

# Daylighting Impact Assessment

246-248 Kilburn High Road

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# 1.0 Executive Summary

This report details the daylight and sunlight impact assessment of the proposed alterations to the new development at 248 Kilburn High Road. The proposed changes to the scheme are assessed in comparison to the previously consented scheme with planning application number 2017/3206/P. The assessment has been completed in accordance with the methodology detailed in the BRE Report 209: Site Layout Planning for Sunlight and Daylight, 2<sup>nd</sup> Edition, 2011.

The results presented here indicate that the alterations to the consented scheme are minimal and have negligible impact on the daylighting amenity experience by the neighbouring properties.

The internal daylighting conditions within the proposed accommodation remains consistent with the standards achieved in the consented scheme.

#### 2.0 Introduction

Fabric Building Physics was appointed to undertake revisions to the skylight and sunlight impact study in relation to the existing residential properties adjacent to the proposed new residential development at 248 Kilburn High Road, London NW6. This report has been drafted to meet the requirements of Camden Council Planning guidance which states:

'A daylight and sunlight assessment should accompany planning applications where a proposed development has the potential to negatively impact the existing levels of daylight or sunlight on neighbouring properties.'

The predicted impact of the proposed development has been assessed in relation to the guideline standards defined in accordance with the BRE Report *BR 209*: *Site Layout Planning for Sunlight and Daylight, 2<sup>nd</sup> Edition 2011* by Paul Littlefair.

The analysis presented in this report is based on the planning drawings submitted by p-ad with this application. The scale, massing and internal layout for the adjacent buildings at 1-23 Grangeway, 240-242, 244 & 254 Kilburn High Road were all accessed from planning submission records on LB Camden planning portal.

#### 2.1 Site Context

The site is situated between Kilburn High Road and Kilburn Grange Park as shown in Figure 1.

The main portion of the site is currently cleared as shown in Figure 2; with a three storey residential building occupying the Northern edge of the site as shown in Figure 2. The site is bounded and overlooked by a number of existing buildings, which are believed to be a mixture of residential and commercial premises. The majority of the nearest windows overlooking the site at the rear of 250-252 Kilburn High Road are believed to be bathroom, as shown by the presence of 100mm soil waste pipes. These are visible in Figure 5 below.



Figure 1: Aerial View of Site Location



Figure 2: Existing Site (Looking South West) towards Kilburn High Road



Figure 3: Existing house at 246 Kilburn High Road



Figure 4: View northeast at boundary wall with 246 Kilburn High Road



Figure 5: View of rear of 250 Kilburn High Road from roof of 246 KHR.

#### 2.2 Consented Scheme

The consented scheme incorporates 27no. flats in two blocks. The proposed alterations to the scheme maintain the same number of units but incorporate a 355mm increase in the height to Block B.



## 3.0 Planning Policy

The requirements for daylight amenity in both existing and proposed accommodation is addressed in Camden Planning Guidance 6 (CPG 6): Amenity www.camden.gov.uk/ccm/cms-service/download/asset?asset id=2694293.

The guidance contained in CPG 6 requires new developments to demonstrate that the amenity standards are maintained in accordance with the methodology defined in BRE 209: Site Layout Planning for Sunlight and Daylight:  $2^{nd}$  Edition 2011 by Dr Paul Littlefair.

#### 3.1 BRE Guidelines

BRE report 209 – Site Layout Planning for Sunlight and Daylight (2011) defines the criteria and methodology for the assessment of daylight, sunlight and overshadowing within new and existing developments. The purpose of the guide is to provide a framework to ensure adequate daylighting is provided in new development and minimise the impact of new development on adjacent existing buildings.

The handbook provides guideline standards to be maintained in existing buildings and a simplified methodology to determine whether any negative impact is 'material' or within acceptable limits. The handbook discusses the limits of applicability of the defined standards, with particular emphasis on the need to interpret the guideline standards flexibly subject to the site context, constraints and design requirements;

The advice given here is not mandatory and this document should not be seen as an instrument of planning policy; its aim is to help rather than constrain the designer. Although it gives numerical guidelines, these should be interpreted flexibly because natural lighting is only one of many factors in site layout design. In special circumstances the Developer or Planning Authority may wish to use different target values. (Page 1, Paragraph 1.6)

Note that numerical values given here are purely advisory. Different criteria may be used, based upon the requirements for daylighting in an area viewed against other site layout constraints. Another important issue is whether the existing building is itself a good neighbour, standing a reasonable distance from the boundary and taking no more than its fair share of light'. (Page 7, Paragraph 2.2.3)

#### 3.2 Daylight

Where a proposed development does not subtend the 25° angle from a point 2m above ground level projected from an existing building, it can be concluded that the development proposals will not have a material impact on the existing daylighting levels and therefore no further analysis is required. This process is to be undertaken for all adjacent / potentially affected buildings.

Where proposed development does subtend the 25° line, the potential impact on existing buildings is assessed using Vertical Sky Component and No Sky Line calculations. The latter requires knowledge of the internal floorplan of the potentially affected building.

For new development, the BRE guidelines state:

Daylight provision in new rooms may be checked using the average daylight factor calculation. The ADF is a measure of the overall amount of daylight in a space... In housing, BS 8206 also gives minimum values of ADF of 2% for kitchens, 1.5% for living rooms and 1% for bedrooms. (Page 7, Paragraph 2.2.3)

#### 3.2.1 Vertical Sky Component

The Vertical Sky Component (VSC) is defined as:

This is the ratio of the direct sky illuminance falling on the vertical wall at a reference point (usually the centre of the window), to the simultaneous horizontal illuminance under an unobstructed sky. The standard CIE (Commission Internationale de L'Eclairage) overcast sky is used, and the ratio is expressed as a percentage.

This is the principle measurement of how much sky is visible from a vertical surface and is used to assess the impact of new development on adjacent properties. An unobstructed vertical surface can achieve a maximum VSC of 39.6%.

