



## CONTIGUOUS PILE FOUNDATION DESIGN

*(Issued subject to mutual agreement of Sub-Contract)*

Contract Number

**16-0036**

Site Address

**Hampstead Green  
London**

Main Contractor

**CAREY LONDON LIMITED**

Date	Rev	Designed By	Approved By	Comments / Drawings Rev.s
20/04/2016	0	Kayvan Kiany Design Manager	Neil Stone Design Manager	

## HAMPSTEAD GREEN, LONDON CFA RETAINING WALL PILE DESIGN REV 0

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## 1.0 Design Brief

The proposed redevelopment of the site involves the installation of Contiguous piles for the Hampstead Green project development in London. The piles are to be constructed using the continuous flight auger (CFA) technique.

Design consists of 400mm male piles at 550mm centres.

Analysis of the wall has been divided into five sections, allowing for varying retained heights and construction sequences.

Piles will be installed to a target verticality of 1:75

Piles will be installed to a plan tolerance of 75mm

Male piles to be constructed using C32/40 concrete providing DC-3 design concrete classification as a minimum.

Pile design requirements are summarised in *Fig. 1*

Wall Section	PPL (mOD)	Retained level (mOD)	Formation level (mOD)	Retained height (m)	Male length (m)
1	75	75	71.5	3.5	10 to 18.1
2	72	72	67.2	4.8	10 to 18.1
3	72	72	67.6	4.4	10 to 18.1
4 (CP27-32)	75	75	67.6	7.4	10 to 18.1
5 (CP321-352)	75	75	71.5	3.5	10 to 18.1

**Fig 1 Pile summary**

## **2.0 Design Input**

### **2.1 Site Investigation**

Card Geotechnics Limited Geotechnical and geo-environmental report, rev 2, dated September 2014.

### **2.2 Drawings**

Relevant Drawings:                   elliottwood Consulting drawings –  
   S/70 Proposed Pile Layout rev C2  
   S/71 Proposed Pile Layout Schedules rev C1  
   S/80 Proposed basement plan rev T1  
   S/80 Proposed basement plan rev T1  
   S/90 Proposed lower GF plan rev T1

### **2.3 Codes & Standards**

CIRIA C580 Embedded retaining walls  
BS EN 1992-1-1:2004 Eurocode 2: Design of Concrete Structures  
ES EN 1997-1:2004 Eurocode 7: Geotechnical Design  
BS EN1536: 2010 Execution of Special Geotechnical Work – Bored Piles

### **2.4 Specification**

ICE Specification for piling and embedded retaining walls, 2<sup>nd</sup> Edition (SPERW), 2007.  
elliottwood specification for piling works, tender issue dated 2015.

### **3.0 Design Philosophy & Ground/ Design Model**

#### **3.1 Design Philosophy**

Design is in accordance with CIRIA report C580: Embedded retaining walls, which is provided as non-contradictory complementary information (NCCI) under BS EN 1997-1:2004. Analyses were performed using WALLAP computer software for both the Ultimate Limit State (ULS) and Serviceability Limit State (SLS). Design has been completed in accordance with design approach A based on a moderately conservative approach.

**We have assessed the structure class to be Category 2 (Section 2.1) “Conventional types of structure and foundation with no exceptional risk or difficult soil and loading conditions”.**

The results from the WALLAP analyses can be viewed in Appendix C.

The results of both analyses are used in the final design of the piles. The ultimate design bending moments and shear forces are taken as the maximum of the result from ULS analysis or the result of the SLS analysis factored by 1.35. Deflections are taken from the results of the SLS analysis. Geotechnical and structural toe levels are taken from the ULS analysis.

Over dig has been allowed for in the ULS analysis, the lesser of 0.5m or 10% of the total retained height.

In the analysis in the temporary condition un-drained shear strength parameters for the London Clay are adopted on both sides of the wall. This approach is based on standard industry practice. We would expect the basement to be constructed before the London Clay reaches its drained state.

As noted in CIRIA C580 section A8.2.5, “**All loads and surcharges are applied in an un-factored manner**” within our analysis.

The resulting bending moments and shear forces have been used to calculate the required bending and shear reinforcement in accordance with BS EN 1992-1-1:2004 (see Appendix D).

#### **3.2 Construction Sequence**

##### **Section 1 (Section 5 with lateral load)**

Install Contiguous piles from a platform level of 75mOD (Retained level 75mOD)  
 Excavate and construct capping beam  
 Excavate to formation level of 71.5mOD  
 Install Base slab to act as permanent support

##### **Section 2**

Install Contiguous piles from a platform level of 72mOD (Retained level 72mOD)  
 Excavate and construct capping beam  
 Excavate to formation level of 67.215mOD  
 Install Base slab to act as permanent support  
 Install GF slab to act as permanent support

##### **Section 3**

Install Contiguous piles from a platform level of 72/75mOD (Retained level 72mOD)  
 Excavate and construct capping beam  
 Excavate to formation level of 67.6mOD  
 Install Base slab to act as permanent support  
 Install GF slab to act as permanent support  
**Ground level to be reduced to 72mOD before excavation of the basement where piles have been installed from a PPL of 75mOD.**

**Section 4**

Install Contiguous piles from a platform level of 75mOD  
 Excavate and construct capping beam  
 (Wall propped by capping beam along GL B and also by the capping beam of piles CP21-26)  
 Excavate to formation level of 67.6mOD  
 Install Base slab to act as permanent support  
 Install GF slab to act as permanent support

**3.3 Site Investigation**

The site Investigation Report provided a total of 5 boreholes up to a maximum depth of 30m. Standard Penetration Tests (SPT's) and un-drained triaxial tests have been carried out.

**3.4 Soil Model**

The soil profile used within the design is illustrated below this profile was developed from a review of the aforementioned site investigation. See *Fig 2*.

Stratum	Level (mOD)
MG	75
Head Deposits	72.5
London Clay	71

**Fig 2 Soil Model**

Design is based on a groundwater level of 13mOD.

**3.5 Soil Parameters**

A correlation value of 5 has been applied to the SPT results to obtain the equivalent Undrained Shear Strength ( $\text{kN/m}^2$ ) of the Clay strata.

The soil parameters shown in *Fig.3* are subsequently used for the design of the piles.

A summary of the characteristic, ULS & SLS design values used within the design is also located in *Fig 4*.

A plot of strength Vs depth can also be found in Appendix A.

STRATUM		BEARING PILE DESIGN PARAMETERS								
<b>London CLAY</b> <i>Firm to V Stiff CLAY (fissured silty CLAY)</i>		Bulk Density	$\gamma_b$	$= 20\text{kN/m}^3$ 'N' $c_u$ $\alpha$ $q_s$ Values as design lines Values as design lines, correlation factor = 5 $= 0.60$ Limited to maximum average of 110kPa						

**Fig 3 Soil Parameters**

CHARACTERISTIC VALUES											
Stratum	$\gamma_{bulk}$ kN/m <sup>3</sup>	$\gamma_{dry}$ kN/m <sup>3</sup>	$K_o$	S <sub>u</sub> (+ gradient)		$c'$ kN/m <sup>2</sup>	$\phi'$	E <sub>un</sub> (+gradient)		E' (+gradient)	
				kN/m <sup>2</sup>	kN/m <sup>2</sup> /m			kN/m <sup>2</sup>	kN/m <sup>2</sup> /m	kN/m <sup>2</sup>	kN/m <sup>2</sup> /m
MG Head deposits London Clay	18.0 20.0 20.0	18.0 20.0 20.0	0.530 0.590 1.000	55.0	6.1	2.5	28.0 24.0 25.0	44000	4880	10000 18000 35200	3904
ULTIMATE LIMIT STATE VALUES											
Stratum	$\gamma_{bulk}$ kN/m <sup>3</sup>	$\gamma_{dry}$ kN/m <sup>3</sup>	$K_o$	S <sub>u</sub> (+ gradient)		$c'$ kN/m <sup>2</sup>	$\phi'$	E <sub>un</sub> (+gradient)		E' (+gradient)	
				kN/m <sup>2</sup>	kN/m <sup>2</sup> /m			kN/m <sup>2</sup>	kN/m <sup>2</sup> /m	kN/m <sup>2</sup>	kN/m <sup>2</sup> /m
MG Head deposits London Clay	18.0 20.0 20.0	18.0 20.0 20.0	0.595 0.652 1.000	29.3	3.3	2.1	23.9 20.4 21.2	22000	2440	5000 9000 17600	1952
SERVICEABILITY LIMIT STATE VALUES											
Stratum	$\gamma_{bulk}$ kN/m <sup>3</sup>	$\gamma_{dry}$ kN/m <sup>3</sup>	$K_o$	S <sub>u</sub> (+ gradient)		$c'$ kN/m <sup>2</sup>	$\phi'$	E <sub>un</sub> (+gradient)		E' (+gradient)	
				kN/m <sup>2</sup>	kN/m <sup>2</sup> /m			kN/m <sup>2</sup>	kN/m <sup>2</sup> /m	kN/m <sup>2</sup>	kN/m <sup>2</sup> /m
MG Head deposits London Clay	18.0 20.0 20.0	18.0 20.0 20.0	0.530 0.590 1.000	44.0	4.9	2.5	28.0 24.0 25.0	44000	4880	10000 18000 35200	3904

**Fig 4 ULS / SLS design values**

## 4.0 Specified Loads

### 4.1 Compression

Piles have been designed for vertical compression loads as specified on drawings listed in section 2.2. Design is based on a partial safety factor approach where characteristic pile resistance is calculated in accordance with BS EN 1997-1:2004, Design Approach 1 (section 2.4.7.3.4.2), design by calculation.

Design has been checked for Geotechnical and Structural Ultimate Limit States (ULS)

Design is based upon design actions < design resistance.

Dead Load (kN/m)	Load (kN/m)	C1 per pile (kN)	C2 per pile (kN)	Pile length (m)
75 - 850	25-200	77-796	60-611	10 to 18.1

The working load of the pile has been taken as the lowest of:

Design Approach 1 Combination 1:

$$R_{b;k} = A_b q_{b;k}$$

$$R_{s;k} = A_{s;i} q_{s;i;k}$$

$$\gamma_b = 1.0 \text{ (Base)}$$

$$\gamma_s = 1.0 \text{ (Shaft Compression)}$$

$$\gamma_s = 1.0 \text{ (Shaft Tension)}$$

$$\gamma_{Rd} = 1.4 \text{ (Model Factor)}$$

$$R_{c;d} = (R_{b;k}/\gamma_b + R_{s;k}/\gamma_s)/\gamma_{Rd}$$

$$\gamma_G = 1.35$$

$$\gamma_Q = 1.5$$

$$\Psi_0 = 0.5 (Q_k > W_{L.})$$

$$F_{c;d} = G_k \cdot \gamma_G + Q_k \cdot \gamma_Q + W_{L.} \cdot \gamma_Q \cdot \Psi_0$$

$$\Psi_0 = 0.7 (Q_k < W_{L.})$$

$$F_{c;d} = G_k \cdot \gamma_G + Q_k \cdot \gamma_Q \cdot \Psi_0 + W_{L.} \cdot \gamma_Q$$

$$F_{c;d} < R_{c;d} : \text{OK}$$

Design Approach 1 Combination 2:

$$R_{b;k} = A_b q_{b;k}$$

$$R_{s;k} = A_{s;i} q_{s;i;k}$$

$$\gamma_b = 2.0 \text{ (Base)}$$

$$\gamma_s = 1.6 \text{ (Compression)}$$

$$\gamma_s = 2.0 \text{ (Tension)}$$

$$\gamma_{Rd} = 1.4 \text{ (Model Factor)}$$

$$R_{c;d} = (R_{b;k}/\gamma_b + R_{s;k}/\gamma_s)/\gamma_{Rd}$$

$$\gamma_G = 1.0$$

$$\gamma_Q = 1.3$$

$$\Psi_0 = 0.5 (Q_k > W_{L.})$$

$$F_{c;d} = G_k \cdot \gamma_G + Q_k \cdot \gamma_Q + W_{L.} \cdot \gamma_Q \cdot \Psi_0$$

$$\Psi_0 = 0.7 (Q_k < W_{L.})$$

$$F_{c;d} = G_k \cdot \gamma_G + Q_k \cdot \gamma_Q \cdot \Psi_0 + W_{L.} \cdot \gamma_Q$$

$$F_{c;d} < R_{c;d} : \text{OK}$$

Tension Loads, combination 1 for structural design and combination 2 for geotechnical design.

Design Approach 1 Combination 1:

$$\text{Tension} = G_{kt} \cdot \gamma_G + Q_{kt} \cdot \gamma_Q + W_{Lt.} \cdot \gamma_Q - (G_k \times 1)$$

Design Approach 1 Combination 2:

$$\text{Tension} = G_{kt} \cdot \gamma_G + Q_{kt} \cdot \gamma_Q + W_{Lt.} \cdot \gamma_Q - (G_k \times 1)$$

$F_{c;d}$	design axial compression load
$\gamma_G$	partial factor for permanent action
$\gamma_O$	partial factor for variable action
$R_{c;d}$	design value $R_c$
$R_{b;k}$	characteristic value for base resistance of pile
$\gamma_b$	partial factor for base resistance of pile
$R_{s;k}$	characteristic value for shaft resistance of pile
$\gamma_s$	partial factor for shaft resistance of pile
$\gamma_{R;d}$	partial factor for uncertainty in a resistance model
$q_{s;i;k}$	characteristic value of shaft resistance in stratum i
$q_{b;k}$	characteristic value of base resistance in stratum i
$A_{s;i}$	pile shaft surface area in stratum i
$G_k$	permanent action
$Q_k$	variable action

#### 4.2 Shear

**Shear loads have not been specified for the Contiguous wall apart from on piles CP321-352 of 100kN/m, please note that these piles can only accommodate a load of 55kN/m run this is currently what they have been designed for.**

#### 4.3 Tension

Tension loads have not been specified for the Contiguous wall

#### 4.4 Moments from Tolerances

Moment loads have not been specified for the Contiguous wall.

#### 4.5 Surcharges

An HA loading of 10kN/m<sup>2</sup> has been applied surrounding the proposed basement.

## 5.0 Bearing Capacity

### 5.1 Bearing Capacity – Cohesive Soils

#### Shaft Resistance - Clay (ULS)

Characteristic Shaft Resistance of Stratum  
 Characteristic Shaft Resistance of Pile

$$\begin{aligned} q_{s;i;k} &= \alpha \times C_{u \text{ av.}} \\ R_{s;k} &= A_{s;i} q_{s;i;k} \end{aligned}$$

Where:

$$A_{s;i} = \pi \times \text{dia} \times \text{length of shaft in clay}$$

$C_{u \text{ av.}}$  = Av. Undrained shear strength over length of shaft

$\alpha$  = adhesion

#### Base Resistance - Clay (ULS)

Characteristic Base Resistance of Stratum  
 Characteristic Base Resistance of Pile

$$\begin{aligned} q_{b;k} &= C_{u \text{ base}} \times N_c \\ R_{b;k} &= A_b q_{b;k} \end{aligned}$$

Where:

$$A_b \text{ (Area of base)} = \pi \times \text{dia}^2 \times 0.25$$

$N_c$  (Bearing capacity factor) = 9.0

$C_{u \text{ base}}$  = Undrained design shear strength at base

Pile capacity calculations can be found in Appendix B

### 5.2 Design Check for Structural ULS – Concrete Compression

Where geotechnical ULS resistances and SLS performance have been satisfied, the structural capacity of the pile is determined in accordance with BS EN 1997-1:2004 and BS EN 1992-1-1:2004. Calculations for the maximum loading case are provided in Appendix E.

## 6.0 Structural Design

### 6.1 Structural Parameters

Pile diameters	=	400mm male piles spaced at 550mm c-c
Concrete, $f_{cu}$	=	32/40 N/mm <sup>2</sup> DC-3
Steel $f_y$	=	500 N/mm <sup>2</sup> [high yield]
Materials factor	=	1.15 (reinforcement)
Cover	=	75mm

### 6.2 Reinforcement Design

- Reinforcement calculations have been undertaken in accordance with BS EN 1992-1-1:2004 with respect to bending moments. Reinforcement calculations are provided in Appendix D.
- Projection steel has been calculated after Table 13, Section 10 in The Concrete Centre 'How to Design Structures Using Eurocode 2' (2006). A good bond is assumed as detailed in Figure 1 of the guide. Based on a capping beam concrete strength of 32/40N/mm<sup>2</sup> the required projection for the H20 bar is 660mm. This requirement can be reduced as the maximum bending moment does not occur at the top of the pile.

Section	SLS		ULS		Design	
	BM	SF	BM	SF	BM	SF
1	90	59	128	68	<b>128</b>	<b>80</b>
2	177	92	232	105	<b>239</b>	<b>124</b>
3	143	83	179	94	<b>193</b>	<b>112</b>
4 (CP27-32)	132	165	224	167	<b>224</b>	<b>223</b>
5 (CP321-352)	244	119	252	120	<b>329</b>	<b>161</b>

**Fig 5 Design Bending moment and shear force summary**

Section	Reinforcement	Cage length (m)
1	6H20, H8@160	10
2	6H25, H8@160	10
3	6H20, H8@160	10 and 12
4 (CP27-32)	6H25, H10@160	10
5 (CP321-352)	6H32, H10@160	10

**Fig 6 Reinforcement Summary**

## 7.0 Serviceability Performance

### 7.1 Wall deflection

A summary of the maximum wall deflection calculated using Wallap is presented below. Benefits from capping beam stiffness have not been considered. We also note that the Wallap analysis software over predicts deflections. We would expect true measured deflections to be in line with Table 2.4 of CIRIA report 580 which provides information on expected movements for cantilever walls in the London Clay from actual field studies. We anticipate deflections to be less than 20mm.

Wall Section	Calculated deflection ignoring capping beam stiffness (mm)	max deflection (mm) predicted from CIRIA C580
1	27	14
2	60	20
3	42	20
4 (CP27-32)	21	20
5 (CP321-352)	67	

Fig 9 Wall deflections

Rock & Alluvium have designed the wall not to exceed the deflection criteria and have made/will make no assessment with respect to any damage criteria. It is important that retention of the soil during breaking down of the piles and construction of the capping beam is maintained to minimise ground disturbance during construction.

As per best practise it is advised that the wall should be monitored for movement. It is recommended that clearly identified and protected "Hilti" nail monitoring points are placed in the capping beam above selected wall piles. These points should be monitored from a remote point away from the excavation. A "zero" reading should be established before bulk excavation commences. The horizontal inward movement of the wall should be checked on a daily basis during excavation and twice weekly (Monday and Friday) until the permanent slabs have been cast

## 8.0 Pile Testing / Validation Requirements

No load pile load testing is required.

## 9.0 Outstanding Issues

- Construction Issue drawings
- The pile layout drawing needs to be revised to show 400mm diameter piles at 550mm spacing, the contiguous pile load table will also need updating.
- **Piles CP321-352 can only accommodate a load of 55kN/m run this is currently what they have been designed for, 100kN/m run is not achievable.**

## Appendix A

### **Strength Vs Depth Plots**

Site Address

Hampstead Green

Reference

16-0036

Rock & Alluvium 

Tel. 01372 389 333

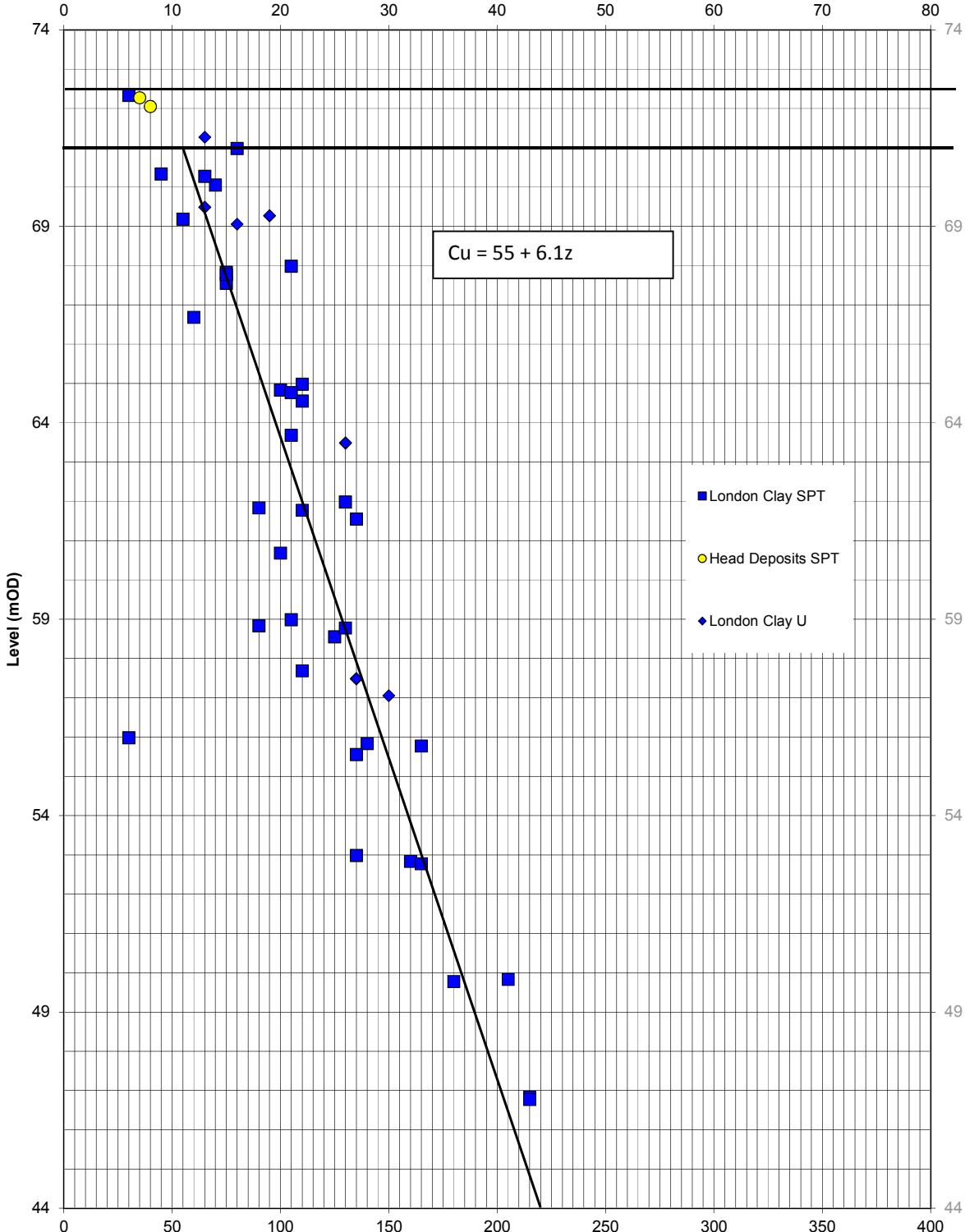
enquiries@rockal.com  
www.rockal.com

Date

22/01/2016

$$Cu = 5 * SPT$$

SPT N



Design based on site investigation report by CGL dated: Sep 2014

## Appendix B

### **CFA Bearing Pile Design Calculations**



## **Appendix C**

### **Wallap Analysis**

ROCK & ALLUVIUM LTD | Sheet No.  
 Program: WALLAP Version 6.05 Revision A45.B58.R49 | Job No. 16-0036  
 Licensed from GEOSOLVE | Made by : KK  
 Data filename/Run ID: Section 1 SLS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types			
		Active side		Passive side	
1	75.00	4 MG		4 MG	
2	72.00	1 Head deposits		1 Head deposits	
3	71.00	3 LC UN		3 LC UN	

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol. state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	18000	0.590	OC	0.376	3.077	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	35200	1.000	OC	0.361	3.253	2.500d
		( 3904)		(0.200)	(1.370)	( 4.831)	
3 LC UN ( 71.00 )	20.00	44000	1.000	OC	1.000	1.000	44.00u
		( 4880)		(0.490)	(2.389)	( 2.390)	( 4.900)
4 MG	18.00	10000	0.530	OC	0.309	3.868	
				(0.200)	(0.000)	( 0.000)	

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---			
Soil	Wall	Back-	Soil	Wall	Back-	
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.	
No. Description						
1 Head deposits	24.00	0.500	0.00	24.00	0.500	0.00
2 LC DR	25.00	0.500	0.00	25.00	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 MG	28.00	0.670	0.00	28.00	0.500	0.00

##### GROUND WATER CONDITIONS

Density of water	= 10.00 kN/m3	Active side	Passive side
Initial water table elevation		71.00	71.00

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side			
profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	74.00	74.00	0.0	1	71.50	71.50	0.0
					2	71.50	74.00	25.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 65.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	71.60	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**SURCHARGE LOADS**

Surch- -arge no.	Elev. m	Distance from wall to wall m	Length parallel to wall m	Width perpend. to wall m	Surcharge kN/m2	Equiv. soil type	Partial factor/ Category
1	75.00	0.50(A)	20.00	20.00	10.00	=	N/A N/A
2	71.50	-0.00(P)	20.00	20.00	25.00	=	N/A N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m2/m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 75.00 No analysis at this stage
3	Excavate to elevation 71.50 on PASSIVE side
4	Install strut or anchor no.1 at elevation 71.60
5	Apply surcharge no.2 at elevation 71.50
6	Apply water pressure profile no.1 No analysis at this stage
7	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
8	Change EI of wall to 31986 kN.m2/m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force	pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No				
2	Apply surcharge no.1 at elev. 75.00	No	No	No				
3	Excav. to elev. 71.50 on PASSIVE side	Yes	Yes	Yes				
4	Install strut no.1 at elev. 71.60	No	No	No				
5	Apply surcharge no.2 at elev. 71.50	No	No	No				
6	Apply water pressure profile no.1	No	No	No				
7	Change soil type 3 to soil type 2	No	No	No				
8	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No				
*	Summary output	Yes	-	Yes				

Program WALLAP - Copyright (C) 2013 by DL Borin, distributed by GEOSOLVE  
69 Rodenhurst Road, London SW4, UK. Tel: +44 20 8674 7251

ROCK & ALLUVIUM LTD | Sheet No.  
 Program: WALLAP Version 6.05 Revision A45.B58.R49 | Job No. 16-0036  
 Licensed from GEOSOLVE | Made by : KK  
 Data filename/Run ID: Section 1 SLS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

Stage No. 8 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 75.00 to 65.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

			FoS for toe elev. = 65.00	Toe elev. for FoS = 1.000		
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment Safety at elev.	Toe elev.	Wall Penetr -ation
Act.	Pass.	Elev.				
8	75.00	71.50	71.60	Conditions not suitable for FoS calc.		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	75.00	0.00	0.027	6.27E-03	0.0	-0.0		31986
2	74.50	3.34	0.024	6.26E-03	0.8	0.1		31986
3	74.00	6.95	0.021	6.26E-03	3.4	1.1		31986
4	73.60	12.34	0.018	6.23E-03	7.3	3.2		31986
5	73.20	17.58	0.016	6.16E-03	13.3	7.2		31986
6	72.60	25.30	0.012	5.92E-03	26.1	18.3		31986
7	72.00	32.92	0.009	5.37E-03	43.6	37.9		31986
		35.74	0.009	5.37E-03	43.6	37.9		
8	71.60	41.31	0.007	4.75E-03	59.0	57.0	67.8	31986
		41.31	0.007	4.75E-03	-8.8	57.0		
9	71.50	42.70	0.006	4.57E-03	-4.6	57.5		31986
		17.70	0.006	4.57E-03	-4.6	57.5		
10	71.00	5.35	0.004	3.65E-03	1.2	62.5		31986
		-12.92	0.004	3.65E-03	1.2	62.5		
11	70.60	-24.44	0.003	2.91E-03	-6.3	66.2		31986
12	70.20	-16.06	0.002	2.18E-03	-14.4	64.0		31986
13	69.60	-9.78	0.001	1.24E-03	-22.1	47.5		31986
14	69.00	3.93	0.000	5.84E-04	-23.9	29.5		31986
15	68.40	13.25	0.000	1.97E-04	-18.7	14.3		31986
16	67.80	12.68	0.000	2.02E-05	-10.9	4.6		31986
17	67.20	8.44	0.000	-3.32E-05	-4.6	0.1		31986
18	66.60	3.98	0.000	-3.48E-05	-0.9	-1.1		31986
19	66.00	0.46	0.000	-2.64E-05	0.4	-0.7		31986
20	65.50	-0.80	0.000	-2.30E-05	0.4	-0.2		31986
21	65.00	-0.60	0.000	-2.24E-05	0.0	0.0		---

At elev. 71.60 Strut force = 67.8 kN/strut = 67.8 kN/m run



Run ID. Section 1 SLS  
Hampstead Green  
Contig wall

| Sheet No.  
| Date:25-04-2016  
| Checked :

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(continued)

Stage No.8 Change EI of wall to 31986 kN.m2/m run  
From elevation 75.00 to 65.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	PASSIVE side					
		Water press.	Vertic -al	Active limit	Passive limit	Earth pressure	Total earth pressure
	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3	
21	65.00	90.00	63.77	19.60	219.51	121.11	211.11
							65468

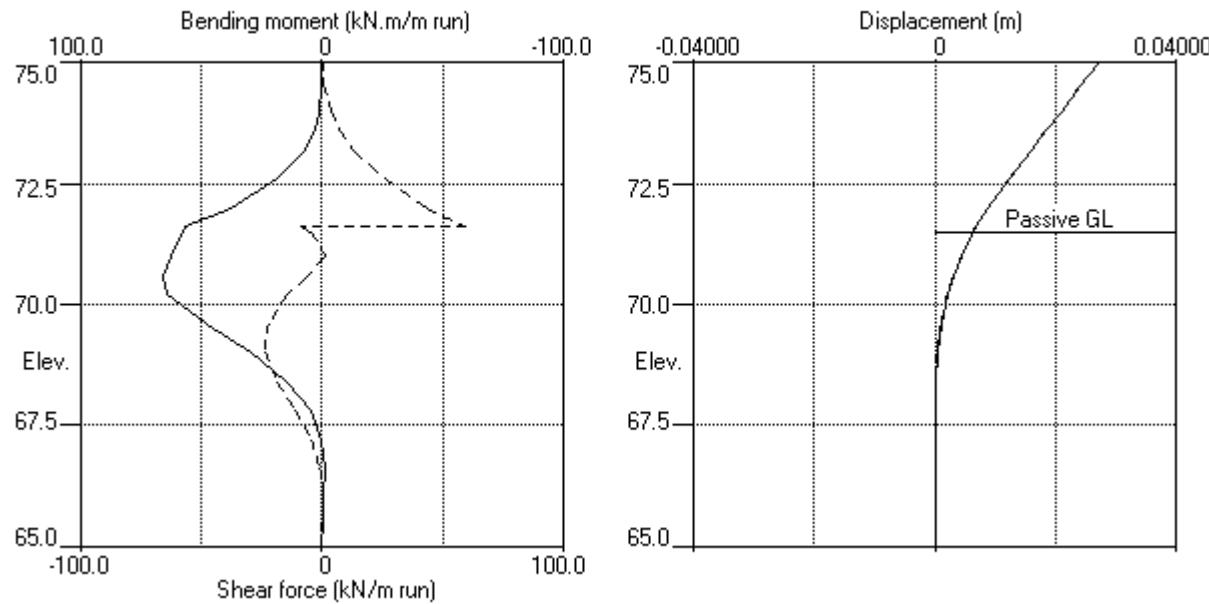
Note: 50.89a Soil pressure at active limit  
117.71p Soil pressure at passive limit

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Contig wall

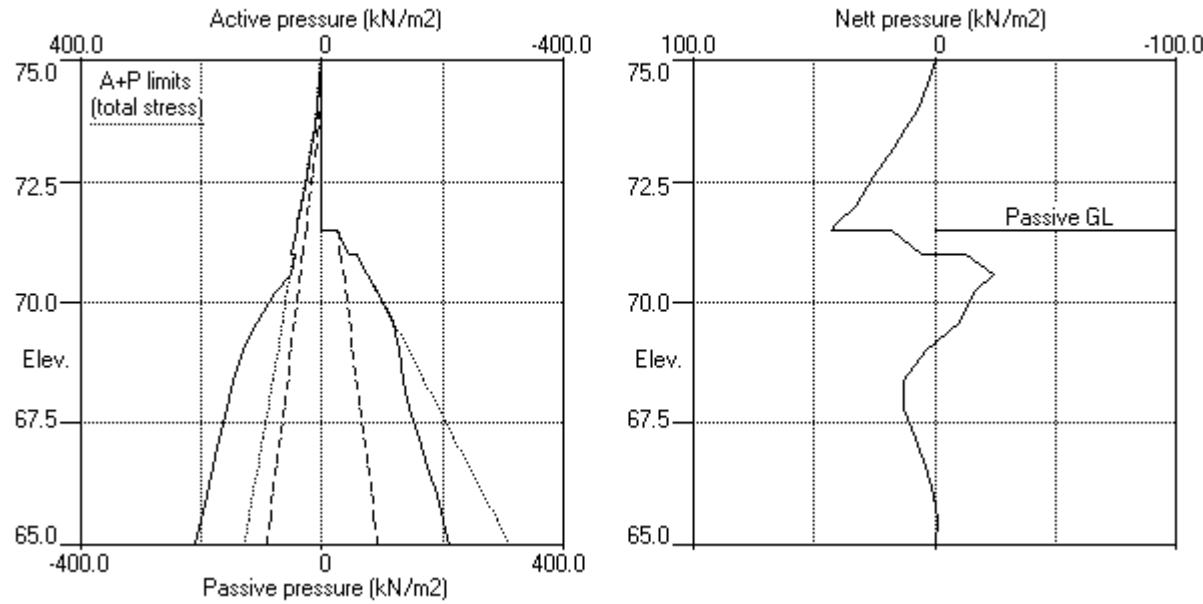
Sheet No.  
Job No. 16-0036  
Made by : KK  
Date: 25-04-2016  
Checked :

Units: kN,m

Stage No.8 Change EI of wall to 31986kN.m<sup>2</sup>/m run



Stage No.8 Change EI of wall to 31986kN.m<sup>2</sup>/m run



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 Data filename/Run ID: Section 1 SLS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000		
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.	Wall Penetr -ation
1	75.00	75.00	Cant.	Conditions not suitable for FoS calc.			
2	75.00	75.00		No analysis at this stage			
3	75.00	71.50	Cant.	2.126	65.84	68.77	2.73
4	75.00	71.50		No analysis at this stage			
5	75.00	71.50	71.60	Conditions not suitable for FoS calc.			
6	75.00	71.50		No analysis at this stage			
7	75.00	71.50		No analysis at this stage			
8	75.00	71.50	71.60	Conditions not suitable for FoS calc.			

