00000	0.00000	0.00000	
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-32	-35	-38	-46	-46	-46	-46
Total Absorption Area of Receiver Room	A (furnished)		12	14	16	16	15	15	15
	$10\log(S/A)$	G	7.1	6.5	5.9	5.9	6.2	6.2	6.2
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	40.4	34.1	27.5	15.4	11.5	7.6	7.6

RESULTANT INTERNAL NOISE LEVEL 29.8

Description	Term	Weighted rating	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	58dBA	62	59	56	53	46	41	
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	Rw 34dB	27	26	28	37	36	36	
External Wall	R_{ew}	R_w 74dB	44	54	72	80	90	88	
Roof Construction	R_{rr}	R_w 58 dB	31	39	45	52	55	64	
Total room absorption (based on RT)	RT_{60}	0.75	12	14	16	16	15	15	15

Derivation	Term	Value
Façade area (including window)	S_f	34
Window area	S_{wi}	6.3
$S_f - S_{wi}$	S_{ew}	27
Area of ceiling	S_{rr}	30
$S_f + S_{rr}$	S	64
Reference absorption area	A_0	10
Room volume	V	75

Description	Term from Equation	Reference letter	125	250	500	1000	2000	Octave Band Centre Frequency (Hz)	4000
Freefield External Noise Level	$L_{eq,ff}$	A	62	59	56	53	46	41	
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100	100
	$(A_0/S) * 10^{(-D_{ne,w}/10)}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	27	26	28	37	36	36		
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.00020	0.00025	0.00016	0.00002	0.00003	0.00003	
External Wall Construction	R_{ew}	44	54	72	80	90	90		
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.00002	0.00000	0.00000	0.00000	0.00000	0.00000	
Roof Construction	R_{rr}	31	39	45	52	55	55		
	$(S_{rr}/S) * 10^{(-R_{rr}/10)}$	E	0.00038	0.00006	0.00001	0.00000	0.00000	0.00000	
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-32	-35	-38	-46	-46	-46	-46
Total Absorption Area of Receiver Room	A (furnished)		12	14	16	16	15	15	15
	$10\log(S/A)$	G	7.1	6.5	5.9	5.9	6.2	6.2	6.2
Total Internal Sound Pressure Level, Leq	$Leq,2$	A+F+G+3	39.8	33.6	26.9	15.2	9.2	4.1	4.1

RESULTANT INTERNAL NOISE LEVEL **29.2**

Description	Term	Weighted rating	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{max,ff}$	74dBA	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,w}$	Dne,w N/A	100	100	100	100	100	100
Glazing 6mm float / 10mm / 4mm float	R_w	$R_w 34dB$	27	26	28	37	36	36
External Wall	R_{ew}	$R_w 74dB$	44	54	72	80	90	88
Roof Construction	R_{rr}	$R_w 58 dB$	31	39	45	52	55	64
Total room absorption (based on RT)	RT_{60}	0.75	12	14	16	16	15	15

Derivation	Term	Value
Façade area (including window)	S_f	34
Window area	S_{wi}	6.3
$S_f - S_{wi}$	S_{ew}	27
Area of ceiling	S_{tr}	30
$S_f + S_{tr}$	S	64
Reference absorption area	A_0	10
Room volume	V	75

Description	Term from Equation	Reference letter	125	250	500	1000	2000	4000
Freefield External Noise Level	$L_{eq,ff}$	A	71	73	75	67	53	39
Mechanical ventilation	$D_{ne,e}$		100	100	100	100	100	100
	$(A_0/S) * 10^{(A_f - D_{ne,w})/10}$	B	0.000000	0.000000	0.000000	0.000000	0.000000	0.000000
Double Glazed Windows	R_{wi}	27	26	28	37	36	36	36
	$(S_{wi}/S) * 10^{(-R_{wi}/10)}$	C	0.000020	0.000025	0.000016	0.000002	0.000003	0.000003
External Wall Construction	R_{ew}	44	54	72	80	90	88	88
	$(S_{ew}/S) * 10^{(-R_{ew}/10)}$	D	0.000002	0.000000	0.000000	0.000000	0.000000	0.000000
Roof Construction	R_{rr}	31	39	45	52	55	64	64
	$(S_{tr}/S) * 10^{(-R_{tr}/10)}$	E	0.000038	0.000006	0.000001	0.000000	0.000000	0.000000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-32	-35	-38	-46	-46	-46
Total Absorption Area of Receiver Room	A (furnished)		12	14	16	16	15	15
	$10\log(S/A)$	G	7.1	6.5	5.9	5.9	6.2	6.2
Total Internal Sound Pressure Level, Leg	Leg,2	A+F+G+3	49.2	47.7	46.2	29.8	16.2	2.7

RESULTANT INTERNAL NOISE LEVEL 44.9

Appendix D



Acoustic Performance

Glazing Configuration

6mm Float Glass

10mm Cavity

4mm Float Glass

Sound Reduction Indices

Frequency, Hz / dB						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000					
27	26	28	37	36	29	34	-1	-3	29	34

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within ±2 dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information please consult Assumptions and Terminology section in Guardian Acoustic Assistant.



Acoustic Performance

Glazing Configuration

6mm Float Glass

10mm Cavity

3mm Float Glass

Sound Reduction Indices

Frequency, Hz / dB						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000					
22	25	28	35	36	27	33	-1	-4	28	32

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within ±2 dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information please consult Assumptions and Terminology section in Guardian Acoustic Assistant.



Acoustic Performance

Glazing Configuration

5mm Float Glass

10mm Cavity

3mm Float Glass

Sound Reduction Indices

Frequency, Hz / dB						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000					
21	25	27	34	39	25	32	0	-3	27	32

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within ±2 dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information please consult Assumptions and Terminology section in Guardian Acoustic Assistant.