The BRE guidelines state that for a room to be able to continue to receive sufficient daylight, the windows should be capable of achieving a VSC of greater than 27 per cent. Furthermore, new development should seek to limit any reduction below this level to within 0.8 times the original value to ensure adequate daylighting potential is maintained.

#### **3.2.2** No Sky Line

The no sky line / view of sky divides points on the working plane (0.85m above FFL for residential) which have and do not have a direct view of the sky. Areas located beyond the no-sky line will usually appear darker and more gloomy compared with the rest of the room. The BRE handbook states:

If, following construction of a new development, the no sky line moves so that the area of the existing room, which does received direct skylight, is reduced to less than 0.8 times its former value this will be noticeable to the occupants, and more of the room will appear poorly lit. This is also true if the no-sky line encroaches on key areas like kitchen sinks and worktops.

#### 3.2.3 Average Daylight Factor

The Average Daylight Factor (ADF) is the ratio of illuminance achieved on a working plane in a room, relative to the unobstructed horizontal illuminance achieved outside. The CIE standard overcast sky is used and the ratio is expressed as a percentage.

### 3.3 Sunlight

For access to direct sunlight, the BRE guidelines propose a single methodology, Annual Probable Sunlight Hours, to assess direct solar access for both existing and new build development. Separate criteria are defined for the assessment of direct sun in external open spaces.

#### 3.3.1 Annual Probable Sunlight Hours

The BRE guidelines states that:

In general a dwelling, or non-domestic building which has a particular requirement for sunlight, will appear reasonably sunlit provided:

- At least one main window wall faces within 90° of due south and
- The centre of at least one window to a main living room can receive 25% of annual probable sunlight hours, including at least 5% of annual probable sunlight hours in the winter months between 21 September and 21 March.
- Where groups of dwellings are planned, site layout design should aim to maximise the number of dwellings with a main living room that meets the above recommendations.

The APSH assesses the likelihood of direct sunlight including the effects of cloud cover rather than relying solely on solar geometry. BR209 defines 'probable sunlight hours' as the total number of hours in the year that sun is expected to shine on unobstructed ground, allowing for average levels of cloud cover for the location in question based on historical climate data. APSH is measured at the window face and are calculated for each window using the sunlight availability indicators provided in BR 209 Appendix A for the latitude that most closely matches the site.

For existing adjacent dwellings, where a main window faces within 90 degrees of south and development proposals subtend the 25° line, there is potential for the existing sunlight amenity to be adversely affected. This will be the case if the centre of the window:

 Receives less than 25% of APSH or less than 5% APSH between 21st September and 21 March and

- Receives less than 0.8 times its former sunlight hours during either period and
- Has a reduction in sunlight hours received over the whole year greater than 4% of APSH

# 3.4 Reference Windows

Refer to Drawing 1817/R/01 for identification of the reference windows for the adjacent properties.

## 4.0 Analysis Results

#### 4.1 Neighbouring Buildings Vertical Sky Component

The VSC results for the windows of surrounding buildings are detailed in drawing 1817/R/01 and are summarised below:

#### 1-23 Grangeway

All windows are predicted to experience a reduction of less than 0.7% of their consented Vertical Sky Component value compared to the existing consented condition.

#### 240-242 Kilburn High Road

Of the 18 windows located here, those self shaded by the balcony above are predicted to experience a reduction to their VSC of less than 3.1% compared to their consented condition. For windows not located beneath a balcony, the reduction is less than 1%.

#### 244 Kilburn High Road

There are 14 windows located at this address. All of the windows, except one, are predicted to experience a reduction to their consented VSC of less than 1.4% of this existing value, which is negligible. Window W46 is predicted to experience an 8.3% loss. This window is considered to be a poor neighbour as it is located directly on the boundary.

It is therefore concluded that the development proposals will not have an unacceptable impact on the existing daylight amenity for the properties at 244 Kilburn High Road.

#### 250-252 Kilburn High Road

There are 11 windows facing the development site at this address. The increased height of the proposed Block B will result in a reduction to the VSC of these windows of less than 1.3% their existing values. This is considered to be negligible and therefore within acceptable limits.

#### 256-260 Kilburn High Road

The reduction to the VSC in these locations is less than 0.6% of their consented value, and therefore considered negligible.

#### 4.2 Neighbouring Buildings – No Sky Line Assessment

The results of the no sky line assessment for the neighbouring dwellings is detailed on drawing 1817/W/06 in the Appendix. This illustrates the comparison of the location of the no sky line in both the consented and proposed condition.

• Of the 19 rooms assessed, 10 are predicted to experience no alteration.

- 8no. rooms are predicted to experience a loss of upto 3% of their consented floor area with a direct view of the sky. In most cases, the loss is predicted to be in the region of 0.1m<sup>2</sup> in real terms.
- One room, 250-03, is predicted to experience a 5% reduction in the consented floor area with a direct view of the sky, equating to 0.7 m<sup>2</sup> of floor area. However, the room retains a direct view of sky for 70% of its' floor area and is therefore considered remain acceptable.

# 4.3 Neighbouring Buildings – Annual Probable Sunlight Hours

The development site is located to the north of all the neighbouring windows of interest and therefore an assessment of the impact on the Annual Probable Sunlight Hours is not required by the BRE assessment methodology.

#### 4.4 Neighbour Buildings Conclusion

It is concluded that the development proposals will not create excessive reductions to the VSC of existing windows or location of the no sky line within the adjacent buildings. It is therefore contended that the development proposals are of a scale and massing that is consistent with the local context.

#### 4.5 Daylighting Within Proposed Accommodation

The Average Daylight Factor and No Sky Line results are detailed on drawing 1817/R/02 in the Appendix. These are to be read with the No Sky Line plots detailed on drawings 1817/W/01-06.

The results indicate that there is no meaningful alteration to the internal daylighting conditions in the proposed scheme compared to the existing consented scheme. The proposed accommodation achieves a acceptable internal daylighting conditions for both ADF and View of Sky calculations in accordance with the BRE requirements.

