

# Basement Impact Assessment

in connection with proposed development at

No. 5 Camden Road

Camden

London

NW1 9LG

for

Kentish Town Spaces (UK) Ltd

LBH4577 Ver. 1.1

September 2019

LBH WEMBLEY  

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ENGINEERING

## Document Control

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## Executive Summary

It is proposed to construct a single level of basement beneath the entire footprint of an existing retail premises at No. 5 Camden Road.

This report provides an assessment of the potential impacts that the basement development may have upon the surrounding area, neighbouring structures and the local environment.

### Geology

The proposed basement will extend into the London Clay.

### Hydrogeological Impacts

There is no shallow groundwater table at this site and hence no scope for the basement to cause adverse hydrogeological impacts to be caused by the proposed basement construction.

### Hydrological Impacts

There will be no change to the flood risk at the site or neighbouring sites.

A SuDS scheme is to be included as part of the development.

### Stability Impacts

Ground movement assessments have been undertaken to demonstrate the acceptability of the proposed construction methodology upon the neighbouring structures, resulting in a prediction of Burland Category 1 "Very Slight" damage.

### Conclusion

The assessment concludes that no adverse residual or cumulative stability, hydrological or hydrogeological impacts are expected to either neighbouring structures or the wider environment as a result of this development.

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## Foreword-Guidance Notes

### GENERAL

This report has been prepared for a specific client and to meet a specific brief. The preparation of this report may have been affected by limitations of scope, resources or time scale required by the client. Should any part of this report be relied on by a third party, that party does so wholly at its own risk and LBH WEMBLEY disclaims any liability to such parties.

The observations and conclusions described in this report are based solely upon the agreed scope of work. LBH WEMBLEY has not performed any observations, investigations, studies or testing not specifically set out in the agreed scope of work and cannot accept any liability for the existence of any condition, the discovery of which would require performance of services beyond the agreed scope of work.

### VALIDITY

Any use of or reliance upon the report in circumstances other than those for which it was commissioned shall be at the client's sole risk. The passage of time may result in changes in site conditions, regulatory or other legal provisions, technology or economic conditions which could render the report inaccurate or unreliable. The information and conclusions contained in this report should therefore not be relied upon in such altered circumstances.

### THIRD PARTY INFORMATION

The report may present an opinion based upon information received from third parties. However, no liability can be accepted for any inaccuracies or omissions in that information.

# 1. Introduction

## 1.1 Background

It is proposed to construct a basement beneath the entire footprint of the existing property at No. 5 Camden Road.

## 1.2 Brief

LBH WEMBLEY have been appointed by Kentish Town Spaces (UK) Ltd to complete a Basement Impact Assessment (BIA) in support of a forthcoming planning application to be submitted to the London Borough of Camden, in order to satisfy the specific requirements of the 2018 Camden Planning Guidance (CPG) on Basements, and associated 2010 Camden Geological, Hydrogeological and Hydrological Study.

## 1.3 Planning Policy

The 2017 Camden Local Plan Policy A5 Basements reads as follows:

*"The Council will only permit basement development where it is demonstrated to its satisfaction that the proposal would not cause harm to:*

- a) neighbouring properties;*
- b) the structural, ground, or water conditions of the area;*
- c) the character and amenity of the area;*
- d) the architectural character of the building; and*
- e) the significance of heritage assets.*

*In determining proposals for basements and other underground development, the Council will require an assessment of the scheme's impact on drainage, flooding, groundwater conditions and structural stability in the form of a Basement Impact Assessment and where appropriate, a Basement Construction Plan.*

*The siting, location, scale and design of basements must have minimal impact on, and be subordinate to, the host building and property. Basement development should:*

- f) not comprise of more than one storey;*
- g) not be built under an existing basement;*
- h) not exceed 50% of each garden within the property;*
- i) be less than 1.5 times the footprint of the host building in area;*
- j) extend into the garden no further than 50% of the depth of the host building measured from the principal rear elevation;*
- k) not extend into or underneath the garden further than 50% of the depth of the garden;*
- l) be set back from neighbouring property boundaries where it extends beyond the footprint of the host building; and*
- m) avoid the loss of garden space or trees of townscape or amenity value.*

*Exceptions to f. to k. above may be made on large comprehensively planned sites.*

*The Council will require applicants to demonstrate that proposals for basements:*

- n. do not harm neighbouring properties, including requiring the provision of a Basement Impact Assessment which shows that the scheme poses a risk of damage to neighbouring properties no higher than Burland Scale 1 'very slight';*
- o. avoid adversely affecting drainage and run-off or causing other damage to the water environment;*
- p. avoid cumulative impacts;*
- q. do not harm the amenity of neighbours;*
- r. provide satisfactory landscaping, including adequate soil depth;*
- s. do not harm the appearance or setting of the property or the established character of the surrounding area;*
- t. protect important archaeological remains; and*
- u. do not prejudice the ability of the garden to support trees where they are part of the character of the area.*

*The Council will not permit basement schemes which include habitable rooms and other sensitive uses in areas prone to flooding.*

*We will generally require a Construction Management Plan for basement developments.*

*Given the complex nature of basement development, the Council encourages developers to offer security for expenses for basement development to adjoining neighbours."*

The following policies in the Local Plan are also relevant to basement development and will be taken into account when assessing basement schemes:

- "Policy A2 Open space";
- "Policy A3 Biodiversity";
- "Policy D1 Design";
- "Policy D2 Heritage"; and
- "Policy CC3 Water and flooding".

In addition to the Local Plan Policy, Camden publishes Camden Planning Guidance on Basements and Lightwells. These CPG documents do not carry the same weight as the main Camden Development Plan documents (including the above Policy A5) but they are important supporting documents.

#### **1.4 Report Structure**

This report commences with a desk study and characterisation of the site, before progressing to BIA screening and scoping assessments, whereby consideration is given to identifying the potential hydrogeological, hydrological and stability impacts to be associated with the proposed development.

A ground model is then developed, which is followed by an outline construction methodology and an assessment of the potential ground movements affecting the neighbouring structures.

Finally, an assessment of the potential impacts of the proposed scheme is presented.



### 1.5 Documents Consulted

2019 Sep	Outline SuDS Strategy by LBH WEMBLEY ENGINEERING	Ref: LBH4577suds v1.0
2019 Sep	Existing Plans & Sections by Ambigram Architects	
2019 Sep	Proposed Plans & Sections by Ambigram Architects	

## 2. The Site

### 2.1 Site Location

The site is situated on the northwestern side of Camden Road, approximately 60m to the northeast of Camden Town underground station.

The site may be located approximately by postcode NW1 9LG or by National Grid Reference 528950, 183940.



Location Plan

### 2.2 Topographical Setting

The site lies on a very gentle southeastwards falling slope on the west bank of the now culverted River Fleet, which runs approximately 200m from the site.



