Mr Mark Golinsky

6 Albert Terrace Mews, Primrose Hill, Camden, NW1 7SU

Basement Impact Assessment

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RSK GENERAL NOTES

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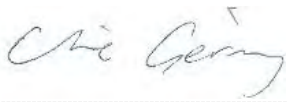
Reviewed and Approved by	Clive Gerring BSc (Hons) PhD CGeol FGS EurGeol RoGEP Principal Engineering Geologist	
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Where field investigations have been carried out, these have been restricted to a level of detail required to achieve the stated objectives of the work.

This work has been undertaken in accordance with the quality management system of RSK Environment Ltd.

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NON-TECHNICAL SUMMARY

NON-TECHNICAL SUMMARY	
Site description	The site is located at No.6 Albert Terrace Mews, Primrose Hill, London NW1 7TA, in the London Borough of Camden. The site is at the junction between Albert Terrace Mews to the east and Regent's Park Road to the north, with the other boundaries formed by the garden of neighbouring No.6 Albert Terrace to the west and No.5 Albert Terrace Mews to the south. The site shares a party wall with this latter property. The site comprises a two storey residential mews building of brick construction, covering the majority of the site, with a small shed in the north eastern corner and garden to the west and north. The area around the site is developed predominantly with residential properties. The available information indicates that the adjacent No.5 Albert Terrace Mews to the south is a brick load bearing wall building, supported by traditional shallow foundations. No basement is expected to be present beneath this property.
Proposed development	The proposed redevelopment comprises construction of a single storey basement beneath the footprint of the existing building, housing a pool plant room and a bike room/storage area. The ground floor and first floor of the existing building will be refurbished to include a swimming pool. The existing building envelope (external walls and roof) will be kept in its entirety, and the existing ground floor will be lowered by 350mm to create a level access. The proposed basement overall depth will be approximately 4m, with formation levels at around 29.45mAOD. The proposed basement retaining wall structure will be formed by 300mm thick underpins, propped at three levels over the excavation depth. Reinforced concrete slabs will be constructed at ground floor/swimming pool level and formation, both forming rigid propping in the permanent condition. The underpinning is likely to extend some 0.5m below the slab level (~ 29mAOD).
Ground / Groundwater conditions	The ground conditions beneath the site comprise a variable thickness of made ground over the London Clay Formation. The made ground is 0.5m to 2.5m thick, and generally comprised both cohesive and granular soil (described as soft to firm) with a variable proportion of brick, concrete flint and occasional chalk fragments. The London Clay Formation was encountered beneath the made ground extending to the base of the borehole at 20.0mbgl (14.0mAOD), without proving its base. The upper part of the London Clay was encountered as firm to still, medium to high strength, brown, weathered, silty clay to a depth of 11.0mbgl (23.0mAOD), below which the London Clay was stiff to very stiff,

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	high to very high strength, dark grey, fissured, silty clay. Water seepage was encountered during the investigation within the claystone band of the London Clay at around 3.80mbgl (31.2mAOD). Following the return monitoring visit this water was recorded at 1.90mbgl (30.20mAOD), while perched water was also recorded within the made ground at the highest level of 1.45mbgl (32.55mAOD).
Screening and scoping	**Subterranean (ground water):** No potential impacts identified beyond the scoping stage **Surface flow and flooding:** No potential impacts identified beyond the scoping stage **Land stability:** Potential impacts identified relate to ground stability associated with: • Retaining wall installation and ground excavation; and • Elastic heave of the London Clay in the basement excavation.
Impact Assessment	The following nearby structures were identified for assessment relating to potential ground movements: • No.5 Albert Terrace Mews adjacent to the south; • No.4 Albert Terrace Mews further to the south; and • The highways of Albert Terrace Mews and Regent's Park Road beyond eastern and northern site boundaries. **Structural stability of adjacent structures from retaining wall installation and basement excavation** In accordance with CIRIA C760 guidance, providing good workmanship and control are exercised during the installation process, the adjacent structure at No.5 Albert Terrace Mews falls into 'Damage Category 1' (Very Slight), while the structure at No.4 Albert Terrace Mews falls into 'Damage Category 0' (Negligible), which is in accordance with the requirements of LBC guidance document Camden Planning Guidance: Basements (2018). The predicted movements associated with the roads/pavements of Albert Terrace Mews and Regent's Park Road indicates one-off very small strains and rotations that will have no damaging effect. **Structural stability of adjacent structures from heave of the basement excavation** No potentially damaging vertical movements are predicted beyond the site's boundary during unloading due to excavation for the new basement, or under full loading following construction of the new basement.
Cumulative Impacts	No potential cumulative impacts have been identified for the proposed development.

NON-TECHNICAL SUMMARY	
	The impact on the adjacent properties from the construction of basements beneath No. 6 Albert Terrace was undertaken under separate assessment. The assessments result in Category 0 and 1 (Negligible and Very Slight) for the relevant adjacent properties and infrastructure. Given the distance between the developments at No.6 Albert Terrace Mews and No.6 and No.5 Albert Terrace (around 10m to 15m), it is considered that the cumulative impact from both developments on the adjacent properties will not be significantly different from the ones calculated by each separate assessment.

1 INTRODUCTION

1.1 Instructions

On the instructions of Alan Baxter Ltd, on behalf of Mr. Mark Golinsky (the 'Client'), RSK Environment Limited (RSK) have produced a Basement Impact Assessment for a proposed development at 6 Albert Terrace Mews, London, NW1 7TA, located within the Camden Town and Primrose Hill Ward of the London Borough of Camden.

1.2 Regulatory Context

This assessment is designed to be compliant with guidance provided by the London Borough of Camden (Camden) in their guidance document 'Camden Planning Guidance: Basements (2018) and its supporting study 'Camden Geological, Hydrogeological and Hydrological Study' produced for Camden by ARUP in November 2010. All the technical analysis and recommendations contained within the planning guidance are taken from this latter study, which is treated as the evidence base and technical advice when Camden are assessing Basement Impact Assessments.

This guidance applies to all developments in Camden that propose a new basement development, or an extension to existing basement accommodation where planning permission is required. In accordance with policy DP27, Camden will only permit basement and other underground development where it can be demonstrated that it will not cause harm to the built and natural environment, including to the local water environment and ground conditions.

Addressing these issues requires the submission of a Basement Impact Assessment (BIA). A BIA will be specific to a particular site and proposed development, but includes the following stages:

- *Screening*; the identification of any matters of concern with regard to hydrogeology, hydrology or ground stability, which should be investigated.
- *Scoping*; production of a statement that defines further the matters of concern identified at the screening stage.
- *Site Investigation and Study*; undertaken to establish the baseline conditions. This can be done by utilising existing information and/or collecting new information.
- *Impact Assessment*; undertaken to determine the impact of the proposed basement on the baseline conditions, taking into account any mitigation measures proposed.
- *Review and Decision-Making*; this final stage is undertaken by Camden and consists of an audit of the information supplied and a decision on the acceptability of the impacts of the basement proposal.

The purpose of the BIA is to enable Camden Council to 'assess whether any predicted damage to neighbouring properties and the water environment is acceptable or can be satisfactorily ameliorated by the developer' as stated in DP27.3.

1.3 Background

By way of background to the current project, a desk study and intrusive site investigation have been undertaken at the site by RSK, as detailed in the report "6 Albert Terrace, Primrose Hill, Camden, NW1 7SU, Geo-environmental Site Assessment Report", reference no. 29481-R01(00), dated May 2018. The current assessment draws on the results of that report. For full details reference should be made to the original report.

The information contained within this report is considered to provide sufficient site specific information compliant with the data requirements as set out in Appendix G of 'Camden Geological, Hydrogeological and Hydrological Study' produced for Camden by ARUP in November 2010.

1.4 Standards and Limitations

This report is based on information available at the time of writing. This report should be considered in the light of any changes in legislation, statutory requirement or industry practices that may have occurred subsequent to the date of issue.

2 SITE DETAILS

2.1 Site description

The site is located at 6 Albert Terrace Mews, London, NW1 7TA, within the Camden Town and Primrose Hill Ward of the London Borough of Camden (LBC), at National Grid reference TQ 104 759, as shown on Figure 1.

The site is approximately rectangular in shape and covers approximately 120 square metres. The western boundary is formed by the rear garden of No. 6 Albert Terrace, (a five story residential building), with Primrose Hill beyond. Regent's Park Road to the north is followed by a row of three to four storey residential properties, while to the south, the site shares a boundary wall with a similar two storey mews building (No.5 Albert Terrace Mews). Three to four storey residential properties facing Regent's Park Road are located beyond Albert Terrace Mews to the east of the site.

The site is located within a predominantly residential area of Primrose Hill and is surrounded by properties of similar size and construction. A London Overground Line tunnel is located some 500m to the northeast, with the Regents Canal some 130m to the south, the latter forming the boundary between LBC and Westminster City Council. The topography of the immediate site area slopes gently from northwest to southeast, with the elevation on the pavement along Albert Terrace Mews (ground level) around 35mAOD.

The site comprises a two storey residential mews building of brick construction, covering the majority of the site, with a small garden in the north western portion and storage shed in the north eastern corner. The current site layout and sections are shown on Figure 2 and Figure 3.

No basement or lightwells are present beneath the existing building.

2.2 Site surroundings

The area around the site is developed predominantly with residential properties. The available information indicates that the adjacent mews building to the south is of a similar brick load bearing wall structure, with no basement beneath.

Furthermore, the search of the publicly available planning records (from 1977 to 2014) on Camden's planning website revealed planning applications for alterations and extensions of basements to a number of properties across Albert Terrace and other surrounding addresses, indicating that basements are likely to be present beneath most of the neighbouring properties in the immediate site vicinity.

2.3 Proposed Development

The proposed redevelopment comprises the construction of a basement beneath the footprint of the existing building, housing a pool plant room and a bike room/storage area. The ground floor and first floor of the existing building will be refurbished to include a swimming pool.

The existing building envelope (external walls and roof) will be kept in its entirety, and the existing ground floor will be lowered by 350mm to create a level access. The proposed basement overall depth will be approximately 4m, with formation levels at around 29.45mAOD.

The proposed basement retaining wall structure will be formed by 300mm thick underpins constructed as a single lift and propped at three levels over the excavation depth. Reinforced concrete slabs will be constructed at ground floor/swimming pool level and formation, both forming rigid propping in the permanent condition. The underpinning is likely to extend some 0.5m below the slab level (~ 29mAOD).

Proposed development plans and sections are given in Appendix A.

2.4 Ground and Groundwater Conditions

2.4.1 British Geological Survey Data

British Geological Survey (BGS) published records for the area (BGS Map Sheet 256 North London) indicates that the site is underlain by the London Clay Formation, which in turn overlies the Lambeth Group, Thanet Sand Formation and the White Chalk Sub-group. No superficial deposits are shown in the site area.

The nearest available BGS boreholes to the site indicate that the London Clay Formation thickness is in excess of 20m, recording the stratum as firm to very stiff brown silty clay. Deeper boreholes in the vicinity of the site indicate the base of the London Clay Formation is at around 55mbgl followed by the Reading Formation of the Lambeth Group.

Based on the published geological map referred to above, the hydrogeology of the site is likely to be characterised by the unproductive strata (non-aquifer) of the London Clay Formation. BGS borehole data suggest groundwater is present at 85.0m below ground level within the Thanet Sand Formation.