# 5.0 Appendix 1 - Glossary

#### **Daylight**

Visible part of the global solar radiation – includes sunlight and skylight components as described below.

#### Sunlight

Visible part of the solar radiation that reaches the Earth's surface directly as parallel rays after selective attenuation by the atmosphere. Note, this is sometimes known as beam radiation.

#### Skylight

Visible part of the solar spectrum that reaches the Earth's surface diffusely as a result of scattering by the Earth's atmosphere.

#### **Obstruction Angle**

The angular altitude of the top of an obstruction above the horizontal, measured from a given reference point in a vertical plane in a section drawn perpendicular to the vertical plane.

#### **Annual Probable Sunlight Hours (APSH)**

Long-term average of the total number of hours during the year that direct sunlight reaches a reference point. The reference point can be located on a horizontal or vertical surface. The APSH calculation includes the statistical likelihood of cloud cover in a specific location. It is therefore a more appropriate predictor of sunlight hours than shadow diagrams which do not consider cloud cover.

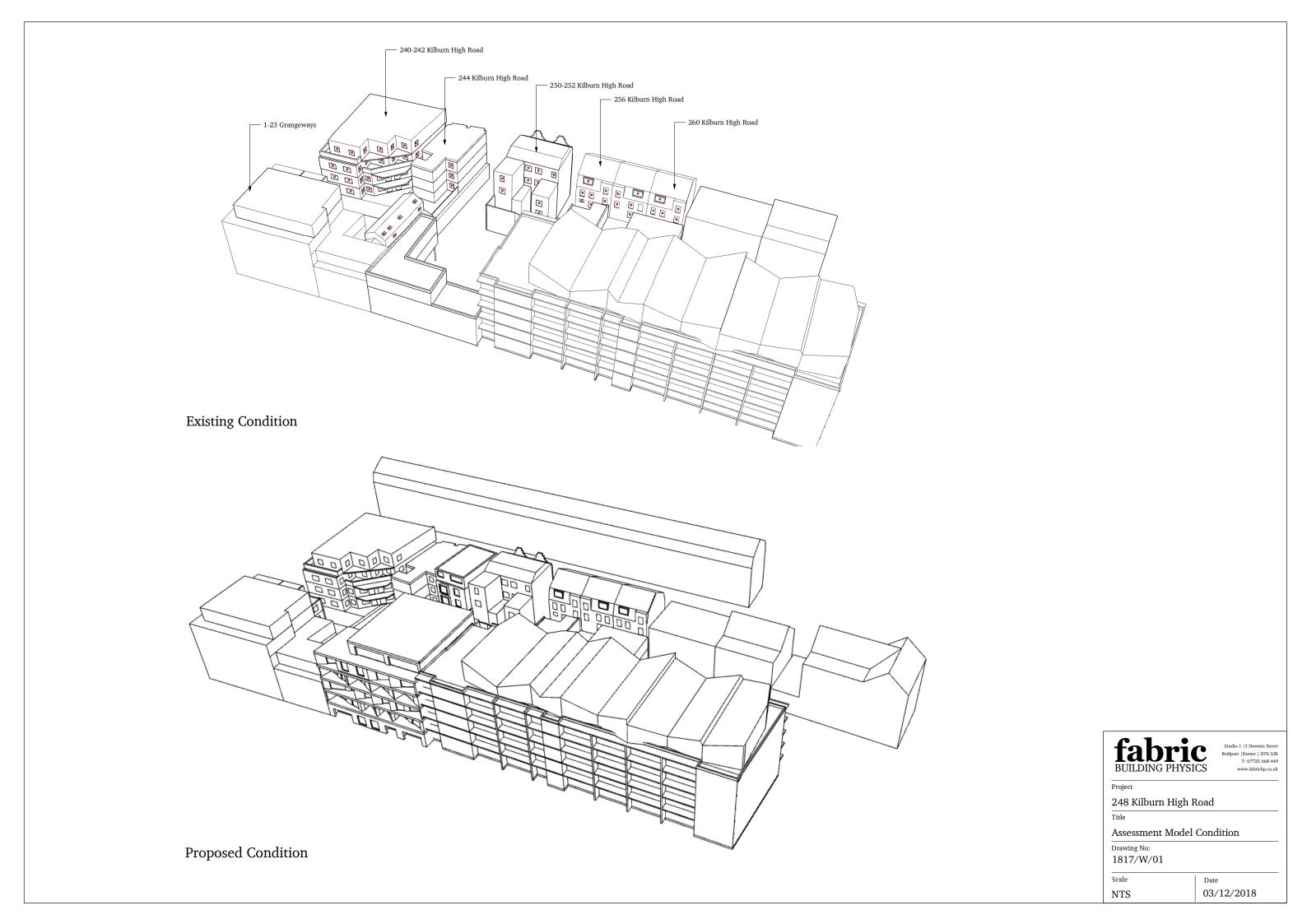
#### Vertical Sky Component (VSC)