#### Slope

0° - 7°

7° - 10°

> 10°

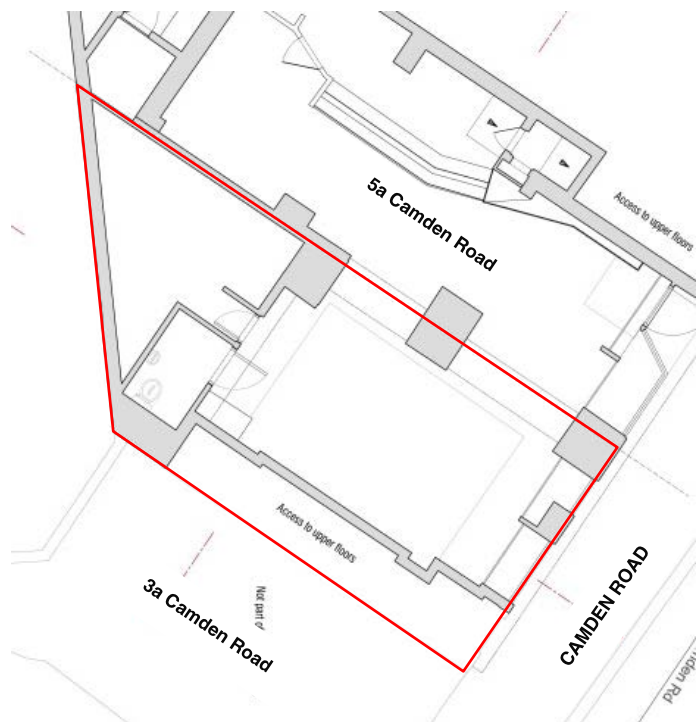
Extract from Figure 16 of the CGHHS

### 2.3 Site Description

The site is occupied by a late 19<sup>th</sup> Century three storey terraced building with ground floor level set at approximately +26.4m OD. The property is occupied by a commercial unit at ground level, with residential flats above.

A single storey extension, roughly triangular in shape, is present to the rear of the site. A manhole connecting to a combined sewer running along the backs of the properties along Camden Road is understood to be present underneath the rear of this extension.

The building is adjoined to the north by a similarly constructed three storey building located at No. 5a Camden Road. No. 5a also comprises a single storey extension to the rear. The ground floors of Nos. 5 & 5a Camden Road are joined together with no separating wall, except between the rear extensions, forming a single open plan ground floor occupied by a commercial unit.



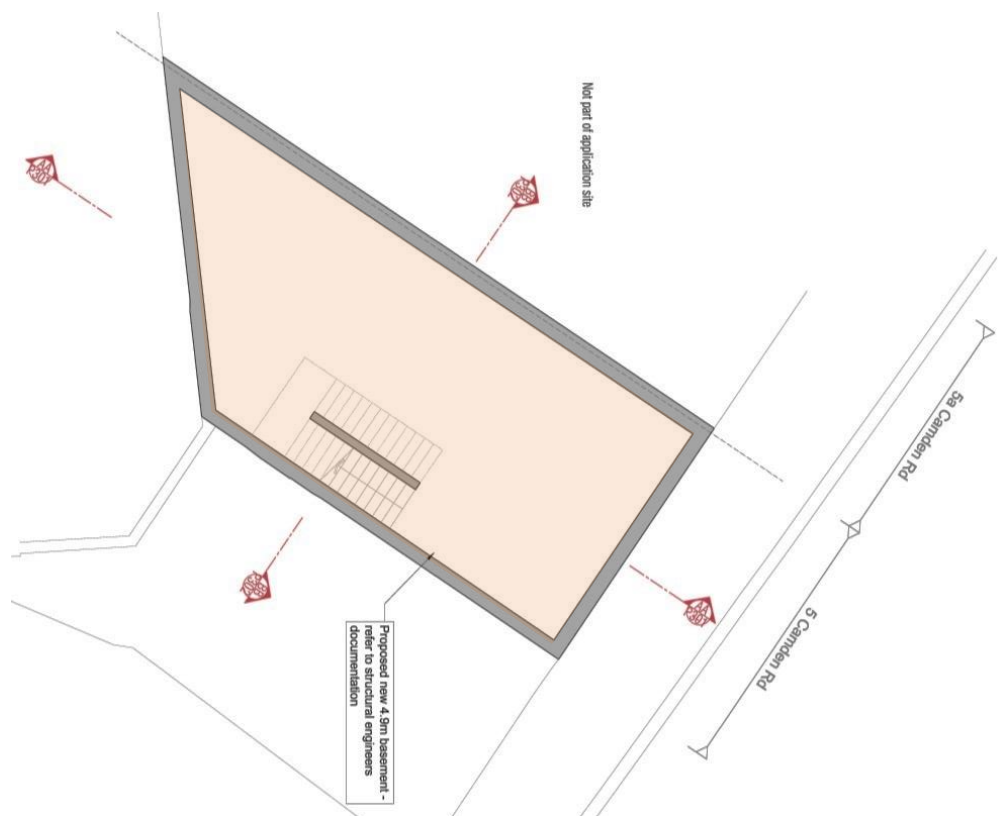
Existing Ground Floor Layout

To the south the building adjoins a similarly constructed three storey terraced property at No. 3a Camden Road. It is understood that a planning application has been submitted to construct a single storey basement beneath the entire footprint of this property. This development is expected to be completed prior to any proposed works at No. 5; hence the party wall is expected to be underpinned to basement level as part of the proposals for No. 3a.

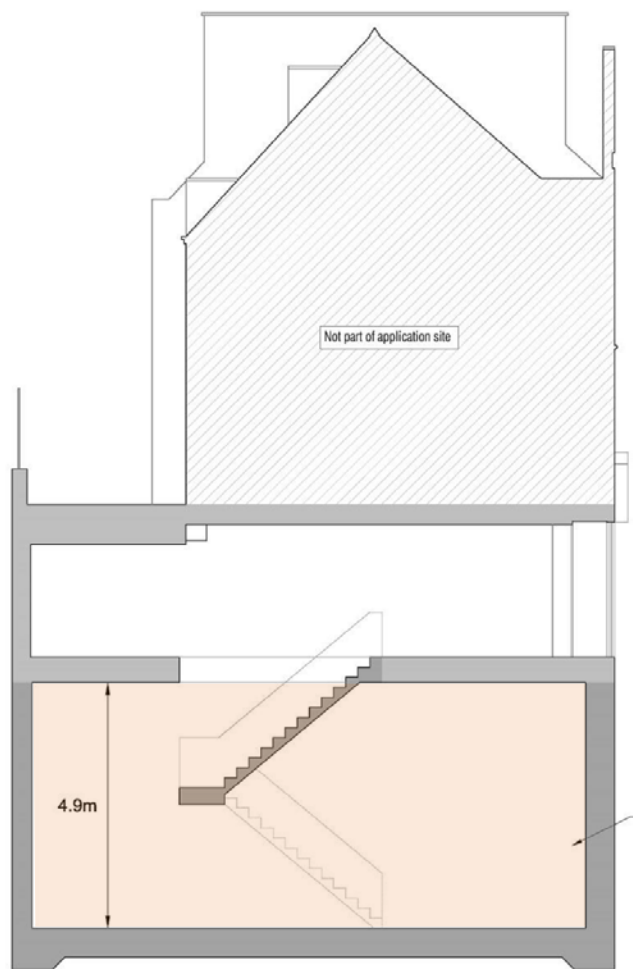
To the rear the site backs onto No. 8 and Nos. 10-12 Kentish Town Road, part two part three storey terraced buildings with mansard roofs. A recent redevelopment of both of these properties included excavation and construction of an approximately 4m deep basement beneath the entire footprints. As a result, the rear party wall to No. 5 has been underpinned to proposed basement level.

### 2.4 Proposed Development

It is proposed to construct a basement floor with internal headroom of 4.9m beneath the entire footprint of the building, including the rear extension. The proposed basement excavation will extend to approximately 5.5m depth beneath the ground floor (+21.0m OD).