It is also possible that localised perched water may be present in any made ground.

2.4.2 Site Specific Intrusive Investigation Data

A site investigation was undertaken at the site by RSK in March 2018, as detailed in the report 'Geo-environmental Site Assessment: 6 Albert Terrace Mews, Primrose Hill, Camden', report ref: 29841-01(00), dated May 2018. In addition, an investigation was also carried out by RSK for the neighbouring No.6 Albert Terrace in February and March 2017, as detailed in the report 'Geo-environmental Site Assessment: 6 Albert Terrace, Primrose Hill, Camden', report ref: 29123-01(01), dated May 2017. The findings of the latter have also been used in the assessment.

In total, the intrusive work comprised one cable-percussive borehole to 20mbgl (front of No.6), a single drive-in sampling borehole to 6.45mbgl (rear garden of No.6 at the boundary with the mews property), the excavation of 8No. trial pits to a maximum 1.2m depth (five in the No.6 building and three against the walls of the mews building), and a single horizontal core of the lightwell wall of No.6 Albert Terrace.

The investigation confirmed the anticipated geology as described in the previous section, encountering a variable thickness of made ground over the London Clay Formation.

The thickness of made ground was recorded as between 0.5m to 2.5m, comprising a mix of granular and cohesive material, ranging between clayey sand and gravel to sandy gravelly clay, and including brick, concrete, flint and occasional chalk fragments. The SPT 'N' values ranged between 5 and 12, indicating variable levels of compaction/density.

The London Clay Formation was encountered beneath the made ground extending to the base of the deep borehole at 20.0mbgl (14.0mAOD), without proving its base. The upper part of the London Clay was encountered as firm to stiff, medium strength, brown, weathered, silty clay to a depth of 11.0mbgl (23.0mAOD), below which the London Clay was stiff to very stiff, high strength to very high strength, dark grey, fissured, silty clay. . A band of weak claystone was encountered between 3.70mbgl to 3.80mbgl (approximately 30.2mAOD to 30.3mAOD).Plasticity classification testing indicates that the clays are of high to very high plasticity, typical of the London Clay.

Groundwater was encountered during the site works in the window sampling borehole, within the claystone band, at 3.80mbgl, with the monitoring during the recent investigation recording the highest groundwater level at 1.45mbgl (32.55mAOD).

Trial pits TP1 and TP2 were both recorded foundations located at 0.35mbgl, consisting of a 3-brick corbel footing underlain by concrete. Trial pit TP7, located on the boundary wall consisted of a 2-brick corbel footing. All exposed foundations were constructed on what appears to be made ground of sandy gravelly clay.

Trial pit TP4A exposed the southern and eastern wall foundations. These both consisted of a 3-brick corbel footing extending between 0.15m and 0.19m from the wall and stepping down to a full depth of 0.70mbgl, founded on sand and gravel.

At the location of TP5A the concrete slab extended to a full depth 0.48m below initial paving slabs, with no apparent foundation. The concrete slab contained 10mm and 20mm rebar that appeared to be tied into the retaining wall.

Core 1, which was horizontally drilled into the lightwell retaining wall, had to be terminated at a depth of 0.42m after an obstruction (possibly metal) stopped any further progress. Based on width measurements taken at the top of the wall and in the trial pit TP5A, the width of the wall is thought to be approximately 0.43m.

TP1A exposed the foundations of the boundary wall and the northern wall of the mews property. The boundary wall sat on a single brick corbel, its base proven at a depth of 0.40mbgl. A thin layer of concrete (50mm) over another brick structure was then encountered at 0.50mbgl, extending some 0.30m from the wall, to a depth of 1.00mbgl. This later structure was interpreted to be a pre-existing wall. The northern wall of the property consisted of two brick corbels stepping out 0.15m from the wall, sitting on concrete that extended across the base of the pit. Breaking out confirmed that the base of the concrete extended to a depth of 1.18mbgl.

The foundations exposed in TP2A located on the northern wall of the property consisted of two brick corbels extending 0.14m from the wall. The corbels sat on a concrete screed that extended 0.40m from the wall. Breaking out confirmed that this concrete

was a thin screed over a brick footing, which extended to a total depth of 0.85mbgl. A large tree root, some 50mm in diameter, was encountered within this trial pit at a depth of around 0.55mbgl, associated with the nearby tree. The root appeared healthy, showing no signs of distress.

The foundations of the building encountered within TP3A comprised of concrete with a single step extending approximately 0.2m from the property, to a depth of 0.76mbgl. The trial pit also uncovered the foundations of the boundary wall with 6 Albert Terrace. These showed a brick foundation extending to a depth of 0.25m.

Boreholes and trial pit logs from both stages of the investigation are provided in Appendix E, and for full details reference should be made to the original report.

3 STAGE 1 - SCREENING

This section of the report provides information for the purpose of screening in accordance with the Camden Planning Guidance: Basements (2018) and addresses all questions raised within the relevant sections of that document. Tables summarising the screening flowcharts are shown as Tables 1 to 3. In accordance with procedure, where a 'yes' or 'unknown' response is returned, the potential issue is taken to the scoping stage in Section 4.

Table 1: Subterranean (ground water) screening

Question		Answer	Evidence/Comment
1	Is the site located directly above an aquifer?	No	The site is underlain by up to 2.5m of mixed cohesive and granular made ground overlying the London Clay Formation. The latter is classified as a non-aquifer (non-productive stratum), extending at least 15m beneath the deepest basement level. Furthermore, the potential piezometric surface within the deep aquifer is around -35mAOD (some 70mbgl). p.19 of the ARUP guidance document (Ref: 213923) which supports the Camden Planning Guidance: Basements (2018), states: *"Although groundwater is contained within the microscopic pores of the clayey strata of the London Clay, it permeates so slowly, due to the narrow pores, that in practice it is generally considered a barrier to groundwater".* Therefore, the site does not lie above an aquifer.
1a	Will the proposed basement extend beneath the water table surface?	No	Groundwater was recorded as only a discrete seepage within the claystone band of the London Clay and as perched water in the made ground, albeit at a highest recorded level above the proposed basement formation level. As indicated in Section 2.3, the basement retaining wall structure will be formed by underpinning the boundary walls and extending below the lowest basement level within the London Clay Formation. Although any water seepage recorded above the basement formation level is likely to require controlling in excavations (probable sump pumping) during the temporary works, it is considered that this water does not constitute a 'water table', and its temporary exclusion from the basement excavation is unlikely to have any effect on either the short-term or long-term groundwater regime In the long-term, the granular blanket surrounding the basement structure will allow water to seep around the basement, maintaining long-term sub-surface water flows.

Question		Answer	Evidence/Comment
			In addition, as required by the current design codes, the effects of hydrostatic pressures acting on the proposed structure will be considered a, and the basement walls will be constructed as waterproof to prevent water ingress.
2	Is the site within 100m of a watercourse, well (used/disused) or potential spring line?	No	The nearest watercourse to the site is the Regents Canal some 125m to the south of the site, with a number of ponds further beyond to the south in Regent's Park. The former is a manmade feature therefore, the canal bed is likely to be clay lined, while the latter are shallow static water bodies, not a watercourse. The site does not lie within the vicinity of any buried or culverted rivers or existing or potential spring lines.
3	Is the site within the catchment of the pond chains on Hampstead Heath?	No	The site does not lie within any Hampstead Heath surface water catchment and drainage areas and will therefore not impact any catchments.
4	Will the proposed basement development result in a change in the proportion of hard surfaced / paved areas?	No	Under the proposed development plans, the new basement will be entirely beneath the existing building (area currently covered by hardstanding). Therefore, there will be no net change in the hard surfaced/paved areas.
5	As part of the site drainage, will more surface water (e.g. rainfall and run-off) than at present be discharged to the ground (e.g. via soakaways and/or SUDS)?	No	See response to Question 4, above. The site is currently predominantly hardstanding or building covered and all drainage is conveyed to the existing sewer system. No Sustainable Urban Drainage Systems (SUDS) components, such as soakaways that allow water to soak into the ground, are likely to be proposed for the redevelopment works that would result in more surface water (e.g. rainfall and run-off) than at present being discharged to the ground. Therefore, surface water flow routes will not be materially changed. It is proposed that the existing drainage connection to the public combined sewer is retained and reused. This will be subject to approvals from Thames Water as well as to its location and condition, which will be confirmed by CCTV survey.

Question		Answer	Evidence/Comment
6	Is the lowest point of the proposed excavation (allowing for any drainage and foundation space under the basement floor) close to, or lower than, the mean water level in any local pond (not just the pond chains on Hampstead Heath) or spring line?	Yes	See Section 4 (Scoping)

Table 2: Surface flow and flooding screening

Question		Answer	Evidence/Comment
1	Is the site within the catchment of the pond chains on Hampstead Heath?	No	The site does not lie within any Hampstead Heath surface water catchment and drainage areas and will therefore not impact any catchments.
2	As part of the proposed site drainage, will surface water flows (e.g. volume of rainfall and peak run off) be materially changed from the existing route?	No	The site is currently predominantly covered by hardstanding or building and all drainage is conveyed to the existing sewer system. Under the proposed development plans, the new basement will be beneath the building footprint, and as such there will be no net change in the areas of hard surfaced/paved areas. No Sustainable Urban Drainage Systems (SUDS) components, such as soakaways that allow water to soak into the ground, are likely to be proposed for the redevelopment works that would result in more surface water (e.g. rainfall and run-off) than at present being discharged to the ground.
3	Will the proposed basement development result in a change in the proportion of hard surfaced / paved external areas?	No	The current proposals do not include change in hard surfaced/paved external areas. (See response to Question 2)
4	Will the proposed basement result in changes to the profile of the inflows (instantaneous and long term) of surface water being received by adjacent properties or downstream watercourses?	No	The site is currently mostly hardstanding or building covered and all drainage is conveyed to the existing sewer system. Therefore, surface water flow routes will not be materially changed. There will be no change to the profile of inflows of surface water and there are no nearby watercourses that could be affected.

Question		Answer	Evidence/Comment
			For the temporary condition, any collected water is likely to be pumped to the existing water system. In the permanent condition, the provision of granular drainage blanket around the basement structure will ensure long-term transmissivity of sub-surface seepage.
5	Will the proposed basement result in changes to the quality of surface water being received by adjacent properties or downstream watercourses?	No	There is the potential for pollution discharge or run-off of silty water during the construction phase to impact the adjacent properties. However, it is considered that any potential risks could be readily managed by employing one or a combination of several mitigation techniques that are regularly and successfully employed throughout the construction industry. Control measures employed at the site should comply with CIRIA Report 532 'Control of Water Pollution from Construction Sites' and Environment Agency pollution prevention guidelines, principally PPG6 'Working at Construction and Demolition Sites' and should be included at the detailed design stage.
6	Is the site in an area known to be at risk from surface water flooding, or is it at risk from flooding, for example because the proposed basement is below the static water level of a nearby surface water feature?	No	Reference to the EA floodplain maps, North London Strategic Flood Assessment and The London Borough of Camden flood risk management strategy shows that the site does not lie within any known flood zones. Albert Terrace, Albert Terrace Mews and Regent's Park Road are not in Camden's own list of streets at risk of surface water flooding (Figure 15 of the ARUP report), and lie in an area of low risk of surface water flooding. The proposed basement level is below the level of the Regents Canal and ponds in Regent's Park. However, given the ground and hydrogeological conditions, it is considered highly unlikely that there would be sufficient hydraulic connectivity between the pond and basement excavations to allow drainage of the pond into the excavations. (See response to Question 6 in Subterranean (ground water) screening table).