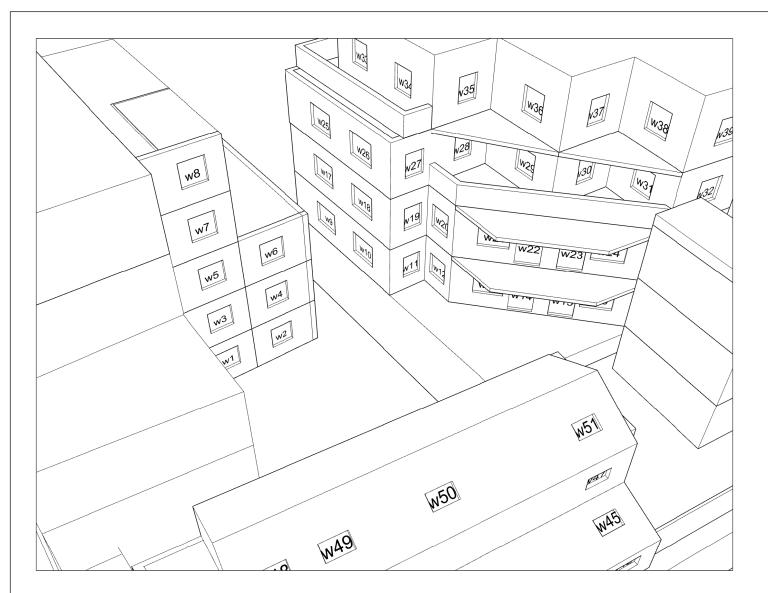
The ratio, expressed as a percentage, of that part of illuminance, at a point on a given vertical plane that is received directly from a standard overcast sky, to illuminance on a horizontal plane due to an unobstructed hemisphere of this sky. This is the principle measurement of how much sky is visible from a vertical surface and is used to assess the impact of new development on adjacent properties.

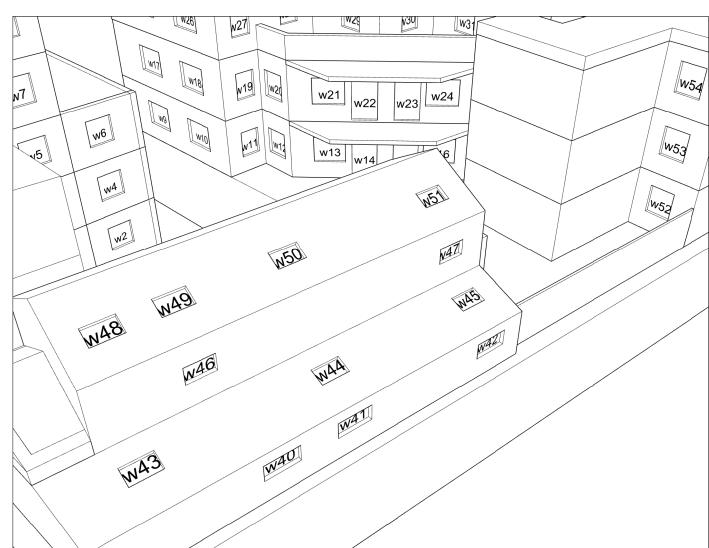
#### Visible Sky Angle θ (VSA)

An angular measurement that results from deducting the obstruction angle from a right angle taken from a given reference point in a vertical plane. Ignoring the effects of shading by window reveals, the VSA is equal to 90° minus the Obstruction Angle.

# 6.0 Appendix – 2 Drawings & Results











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Project

248 Kilburn High Road

ri+lo

Window Reference Location

Drawing No:

1817/R/01

Scale NTS

Date 03/12/2018

	ID	Consented Scheme VSC	2018 Scheme	2018 reduction	Notes
	w1	12.72	12.65	0.6%	
ay	w2	14.09	13.99	0.7%	
1-23 Grangeway	w3	16.01	15.92	0.6%	
ang	w4	17.92	17.81	0.6%	
Gra	w5	19.93	19.88	0.3%	
23	w6	22.41	22.3	0.5%	
+	w7	23.61	23.57	0.2%	
	w8	27.75	27.76	0.0%	
	w9	12.27	12.16	0.9%	
	w10	14.52	14.41	0.8%	
	w11	16.67	16.55	0.7%	
	w12	13.76	13.69	0.5%	
	w13	6.35	6.24	1.7%	Reduction due to balcony above
	w14	6.56	6.46	1.5%	Reduction due to balcony above
	w15	5.93	5.81	2.0%	Reduction due to balcony above
	w16	2.6	2.52	3.1%	Reduction due to balcony above
	w17	19.49	19.38	0.6%	
	w18	20.66	20.55	0.5%	
	w19	20.37	20.24	0.6%	
ad	w20	17.45	17.35	0.6%	
Ro	w21	9.94	9.82	1.2%	Reduction due to balcony above
igh	w22	9.69	9.56	1.3%	Reduction due to balcony above
Hu	w23	8.64	8.55	1.0%	Reduction due to balcony above
240-242 Kilburn High Road	w24	4.89	4.78	2.2%	Reduction due to balcony above
Kill	w25	27	26.87	0.5%	
45	w26	27.45	27.35	0.4%	
)-2,	w27	28.57	28.56	0.0%	
24(	w28	9.09	8.99	1.1%	
	w29	13.75	13.65	0.7%	
	w30	8.58	8.57	0.1%	
	w31	11.86	11.82	0.3%	
	w32	22.43	22.37	0.3%	
	w33	34.09	33.92	0.5%	
	w34	34	33.91	0.3%	
	w35	26.85	26.66	0.7%	
	w36	31.38	31.27	0.4%	
	w37	26.84	26.71	0.5%	
	w38	29.22	29.09	0.4%	
	w39	34.63	34.94	-0.9%	
	w40	0	0	0.0%	Window located on boundary
	w41	0	0	0.0%	Window located on boundary