Proposed Basement Plan



Section showing proposed basement

## 3. Desk Study

### 3.1 Site History

Earlier buildings on and adjacent to the site were demolished at the end of the 19<sup>th</sup> century and replaced by the existing row of terraced buildings.

No. 5 and No. 5a Camden Road were originally constructed with separate ground floor areas, divided by a party wall, until the 1970s.

A major refurbishment to combine the two properties at every floor level was approved in July 1939, but it appears this was never undertaken; which is most likely due to the breaking out of the Second World War.

The ground floor of No. 5 Camden Road therefore remained a single commercial unit until the ground floors of No. 5 and 5a were combined during the 1970s to provide a larger open plan commercial unit. The party wall was therefore removed and the loads transferred to a single central column.

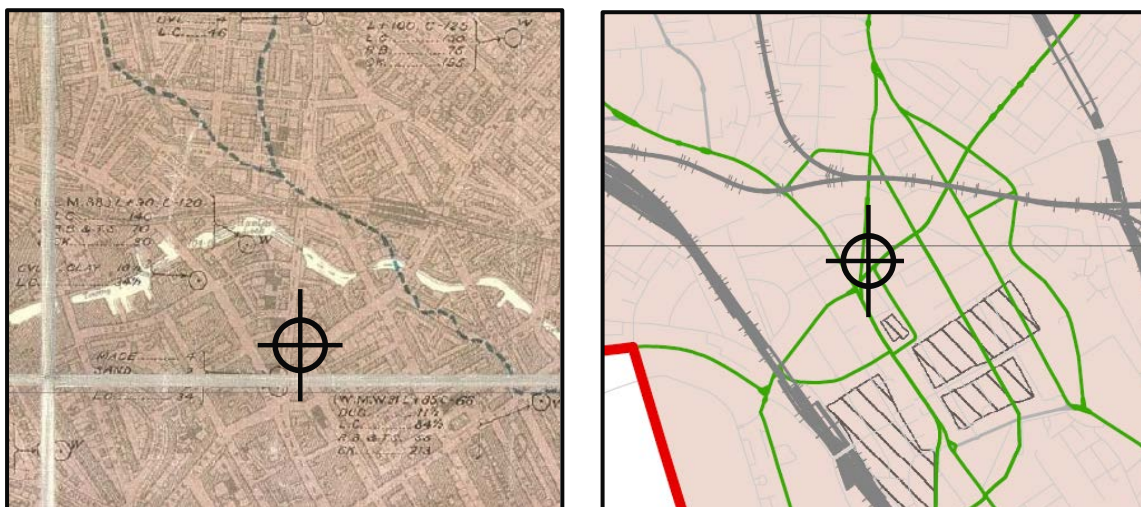
The site itself has remained relatively unchanged, albeit extensive redevelopment has recently taken place in the surrounding area.

No. 3 Camden Road has recently been developed, including conversion of the upper floors to provide residential accommodation and excavation of a single storey basement.

Basements have also recently been excavated beneath No. 8 & Nos. 10-12 Kentish Town Road, adjoining the site to the rear, and it is understood that a basement is proposed beneath No. 3a Camden Road, adjoining the site to the southwest.

### 3.2 Geological Information

The British Geological Survey (BGS) records indicate that the site is underlain by the London Clay Formation.



Extracts of Figure 2 (left) and Figure 3 (right) of the CGHHS



### 3.3 Hydrogeological Information

The London Clay Formation may be considered virtually impermeable; hence no significant groundwater flow is expected to occur beneath the site.

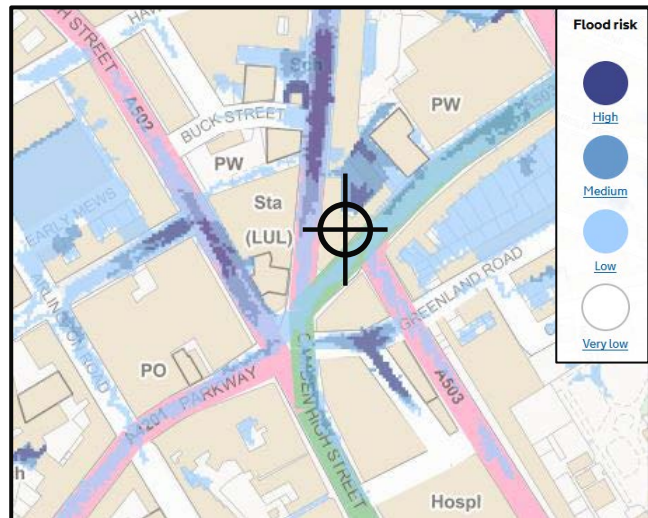
### 3.4 Hydrological, Drainage and Flood Risk Information

Figure 2 of the CGHHS indicates that the River Fleet passes approximately 200m to the northeast of the site. There are no surface water features in the vicinity of the site.

Environment Agency (EA) surface water flood maps indicate that the site itself is at a very low risk, although Camden Road is at a low risk of surface water flooding.

Figure 6 of the Camden SFRA indicates that the site lies within a Critical Drainage Area (Group 3 003).

The existing building occupies the entirety of the site.



Extract of EA surface water flood risk map

## 4. Screening & Scoping Assessments

The Screening & Scoping Assessments have been undertaken with reference to Appendices E and F of the CGHSS, which is a process for determining whether or not a BIA is usually required.

### 4.1 Screening Assessment

The Screening Assessment consists of a series of checklists that identifies any matters of concern relating to the following:

- Subterranean (groundwater) flow
- Surface flow and flooding
- Slope stability

#### 4.1.1 Screening Checklist for Subterranean (Groundwater) Flow

Question	Response	Justification
Is the site located directly above an aquifer?	No	The Environment Agency (EA) maps indicate that the site is not underlain by an aquifer.
Will the proposed basement extend beneath the water table surface?	No	
Is the site within 100m of a watercourse, well (used/disused) or potential spring line?	No	The nearest watercourse is the culverted River Fleet, approximately 200m to the northeast of the site.
Is the site within the catchment of the pond chains on Hampstead Heath?	No	See CGHHS Fig.14.
Will the proposed development result in a change in the area of hard-surfaced/paved areas?	No	Both the existing site and proposed development are entirely hard surfaced.
Will more surface water (e.g. rainfall and run-off) than at present will be discharged to the ground (e.g. via soakaways and/or SUDS)?	No	All surface water falling within the development will be attenuated and discharged to the Thames Water combined sewer.
Is the lowest point of the proposed excavation (allowing for any drainage and foundation space under the basement floor) close to or lower than the mean water level in any local pond?	No	See CGHHS Fig.12.

#### 4.1.2 Screening Checklist for Surface Flow and Flooding

Question	Response	Justification
Is the site within the catchment area of the pond chains on Hampstead Heath?	No	See CGHHS Fig.14.
As part of the site drainage, will surface water flows (e.g. rainfall and run-off) be materially changed from the existing route?	No	The existing drainage arrangement will be maintained.
Will the proposed basement development result in a change in the proportion of hard-surfaced/paved areas?	No	Both the existing site and proposed development are entirely hard surfaced.
Will the proposed basement result in changes to the profile of the inflows (instantaneous and long-term) of surface-water being received by adjacent properties or downstream watercourses?	No	The existing drainage arrangement will be maintained.
Will the proposed basement result in changes to the quality of surface water being received by adjacent properties or downstream watercourses?	No	The existing drainage arrangement will be maintained.
Is the site in an area known to be at risk from surface water flooding, or is it at risk from flooding for example because the proposed basement is below the static water level of a nearby surface water feature?	No	Although Camden Road is indicated to be at a low risk of surface water flooding, the site itself is indicated to be at a very low risk.