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 Contig wall

	Sheet No.
	Job No. 16-0036
	Made by : KK
	Date: 25-04-2016
	Checked :

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Units: kN,m

### Summary of results

#### BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall

##### Analysis options

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
Passive side 20.00 from wall

#### Bending moment, shear force and displacement envelopes

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	75.00	0.027	0.000	0.0	-0.0	0.0	0.0
2	74.50	0.024	0.000	0.1	0.0	0.9	0.0
3	74.00	0.021	0.000	1.2	0.0	3.7	0.0
4	73.60	0.018	0.000	3.4	0.0	7.3	0.0
5	73.20	0.016	0.000	7.2	0.0	13.3	0.0
6	72.60	0.012	0.000	18.3	0.0	26.1	0.0
7	72.00	0.009	0.000	37.9	0.0	43.6	0.0
8	71.60	0.007	0.000	57.0	0.0	59.0	-8.8
9	71.50	0.006	0.000	57.5	0.0	45.5	-4.6
10	71.00	0.004	0.000	75.8	0.0	50.3	0.0
11	70.60	0.003	0.000	89.5	0.0	9.9	-6.3
12	70.20	0.002	0.000	87.9	0.0	0.0	-23.0
13	69.60	0.001	0.000	63.5	0.0	0.0	-42.7
14	69.00	0.001	-0.000	36.6	0.0	0.0	-39.7
15	68.40	0.001	-0.000	15.9	0.0	0.0	-27.7
16	67.80	0.001	-0.000	4.6	0.0	0.0	-15.0
17	67.20	0.001	0.000	0.1	-2.1	0.0	-5.4
18	66.60	0.001	0.000	0.0	-3.1	0.2	-0.9
19	66.00	0.001	0.000	0.0	-1.9	2.3	0.0
20	65.50	0.001	0.000	0.0	-0.7	1.9	0.0
21	65.00	0.001	0.000	0.0	0.0	0.0	-0.0

#### Maximum and minimum bending moment and shear force at each stage

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. 75.00	minimum kN.m/m	elev. 75.00	maximum kN/m	elev. 75.00	minimum kN/m	elev. 75.00
1	0.0	75.00	0.0	75.00	0.0	75.00	0.0	75.00
2	No calculation at this stage							
3	85.2	70.60	-2.9	66.60	49.2	71.00	-40.9	69.60
4	No calculation at this stage							
5	89.5	70.60	-3.1	66.60	50.3	71.00	-42.7	69.60
6	No calculation at this stage							
7	No calculation at this stage							
8	66.2	70.60	-1.1	66.60	59.0	71.60	-23.9	69.00

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
1	0.000	75.00	0.000	75.00	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 75.00
3	0.023	75.00	0.000	75.00	Excav. to elev. 71.50 on PASSIVE side
4	No calculation at this stage				Install strut no.1 at elev. 71.60
5	0.023	75.00	-0.000	68.40	Apply surcharge no.2 at elev. 71.50
6	No calculation at this stage				Apply water pressure profile no.1
7	No calculation at this stage				Change soil type 3 to soil type 2
8	0.027	75.00	0.000	75.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	--- Strut no. 1 ---
	at elev. 71.60
	kN/m run      kN/strut
5	slack      slack
8	67.76      67.76

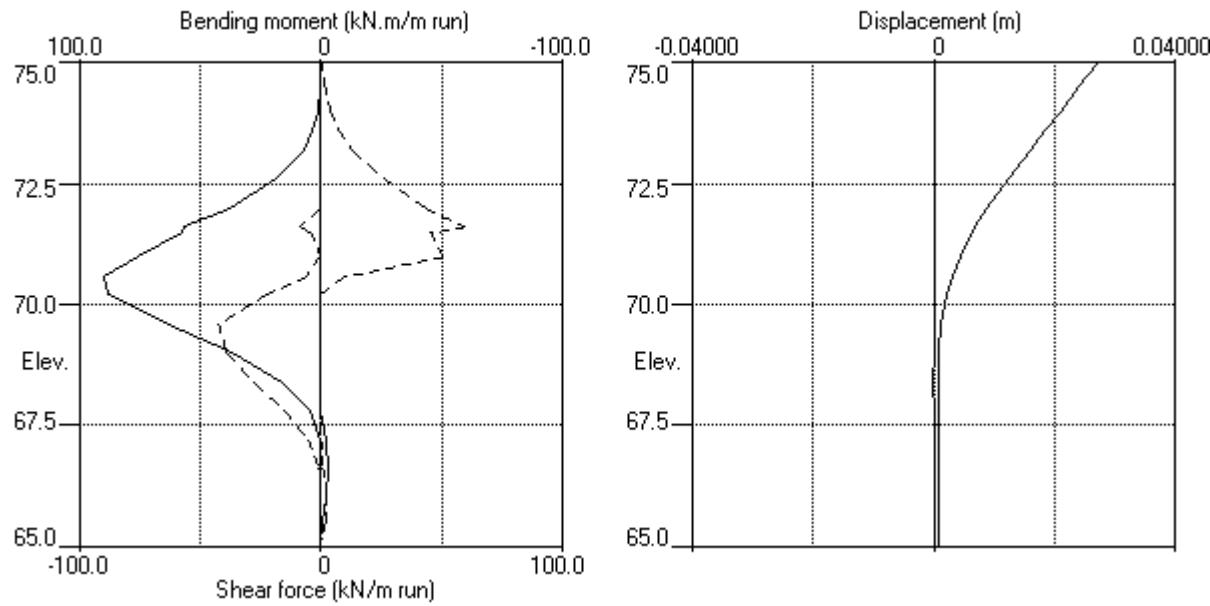
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Units: kN,m

Bending moment, shear force, displacement envelopes



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 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
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Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types			
		Active side		Passive side	
1	75.00	4 MG		4 MG	
2	72.00	1 Head deposits		1 Head deposits	
3	71.00	3 LC UN		3 LC UN	

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol. state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	9000	0.650	OC	0.436	2.540	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	17600	1.000	OC	0.422	2.648	2.100d
		( 1952)		(0.200)	(1.489)	( 4.248)	
3 LC UN ( 71.00 )	20.00	22000	1.000	OC	1.000	1.000	29.30u
		( 2440)		(0.490)	(2.389)	( 2.390)	( 3.300)
4 MG	18.00	5000	0.590	OC	0.368	3.060	
				(0.200)	(0.000)	( 0.000)	

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---				--- parameters for Kp ---			
Soil	Wall	Back-	Soil	Wall	Back-	angle	
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.	fill angle	
No. Description							
1 Head deposits	20.40	0.500	0.00	20.40	0.500	0.00	
2 LC DR	21.20	0.500	0.00	21.20	0.500	0.00	
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00	
4 MG	23.90	0.670	0.00	23.90	0.500	0.00	

##### GROUND WATER CONDITIONS

Density of water	= 10.00 kN/m3	Active side	Passive side
Initial water table elevation		71.00	71.00

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side			
profile no.	Point no.	Elev. m	Piez. elev. m	Water press. kN/m2	Point no.	Elev. m	Piez. elev. m	Water press. kN/m2
1	1	74.00	74.00	0.0	1	71.50	71.50	0.0
					2	71.50	74.00	25.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 65.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	71.60	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**SURCHARGE LOADS**

Surch- -arge no.	Elev. m	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge kN/m <sup>2</sup>	soil type	Equiv. factor/ Category
1	75.00	0.50(A)	20.00	20.00	10.00	=	N/A N/A
2	71.50	-0.00(P)	20.00	20.00	25.00	=	N/A N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m <sup>2</sup> /m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 75.00 No analysis at this stage
3	Excavate to elevation 71.15 on PASSIVE side
4	Fill to elevation 71.50 on PASSIVE side with soil type 1
5	Install strut or anchor no.1 at elevation 71.60
6	Apply surcharge no.2 at elevation 71.50
7	Apply water pressure profile no.1 No analysis at this stage
8	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
9	Change EI of wall to 31986 kN.m <sup>2</sup> /m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 75.00	No	No	No			
3	Excav. to elev. 71.15 on PASSIVE side	Yes	Yes	Yes			
4	Fill to elev. 71.50 on PASSIVE side	No	No	No			
5	Install strut no.1 at elev. 71.60	No	No	No			
6	Apply surcharge no.2 at elev. 71.50	No	No	No			
7	Apply water pressure profile no.1	No	No	No			
8	Change soil type 3 to soil type 2	No	No	No			
9	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
*	Summary output	Yes	-	Yes			

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 Contig wall

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	Job No. 16-0036
	Made by : KK
	Date: 25-04-2016
	Checked :

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Units: kN,m

Stage No. 9 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 75.00 to 65.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

### STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method

Factor of safety on soil strength

			FoS for toe elev. = 65.00	Toe elev. for FoS = 1.000		
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment	Toe elev.	Wall Penetr
9	75.00	71.50	71.60	Conditions not suitable for FoS calc.		

### BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall

#### Analysis options

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	75.00	0.00	0.052	1.03E-02	0.0	0.0		31986
2	74.50	3.98	0.047	1.03E-02	1.0	0.1		31986
3	74.00	8.28	0.041	1.03E-02	4.1	1.4		31986
4	73.60	13.93	0.037	1.02E-02	8.5	3.9		31986
5	73.20	19.41	0.033	1.02E-02	15.2	8.5		31986
6	72.60	28.50	0.027	9.92E-03	29.5	21.5		31986
7	72.00	37.50	0.021	9.29E-03	49.3	44.0		31986
		41.53	0.021	9.29E-03	49.3	44.0		
8	71.60	48.35	0.018	8.58E-03	67.3	66.0	73.1	31986
		48.35	0.018	8.58E-03	-5.7	66.0		
9	71.50	50.01	0.017	8.37E-03	-0.8	67.0		31986
		25.01	0.017	8.37E-03	-0.8	67.0		
10	71.15	18.34	0.014	7.62E-03	6.8	72.4		31986
11	71.00	16.09	0.013	7.29E-03	9.3	75.5		31986
		-3.24	0.013	7.29E-03	9.3	75.5		
12	70.60	-12.10	0.010	6.40E-03	6.3	82.9		31986
13	70.20	-20.95	0.008	5.47E-03	-0.3	86.4		31986
14	69.60	-19.98	0.005	4.07E-03	-12.6	86.2		31986
15	69.00	-10.59	0.003	2.75E-03	-21.8	75.3		31986
16	68.40	-7.70	0.002	1.65E-03	-27.3	55.5		31986
17	67.80	8.40	0.001	8.80E-04	-27.1	35.0		31986
18	67.20	13.71	0.001	4.07E-04	-20.4	18.6		31986
19	66.60	12.71	0.000	1.64E-04	-12.5	8.0		31986
20	66.00	8.65	0.000	6.19E-05	-6.1	2.5		31986
21	65.50	4.32	0.000	3.27E-05	-2.8	0.7		31986
22	65.00	7.08	0.000	2.58E-05	0.0	0.0		---

At elev. 71.60 Strut force = 73.1 kN/strut = 73.1 kN/m run

(continued)

Stage No.9 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 75.00 to 65.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total earth pressure kN/m <sup>2</sup>	Soil stiffness kN/m <sup>3</sup>
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>			
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	959
2	74.50	0.00	10.82	3.98	33.10	3.98	3.98a	3.98a	959
3	74.00	0.00	22.50	8.28	68.85	8.28	8.28a	8.28a	959
4	73.60	4.00	26.99	9.93	82.59	9.93	13.93a	13.93a	959
5	73.20	8.00	31.01	11.41	94.89	11.41	19.41a	19.41a	959
6	72.60	14.00	36.57	13.46	111.90	14.50	28.50	28.50	959
7	72.00	20.00	41.81	15.39	127.95	17.50	37.50	37.50	959
		20.00	41.81	18.24	106.20	21.53	41.53	41.53	1725
8	71.60	24.00	46.01	20.07	116.85	24.35	48.35	48.35	1725
9	71.50	25.00	47.05	20.53	119.49	25.01	50.01	50.01	1725
10	71.15	28.50	50.66	22.10	128.66	27.22	55.72	55.72	1725
11	71.00	30.00	52.20	22.77	132.57	28.13	58.13	58.13	1725
		30.00	52.20	18.91	147.12	18.91	48.91a	48.91a	3374
12	70.60	34.00	56.27	20.63	157.91	20.63	54.63a	54.63a	3524
13	70.20	38.00	60.31	22.34	168.61	22.34	60.34a	60.34a	3674
14	69.60	44.00	66.33	24.88	184.54	39.11	83.11	83.11	3898
15	69.00	50.00	72.30	27.40	200.35	64.23	114.23	114.23	4123
16	68.40	56.00	78.23	29.91	216.06	82.25	138.25	138.25	4347
17	67.80	62.00	84.13	32.40	231.69	94.39	156.39	156.39	4572
18	67.20	68.00	90.01	34.89	247.26	102.43	170.43	170.43	4796
19	66.60	74.00	95.88	37.36	262.78	108.06	182.06	182.06	5021
20	66.00	80.00	101.73	39.83	278.27	112.51	192.51	192.51	5245
21	65.50	85.00	106.59	41.89	291.15	115.84	200.84	200.84	5432
22	65.00	90.00	111.45	43.94	304.02	122.76	212.76	212.76	163195

Node no.	Y coord	PASSIVE side						Total earth pressure kN/m <sup>2</sup>	Soil stiffness kN/m <sup>3</sup>
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>			
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	74.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	73.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	73.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	72.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	71.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		25.00	0.00	0.00	0.00	0.00	25.00	25.00	2128
10	71.15	28.50	3.50	1.53	8.89	8.89	37.39p	37.39p	2128
11	71.00	30.00	5.00	2.18	12.69	12.05	42.05	42.05	2128
		30.00	5.00	0.00	22.16	22.16	52.16p	52.16p	4161
12	70.60	34.00	8.99	0.67	32.73	32.73	66.73p	66.73p	4345
13	70.20	38.00	12.98	2.35	43.30	43.30	81.30p	81.30p	4530
14	69.60	44.00	18.95	4.87	59.09	59.09	103.09p	103.09p	4807
15	69.00	50.00	24.89	7.38	74.82	74.82	124.82p	124.82p	5084
16	68.40	56.00	30.80	9.88	90.46	89.95	145.95	145.95	5360
17	67.80	62.00	36.67	12.36	106.02	85.98	147.98	147.98	5637
18	67.20	68.00	42.52	14.83	121.50	88.72	156.72	156.72	5914
19	66.60	74.00	48.34	17.29	136.91	95.35	169.35	169.35	6191

Run ID. Section 1 ULS  
Hampstead Green  
Contig wall

| Sheet No.  
| Date: 25-04-2016  
| Checked :

(continued)

Stage No.9 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
From elevation 75.00 to 65.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	PASSIVE side						Soil stiffness	
		Effective stresses							
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>	Total earth pressure kN/m <sup>2</sup>		
20	66.00	80.00	54.14	19.73	152.26	103.85	183.85	6468	
21	65.50	85.00	58.96	21.77	165.03	111.52	196.52	6699	
22	65.00	90.00	63.77	23.80	177.77	115.68	205.68	163195	

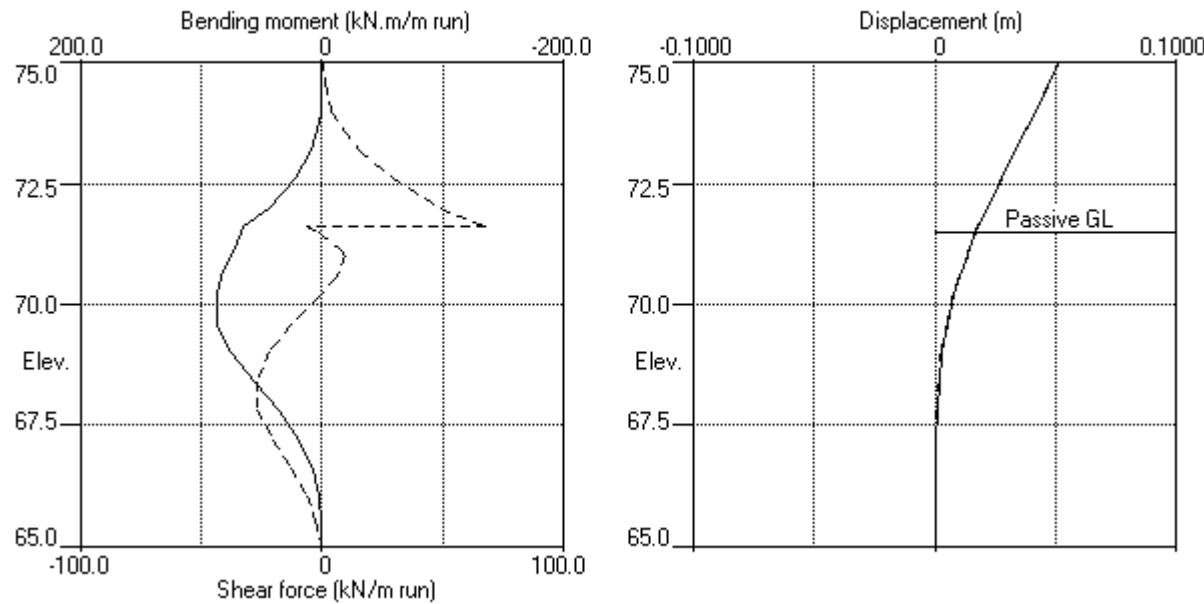
Note: 60.34a Soil pressure at active limit  
124.82p Soil pressure at passive limit

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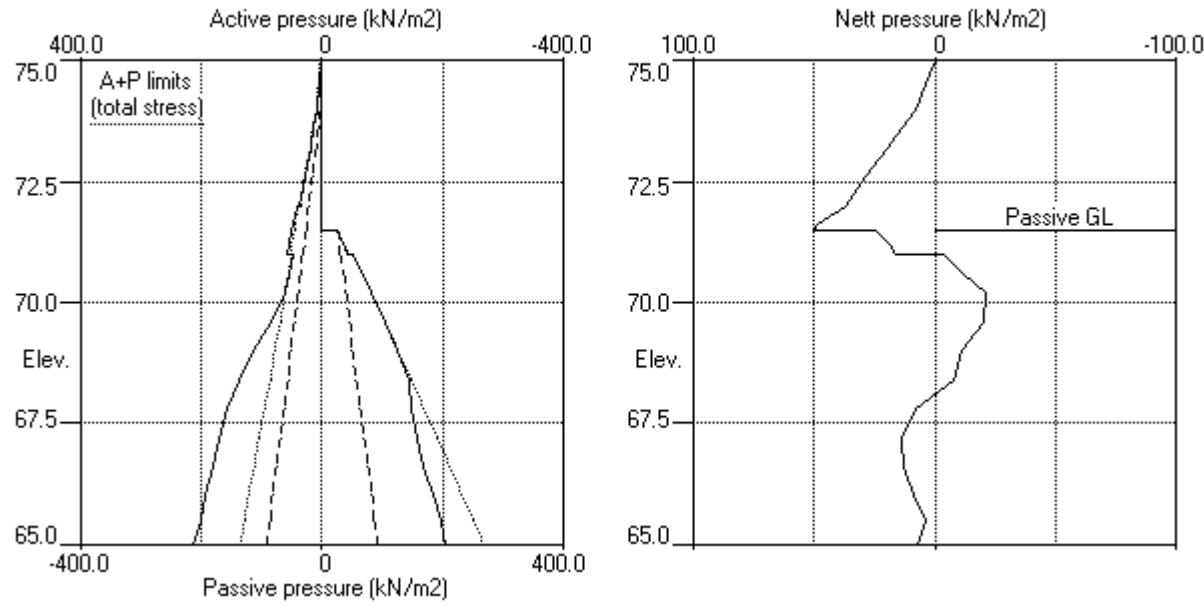
Sheet No.  
Job No. 16-0036  
Made by : KK  
Date: 25-04-2016  
Checked :

Units: kN,m

Stage No.9 Change EI of wall to 31986kN.m<sup>2</sup>/m run



Stage No.9 Change EI of wall to 31986kN.m<sup>2</sup>/m run



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Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000		
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.	Wall Penetr -ation
1	75.00	75.00	Cant.	Conditions not suitable for FoS calc.			
2	75.00	75.00		No analysis at this stage			
3	75.00	71.15	Cant.	1.403	65.75	67.62	3.53
4	75.00	71.50	Cant.	1.485	65.79	67.88	3.62
5	75.00	71.50		No analysis at this stage			
6	75.00	71.50	71.60	Conditions not suitable for FoS calc.			
7	75.00	71.50		No analysis at this stage			
8	75.00	71.50		No analysis at this stage			
9	75.00	71.50	71.60	Conditions not suitable for FoS calc.			

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	Job No. 16-0036
	Made by : KK
	Date: 25-04-2016
	Checked :

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Units: kN,m

### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached  
Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	75.00	0.052	0.000	0.0	0.0	0.0	0.0
2	74.50	0.047	0.000	0.2	0.0	1.2	0.0
3	74.00	0.041	0.000	1.6	0.0	4.8	0.0
4	73.60	0.037	0.000	4.3	0.0	9.2	0.0
5	73.20	0.033	0.000	9.1	0.0	15.2	0.0
6	72.60	0.027	0.000	21.5	0.0	29.5	0.0
7	72.00	0.021	0.000	44.0	0.0	49.3	0.0
8	71.60	0.018	0.000	66.0	0.0	67.3	-5.7
9	71.50	0.017	0.000	67.0	0.0	55.0	-0.8
10	71.15	0.014	0.000	84.3	0.0	63.3	0.0
11	71.00	0.013	0.000	94.1	0.0	66.9	0.0
12	70.60	0.010	0.000	115.9	0.0	43.3	0.0
13	70.20	0.008	0.000	127.3	0.0	16.6	-0.3
14	69.60	0.005	0.000	127.0	0.0	0.0	-24.8
15	69.00	0.003	0.000	106.4	0.0	0.0	-48.6
16	68.40	0.002	0.000	73.4	0.0	0.0	-52.5
17	67.80	0.002	-0.000	43.4	0.0	0.0	-43.5
18	67.20	0.001	-0.000	21.2	0.0	0.0	-29.8
19	66.60	0.002	-0.000	8.0	0.0	0.0	-16.5
20	66.00	0.002	-0.000	2.5	0.0	0.0	-6.5
21	65.50	0.002	0.000	0.7	-0.1	0.0	-2.8
22	65.00	0.002	0.000	0.0	0.0	0.0	-0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. 75.00	minimum 0.0	elev. 75.00	maximum kN/m	elev. 75.00	minimum 0.0	elev. 75.00
1	0.0	75.00	0.0	75.00	0.0	75.00	0.0	75.00
2	No calculation at this stage							
3	121.8	69.60	-0.0	65.50	66.3	71.00	-50.3	68.40
4	123.1	69.60	-0.0	65.50	66.8	71.00	-50.8	68.40
5	No calculation at this stage							
6	127.3	70.20	-0.1	65.50	66.9	71.00	-52.5	68.40
7	No calculation at this stage							
8	No calculation at this stage							
9	86.4	70.20	0.0	75.00	67.3	71.60	-27.3	68.40

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
	m		m		
1	0.000	75.00	0.000	75.00	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 75.00
3	0.049	75.00	0.000	75.00	Excav. to elev. 71.15 on PASSIVE side
4	0.049	75.00	0.000	75.00	Fill to elev. 71.50 on PASSIVE side
5	No calculation at this stage				Install strut no.1 at elev. 71.60
6	0.048	75.00	-0.000	67.20	Apply surcharge no.2 at elev. 71.50
7	No calculation at this stage				Apply water pressure profile no.1
8	No calculation at this stage				Change soil type 3 to soil type 2
9	0.052	75.00	0.000	75.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 ---	
	at elev.	71.60
	kN/m run	kN/strut
6	slack	slack
9	73.06	73.06

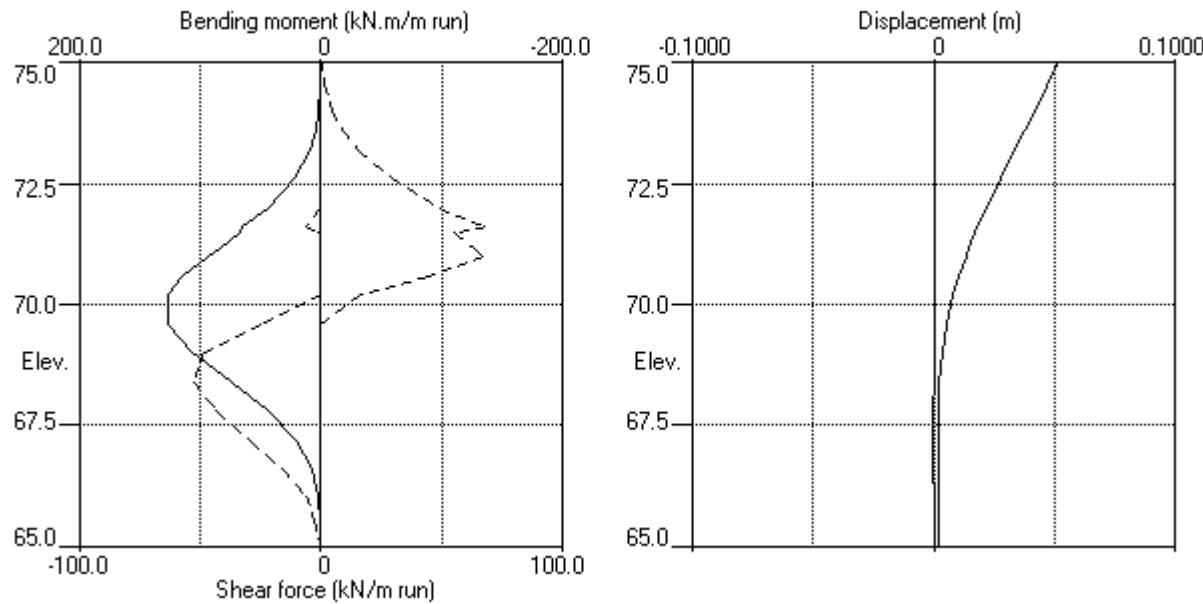
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Bending moment, shear force, displacement envelopes



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Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types			
		Active side		Passive side	
1	72.00	1 Head deposits		1 Head deposits	
2	71.00	3 LC UN		3 LC UN	
3	67.20	3 LC UN		4 LC UN	
4	66.70	3 LC UN		3 LC UN	

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC (Nu)	Ka (Kac)	Kp (Kpc)	kN/m2 (dc/dy)
1 Head deposits	20.00	18000	0.590	OC (0.200)	0.376 (0.000)	3.077 (0.000)	
2 LC DR ( 71.00 )	20.00	35200	1.000	OC (0.200)	0.361 (1.370)	3.253 (4.831)	2.500d
3 LC UN ( 71.00 )	20.00	44000	1.000	OC (0.490)	1.000 (2.389)	1.000 (2.390)	44.00u ( 4.900)
4 LC UN ( 71.00 )	20.00	44000	1.000	OC (0.490)	1.000 (2.389)	1.000 (2.390)	44.00u ( 4.900)
5 LC soft ( 67.20 )	20.00	1 ( 125088 )	1.000	OC (0.490)	1.000 (2.389)	1.000 (2.390)	1.000u ( 125.0 )

##### Additional soil parameters associated with Ka and Kp

----- Soil type -----	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction	Wall adhesion	Backfill	Soil friction	Wall adhesion	Backfill
No. Description	angle	coeff.	angle	angle	coeff.	angle
1 Head deposits	24.00	0.500	0.00	24.00	0.500	0.00
2 LC DR	25.00	0.500	0.00	25.00	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
5 LC soft	0.00	0.500	0.00	0.00	0.500	0.00

##### GROUND WATER CONDITIONS

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	67.00	67.00

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side				
	profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
	1	1	71.00	71.00	0.0	1	67.20	67.20	0.0
						2	67.20	71.00	38.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 62.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	67.90	1.00	0.400000	1.500E+07	20.00	0.00	0 No
2	71.50	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**SURCHARGE LOADS**

Surcharge no.	Elev. m	Distance from wall 0.50(A) -0.00(P)	Length parallel to wall 20.00	Width perpend. to wall 20.00	Surcharge kN/m2 Near edge 10.00	Equiv. soil type =	Partial factor/ Category
1	72.00	0.50(A)	20.00	20.00	10.00	=	N/A N/A
2	67.20	-0.00(P)	20.00	20.00	38.00	=	N/A N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m2/m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 72.00 No analysis at this stage
3	Excavate to elevation 67.20 on PASSIVE side
4	Change properties of soil type 4 to soil type 5 Ko pressures will not be reset
5	Install strut or anchor no.1 at elevation 67.90
6	Apply surcharge no.2 at elevation 67.20
7	Install strut or anchor no.2 at elevation 71.50
8	Apply water pressure profile no.1 No analysis at this stage
9	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
10	Change properties of soil type 5 to soil type 2 No analysis at this stage Ko pressures will not be reset
11	Change EI of wall to 31986 kN.m2/m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 5.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 72.00	No	No	No			
3	Excav. to elev. 67.20 on PASSIVE side	Yes	Yes	Yes			
4	Change soil type 4 to soil type 5	No	No	No			
5	Install strut no.1 at elev. 67.90	No	No	No			
6	Apply surcharge no.2 at elev. 67.20	No	No	No			
7	Install strut no.2 at elev. 71.50	No	No	No			
8	Apply water pressure profile no.1	No	No	No			
9	Change soil type 3 to soil type 2	No	No	No			
10	Change soil type 5 to soil type 2	No	No	No			
11	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
*	Summary output	Yes	-	Yes			

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Units: kN,m

Stage No. 11 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

			FoS for toe elev. = 62.00	Toe elev. for FoS = 1.000	
Stage --- G.L. ---	Strut No.	Factor Act. Pass. Elev.	Moment of equilib.	Toe elev. Safety at elev.	Wall Penetr-ation
11	72.00	67.20		More than one strut	

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	72.00	0.00	0.060	1.10E-02	0.0	0.0		31986
2	71.50	4.45	0.054	1.10E-02	1.1	0.2	4.7	31986
		4.45	0.054	1.10E-02	-3.6	0.2		
3	71.00	9.22	0.049	1.11E-02	-0.2	-0.3		31986
		5.42	0.049	1.11E-02	-0.2	-0.3		
4	70.60	11.33	0.044	1.11E-02	3.2	0.6		31986
5	70.20	17.07	0.040	1.10E-02	8.9	3.2		31986
6	69.60	25.51	0.033	1.09E-02	21.7	11.9		31986
7	69.00	33.84	0.027	1.06E-02	39.5	28.8		31986
8	68.45	42.66	0.021	9.86E-03	60.5	54.2		31986
9	67.90	50.73	0.016	8.55E-03	86.2	91.5	128.1	31986
		50.73	0.016	8.55E-03	-41.9	91.5		
10	67.55	53.74	0.013	7.55E-03	-23.6	87.4		31986
11	67.20	58.52	0.011	6.65E-03	-4.0	89.9		31986
		8.44	0.011	6.65E-03	-4.0	89.9		
12	67.00	2.67	0.009	6.16E-03	-2.9	93.3		31986
13	66.70	-6.01	0.008	5.42E-03	-3.4	97.4		31986
14	66.35	-16.11	0.006	4.56E-03	-7.2	99.9		31986
15	66.00	-26.20	0.005	3.72E-03	-14.6	97.6		31986
16	65.40	-9.04	0.003	2.43E-03	-25.2	74.6		31986
17	64.80	2.54	0.002	1.47E-03	-27.2	46.5		31986
18	64.20	10.91	0.001	8.38E-04	-23.1	26.0		31986
19	63.60	13.49	0.000	4.57E-04	-15.8	12.1		31986
20	63.00	7.69	0.000	2.53E-04	-9.5	5.3		31986
21	62.50	0.83	0.000	1.68E-04	-7.3	2.4		31986
22	62.00	28.50	0.000	1.40E-04	0.0	-0.0		---

At elev. 71.50 Strut force = 4.7 kN/strut = 4.7 kN/m run

At elev. 67.90 Strut force = 128.1 kN/strut = 128.1 kN/m run

(continued)

Stage No.11 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total pressure kN/m <sup>2</sup>	Soil stiffness kN/m <sup>3</sup>		
		Effective stresses									
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>					
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	31863		
2	71.50	0.00	11.82	4.45	36.36	4.45	4.45a	4.45a	4793		
3	71.00	0.00	24.50	9.22	75.38	9.22	9.22a	9.22a	4793		
		0.00	24.50	5.42	91.76	5.42	5.42a	5.42a	9373		
4	70.60	4.00	29.79	7.33	108.97	7.33	11.33a	9789			
5	70.20	8.00	34.61	9.07	124.65	9.07	17.07a	10204			
6	69.60	14.00	41.37	11.51	146.63	11.51	25.51a	10828			
7	69.00	20.00	47.81	13.84	167.60	13.84	33.84a	11452			
8	68.45	25.50	53.56	15.91	186.31	17.16	42.66	12023			
9	67.90	31.00	59.22	17.95	204.70	19.73	50.73	12595			
10	67.55	34.50	62.78	19.24	216.27	19.24	53.74a	12959			
11	67.20	38.00	66.31	20.52	227.78	20.52	58.52a	13323			
12	67.00	40.00	68.32	21.24	234.32	21.24	61.24a	13531			
13	66.70	43.00	71.33	22.33	244.09	22.33	65.33a	13843			
14	66.35	46.50	74.82	23.59	255.45	23.59	70.09a	14206			
15	66.00	50.00	78.30	24.84	266.76	24.84	74.84a	14570			
16	65.40	56.00	84.23	26.98	286.06	61.37	117.37	15194			
17	64.80	62.00	90.13	29.12	305.26	92.18	154.18	15818			
18	64.20	68.00	96.01	31.24	324.39	110.75	178.75	16441			
19	63.60	74.00	101.88	33.35	343.46	120.62	194.62	17065			
20	63.00	80.00	107.73	35.47	362.48	126.44	206.44	17689			
21	62.50	85.00	112.59	37.22	378.31	130.03	215.03	18209			
22	62.00	90.00	117.45	38.98	394.12	150.82	240.82	149417			

Node no.	Y coord	PASSIVE side						Total pressure kN/m <sup>2</sup>	Soil stiffness kN/m <sup>3</sup>		
		Effective stresses									
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>					
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
2	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
3	71.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
4	70.60	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
5	70.20	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
6	69.60	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
7	69.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
8	68.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
9	67.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
10	67.55	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
11	67.20	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
	38.00	-0.00	0.00	12.08	12.08	50.08p	13993				
12	67.00	40.00	2.00	0.00	18.57	18.57	58.57p	14211			
13	66.70	43.00	5.00	0.00	28.33	28.33	71.33p	14539			
14	66.35	46.50	8.49	0.00	39.70	39.70	86.20p	14921			
15	66.00	50.00	11.98	0.90	51.04	51.04	101.04p	15303			
16	65.40	56.00	17.93	3.05	70.41	70.41	126.41p	15958			
17	64.80	62.00	23.85	5.18	89.65	89.65	151.65p	16613			
18	64.20	68.00	29.71	7.30	108.73	99.84	167.84	17268			
19	63.60	74.00	35.53	9.40	127.66	107.12	181.12	17923			
20	63.00	80.00	41.31	11.49	146.44	118.76	198.76	18578			
21	62.50	85.00	46.08	13.21	161.98	129.20	214.20	19124			