Table 3: Land Stability Screening

Question		Answer	Evidence/Comment
1	Does the existing site include slopes, natural or manmade, greater than 7º?	No	Information obtained from a site reconnaissance survey, site plans and Ordnance Survey maps indicates that the site area is essentially flat (< 1º). Observations made at the site have not revealed any issues associated with the stability of slopes.
2	Will the proposed re-profiling of landscaping at the site change slopes at the property boundary to more than 7º?	No	The site will be underlain in the majority by the new basement and no re-grading of the site is proposed.
3	Does the development neighbour land, including railway cuttings and the like, with a slope greater than 7º?	No	The neighbouring area follows the general slope angle of the site.
4	Is the site within a wider hillside setting in which the general slope is greater than 7º?	Yes	See Section 4 (Scoping)
5	Is the London Clay the shallowest stratum at the site?	Yes	See Section 4 (Scoping)
6	Will any tree/s be felled as part of the proposed development and/or are any works proposed within any tree protection zones where trees are to be retained?	No	As stated in the arboricultural report (provided under separate cover), the current proposals do not include removal on the existing trees on the site, or new tree planting following the completion of the development, therefore, it is considered that the soil moisture conditions are unlikely to be affected such as to cause swelling/shrinkage that may affect ground stability.
7	Is there a history of seasonal shrink-swell subsidence in the local area, and/or evidence of such effects at the site?	No	There is no immediate or direct evidence of seasonal shrink-swell effects on site. However, given that the underlying natural ground is high volume change potential London Clay there is potential for such effects, but it is not known whether there are any structures that have been affected in the wider area, and in any case, these would be unrelated to the subject site and proposed development.
8	Is the site within 100m of a watercourse or a potential spring line?	No	The nearest watercourse to the site is the Regents Canal some 125m to the south of the site, with a number of ponds further beyond to the south in Regent's Park. The former is a manmade feature, therefore, the canal bed is likely to be clay lined, while the latter are shallow static water bodies, not

Question		Answer	Evidence/Comment
			a watercourse. The site does not lie within the vicinity of any buried or culverted rivers or existing or potential spring lines.
9	Is the site within an area of previously worked ground?	No	A natural ground stability hazard dataset supplied by the BGS and historical and geological mapping (included in the previous RSK desk study and site investigation reports) reveal that there is no hazards associated with previously worked ground, landfilling or compressible ground, and very low hazard with regards to collapsible ground at the site that could lead to stability issues. The site investigations undertaken at the site confirm these ground conditions. Although between up to 2.5m of Made Ground have been recorded, these soils appear to comprise reworked materials associated with previous development of the land and are not considered to present a risk with regard to land stability, particularly as all of this material will be removed as part of the development and the new structure will be supported by natural soils.
10	Is the site within an aquifer? If so, will the proposed basement extend beneath the water table such that dewatering may be required during construction?	No	The site is underlain by up to 2.5m of variable made ground overlying the London Clay Formation. The latter is classified as a non-aquifer (non-productive stratum), extending at least 15m beneath the deepest basement level. Furthermore, the potential piezometric surface within the deep aquifer is around -35mAOD (some 70mbgl). Therefore, the site does not lie above an aquifer. Although the groundwater recorded as seepage within the claystone band of the London Clay and any perched water in the made ground is likely to require controlling in excavations (probable sump pumping) during the temporary works, this water does not constitute ground water with a 'water table', and its temporary exclusion from the basement excavation is unlikely to have any effect on either the short-term or long-term groundwater regime or ground stability. In the long-term, the granular blanket surrounding the basement structure

Question		Answer	Evidence/Comment
			will allow water to seep around the basement, maintaining long-term sub-surface water flows.
11	Is the site within 50m of the Hampstead Heath ponds?	No	The site does not lie within any Hampstead Heath surface water catchment and drainage areas and will therefore not impact any catchments.
12	Is the site within 5m of a highway or pedestrian right of way?	Yes	See Section 4 (Scoping)
13	Will the proposed basement significantly increase the differential depth of foundations relative to neighbouring properties?	Yes	Absence of basement beneath No.5 Albert Terrace Mews is confirmed by Humphrey Kelsey of Humphrey Kelsey Architecture, while as a conservative approach, it is considered that the structure at No.4 Albert Terrace Mews is with a similar configuration. Foundation depths to No.5 ATM and No.4 ATM are assumed to be similar to No.6 ATM, as there are no records of alterations to the super structure and sub-structure of these buildings. It is likely, however, that a number of the neighbouring buildings have basement structures with various depths beneath. Based on the above, potential damaging movements could occur due to basement construction associated with retaining walls and excavation. See Section 4 (Scoping)
14	Is the site over (or within the exclusion zone of) any tunnels?	No	There are no known tunnels, tunnel exclusion zones, or other buried infrastructure directly beneath the site that could be affected by the proposed redevelopment of the site.

4 STAGE 2 – SCOPING

As defined in Camden Planning Guidance: Basements (2018), the scoping stage is used to identify the potential impacts of the proposed scheme for each of the matters of concern identified in the previous screening stage (i.e. those questions answered with a "yes" or "unknown" response). The sections below present statements that define further the matters of concern identified at the screening stage. The data summarised in Section 2 and Section 3 has been used to develop a conceptual ground model to carry out the scoping stage.

4.1 Subterranean (Ground water) Scoping

4.1.1 Is the lowest point of the proposed excavation (allowing for any drainage and foundation space under the basement floor) close to, or lower than, the mean water level in any local pond (not just the pond chains on Hampstead Heath) or spring line?

POTENTIAL IMPACT: Groundwater may drain from the pond or spring and flow into the basement/excavation space.

The lowest excavations at the site are for the sub-basement structures, within which excavations will extend to 29.45mAOD. This will possibly take the excavation below the base of the Regents Canal and nearby ponds in Regent's Park.

As stated above, the site is underlain by up to 2.5m of variable made ground, below which the London Clay Formation was encountered. The London Clay on site has been determined, both by field and laboratory testing, to be high plasticity silty clay.

Groundwater has been encountered during the investigation as a seepage in the made ground and within the claystone band in the London Clay at a highest recorded level of 32.55mAOD. However, as stated previously, this is not considered to be a 'groundwater table' in hydraulic continuity with any watercourses in the vicinity of the site. The porosity of the London Clay is so low that it does not contain significant volumes of water, and is of very low permeability and poor drainage characteristics.

Therefore, although there is possibly a 'head differential' between the water in Regents Canal and ponds and the basement excavations, it is considered, given the encountered ground and hydrogeological conditions, highly unlikely that there would be sufficient hydraulic connectivity between the pond and basement excavations to allow drainage of the pond into the excavations.

4.2 Land Stability Scoping

4.2.1 Is the site within a wider hillside setting in which the general slope is greater than 7?

POTENTIAL IMPACT: Slope stability within neighbouring site(s).

Figure 16 of the ARUP guidance document (ref: 213923) which supports Camden Planning Guidance: Basements (2018), indicates that slopes in the site area (Primrose

Hill to the west of the site) are locally in the range 7º to 10º, although the regional slope in the site area is generally <7º. The site area is urbanised and as such the slopes in the site's vicinity are likely to have been cut or altered historically due to development and landscaping.

The 1:50,000 scale geological map for the area indicates that the site does not lie within an 'Area of Significant Landslide Potential'. The BGS landslide potential map is reproduced as figure 17 of the ARUP report. With reference to topographical site plans, there are no identified significant slopes across the sites boundaries.

Therefore, it is considered that there are no significant slopes in neighbouring land that could potentially be affected by the proposed works at No.6 Albert Terrace Mews.

4.2.2 QUESTION: Is the London Clay the shallowest stratum at the site?

POTENTIAL IMPACT: The London Clay is prone to seasonal shrink-swell (subsidence and heave)

The existing building on site and the proposed basement development will share a party wall with No.5 Albert Terrace Mews. However, the new structure will have a basement level and will be supported on foundations that will be at depths where there is no influence from seasonal shrink-swell.

Similarly, it is considered unlikely that the proposed development could affect changes to the 'shrink-swell' regime at the site that could extend beyond the site boundary to affect other structures in the area.

4.2.3 QUESTION: Is the site within 5m of a highway or pedestrian right of way?

POTENTIAL IMPACT: Excavation for a basement may result in damage to the road, pavement or any underground services buried in trenches beneath the road or pavement.

The eastern and northern boundaries of the site are within 5m of the pavements along Albert Terrace Mews and Regent's Park Road, respectively.

There is the potential for ground movements associated with basement underpins installation and basement excavation to impact the adjacent road. An impact assessment addressing this issue is reported on in Section 6.

4.2.4 QUESTION: Will the proposed basement significantly increase the differential depth of foundations relative to neighbouring properties?

POTENTIAL IMPACT: Excavation for a basement may result in structural damage to neighbouring properties/structures if there is a significant differential depth between adjacent foundations.

The proposed structure shares a party wall with No.5 Albert Terrace Mews, but is widely separated from other neighbouring properties (>15m distant from buildings along Regent's Park Road to the north of the site, and >10m from the properties located along Albert Terrace to the west of the site). Given its age, it is probable that the adjacent No.5 building is founded on traditional spread foundations, confirmed by the Architects. As a conservative approach, it is considered that the structure at No.4 Albert Terrace Mews is with a similar configuration.

It is almost certainly the case that the proposed basement construction will result in differential foundation depths. Therefore, identified hazards are associated with ground movements from perimeter retaining wall installation and ground excavation, and elastic heave of the London Clay in the basement excavation associated with stress release.

As part of this assessment the following nearby structures have been identified as being potentially at risk from damaging ground movements:

- No.5 Albert Terrace Mews at the southern boundary;
- No.4 Albert Terrace Mews at the southern boundary; and
- The adjacent highways of Albert Terrace Mews and Regent's Park Road beyond the eastern and northern boundaries of the site.

An impact assessment addressing these issues is reported on in Section 6.

5 STAGE 3 – SITE INVESTIGATION AND STUDY

As previously noted, a desk study and an intrusive site investigation were undertaken at the site of No. 6 Albert Terrace, by RSK between February and March 2017, as detailed in the report 'Geo-environmental Site Assessment: 6 Albert Terrace, Primrose Hill, Camden', reference no. 29123-01(01), dated May 2017. This was followed by further investigations at No.6 Albert Terrace Mews, carried out in March 2018, as detailed in report 'Geo-environmental Site Assessment: 6 Albert Terrace Mews, Primrose Hill, Camden', reference no. 29841-01(00), dated May 2018. Both investigations are compliant with the data requirements as set out in Appendix G of 'Camden Geological, Hydrogeological and Hydrological Study' produced for Camden by ARUP in November 2010.

A summary of the findings is provided in Section 2.4.2, while extract of the borehole and trail pit logs if provided in Appendix E.

The results of the initial and additional works have been utilised to inform the scoping stage of the BIA and the current assessment draws on the results of those reports.

6 STAGE 4 - IMPACT ASSESSMENT

6.1 Introduction

This stage is concerned with evaluating the direct and indirect implications of the proposed basement development. It involves describing, quantifying and aggregating the effects of the development on those attributes or features which have been identified in the scoping stage as being potentially affected.