	ID	Consented Scheme	2018 Scheme	2018 reduction	Notes
	w42	13.34	13.15	1.4%	Window on boundary. Room is also served by skylight
1 1	w43	28.97	28.96	0.0%	
	w44	31.2	31.2	0.0%	
coac	w45	52.99	52.93	0.1%	
h B	w46	1.93	1.77	8.3%	Window close to boundary. Room also served by W48 & W49
Hig	w47	16.15	15.94	1.3%	Window close to boundary. Room also served by W51
244 Kilburn High Road	w48	61.2	60.49	1.2%	
	w49	62.8	62.02	1.2%	
.X	w50	65.04	64.34	1.1%	
244	w51	73.44	72.96	0.7%	
1 `` [	w52	12.84	12.69	1.2%	
1 1	w53	16.48	16.26	1.3%	
	w54	23.21	23.01	0.9%	
	w55	21.83	21.69	0.6%	Window serves bathroom
oad	w56	15.37	15.3	0.5%	
ı Rc	w57	27.16	26.98	0.7%	
ligh	w58	22.72	22.62	0.4%	
l II	w59	8.24	8.17	0.8%	Window obstructed by own existing rear extension
ınc	w60	16.79	16.6	1.1%	Close to boundary. Previously obstructed by high wall
250-252 Kilburn High Road	w61	14.42	14.27	1.0%	Window heavily obstructed by own existing rear extension
52	w62	8.73	8.62	1.3%	
0-2	w63	20.57	20.48	0.4%	Window serves bathroom
25	w64	28.35	28.32	0.1%	
	w65	28.97	28.82	0.5%	
h	w66	20.22	20	1.1%	
Hig	w67	18.22	18.1	0.7%	
d d	w68	25.71	25.61	0.4%	
ilburn Road	w69	25.63	25.48	0.6%	
256 Kilburn High Road	w70	24.48	24.38	0.4%	
526	w71	30.38	30.22	0.5%	
.,	w72	28.11	28.03	0.3%	
f 75	w73	19.05	18.98	0.4%	
258 Kilburn High Road	w74	24.33	24.18	0.6%	
Kil h R	w75	25.04	24.9	0.6%	
.58 Hig	w76	27.96	27.82	0.5%	
7 _	w77	29.71	29.57	0.5%	
4.4	w78	24.78	24.68	0.4%	
bur	w79	24.7	24.61	0.4%	
Kil h R	w80	23.73	23.64	0.4%	
260 Kilburn High Road	w81	29.46	29.37	0.3%	
77	w82	27.3	27.18	0.4%	



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248 Kilburn High Road

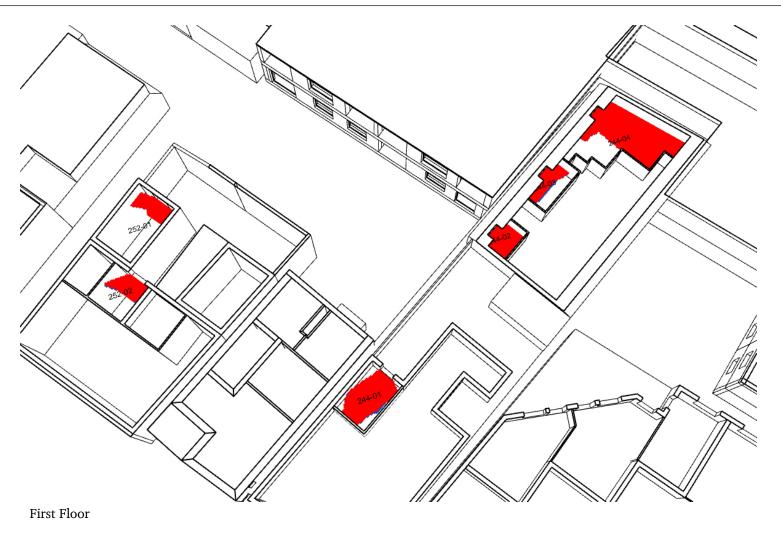
Vertical Sky Component Results

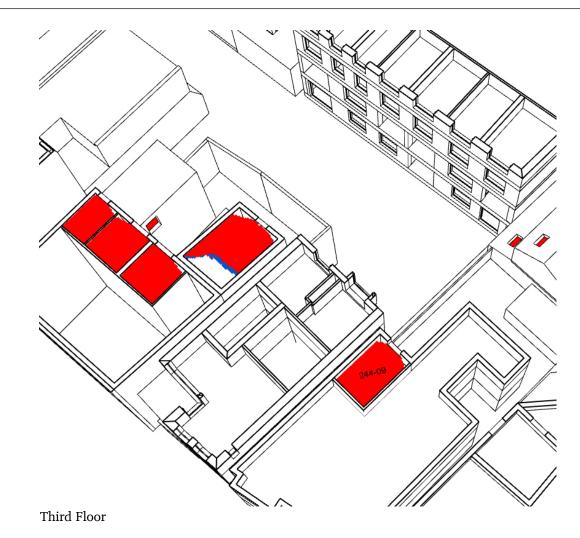
Drawing No:

1817/R/01

Scale

NA 03/12/2018





252- <sup>57</sup>
244.06
2AA-05
Second Floor

Room Reference	Floor Area m <sup>2</sup>	Consented Scheme VOS m <sup>2</sup>	Proposed VOS m <sup>2</sup>	Ratio
244-01	10.5	8.2	8.0	0.98
244-02	6.9	6.4	6.4	1.00
244-03	10.7	5.9	5.7	0.96
244-04	36.7	23.3	23.2	1.00
244-05	10.5	9.7	9.5	0.98
244-06	12.2	12.2	12.2	1.00
244-07	9.3	9.2	9.2	1.00
244-08	19.1	19.1	19.1	1.00
244-09	10.5	10.3	10.3	1.00
250-01	17.1	7.2	7.0	0.97
250-02	9.0	3.3	3.2	0.97
250-03	17.1	12.8	12.1	0.95
250-04	9.0	8.8	8.8	1.00
252-01	15.6	3.8	3.8	1.00
252-02	9.0	3.3	3.2	0.97
252-03	15.6	7.3	7.3	0.99
252-04	9.0	5.2	5.0	0.97
252-05	9.0	8.8	8.8	1.00
252-06	6.5	6.3	6.3	1.00