Run ID. Section 2 SLS  
Hampstead Green  
Contig wall

| Sheet No.  
| Date:25-04-2016  
| Checked :

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(continued)

Stage No.11 Change EI of wall to 31986 kN.m2/m run  
From elevation 72.00 to 62.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	PASSIVE side						
		Water press. kN/m2	Vertic -al limit kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2	Total earth pressure kN/m2	Soil stiffness coeff. kN/m3
22	62.00	90.00	50.84	14.93	177.44	122.32	212.32	149417

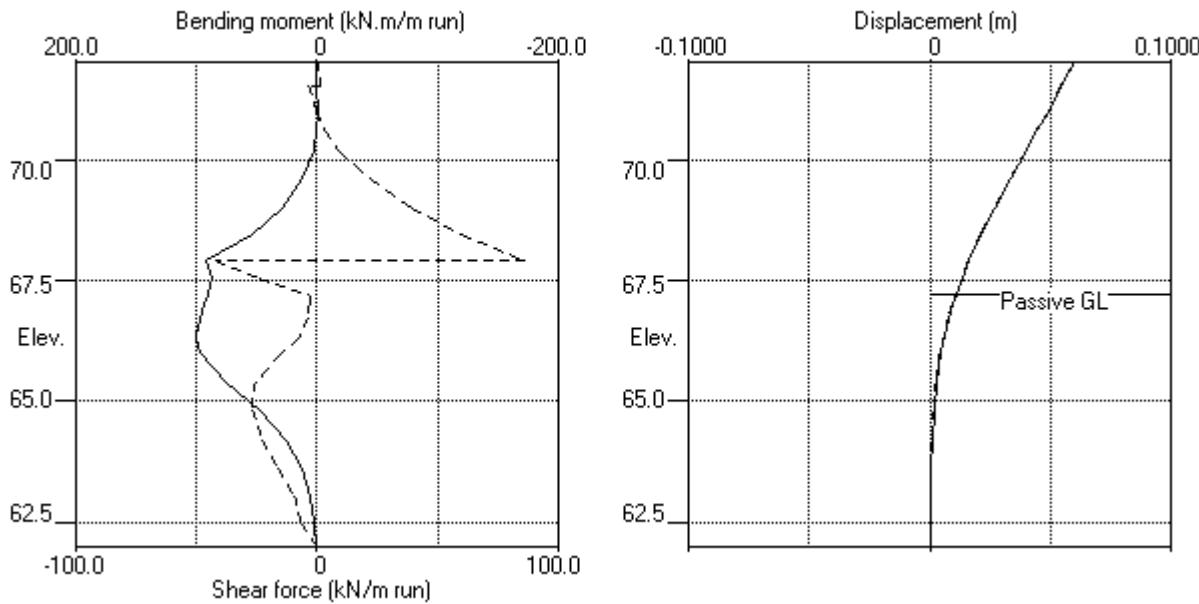
Note: 74.84a Soil pressure at active limit  
151.65p Soil pressure at passive limit

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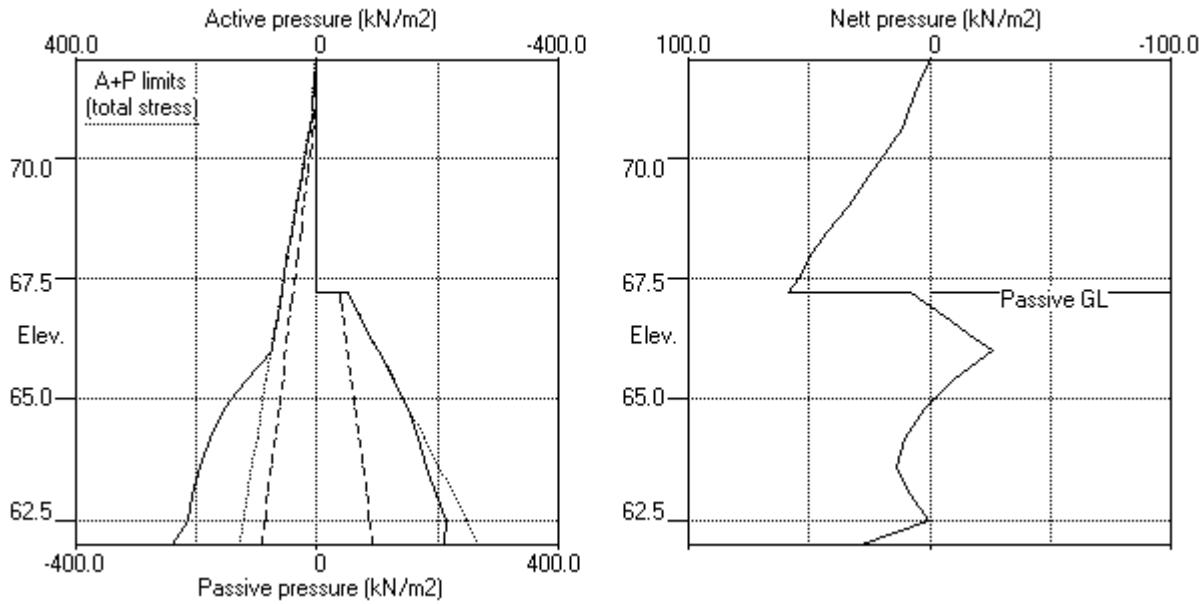
Sheet No.  
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Units: kN,m

Stage No.11 Change EI of wall to 31986kN.m<sup>2</sup>/m run



Stage No.11 Change EI of wall to 31986kN.m<sup>2</sup>/m run



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Contig wall | Checked :  
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Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000		
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.	Wall Penetr -ation
1	72.00	72.00	Cant.	Conditions not suitable for FoS calc.			
2	72.00	72.00		No analysis at this stage			
3	72.00	67.20	Cant.	2.175	62.70	64.52	2.68
4	72.00	67.20	Cant.	2.049	62.76	64.12	3.08
5	72.00	67.20		No analysis at this stage			
6	72.00	67.20	67.90	Conditions not suitable for FoS calc.			
7	72.00	67.20		No analysis at this stage			

All remaining stages have more than one strut - FoS calculation n/a

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	Date: 25-04-2016
	Checked :

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Units: kN,m

### Summary of results

#### BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall

##### Analysis options

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall

Passive side 20.00 from wall

#### Bending moment, shear force and displacement envelopes

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	72.00	0.060	0.000	0.0	0.0	0.0	0.0
2	71.50	0.054	0.000	0.2	0.0	1.1	-3.6
3	71.00	0.049	0.000	1.5	-0.3	4.5	-0.2
4	70.60	0.044	0.000	3.8	-0.0	6.9	0.0
5	70.20	0.040	-0.000	7.1	-0.0	10.1	0.0
6	69.60	0.033	-0.000	15.1	-0.0	21.7	0.0
7	69.00	0.027	-0.000	28.8	-0.0	39.5	0.0
8	68.45	0.021	-0.000	54.2	-0.0	60.5	0.0
9	67.90	0.016	-0.000	91.5	0.0	86.2	-41.9
10	67.55	0.013	-0.000	96.5	0.0	73.1	-23.6
11	67.20	0.011	-0.000	124.8	0.0	89.2	-4.0
12	67.00	0.009	-0.000	142.5	0.0	85.7	-2.9
13	66.70	0.008	-0.000	164.5	0.0	57.2	-3.4
14	66.35	0.006	-0.000	176.9	0.0	5.9	-29.2
15	66.00	0.005	0.000	171.7	0.0	0.0	-64.0
16	65.40	0.003	0.000	121.4	0.0	0.0	-91.4
17	64.80	0.002	-0.000	64.7	0.0	0.0	-80.5
18	64.20	0.001	-0.000	26.0	0.0	0.0	-50.4
19	63.60	0.001	-0.000	12.1	-1.9	0.0	-22.3
20	63.00	0.001	-0.000	5.3	-3.3	0.9	-9.5
21	62.50	0.001	0.000	2.4	-1.5	3.4	-7.3
22	62.00	0.001	0.000	0.0	-0.0	0.0	0.0

#### Maximum and minimum bending moment and shear force at each stage

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. kn. m/m	minimum kN.m/m	elev. kn. m/m	maximum kN/m	elev. kn. m/m	minimum kN/m	elev. kn. m/m
1	0.0	64.80	-0.0	63.00	0.0	72.00	0.0	72.00
2	No calculation at this stage							
3	144.4	66.70	-3.3	63.00	79.4	67.20	-77.7	65.40
4	169.4	66.35	-1.9	63.00	80.4	67.00	-88.0	65.40
5	No calculation at this stage							
6	176.9	66.35	-1.9	63.00	89.2	67.20	-91.4	65.40
7	No calculation at this stage							
8	No calculation at this stage							
9	No calculation at this stage							
10	No calculation at this stage							
11	99.9	66.35	-0.3	71.00	86.2	67.90	-41.9	67.90

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
	m		m		
1	0.000	62.00	-0.000	67.20	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 72.00
3	0.048	72.00	0.000	72.00	Excav. to elev. 67.20 on PASSIVE side
4	0.059	72.00	0.000	72.00	Change soil type 4 to soil type 5
5	No calculation at this stage				Install strut no.1 at elev. 67.90
6	0.060	72.00	-0.000	64.20	Apply surcharge no.2 at elev. 67.20
7	No calculation at this stage				Install strut no.2 at elev. 71.50
8	No calculation at this stage				Apply water pressure profile no.1
9	No calculation at this stage				Change soil type 3 to soil type 2
10	No calculation at this stage				Change soil type 5 to soil type 2
11	0.060	72.00	0.000	72.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	--- Strut no. 1 ---	at elev. 67.90	kN/m run	--- Strut no. 2 ---	at elev. 71.50	kN/m run
6	slack	slack		---	---	
11	128.08	128.08		4.68	4.68	

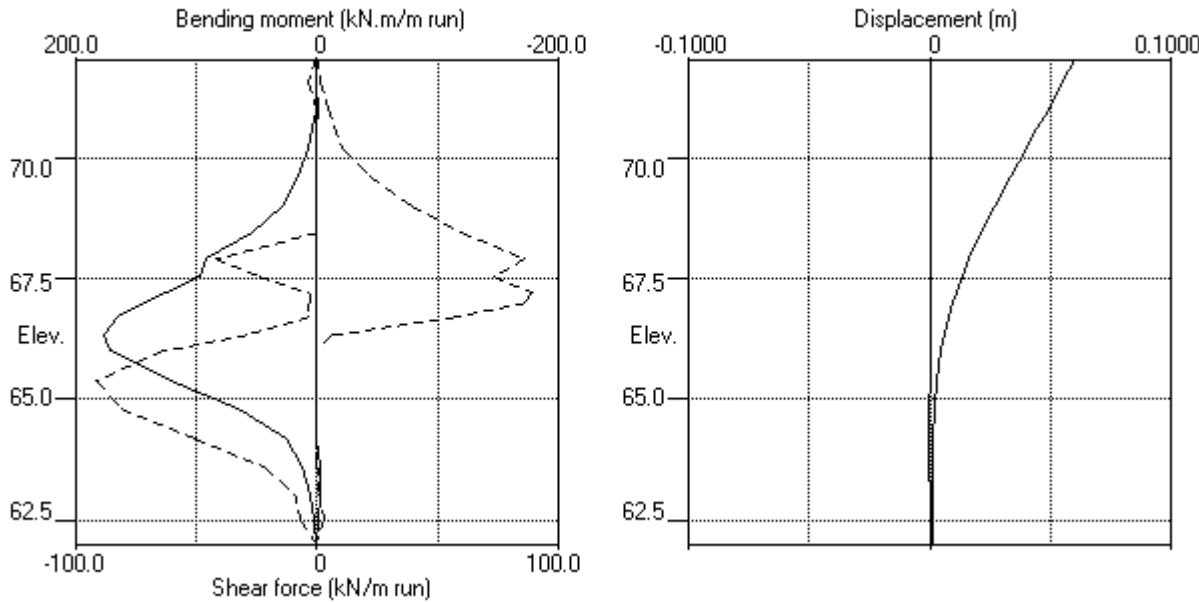
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Bending moment, shear force, displacement envelopes



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 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
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Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	72.00	1 Head deposits	1 Head deposits
2	71.00	3 LC UN	3 LC UN

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description (Datum elev.)	kN/m3	Eh, kN/m2 (dEh/dy)	Ko (dKo/dy)	NC/OC (Nu)	Ka (Kac)	Kp (Kpc)	kN/m2 (dc/dy)
1 Head deposits	20.00	9000	0.650	OC (0.200)	0.436 (0.000)	2.540 (0.000)	
2 LC DR ( 71.00 )	20.00	17600 ( 1952)	1.000	OC (0.200)	0.422 (1.489)	2.648 (4.248)	2.100d
3 LC UN ( 71.00 )	20.00	22000 ( 2440)	1.000	OC (0.490)	1.000 (2.389)	1.000 (2.390)	29.30u (3.300)

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---		
Soil friction angle	Wall adhesion coeff.	Backfill angle	Soil friction angle	Wall adhesion coeff.	Backfill angle
1 Head deposits	20.40	0.500	0.00	20.40	0.500
2 LC DR	21.20	0.500	0.00	21.20	0.500
3 LC UN	0.00	0.500	0.00	0.00	0.500

##### GROUND WATER CONDITIONS

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	66.20	66.20

Automatic water pressure balancing at toe of wall : No

Water press. -----	Active side				Passive side			
profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	71.00	71.00	0.0	1	67.20	67.20	0.0
					2	67.20	71.00	38.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 62.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

##### STRUTS and ANCHORS

Strut/ anchor no.	X-section	Inclin	Pre-
	Strut area	Youngs modulus	-ation
	Strut spacing	modulus kN/m2	length (degs)
1	1.00	0.400000	20.00 0.00 0
2	1.00	0.400000	20.00 0.00 0

**SURCHARGE LOADS**

Surcharge no.	Elev.	Distance from wall	Length parallel to wall	Width perpendicular to wall	Surcharge		Equiv. soil type	Partial factor/Category
					(kN/m <sup>2</sup> )	(Near edge)		
1	72.00	0.50 (A)	20.00	20.00	10.00	=	N/A	N/A
2	67.20	-0.00 (P)	20.00	20.00	38.00	=	N/A	N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m <sup>2</sup> /m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 72.00 No analysis at this stage
3	Excavate to elevation 66.70 on PASSIVE side
4	Fill to elevation 67.20 on PASSIVE side with soil type 3
5	Install strut or anchor no.1 at elevation 67.90
6	Apply surcharge no.2 at elevation 67.20
7	Install strut or anchor no.2 at elevation 71.50
8	Apply water pressure profile no.1 No analysis at this stage
9	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
10	Change EI of wall to 31986 kN.m <sup>2</sup> /m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 5.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 72.00	No	No	No			
3	Excav. to elev. 66.70 on PASSIVE side	Yes	Yes	Yes			
4	Fill to elev. 67.20 on PASSIVE side	No	No	No			
5	Install strut no.1 at elev. 67.90	No	No	No			
6	Apply surcharge no.2 at elev. 67.20	No	No	No			
7	Install strut no.2 at elev. 71.50	No	No	No			
8	Apply water pressure profile no.1	No	No	No			
9	Change soil type 3 to soil type 2	No	No	No			
10	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
*	Summary output	Yes	-	Yes			

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Units: kN,m

Stage No. 10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

			FoS for toe elev. = 62.00	Toe elev. for FoS = 1.000		
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment	Toe elev.	Wall Penetr
	No.	Act.	Pass.	Elev.	Safety at elev.	-ation
10		72.00	67.20		More than one strut	

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	72.00	0.00	0.116	1.89E-02	0.0	0.0		31986
2	71.50	5.16	0.106	1.89E-02	1.3	0.2	2.1	31986
		5.16	0.106	1.89E-02	-0.8	0.2		
3	71.00	10.69	0.097	1.89E-02	3.1	0.9		31986
		7.22	0.097	1.89E-02	3.1	0.9		
4	70.60	13.45	0.089	1.89E-02	7.2	3.0		31986
5	70.20	19.49	0.082	1.89E-02	13.8	7.1		31986
6	69.60	28.34	0.070	1.86E-02	28.2	18.5		31986
7	69.00	37.06	0.059	1.80E-02	47.8	39.0		31986
8	68.45	46.23	0.050	1.70E-02	70.7	68.4		31986
9	67.90	55.26	0.041	1.54E-02	98.6	110.7	144.5	31986
		55.26	0.041	1.54E-02	-45.9	110.7		
10	67.55	59.31	0.035	1.41E-02	-25.9	106.2		31986
11	67.20	62.88	0.031	1.30E-02	-4.5	108.4		31986
		15.95	0.031	1.30E-02	-4.5	108.4		
12	66.70	4.84	0.024	1.14E-02	0.7	118.3		31986
13	66.20	-6.27	0.019	9.86E-03	0.4	127.2		31986
14	65.80	-15.13	0.015	8.59E-03	-3.9	129.7		31986
15	65.40	-23.96	0.012	7.35E-03	-11.7	126.7		31986
16	64.80	-31.72	0.008	5.58E-03	-28.5	115.7		31986
17	64.20	-7.47	0.006	4.03E-03	-40.2	88.6		31986
18	63.60	4.72	0.003	2.92E-03	-41.0	52.9		31986
19	63.00	15.95	0.002	2.28E-03	-34.8	24.1		31986
20	62.50	35.30	0.001	2.06E-03	-22.0	6.9		31986
21	62.00	52.82	-0.000	2.01E-03	0.0	-0.0		---

At elev. 71.50 Strut force = 2.1 kN/strut = 2.1 kN/m run

At elev. 67.90 Strut force = 144.5 kN/strut = 144.5 kN/m run

(continued)

Stage No.10 Change EI of wall to 31986 kN.m2/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total earth pressure	Soil stiffness
		Water press.	Vertic -al	Active limit	Passive limit	Earth pressure	kN/m <sup>2</sup>		
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	23725
2	71.50	0.00	11.82	5.16	30.01	5.16	5.16a	2143	
3	71.00	0.00	24.50	10.69	62.22	10.69	10.69a	2143	
		0.00	24.50	7.22	73.79	7.22	7.22a	4191	
4	70.60	4.00	29.79	9.45	87.79	9.45	13.45a	4377	
5	70.20	8.00	34.61	11.49	100.56	11.49	19.49a	4563	
6	69.60	14.00	41.37	14.34	118.45	14.34	28.34a	4842	
7	69.00	20.00	47.81	17.06	135.52	17.06	37.06a	5121	
8	68.45	25.50	53.56	19.49	150.75	20.73	46.23	5377	
9	67.90	31.00	59.22	21.88	165.71	24.26	55.26	5633	
10	67.55	34.50	62.78	23.38	175.14	24.81	59.31	5795	
11	67.20	38.00	66.31	24.88	184.50	24.88	62.88a	5958	
12	66.70	43.00	71.33	26.99	197.78	26.99	69.99a	6190	
13	66.20	48.00	76.31	29.10	210.98	29.10	77.10a	6423	
14	65.80	52.00	80.28	30.77	221.48	30.77	82.77a	6609	
15	65.40	56.00	84.23	32.44	231.94	32.44	88.44a	6795	
16	64.80	62.00	90.13	34.94	247.58	40.34	102.34	7074	
17	64.20	68.00	96.01	37.42	263.15	80.13	148.13	7353	
18	63.60	74.00	101.88	39.90	278.67	107.72	181.72	7631	
19	63.00	80.00	107.73	42.36	294.15	127.61	207.61	7910	
20	62.50	85.00	112.59	44.42	307.04	141.43	226.43	8143	
21	62.00	90.00	117.45	46.47	319.90	154.75	244.75	8375	

Node no.	Y coord	PASSIVE side						Total earth pressure	Soil stiffness
		Water press.	Vertic -al	Active limit	Passive limit	Earth pressure	kN/m <sup>2</sup>		
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	71.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	70.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	70.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	69.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	69.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	68.45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	67.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	67.55	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
11	67.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
	38.00	-0.00	0.00	8.92	8.92	46.92p	5958		
12	66.70	43.00	5.00	0.00	22.15	22.15	65.15p	6190	
13	66.20	48.00	9.99	1.09	35.37	35.37	83.37p	6423	
14	65.80	52.00	13.97	2.77	45.90	45.90	97.90p	6609	
15	65.40	56.00	17.93	4.45	56.40	56.40	112.40p	6795	
16	64.80	62.00	23.85	6.94	72.06	72.06	134.06p	7074	
17	64.20	68.00	29.71	9.42	87.60	87.60	155.60p	7353	
18	63.60	74.00	35.53	11.88	103.01	103.01	177.01p	7631	
19	63.00	80.00	41.31	14.32	118.29	111.66	191.66	7910	
20	62.50	85.00	46.08	16.33	130.94	106.13	191.13	8143	
21	62.00	90.00	50.84	18.34	143.52	101.93	191.93	8375	

Run ID. Section 2 ULS  
Hampstead Green  
Contig wall

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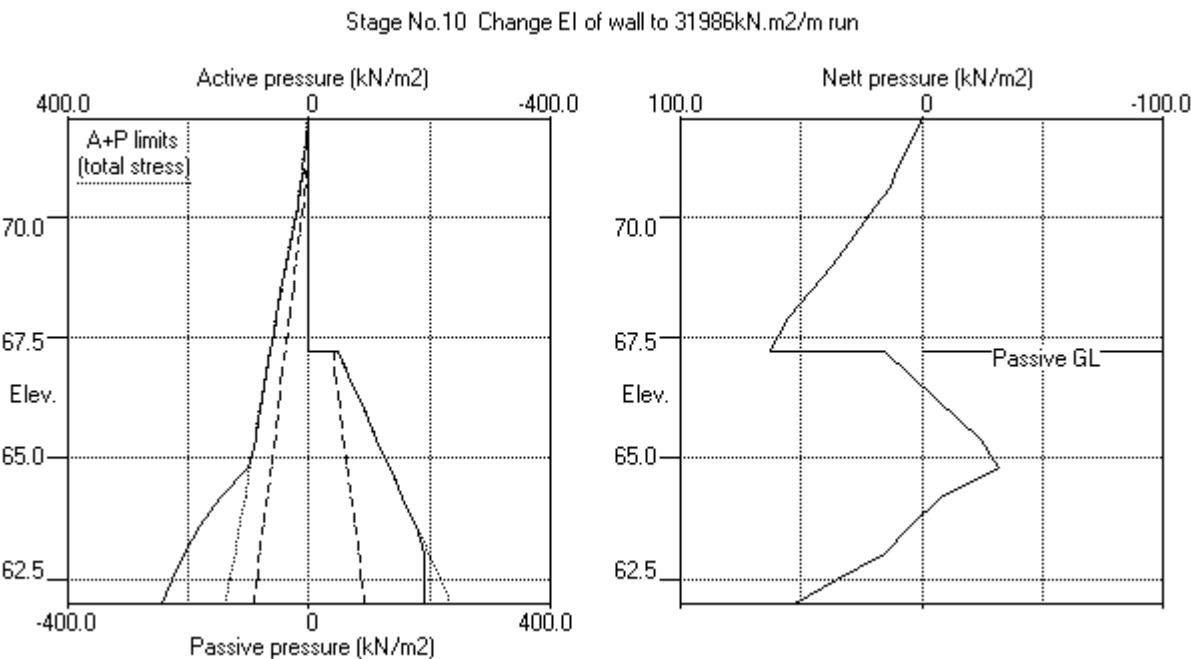
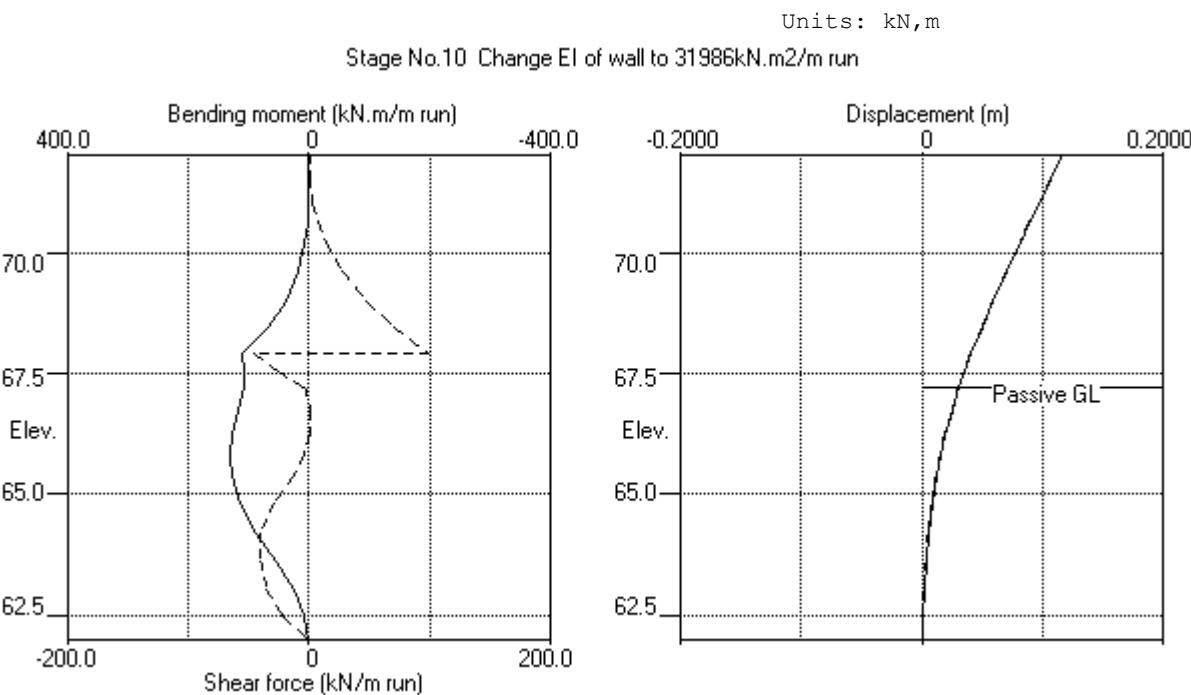
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(continued)

Stage No.10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
From elevation 72.00 to 62.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Note: 88.44a Soil pressure at active limit  
177.01p Soil pressure at passive limit

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 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

#### **Summary of results**

#### **STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000	
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.
1	72.00	72.00	Cant.	Conditions not suitable for FoS calc.		
2	72.00	72.00		No analysis at this stage		
3	72.00	66.70	Cant.	1.224	62.81	62.84 3.86
4	72.00	67.20	Cant.	1.463	62.69	63.79 3.41
5	72.00	67.20		No analysis at this stage		
6	72.00	67.20	67.90	Conditions not suitable for FoS calc.		
7	72.00	67.20		No analysis at this stage		

All remaining stages have more than one strut - FoS calculation n/a

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Units: kN,m

### Summary of results

#### BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall

##### Analysis options

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### Bending moment, shear force and displacement envelopes

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	72.00	0.116	0.000	0.0	-0.0	0.0	0.0
2	71.50	0.106	0.000	0.2	0.0	1.3	-0.8
3	71.00	0.097	0.000	1.7	-0.0	5.3	0.0
4	70.60	0.089	-0.000	4.3	-0.0	7.7	0.0
5	70.20	0.082	-0.000	8.0	-0.0	13.8	0.0
6	69.60	0.070	-0.000	18.5	-0.0	28.2	0.0
7	69.00	0.059	-0.000	39.0	0.0	47.8	0.0
8	68.45	0.050	-0.000	68.4	0.0	70.7	0.0
9	67.90	0.041	-0.000	110.7	0.0	98.6	-45.9
10	67.55	0.035	-0.000	106.2	0.0	75.9	-25.9
11	67.20	0.031	-0.000	130.3	0.0	92.6	-4.5
12	66.70	0.024	-0.000	178.8	0.0	101.8	0.0
13	66.20	0.019	0.000	217.8	0.0	55.1	0.0
14	65.80	0.015	0.000	231.6	0.0	17.3	-3.9
15	65.40	0.012	0.000	228.8	0.0	0.0	-28.2
16	64.80	0.008	0.000	198.3	0.0	0.0	-82.7
17	64.20	0.006	0.000	142.6	0.0	0.0	-104.8
18	63.60	0.003	-0.000	79.4	-0.0	0.0	-92.5
19	63.00	0.002	-0.001	31.6	-0.0	0.0	-62.0
20	62.50	0.001	-0.001	8.0	-0.0	0.0	-31.6
21	62.00	0.001	-0.001	0.0	-0.0	0.0	0.0

#### Maximum and minimum bending moment and shear force at each stage

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. kn. m/m	minimum kN.m/m	elev. kn. m/m	maximum kN/m	elev. kn. m/m	minimum kN/m	elev. kn. m/m
1	0.0	65.40	-0.0	63.00	0.0	72.00	0.0	72.00
2	No calculation at this stage							
3	219.2	65.80	0.0	72.00	96.3	66.70	-100.4	64.20
4	221.8	65.80	0.0	72.00	98.1	66.70	-101.3	64.20
5	No calculation at this stage							
6	231.6	65.80	-0.0	62.00	101.8	66.70	-104.8	64.20
7	No calculation at this stage							
8	No calculation at this stage							
9	No calculation at this stage							
10	129.7	65.80	-0.0	62.00	98.6	67.90	-45.9	67.90

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
1	0.000	62.00	-0.000	67.55	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 72.00
3	0.114	72.00	0.000	72.00	Excav. to elev. 66.70 on PASSIVE side
4	0.114	72.00	0.000	72.00	Fill to elev. 67.20 on PASSIVE side
5	No calculation at this stage				Install strut no.1 at elev. 67.90
6	0.116	72.00	-0.001	62.50	Apply surcharge no.2 at elev. 67.20
7	No calculation at this stage				Install strut no.2 at elev. 71.50
8	No calculation at this stage				Apply water pressure profile no.1
9	No calculation at this stage				Change soil type 3 to soil type 2
10	0.116	72.00	-0.000	62.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 at elev. 67.90	kN/m run	Strut no. 2 at elev. 71.50	kN/m run	Strut no. 2 at elev. 71.50	kN/m run
6	slack	slack	---	---	---	---
10	144.55	144.55		2.14	2.14	

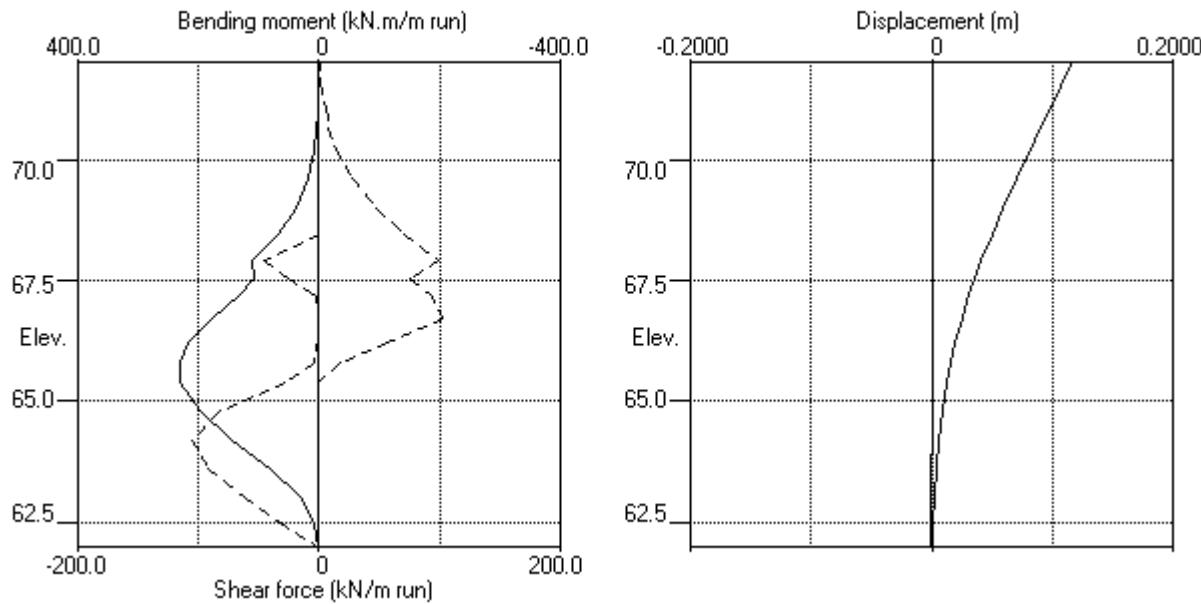
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Bending moment, shear force, displacement envelopes



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Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types			
		Active side		Passive side	
1	72.00	1 Head deposits		1 Head deposits	
2	71.00	3 LC UN		3 LC UN	
3	67.60	3 LC UN		4 LC UN	
4	67.10	3 LC UN		3 LC UN	

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	18000	0.590	OC	0.376	3.077	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	35200	1.000	OC	0.361	3.253	2.500d
		( 3904)		(0.200)	(1.370)	( 4.831)	
3 LC UN ( 71.00 )	20.00	44000	1.000	OC	1.000	1.000	44.00u
		( 4880)		(0.490)	(2.389)	( 2.390)	( 4.900)
4 LC UN ( 71.00 )	20.00	44000	1.000	OC	1.000	1.000	44.00u
		( 4880)		(0.490)	(2.389)	( 2.390)	( 4.900)
5 LC soft ( 67.60 )	20.00	1	1.000	OC	1.000	1.000	1.000u
		( 126064)		(0.490)	(2.389)	( 2.390)	( 126.0)

##### Additional soil parameters associated with Ka and Kp

----- Soil type -----	--- parameters for Ka ---			--- parameters for Kp ---		
	Soil friction	Wall adhesion	Backfill	Soil friction	Wall adhesion	Backfill
No. Description	angle	coeff.	angle	angle	coeff.	angle
1 Head deposits	24.00	0.500	0.00	24.00	0.500	0.00
2 LC DR	25.00	0.500	0.00	25.00	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
5 LC soft	0.00	0.500	0.00	0.00	0.500	0.00

##### GROUND WATER CONDITIONS

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	67.40	67.40

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side				
	profile no.	Point no.	Elev. m	Piezoelev. m	Water press. kN/m2	Point no.	Elev. m	Piezoelev. m	Water press. kN/m2
1	1	71.00	71.00	71.00	0.0	1	67.60	67.60	0.0
						2	67.60	71.00	34.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 62.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	67.90	1.00	0.400000	1.500E+07	20.00	0.00	0 No
2	71.50	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**SURCHARGE LOADS**