The only potential impacts that have been identified by this assessment relate to ground stability hazards associated with:

- Movements associated with basement retaining wall installation and ground excavation; and
- Elastic heave of the London Clay in the basement excavation associated with stress release.

The following nearby structures have been identified for assessment in relation to potential ground movements

- No.5 Albert Terrace Mews at the southern boundary;
- No.4 Albert Terrace Mews at the southern boundary; and
- The adjacent highways of Albert Terrace Mews and Regent's Park Road beyond the eastern and northern boundaries of the site.

6.2 Scope of Works

The scope of works following the screening and scoping stages has been summarised and is as presented below:

- Model the construction sequence on site from excavation through to the proposed development using OASYS PDISP 19.3 elastic analysis package;
- Output displacements along the line of the neighbouring building foundations at the various stages of construction;
- Estimate the likely ground movements resulting from installation of the proposed underpinnig and basement excavation based on the empirical information contained in CIRIA C760 "Guidance on Embedded Retaining Wall Design" 2017 using the OASYS XDISP 19.4 software;
- Use the program XDISP to combine the ground displacements determined from the numerical analyses PDISP and the CIRIA C760 assessment; and
- From the resulting displacements determine the strains that are likely to be induced in the neighbouring buildings / highways to derive a likely damage classification.

6.3 Vertical Elastic Displacements Analysis

6.3.1 PDISP Ground Model Construction

A settlement/heave analysis has been completed adopting the OASYS PDISP 19.3.0.16 software produced by ARUP to assess the likely vertical ground movements to be expected from the proposed development activities.

The PDISP computer package adopts the Boussinesq method of elastic analysis to calculate the stresses and strains generated within the soil due to an applied loading, and to determine the associated displacements by integrating the vertical strains. Settlements are defined as positive movements and heave as negative movements. It should be noted, however, that the calculated results do not take into consideration the influence of the basement perimeter wall, as the increased stiffness at this boundary cannot be incorporated into the model. As such, the analyses can be considered conservative.

The loads applied in the PDISP model are split into various elements, those applied from unloading, and those applied from loading of the underpinning around the perimeter. The application of loads to represent excavation is completed by applying negative load at the base of excavation, whereas the loads applied from reloading or construction are applied by inducing a positive load.

Stiffness (Young's modulus) for the London Clay Formation this has been estimated from the undrained shear strength (C_u) obtained from the SPT 'N' values and the triaxial laboratory testing, using the correlation $E_u=400C_u$, presented by Jamiolkowski, et al, contained within CIRIA Special Publication 27, Settlement of Structures on Clay Soils, 1983. The drained soil stiffness was obtained from the correlation $E' = 0.8E_u$.

The final adopted ground profile and associated parameters are presented in the table below:

Table 4: Summary of adopted ground profile and associated stiffness parameters

Strata	Level of top of stratum mAOD	Level of base of stratum mAOD	Undrained Conditions		Drained Conditions	
			E_u MN/m²	ν	E' MN/m²	ν'
Made Ground (assumed cohesive)	35.0	32.5	9.6	0.5	7.68	0.2
London Clay Formation	32.5	15.0	20.0 – at surface 75.0 – at base		16.0 at surface 60.0 at base	

For the purpose of the assessment, a rigid boundary was assumed to be at -15mAOD, below which no movement is considered to occur.

The following PDISP analyses have been undertaken to determine the ground movements at key stages in the constructions process:

- **Basement Excavation**. This has been calculated by the removal of an overburden pressure for the proposed areas of basement extension. For the proposed development, around 4m excavation is expected in the area of the new basement. This equates to a uniform unloading across the basement footprint of some 80kN/m^2, assuming 20kN/m^3 unit weight of soil.

- **Loading from the proposed new basement on underpins and basement slab.** The loading from the proposed new development were modelled as linear loads along the boundary walls, with the internal column loading spread as a uniform load applied across the entire slab area.

The analysis has considered both undrained and drained soil conditions to give an indication of the immediate short term and the maximum expected long term ground movements resulting from the proposed development.

The first of these analyses allows an assessment of the immediate elastic heave that would result from excavation. This would typically be expected to occur over a period of a few weeks. The second analysis allows for long term net movements following construction of the new development, which will include the total heave that would develop in the long term and settlement following consolidation of the underlying clay following the loading. The fully drained (long term) conditions would typically take many years to develop (10 years or more).

6.3.2 Analysis Results

6.3.2.1 Basement Construction

For the unloading stage, the results indicate that the unloading will result in a maximum short-term heave displacement of up to 9.5mm towards the centre of the basement, reducing to between 3mm and 4.5mm at the boundaries and up to 5.5mm at the boundary with No.5 Albert Terrace Mews.

For the long-term (drained) conditions, maximum heave displacements of around 17.5mm are anticipated in the centre, and 5mm to 8mm at the boundaries (around 10.5m at the boundary with No.5 Albert Terrace Mews). However, it is considered extremely unlikely that this condition will arise during a standard construction programme.

6.3.2.2 Reloading Following Construction

For the final loading stage, a drained analysis has been undertaken as fully drained conditions are expected to occur in the long-term.

The results indicate a reduction of the net heave movements to around 14.5mm following the construction of the basement, with the anticipated movements at the boundaries between 5mm and 7mm (8mm at No.5 Albert Terrace Mews).

The results of the numerical analysis and graphical presentation of these results are presented in Appendix D.

6.4 Empirical Assessment of Building Damage

6.4.1 Preamble

The approach adopted for the purpose of this assessment, combines both CIRIA C760 and the net long term vertical movements for the various construction stages obtained from PDISP.

In this case, the results of numerical modelling using PDISP for various construction stages have been imported into the XDISP software and an assessment of potential damage for each stage has been completed using the C760 approach of assessing lateral strain and deflection ratio to determine potential damage category.

The deformations and associated potential damage of the various adjacent buildings have been determined at the end of the stages of construction presented in Table 5.

Table 5: Stages of Construction at which Building Damage is assessed

No.	Construction Stage	Short / Long Term	Cumulative Effect
1	Basement construction	Short	(A) + (B)
2	Basement construction and proposed development	Long	(A) + (B) + {(D) – (C)} + (F)

The various elements of work used to determine the deformations for the buildings at the various stages of construction are given in Table 6. This table also defines how the associated movements have been determined and whether they are long or short term.

Table 6: Construction Sequence

Element	Construction Component	Calculation Method	Short or Long Term
A	Basement wall installation	CIRIA C760 (XDISP)	Short Term
B	Basement excavation	CIRIA C760 (XDISP)	Short Term
C	Basement excavation	PDISP	Short Term
D	Basement excavation	PDISP	Long Term
E	Loading of new structure	PDISP	Short Term
F	Loading of new structure	PDISP	Long Term

The ground deformations and building damage categories following each of these stages of construction have been derived by combining the deformations calculated for the various elements of work carried out as indicated in Table 5.

The assessment has been undertaken using XDISP version 19.4.0.10 computer package supplied by OASYS, which uses the empirical approach outlined in CIRIA C580 to assess vertical and horizontal ground movements resulting from installation of embedded retaining walls and excavation in front of walls. It should be noted that XDISP version 19.4.0.10 was developed at which time CIRIA C580 was still the current guidance, the only observable difference with regards to assessing building damage is

a change to the ground movement curves for excavation in front of a low stiffness wall which were reduced in CIRIA C760.

The empirical approach is well described in CIRIA C760 “Guidance on Embedded Retaining Wall Design” 2017. This document provides charts of vertical and horizontal ground movements resulting from installation of embedded retaining walls and excavation in front of the walls. These charts have been normalised with wall length and excavation depth to facilitate their use for new development. As noted above the charts remain applicable for the purpose of this assessment, the only difference being a more conservative approach has been adopted for excavations in front of a low stiffness wall in the updated CIRIA C760.

6.4.2 Assessment of Damage to Adjacent Properties

CIRIA C760 also provides a methodology for assessing the potential damage to properties within the zone of influence of the basement excavation. Figures 6.17 and 6.27 of CIRIA C760 summarise this approach. This methodology uses the relationship between Damage Category, horizontal strain and deflection ratio developed by Boscardin and Cording (1989) and Burland (2001).

The definition of the categories is presented in Table 7, below.

Table 7: Classification of damage category (from Table 6.4, CIRIA C760)

Category of damage	Description of typical damage	Approximate crack width (mm)	Limiting tensile strain ε_{lim} (%)
0 Negligible	Hairline cracks of less than about 0.1mm are classed as negligible.	<0.1	0.00 - 0.05
1 Very slight	Fine cracks that can easily be treated during normal decoration. Cracks in external brickwork visible on inspection.	<1	0.05 - 0.075
2 Slight	Cracks easily filled. Redecoration probably required. Cracks are visible externally and some repointing may be required externally to ensure watertightness. Doors and windows may stick slightly.	<5	0.075 - 0.15
3 Moderate	The cracks require some opening up and can be patched by a mason. Repointing of external brickwork and possibly a small amount of brickwork to be replaced. Doors and windows sticking. Service pipes may fracture. Weathertightness often impaired.	5 – 15 or a number of cracks >3	0.15 - 0.3
4 Severe	Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows. Windows and frames distorted, floor sloping noticeably. Walls leaning or bulging noticeably, some loss of bearing in beams. Service pipes disrupted.	15 – 25 but also depends on number of cracks	>0.3

Category of damage	Description of typical damage	Approximate crack width (mm)	Limiting tensile strain ε_{lim} (%)
5 Very severe	This requires a major repair involving partial or complete rebuilding. Beams lose bearings, walls lean badly and require shoring. Windows broken with distortion. Danger of instability.	Usually >25 but depends on number of cracks	

6.4.3 Buildings to be Assessed

As specified in the previous sections a number of buildings surround the site. However, the property considered to be potentially most at risk is No.5 Albert Terrace Mews, which shares a party wall at the southern site boundary and No.4 Albert Terrace Mews, which is considered to be within the zone of influence of the proposed basement.

Absence of basement beneath No.5 Albert Terrace Mews is confirmed by Humphrey Kelsey of Humphrey Kelsey Architecture. Foundation depths to No.5 and No.4 Albert Terrace Mews are assumed to be similar to No.6, as there are no records of alterations to the super structure and sub-structure of these buildings. Other information was obtained during the walkover, investigation works, and what is known about the existing development construction. Where site specific information is not known then conservative assumptions have been made.

On the basis of the available information, a summary of the specific dimensions and construction details used for these analyses are presented in Table 8 and Table 9, below.

Table 8: Specific dimensions used for C760 analyses

Adjacent Structure	Estimated Wall Depth (mAOD)	Excavation Depth (mAOD)	Distance to Face of Structure (m)	Length of Structure Perpend. to Basement (m)	Height of Property (m)
No.5 Albert Terrace Mews	28.95	29.45	adjacent	10.0	2 storey (6m)
No.4 Albert Terrace Mews			10.0	10.0	

Table 9: Construction details used for C760 analyses

Adjacent Structure	Building Material[1)]	Foundation Type[1)]	Foundation Level (mAOD) [1)]
No.5 Albert Terrace Mews	Brick Masonry	Strip/Raft	32.67
No.4 Albert Terrace Mews			

[1)] assumed values in absence of further information

6.4.4 Results of Empirical Assessment of Ground Movements and Building Strains

In the temporary condition, the proposed basement excavation will be retained by underpinning supported by rigid propping, while in the permanent condition the retaining wall will be rigidly propped by the basement floor and ground floor reinforced concrete slabs. Whilst the underpinning falls outside of the C760 guidance, it has been assumed that comparable movements associated with diaphragm wall installation may be expected.