#### 4.1.3 Screening Checklist for Stability

Question	Response	Justification
Does the existing site include slopes, natural or manmade, greater than 7 degrees?	No	There are no slopes greater than 7 degrees within the site.
Does the proposed re-profiling of landscaping at the site change slopes at the property boundary to more than 7 degrees?	No	No re-profiling is planned at the site.
Does the development neighbour land, including railway cuttings and the like, with a slope greater than 7 degrees?	No	There are no slopes greater than 7 degrees within the development land.



Is the site within a wider hillside setting in which the general slope is greater than 7 degrees?	<b>No</b>	Figure 6 of the CGHHS indicates that the general slope of the wider hillside is less than 7 degrees.
Is London Clay the shallowest strata at the site?	<b>Yes</b>	The site is underlain by London Clay.
Will trees be felled as part of the proposed development and/or are works proposed within tree protection zones where trees are to be retained?	<b>No</b>	There are no trees on the site.
Is there a history of seasonal shrink-swell subsidence in the local area, and/or evidence of such effects at the site?	<b>No</b>	
Is the site within 100m of a watercourse or a potential spring line?	<b>No</b>	The nearest watercourse is the culverted River Fleet, roughly 200m to the northeast of the site.
Is the site within an area of previously worked ground?	<b>No</b>	The British Geological Survey (BGS) records do not indicate that the site lies within an area of previously worked ground.
Is the site within an aquifer?	<b>No</b>	The Environment Agency (EA) maps indicate that the site is not underlain by an aquifer.
Will the proposed basement extend beneath the water table such that dewatering may be required during construction?	<b>No</b>	
Is the site within 50m of the Hampstead Heath ponds?	<b>No</b>	See CGHHS Fig.14.
Is the site within 5m of a highway or pedestrian right of way?	<b>Yes</b>	The proposed basement adjoins the pedestrian right of way on Camden Road.
Will the proposed basement significantly increase the differential depth of foundations relative to the neighbouring properties?	<b>Yes</b>	The proposed basement will increase the differential depth to foundations to No. 5a Camden Road.
Is the site over (or within the exclusion zone of) tunnels, e.g. railway lines?	<b>No</b>	The site is approx. 25m away from the LUL Northern Line tunnels which run beneath Kentish Town Road.

## 4.2 Scoping Assessment

Where the checklist is answered with a “yes” or “unknown” to any of the questions posed in the flowcharts, these matters are carried forward to the scoping stage of the BIA process. The other potential concerns considered within the screening process have been demonstrated to be not applicable or not significant when applied to the proposed development.

The scoping produces a statement which defines further the matters of concern identified in the screening stage. This defining should be in terms of ground processes, in order that a site specific BIA can be designed and executed (Section 6.3 of the CGHHS).

### 4.2.1 Scoping for Stability

- **Is the London Clay the shallowest strata at the site?**

The guidance advises that of the soil strata present in LB Camden, the London Clay is the most prone to seasonal shrink-swell (subsidence and heave).

- **Is the site within 5m of a highway or pedestrian right of way?**

The guidance advises that excavation for a basement may result in damage to the road, pathway or any underground services buried in trenches beneath the road or pathway.

- **Will the proposed basement significantly increase the differential depth of foundations relative to neighbouring properties?**

The guidance advises that excavation for a basement may result in structural damage to neighbouring properties if there is a significant differential depth between adjacent foundations.

## 5. Site Investigation

Due to existing access restrictions to the site, a site specific ground investigation has not yet been undertaken. It is understood a series of trial pits will be undertaken at the beginning of the construction programme in order to confirm the expected ground conditions.

Recent investigations were carried out in the adjacent properties of 3a Camden Road and 8 Kentish Town Road, comprising a total of four window sample boreholes and six hand excavated trial pits, including a trial pit against the party wall between No. 3a and No. 5 Camden Road, and another between No. 8 Kentish Town Road and No. 5 Camden Road.

### 5.1 Ground Conditions

Below a cover of made ground, the London Clay Formation is expected to be present at shallow depth and to consist of typical firm, becoming stiff, pale brown silty clay.

### 5.2 Groundwater

No shallow groundwater table is expected beneath the site.

## 6. Outline Basement Construction Methodology

### 6.1 Excavation

The basement excavation will require approximately 5.5m of excavation and will extend down into the London Clay Formation.

The basement perimeter walls will be formed by conventional underpinning and the construction of L-shaped reinforced concrete segments excavated and cast in-situ in a 'hit and miss' sequence of 1m wide sections.

The rear party wall with No. 8 and Nos. 10-12 Kentish Town Road is known to be already underpinned to approximately 4m depth below ground level; therefore only a single stage underpinning of no more than 2m is envisaged.

At the boundary between No. 5 and No. 5a, the upper floors are supported by a single, centrally placed column. It is expected the column can be retained and accommodated in the permanent scenario, with underpinning of the existing column foundation connecting to the new basement wall.

Previous investigations undertaken at No. 8 Kentish Town Road indicated that, prior to underpinning, the party wall with No. 5 Camden Road was supported by a 1.8m deep strip foundation. It is therefore likely that the strip foundations supporting No. 5 that are yet to be underpinned extend to a similar depth.

On this basis, the required depth of underpinning of the party wall with No. 5a Camden Road and the front wall of the property is likely to be around 4m; however, in order to model a worst case scenario, the existing foundations are assumed to extend to 0.5m depth below existing ground floor level, including the necessity for two stages of underpinning.

During the works, propping will be installed to ensure that lateral ground movements are minimised. As a precursor to the main basement excavation, it is envisaged full width propping will be provided at ground floor level to restrain the newly underpinned walls during the main basement excavation.

As the main basement excavation proceeds, additional temporary propping will be installed at lower levels where necessary to ensure that lateral ground movements are prevented.

In the permanent situation the reinforced concrete underpins will connect to the basement slab and the new ground floor slab to form a rigid concrete box to support the vertical structural loading of the overlying building. Both the basement raft slab and the ground floor slab will act as props.

#### 6.1.1 Waterproofing

There is potential for water to collect around the basement in the long term. Hence, the basement is to be fully waterproofed and designed to withstand hydrostatic pressures in accordance with BS8102:2009, Code of Practice for the Protection of Below-Ground Structures against Water from the Ground. An assumed hydrostatic level at 1m depth is to be adopted for the purposes of assessing hydrostatic pressures.

#### 6.1.2 Basement Heave

Given the depth of excavation, it is evident that the self-weight of the new structure will not match the weight of soil removed and that there may as a result be some potential for residual net uplift.

An assessment of the likely extent of any long term uplift is made in Section 7 of this report.

## 6.2 Underpinning

Underpinning sections will be excavated in short widths not exceeding 1000mm.

The sequence of the underpinning will be in an extended 1, 3, 5, 2, 4 & 6 type numbering sequence, such that any given underpin will be completed, dry packed, and a minimum period of 48 hours lapsed before and adjacent excavation is commenced to form another underpin.

Each pin excavation will be undertaken only under the direct supervision of a suitably experienced and competent person. In the event that the vertical soil face to an underpin is judged to be potentially unstable, face support and lateral propping will be provided by perforated plywood sheeting supported by timber walings held by adjustable steel trench "acrow" props.