fabric BUILDING PHYSICS

Consented

Proposed

248 Kilburn High Road

View of Sky - 244 & 250-252 KHR

Drawing No: 1817/W/06

Scale 03/12/2018 NTS

¥	· .	u	W	R m²	# W	ır W	2.0	1.5	1.0 Floor Area		
Block	FLAT	Room	Window ID	FLOOR AREA m²	Lower Window ADF	Upper Window ADF	Kitchen	Living	Bed	with View of Sky	
			A1	29.48	0.14	0.42					
			A2	29.48	0.03	0.10				Hoor Area with View of Sky	
		L/K/D	A3	29.48	0.08	0.57	2.15	2.15	-	52%	
Α	1		A4	29.48	0.08	0.57					
			A5	29.48	0.00	0.15					
		Bed 2	A19	11.38	0.17	1.22	-	-	1.39	48%	
		Bed 1	A18	11.41	0.23	1.61	-	-	1.84	54%	
			A6	29.48	0.18	0.53					
			A7	29.48	0.04	0.11					
		L/K/D	A8	29.48	0.09	0.62	2.42	2.42	-	76%	
Α	2		A9	29.48	0.09	0.62					
			A10	29.48	0.00	0.15					
		Bed 2	A20	11.38	0.44	0.98	-	-	1.42	65%	
		Bed 1	A21	11.41	0.54	1.21	-	-	1.75	70%	
			A11	29.48	0.21	0.63					
			A12	29.48	0.04	0.12					
		L/K/D	A13	29.48	0.09	0.66	2.71	2.71	-	96%	
Α	3		A14	29.48	0.09	0.66					
			A15	29.48	0.00	0.18					
		Bed 2	A22	11.38	0.24	1.65	-	-		80%	
		Bed 1	A23	11.41	0.29	2.02	1	1		81%	
		L/K/D	A16	27.57	0.37	0.83	2.44	2.44		000%	
Α	4	L/ N/ D	A17	27.57	0.38	0.86	2.44	2. <del>44</del>	-	96%	
Α	4	Bed 1	A25	11.60	0.00	3.43	1	1	3.43	96%	
		Bed 2	A24	9.22	0.00	1.92	-	1	1.92	95%	
		L/K/D	B43	30.6	0.87	2.55	3.42	3.42	-	88%	
В	1	Bed 3	B1	18.63	0.47	1.38	1	1	1.85	29%	
ъ	1	Bed 2	B2	14.44	0.57	1.68	-	-	2.26	54%	
		Bed 1	В3	19.67	0.36	1.07	-	-	1.43	69%	
		L/K/D	B42	27.85	0.60	1.76	2.36	2.36	-	99%	
В	2	Bed 2	B41	12	0.78	2.28	-	-	3.06	99%	
		Bed 1	B40	13.6	0.71	2.08	-	-	2.79	91%	
		L/K/D	B39	28.4	0.93	2.75	3.68	3.68	-	93%	
В	3	Bed 2	B5	15.1	0.30	0.90	-	-	1.20	34%	
		Bed 1	B4	17.52	0.15	1.02	-	-	1.16	40%	
		I /K/D	L/K/D	В8	25.68	0.21	1.75	2.22	2.22	_	59%
В	4	ц ц д	В7	25.68	0.07	0.20	2,22	2.22		3770	
		Bed 1	В6	12.06	0.35	1.03	-	-	1.39	68%	
В	5	L/K/D	B49	21.3	0.59	2.35	2.93	2.93	-	100%	
	Ŭ	Bed 1	B48	11.01	0.51	1.51	-	-	2.02	95%	
В	6	L/K/D	B47	22.9	0.41	1.66	2.07	2.07	-	96%	
	J	Bed 1	В9	12.8	0.26	0.75	-	-	1.01	39%	
В	7	L/K/D	B46	22.91	0.43	1.72	2.14	2.14	-	99%	
٠	′	Bed 1	B10	12.66	0.25	0.98	-	-	1.23	37%	
В	8	L/K/D	B44	21.79	0.52	2.09	2.61	2.61	-	95%	
٠	J	Bed 1	B45	12.05	0.78	3.13	-	-	3.91	98%	
		L/K/D	B11	23.03	0.21	1.79	2.16	2.16		46%	
В	9	ц/ ц/ Д	B12	23.03	0.04	0.12	2.10	2.10		7070	
		Bed 1	B13	11.48	0.22	0.88	-	-	1.10	36%	