Surcharge no.	Elev. m	Distance from wall 0.50(A) -0.00(P)	Length parallel to wall 20.00	Width perpend. to wall 20.00	Surcharge kN/m2 Near edge 10.00	Equiv. soil type =	Partial factor/ Category
1	72.00	0.50(A)	20.00	20.00	10.00	=	N/A N/A
2	67.60	-0.00(P)	20.00	20.00	34.00	=	N/A N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m2/m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 72.00 No analysis at this stage
3	Excavate to elevation 67.60 on PASSIVE side
4	Change properties of soil type 4 to soil type 5 Ko pressures will not be reset
5	Install strut or anchor no.1 at elevation 67.90
6	Apply surcharge no.2 at elevation 67.60
7	Install strut or anchor no.2 at elevation 71.50
8	Apply water pressure profile no.1 No analysis at this stage
9	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
10	Change properties of soil type 5 to soil type 2 No analysis at this stage Ko pressures will not be reset
11	Change EI of wall to 31986 kN.m2/m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 5.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force	pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No				
2	Apply surcharge no.1 at elev. 72.00	No	No	No				
3	Excav. to elev. 67.60 on PASSIVE side	Yes	Yes	Yes				
4	Change soil type 4 to soil type 5	No	No	No				
5	Install strut no.1 at elev. 67.90	No	No	No				
6	Apply surcharge no.2 at elev. 67.60	No	No	No				
7	Install strut no.2 at elev. 71.50	No	No	No				
8	Apply water pressure profile no.1	No	No	No				
9	Change soil type 3 to soil type 2	No	No	No				
10	Change soil type 5 to soil type 2	No	No	No				
11	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No				
*	Summary output	Yes	-	Yes				

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Units: kN,m

Stage No. 11 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

			FoS for toe elev. = 62.00	Toe elev. for FoS = 1.000		
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment	Toe elev.	Wall Penetr
No.	Act.	Pass.	Elev.	Safety at elev.	-ation	
11	72.00	67.60		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	72.00	0.00	0.041	7.99E-03	0.0	-0.0		31986
2	71.50	4.45	0.037	7.99E-03	1.1	0.2	8.2	31986
		4.45	0.037	7.99E-03	-7.0	0.2		
3	71.00	9.22	0.033	8.01E-03	-3.6	-1.7		31986
		5.42	0.033	8.01E-03	-3.6	-1.7		
4	70.60	11.33	0.030	8.04E-03	-0.3	-1.8		31986
5	70.20	17.07	0.027	8.08E-03	5.4	-0.3		31986
6	69.60	25.51	0.022	8.06E-03	18.2	6.7		31986
7	69.00	33.84	0.017	7.83E-03	36.0	22.0		31986
8	68.45	41.87	0.013	7.27E-03	56.8	46.1		31986
9	67.90	52.18	0.009	6.15E-03	82.7	81.9	112.5	31986
		52.18	0.009	6.15E-03	-29.8	81.9		
10	67.60	56.54	0.008	5.40E-03	-13.5	81.4		31986
		10.47	0.008	5.40E-03	-13.5	81.4		
11	67.40	4.54	0.007	4.92E-03	-12.0	82.6		31986
12	67.10	-6.71	0.005	4.24E-03	-12.3	83.7		31986
13	66.55	-23.32	0.003	3.00E-03	-20.6	88.1		31986
14	66.00	-1.83	0.002	1.91E-03	-27.5	66.0		31986
15	65.40	5.38	0.001	1.08E-03	-26.4	40.1		31986
16	64.80	12.59	0.001	5.70E-04	-21.0	21.1		31986
17	64.20	13.88	0.000	2.91E-04	-13.1	8.6		31986
18	63.60	8.85	0.000	1.59E-04	-6.3	2.7		31986
19	63.00	3.17	0.000	9.72E-05	-2.7	0.9		31986
20	62.50	-1.37	0.000	7.00E-05	-2.2	0.6		31986
21	62.00	10.23	0.000	6.00E-05	0.0	-0.0		---

At elev. 71.50 Strut force = 8.2 kN/strut = 8.2 kN/m run

At elev. 67.90 Strut force = 112.5 kN/strut = 112.5 kN/m run

(continued)

Stage No.11 Change EI of wall to 31986 kN.m2/m run  
From elevation 72.00 to 62.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total earth pressure	Soil stiffness coeff.
		Water press.	Vertic al	Active limit	Passive limit	Earth pressure			
								kN/m2	kN/m3
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	30298
2	71.50	0.00	11.82	4.45	36.36	4.45	4.45a	4.45a	4566
3	71.00	0.00	24.50	9.22	75.38	9.22	9.22a	9.22a	4566
		0.00	24.50	5.42	91.76	5.42	5.42a	5.42a	8929
4	70.60	4.00	29.79	7.33	108.97	7.33	11.33a	9325	
5	70.20	8.00	34.61	9.07	124.65	9.07	17.07a	9722	
6	69.60	14.00	41.37	11.51	146.63	11.51	25.51a	10316	
7	69.00	20.00	47.81	13.84	167.60	13.84	33.84a	10910	
8	68.45	25.50	53.56	15.91	186.31	16.37	41.87	11455	
9	67.90	31.00	59.22	17.95	204.70	21.18	52.18	11999	
10	67.60	34.00	62.27	19.06	214.63	22.54	56.54	12296	
11	67.40	36.00	64.29	19.79	221.21	23.11	59.11	12495	
12	67.10	39.00	67.32	20.88	231.05	21.62	60.62	12792	
13	66.55	44.50	72.83	22.87	248.97	22.87	67.37a	13336	
14	66.00	50.00	78.30	24.84	266.76	62.16	112.16	13881	
15	65.40	56.00	84.23	26.98	286.06	88.68	144.68	14475	
16	64.80	62.00	90.13	29.12	305.26	103.87	165.87	15069	
17	64.20	68.00	96.01	31.24	324.39	111.96	179.96	15664	
18	63.60	74.00	101.88	33.35	343.46	117.12	191.12	16258	
19	63.00	80.00	107.73	35.47	362.48	121.56	201.56	16852	
20	62.50	85.00	112.59	37.22	378.31	125.07	210.07	51374	
21	62.00	90.00	117.45	38.98	394.12	136.61	226.61	108298	

Node no.	Y coord	PASSIVE side						Total earth pressure	Soil stiffness coeff.
		Water press.	Vertic al	Active limit	Passive limit	Earth pressure			
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m3		
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
2	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
3	71.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
4	70.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
5	70.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
6	69.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
7	69.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
8	68.45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
9	67.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
10	67.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0
		34.00	-0.00	0.00	12.08	12.08	46.08p	13256	
11	67.40	36.00	2.00	0.00	18.58	18.58	54.58p	13470	
12	67.10	39.00	5.00	0.00	28.33	28.33	67.33p	13790	
13	66.55	44.50	10.49	0.36	46.19	46.19	90.69p	14378	
14	66.00	50.00	15.96	2.34	63.98	63.98	113.98p	14965	
15	65.40	56.00	21.89	4.48	83.29	83.29	139.29p	15605	
16	64.80	62.00	27.79	6.61	102.48	91.28	153.28	16246	
17	64.20	68.00	33.65	8.72	121.52	98.08	166.08	16887	
18	63.60	74.00	39.46	10.82	140.43	108.28	182.28	17527	
19	63.00	80.00	45.23	12.90	159.21	118.39	198.39	18168	
20	62.50	85.00	50.02	14.63	174.78	126.44	211.44	51374	
21	62.00	90.00	54.79	16.35	190.29	126.38	216.38	108298	

Run ID. Section 3 SLS  
Hampstead Green  
Contig wall

| Sheet No.  
| Date:25-04-2016  
| Checked :

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(continued)

Stage No.11 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
From elevation 72.00 to 62.00  
Yield moment not defined  
Allow wall to relax with new modulus value

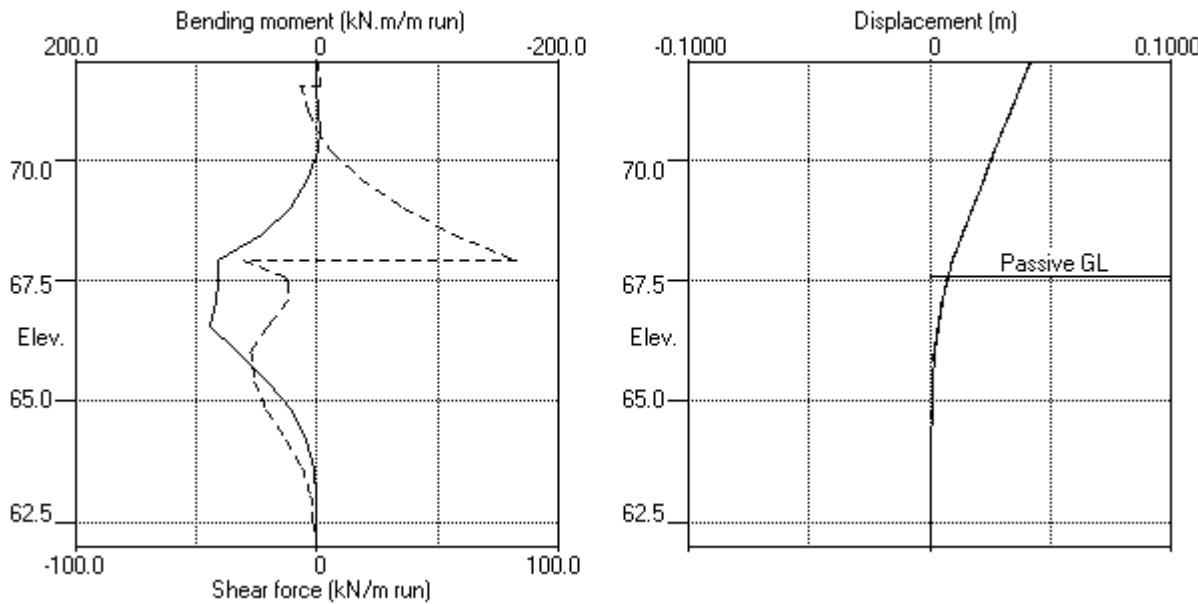
Note: 67.37a Soil pressure at active limit  
139.29p Soil pressure at passive limit

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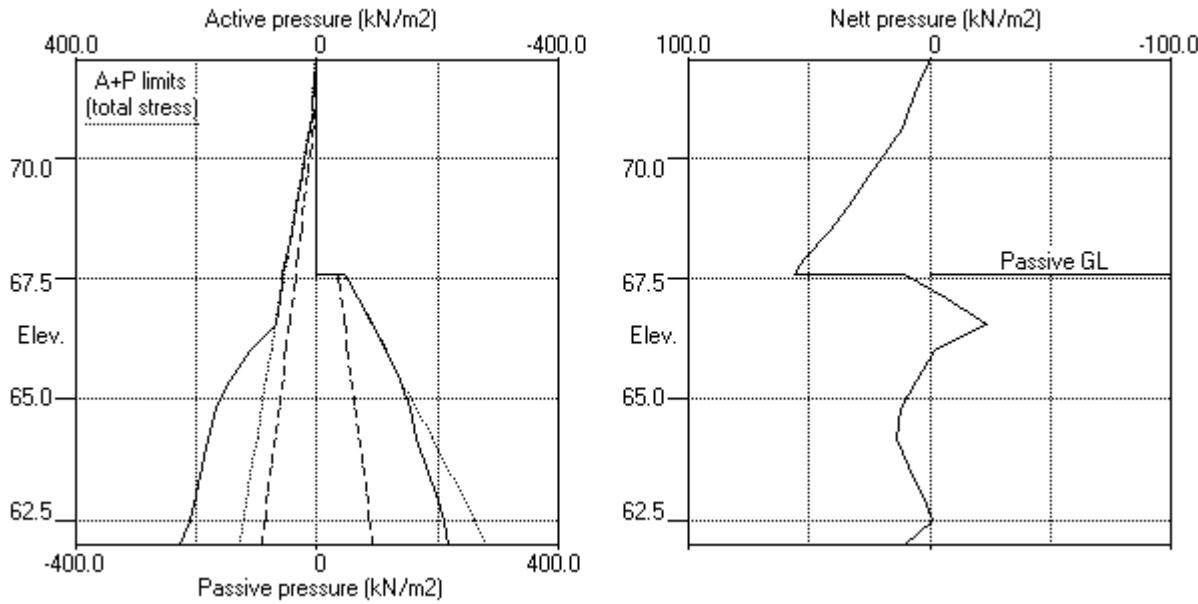
Sheet No.  
Job No. 16-0036  
Made by : KK  
Date: 25-04-2016  
Checked :

Units: kN,m

Stage No.11 Change EI of wall to 31986kN.m<sup>2</sup>/m run



Stage No.11 Change EI of wall to 31986kN.m<sup>2</sup>/m run



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 Contig wall | Checked :  
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Units: kN,m

#### **Summary of results**

#### **STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000		Wall Penetr -ation
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.	
1	72.00	72.00	Cant.	Conditions not suitable for FoS calc.			
2	72.00	72.00		No analysis at this stage			
3	72.00	67.60	Cant.	2.487	62.59	65.22	2.38
4	72.00	67.60	Cant.	2.388	62.63	64.83	2.77
5	72.00	67.60		No analysis at this stage			
6	72.00	67.60	67.90	Conditions not suitable for FoS calc.			
7	72.00	67.60		No analysis at this stage			

All remaining stages have more than one strut - FoS calculation n/a

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	Job No. 16-0036
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	Date: 25-04-2016
	Checked :

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Units: kN,m

### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	72.00	0.042	0.000	0.0	-0.0	0.0	0.0
2	71.50	0.037	0.000	0.2	-0.0	1.1	-7.0
3	71.00	0.033	0.000	1.5	-1.7	4.5	-3.6
4	70.60	0.030	0.000	3.8	-1.8	6.9	-0.3
5	70.20	0.027	0.000	7.1	-0.3	10.1	0.0
6	69.60	0.022	0.000	15.1	-0.0	18.2	0.0
7	69.00	0.017	-0.000	28.2	-0.0	36.0	0.0
8	68.45	0.013	-0.000	47.2	-0.0	56.8	0.0
9	67.90	0.009	-0.000	81.9	-0.0	82.7	-29.8
10	67.60	0.008	-0.000	95.6	-0.0	73.9	-13.5
11	67.40	0.007	-0.000	110.2	-0.0	70.0	-12.0
12	67.10	0.005	-0.000	127.6	0.0	43.1	-12.3
13	66.55	0.003	-0.000	142.6	0.0	0.0	-44.3
14	66.00	0.002	-0.000	106.8	0.0	0.0	-71.3
15	65.40	0.001	-0.000	59.9	0.0	0.0	-68.5
16	64.80	0.001	-0.000	24.6	0.0	0.0	-46.0
17	64.20	0.001	-0.000	8.6	-0.6	0.0	-23.1
18	63.60	0.001	-0.000	2.7	-3.9	0.0	-6.8
19	63.00	0.001	0.000	0.9	-3.5	2.8	-2.7
20	62.50	0.001	0.000	0.6	-1.6	3.5	-2.2
21	62.00	0.001	0.000	0.0	-0.0	0.0	0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. kn.20	minimum kN.m/m	elev. -0.0	maximum kN/m	elev. 72.00	minimum kN/m	elev. 0.0
1	0.0	64.20	-0.0	63.00	0.0	72.00	0.0	72.00
2	No calculation at this stage							
3	108.7	67.10	-3.9	63.60	65.0	67.60	-60.8	66.00
4	136.0	66.55	-3.4	63.00	65.1	67.40	-68.3	66.00
5	No calculation at this stage							
6	142.6	66.55	-3.5	63.00	73.9	67.60	-71.3	66.00
7	No calculation at this stage							
8	No calculation at this stage							
9	No calculation at this stage							
10	No calculation at this stage							
11	88.1	66.55	-1.8	70.60	82.7	67.90	-29.8	67.90

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
	m		m		
1	0.000	62.00	-0.000	66.55	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 72.00
3	0.033	72.00	0.000	72.00	Excav. to elev. 67.60 on PASSIVE side
4	0.041	72.00	0.000	72.00	Change soil type 4 to soil type 5
5	No calculation at this stage				Install strut no.1 at elev. 67.90
6	0.042	72.00	-0.000	64.80	Apply surcharge no.2 at elev. 67.60
7	No calculation at this stage				Install strut no.2 at elev. 71.50
8	No calculation at this stage				Apply water pressure profile no.1
9	No calculation at this stage				Change soil type 3 to soil type 2
10	No calculation at this stage				Change soil type 5 to soil type 2
11	0.041	72.00	0.000	72.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	--- Strut no. 1 ---	at elev. 67.90	kN/m run	--- Strut no. 2 ---	at elev. 71.50	kN/m run
6	slack	slack		---	---	
11	112.47	112.47		8.15	8.15	

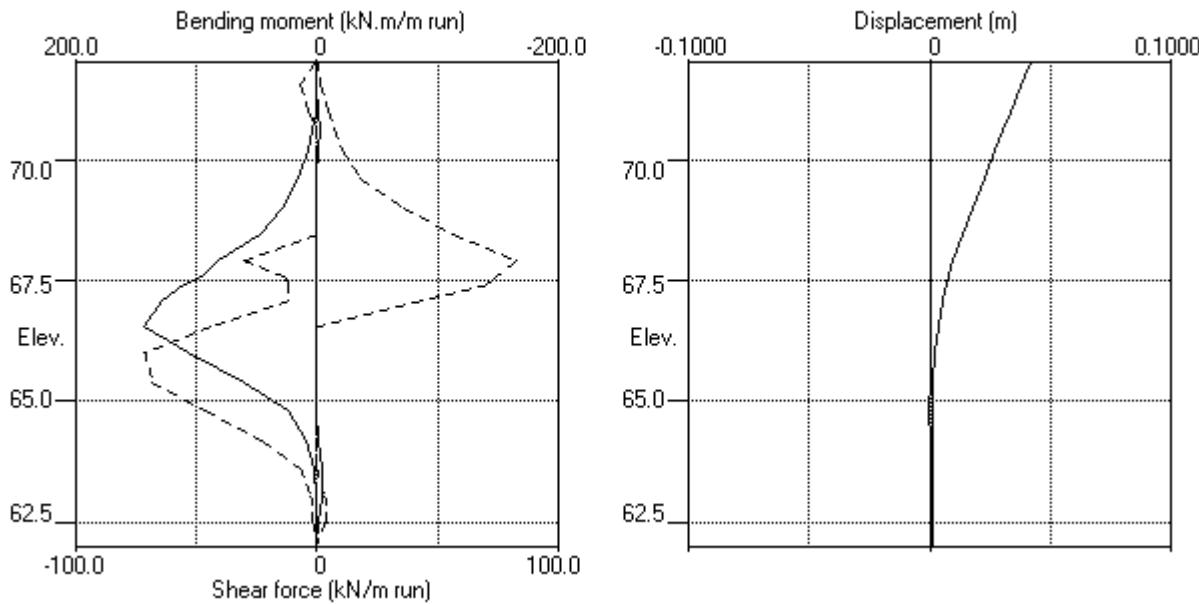
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Bending moment, shear force, displacement envelopes



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Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	72.00	1 Head deposits	1 Head deposits
2	71.00	3 LC UN	3 LC UN

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	9000	0.650	OC	0.436	2.540	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	17600	1.000	OC	0.422	2.648	2.100d
		( 1952 )		(0.200)	(1.489)	( 4.248 )	
3 LC UN ( 71.00 )	20.00	22000	1.000	OC	1.000	1.000	29.30u
		( 2440 )		(0.490)	(2.389)	( 2.390 )	( 3.300 )

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---		
Soil friction angle	Wall adhesion coeff.	Backfill angle	Soil friction angle	Wall adhesion coeff.	Backfill angle
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.
No. Description					
1 Head deposits	20.40	0.500	0.00	20.40	0.500
2 LC DR	21.20	0.500	0.00	21.20	0.500
3 LC UN	0.00	0.500	0.00	0.00	0.500

##### GROUND WATER CONDITIONS

Density of water	= 10.00 kN/m3	Active side	Passive side
Initial water table elevation		67.00	67.00

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side			
profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	71.00	71.00	0.0	1	67.60	67.60	0.0
					2	67.60	71.00	34.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 62.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

##### STRUTS and ANCHORS

Strut/ anchor no.	X-section	Inclin	Pre-
	Strut area	Youngs modulus	-ation stress /strut
	Strut spacing	Youngs modulus	Tension allowed
	m	sq.m	kN
1	67.90	1.00	0.400000 1.500E+07 20.00 0.00 0 No
2	71.50	1.00	0.400000 1.500E+07 20.00 0.00 0 No

**SURCHARGE LOADS**

Surcharge no.	Elev.	Distance from wall	Length parallel to wall	Width perpendicular to wall	Surcharge		Equiv. soil type	Partial factor/Category
					(kN/m <sup>2</sup> )	(Near edge = Far edge)		
1	72.00	0.50 (A)	20.00	20.00	10.00	=	N/A	N/A
2	67.60	-0.00 (P)	20.00	20.00	34.00	=	N/A	N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m <sup>2</sup> /m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 72.00 No analysis at this stage
3	Excavate to elevation 67.20 on PASSIVE side
4	Fill to elevation 67.60 on PASSIVE side with soil type 3
5	Install strut or anchor no.1 at elevation 67.90
6	Apply surcharge no.2 at elevation 67.60
7	Install strut or anchor no.2 at elevation 71.50
8	Apply water pressure profile no.1 No analysis at this stage
9	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
10	Change EI of wall to 31986 kN.m <sup>2</sup> /m run From elevation 72.00 to 62.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 5.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force	pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No				
2	Apply surcharge no.1 at elev. 72.00	No	No	No				
3	Excav. to elev. 67.20 on PASSIVE side	Yes	Yes	Yes				
4	Fill to elev. 67.60 on PASSIVE side	No	No	No				
5	Install strut no.1 at elev. 67.90	No	No	No				
6	Apply surcharge no.2 at elev. 67.60	No	No	No				
7	Install strut no.2 at elev. 71.50	No	No	No				
8	Apply water pressure profile no.1	No	No	No				
9	Change soil type 3 to soil type 2	No	No	No				
10	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No				
*	Summary output	Yes	-	Yes				

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 Contig wall | Checked :  
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Units: kN,m

Stage No. 10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

			FoS for toe elev. = 62.00	Toe elev. for FoS = 1.000	
			-----	-----	
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment Toe elev. Penetr	
Act.	No.	Pass.	Elev.	Safety at elev.	-ation
10	72.00	67.60		More than one strut	

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	72.00	0.00	0.075	1.30E-02	0.0	0.0		31986
2	71.50	5.16	0.068	1.30E-02	1.3	0.2	7.0	31986
		5.16	0.068	1.30E-02	-5.7	0.2		
3	71.00	10.69	0.062	1.30E-02	-1.8	-1.0		31986
		7.22	0.062	1.30E-02	-1.8	-1.0		
4	70.60	13.45	0.057	1.31E-02	2.4	-0.4		31986
5	70.20	19.49	0.051	1.31E-02	9.0	2.1		31986
6	69.60	28.34	0.043	1.30E-02	23.3	11.3		31986
7	69.00	37.06	0.036	1.26E-02	42.9	29.5		31986
8	68.45	46.01	0.029	1.19E-02	65.8	57.0		31986
9	67.90	56.14	0.023	1.05E-02	93.9	97.5	125.2	31986
		56.14	0.023	1.05E-02	-31.3	97.5		
10	67.60	60.69	0.020	9.58E-03	-13.8	96.9		31986
		17.77	0.020	9.58E-03	-13.8	96.9		
11	67.20	8.41	0.016	8.41E-03	-8.5	100.7		31986
12	67.00	3.56	0.015	7.84E-03	-7.3	102.9		31986
13	66.50	-10.17	0.011	6.47E-03	-9.0	104.8		31986
14	66.00	-21.24	0.008	5.16E-03	-16.8	103.7		31986
15	65.40	-10.41	0.005	3.69E-03	-26.3	92.3		31986
16	64.80	2.07	0.004	2.48E-03	-28.8	65.6		31986
17	64.20	5.19	0.002	1.65E-03	-26.7	41.1		31986
18	63.60	9.04	0.002	1.12E-03	-22.4	22.5		31986
19	63.00	13.26	0.001	8.46E-04	-15.7	9.0		31986
20	62.50	13.43	0.001	7.54E-04	-9.0	2.6		31986
21	62.00	22.67	0.000	7.31E-04	0.0	-0.0		---

At elev. 71.50 Strut force = 7.0 kN/strut = 7.0 kN/m run

At elev. 67.90 Strut force = 125.2 kN/strut = 125.2 kN/m run

(continued)

Stage No.10 Change EI of wall to 31986 kN.m2/m run  
 From elevation 72.00 to 62.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total earth pressure	Soil stiffness coeff.		
		Effective stresses									
		Water press.	Vertic -al	Active limit	Passive limit	Earth pressure	kN/m2				
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2				
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	15027		
2	71.50	0.00	11.82	5.16	30.01	5.16	5.16a	2147			
3	71.00	0.00	24.50	10.69	62.22	10.69	10.69a	2147			
		0.00	24.50	7.22	73.79	7.22	7.22a	4199			
4	70.60	4.00	29.79	9.45	87.79	9.45	13.45a	4385			
5	70.20	8.00	34.61	11.49	100.56	11.49	19.49a	4572			
6	69.60	14.00	41.37	14.34	118.45	14.34	28.34a	4851			
7	69.00	20.00	47.81	17.06	135.52	17.06	37.06a	5131			
8	68.45	25.50	53.56	19.49	150.75	20.51	46.01	5387			
9	67.90	31.00	59.22	21.88	165.71	25.14	56.14	5643			
10	67.60	34.00	62.27	23.17	173.80	26.69	60.69	5783			
11	67.20	38.00	66.31	24.88	184.50	27.92	65.92	5969			
12	67.00	40.00	68.32	25.73	189.82	28.36	68.36	6062			
13	66.50	45.00	73.33	27.84	203.07	27.84	72.84a	6295			
14	66.00	50.00	78.30	29.94	216.23	29.94	79.94a	6528			
15	65.40	56.00	84.23	32.44	231.94	56.48	112.48	6807			
16	64.80	62.00	90.13	34.94	247.58	84.58	146.58	7087			
17	64.20	68.00	96.01	37.42	263.15	103.20	171.20	7366			
18	63.60	74.00	101.88	39.90	278.67	115.54	189.54	7645			
19	63.00	80.00	107.73	42.36	294.15	124.39	204.39	7925			
20	62.50	85.00	112.59	44.42	307.04	130.63	215.63	8158			
21	62.00	90.00	117.45	46.47	319.90	141.55	231.55	613005			

Node no.	Y coord	PASSIVE side						Total earth pressure	Soil stiffness coeff.		
		Effective stresses									
		Water press.	Vertic -al	Active limit	Passive limit	Earth pressure	kN/m2				
		kN/m2	kN/m2	kN/m2	kN/m2	kN/m2	kN/m2				
1	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
2	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
3	71.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
4	70.60	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
5	70.20	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
6	69.60	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
7	69.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
8	68.45	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
9	67.90	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
10	67.60	0.00	0.00	0.00	0.00	0.00	0.00	0.0			
		34.00	-0.00	0.00	8.92	8.92	42.92p	5783			
11	67.20	38.00	4.00	0.00	19.51	19.51	57.51p	5969			
12	67.00	40.00	6.00	0.00	24.80	24.80	64.80p	6062			
13	66.50	45.00	10.99	1.51	38.01	38.01	83.01p	6295			
14	66.00	50.00	15.96	3.61	51.17	51.17	101.17p	6528			
15	65.40	56.00	21.89	6.12	66.89	66.89	122.89p	6807			
16	64.80	62.00	27.79	8.61	82.51	82.51	144.51p	7087			
17	64.20	68.00	33.65	11.08	98.01	98.01	166.01p	7366			
18	63.60	74.00	39.46	13.54	113.40	106.50	180.50	7645			
19	63.00	80.00	45.23	15.97	128.69	111.13	191.13	7925			
20	62.50	85.00	50.02	18.00	141.36	117.20	202.20	8158			
21	62.00	90.00	54.79	20.01	153.98	118.88	208.88	613005			

Run ID. Section 3 ULS  
Hampstead Green  
Contig wall

| Sheet No.  
| Date:25-04-2016  
| Checked :

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(continued)

Stage No.10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
From elevation 72.00 to 62.00  
Yield moment not defined  
Allow wall to relax with new modulus value

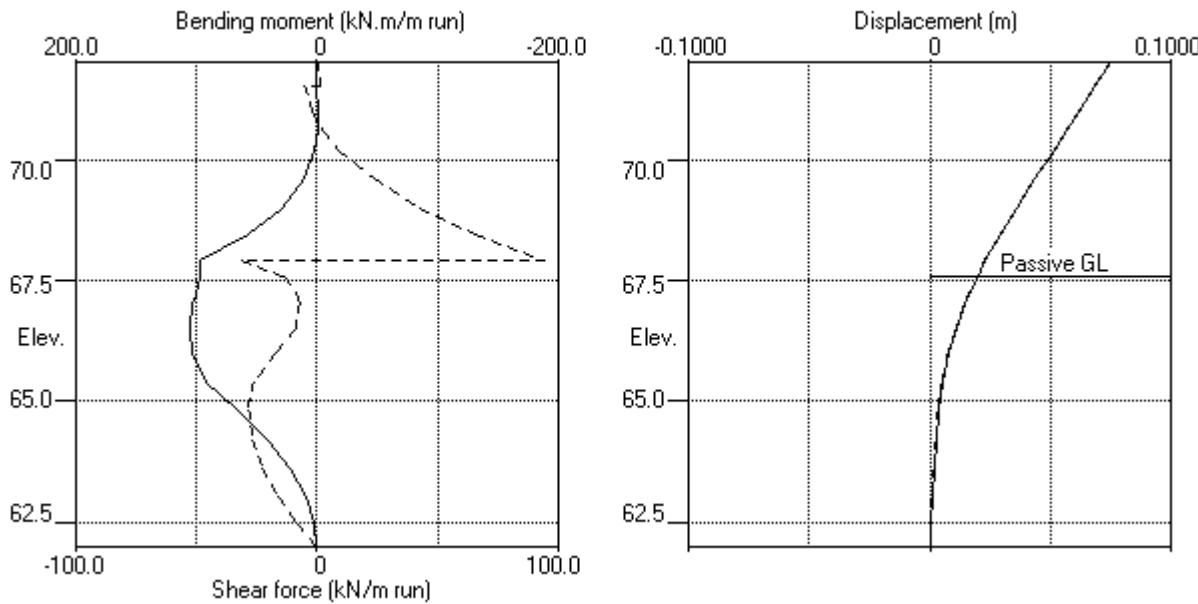
Note: 79.94a Soil pressure at active limit  
166.01p Soil pressure at passive limit

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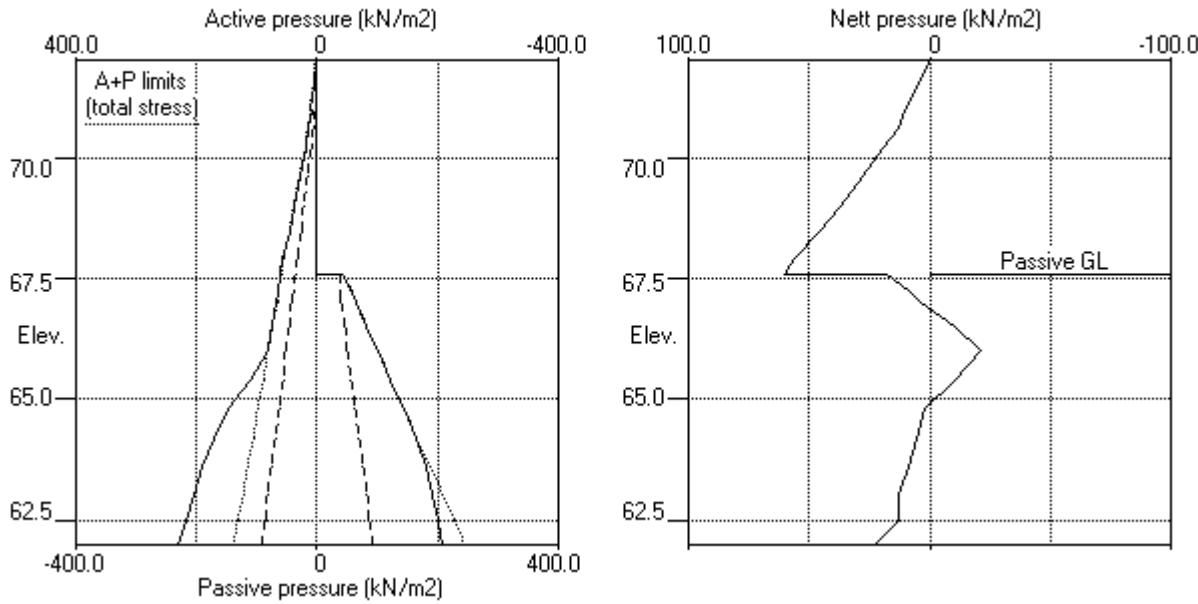
Sheet No.  
Job No. 16-0036  
Made by : KK  
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Checked :

Units: kN,m

Stage No.10 Change EI of wall to 31986kN.m<sup>2</sup>/m run



Stage No.10 Change EI of wall to 31986kN.m<sup>2</sup>/m run



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 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
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Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000		Wall Penetr -ation
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.	
1	72.00	72.00	Cant.	Conditions not suitable for FoS calc.			
2	72.00	72.00		No analysis at this stage			
3	72.00	67.20	Cant.	1.462	62.69	63.74	3.46
4	72.00	67.60	Cant.	1.670	62.58	64.50	3.10
5	72.00	67.60		No analysis at this stage			
6	72.00	67.60	67.90	Conditions not suitable for FoS calc.			
7	72.00	67.60		No analysis at this stage			

All remaining stages have more than one strut - FoS calculation n/a

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	Job No. 16-0036
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	Date: 25-04-2016
	Checked :

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Units: kN,m

### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	72.00	0.075	0.000	0.0	0.0	0.0	0.0
2	71.50	0.068	0.000	0.2	0.0	1.3	-5.7
3	71.00	0.062	0.000	1.7	-1.0	5.3	-1.8
4	70.60	0.057	-0.000	4.3	-0.4	7.7	0.0
5	70.20	0.051	-0.000	8.0	-0.0	10.9	0.0
6	69.60	0.043	-0.000	16.4	-0.0	23.3	0.0
7	69.00	0.036	-0.000	30.1	0.0	42.9	0.0
8	68.45	0.029	-0.000	57.0	0.0	65.8	0.0
9	67.90	0.023	-0.000	97.5	0.0	93.9	-31.3
10	67.60	0.020	-0.000	100.5	0.0	76.9	-13.8
11	67.20	0.016	-0.000	132.9	0.0	86.3	-8.5
12	67.00	0.015	-0.000	148.6	0.0	71.0	-7.3
13	66.50	0.011	-0.000	173.4	0.0	28.1	-9.0
14	66.00	0.008	0.000	178.2	0.0	0.0	-21.2
15	65.40	0.005	0.000	154.8	0.0	0.0	-64.9
16	64.80	0.004	0.000	106.7	0.0	0.0	-77.9
17	64.20	0.002	-0.000	61.4	0.0	0.0	-65.4
18	63.60	0.002	-0.000	28.2	-0.0	0.0	-43.7
19	63.00	0.001	-0.000	9.0	-0.0	0.0	-22.6
20	62.50	0.002	-0.000	2.6	-0.0	0.0	-9.0
21	62.00	0.002	0.000	0.0	-0.0	0.0	-0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. kn. m/m	minimum kN.m/m	elev. kn. m/m	maximum kN/m	elev. kn. m/m	minimum kN/m	elev. kn. m/m
1	0.0	65.40	-0.0	63.00	0.0	72.00	0.0	72.00
2	No calculation at this stage							
3	167.6	66.00	-0.0	62.00	80.2	67.20	-73.7	64.80
4	169.7	66.00	-0.0	62.00	81.8	67.20	-74.5	64.80
5	No calculation at this stage							
6	178.2	66.00	-0.0	62.00	86.3	67.20	-77.9	64.80
7	No calculation at this stage							
8	No calculation at this stage							
9	No calculation at this stage							
10	104.8	66.50	-1.0	71.00	93.9	67.90	-31.3	67.90