## 6.3 Retaining Walls

The following parameters may be considered in the design of the retaining walls:-

Suggested Retaining Wall Design Parameters			
Stratum	Bulk Unit Weight	Effective Cohesion	Effective Friction Angle
	(kN/m <sup>3</sup> )	(c' - kN/m <sup>2</sup> )	( $\phi'$ - degrees)
London Clay	20	Zero	20

## 6.4 Underground Infrastructure

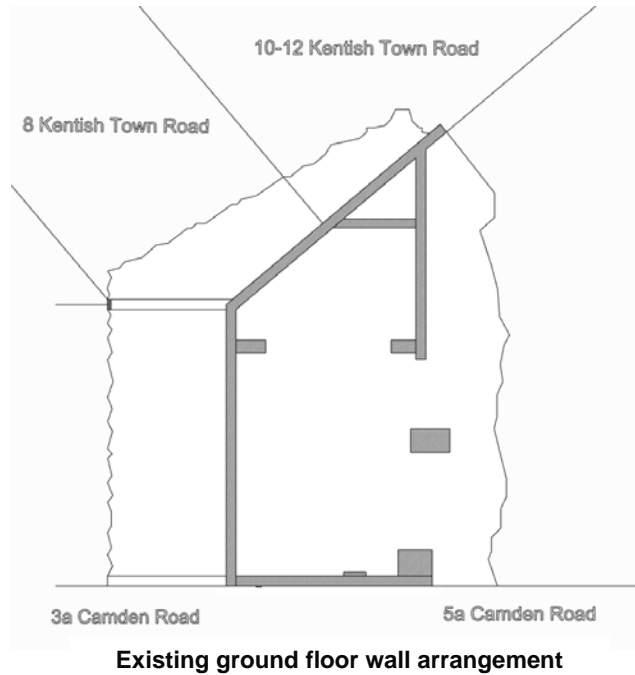
The southbound and northbound tunnels of the Northern Line, High Barnet branch are present approximately 30m to the west of the property, beneath Kentish Town Road.

A 230mm diameter combined sewer is indicated beneath the rear extension of the property, running parallel to the rear boundary. A manhole is present in the small yard connecting to a manhole beneath the rear extension at No. 5a.

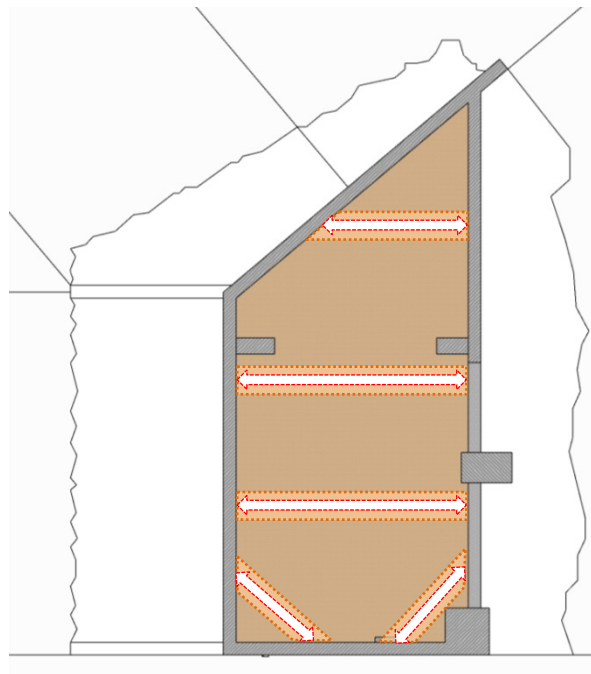
This sewer will need to be investigated further and, if still in use, it will be necessary to re-route the sewer as part of the development.

## 6.5 Construction Sequence

The following indicative construction sequence is proposed, and will be subject to detailed design by a structural engineer:



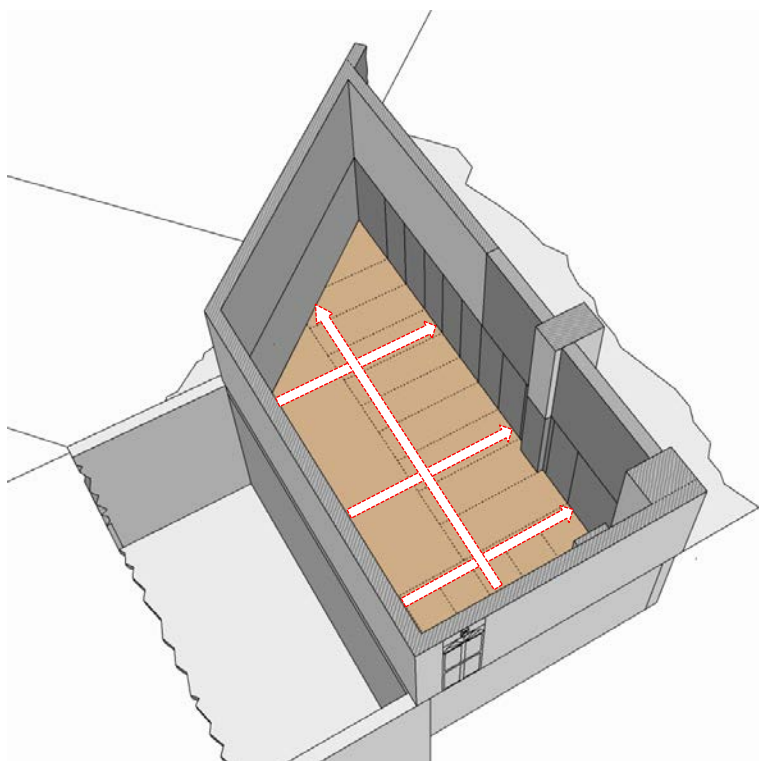
1. Install temporary ground floor level propping in shallow trenches across the building footprint.



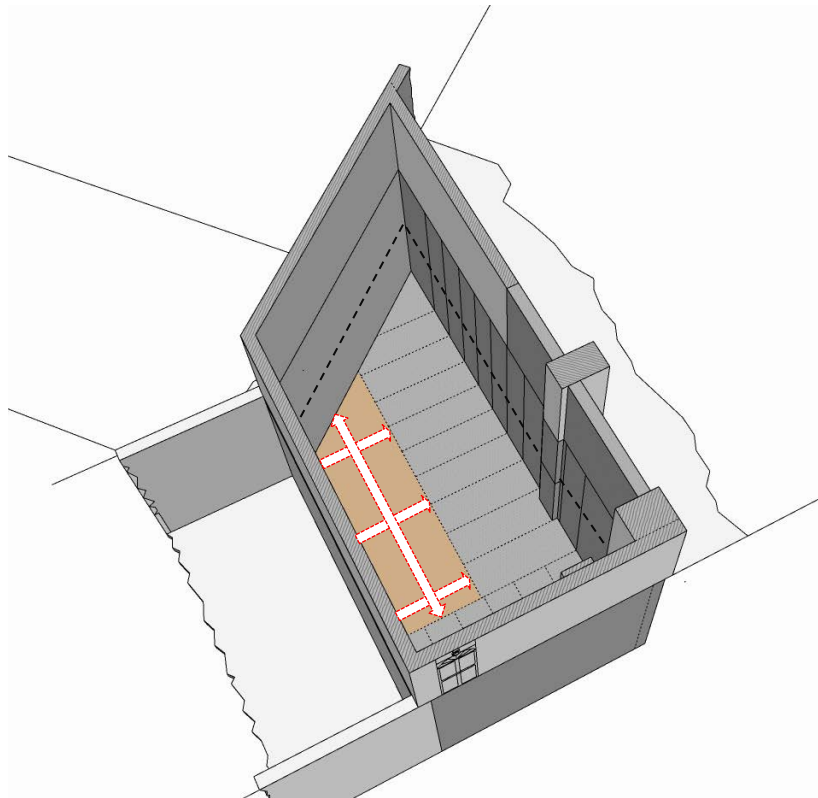
2. Excavate the area adjacent to the existing basements and underpin the façade and the party wall with No. 5 Camden Road in reinforced concrete L-sections as the first stage of underpinning. Suggested underpinning sequence presented below.