Providing good workmanship and adequate precautions are taken during the construction, the anticipated settlements of the party walls onto the underpins are likely to be significantly reduced, while the lateral displacements are also anticipated to me minimal. On that basis, it is considered that the movements resulting from the installation of the underpinning are likely to be highly overestimated.

The results of the numerical analysis during the key stages of construction are given in Appendix B and D and summarised below.

6.4.4.1 Basement Construction

A summary of the estimated ground movements likely to be experienced following completion of the basement construction are presented in Table 10, below.

Table 10: Ground Movements Resulting from Basement Construction

Adjacent Property	Ground Movement at Front of Adjacent Property		Ground Movement at Rear of Adjacent Property	
	Lateral (mm)	Vertical (mm)	Lateral (mm)	Vertical (mm)
No.5 Albert Terrace Mews	7.16	7.88	2.66	1.32
No.4 Albert Terrace Mews	2.21	0.84	0.00	0.00

Notes:

- Lateral displacement recorded as movement along the line.
- Positive lateral displacement values indicate ground movement towards the excavation.
- Negative vertical displacement values indicate ground heave.

Reference to monitoring information for underpinning on similar sites in London indicate that movements of between 5mm to 10mm are anticipated for a single lift of underpinning. The above movements are within those limits and considered to be a relatively accurate reflection of the actual movements anticipated at this stage.

The associated horizontal strains and deflection ratios and a resulting damage category are provided in Table 11.

Table 11: Calculated Horizontal Strains and Deflection Ratios

Adjacent Building	Horizontal Strain (%)	Deflection Ratio (%)	Damage Category
No.5 Albert Terrace Mews	0.045000	0.0188570	1 (Very Slight)

Adjacent Building	Horizontal Strain (%)	Deflection Ratio (%)	Damage Category
No.4 Albert Terrace Mews	0.045000	0.0065643	0 (Negligible)

6.4.4.2 Reloading Following Construction

A summary of the estimated ground movements and the maximum resulting horizontal strains and deflection ratios following completion of the development are presented in Table 12 and Table 13, overleaf.

Table 12: Ground Movements Resulting from Long Term Loading

Adjacent Property	Ground Movement at Front of Adjacent Property		Ground Movement at Rear of Adjacent Property	
	Lateral (mm)	Vertical (mm)	Lateral (mm)	Vertical (mm)
No.5 Albert Terrace Mews	7.16	6.13	2.66	0.96
No.4 Albert Terrace Mews	2.21	0.52	0.00	-0.12

Notes:

- Lateral displacement recorded as movement along the line.
- Positive lateral displacement values indicate ground movement towards the excavation.
- Negative vertical displacement values indicate ground heave.

Table 13: Calculated Horizontal Strains and Deflection Ratios

Adjacent Building	Horizontal Strain (%)	Deflection Ratio (%)	Damage Category
No.5 Albert Terrace Mews	0.450000	0.0231620	1 (Very Slight)
No.4 Albert Terrace Mews	0.033582	0.0061583	0 (Negligible)

On the basis of the above, it is considered that the damage category for the adjacent No.5 Albert Terrace Mews will be 'Very Slight' (Category 1), while the damage category for No.4 Albert Terrace Mews will be 'Negligible' (Category 0), which fulfils the requirements of the LBC guidance document Camden Planning Guidance: Basements (2018).

However, note that that this is fully dependent on the good workmanship and control during the installation process, which is identified in the Construction Method Statement. In particular, it is recommended that the underpins are founded in competent strata (ideally the natural London Clay), and the water seepage excluded from the excavation, to reduce the risk of local instability in the shallow made ground during the excavation.

The above damage categories would only apply strictly to structures of brick/mortar construction, which applies to No.5 and No.4 Albert Terrace Mews. The roads/pavements along Albert Terrace Mews and Regent's Park Road do not fall into

that category of structures. With regards to these structures, small vertical differential movements of up to <1mm are calculated over the width of the Albert Terrace Mews pavement (taken as 4m), while the vertical differential movements over 10m width of Regent's Park Road are calculated to be 3.8mm. No damaging deflections are recorded and the differential movement is rotational (tilt). These small vertical differentials equate to gradients of between 1:2650 to 1:8000, or slope angles of between 0.0072º to 0.0216º. Tensile horizontal strains are calculated to be between 0.072247% and 0.076454%. Given that road pavements are flexible structures it is considered that these small strains and rotations will have no damaging effect on the highways of Albert Terrace Mews and Regent's Park Road.

7 CUMMULATIVE IMPACTS

A requirement of Camden Planning Guidance: Basements (2018) is to consider the aggregate (cumulative) potential for impacts associated with basement construction.

A search of publicly available planning records (dating back to 1924) on Camden's planning website revealed records of granted permissions for basement/lower ground floor development/extension or other subterranean development (e.g. swimming pool accommodation space) for properties in the site area located along the Regent's Park Road, Albert Terrace and Albert Terrace Mews.

7.1 Hydrogeology

In regard to cumulative impacts, the concern is that due to the lowest excavations at the site extending below the recorded perched water seepages the basement could form a barrier to groundwater flow if it is contiguous with adjacent basements. This is understood not to be the case in this instance due to the absence of contiguous basements and that, in any case, the recorded perched water seepages do not constitute a wider and significant groundwater body.

Following construction, a granular blanket surrounding the basement structure will allow water to seep around the basement, maintaining any long-term sub-surface perched water movement.

On that basis we consider that the construction of the proposed basement at the No.6 Albert Terrace Mews would not contribute further to any cumulative effects.

7.2 Hydrology

There will be negligible potential for impact and no cumulative impact on surface water flows in the vicinity of the proposed development.

7.3 Land Stability

From the results of the elastic displacement analyses it is indicated that in both the short-term and long-term (once building loads are applied), net movements beyond the site boundary will be relatively low and within acceptable limits.

Providing good workmanship and control during the installation process are maintained, the associated displacements are likely to result in relatively small horizontal strains and deflection ratios, which are unlikely to be damaging to the identified features (i.e. 'Very Slight' (Category 1).

The impact on the adjacent properties from the construction of basements beneath No. 6 Albert Terrace was undertaken under separate assessment. The assessments result in Category 0 and 1 (Negligible and Very Slight) for the relevant adjacent properties and infrastructure. Given the distance between the developments at No.6 Albert Terrace Mews and No.6 and No.5 Albert Terrace (around 10m to 15m), it is considered that the cumulative impact from both developments on the adjacent properties will not be significantly different from the ones calculated by each separate assessment.

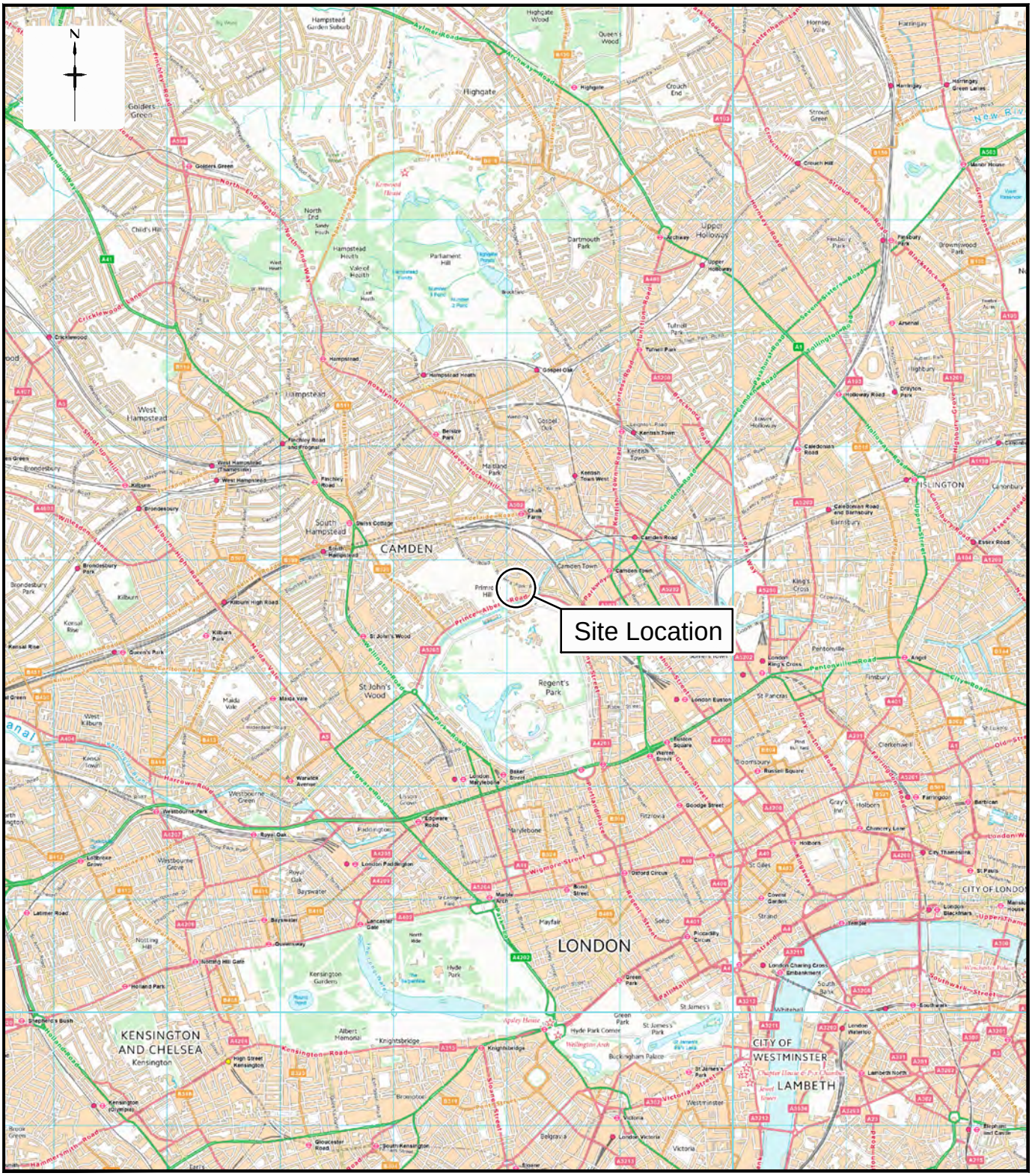
It should be noted that the calculations undertaken as part of this assessment are necessarily preliminary and these calculations should be re-checked at the detailed design stage to ensure that more detailed predicted movements are within tolerable limits.

7.3.1 Control of ground movements

In order to reduce the potential for any movement over and above that expected, the following methods of safe practice should be considered prior to and during construction:

- Good workmanship will be required to ensure that underpinning installation induced settlements are kept to a minimum;
- The underpinning should be taken in competent strata (ideally the natural London Clay), and the water seepage excluded from the excavation, to reduce the risk of local instability in the shallow made ground during the excavation.
- It should be ensured that basement slab is cast as early as possible and tight to the underpinning wall.;
- Where temporary props are required they should be designed to provide adequate restraint to limit lateral ground movements. Walings should be tied in so they do not rely on friction or adhesion between the prop end and waling to be held in place;
- The first stage of excavation should be minimised and the first (stiff) support should be installed as early as possible in the construction sequence;
- The construction of the wall and its support systems should not be delayed;
- Over-excavation should be avoided;
- Monitoring both above and below ground should be carried out to ensure that the expected displacements are not exceeded. Limits of lateral and vertical displacement should be set beyond which the method of construction should be re-assessed.