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
1	0.000	62.00	-0.000	67.60	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 72.00
3	0.074	72.00	0.000	72.00	Excav. to elev. 67.20 on PASSIVE side
4	0.074	72.00	0.000	72.00	Fill to elev. 67.60 on PASSIVE side
5	No calculation at this stage				Install strut no.1 at elev. 67.90
6	0.075	72.00	-0.000	63.60	Apply surcharge no.2 at elev. 67.60
7	No calculation at this stage				Install strut no.2 at elev. 71.50
8	No calculation at this stage				Apply water pressure profile no.1
9	No calculation at this stage				Change soil type 3 to soil type 2
10	0.075	72.00	0.000	72.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 at elev. 67.90	kN/m run	Strut no. 2 at elev. 71.50	kN/m run	Strut no. 2 at elev. 71.50	kN/m run
6	slack	slack	---	---	---	---
10	125.15	125.15		7.01	7.01	

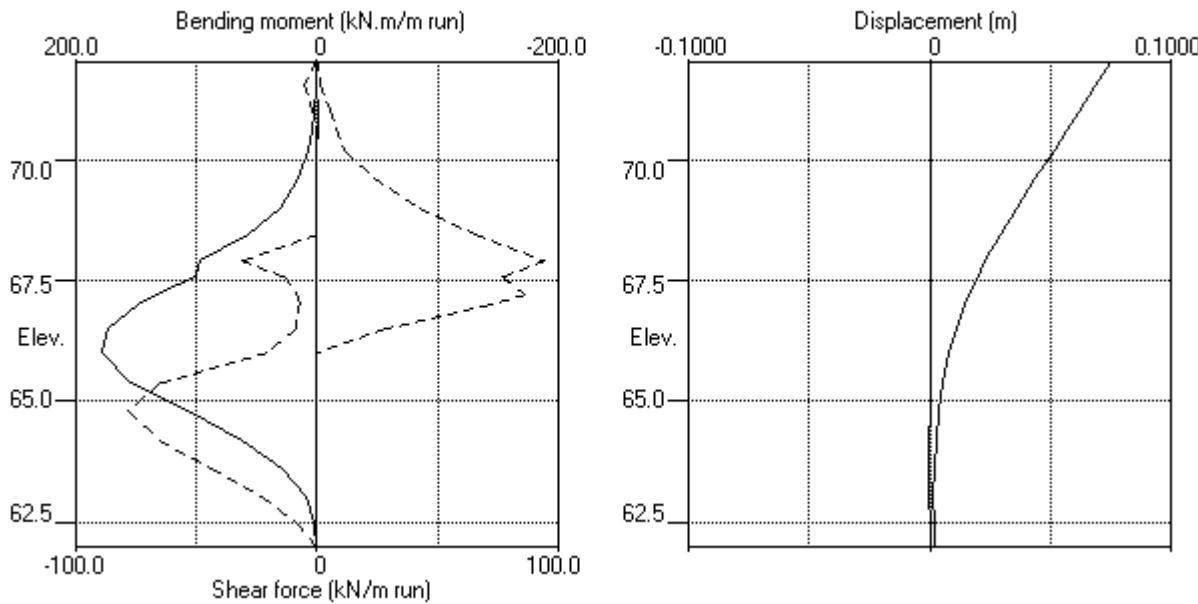
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Contig wall

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Bending moment, shear force, displacement envelopes



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 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
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Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types			
		Active side		Passive side	
1	75.00	4 MG		4 MG	
2	72.00	1 Head deposits		1 Head deposits	
3	71.00	3 LC UN		3 LC UN	

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	18000	0.652	OC	0.376	3.077	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	35200	1.000	OC	0.361	3.253	2.500d
		( 3904)		(0.200)	(1.370)	( 4.831)	
3 LC UN ( 71.00 )	20.00	44000	1.000	OC	1.000	1.000	44.00u
		( 4880)		(0.490)	(2.389)	( 2.390)	( 4.900)
4 MG	18.00	10000	0.530	OC	0.309	3.868	
				(0.200)	(0.000)	( 0.000)	

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---			
Soil	Wall	Back-	Soil	Wall	Back-	
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.	
No. Description						
1 Head deposits	24.00	0.500	0.00	24.00	0.500	0.00
2 LC DR	25.00	0.500	0.00	25.00	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 MG	28.00	0.670	0.00	28.00	0.500	0.00

##### GROUND WATER CONDITIONS

Density of water	= 10.00 kN/m3	Active side	Passive side
Initial water table elevation		67.30	67.30

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side			
profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	74.00	74.00	0.0	1	67.60	67.60	0.0
					2	67.60	74.00	64.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 65.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	67.90	1.00	0.400000	1.500E+07	20.00	0.00	0 No
2	74.75	10.00	0.030000	1.600E+06	0.10	0.00	0 No
3	71.50	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**SURCHARGE LOADS**

Surcharge no.	Elev. from wall	Distance parallel to wall	Length perpend. to wall	Width kN/m2	Surcharge Near edge	Equiv. soil type	Partial factor/ Category
1	75.00	0.50 (A)	20.00	20.00	10.00 =	N/A	N/A
2	67.60	-0.00 (P)	20.00	20.00	64.00 =	N/A	N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m2/m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 75.00
3	Install strut or anchor no.2 at elevation 74.75
4	Excavate to elevation 67.60 on PASSIVE side
5	Install strut or anchor no.1 at elevation 67.90
6	Install strut or anchor no.3 at elevation 71.50
7	Apply surcharge no.2 at elevation 67.60
8	Apply water pressure profile no.1 No analysis at this stage
9	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
10	Change EI of wall to 31986 kN.m2/m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m3  
Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 75.00	No	No	No			
3	Install strut no.2 at elev. 74.75	No	No	No			
4	Excav. to elev. 67.60 on PASSIVE side	Yes	Yes	Yes			
5	Install strut no.1 at elev. 67.90	No	No	No			
6	Install strut no.3 at elev. 71.50	No	No	No			
7	Apply surcharge no.2 at elev. 67.60	No	No	No			
8	Apply water pressure profile no.1	No	No	No			
9	Change soil type 3 to soil type 2	No	No	No			
10	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
*	Summary output	Yes	-	Yes			

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 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
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Units: kN,m

Stage No. 10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 75.00 to 65.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**

Factor of safety on soil strength

			FoS for toe elev. = 65.00	Toe elev. for FoS = 1.000		
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment	Toe elev.	Wall Penetr
Act.	Pass.	Elev.	Safety at elev.			-ation
10		75.00	67.60	More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	75.00	0.00	-0.001	-7.69E-03	0.0	-0.0		31986
2	74.75	2.96	0.001	-7.69E-03	0.4	0.0	42.3	31986
		2.96	0.001	-7.69E-03	-41.9	0.0		
3	74.38	5.37	0.004	-7.60E-03	-40.4	-16.4		31986
4	74.00	7.72	0.007	-7.34E-03	-37.9	-32.2		31986
5	73.60	13.05	0.010	-6.87E-03	-33.7	-47.8		31986
6	73.20	18.30	0.012	-6.24E-03	-27.5	-61.4		31986
7	72.60	26.09	0.016	-5.05E-03	-14.2	-76.5		31986
8	72.00	33.77	0.018	-3.72E-03	3.8	-83.1		31986
		37.67	0.018	-3.72E-03	3.8	-83.1		
9	71.50	44.24	0.020	-2.63E-03	24.3	-79.7	89.3	31986
		44.24	0.020	-2.63E-03	-65.0	-79.7		
10	71.00	49.94	0.021	-1.39E-03	-41.5	-101.3		31986
		45.42	0.021	-1.39E-03	-41.5	-101.3		
11	70.60	50.89	0.021	-1.61E-04	-22.2	-110.9		31986
12	70.20	56.35	0.021	1.18E-03	-0.8	-113.4		31986
13	69.60	64.52	0.020	3.15E-03	35.5	-102.1		31986
14	69.00	72.68	0.017	4.71E-03	76.7	-70.5		31986
15	68.45	80.14	0.015	5.40E-03	118.7	-21.3		31986
16	67.90	87.59	0.012	4.97E-03	164.8	49.6	217.5	31986
		87.59	0.012	4.97E-03	-52.6	49.6		
17	67.60	91.66	0.010	4.42E-03	-25.8	47.5		31986
		15.58	0.010	4.42E-03	-25.8	47.5		
18	67.30	6.89	0.009	3.96E-03	-22.4	48.2		31986
19	66.95	-3.24	0.008	3.50E-03	-21.7	48.3		31986
20	66.60	-10.59	0.007	3.11E-03	-24.2	42.6		31986
21	66.00	7.83	0.005	2.60E-03	-25.0	30.5		31986
22	65.50	21.05	0.004	2.37E-03	-17.8	10.7		31986
23	65.00	50.03	0.002	2.31E-03	0.0	0.0		---

At elev. 74.75 Strut force = 422.9 kN/strut = 42.3 kN/m run

At elev. 71.50 Strut force = 89.3 kN/strut = 89.3 kN/m run

At elev. 67.90 Strut force = 217.5 kN/strut = 217.5 kN/m run

(continued)

Stage No.10 Change EI of wall to 31986 kN.m2/m run  
From elevation 75.00 to 65.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total earth pressure kN/m2	Soil stiffness kN/m3		
		Effective stresses				Earth pressure kN/m2					
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2						
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	5792		
2	74.75	0.00	4.91	1.52	18.97	2.96	2.96	0.00	5792		
3	74.38	0.00	13.85	4.28	53.57	5.37	5.37	0.00	5792		
4	74.00	0.00	22.50	6.95	87.03	7.72	7.72	0.00	5792		
5	73.60	4.00	26.99	8.34	104.40	9.05	13.05	0.00	5792		
6	73.20	8.00	31.01	9.58	119.95	10.30	18.30	0.00	5792		
7	72.60	14.00	36.57	11.30	141.45	12.09	26.09	0.00	3121		
8	72.00	20.00	41.81	12.92	161.74	13.77	33.77	0.00	3121		
		20.00	41.81	15.74	128.66	17.67	37.67	0.00	5618		
9	71.50	25.00	47.05	17.70	144.76	19.24	44.24	0.00	5618		
10	71.00	30.00	52.20	19.64	160.61	19.94	49.94	0.00	5618		
		30.00	52.20	15.42	181.86	15.42	45.42a	0.00	10986		
11	70.60	34.00	56.27	16.89	195.11	16.89	50.89a	0.00	11473		
12	70.20	38.00	60.31	18.35	208.26	18.35	56.35a	0.00	11960		
13	69.60	44.00	66.33	20.52	227.83	20.52	64.52a	0.00	12692		
14	69.00	50.00	72.30	22.68	247.24	22.68	72.68a	0.00	13423		
15	68.45	55.50	77.74	24.64	264.94	24.64	80.14a	0.00	14093		
16	67.90	61.00	83.15	26.59	282.55	26.59	87.59a	0.00	14763		
17	67.60	64.00	86.10	27.66	292.13	27.66	91.66a	0.00	15128		
18	67.30	67.00	89.04	28.72	301.69	28.72	95.72a	0.00	15494		
19	66.95	70.50	92.46	29.95	312.83	29.95	100.45a	0.00	15920		
20	66.60	74.00	95.88	31.19	323.95	33.95	107.95	0.00	16347		
21	66.00	80.00	101.73	33.30	342.97	71.68	151.68	0.00	17078		
22	65.50	85.00	106.59	35.06	358.79	100.84	185.84	0.00	17687		
23	65.00	90.00	111.45	36.81	374.60	137.40	227.40	0.00	18296		

Node no.	Y coord	PASSIVE side						Total earth pressure kN/m2	Soil stiffness kN/m3		
		Effective stresses				Earth pressure kN/m2					
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2						
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
2	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
3	74.38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
4	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
5	73.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
6	73.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
7	72.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
8	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
9	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
10	71.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
11	70.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
12	70.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
13	69.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
14	69.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
15	68.45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
16	67.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
17	67.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
		64.00	-0.00	0.00	12.08	12.08	76.08p	0.00	15128		
18	67.30	67.00	3.00	0.00	21.82	21.82	88.82p	0.00	15494		
19	66.95	70.50	6.49	0.00	33.20	33.20	103.70p	0.00	15920		

(continued)

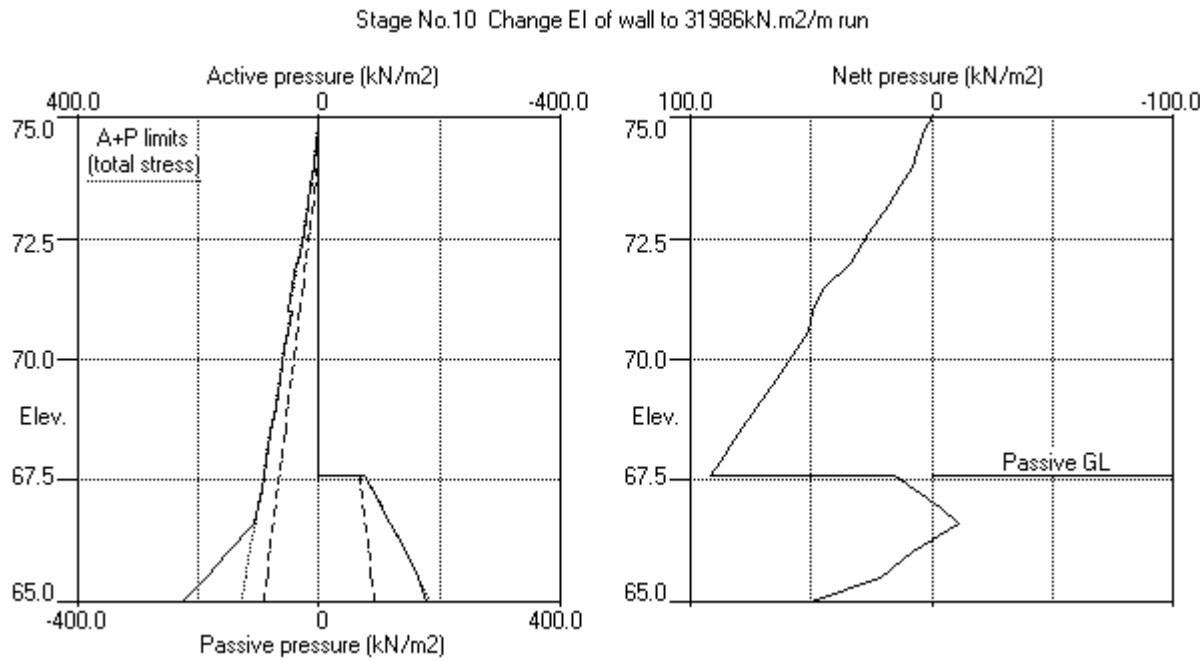
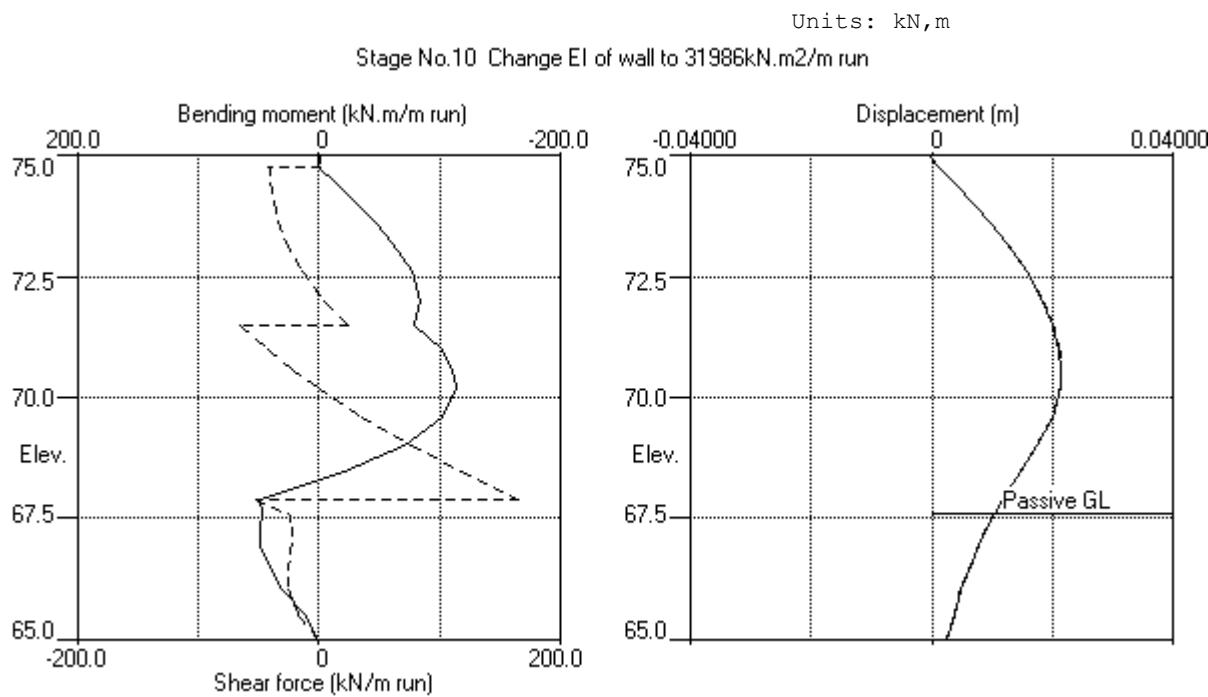
Stage No.10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
From elevation 75.00 to 65.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	PASSIVE side						Soil stiffness coeff.	
		Effective stresses				Total earth pressure			
		Water press.	Vertical -al limit	Active limit	Passive limit				
20	66.60	74.00	9.98	0.18	44.53	44.53	118.53p	16347	
21	66.00	80.00	15.91	2.32	63.85	63.85	143.85p	17078	
22	65.50	85.00	20.81	4.09	79.78	79.78	164.78p	17687	
23	65.00	90.00	25.66	5.84	95.54	87.36	177.36	18296	

Note: 100.45a Soil pressure at active limit  
164.78p Soil pressure at passive limit

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 Hampstead Green  
 Contig wall

Sheet No.  
 Job No. 16-0036  
 Made by : KK  
 Date: 25-04-2016  
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Hampstead Green  
Contig wall

| Sheet No.  
| Job No. 16-0036  
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| Checked :

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Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000	Wall Penetr -ation
	Act.	Pass.		Factor of equilib.	Moment Safety at elev.	
1	75.00	75.00	Cant.	Conditions not suitable for FoS calc.		
2	75.00	75.00	Cant.	Conditions not suitable for FoS calc.		
3	75.00	75.00		No analysis at this stage		
4	75.00	67.60	74.75	1.649 n/a	66.84	0.76
5	75.00	67.60		No analysis at this stage		

All remaining stages have more than one strut - FoS calculation n/a

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 Contig wall

	Sheet No.
	Job No. 16-0036
	Made by : KK
	Date: 25-04-2016
	Checked :

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Units: kN,m

### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	75.00	0.000	-0.001	0.0	-0.0	0.0	0.0
2	74.75	0.001	0.000	0.0	0.0	0.4	-54.0
3	74.38	0.004	0.000	0.0	-20.1	0.0	-52.9
4	74.00	0.007	0.000	0.0	-39.5	0.0	-50.8
5	73.60	0.010	0.000	0.0	-59.3	0.0	-47.5
6	73.20	0.012	0.000	0.0	-77.4	0.0	-43.2
7	72.60	0.016	0.000	0.0	-101.0	0.0	-34.9
8	72.00	0.018	0.000	0.0	-118.9	3.8	-24.5
9	71.50	0.020	0.000	0.0	-128.1	24.3	-65.0
10	71.00	0.021	0.000	0.0	-131.8	2.8	-41.5
11	70.60	0.021	0.000	0.0	-130.2	11.2	-22.2
12	70.20	0.021	0.000	0.0	-125.0	20.4	-0.8
13	69.60	0.020	0.000	0.0	-109.7	35.7	0.0
14	69.00	0.017	0.000	0.0	-83.7	76.7	0.0
15	68.45	0.015	0.000	0.1	-48.9	118.7	0.0
16	67.90	0.012	0.000	49.6	-1.4	164.8	-52.6
17	67.60	0.010	0.000	47.5	0.0	115.0	-25.8
18	67.30	0.009	0.000	59.0	0.0	74.2	-22.4
19	66.95	0.008	0.000	78.8	0.0	26.5	-21.7
20	66.60	0.007	0.000	79.7	0.0	0.0	-24.2
21	66.00	0.005	0.000	59.4	0.0	0.0	-62.2
22	65.50	0.004	0.000	22.6	0.0	0.0	-59.4
23	65.00	0.002	-0.001	0.0	-0.0	0.0	0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. kn. 75.00	minimum kN.m/m	elev. 0.0	maximum kN/m	elev. 75.00	minimum kN/m	elev. 0.0
1	0.0	75.00	0.0	75.00	0.0	75.00	0.0	75.00
2	0.1	67.60	-0.8	72.60	0.4	72.00	-0.5	74.00
3	No calculation at this stage							
4	72.7	66.60	-129.7	71.00	99.7	67.60	-57.0	66.00
5	No calculation at this stage							
6	No calculation at this stage							
7	79.7	66.60	-131.8	71.00	115.0	67.60	-62.2	66.00
8	No calculation at this stage							
9	No calculation at this stage							
10	49.6	67.90	-113.4	70.20	164.8	67.90	-65.0	71.50

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
1	0.000	75.00	0.000	75.00	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	0.000	72.60	0.000	75.00	Apply surcharge no.1 at elev. 75.00
3	No calculation at this stage				Install strut no.2 at elev. 74.75
4	0.020	70.60	-0.000	75.00	Excav. to elev. 67.60 on PASSIVE side
5	No calculation at this stage				Install strut no.1 at elev. 67.90
6	No calculation at this stage				Install strut no.3 at elev. 71.50
7	0.020	70.60	-0.001	65.00	Apply surcharge no.2 at elev. 67.60
8	No calculation at this stage				Apply water pressure profile no.1
9	No calculation at this stage				Change soil type 3 to soil type 2
10	0.021	70.60	-0.001	75.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 at elev. 67.90	kN/m run	Strut no. 2 at elev. 74.75	kN/m run	Strut no. 3 at elev. 71.50	kN/m run
4	---	---	54.01	540.14	---	---
7	slack	slack	54.21	542.14	2.74	2.74
10	217.46	217.46	42.29	422.85	89.29	89.29

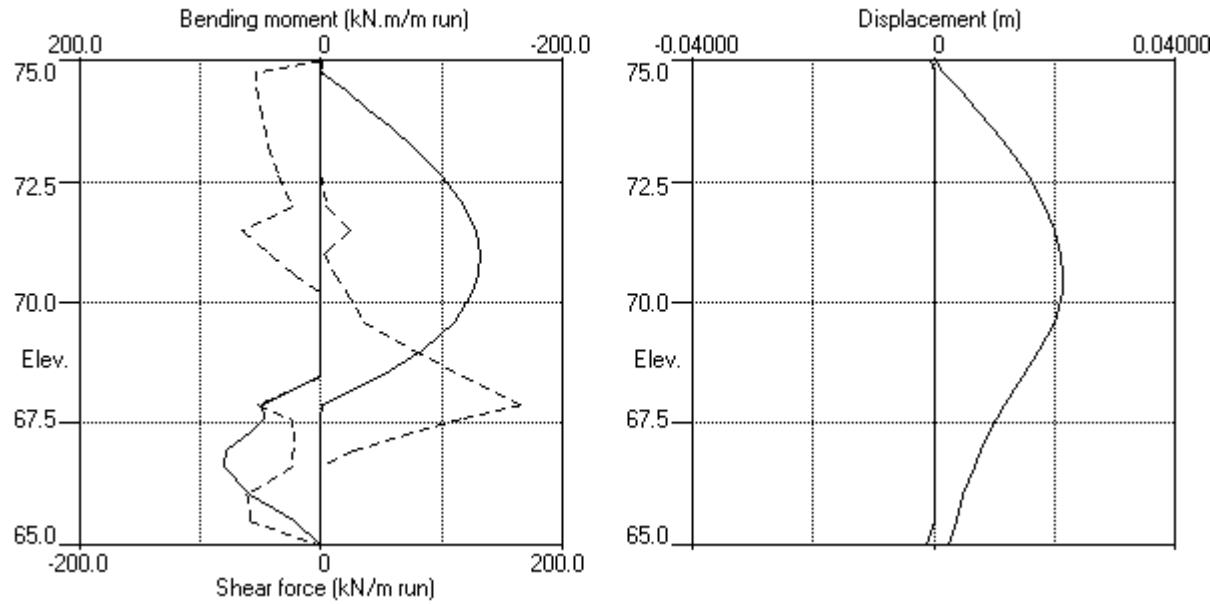
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Hampstead Green  
Contig wall

| Sheet No.  
| Job No. 16-0036  
| Made by : KK  
| Date: 25-04-2016  
| Checked :

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Units: kN,m

Bending moment, shear force, displacement envelopes



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 Program: WALLAP Version 6.05 Revision A45.B58.R49 | Job No. 16-0036  
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 Data filename/Run ID: Section 4 CP27-32 ULS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
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Units: kN,m

### INPUT DATA

#### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	75.00	4 MG	4 MG
2	72.00	1 Head deposits	1 Head deposits
3	71.00	3 LC UN	3 LC UN

#### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol. state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	9000	0.652	OC	0.436	2.540	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	17600	1.000	OC	0.422	2.648	2.100d
		( 1952)		(0.200)	(1.489)	( 4.248)	
3 LC UN ( 71.00 )	20.00	22000	1.000	OC	1.000	1.000	29.30u
		( 2440)		(0.490)	(2.389)	( 2.390)	( 3.300)
4 MG	18.00	5000	0.530	OC	0.368	3.060	
				(0.200)	(0.000)	( 0.000)	

#### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---			
Soil	Wall	Back-	Soil	Wall	Back-	
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.	
No. Description						
1 Head deposits	20.40	0.500	0.00	20.40	0.500	0.00
2 LC DR	21.20	0.500	0.00	21.20	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 MG	23.90	0.670	0.00	23.90	0.500	0.00

#### GROUND WATER CONDITIONS

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	67.30	67.30

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side			
profile	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	74.00	74.00	0.0	1	67.60	67.60	0.0
					2	67.60	74.00	64.0

#### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 65.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut sq.m	Youngs modulus kN/m2	Free length m	-ation (degs)	Inclin /strut	Pre- stress kN	Tension allowed
1	67.90	1.00	0.400000	1.500E+07	20.00	0.00	0	No
2	74.75	10.00	0.030000	1.600E+06	0.10	0.00	0	No
3	71.50	1.00	0.400000	1.500E+07	20.00	0.00	0	No

**SURCHARGE LOADS**

Surcharge no.	Elev. from wall	Distance parallel to wall	Length perpend. to wall	Width kN/m2	Surcharge Near edge	Equiv. soil type	Partial factor/	Category
1	75.00	0.50 (A)	20.00	20.00	10.00	=	N/A	N/A
2	67.60	-0.00 (P)	20.00	20.00	64.00	=	N/A	N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m2/m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 75.00
3	Install strut or anchor no.2 at elevation 74.75
4	Excavate to elevation 67.60 on PASSIVE side
5	Install strut or anchor no.1 at elevation 67.90
6	Install strut or anchor no.3 at elevation 71.50
7	Apply surcharge no.2 at elevation 67.60
8	Apply water pressure profile no.1 No analysis at this stage
9	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
10	Change EI of wall to 31986 kN.m2/m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
 Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m3  
 Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
 Open Tension Crack analysis? - No  
 Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
 Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
 Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 75.00	No	No	No			
3	Install strut no.2 at elev. 74.75	No	No	No			
4	Excav. to elev. 67.60 on PASSIVE side	Yes	Yes	Yes			
5	Install strut no.1 at elev. 67.90	No	No	No			
6	Install strut no.3 at elev. 71.50	No	No	No			
7	Apply surcharge no.2 at elev. 67.60	No	No	No			
8	Apply water pressure profile no.1	No	No	No			
9	Change soil type 3 to soil type 2	No	No	No			
10	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
*	Summary output	Yes	-	Yes			

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 Program: WALLAP Version 6.05 Revision A45.B58.R49 | Job No. 16-0036  
 Licensed from GEOSOLVE | Made by : KK  
 Data filename/Run ID: Section 4 CP27-32 ULS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

Stage No. 10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
 From elevation 75.00 to 65.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

			FoS for toe elev. = 65.00	Toe elev. for FoS = 1.000		
Stage No.	---	G.L. ---	Strut Factor of equilib.	Moment Safety at elev.	Toe elev. Penetr	Wall -ation
Act.	Pass.	Elev.				
10	75.00	67.60		More than one strut		

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	75.00	0.00	-0.002	-1.48E-02	0.0	0.0		31986
2	74.75	3.08	0.002	-1.48E-02	0.4	0.0	61.8	31986
		3.08	0.002	-1.48E-02	-61.4	0.0		
3	74.38	6.10	0.008	-1.47E-02	-59.7	-24.3		31986
4	74.00	9.02	0.013	-1.43E-02	-56.9	-47.8		31986
5	73.60	14.90	0.019	-1.36E-02	-52.1	-71.5		31986
6	73.20	20.66	0.024	-1.26E-02	-45.0	-92.9		31986
7	72.60	29.14	0.031	-1.08E-02	-30.0	-119.0		31986
8	72.00	37.55	0.037	-8.70E-03	-10.0	-135.4		31986
		41.61	0.037	-8.70E-03	-10.0	-135.4		
9	71.50	49.11	0.041	-6.82E-03	12.7	-139.2	92.4	31986
		49.11	0.041	-6.82E-03	-79.7	-139.2		
10	71.00	56.11	0.044	-4.67E-03	-53.4	-168.0		31986
		48.91	0.044	-4.67E-03	-53.4	-168.0		
11	70.60	54.63	0.045	-2.64E-03	-32.7	-182.5		31986
12	70.20	60.34	0.046	-4.53E-04	-9.7	-189.5		31986
13	69.60	68.88	0.045	2.86E-03	29.1	-183.9		31986
14	69.00	77.40	0.042	5.84E-03	73.0	-156.4		31986
15	68.45	85.20	0.039	7.87E-03	117.7	-109.3		31986
16	67.90	92.99	0.034	8.79E-03	166.7	-38.6	196.9	31986
		92.99	0.034	8.79E-03	-30.2	-38.6		
17	67.60	97.23	0.031	8.94E-03	-1.7	-35.1		31986
		24.31	0.031	8.94E-03	-1.7	-35.1		
18	67.30	17.62	0.029	9.12E-03	4.6	-27.5		31986
19	66.95	9.81	0.025	9.31E-03	9.4	-18.9		31986
20	66.60	2.02	0.022	9.47E-03	11.4	-11.3		31986
21	66.00	-11.23	0.016	9.65E-03	8.7	-3.1		31986
22	65.50	-20.59	0.011	9.69E-03	0.7	3.1		31986
23	65.00	17.68	0.007	9.68E-03	0.0	0.0		---

At elev. 74.75 Strut force = 618.0 kN/strut = 61.8 kN/m run

At elev. 71.50 Strut force = 92.4 kN/strut = 92.4 kN/m run

At elev. 67.90 Strut force = 196.9 kN/strut = 196.9 kN/m run

(continued)

Stage No.10 Change EI of wall to 31986 kN.m2/m run  
 From elevation 75.00 to 65.00  
 Yield moment not defined  
 Allow wall to relax with new modulus value

Node no.	Y coord	ACTIVE side						Total earth pressure	Soil stiffness coeff.		
		Effective stresses				Earth pressure					
		Water press. kN/m2	Vertic -al limit kN/m2	Active limit kN/m2	Passive limit kN/m2						
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	3237		
2	74.75	0.00	4.91	1.81	15.01	3.08	3.08	3.08	3237		
3	74.38	0.00	13.85	5.10	42.38	6.10	6.10	6.10	3237		
4	74.00	0.00	22.50	8.28	68.85	9.02	9.02	9.02	3237		
5	73.60	4.00	26.99	9.93	82.59	10.90	14.90	14.90	3237		
6	73.20	8.00	31.01	11.41	94.89	12.66	20.66	20.66	3237		
7	72.60	14.00	36.57	13.46	111.90	15.14	29.14	29.14	2005		
8	72.00	20.00	41.81	15.39	127.95	17.55	37.55	37.55	2004		
		20.00	41.81	18.24	106.20	21.61	41.61	41.61	3606		
9	71.50	25.00	47.05	20.53	119.49	24.11	49.11	49.11	3606		
10	71.00	30.00	52.20	22.77	132.57	26.11	56.11	56.11	3606		
		30.00	52.20	18.91	147.12	18.91	48.91a	48.91a	7052		
11	70.60	34.00	56.27	20.63	157.91	20.63	54.63a	54.63a	7365		
12	70.20	38.00	60.31	22.34	168.61	22.34	60.34a	60.34a	7678		
13	69.60	44.00	66.33	24.88	184.54	24.88	68.88a	68.88a	8148		
14	69.00	50.00	72.30	27.40	200.35	27.40	77.40a	77.40a	8617		
15	68.45	55.50	77.74	29.70	214.75	29.70	85.20a	85.20a	9047		
16	67.90	61.00	83.15	31.99	229.09	31.99	92.99a	92.99a	9477		
17	67.60	64.00	86.10	33.23	236.89	33.23	97.23a	97.23a	9712		
18	67.30	67.00	89.04	34.47	244.67	34.47	101.47a	101.47a	9947		
19	66.95	70.50	92.46	35.92	253.73	35.92	106.42a	106.42a	10220		
20	66.60	74.00	95.88	37.36	262.78	37.36	111.36a	111.36a	10494		
21	66.00	80.00	101.73	39.83	278.27	39.83	119.83a	119.83a	10963		
22	65.50	85.00	106.59	41.89	291.15	43.44	128.44	128.44	11355		
23	65.00	90.00	111.45	43.94	304.02	94.54	184.54	184.54	11746		