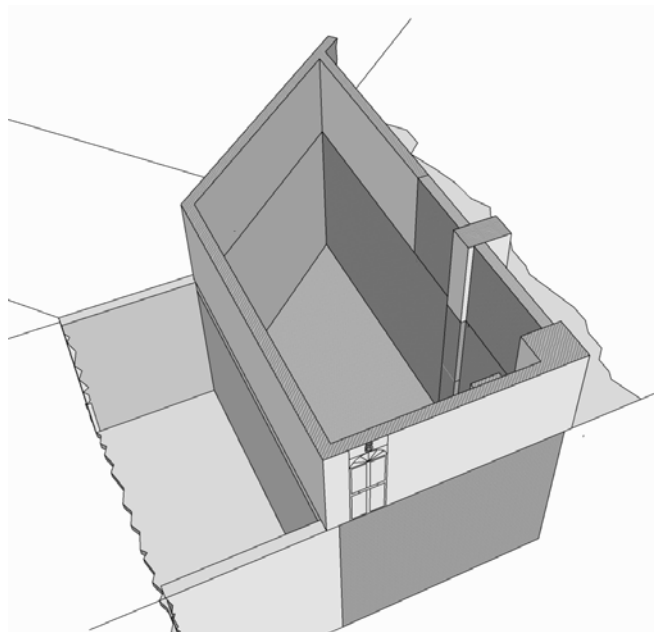
3. Install basement level propping across the constructed underpinning.



4. Commence the second stage of underpinning to reach the proposed final basement depth. Similarly to the previous stage, first excavate the area adjacent to the existing neighbouring basements, followed by underpinning of the front wall and the party wall with No. 5a.
5. Construct basement level lateral propping to the second stage underpins.

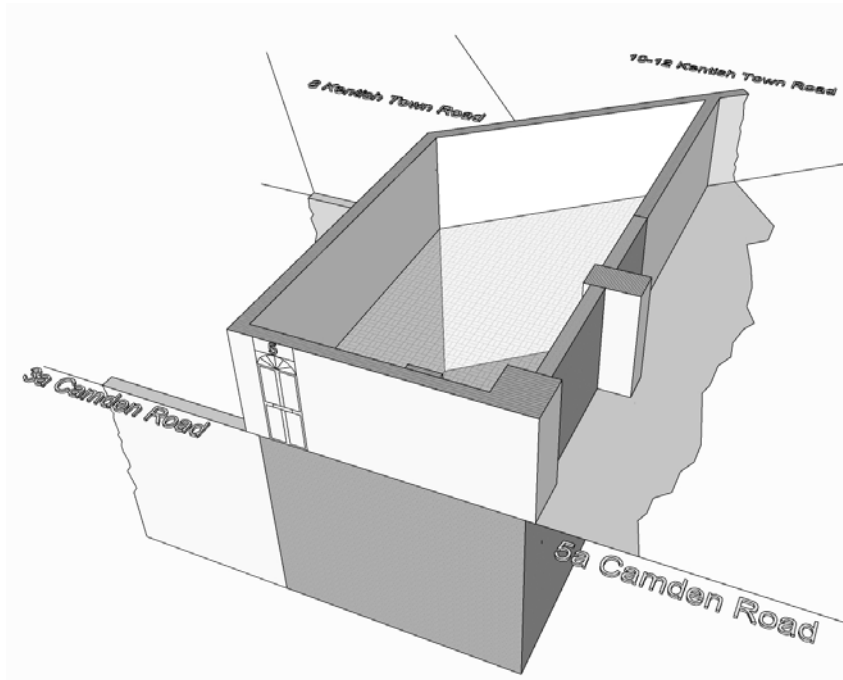


6. Install below-slab drainage for foul and ground water, sumps and pumps.
7. Place slab reinforcement and cast remaining basement slab.





8. Remove low level temporary propping.
9. Construct basement liner walls, membranes, cavity drainage, insulation and screed.
10. Construct ground floor slab.
11. Remove ground level propping.



## 7. Ground Movement to Neighbouring Properties

Camden Council seeks to ensure that harm will not be caused to neighbouring properties by basement development.

Camden Local Plan (June 2017) states that the BIA must demonstrate that the proposed basement scheme has a risk of damage to the neighbouring properties no higher than Burland Scale 1 'Very Slight'.

### 7.1 Structures Assessed for Ground Movement

#### 7.1.1 No. 3a Camden Road

No. 3a Camden Road is a three storey terraced building that adjoins the site to the southwest.

This building is expected to comprise a single storey basement to approximately 5.5m depth (+21m OD) by the time the development at No. 5 commences. In this case no underpinning of the party wall between the properties would be necessary, resulting in negligible movement and damage to the neighbouring building.

Nevertheless, an assessment of the worst case scenario has been undertaken, assuming the basement has not been excavated and No. 3a is therefore supported by shallow strip foundations extending to approx. 0.5m below ground level.

Two stages of underpinning will therefore be required in this case.

#### 7.1.2 No. 5a Camden Road

No. 5a Camden Road is a three storey terraced building, which adjoins the site to the northeast.

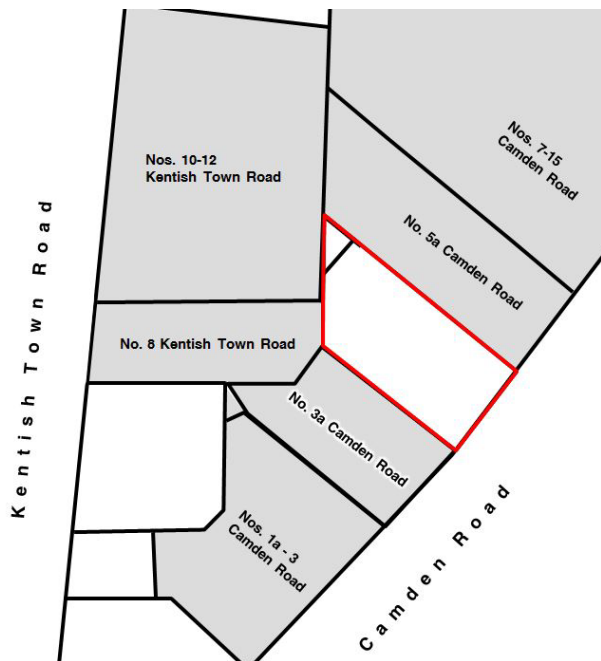
No. 5 and 5a currently share an open plan ground floor, with what is understood to be a single load bearing column present at the midpoint of the boundary between the two. It is expected that the column, as well as the remaining load bearing walls at No. 5a, are supported by shallow pad/strip foundations, where not adjoining recently excavated basements such as at Nos 10-12 Kentish Town Road. Two stages of underpinning will therefore be required.