FIGURES



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Drawing Title: SITE LOCATION PLAN

Rev	Drawn	Date	Checked	Date	Approved	Date
01	ASC	19.06.18	CJB	19.06.18	ST	19.06.18

Dimensions	Scale	Original Size
m	1:50,000	A4

Project Number	Drawing File	Drawing Number
29841 - R02 (02)	29841 - SLP.dwg	FIGURE 1

LEGEND

Trial pit location

Rev.	Date	Amendment	Drawn	Chkd.	Appd.
P1	19.06.18	FIRST ISSUE	ASC	ST	ST

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Web: www.rsk.co.uk

Client

MR. MARK GOLINSKY

Project Title

6 ALBERT TERRACE MEWS, PRIMROSE HILL

Drawing Title

EXPLORATORY HOLE LOCATION PLAN

Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

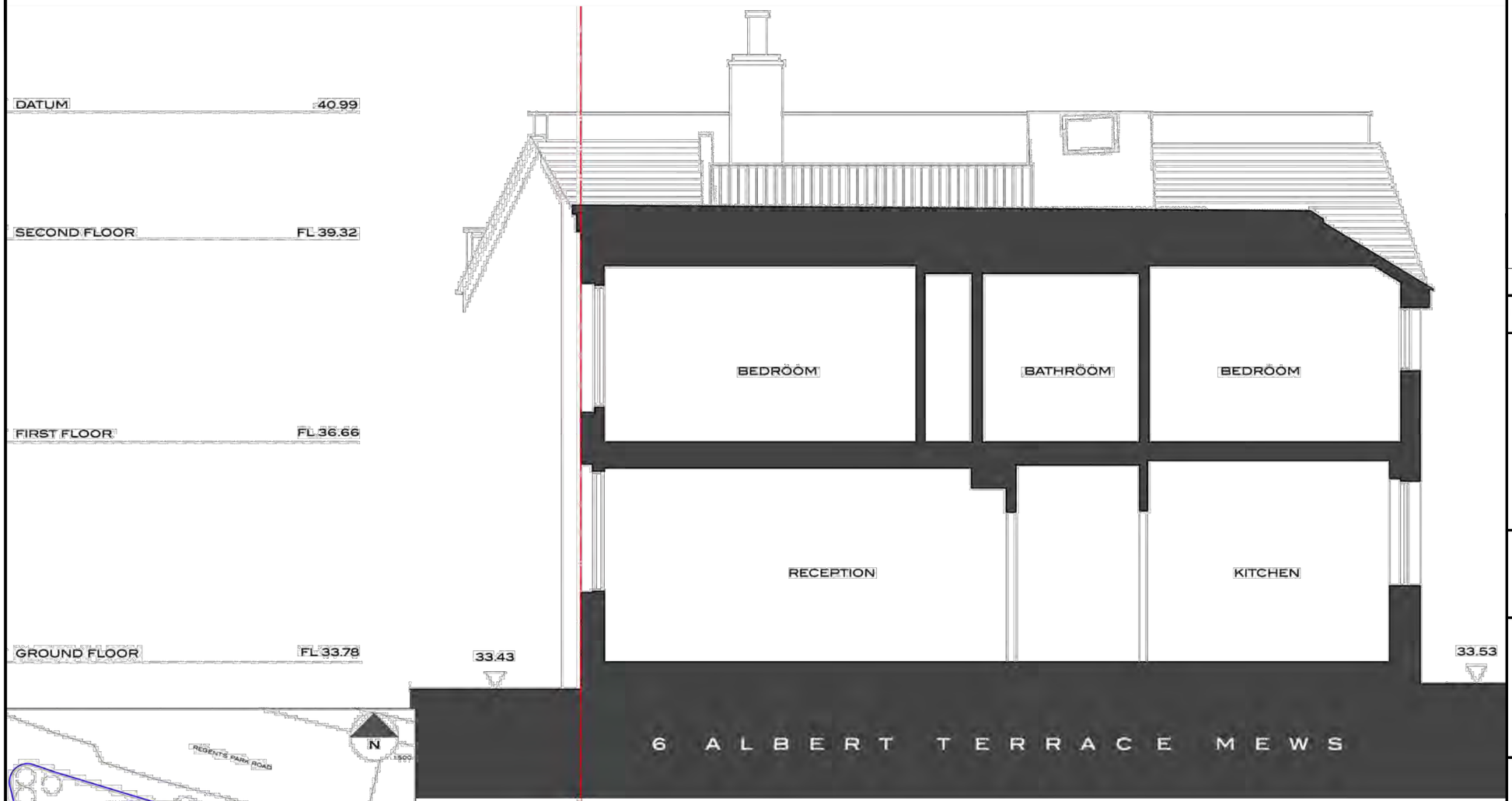
Scale	Orig Size	Dimensions
1:100	A3	m

Project No.	Drawing File
29841 - R02 (02)	29841 (R02-00) Fig 2.dwg

Drawing No.	Rev.
FIGURE 2	P1

Scale 1 : 100

0 1 2 3 4 5m



LEGEND

Rev.	Date	Amendment	Drawn	Chkd.	Appd.
P1	29.06.18	FIRST ISSUE	ASC	ST	ST

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MR. MARK GOLINSKY

Project Title

6 ALBERT TERRACE MEWS,
PRIMROSE HILL

Drawing Title

EXISTING SECTIONS
D-D'

Drawn	Date	Checked	Date	Approved	Date
ASC	29.06.18	ST	29.06.18	ST	29.06.18

Scale	Orig Size	Dimensions
1:125	A3	m

Project No.	Drawing File
29841 - R01(02)	29841 (R02-00) Fig 3.dwg

Drawing No.	Rev.
FIGURE 3	P1

Scale 1 : 125

0 1 2 3 4 5m

APPENDIX A
PROPOSED DEVELOPMENT PLANS AND SECTIONS

Scale 1 : 125

0 1 2 3 4 5 6 7 8 9 10m

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	29.06.18	ST	29.06.18	ST	29.06.18

Scale	Orig Size	Dimensions
1:125	A3	m

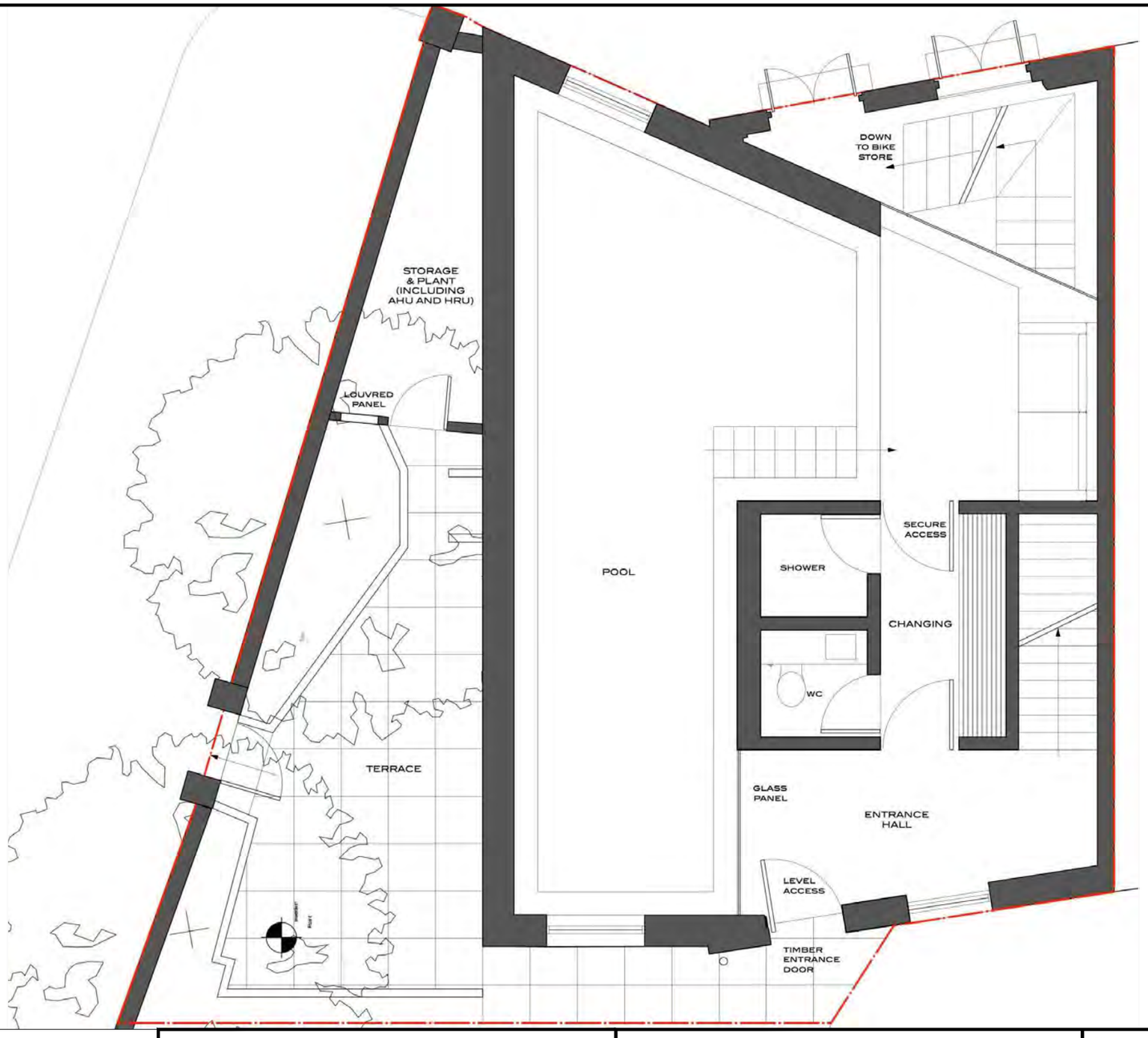
Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS,
PRIMROSE HILL, LONDON

Drawing Title
PROPOSED
BASEMENT PLAN

Project No.	Drawing File
29841 - R01 (00)	29841 (R02-00) App A.1.dwg

Drawing No.	Rev.
APPENDIX A.1	P1



Scale 1 : 125

0 1 2 3 4 5 6 7 8 9 10m

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

RSK
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Drawn	Date	Checked	Date	Approved	Date
ASC	29.06.18	ST	29.06.18	ST	29.06.18