Node no.	Y coord	PASSIVE side						Total earth pressure	Soil stiffness coeff.		
		Effective stresses				Earth pressure					
		Water press. kN/m2	Vertic -al limit kN/m2	Active limit kN/m2	Passive limit kN/m2						
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
2	74.75	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
3	74.38	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
4	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
5	73.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
6	73.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
7	72.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
8	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
9	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
10	71.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
11	70.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
12	70.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
13	69.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
14	69.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
15	68.45	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
16	67.90	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
17	67.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
		64.00	-0.00	0.00	8.92	8.92	72.92p	72.92p	9720		
18	67.30	67.00	3.00	0.00	16.85	16.85	83.85p	83.85p	9955		
19	66.95	70.50	6.49	0.00	26.11	26.11	96.61p	96.61p	10229		

(continued)

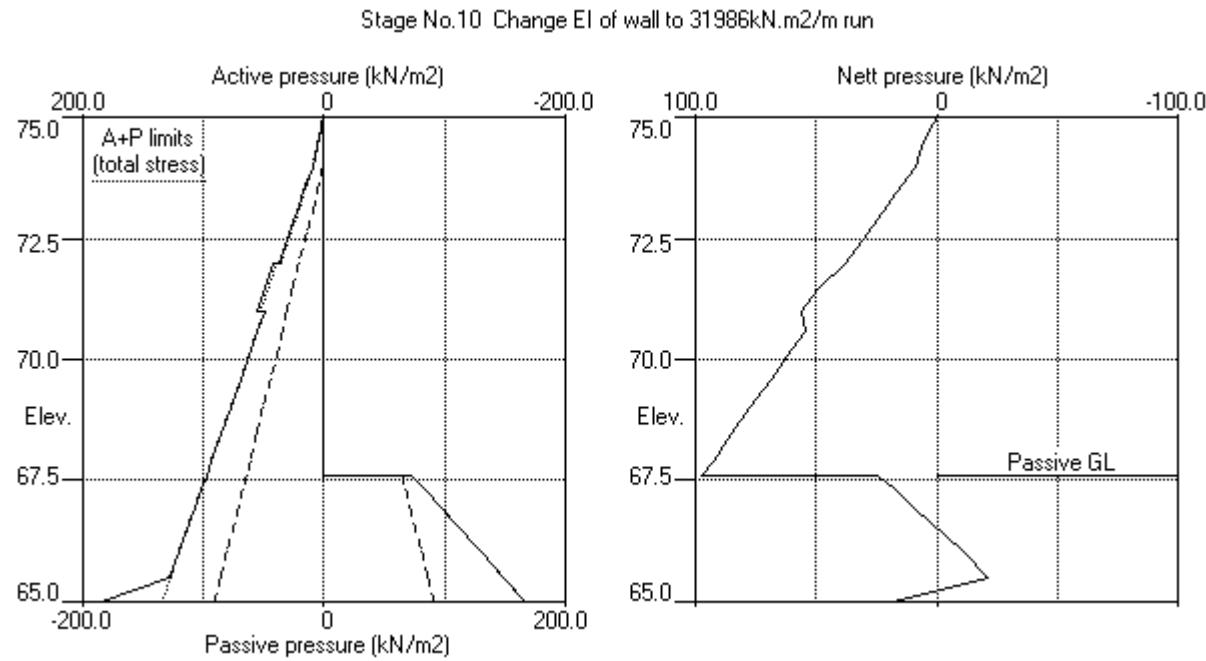
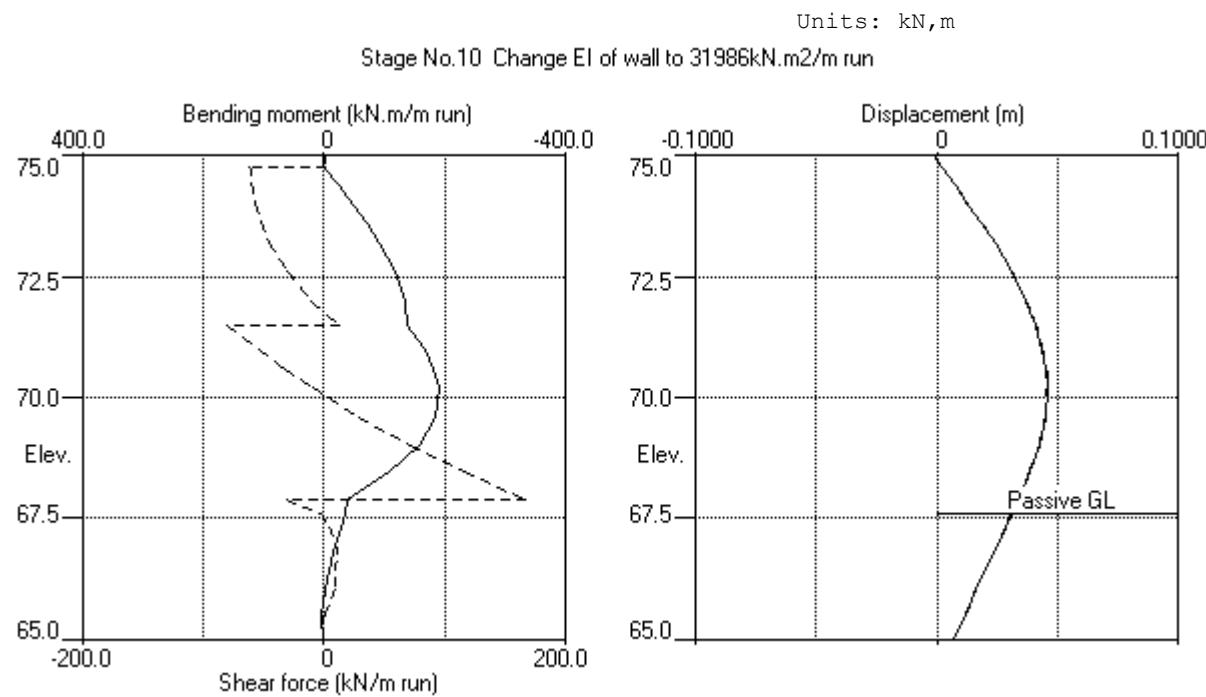
Stage No.10 Change EI of wall to 31986 kN.m<sup>2</sup>/m run  
From elevation 75.00 to 65.00  
Yield moment not defined  
Allow wall to relax with new modulus value

Node no.	Y coord	PASSIVE side						Soil stiffness coeff.	
		Effective stresses				Total earth pressure			
		Water press. kN/m <sup>2</sup>	Vertic -al limit kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>				
20	66.60	74.00	9.98	1.09	35.34	35.34	109.34p	10503	
21	66.00	80.00	15.91	3.59	51.06	51.06	131.06p	10973	
22	65.50	85.00	20.81	5.66	64.03	64.03	149.03p	11364	
23	65.00	90.00	25.66	7.71	76.86	76.86	166.86p	11756	

Note: 119.83a Soil pressure at active limit  
166.86p Soil pressure at passive limit

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Contig wall

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Contig wall

| Sheet No.  
| Job No. 16-0036  
| Made by : KK  
| Date: 25-04-2016  
| Checked :

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Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000	Wall Penetr -ation
	Act.	Pass.		Factor of equilib.	Moment Safety at elev.	
1	75.00	75.00	Cant.	Conditions not suitable for FoS calc.		
2	75.00	75.00	Cant.	Conditions not suitable for FoS calc.		
3	75.00	75.00		No analysis at this stage		
4	75.00	67.60	74.75	1.107 n/a	65.84	1.76
5	75.00	67.60		No analysis at this stage		

All remaining stages have more than one strut - FoS calculation n/a

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	Date: 25-04-2016
	Checked :

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Units: kN,m

#### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	75.00	0.001	-0.002	0.0	0.0	0.0	0.0
2	74.75	0.002	0.000	0.0	0.0	0.4	-80.5
3	74.38	0.008	0.000	0.0	-30.0	0.0	-79.2
4	74.00	0.013	0.000	0.0	-59.2	0.0	-76.7
5	73.60	0.019	0.000	0.0	-89.2	0.0	-72.8
6	73.20	0.024	0.000	0.0	-117.3	0.0	-67.6
7	72.60	0.031	0.000	0.0	-155.0	0.0	-57.7
8	72.00	0.037	0.000	0.0	-186.0	0.3	-45.3
9	71.50	0.041	0.000	0.0	-205.1	12.7	-79.7
10	71.00	0.044	0.000	0.0	-217.7	0.2	-53.4
11	70.60	0.045	0.000	0.0	-222.6	0.3	-32.7
12	70.20	0.046	0.000	0.0	-223.9	4.6	-9.7
13	69.60	0.045	0.000	0.0	-217.8	29.1	0.0
14	69.00	0.042	0.000	0.0	-199.9	73.0	0.0
15	68.45	0.039	0.000	0.0	-170.0	117.7	0.0
16	67.90	0.034	0.000	0.1	-124.2	166.7	-30.2
17	67.60	0.031	0.000	0.1	-93.5	120.3	-1.7
18	67.30	0.029	0.000	0.1	-64.5	98.9	0.0
19	66.95	0.025	0.000	0.1	-36.3	74.1	-0.0
20	66.60	0.022	0.000	0.1	-14.7	51.7	-0.0
21	66.00	0.016	0.000	9.8	-3.1	13.1	-0.1
22	65.50	0.011	0.000	8.8	0.0	0.7	-18.3
23	65.00	0.007	-0.001	0.0	-0.0	0.0	0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. kn. 75.00	minimum kN.m/m	elev. 0.0	maximum kN/m	elev. 75.00	minimum kN/m	elev. 0.0
1	0.0	75.00	0.0	75.00	0.0	75.00	0.0	75.00
2	0.1	67.30	-0.9	72.60	0.3	72.00	-0.6	74.00
3	No calculation at this stage							
4	7.1	65.50	-216.6	70.20	103.2	67.60	-79.6	74.75
5	No calculation at this stage							
6	No calculation at this stage							
7	9.8	66.00	-223.9	70.20	120.3	67.60	-80.5	74.75
8	No calculation at this stage							
9	No calculation at this stage							
10	3.1	65.50	-189.5	70.20	166.7	67.90	-79.7	71.50

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
1	0.000	75.00	0.000	75.00	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	0.001	73.60	0.000	75.00	Apply surcharge no.1 at elev. 75.00
3	No calculation at this stage				Install strut no.2 at elev. 74.75
4	0.045	70.20	-0.001	75.00	Excav. to elev. 67.60 on PASSIVE side
5	No calculation at this stage				Install strut no.1 at elev. 67.90
6	No calculation at this stage				Install strut no.3 at elev. 71.50
7	0.045	70.20	-0.001	75.00	Apply surcharge no.2 at elev. 67.60
8	No calculation at this stage				Apply water pressure profile no.1
9	No calculation at this stage				Change soil type 3 to soil type 2
10	0.046	70.20	-0.002	75.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 at elev. 67.90	kN/m run	Strut no. 2 at elev. 74.75	kN/m run	Strut no. 3 at elev. 71.50	kN/m run
4	---	---	79.85	798.45	---	---
7	slack	slack	80.72	807.22	2.65	2.65
10	196.92	196.92	61.80	618.02	92.36	92.36

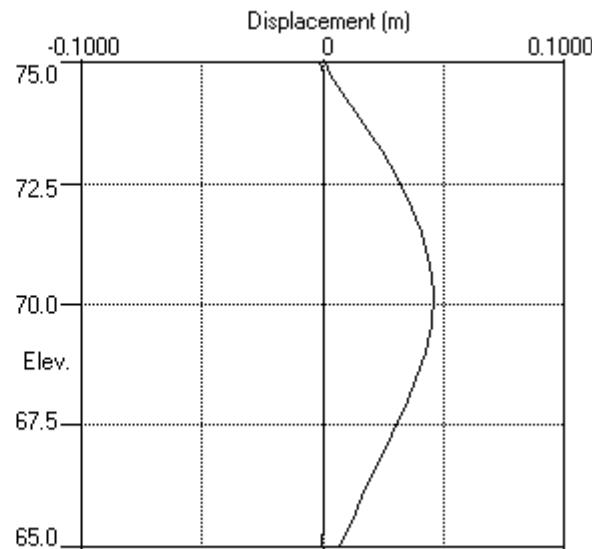
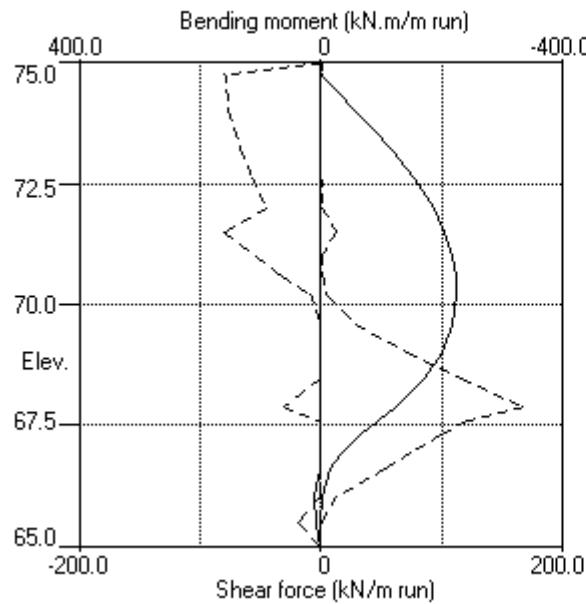
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Contig wall

| Sheet No.  
| Job No. 16-0036  
| Made by : KK  
| Date: 25-04-2016  
Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: Section 5 CP321-352 SLS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	75.00	4 MG	4 MG
2	72.00	1 Head deposits	1 Head deposits
3	71.00	3 LC UN	3 LC UN

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol. state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	18000	0.590	OC	0.376	3.077	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	35200	1.000	OC	0.361	3.253	2.500d
		( 3904)		(0.200)	(1.370)	( 4.831)	
3 LC UN ( 71.00 )	20.00	44000	1.000	OC	1.000	1.000	44.00u
		( 4880)		(0.490)	(2.389)	( 2.390)	( 4.900)
4 MG	18.00	10000	0.530	OC	0.309	3.868	
				(0.200)	(0.000)	( 0.000)	

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---			
Soil	Wall	Back-	Soil	Wall	Back-	
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.	
No. Description						
1 Head deposits	24.00	0.500	0.00	24.00	0.500	0.00
2 LC DR	25.00	0.500	0.00	25.00	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 MG	28.00	0.670	0.00	28.00	0.500	0.00

##### GROUND WATER CONDITIONS

Density of water	= 10.00 kN/m3	Active side	Passive side
Initial water table elevation		71.00	71.00

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side			
profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	74.00	74.00	0.0	1	71.50	71.50	0.0
					2	71.50	74.00	25.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 65.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut sq.m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	71.60	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**HORIZONTAL and MOMENT LOADS/RESTRAINTS**

Load no.	Elevation	Horizontal load kN/m run	Moment load kN.m/m run	Moment restraint kN.m/m/rad	Partial factor/ Category
1	75.00	55.00	0	0	N/A

**SURCHARGE LOADS**

Surcharge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge Near edge	Surcharge Far edge	Equiv. soil type	Partial factor/ Category
1	75.00	0.50 (A)	20.00	20.00	10.00	=	N/A	N/A
2	71.50	-0.00 (P)	20.00	20.00	25.00	=	N/A	N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m <sup>2</sup> /m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 75.00 No analysis at this stage
3	Excavate to elevation 71.50 on PASSIVE side
4	Install strut or anchor no.1 at elevation 71.60
5	Apply surcharge no.2 at elevation 71.50
6	Apply water pressure profile no.1 No analysis at this stage
7	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
8	Change EI of wall to 31986 kN.m <sup>2</sup> /m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
9	Apply load no.1 at elevation 75.00

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 75.00	No	No	No			
3	Excav. to elev. 71.50 on PASSIVE side	Yes	Yes	Yes			
4	Install strut no.1 at elev. 71.60	No	No	No			
5	Apply surcharge no.2 at elev. 71.50	No	No	No			
6	Apply water pressure profile no.1	No	No	No			
7	Change soil type 3 to soil type 2	No	No	No			
8	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
9	Apply load no.1 at elev. 75.00	No	No	No			
*	Summary output	Yes	-	Yes			

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ROCK & ALLUVIUM LTD | Sheet No.  
 Program: WALLAP Version 6.05 Revision A45.B58.R49 | Job No. 16-0036  
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 Data filename/Run ID: Section 5 CP321-352 SLS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

Stage No. 9 Apply load no.1 at elevation 75.00

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

			FoS for toe elev. = 65.00	Toe elev. for FoS = 1.000
<hr/>				
Stage --- G.L. ---	Strut No.	Factor Act.	Moment of equilib.	Toe elev. Penetr
			Safety at elev.	-ation
9	75.00	71.50	71.60	Conditions not suitable for FoS calc.

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kN.m <sup>2</sup> /m
1	75.00	0.00	0.067	2.10E-02	55.0	0.0	-55.0	31986
2	74.50	3.34	0.056	2.07E-02	55.8	27.6		31986
3	74.00	6.95	0.046	2.01E-02	58.4	56.1		31986
4	73.60	12.34	0.038	1.92E-02	62.3	80.2		31986
5	73.20	17.58	0.030	1.81E-02	68.3	106.2		31986
6	72.60	25.30	0.020	1.57E-02	81.1	150.3		31986
7	72.00	32.92	0.012	1.23E-02	98.6	202.9		31986
		35.74	0.012	1.23E-02	98.6	202.9		
8	71.60	41.31	0.007	9.55E-03	114.0	244.0	232.4	31986
		41.31	0.007	9.55E-03	-118.4	244.0		
9	71.50	42.70	0.006	8.80E-03	-114.2	233.5		31986
		17.70	0.006	8.80E-03	-114.2	233.5		
10	71.00	21.46	0.003	5.55E-03	-104.4	183.7		31986
		18.59	0.003	5.55E-03	-104.4	183.7		
11	70.60	20.03	0.001	3.55E-03	-96.7	147.7		31986
12	70.20	32.24	-0.000	2.00E-03	-86.2	112.9		31986
13	69.60	33.26	-0.001	4.73E-04	-66.6	61.9		31986
14	69.00	35.49	-0.001	-2.80E-04	-45.9	25.1		31986
15	68.40	32.64	-0.000	-5.13E-04	-25.5	2.3		31986
16	67.80	22.16	-0.000	-4.59E-04	-9.1	-7.9		31986
17	67.20	11.27	0.000	-3.03E-04	1.0	-9.7		31986
18	66.60	2.73	0.000	-1.59E-04	5.2	-7.0		31986
19	66.00	-3.24	0.000	-7.21E-05	5.0	-3.2		31986
20	65.50	-5.45	0.000	-4.42E-05	2.8	-0.9		31986
21	65.00	-5.88	0.000	-3.84E-05	0.0	0.0		---

At elev. 71.60 Strut force = 232.4 kN/strut = 232.4 kN/m run

(continued)

Stage No.9 Apply load no.1 at elevation 75.00

Node no.	Y coord	ACTIVE side						Total earth pressure kN/m2	Soil stiffness kN/m <sup>3</sup>		
		Effective stresses									
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>					
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4412		
2	74.50	0.00	10.82	3.34	41.84	3.34	3.34a	3.34a	4412		
3	74.00	0.00	22.50	6.95	87.03	6.95	6.95a	6.95a	4412		
4	73.60	4.00	26.99	8.34	104.40	8.34	12.34a	12.34a	4412		
5	73.20	8.00	31.01	9.58	119.95	9.58	17.58a	17.58a	4412		
6	72.60	14.00	36.57	11.30	141.45	11.30	25.30a	25.30a	4412		
7	72.00	20.00	41.81	12.92	161.74	12.92	32.92a	32.92a	4412		
		20.00	41.81	15.74	128.66	15.74	35.74a	35.74a	7941		
8	71.60	24.00	46.01	17.31	141.56	17.31	41.31a	41.31a	7941		
9	71.50	25.00	47.05	17.70	144.76	17.70	42.70a	42.70a	7941		
10	71.00	30.00	52.20	19.64	160.61	28.78	58.78	58.78	5749		
		30.00	52.20	15.42	181.86	31.17	61.17	61.17	11242		
11	70.60	34.00	56.27	16.89	195.11	39.13	73.13	73.13	11741		
12	70.20	38.00	60.31	18.35	208.26	62.40	100.40	100.40	12240		
13	69.60	44.00	66.33	20.52	227.83	85.45	129.45	129.45	12988		
14	69.00	50.00	72.30	22.68	247.24	96.14	146.14	146.14	13736		
15	68.40	56.00	78.23	24.82	266.54	99.93	155.93	155.93	14484		
16	67.80	62.00	84.13	26.95	285.75	101.20	163.20	163.20	15232		
17	67.20	68.00	90.01	29.07	304.88	102.63	170.63	170.63	15980		
18	66.60	74.00	95.88	31.19	323.95	105.14	179.14	179.14	24006		
19	66.00	80.00	101.73	33.30	342.97	108.68	188.68	188.68	25080		
20	65.50	85.00	106.59	35.06	358.79	112.87	197.87	197.87	25975		
21	65.00	90.00	111.45	36.81	374.60	117.86	207.86	207.86	26869		

Node no.	Y coord	PASSIVE side						Total earth pressure kN/m2	Soil stiffness kN/m <sup>3</sup>		
		Effective stresses									
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>					
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
2	74.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
3	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
4	73.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
5	73.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
6	72.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
7	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
8	71.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
9	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
		25.00	0.00	0.00	0.00	0.00	25.00	84580			
10	71.00	30.00	5.00	1.88	15.38	7.32	37.32	37.32	5749		
		30.00	5.00	0.00	28.34	12.58	42.58	42.58	11242		
11	70.60	34.00	8.99	0.00	41.33	19.10	53.10	53.10	11741		
12	70.20	38.00	12.98	1.26	54.31	30.16	68.16	68.16	12240		
13	69.60	44.00	18.95	3.42	73.71	52.19	96.19	96.19	12988		
14	69.00	50.00	24.89	5.56	93.03	60.65	110.65	110.65	13736		
15	68.40	56.00	30.80	7.69	112.25	67.30	123.30	123.30	14484		
16	67.80	62.00	36.67	9.81	131.37	79.03	141.03	141.03	15232		
17	67.20	68.00	42.52	11.93	150.38	91.36	159.36	159.36	15980		
18	66.60	74.00	48.34	14.03	169.31	102.41	176.41	176.41	24006		
19	66.00	80.00	54.14	16.12	188.17	111.93	191.93	191.93	25080		
20	65.50	85.00	58.96	17.86	203.85	118.31	203.31	203.31	25975		
21	65.00	90.00	63.77	19.60	219.51	123.75	213.75	213.75	26869		

Run ID. Section 5 CP321-352 SLS  
Hampstead Green  
Contig wall

| Sheet No.  
| Date:25-04-2016  
| Checked :

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(continued)

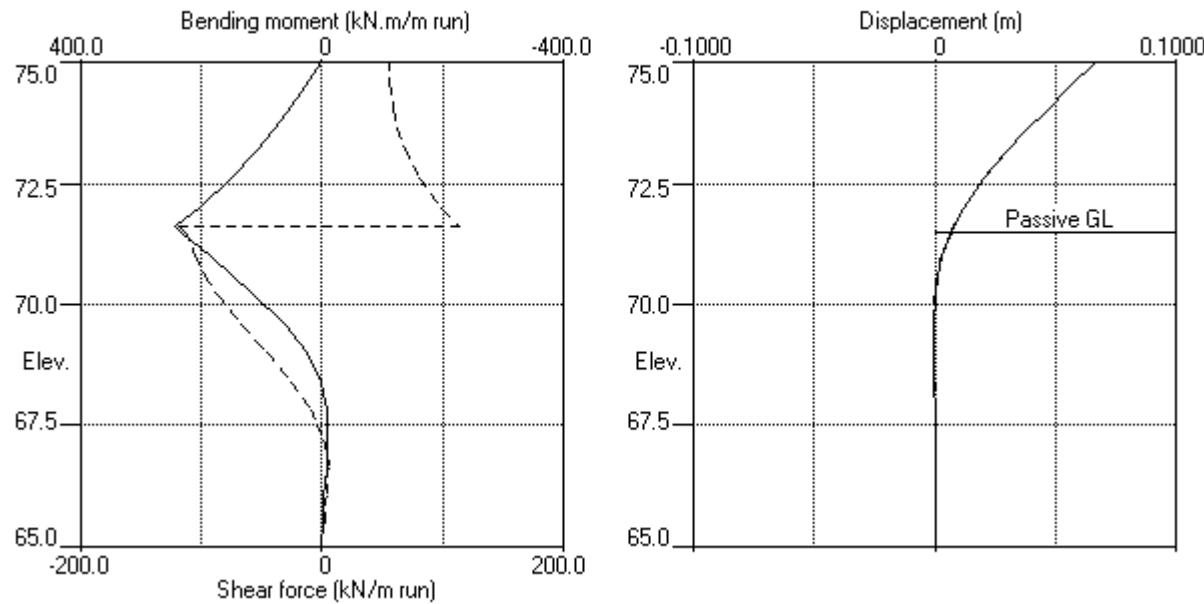
Stage No.9 Apply load no.1 at elevation 75.00  
Note: 42.70a Soil pressure at active limit  
123.45p Soil pressure at passive limit

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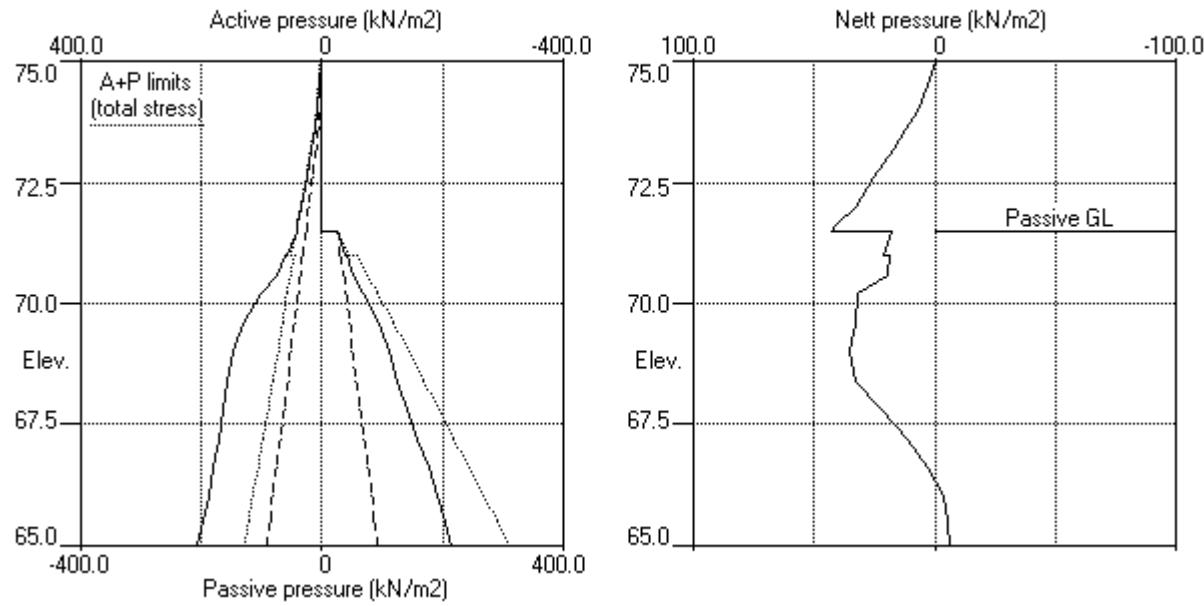
Sheet No.  
Job No. 16-0036  
Made by : KK  
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Checked :

Units: kN,m

Stage No.9 Apply load no.1 at elev. 75.00



Stage No.9 Apply load no.1 at elev. 75.00



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Contig wall

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| Job No. 16-0036  
| Made by : KK  
| Date: 25-04-2016  
Checked :

Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS = 1.000		
	Act.	Pass.		Factor of equilib.	Moment	Toe elev.	Wall Penetr ation
1	75.00	75.00	Cant.	Conditions not suitable for FoS calc.			
2	75.00	75.00		No analysis at this stage			
3	75.00	71.50	Cant.	2.126	65.84	68.77	2.73
4	75.00	71.50		No analysis at this stage			
5	75.00	71.50	71.60	Conditions not suitable for FoS calc.			
6	75.00	71.50		No analysis at this stage			
7	75.00	71.50		No analysis at this stage			
8	75.00	71.50	71.60	Conditions not suitable for FoS calc.			
9	75.00	71.50	71.60	Conditions not suitable for FoS calc.			

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 Contig wall

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	Job No. 16-0036
	Made by : KK
	Date: 25-04-2016
	Checked :

---

Units: kN,m

### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	75.00	0.067	0.000	0.0	-0.0	55.0	0.0
2	74.50	0.056	0.000	27.6	0.0	55.8	0.0
3	74.00	0.046	0.000	56.1	0.0	58.4	0.0
4	73.60	0.038	0.000	80.2	0.0	62.3	0.0
5	73.20	0.030	0.000	106.2	0.0	68.3	0.0
6	72.60	0.020	0.000	150.3	0.0	81.1	0.0
7	72.00	0.012	0.000	202.9	0.0	98.6	0.0
8	71.60	0.007	0.000	244.0	0.0	114.0	-118.4
9	71.50	0.006	0.000	233.5	0.0	45.5	-114.2
10	71.00	0.004	0.000	183.7	0.0	50.3	-104.4
11	70.60	0.003	0.000	147.7	0.0	9.9	-96.7
12	70.20	0.002	-0.000	112.9	0.0	0.0	-86.2
13	69.60	0.001	-0.001	63.5	0.0	0.0	-66.6
14	69.00	0.001	-0.001	36.6	0.0	0.0	-45.9
15	68.40	0.001	-0.000	15.9	0.0	0.0	-27.7
16	67.80	0.001	-0.000	4.6	-7.9	0.0	-15.0
17	67.20	0.001	0.000	0.1	-9.7	1.0	-5.4
18	66.60	0.001	0.000	0.0	-7.0	5.2	-0.9
19	66.00	0.001	0.000	0.0	-3.2	5.0	0.0
20	65.50	0.001	0.000	0.0	-0.9	2.8	0.0
21	65.00	0.001	0.000	0.0	0.0	0.0	-0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. 75.00	minimum kN.m/m	elev. 75.00	maximum kN/m	elev. 75.00	minimum kN/m	elev. 75.00
1	0.0	75.00	0.0	75.00	0.0	75.00	0.0	75.00
2	No calculation at this stage							
3	85.2	70.60	-2.9	66.60	49.2	71.00	-40.9	69.60
4	No calculation at this stage							
5	89.5	70.60	-3.1	66.60	50.3	71.00	-42.7	69.60
6	No calculation at this stage							
7	No calculation at this stage							
8	66.2	70.60	-1.1	66.60	59.0	71.60	-23.9	69.00
9	244.0	71.60	-9.7	67.20	114.0	71.60	-118.4	71.60

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
	m		m		
1	0.000	75.00	0.000	75.00	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 75.00
3	0.023	75.00	0.000	75.00	Excav. to elev. 71.50 on PASSIVE side
4	No calculation at this stage				Install strut no.1 at elev. 71.60
5	0.023	75.00	-0.000	68.40	Apply surcharge no.2 at elev. 71.50
6	No calculation at this stage				Apply water pressure profile no.1
7	No calculation at this stage				Change soil type 3 to soil type 2
8	0.027	75.00	0.000	75.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run
9	0.067	75.00	-0.001	69.00	Apply load no.1 at elev. 75.00

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 ---	
	at elev.	71.60
	kN/m run	kN/strut
5	slack	slack
8	67.76	67.76
9	232.38	232.38

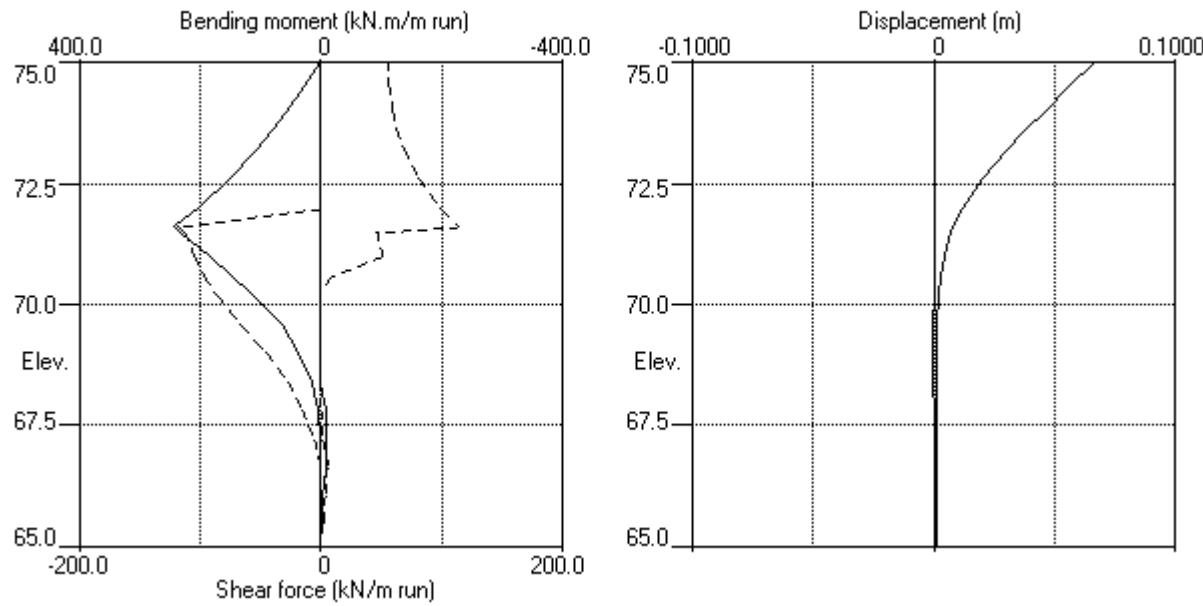
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Hampstead Green  
Contig wall

| Sheet No.  
| Job No. 16-0036  
| Made by : KK  
|  
| Date: 25-04-2016  
Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



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 Data filename/Run ID: Section 5 CP321-352 ULS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

#### INPUT DATA

##### SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	75.00	4 MG	4 MG
2	72.00	1 Head deposits	1 Head deposits
3	71.00	3 LC UN	3 LC UN

##### SOIL PROPERTIES

-- Soil type --	Bulk density	Young's Modulus	At rest coeff.	Consol. state.	Active limit	Passive limit	Cohesion
No. Description	kN/m3	Eh, kN/m2	Ko	NC/OC	Ka	Kp	kN/m2
(Datum elev.)		(dEh/dy )	(dKo/dy)	( Nu )	( Kac )	( Kpc )	( dc/dy )
1 Head deposits	20.00	9000	0.650	OC	0.436	2.540	
				(0.200)	(0.000)	( 0.000)	
2 LC DR ( 71.00 )	20.00	17600	1.000	OC	0.422	2.648	2.100d
		( 1952)		(0.200)	(1.489)	( 4.248)	
3 LC UN ( 71.00 )	20.00	22000	1.000	OC	1.000	1.000	29.30u
		( 2440)		(0.490)	(2.389)	( 2.390)	( 3.300)
4 MG	18.00	5000	0.590	OC	0.368	3.060	
				(0.200)	(0.000)	( 0.000)	

##### Additional soil parameters associated with Ka and Kp

--- parameters for Ka ---			--- parameters for Kp ---			
Soil	Wall	Back-	Soil	Wall	Back-	
----- Soil type -----	friction angle	adhesion coeff.	fill angle	friction angle	adhesion coeff.	
No. Description						
1 Head deposits	20.40	0.500	0.00	20.40	0.500	0.00
2 LC DR	21.20	0.500	0.00	21.20	0.500	0.00
3 LC UN	0.00	0.500	0.00	0.00	0.500	0.00
4 MG	23.90	0.670	0.00	23.90	0.500	0.00

##### GROUND WATER CONDITIONS

Density of water = 10.00 kN/m3

	Active side	Passive side
Initial water table elevation	71.00	71.00

Automatic water pressure balancing at toe of wall : No

Water press.	Active side				Passive side				
	profile no.	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	74.00	74.00	0.0	0.0	1	71.50	71.50	0.0
						2	71.50	74.00	25.0

##### WALL PROPERTIES

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 65.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.8000E+07 kN/m2  
 Moment of inertia of wall I = 2.2847E-03 m4/m run  
 E.I = 63972 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	X-section Strut spacing of strut m	Youngs modulus kN/m <sup>2</sup>	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	71.60	1.00	0.400000	1.500E+07	20.00	0.00	0 No

**HORIZONTAL and MOMENT LOADS/RESTRAINTS**

Load no.	Elevation	Horizontal load kN/m run	Moment load kN.m/m run	Moment restraint kN.m/m/rad	Partial factor/ Category
1	75.00	55.00	0	0	N/A

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge Near edge	-----	Equiv. soil type	Partial factor/ Category
1	75.00	0.50 (A)	20.00	20.00	10.00	=	N/A	N/A
2	71.50	-0.00 (P)	20.00	20.00	25.00	=	N/A	N/A

Note: A = Active side, P = Passive side

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Change EI of wall to 44780 kN.m <sup>2</sup> /m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
2	Apply surcharge no.1 at elevation 75.00 No analysis at this stage
3	Excavate to elevation 71.15 on PASSIVE side
4	Fill to elevation 71.50 on PASSIVE side with soil type 1
5	Install strut or anchor no.1 at elevation 71.60
6	Apply surcharge no.2 at elevation 71.50
7	Apply water pressure profile no.1 No analysis at this stage
8	Change properties of soil type 3 to soil type 2 No analysis at this stage Ko pressures will not be reset
9	Change EI of wall to 31986 kN.m <sup>2</sup> /m run From elevation 75.00 to 65.00 Yield moment not defined Allow wall to relax with new modulus value
10	Apply load no.1 at elevation 75.00

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

## Stability analysis:

Method of analysis - Strength Factor method  
Factor on soil strength for calculating wall depth = 1.00

## Parameters for undrained strata:

Minimum equivalent fluid density = 5.00 kN/m<sup>3</sup>  
Maximum depth of water filled tension crack = 0.00 m

## Bending moment and displacement calculation:

Method - Subgrade reaction model using Influence Coefficients  
Open Tension Crack analysis? - No  
Non-linear Modulus Parameter (L) = 10.00 m

## Boundary conditions:

Length of wall (normal to plane of analysis) = 20.00 m

Width of excavation on active side of wall = 20.00 m  
Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m  
Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

Stage no.	Stage description	Output options	Displacement	Active, Graph.	Bending mom.	Passive output	Shear force pressures
1	Change EI of wall to 44780kN.m <sup>2</sup> /m run	No	No	No			
2	Apply surcharge no.1 at elev. 75.00	No	No	No			
3	Excav. to elev. 71.15 on PASSIVE side	Yes	Yes	Yes			
4	Fill to elev. 71.50 on PASSIVE side	No	No	No			
5	Install strut no.1 at elev. 71.60	No	No	No			
6	Apply surcharge no.2 at elev. 71.50	No	No	No			
7	Apply water pressure profile no.1	No	No	No			
8	Change soil type 3 to soil type 2	No	No	No			
9	Change EI of wall to 31986kN.m <sup>2</sup> /m run	No	No	No			
10	Apply load no.1 at elev. 75.00	No	No	No			
*	Summary output	Yes	-	Yes			

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Units: kN, m

Stage No. 10 Apply load no.1 at elevation 75.00

## STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method

## Factor of safety on soil strength

FoS for toe elev. = 65.00 Toe elev. for FoS = 1.000

Stage	--- G.L. ---		Strut	Factor	Moment	Toe	Wall
No.	Act.	Pass.	Elev.	of Safety	equilib. at elev.	elev.	Penetr -ation
10	75.00	71.50	71.60	Conditions not suitable for FoS calc.			

## BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall

## Analysis options

Length of wall perpendicular to section = 20.00m

### Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
Passive side 20.00 from wall

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m	EI of wall kNm <sup>2</sup> /m
1	75.00	0.00	0.094	2.58E-02	55.0	-0.0	-55.0	31986
2	74.50	3.98	0.081	2.56E-02	56.0	27.6		31986
3	74.00	8.28	0.068	2.50E-02	59.1	56.4		31986
4	73.60	13.93	0.058	2.41E-02	63.5	80.9		31986
5	73.20	19.41	0.049	2.29E-02	70.2	107.5		31986
6	72.60	27.46	0.036	2.05E-02	84.2	153.5		31986
7	72.00	35.39	0.025	1.71E-02	103.1	208.5		31986
		38.24	0.025	1.71E-02	103.1	208.5		
8	71.60	46.44	0.018	1.42E-02	120.0	251.9	218.3	31986
		46.44	0.018	1.42E-02	-98.3	251.9		
9	71.50	50.14	0.017	1.34E-02	-93.4	243.5		31986
		25.14	0.017	1.34E-02	-93.4	243.5		
10	71.15	25.97	0.013	1.09E-02	-84.5	216.6		31986
11	71.00	25.98	0.011	9.96E-03	-80.6	206.1		31986
		16.12	0.011	9.96E-03	-80.6	206.1		
12	70.60	16.08	0.008	7.65E-03	-74.2	179.0		31986
13	70.20	11.50	0.005	5.71E-03	-68.7	152.6		31986
14	69.60	12.58	0.002	3.39E-03	-61.4	117.2		31986
15	69.00	17.37	0.001	1.71E-03	-52.4	82.9		31986
16	68.40	13.61	0.000	6.02E-04	-43.2	49.7		31986
17	67.80	22.90	-0.000	-1.38E-05	-32.2	23.5		31986
18	67.20	22.29	0.000	-2.67E-04	-18.6	6.7		31986
19	66.60	16.64	0.000	-3.11E-04	-7.0	-1.3		31986
20	66.00	9.05	0.000	-2.77E-04	0.7	-2.7		31986
21	65.50	-2.37	0.000	-2.51E-04	2.4	-1.1		31986
22	65.00	-7.27	0.001	-2.44E-04	0.0	0.0		--
At elev. 71.60 Strut force =				218.3 kN/strut =		218.3 kN/m run		

(continued)

Stage No.10 Apply load no.1 at elevation 75.00

Node no.	Y coord	ACTIVE side						Total earth pressure kN/m2	Soil stiffness kN/m <sup>3</sup>		
		Effective stresses									
		Water press. kN/m <sup>2</sup>	Vertic -al limit kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>					
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	2189		
2	74.50	0.00	10.82	3.98	33.10	3.98	3.98a	3.98a	2189		
3	74.00	0.00	22.50	8.28	68.85	8.28	8.28a	8.28a	2189		
4	73.60	4.00	26.99	9.93	82.59	9.93	13.93a	13.93a	2189		
5	73.20	8.00	31.01	11.41	94.89	11.41	19.41a	19.41a	2189		
6	72.60	14.00	36.57	13.46	111.90	13.46	27.46a	27.46a	2189		
7	72.00	20.00	41.81	15.39	127.95	15.39	35.39a	35.39a	2189		
		20.00	41.81	18.24	106.20	18.24	38.24a	38.24a	3941		
8	71.60	24.00	46.01	20.07	116.85	22.44	46.44	46.44	3941		
9	71.50	25.00	47.05	20.53	119.49	25.14	50.14	50.14	2531		
10	71.15	28.50	50.66	22.10	128.66	31.04	59.54	59.54	2531		
11	71.00	30.00	52.20	22.77	132.57	33.08	63.08	63.08	2531		
		30.00	52.20	18.91	147.12	28.59	58.59	58.59	4950		
12	70.60	34.00	56.27	20.63	157.91	34.72	68.72	68.72	5170		
13	70.20	38.00	60.31	22.34	168.61	38.57	76.57	76.57	5389		
14	69.60	44.00	66.33	24.88	184.54	55.39	99.39	99.39	5719		
15	69.00	50.00	72.30	27.40	200.35	78.21	128.21	128.21	6048		
16	68.40	56.00	78.23	29.91	216.06	92.90	148.90	148.90	6377		
17	67.80	62.00	84.13	32.40	231.69	101.64	163.64	163.64	6707		
18	67.20	68.00	90.01	34.89	247.26	106.72	174.72	174.72	7036		
19	66.60	74.00	95.88	37.36	262.78	110.02	184.02	184.02	7366		
20	66.00	80.00	101.73	39.83	278.27	112.71	192.71	192.71	7695		
21	65.50	85.00	106.59	41.89	291.15	112.49	197.49	197.49	26102		
22	65.00	90.00	111.45	43.94	304.02	115.59	205.59	205.59	27001		

Node no.	Y coord	PASSIVE side						Total earth pressure kN/m2	Soil stiffness kN/m <sup>3</sup>		
		Effective stresses									
		Water press. kN/m <sup>2</sup>	Vertic -al limit kN/m <sup>2</sup>	Active limit kN/m <sup>2</sup>	Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>					
1	75.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
2	74.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
3	74.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
4	73.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
5	73.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
6	72.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
7	72.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
8	71.60	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
9	71.50	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0		
		25.00	0.00	0.00	0.00	0.00	25.00	25.00	2531		
10	71.15	28.50	3.50	1.53	8.89	5.07	33.57	33.57	2531		
11	71.00	30.00	5.00	2.18	12.69	7.10	37.10	37.10	2531		
		30.00	5.00	0.00	22.16	12.48	42.48	42.48	4950		
12	70.60	34.00	8.99	0.67	32.73	18.65	52.65	52.65	5170		
13	70.20	38.00	12.98	2.35	43.30	27.07	65.07	65.07	5389		
14	69.60	44.00	18.95	4.87	59.09	42.81	86.81	86.81	5719		
15	69.00	50.00	24.89	7.38	74.82	60.84	110.84	110.84	6048		
16	68.40	56.00	30.80	9.88	90.46	79.29	135.29	135.29	6377		
17	67.80	62.00	36.67	12.36	106.02	78.74	140.74	140.74	6707		
18	67.20	68.00	42.52	14.83	121.50	84.43	152.43	152.43	7036		
19	66.60	74.00	48.34	17.29	136.91	93.39	167.39	167.39	7366		
20	66.00	80.00	54.14	19.73	152.26	103.66	183.66	183.66	7695		
21	65.50	85.00	58.96	21.77	165.03	114.86	199.86	199.86	26102		
22	65.00	90.00	63.77	23.80	177.77	122.86	212.86	212.86	27001		

Run ID. Section 5 CP321-352 ULS  
Hampstead Green  
Contig wall

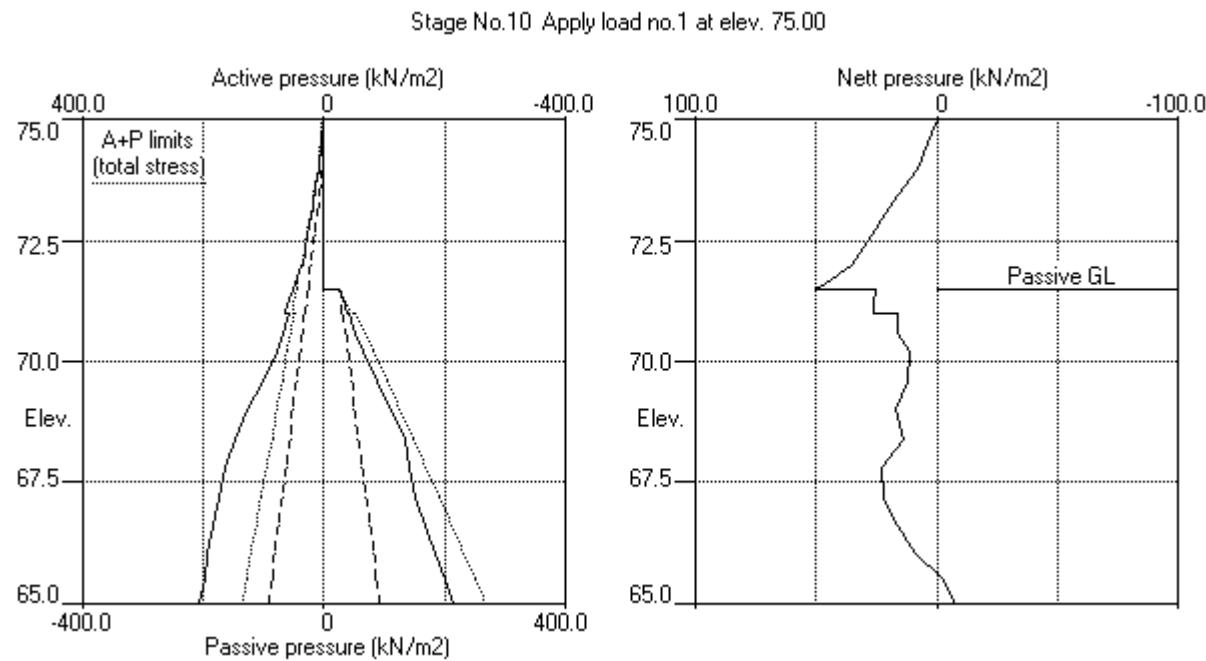
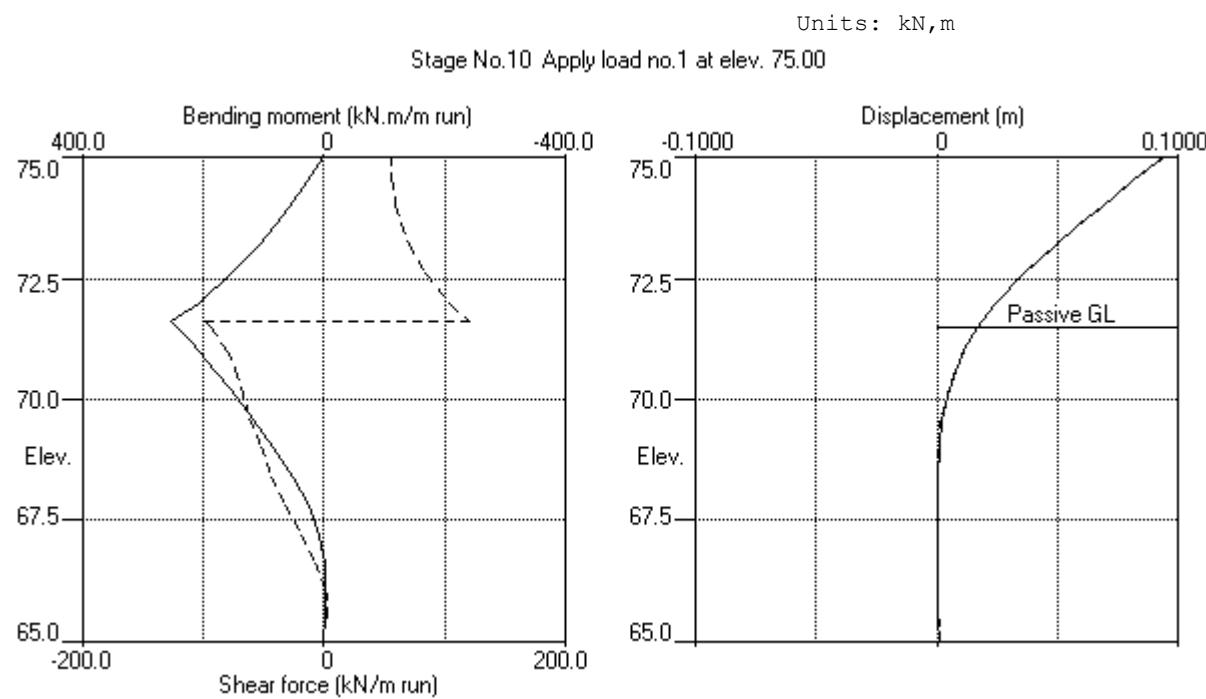
| Sheet No.  
| Date:25-04-2016  
| Checked :

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(continued)

Stage No.10 Apply load no.1 at elevation 75.00  
Note: 38.24a Soil pressure at active limit  
123.45p Soil pressure at passive limit

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Contig wall

Sheet No.  
Job No. 16-0036  
Made by : KK  
Date: 25-04-2016  
Checked :



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 Data filename/Run ID: Section 5 CP321-352 ULS |  
 Hampstead Green | Date: 25-04-2016  
 Contig wall | Checked :  
 -----

Units: kN,m

**Summary of results**

**STABILITY ANALYSIS of Fully Embedded Wall according to Strength Factor method**  
 Factor of safety on soil strength

Stage No.	--- G.L. ---		Strut Elev.	FoS for toe elev. =	Toe elev. for FoS =	Wall Penetr -ation
	Act.	Pass.		Factor of equilib.	Moment Safety at elev.	Toe elev.
1	75.00	75.00	Cant.	Conditions not suitable for FoS calc.		
2	75.00	75.00		No analysis at this stage		
3	75.00	71.15	Cant.	1.403	65.75	67.62 3.53
4	75.00	71.50	Cant.	1.485	65.79	67.88 3.62
5	75.00	71.50		No analysis at this stage		
6	75.00	71.50	71.60	Conditions not suitable for FoS calc.		
7	75.00	71.50		No analysis at this stage		
8	75.00	71.50		No analysis at this stage		
9	75.00	71.50	71.60	Conditions not suitable for FoS calc.		
10	75.00	71.50	71.60	Conditions not suitable for FoS calc.		

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 Contig wall

	Sheet No.
	Job No. 16-0036
	Made by : KK
	Date: 25-04-2016
	Checked :

---

Units: kN,m

### **Summary of results**

#### **BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

##### **Analysis options**

Length of wall perpendicular to section = 20.00m

Subgrade reaction model - Boussinesq Influence coefficients

Soil deformations are elastic until the active or passive limit is reached

Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

#### **Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement		Bending moment		Shear force	
		maximum m	minimum m	maximum kN.m/m	minimum kN.m/m	maximum kN/m	minimum kN/m
1	75.00	0.094	0.000	0.0	-0.0	55.0	0.0
2	74.50	0.081	0.000	27.6	0.0	56.0	0.0
3	74.00	0.068	0.000	56.4	0.0	59.1	0.0
4	73.60	0.058	0.000	80.9	0.0	63.5	0.0
5	73.20	0.049	0.000	107.5	0.0	70.2	0.0
6	72.60	0.036	0.000	153.5	0.0	84.2	0.0
7	72.00	0.025	0.000	208.5	0.0	103.1	0.0
8	71.60	0.018	0.000	251.9	0.0	120.0	-98.3
9	71.50	0.017	0.000	243.5	0.0	55.0	-93.4
10	71.15	0.014	0.000	216.6	0.0	63.3	-84.5
11	71.00	0.013	0.000	206.1	0.0	66.9	-80.6
12	70.60	0.010	0.000	179.0	0.0	43.3	-74.2
13	70.20	0.008	0.000	152.6	0.0	16.6	-68.7
14	69.60	0.005	0.000	127.0	0.0	0.0	-61.4
15	69.00	0.003	0.000	106.4	0.0	0.0	-52.4
16	68.40	0.002	0.000	73.4	0.0	0.0	-52.5
17	67.80	0.002	-0.000	43.4	0.0	0.0	-43.5
18	67.20	0.001	-0.000	21.2	0.0	0.0	-29.8
19	66.60	0.002	-0.000	8.0	-1.3	0.0	-16.5
20	66.00	0.002	-0.000	2.5	-2.7	0.7	-6.5
21	65.50	0.002	0.000	0.7	-1.1	2.4	-2.8
22	65.00	0.002	0.000	0.0	0.0	0.0	-0.0

#### **Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	maximum kN.m/m	elev. 75.00	minimum 0.0	elev. 75.00	maximum kN/m	elev. 75.00	minimum 0.0	elev. 75.00
1	0.0	75.00	0.0	75.00	0.0	75.00	0.0	75.00
2	No calculation at this stage							
3	121.8	69.60	-0.0	65.50	66.3	71.00	-50.3	68.40
4	123.1	69.60	-0.0	65.50	66.8	71.00	-50.8	68.40
5	No calculation at this stage							
6	127.3	70.20	-0.1	65.50	66.9	71.00	-52.5	68.40
7	No calculation at this stage							
8	No calculation at this stage							
9	86.4	70.20	0.0	75.00	67.3	71.60	-27.3	68.40
10	251.9	71.60	-2.7	66.00	120.0	71.60	-98.3	71.60

**Summary of results (continued)**

**Maximum and minimum displacement at each stage**

Stage no.	Displacement maximum	elev.	Displacement minimum	elev.	Stage description
	m		m		
1	0.000	75.00	0.000	75.00	Change EI of wall to 44780kN.m <sup>2</sup> /m run
2	No calculation at this stage				Apply surcharge no.1 at elev. 75.00
3	0.049	75.00	0.000	75.00	Excav. to elev. 71.15 on PASSIVE side
4	0.049	75.00	0.000	75.00	Fill to elev. 71.50 on PASSIVE side
5	No calculation at this stage				Install strut no.1 at elev. 71.60
6	0.048	75.00	-0.000	67.20	Apply surcharge no.2 at elev. 71.50
7	No calculation at this stage				Apply water pressure profile no.1
8	No calculation at this stage				Change soil type 3 to soil type 2
9	0.052	75.00	0.000	75.00	Change EI of wall to 31986kN.m <sup>2</sup> /m run
10	0.094	75.00	-0.000	67.80	Apply load no.1 at elev. 75.00

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 ---	
	at elev.	71.60
	kN/m run	kN/strut
6	slack	slack
9	73.06	73.06
10	218.29	218.29

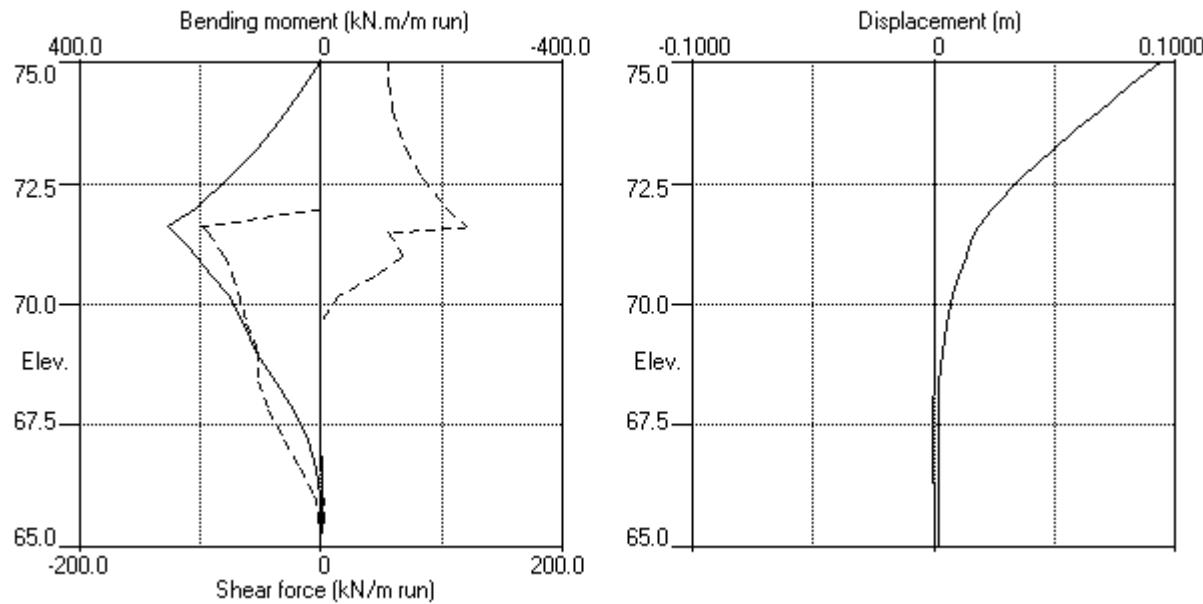
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load.  
Force components are listed in the detailed results for individual stages.

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Program: WALLAP Version 6.05 Revision A45.B58.R49  
Licensed from GEOSOLVE  
Data filename/Run ID: Section 5 CP321-352 ULS  
Hampstead Green  
Contig wall

| Sheet No.  
| Job No. 16-0036  
| Made by : KK  
|  
| Date: 25-04-2016  
Checked :

Units: kN,m

Bending moment, shear force, displacement envelopes



## **Appendix D**

### **Structural Analysis**

TITLE or DESCRIPTION:	ORIG by	Date	VERIF	Date	Ref. No.	SHEET No
	KK				16-0036	of

REFERENCE	Rev:	
EC2	Bending and Axial Force to EN 1992-1-1:2004 (EC2) - Secant Wall	
	Circular Sections (Cast In-situ)	
4.4.1.3(4)	Pile section	
	pile diameter = <b>400</b> mm	
	Pile spacing = <b>550</b> mm	
	design pile diameter h = <b>380</b> mm	
	Ac = <b>113411</b> mm <sup>2</sup>	
	cover <sup>1</sup> c <sub>nom</sub> = <b>65</b> mm	k <sub>2</sub> = <b>75</b> mm
	cage diameter d = <b>214</b> mm	
	ratio d/h = <b>0.6</b>	
	f <sub>ck</sub> = <b>32</b> MPa	γ <sub>c</sub> = <b>1.65</b>
	f <sub>yk</sub> = <b>500</b> MPa	α <sub>cc</sub> = <b>0.85</b> {NA 3.1.6 (1)}
		γ <sub>s</sub> = <b>1.15</b>
	Design Actions on pile	
	Actions N = <b>0</b> kN	
	Factored Actions N = <b>796</b> kN	
	Wallap shear = <b>81</b> kN/m	
	Shear V <sub>Ed</sub> = <b>44.55</b> kN	BM/SF factor = <b>1.0</b>
	Ult Shear V <sub>Ed</sub> = <b>44.55</b> kN	
	Wallap moment = <b>128</b> kNm/m	
	Induced Moment M <sub>i</sub> = <b>70.4</b> kNm	
	Applied Moment M <sub>Ed</sub> = <b>70</b> kNm	
	Σ Moments M = <b>70</b> kNm	
	Factored Ult M = <b>70</b> kNm	
	Using IstructE design charts for circular columns:-	
	M/h <sup>3</sup> f <sub>ck</sub> = <b>0.047</b> (also checked for M/h3=0.0 for zero vertical load)	
	Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.00</b>	
	Factored Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.20</b>	
	therefore from charts;	
	ρ f <sub>yk</sub> / f <sub>ck</sub> = <b>0.2</b> From charts	
	ρ = <b>4A<sub>st</sub> / π.h<sup>2</sup></b>	
	therefore, adopt greater of:	
	Area of main steel A <sub>st</sub> = <b>1234</b> mm <sup>2</sup>	
	main bar dia = <b>20</b> mm	
	no. main bars = <b>6</b> no.	
	helical dia = <b>8</b> mm	
	Area of main steel, A <sub>st</sub> = <b>1885</b> mm <sup>2</sup>	
	Bar spacing (face to face) = <b>92</b> mm	

PROJECT: <b>Hampstead Green</b>		<b>Rock &amp; Alluvium</b> 																																																																				
TITLE or DESCRIPTION:	Section 1	ORIG by	Date	VERIF	Date	Ref. No	SHEET No																																																															
		KK				16-0036	of																																																															
REFERENCE	<b>[Rev:</b>																																																																					
EC2	<b>Shear to EN 1992-1-1:2004 (EC2) - Secant Wall</b>						<b>Circular Sections (Cast In-situ) using helical reinforcement</b>																																																															
4.4.1.3(4)	<p><u>Pile section</u></p> <table> <tr><td>pile dia</td><td>=</td><td>400</td><td>mm</td></tr> <tr><td>Pile spacing</td><td>=</td><td>550</td><td>mm</td></tr> <tr><td>pile diameter dnom</td><td>=</td><td>380</td><td>mm</td></tr> <tr><td>Ac</td><td>=</td><td>113411</td><td>mm<sup>2</sup></td></tr> <tr><td>cover c<sub>nom</sub></td><td>=</td><td>65</td><td>mm</td></tr> <tr><td>main bar dia</td><td>=</td><td>20</td><td>mm</td></tr> <tr><td>no. main bars</td><td>=</td><td>6</td><td>no.</td></tr> <tr><td>helical dia</td><td>=</td><td>8</td><td>mm</td></tr> <tr><td>d</td><td>=</td><td>252</td><td>mm</td></tr> <tr><td>f<sub>ck</sub></td><td>=</td><td>32</td><td>MPa</td></tr> <tr><td>f<sub>yk</sub></td><td>=</td><td>500</td><td>MPa</td></tr> <tr><td>Wallap shear</td><td>=</td><td>81</td><td>kN/m</td></tr> <tr><td>Ult V<sub>Ed</sub></td><td>=</td><td>44.55</td><td>kN</td></tr> <tr><td>Ult V<sub>Ed</sub></td><td>=</td><td><b>44.55</b></td><td>kN</td></tr> <tr><td>Actions N</td><td>=</td><td></td><td>kN</td></tr> <tr><td>factored actions N<sub>Ed</sub></td><td>=</td><td></td><td>kN</td></tr> </table>	pile dia	=	400	mm	Pile spacing	=	550	mm	pile diameter dnom	=	380	mm	Ac	=	113411	mm <sup>2</sup>	cover c <sub>nom</sub>	=	65	mm	main bar dia	=	20	mm	no. main bars	=	6	no.	helical dia	=	8	mm	d	=	252	mm	f <sub>ck</sub>	=	32	MPa	f <sub>yk</sub>	=	500	MPa	Wallap shear	=	81	kN/m	Ult V <sub>Ed</sub>	=	44.55	kN	Ult V <sub>Ed</sub>	=	<b>44.55</b>	kN	Actions N	=		kN	factored actions N <sub>Ed</sub>	=		kN	<p><math>k_2 = 75</math> mm [NA.4.4.1.3 (4)]</p> <p><math>\gamma_c = 1.5</math> (This is adjusted by <math>K_f=1.1</math> [2.4.2.5 (2)] to give 1.65)</p> <p><math>\gamma_c = 1.65</math>   <math>\alpha_{cc} = 0.85</math> [NA. 3.1.6 (1)]</p> <p><math>\gamma_s = 1.15</math></p> <p>SF factor <b>1.0</b></p>				
pile dia	=	400	mm																																																																			
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Actions N	=		kN																																																																			
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6.2.2	Check requirement for shear reinforcement																																																																					
	$V_{Rd,c} = [C_{Rd,c}k(100\rho_1 f_{ck})^{1/3} + k_1 \sigma_{cp}] b_w d$ with minimum $= (\gamma_{min} + k_1 \sigma_{cp}) b_w d$ $V_{min} = 0.035k^{3/2}f_{ck}^{1/2}$ <b>0.51497585</b>						$CR_{d,c} = 0.18 / \gamma_c$ <b>0.11</b> $k = 1 + (200/d)^{1/2}$ <b>1.89</b> $\leq 2.0$ $\rho_1 = A_s/b_w d$ <b>0.01</b> $\leq 0.02$ $\sigma_{cp} = N_{ed}/A_c$ <b>0</b> $< 0.2f_{cd}$ $k_1 = 0.15$ [NA.6.2.2(1)]																																																															
	$V_{Rd,c} = 49$ kN Is $V_{Rd,c} > V_{Ed}$ => <b>YES</b> Action: <b>No shear links needed - provide nominal links as req'd</b>																																																																					
6.2.3	Design Shear Reinforcement																																																																					
6.2.3 (3) exp 6.9	Check concrete strut capacity at Cot $\theta = 2.5$ :- $V_{Rd,max} = \alpha_{cw} \cdot b_w \cdot z \cdot v_1 \cdot f_{cd} / (\text{Cot}\theta + \tan\theta)$ (6.9) $V_{Rd,max} = 297$ kN						$\cot\theta = 2$ $\tan\theta = 0.5$ $\alpha_{cw} = 1$ [NA.6.2.3(3)] $z = 0.9d$ <b>227</b> mm $v_1 = 0.6 (1 - (f_{ck}/250))$ <b>0.52</b> [6.6N]																																																															
	Is $V_{Rd,max} > V_{Ed}$ => <b>NA</b> Action: Calculation for strut inclination:- $\theta = 0.5 \cdot \sin^{-1} [(6.54 \cdot V_{Ed}) / (b_w \cdot d \cdot (1 - f_{ck}/250) \cdot f_{ck})]$ $\theta = NA$ rad $\cot\theta = 2.5 > 1.0$																																																																					
	Calculate shear reinforcement spacing after Turmo et al (2008);-																																																																					
	$V_{Rd,s} = z \cdot \cot\theta \cdot (A_\phi / 0.5s) \cdot f_{ywd} \cdot 0.85$ $s = 2 \cdot ([z \cdot \cot\theta \cdot A_\phi \cdot f_{ywd} \cdot 0.85] / V_{Rd,s})$ $= 378$ mm						$A_{sw} = 50.3$ mm <sup>2</sup> $f_{ywd} = 435$ MPa																																																															
	Check maximum shear link spacing:- Is $s_{l,max} > 0.75d$ <b>YES</b>																																																																					
	<table border="1"> <tr><td>Provide</td><td><b>8</b></td><td>mm</td><td>helical at nominal pitch</td><td><b>185</b></td><td>mm</td></tr> </table>						Provide	<b>8</b>	mm	helical at nominal pitch	<b>185</b>	mm																																																										
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	Turo, J, et al. Shear truss analogy for concrete members of solid and hollow circular cross section. <b>Eng. Struc.</b> (2008)																																																																					