<b>×</b>	-	T.	ě	${ m R}$	ssı	ı ×	ř	2.0	1.5	1.0	Floor Area
Block	FLAT	Room	Window ID	FLOOR AREA m²	Net Glass Area	Lower Window ADF	Upper Window ADF	hen	Living	Bed	with View
В	F	В	Wi	FI	Net /	L,	U Wi	Kitchen	Livi	Be	of Sky
		I /II /D	B55	40	5.59	0.28	1.12	0.51	0.51		000/
		L/K/D	B45	40	3.20	0.22	0.89	2.51	2.51	-	99%
В	10	Bed 2	B16	14.2	2.02	0.14	1.22			2.46	92%
		Deu 2	B15	14.2	2.02	0.15	1.24		,	2.40	92%
		Bed 1	B14	14.4	3.18	0.26	2.22	-	-	2.49	92%
В	11	L/K/D	B53	22.66	6.07	0.43	1.71	2.14	2.14	-	97%
Б	11	Bed 1	B17	12.7	3.18	0.28	2.41	1	-	2.69	96%
В	12	L/K/D	B52	22.65	6.07	0.42	1.69	2.12	2.12	-	97%
	12	Bed 1	B18	12.7	3.18	0.28	2.38	-	-	2.66	89%
		L/K/D	B50	26.73	6.43	0.56	2.25	2.81	2.81	-	99%
В	13	Bed 3	B51	8.95	4.40	0.84	3.35	-	-	4.18	97%
"	13	Bed 2	B20	14.69	3.18	0.25	2.10	-	-	2.35	91%
		Bed 1	B19	13.66	3.18	0.26	2.25	-	-	2.51	90%
		L/K/D	B60	37.1	7.79	0.43	1.70	2.13	2.13	-	98%
В	14	Bed 2	B22	8.2	2.02	0.26	2.17	-	-	2.43	99%
		Bed 1	B21	13.8	3.18	0.29	2.49	-	-	2.79	99%
		L/K/D	B59	32.3	6.60	0.38	1.51	1.89	1.89	-	96%
В	15	Bed 2	B25	8.6	3.18	0.40	3.36	-	-	3.76	99%
		Bed 1	B26	13.2	2.02	0.18	1.53	-	-	1.71	99%
		L/K/D 16 Bed 2	B58	31.40	6.79	0.40	1.59	1.99	1.99	-	96%
В	16		B26	14.2	3.18	0.26	2.22	-	-	2.48	99%
		Bed 1	B25	11.60	3.18	0.31	2.67	-	-	2.98	99%
		L/K/D	B56	24.82	6.07	0.40	1.62	2.02	2.02	-	99%
В	17	Bed 2	B57	9.83	3.92	0.75	3.00	-	-	3.75	99%
		Bed 1	B27	15.58	3.18	0.27	2.32	-	-	2.59	98%
		L/K/D	B65	38	7.79	0.44	1.75	2.19	2.19	-	98%
В	18	Bed 2	B29	8.3	2.02	0.28	2.35	-	-	2.62	99%
		Bed 1	B28	13.8	3.18	0.32	2.71	-	-	3.03	99%
		L/K/D	B64	32.1	5.88	0.36	1.46	1.82	1.82	-	98%
В	19	Bed 2	B30	8.7	3.18	0.43	3.62	-	-	4.04	99%
		Bed 1	B31	17.1	2.02	0.21	1.76	-	-	1.96	99%
		L/K/D	B61	28.84	6.79	0.46	1.82	4.15	4.15	_	99%
В	20	-, -, -	B72	28.85	4.35	0.48	1.40				
		Bed 2	B62	12	2.60	0.33	2.84	-	-	3.17	98%
		Bed 1	B63	9.8	2.60	0.36	3.10	-	-	3.46	97%
		L/K/D	В33	18.4	3.20	0.27	2.29	9.39	9.39	_	99%
В	21	2,142	B73 18.4 11.23 1.73 5.10 9.39	7.07		,,,,					
		Bed 1	B32	11.3	3.18	0.38	3.19	-	-	3.57	100%
		L/K/D	B71	27.95	14.20	1.41	5.63	7.04	7.04	-	100%
В	22	Bed 3	B36	11.87	3.18	0.39	3.29	-	-	3.68	100%
_		Bed 2	B35	8.96	3.18	0.48	4.05	-	-	4.53	100%
		Bed 1	B34	13.55	3.18	0.35	2.94	-	-	3.29	99%
		L/K/D	B68	51.32	9.78	0.67	2.69	8.10	8.10	_	100%
		_, ., .	B69	51.33	13.60	0.95	3.78	5.25	3.20		
В	23	Bed 3	B67	13.43	3.18	0.36	3.04	-	-	3.39	99%
		Bed 2	B66	11.87	4.35	0.53	4.52	_	-	8.72	93%
			B38	11.88	3.18	0.39	3.28			J., <u>2</u>	, , , ,
		BEd 1	B37	12.85	3.18	0.37	3.12	-	-	3.49	99%



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Proposed Accomodation Results

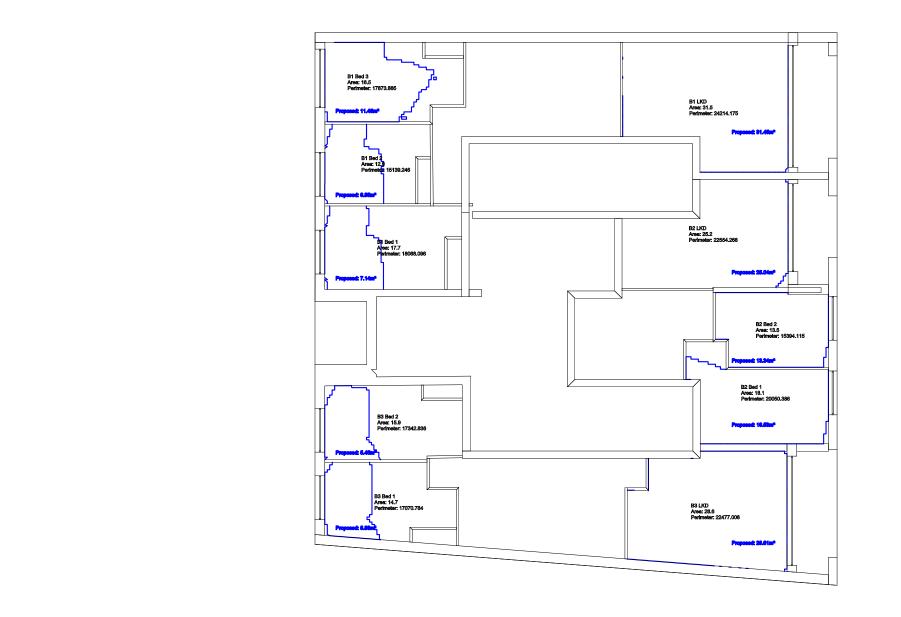
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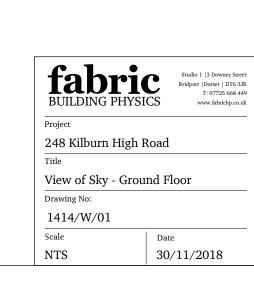
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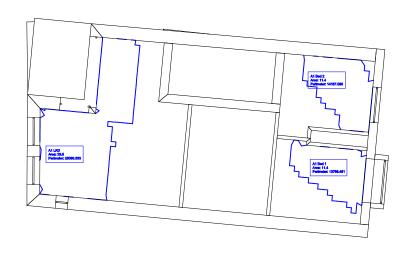
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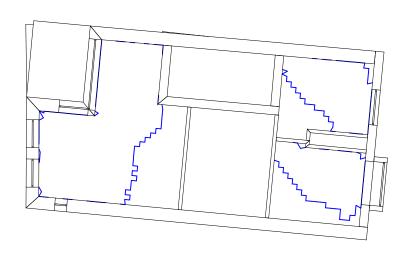
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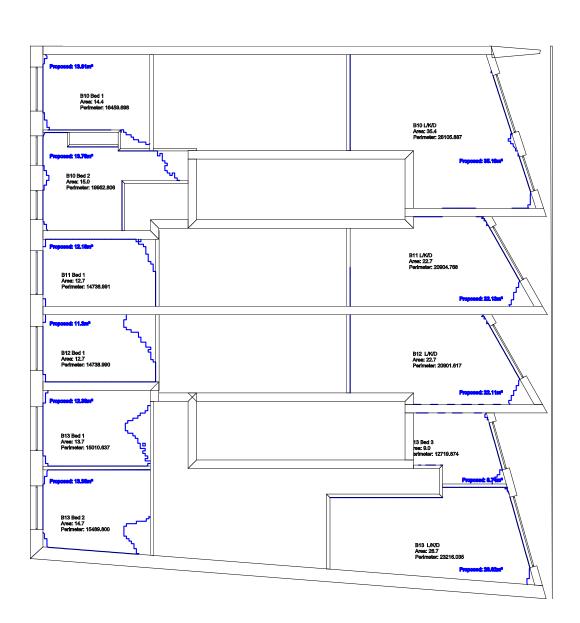
View of Sky - First Floor