Scale	Orig Size	Dimensions
1:125	A3	m

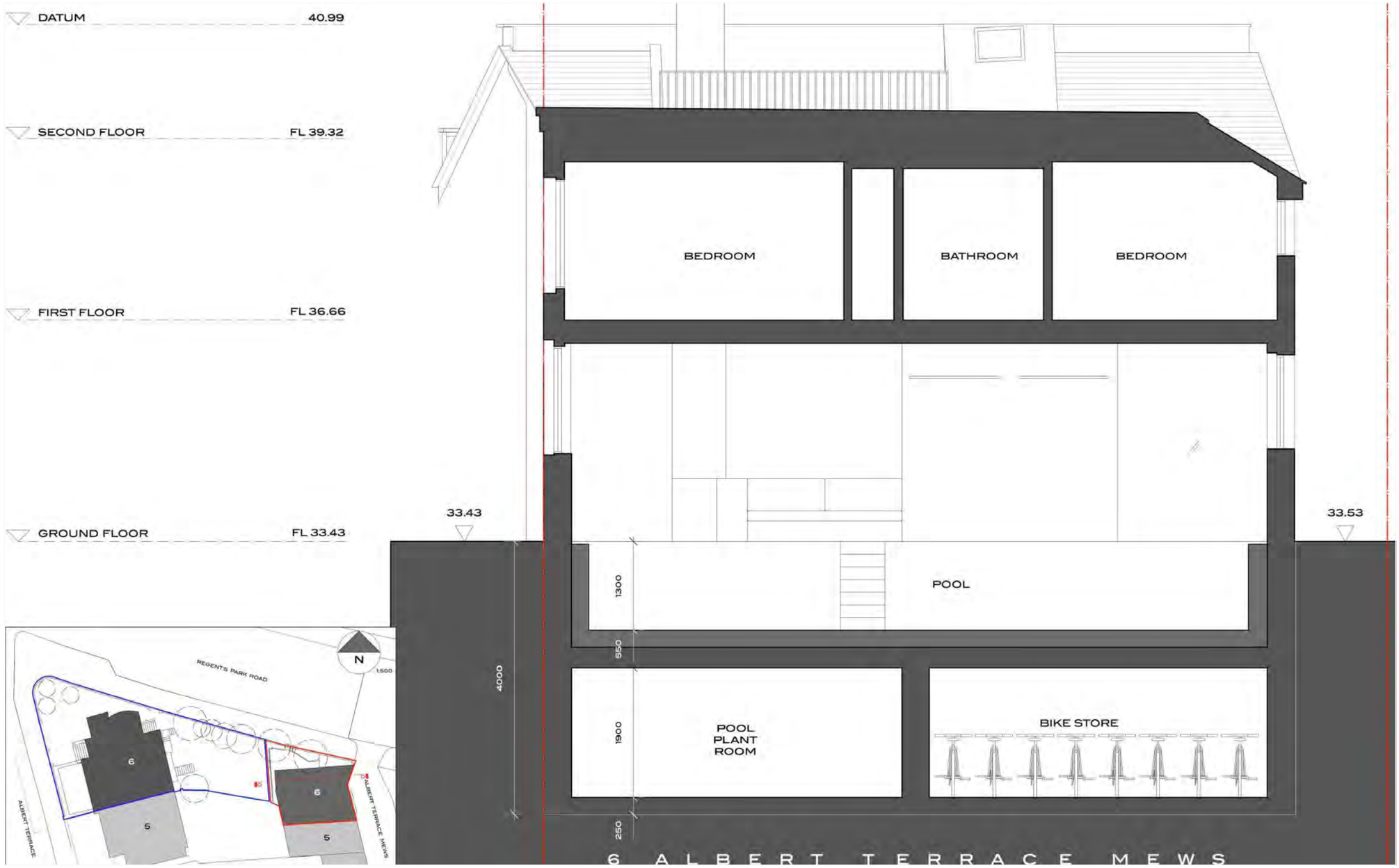
Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS,
PRIMROSE HILL, LONDON

Drawing Title
PROPOSED
GROUND FLOOR PLAN

Project No.	Drawing File
29841 - R02 (00)	29841 (R02-00) App A.2.dwg

Drawing No.	Rev.
APPENDIX A.2	P1



Scale 1 : 125

0 1 2 3 4 5 6 7 8 9 10m

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

Scale	Orig Size	Dimensions
1:125	A3	m

Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS,
PRIMROSE HILL, LONDON

Drawing Title
PROPOSED
SECTION D-D'

Project No.	Drawing File
29841 - R01 (00)	29841 (R02-00) App A.3.dwg

Drawing No.	Rev.
APPENDIX A.3	P1

DATUM 40.99

SECOND FLOOR FL 39.32

FIRST FLOOR FL 36.66

GROUND FLOOR FL 33.43

Scale 1 : 125

0 1 2 3 4 5 6 7 8 9 10m

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	29.06.18	ST	29.06.18	ST	29.06.18

Scale	Orig Size	Dimensions
1:125	A3	m

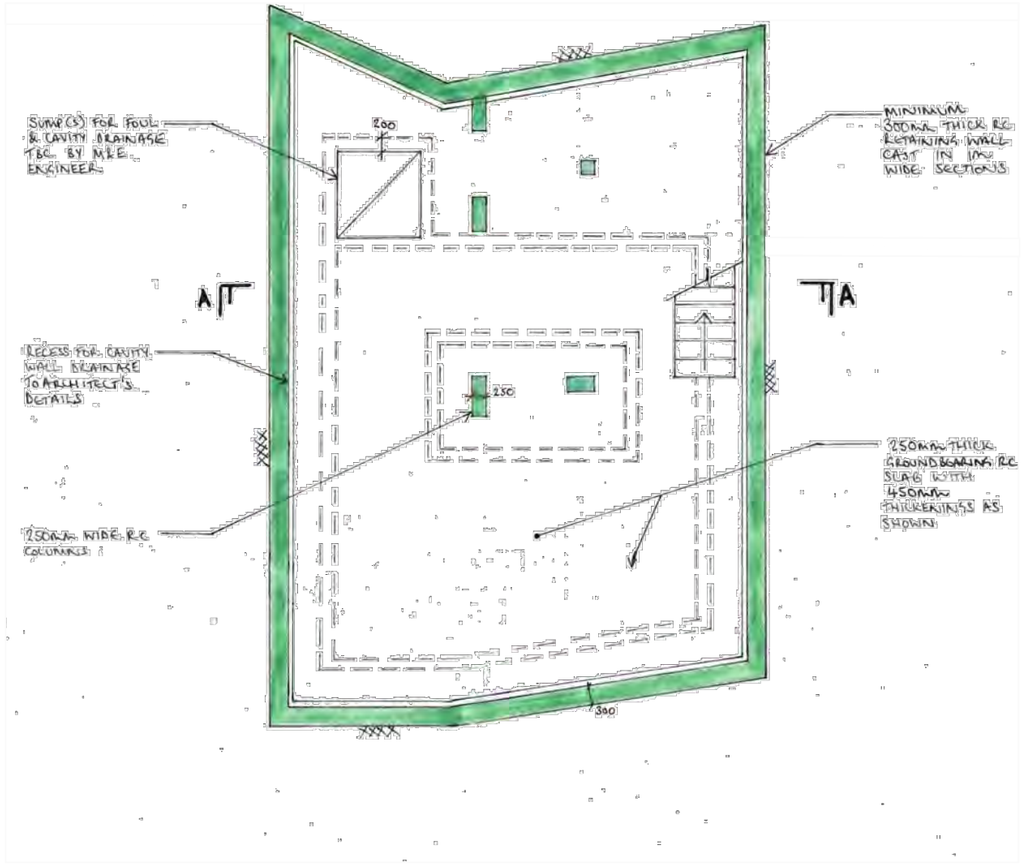
Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS,
PRIMROSE HILL, LONDON

Drawing Title
PROPOSED
SECTION E-E'

Project No.	Drawing File
29841 - R02 (00)	29841 (R02-00) App A.4.dwg

Drawing No.	Rev.
APPENDIX A.4	P1



Scale 1 : 100

0 1 2 3 4 5 6 7 8 9 10m

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

Scale	Orig Size	Dimensions
1:100	A3	m

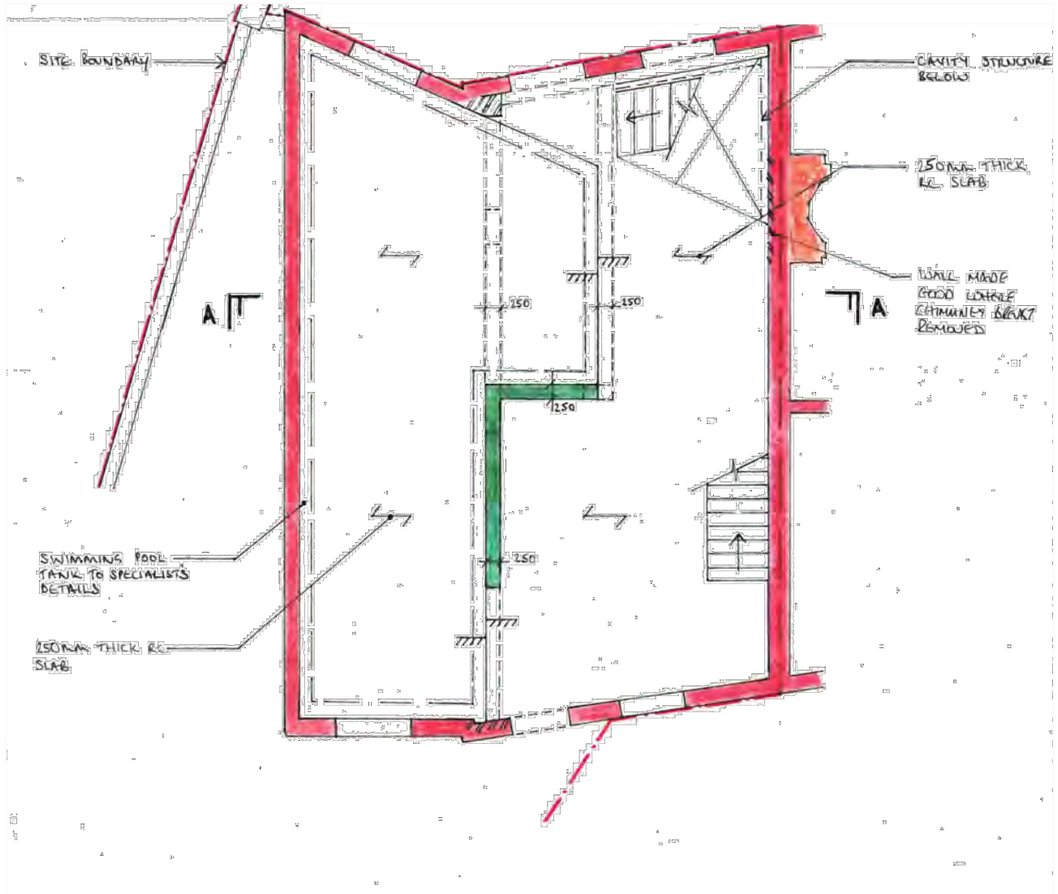
Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS,
PRIMROSE HILL, LONDON