#### 7.1.3 No. 8 Kentish Town Road & Nos. 10-12 Kentish Town Road

No. 8 and Nos. 10-12 Kentish Town Road located to the northwest of No. 5 Camden Road are already underpinned to the required depth by virtue of the existing basement at these properties.

### 7.2 Modelled Ground Conditions

Excavation of the basement will result in unloading of the clay leading to theoretical heave movement of the underlying soil in both the short and long term. An analysis of the vertical movements has been carried out using the soil stiffness model detailed in the table overleaf.



Plan showing the nearby buildings

For design purposes a conservative undrained strength profile has been adopted, assuming an average  $C_u$  of  $70\text{kN/m}^2$  at the surface of the London Clay Formation, increasing by  $8\text{kN/m}^2$  per m depth.

The Undrained Modulus of Elasticity ( $E_u$ ) has been based upon an empirical relationship of  $E_u = 750 \times$  undrained cohesion ( $C_u$ ), and the Drained Modulus of Elasticity ( $E'$ ) has been based upon an empirical relationship of  $350 \times C_u$ .

Stratum:	Undrained Elastic Modulus $E_u$ ( $\text{kN/m}^2$ )	Drained Elastic Modulus $E'$ ( $\text{kN/m}^2$ )
London Clay Formation	$52,500\text{kN/m}^2$ at surface increasing linearly to $232,500\text{kN/m}^2$ at 30m depth	$35,000\text{kN/m}^2$ at surface increasing linearly to $155,000\text{kN/m}^2$ at 30m depth

Poisson's Ratios of 0.5 and 0.2 have been used for short term (undrained) and long term (drained) conditions respectively.

The analysis uses the above parameters for stratified homogeneity with the introduction of an assumed rigid boundary at approximately 30m depth.

### 7.3 Short Term Vertical Movements

There are two components of short term movement that will interact to affect the neighbouring structures.

These components are firstly progressive sagging movements of the underpinned walls due to imperfections in the underpinning process itself and then secondly elastic heave of the ground as a direct response to a net unloading of  $-110\text{kN/m}^2$  unloading caused by excavation of the new basement.

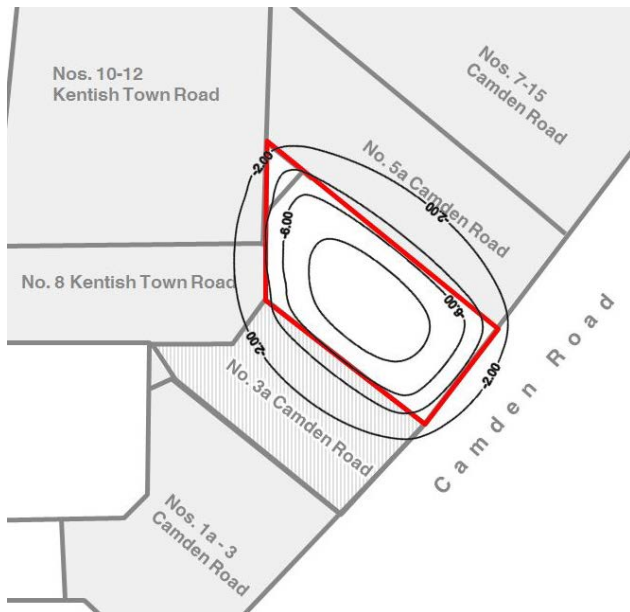
#### 7.3.1 Short Term Movement due to Underpinning

It is not possible to rigorously model the extent of party wall settlement arising from underpinning and experience indicates that amount of any movements are very much dependent on workmanship. However, it is suggested that given dry conditions and good workmanship, the amount of vertical movement of the party walls can reasonably be expected to be a maximum of 5mm per stage of underpinning.

On the simplistic assumption of a 45 degree angle of support to any walls extending away in a direction perpendicular to the party walls, the scale of this vertical movement associated with the underpinning process itself is assumed to extend to a distance of 5.5m behind the wall.

### 7.3.2 Short Term Movements due to Excavation heave

Any short term movements below the excavation itself will go un-noticed, and the analysis suggests less than 6mm heave movement at the surrounding party walls and new underpinning.

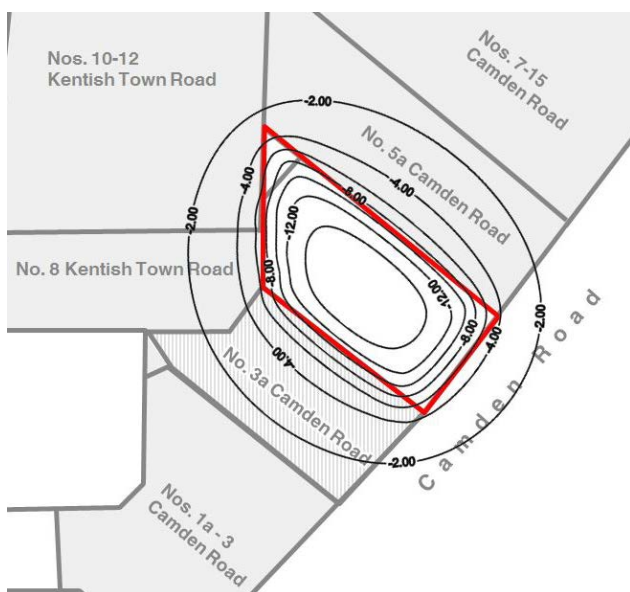


Plan showing theoretical approximate short term heave contours (mm) due to basement excavation

### 7.4 Post Construction Vertical Movements

There will be a mismatch between the weight of soil that is removed and the weight of the new structure. In this situation, a component of long term heave is inevitable and this could proceed for decades.

The results of the heave analysis, as presented on the plan shown below, suggest that the scale of this post-construction heave will potentially amount up to 15mm within the new basement, decreasing to approximately 10mm beneath the party walls to No. 3a Camden Road, No. 5a Camden Road and No. 8 Kentish Town Road.



Plan showing theoretical approximate post-construction heave (mm) due to basement excavation

#### **7.4.1 Cumulative Post Construction Movements**

Given the recent basement excavation at No. 8 Kentish Town Road and Nos. 10-12 Kentish Town Road, as well as the proposed basement excavation at No. 3a Camden Road, consideration has been given to the potential cumulative movements.

The results suggest that the scale of the cumulative post-construction heave may theoretically reach up to 15mm beneath the party walls to No. 3a Camden Road, No. 8 and Nos. 10-12 Kentish Town Road.

#### **7.5 Horizontal Movements**

Horizontal soil movements are expected to occur due to yielding of the soil behind the underpinned wall during the basement excavation. For embedded retaining walls, this yielding has been found to extend to a distance approximately equivalent to four times the depth of excavation in front of the wall.

As a first approximation, the magnitude of the horizontal movement at the basement perimeter is assumed to be 5mm, which is equal to the vertical movement at the underpinned wall

This horizontal movement is assumed to reduce to zero at a maximum distance of  $4 \times 5.5\text{m}$  (excavation depth) = 22m behind the wall.