Drawing No:

1414/W/02

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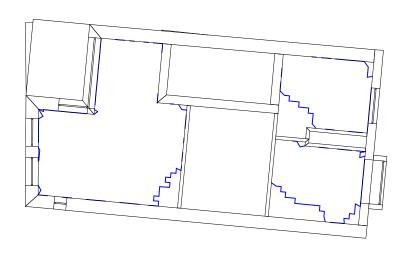
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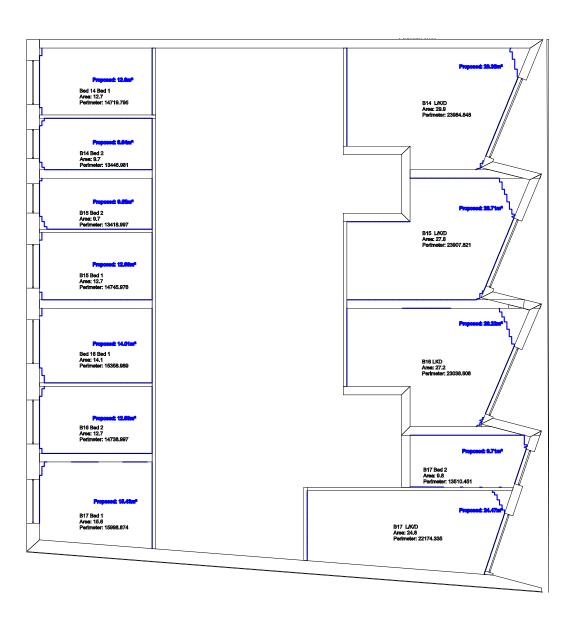
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Drawing No:

1414/W/03

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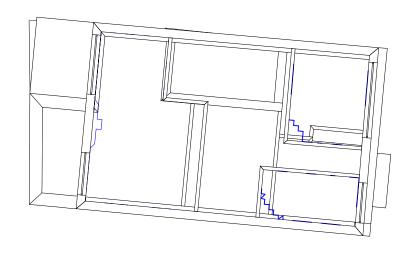


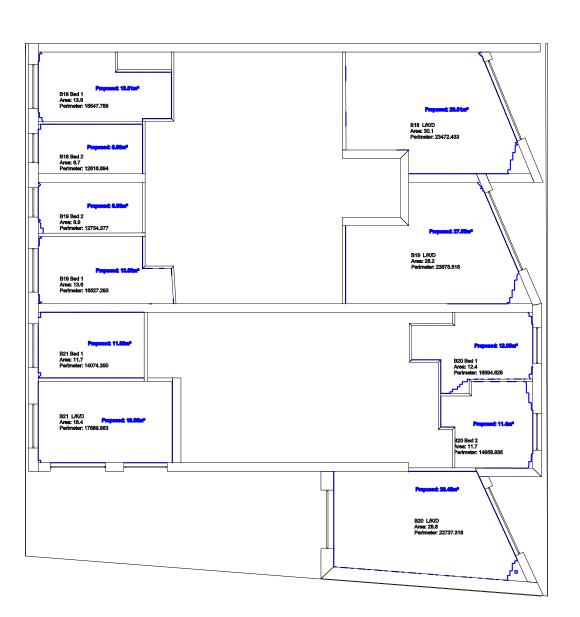


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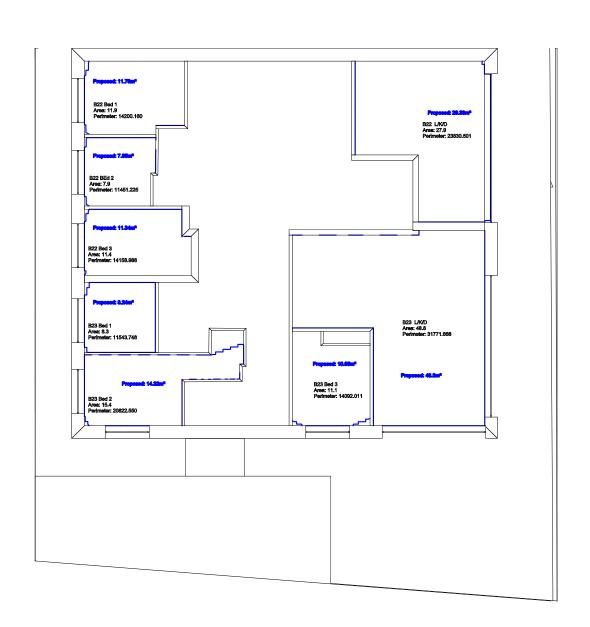
View of Sky - Fourth Floor

Drawing No:

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View of Sky - Fifth Floor

Drawing No:

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