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	Circular Sections (Cast In-situ)	
4.4.1.3(4)	Pile section	
	pile diameter = <b>400</b> mm	
	Pile spacing = <b>550</b> mm	
	design pile diameter h = <b>380</b> mm	
	Ac = <b>113411</b> mm <sup>2</sup>	
	cover <sup>1</sup> c <sub>nom</sub> = <b>65</b> mm	k <sub>2</sub> = <b>75</b> mm
	cage diameter d = <b>209</b> mm	
	ratio d/h = <b>0.6</b>	
	f <sub>ck</sub> = <b>32</b> MPa	γ <sub>c</sub> = <b>1.65</b>
	f <sub>yk</sub> = <b>500</b> MPa	α <sub>cc</sub> = <b>0.85</b> [NA 3.1.6 (1)]
		γ <sub>s</sub> = <b>1.15</b>
	Design Actions on pile	
	Actions N = <b>0</b> kN	
	Factored Actions N = <b>796</b> kN	
	Wallap shear = <b>124</b> kN/m	
	Shear V <sub>Ed</sub> = <b>68.2</b> kN	BM/SF factor = <b>1.0</b>
	Ult Shear V <sub>Ed</sub> = <b>68.2</b> kN	
	Wallap moment = <b>239</b> kNm/m	
	Induced Moment M <sub>i</sub> = <b>131.45</b> kNm	
	Applied Moment M <sub>Ed</sub> = <b>0</b> kNm	
	Σ Moments M = <b>131</b> kNm	
	Factored Ult M = <b>131</b> kNm	
	Using IstructE design charts for circular columns:-	
	M/h <sup>3</sup> f <sub>ck</sub> = <b>0.088</b> (also checked for M/h3=0.0 for zero vertical load)	
	Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.00</b>	
	Factored Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.20</b>	
	therefore from charts;	
	ρ f <sub>yk</sub> / f <sub>ck</sub> = <b>0.43</b> From charts	
	ρ = <b>4A<sub>st</sub> / π.h<sup>2</sup></b>	
	therefore, adopt greater of:	
	Area of main steel A <sub>st</sub> = <b>2653</b> mm <sup>2</sup>	
	main bar dia = <b>25</b> mm	
	no. main bars = <b>6</b> no.	
	helical dia = <b>8</b> mm	
	Area of main steel, A <sub>st</sub> = <b>2945</b> mm <sup>2</sup>	
	Bar spacing (face to face) = <b>84</b> mm	

PROJECT: <b>Hampstead Green</b>		<b>Rock &amp; Alluvium</b> 																																																																
TITLE or DESCRIPTION:	Section 2	ORIG by	Date	VERIF	Date	Ref. No	SHEET No																																																											
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pile dia	=	400	mm																																																															
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6.2.2	<p>Check requirement for shear reinforcement</p> <table> <tr><td>V<sub>Rd,c</sub></td><td>=</td><td><math>[C_{Rd,c}k(100\rho_1 f_{ck})^{1/3} + k_1 \sigma_{cp}] b_w d</math></td><td>CRd,c</td><td>=</td><td>0.18 / <math>\gamma_c</math></td><td>0.11</td></tr> <tr><td>with minimum</td><td>=</td><td><math>(v_{min} + k_1 \sigma_{cp}) b_w d</math></td><td>k</td><td>=</td><td><math>1 + (200/d)^{1/2}</math></td><td>1.90 <math>\leq 2.0</math></td></tr> <tr><td>v<sub>min</sub></td><td>=</td><td><math>0.035k^{3/2}f_{ck}^{1/2}</math></td><td><math>\rho_1</math></td><td>=</td><td><math>A_{si}/b_w d</math></td><td>0.02 <math>\leq 0.02</math></td></tr> <tr><td></td><td></td><td>0.51730105</td><td><math>\sigma_{cp}</math></td><td>=</td><td><math>N_{ed}/A_c</math></td><td><math>0 &lt; 0.2f_{cd}</math></td></tr> <tr><td></td><td></td><td></td><td>k<sub>1</sub></td><td>=</td><td>0.15</td><td>[NA.6.2.2(1)]</td></tr> <tr><td></td><td></td><td>V<sub>Rd,c</sub> = 49 kN</td><td></td><td></td><td></td><td></td></tr> </table>	V <sub>Rd,c</sub>	=	$[C_{Rd,c}k(100\rho_1 f_{ck})^{1/3} + k_1 \sigma_{cp}] b_w d$	CRd,c	=	0.18 / $\gamma_c$	0.11	with minimum	=	$(v_{min} + k_1 \sigma_{cp}) b_w d$	k	=	$1 + (200/d)^{1/2}$	1.90 $\leq 2.0$	v <sub>min</sub>	=	$0.035k^{3/2}f_{ck}^{1/2}$	$\rho_1$	=	$A_{si}/b_w d$	0.02 $\leq 0.02$			0.51730105	$\sigma_{cp}$	=	$N_{ed}/A_c$	$0 < 0.2f_{cd}$				k <sub>1</sub>	=	0.15	[NA.6.2.2(1)]			V <sub>Rd,c</sub> = 49 kN					Is V <sub>Rd,c</sub> > V <sub>Ed</sub> => NO Action: <b>Design of shear reinforcement required</b>																						
V <sub>Rd,c</sub>	=	$[C_{Rd,c}k(100\rho_1 f_{ck})^{1/3} + k_1 \sigma_{cp}] b_w d$	CRd,c	=	0.18 / $\gamma_c$	0.11																																																												
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6.2.3	<p>Design Shear Reinforcement</p> <p>Check concrete strut capacity at Cot θ = 2.5 :-</p> <table> <tr><td>V<sub>Rd,max</sub></td><td>=</td><td><math>\alpha_{cw} \cdot b_w \cdot z \cdot v_1 \cdot f_{cd} / (\cot\theta + \tan\theta)</math></td><td>(6.9)</td><td>cot θ</td><td>=</td><td>2</td></tr> <tr><td>V<sub>Rd,max</sub></td><td>=</td><td>293 kN</td><td></td><td>tan θ</td><td>=</td><td>0.5</td></tr> <tr><td></td><td></td><td></td><td></td><td><math>\alpha_{cw}</math></td><td>=</td><td>1</td></tr> <tr><td></td><td></td><td></td><td></td><td>z</td><td>=</td><td>0.9d 224 mm</td></tr> <tr><td></td><td></td><td></td><td></td><td>v<sub>1</sub></td><td>=</td><td>0.6 (1-fck/250) 0.52 [6.6N]</td></tr> </table>	V <sub>Rd,max</sub>	=	$\alpha_{cw} \cdot b_w \cdot z \cdot v_1 \cdot f_{cd} / (\cot\theta + \tan\theta)$	(6.9)	cot θ	=	2	V <sub>Rd,max</sub>	=	293 kN		tan θ	=	0.5					$\alpha_{cw}$	=	1					z	=	0.9d 224 mm					v <sub>1</sub>	=	0.6 (1-fck/250) 0.52 [6.6N]	Is V <sub>Rd,max</sub> > V <sub>Ed</sub> => YES Action: <b>Calculate link spacing</b>																													
V <sub>Rd,max</sub>	=	$\alpha_{cw} \cdot b_w \cdot z \cdot v_1 \cdot f_{cd} / (\cot\theta + \tan\theta)$	(6.9)	cot θ	=	2																																																												
V <sub>Rd,max</sub>	=	293 kN		tan θ	=	0.5																																																												
				$\alpha_{cw}$	=	1																																																												
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				v <sub>1</sub>	=	0.6 (1-fck/250) 0.52 [6.6N]																																																												
6.2.3 (3) exp 6.9	<p>Calculation for strut inclination:-</p> $\theta = 0.5 \cdot \sin^{-1} [(6.54 \cdot V_{Ed}) / (b_w \cdot d \cdot (1 - f_{ck}/250) \cdot f_{ck})]$ $\theta = NA \text{ rad}$	$\cot \theta = 2.5 > 1.0$																																																																
	<p>Calculate shear reinforcement spacing after Turmo et al (2008);-</p> <table> <tr><td>V<sub>Rd,s</sub></td><td>=</td><td><math>z \cdot \cot \theta \cdot (A_\phi / 0.5s) \cdot f_{ywd} \cdot 0.85</math></td><td>A<sub>sw</sub></td><td>=</td><td>50.3 mm<sup>2</sup></td></tr> <tr><td>s</td><td>=</td><td><math>2 \cdot ([z \cdot \cot \theta \cdot A_\phi \cdot f_{ywd} \cdot 0.85] / V_{Rd,s})</math></td><td>f<sub>ywd</sub></td><td>=</td><td>435 MPa</td></tr> <tr><td></td><td>=</td><td>244 mm</td><td></td><td></td><td></td></tr> </table>	V <sub>Rd,s</sub>	=	$z \cdot \cot \theta \cdot (A_\phi / 0.5s) \cdot f_{ywd} \cdot 0.85$	A <sub>sw</sub>	=	50.3 mm <sup>2</sup>	s	=	$2 \cdot ([z \cdot \cot \theta \cdot A_\phi \cdot f_{ywd} \cdot 0.85] / V_{Rd,s})$	f <sub>ywd</sub>	=	435 MPa		=	244 mm				Check maximum shear link spacing:- is s <sub>l,max</sub> > 0.75d YES																																														
V <sub>Rd,s</sub>	=	$z \cdot \cot \theta \cdot (A_\phi / 0.5s) \cdot f_{ywd} \cdot 0.85$	A <sub>sw</sub>	=	50.3 mm <sup>2</sup>																																																													
s	=	$2 \cdot ([z \cdot \cot \theta \cdot A_\phi \cdot f_{ywd} \cdot 0.85] / V_{Rd,s})$	f <sub>ywd</sub>	=	435 MPa																																																													
	=	244 mm																																																																
	<table border="1"> <tr><td>Provide</td><td>8</td><td>mm</td><td>helical at nominal pitch</td><td>185</td><td>mm</td></tr> </table>	Provide	8	mm	helical at nominal pitch	185	mm	Turo, J, et al. Shear truss analogy for concrete members of solid and hollow circular cross section. <b>Eng. Struc.</b> (2008)																																																										
Provide	8	mm	helical at nominal pitch	185	mm																																																													

TITLE or DESCRIPTION:	ORIG by	Date	VERIF	Date	Ref. No.	SHEET No
	KK				16-0036	of

REFERENCE	Rev:	
EC2	Bending and Axial Force to EN 1992-1-1:2004 (EC2) - Secant Wall	
	Circular Sections (Cast In-situ)	
4.4.1.3(4)	Pile section	
	pile diameter = <b>400</b> mm	
	Pile spacing = <b>550</b> mm	
	design pile diameter h = <b>380</b> mm	
	Ac = <b>113411</b> mm <sup>2</sup>	
	cover <sup>1</sup> c <sub>nom</sub> = <b>65</b> mm	k <sub>2</sub> = <b>75</b> mm
	cage diameter d = <b>214</b> mm	
	ratio d/h = <b>0.6</b>	
	f <sub>ck</sub> = <b>32</b> MPa	γ <sub>c</sub> = <b>1.65</b>
	f <sub>yk</sub> = <b>500</b> MPa	γ <sub>s</sub> = <b>1.15</b>
	a <sub>cc</sub> = <b>0.85</b> [NA 3.1.6 (1)}	
	Design Actions on pile	
	Actions N = <b>0</b> kN	
	Factored Actions N = <b>796</b> kN	
	Wallap shear = <b>112</b> kN/m	
	Shear V <sub>Ed</sub> = <b>61.6</b> kN	BM/SF factor <b>1.0</b>
	Ult Shear V <sub>Ed</sub> = <b>61.6</b> kN	
	Wallap moment = <b>193</b> kNm/m	
	Induced Moment M <sub>i</sub> = <b>106.15</b> kNm	
	Applied Moment M <sub>Ed</sub> = <b>106</b> kNm	
	Σ Moments M = <b>106</b> kNm	
	Factored Ult M = <b>106</b> kNm	
	Using IstructE design charts for circular columns:-	
	M/h <sup>3</sup> f <sub>ck</sub> = <b>0.07</b> (also checked for M/h3=0.0 for zero vertical load)	
	Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.00</b>	
	Factored Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.20</b>	
	therefore from charts;	
	ρ f <sub>yk</sub> / f <sub>ck</sub> = <b>0.3</b>	From charts
	ρ = <b>4A<sub>st</sub> / π.h<sup>2</sup></b>	
	therefore, adopt greater of:	
	Area of main steel A <sub>st</sub> = <b>1851</b> mm <sup>2</sup>	
	main bar dia = <b>20</b> mm	
	no. main bars = <b>6</b> no.	
	helical dia = <b>8</b> mm	
	Area of main steel, A <sub>st</sub> = <b>1885</b> mm <sup>2</sup>	
	Bar spacing (face to face) = <b>92</b> mm	

PROJECT: <b>Hampstead Green</b>		<b>Rock &amp; Alluvium</b> 																																																																
TITLE or DESCRIPTION:	Section 3	ORIG by	Date	VERIF	Date	Ref. No	SHEET No																																																											
		KK				16-0036	of																																																											
REFERENCE	<b>[Rev:</b>																																																																	
EC2	<b>Shear to EN 1992-1-1:2004 (EC2) - Secant Wall</b>						<b>Circular Sections (Cast In-situ) using helical reinforcement</b>																																																											
4.4.1.3(4)	<p><u>Pile section</u></p> <table> <tr><td>pile dia</td><td>=</td><td>400</td><td>mm</td></tr> <tr><td>Pile spacing</td><td>=</td><td>550</td><td>mm</td></tr> <tr><td>pile diameter dnom</td><td>=</td><td>380</td><td>mm</td></tr> <tr><td>Ac</td><td>=</td><td>113411</td><td>mm<sup>2</sup></td></tr> <tr><td>cover c<sub>nom</sub></td><td>=</td><td>65</td><td>mm</td></tr> <tr><td>main bar dia</td><td>=</td><td>20</td><td>mm</td></tr> <tr><td>no. main bars</td><td>=</td><td>6</td><td>no.</td></tr> <tr><td>helical dia</td><td>=</td><td>8</td><td>mm</td></tr> <tr><td>d</td><td>=</td><td>252</td><td>mm</td></tr> <tr><td>f<sub>ck</sub></td><td>=</td><td>32</td><td>MPa</td></tr> <tr><td>f<sub>yk</sub></td><td>=</td><td>500</td><td>MPa</td></tr> <tr><td>Wallap shear</td><td>=</td><td>112</td><td>kN/m</td></tr> <tr><td>Ult V<sub>Ed</sub></td><td>=</td><td>61.6</td><td>kN</td></tr> <tr><td>Actions N</td><td>=</td><td></td><td>kN</td></tr> <tr><td>factored actions N<sub>Ed</sub></td><td>=</td><td></td><td>kN</td></tr> </table>	pile dia	=	400	mm	Pile spacing	=	550	mm	pile diameter dnom	=	380	mm	Ac	=	113411	mm <sup>2</sup>	cover c <sub>nom</sub>	=	65	mm	main bar dia	=	20	mm	no. main bars	=	6	no.	helical dia	=	8	mm	d	=	252	mm	f <sub>ck</sub>	=	32	MPa	f <sub>yk</sub>	=	500	MPa	Wallap shear	=	112	kN/m	Ult V <sub>Ed</sub>	=	61.6	kN	Actions N	=		kN	factored actions N <sub>Ed</sub>	=		kN	$k_2 = 75 \text{ mm}$ [NA.4.4.1.3 (4)]		$\gamma_c = 1.5$ (This is adjusted by K <sub>f</sub> =1.1 [2.4.2.5 (2)] to give 1.65)		
pile dia	=	400	mm																																																															
Pile spacing	=	550	mm																																																															
pile diameter dnom	=	380	mm																																																															
Ac	=	113411	mm <sup>2</sup>																																																															
cover c <sub>nom</sub>	=	65	mm																																																															
main bar dia	=	20	mm																																																															
no. main bars	=	6	no.																																																															
helical dia	=	8	mm																																																															
d	=	252	mm																																																															
f <sub>ck</sub>	=	32	MPa																																																															
f <sub>yk</sub>	=	500	MPa																																																															
Wallap shear	=	112	kN/m																																																															
Ult V <sub>Ed</sub>	=	61.6	kN																																																															
Actions N	=		kN																																																															
factored actions N <sub>Ed</sub>	=		kN																																																															
6.2.2	<p>Check requirement for shear reinforcement</p> $V_{Rd,c} = [C_{Rd,c}k(100\rho_1 f_{ck})^{1/3} + k_1 \sigma_{cp}] b_w d$ with minimum $= (\nu_{min} + k_1 \sigma_{cp}) b_w d$	$CR_{d,c} = 0.18 / \gamma_c$ 0.11 $k = 1 + (200/d)^{1/2}$ 1.89 <=2.0 $\rho_1 = A_{si}/b_w d$ 0.01 <=0.02 $\sigma_{cp} = N_{ed}/A_c$ 0 < 0.2f <sub>cd</sub> $k_1 = 0.15$ [NA.6.2.2(1)]																																																																
	$V_{Rd,c} = 49 \text{ kN}$																																																																	
6.2.3	Is $V_{Rd,c} > V_{Ed}$ => NO Action: <b>Design of shear reinforcement required</b>																																																																	
6.2.3 (3) exp 6.9	<p>Design Shear Reinforcement</p> <p>Check concrete strut capacity at Cot θ = 2.5 :-</p> $V_{Rd,max} = \alpha_{cw} \cdot b_w \cdot z \cdot v_1 \cdot f_{cd} / (\text{Cot}\theta + \tan\theta)$ (6.9)	$\cot\theta = 2$ $\tan\theta = 0.5$ $\alpha_{cw} = 1$ $z = 0.9d$ 227 mm $v_1 = 0.6 (1 - (f_{ck}/250))$ 0.52 [6.6N]		[NA.6.2.3(3)]																																																														
	Is $V_{Rd,max} > V_{Ed}$ => YES Action: <b>Calculate link spacing</b>																																																																	
	Calculation for strut inclination:- $\theta = 0.5 \cdot \sin^{-1} [(6.54 \cdot V_{Ed}) / (b_w \cdot d \cdot (1 - f_{ck}/250) \cdot f_{ck})]$ $\theta = \text{NA rad}$	$\cot\theta = 2.5 > 1.0$																																																																
	Calculate shear reinforcement spacing after Turmo et al (2008);-																																																																	
	$V_{Rd,s} = z \cdot \cot\theta \cdot (A_\phi / 0.5s) \cdot f_{ywd} \cdot 0.85$ $s = 2 \cdot ([z \cdot \cot\theta \cdot A_\phi \cdot f_{ywd} \cdot 0.85] / V_{Rd,s})$ $= 273 \text{ mm}$	$A_{sw} = 50.3 \text{ mm}^2$ $f_{ywd} = 435 \text{ MPa}$																																																																
	Check maximum shear link spacing:- Is $s_{l,max} > 0.75d$ YES																																																																	
	Provide 8 mm helical at nominal pitch 185 mm																																																																	
	Turo, J, et al. Shear truss analogy for concrete members of solid and hollow circular cross section. <b>Eng. Struc.</b> (2008)																																																																	

PROJECT:

**Hampstead Green****Rock & Alluvium**

Ref: QR-32/01

TITLE or DESCRIPTION:	ORIG by	Date	VERIF	Date	Ref. No.	SHEET No
	KK				16-0036	of

REFERENCE	Bending and Axial Force to EN 1992-1-1:2004 (EC2) - Secant Wall		Rev:
EC2	Circular Sections (Cast In-situ)		
4.4.1.3(4)	<u>Pile section</u> pile diameter = <b>400</b> mm Pile spacing = <b>550</b> mm design pile diameter h = <b>380</b> mm Ac = <b>113411</b> mm <sup>2</sup> cover <sup>1</sup> c <sub>nom</sub> = <b>65</b> mm cage diameter d = <b>205</b> mm ratio d/h = <b>0.5</b> f <sub>ck</sub> = <b>32</b> MPa      γ <sub>c</sub> = <b>1.65</b> α <sub>cc</sub> = <b>0.85</b> {NA 3.1.6 (1)} f <sub>yk</sub> = <b>500</b> MPa      γ <sub>s</sub> = <b>1.15</b>		
	<u>Design Actions on pile</u>		
	Actions N = <b>0</b> kN Factored Actions N = <b>285</b> kN Wallap shear = <b>224</b> kN/m Shear V <sub>Ed</sub> = <b>123.2</b> kN      BM/SF factor = <b>1.0</b> Ult Shear V <sub>Ed</sub> = <b>123.2</b> kN Wallap moment = <b>223</b> kNm/m Induced Moment M <sub>i</sub> = <b>122.65</b> kNm Applied Moment M <sub>Ed</sub> = <b>0</b> kNm Σ Moments M = <b>123</b> kNm Factored Ult M = <b>123</b> kNm		
	<u>Using IstructE design charts for circular columns:-</u>		
	M/h <sup>3</sup> f <sub>ck</sub> = <b>0.082</b> (also checked for M/h3=0.0 for zero vertical load)		
	Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.00</b>		
	Factored Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.07</b>		
	therefore from charts;		
	ρ f <sub>yk</sub> / f <sub>ck</sub> = <b>0.39</b> From charts		
	ρ = <b>4A<sub>st</sub> / π.h<sup>2</sup></b>		
	<u>therefore, adopt greater of:</u>		
	Area of main steel A <sub>st</sub> = <b>2406</b> mm <sup>2</sup>		
	main bar dia = <b>25</b> mm		
	no. main bars = <b>6</b> no.		
	helical dia = <b>10</b> mm		
	Area of main steel, A <sub>st</sub> = <b>2945</b> mm <sup>2</sup>		
	Bar spacing (face to face) = <b>82</b> mm		

PROJECT: <b>Hampstead Green</b>		<b>Rock &amp; Alluvium</b> 										
TITLE or DESCRIPTION: <b>Section 4 (CP Piles 27-32)</b>		ORIG by	Date	VERIF	Date	Ref. No	SHEET No					
		KK				16-0036	of					
REFERENCE		[Rev:										
EC2 Shear to EN 1992-1-1:2004 (EC2) - Secant Wall		Circular Sections (Cast In-situ) using helical reinforcement										
4.4.1.3(4)	<u>Pile section</u> pile dia = <b>400</b> mm Pile spacing = <b>550</b> mm pile diameter dnom = <b>380</b> mm Ac = <b>113411</b> mm <sup>2</sup> cover c <sub>nom</sub> = <b>65</b> mm main bar dia = <b>25</b> mm no. main bars = <b>6</b> no. helical dia = <b>10</b> mm d = <b>247</b> mm f <sub>ck</sub> = <b>32</b> MPa f <sub>yk</sub> = <b>500</b> MPa Wallap shear = <b>224</b> kN/m Ult V <sub>Ed</sub> = <b>123.2</b> kN Actions N = <b> </b> kN factored actions N <sub>Ed</sub> = <b> </b> kN						k <sub>2</sub> = <b>75</b> mm [NA.4.4.1.3 (4)]					
	$\gamma_c = 1.5$ (This is adjusted by K <sub>f</sub> =1.1 [2.4.2.5 (2)] to give 1.65) $\gamma_c = 1.65$ $\alpha_{cc} = 0.85$ [NA. 3.1.6 (1)} $\gamma_s = 1.15$											
	SF factor <b>1.0</b>											
	Check requirement for shear reinforcement											
	$V_{Rd,c} = [C_{Rd,c}k(100\rho_1f_{ck})^{1/3} + k_1\sigma_{cp}]b_w d$ with minimum = $(v_{min} + k_1\sigma_{cp})b_w d$ $v_{min} = 0.035k^{3/2}f_{ck}^{1/2}$ <b>0.51824467</b>						$CR_{d,c} = 0.18 / \gamma_c$ <b>0.11</b> $k = 1 + (200/d)^{1/2}$ <b>1.90</b> <=2.0 $\rho_1 = A_{si}/b_w d$ <b>0.02</b> <=0.02 $\sigma_{cp} = N_{ed}/A_c$ <b>0</b> < 0.2f <sub>cd</sub> $k_1 = 0.15$ [NA.6.2.2(1)]					
	$V_{Rd,c} = 49$ kN											
	Is $V_{Rd,c} > V_{Ed}$ => <b>NO</b> Action: <b>Design of shear reinforcement required</b>											
	Design Shear Reinforcement											
	Check concrete strut capacity at Cot θ = 2.5 :- $V_{Rd,max} = \alpha_{cw} \cdot b_w \cdot z \cdot v_1 \cdot f_{cd} / (\text{Cot}\theta + \tan\theta)$ (6.9)						$\cot\theta = 2$ $\tan\theta = 0.5$ $\alpha_{cw} = 1$ [NA.6.2.3(3)] $z = 0.9d$ <b>223</b> mm $v_1 = 0.6(1-f_{ck}/250)$ <b>0.52</b> [6.6N]					
	$V_{Rd,max} = 292$ kN											
6.2.3 exp 6.9	Is $V_{Rd,max} > V_{Ed}$ => <b>YES</b> Action: <b>Calculate link spacing</b>											
	Calculation for strut inclination:- $\theta = 0.5 \cdot \sin^{-1}[(6.54 \cdot V_{Ed}) / (b_w \cdot d \cdot (1 - f_{ck}/250) \cdot f_{ck})]$ $\theta = NA$ rad						$\cot\theta = 2.5 > 1.0$					
	Calculate shear reinforcement spacing after Turmo et al (2008);-											
	$V_{Rd,s} = z \cdot \cot\theta \cdot (A_\phi / 0.5s) \cdot f_{ywd} \cdot 0.85$ $s = 2 \cdot ([z \cdot \cot\theta \cdot A_\phi \cdot f_{ywd} \cdot 0.85] / V_{Rd,s})$ <b>= 210</b> mm						$A_{sw} = 78.5$ mm <sup>2</sup> $f_{ywd} = 435$ MPa					
	Check maximum shear link spacing:- Is $s_{l,max} > 0.75d$ <b>YES</b>											
	<table border="1"> <tr> <td>Provide</td> <td><b>10</b></td> <td>mm</td> <td>helical at nominal pitch</td> <td><b>185</b></td> <td>mm</td> </tr> </table>						Provide	<b>10</b>	mm	helical at nominal pitch	<b>185</b>	mm
Provide	<b>10</b>	mm	helical at nominal pitch	<b>185</b>	mm							
Turo, J, et al. Shear truss analogy for concrete members of solid and hollow circular cross section. <b>Eng. Struc.</b> (2008)												

PROJECT:

**Hampstead Green****Rock & Alluvium**

Ref: QR-32/01

TITLE or DESCRIPTION:	ORIG by	Date	VERIF	Date	Ref. No.	SHEET No
	KK				16-0036	of

REFERENCE	Rev:	
EC2	Bending and Axial Force to EN 1992-1-1:2004 (EC2) - Secant Wall	
	Circular Sections (Cast In-situ)	
4.4.1.3(4)	Pile section	
	pile diameter = <b>400</b> mm	
	Pile spacing = <b>550</b> mm	
	design pile diameter h = <b>380</b> mm	
	Ac = <b>113411</b> mm <sup>2</sup>	
	cover <sup>1</sup> c <sub>nom</sub> = <b>65</b> mm	k <sub>2</sub> = <b>75</b> mm
	cage diameter d = <b>198</b> mm	
	ratio d/h = <b>0.5</b>	
	f <sub>ck</sub> = <b>32</b> MPa	γ <sub>c</sub> = <b>1.65</b>
	f <sub>yk</sub> = <b>500</b> MPa	α <sub>cc</sub> = <b>0.85</b> [NA 3.1.6 (1)]
		γ <sub>s</sub> = <b>1.15</b>
	Design Actions on pile	
	Actions N = <b>0</b> kN	
	Factored Actions N = <b>285</b> kN	
	Wallap shear = <b>161</b> kN/m	
	Shear V <sub>Ed</sub> = <b>88.55</b> kN	BM/SF factor = <b>1.0</b>
	Ult Shear V <sub>Ed</sub> = <b>88.55</b> kN	
	Wallap moment = <b>329</b> kNm/m	
	Induced Moment M <sub>i</sub> = <b>180.95</b> kNm	
	Applied Moment M <sub>Ed</sub> = <b>181</b> kNm	
	Σ Moments M = <b>181</b> kNm	
	Factored Ult M = <b>181</b> kNm	
	Using IstructE design charts for circular columns:-	
	M/h <sup>3</sup> f <sub>ck</sub> = <b>0.121</b> (also checked for M/h3=0.0 for zero vertical load)	
	Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.00</b>	
	Factored Actions N N/h <sup>2</sup> f <sub>ck</sub> = <b>0.07</b>	
	therefore from charts;	
	ρ f <sub>yk</sub> / f <sub>ck</sub> = <b>0.64</b> From charts	
	ρ = <b>4A<sub>st</sub> / π.h<sup>2</sup></b>	
	therefore, adopt greater of:	
	Area of main steel A <sub>st</sub> = <b>3949</b> mm <sup>2</sup>	
	main bar dia = <b>32</b> mm	
	no. main bars = <b>6</b> no.	
	helical dia = <b>10</b> mm	
	Area of main steel, A <sub>st</sub> = <b>4825</b> mm <sup>2</sup>	
	Bar spacing (face to face) = <b>72</b> mm	



## Appendix E

### **Concrete Stress Check**

PROJECT One Parkside	Rock & Alluvium				
TITLE EC2 structural Capacity Check	Orig.	Date	Verif.	Date	Ref. No./rev.
Section Case 1 - 400mm	KK				Sheet 16-0036 Date 21/04/2016

**Based on EC2 Design**  
**Maximum Structural Capacity for 400 mm diameter pile**

The Value of design compressive strength of concrete is defined as:

$$f_{cd} = (\alpha_{cc} * f_{ck}) / (y_c * k_f) \quad \text{Clauses 2.4.2.5 & 3.15}$$

Therefore for C 32/40 | Concrete, characteristic cylinder strength = 32 N/mm<sup>2</sup>

Where:

$\alpha_{cc} =$	0.85
$f_{ck} =$	32 N/mm <sup>2</sup>
$y_c =$	1.50
$k_f =$	1.10

Therefore

$$f_{cd} = 16.48 \text{ N/mm}^2$$

Design Axial Resistance of 400 mm diameter pile

$$N_{rd} = A_c * f_{cd} + A_s * f_{yd}$$

Where:

$d_{nom}$	380 mm <sup>2</sup>
$A_c =$	113411 mm <sup>2</sup>
$f_{cd} =$	16.48 N/mm <sup>2</sup>
$A_s$	Ignore
$f_{yd}$	Ignore

Basing Design on Compressive Strength of Concrete Area alone

$$N_{rd} = A_c * f_{cd}$$

For a 400 mm diameter pile  
 $A_c = 113411 \text{ mm}^2$

Therefore pile resistance is

$$N_{rd} = 1870 \text{ kN}$$

Therefore max Com 1 action from schedule is

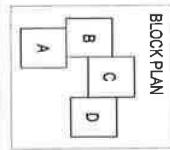
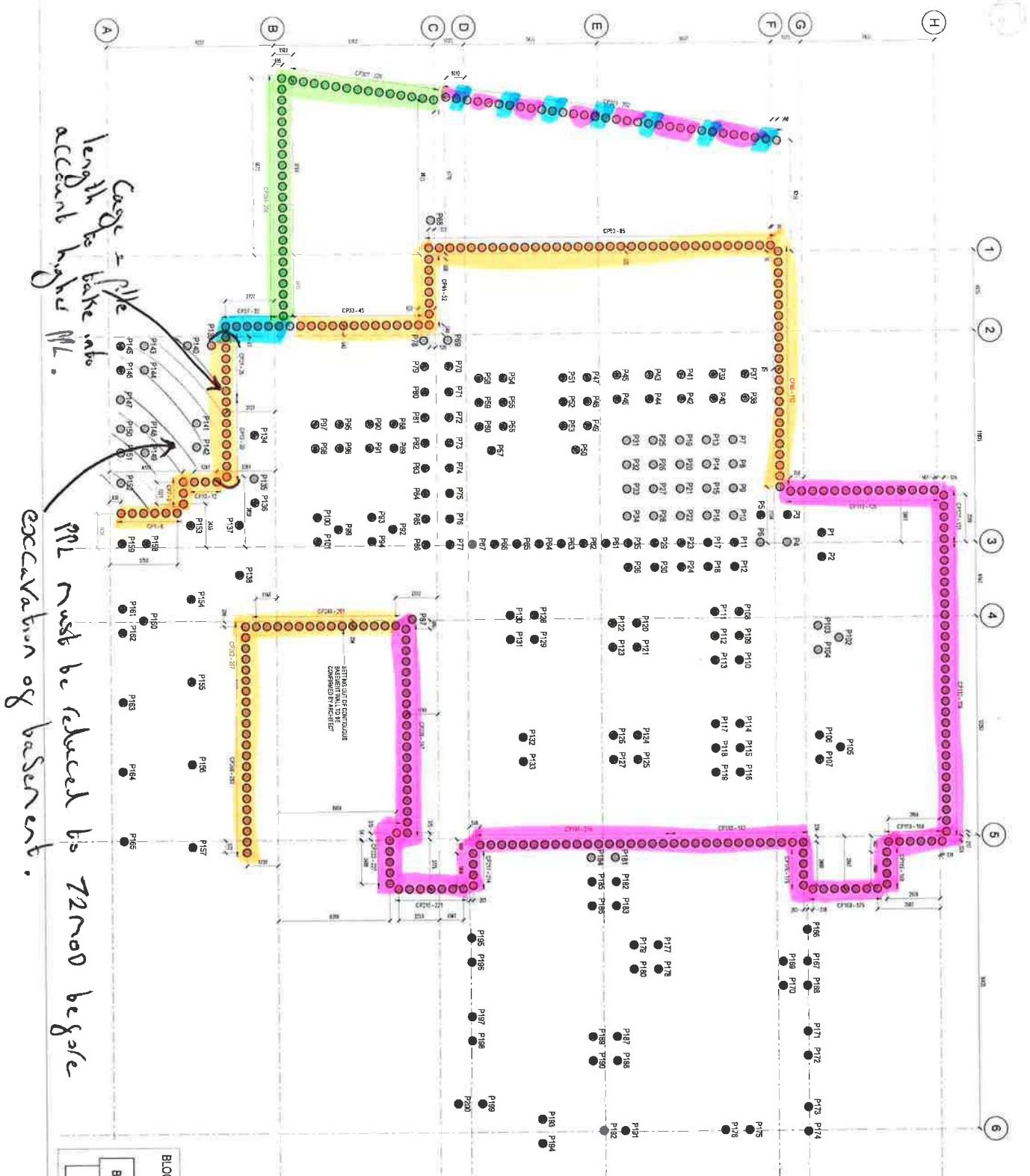
$$F_{cd} = 796 \text{ kN Total}$$

Check Compressive Stress on Pile,  $N_{rd} > F_{cd}$

**Nrd > Fcd therefore no additional compression steel required**

## **Appendix F**

### **Section Location Plan**



## SECTION 1

## SECTION 2

## SECTION 3

## SECTION 4

Proposed Pile Layout

elliottwood

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NW2 2AB

Construction	Architectural	Structural	Mechanical	Electrical	Plumbing
213839	B03	SJ70	C2		

This drawing is to be used in conjunction with all other relevant drawings and specifications.  
Do not use from this drawing.

### LEGEND

- Existing Structure
- New/old building boundary
- New/revised boundary
- New/old structure
- Revised
- Underpinning
- Non load bearing Party walls
- Load bearing structure/away from party wall
- Non steel walls
- Reinforced concrete
- Thermal insulation
- Non structural openings
- Structural opening
- Piles (vertical projection)
- Proposed vertical projection
- Existing vertical projection
- Piles to be removed