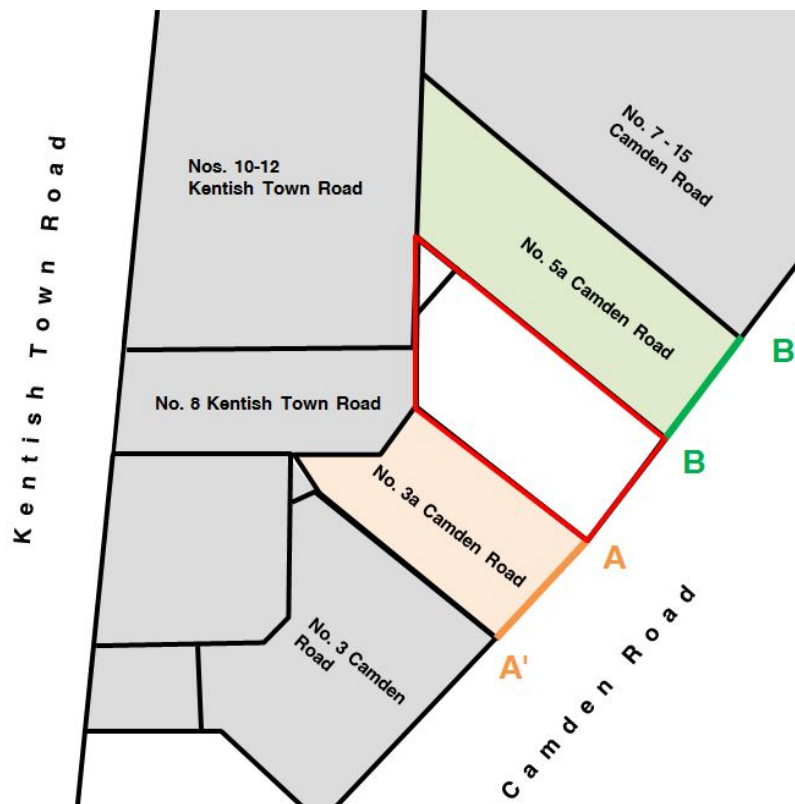
#### **7.6 Impact on Neighbouring Structures**

In practice, although the various movements described above will interact so that the soil basement heave effects will tend to counteract the underpinning wall settlement movements, it is considered prudent to ignore this counteraction for the assessment of building damage.

The effect of the predicted vertical and horizontal deflections have been assessed using the Burland damage category assessment process, which is based upon consideration of a theoretical masonry panel of a given length (L) and height (H).

The potential degree of the predicted ground movements on the assessed structures can be estimated by the correlation of maximum horizontal strain,  $\epsilon_h$ , with the maximum deflection ratio,  $\Delta/L$ , where  $\Delta$  is the vertical distortion over the wall length under assessment (where the wall length L is actually less than the distance to the point at which zero vertical movement is assumed, a minimum distortion of 1mm is assumed).

The potential degree of damage due to the proposed basement construction has been assessed and a summary is shown below.



Plan showing line of sections used for damage category assessment

#### 7.6.1 No. 3a Camden Road – Section A-A'

The length of section (L) is taken as 7m and the wall height (H) as 10m.

The maximum horizontal strain,  $\epsilon_h (\Delta h / L)$  is assessed as 0.041%, producing a maximum deflection ratio  $\Delta / L = -0.024$ , within a limiting tensile strain of 0.050%, for a Burland Category 0 “Negligible” condition.

#### 7.6.2 No. 5a Camden Road – Section B-B'

The length of section (L) is taken as 6m and the wall height (H) as 10m.

The maximum horizontal strain,  $\epsilon_h (\Delta h / L)$  is assessed as 0.045%, producing a maximum deflection ratio  $\Delta / L = -0.05$ , within a limiting tensile strain of 0.075%, for a Burland Category 1 “Very Slight” condition.

#### 7.6.3 Public Highway

The proposed basement lies directly adjacent to the pavement, where there is expected to be various buried utilities located.

Given reasonable standards of workmanship during the underpinning works, negligible movement (<5mm settlement) is anticipated and this may be counteracted in practice by some small amounts of heave.

## 8. Impact Assessment

The screening and scoping stages identified potential aspects of the geological, hydrogeological and hydrological environment that could lead to the development having an unacceptable impact.

This stage is concerned with evaluating the direct and indirect implications of each of these potential impacts.

### 8.1 Hydrogeological Impact Assessment

The site is underlain by clay soils and there is consequently no shallow groundwater table at this site.

It is therefore considered that the development will not have any impact upon groundwater flow and there is additionally no scope for any cumulative impact.

### 8.2 Hydrological Impact Assessment

There will be no change to the flood risk at the site or neighbouring sites.

Nevertheless, there will be a need to maintain the present water discharge regime and provide Sustainable Drainage Systems (SuDS) to meet the planning policy requirements.

An Outline SuDS Strategy is presented as a separate report (LBH4577suds).

### 8.3 Potential Stability Impacts

#### 8.3.1 London Clay

The London Clay soils are of high volume change potential.

However, the depth of the proposed construction will obviate any concerns regarding potential seasonal movement.

#### 8.3.2 Ground Movements

The Local Plan states that proposed basements should pose a risk of damage to neighbouring properties no higher than Burland scale Category 0 'Very Slight', and mitigation measures should be incorporated if the assessed damage is not acceptable.

The predicted neighbouring buildings damage levels due to ground movements associated with the proposed development have been analysed in section 7 and found to be acceptable (Limited to Burland scale Category 0 'Negligible').

In addition, negligible movement to the public highway due to the proposed basement development is predicted.

### 8.4 Residual Impacts

The proposed basement will have no residual unacceptable impacts upon the surrounding structures, infrastructure and environment. The cumulative impact of this development, in conjunction with the recent developments at No. 8 and Nos. 10-12 Kentish Town Road as well as the proposed basement development at No. 3a Camden Road, have been analysed and are assessed to be acceptable.

## 9. Outline Structural Monitoring Plan

The ground movement assessment suggests Burland Scale Category 1 (Very Slight) damage may be expected to the neighbouring properties.

Nevertheless, structural monitoring should be undertaken to ensure the movements remain within acceptable limits and to enable mitigation to be effectively implemented in the event of agreed trigger values for movement being exceeded.

Monitoring positions should be located along all the perimeter party walls.

Before any excavation or construction works commence, monitoring is to be undertaken in order to establish a baseline situation.

During all underpinning works and basement excavation works, monitoring should be undertaken daily at the start and end of every work shift. At other times monitoring should be undertaken weekly to cover a period prior to commencement of any works and ceasing after completion of the works, by agreement of all interested parties.

Precise survey equipment should be used to record all vertical and horizontal components of movement (in three perpendicular directions) to a minimum accuracy of 1mm.

### 9.1 Criteria for assessment of Monitoring data and Comparison with Predicted Movements

The cumulative movements in any direction of any monitoring point are to be compared with the predicted movements at any stage and using the following decision table:

MONITORING CRITERIA		
Total movement less than 10mm in any direction		Green
Total movement in excess of 10mm in any direction or additional movement of 10mm in any direction	Notify Structural Engineer and Party Wall Surveyor	Red

### 9.2 Contingent Actions

Contingency actions should be undertaken using the following decision table:

CONTINGENT ACTIONS	
Green	None
Red	Cease work and Notify Structural Engineer and Party Wall Surveyor immediately. Commence backfilling / installation of additional propping. Undertake repeated monitoring as necessary to ensure that movement has ceased. Works to commence only once a revised construction methodology has been agreed with the Structural Engineer



## 10. Conclusion

The assessment has demonstrated that no adverse residual or cumulative stability, hydrological or hydrogeological impacts are expected to either neighbouring structures or the wider environment as a result of this development.