Drawing Title
PROPOSED
BASEMENT STRUCUTRE

Project No.	Drawing File
29841 - R01 (00)	29841 (R02-00) App A.5.dwg

Drawing No.	Rev.
APPENDIX A.5	P1



Scale 1 : 100

0 1 2 3 4 5 6 7 8 9 10m

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

Scale	Orig Size	Dimensions
1:100	A3	m

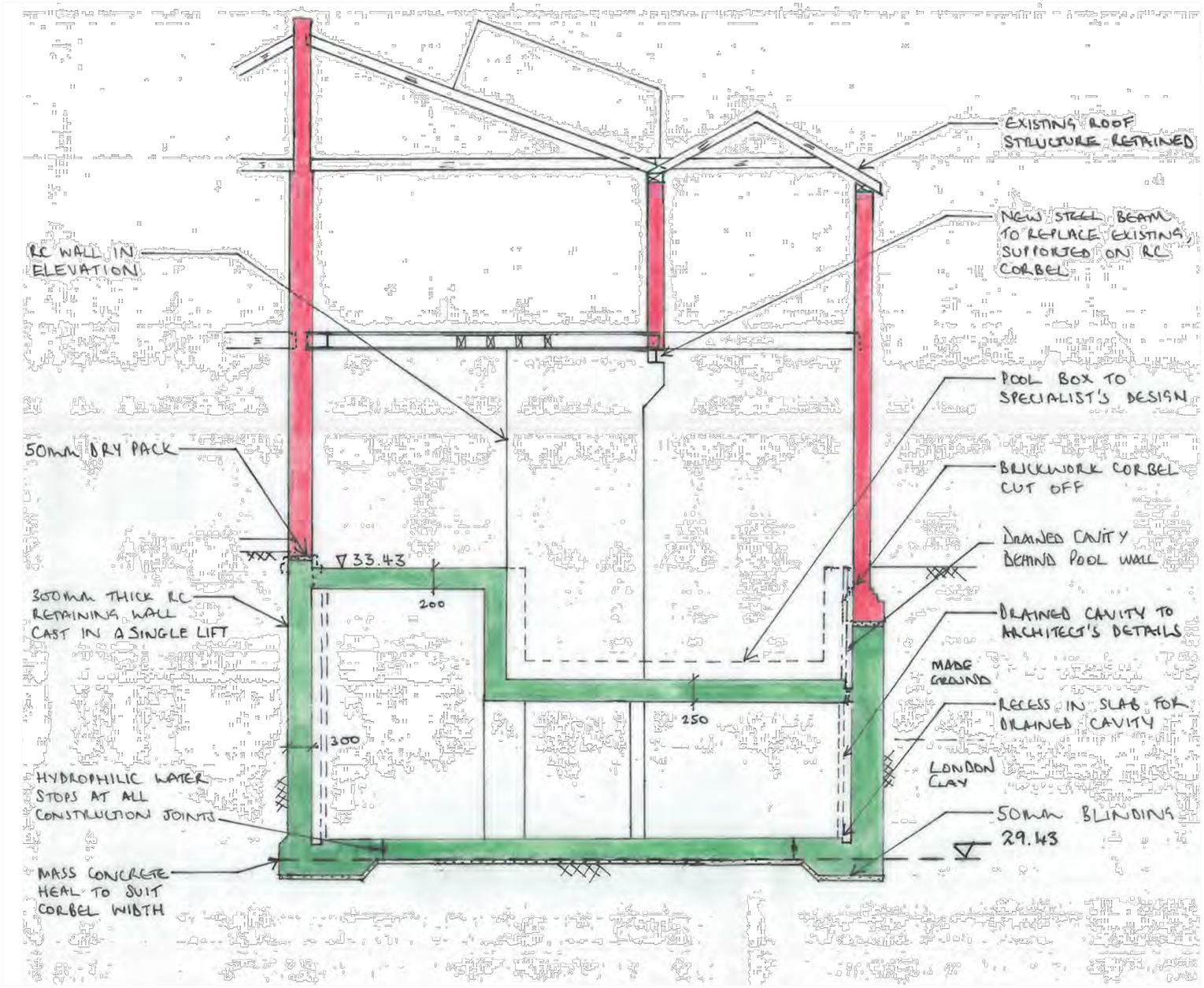
Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS,
PRIMROSE HILL, LONDON

Drawing Title
PROPOSED
GROUND FLOOR STRUCUTRE

Project No.	Drawing File
29841 - R01 (00)	29841 (R02-00) App A.6.dwg

Drawing No.	Rev.
APPENDIX A.6	P1



Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

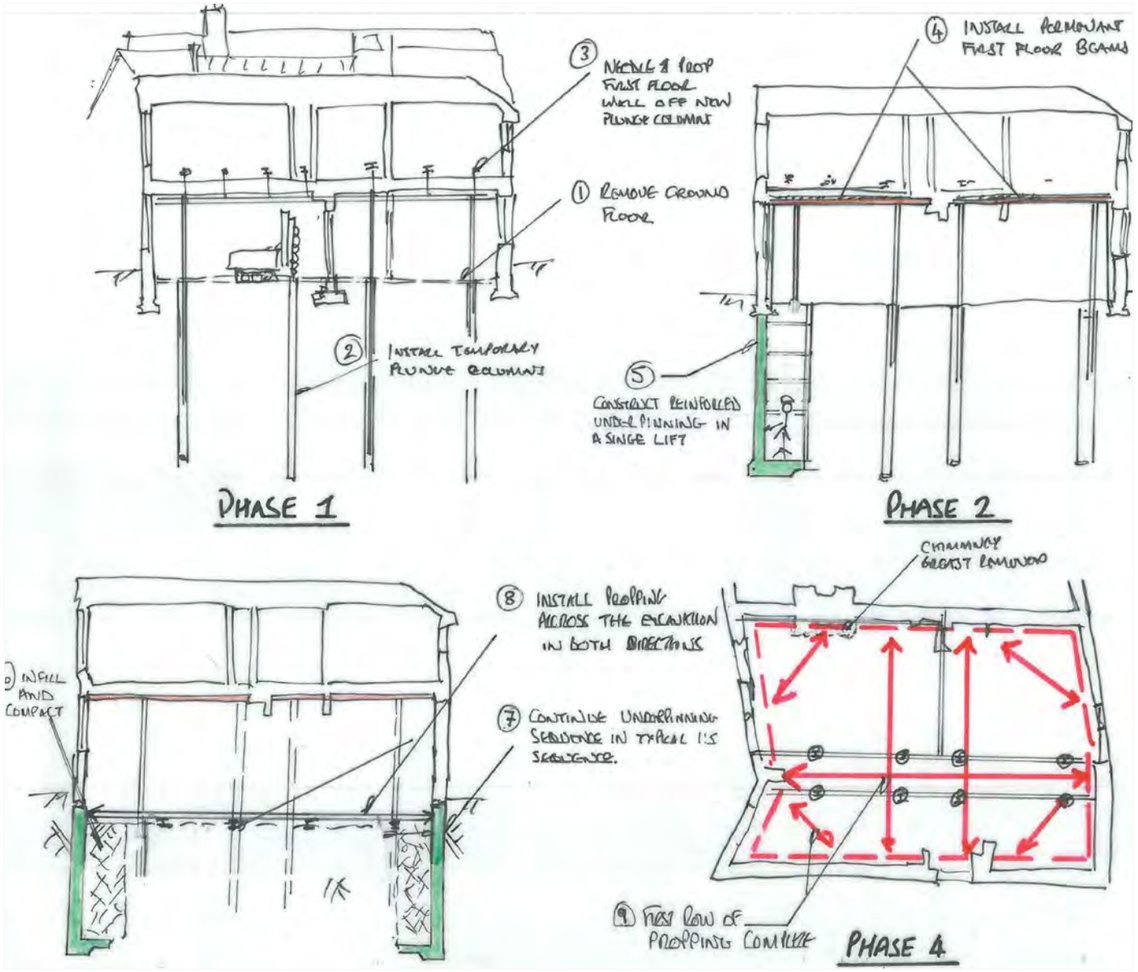
Client: MR. MARK GOLINSKY

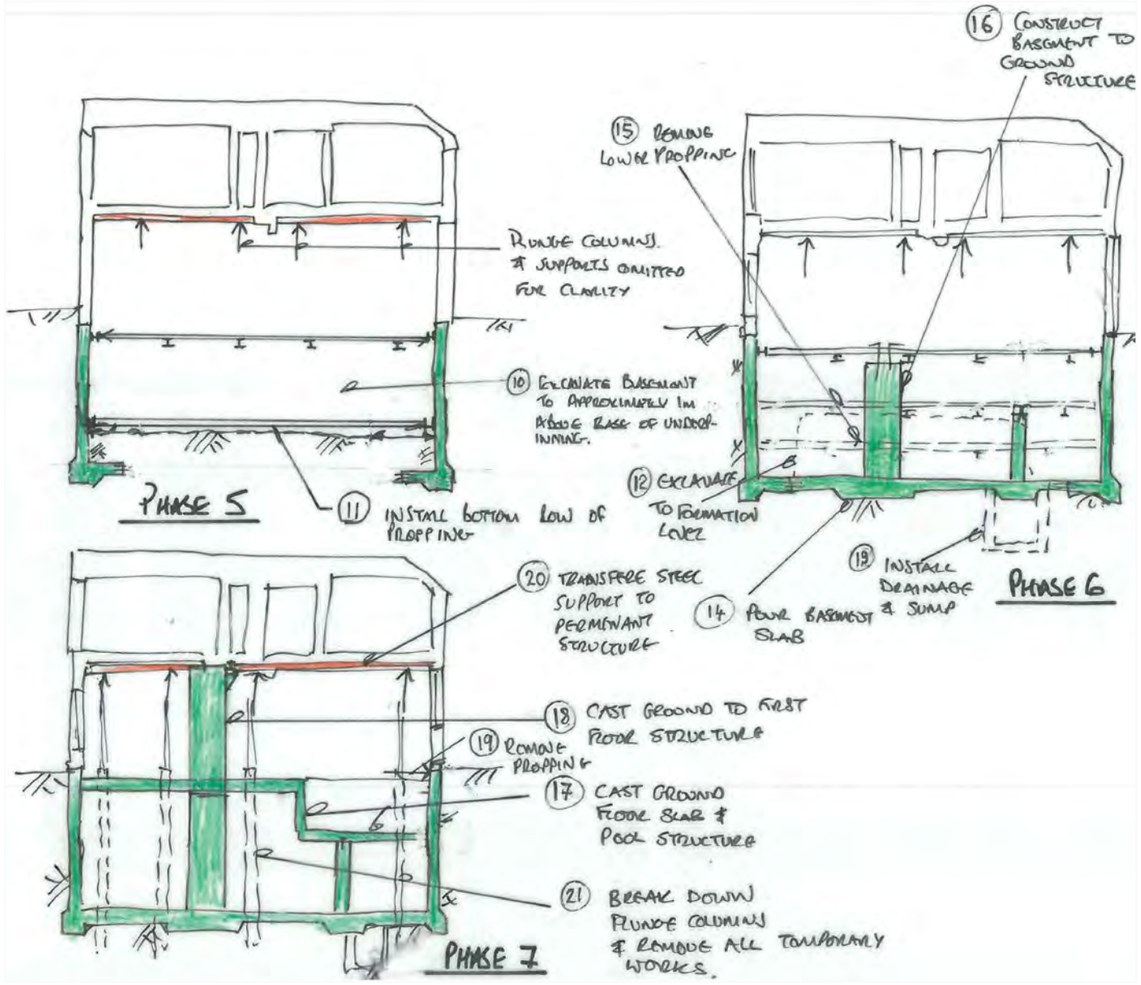
Project Title: 6 ALBERT TERRACE MEWS, PRIMROSE HILL, LONDON

Drawing Title: PROPOSED STRUCUTRE SECTION A-A'

Project No.	Drawing File
29841 - R01 (00)	29841 (R02-00) App A.7.dwg

Scale	Orig Size	Dimensions	Drawing No.	Rev.
NTS	A3	m	APPENDIX A.7	P1





Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

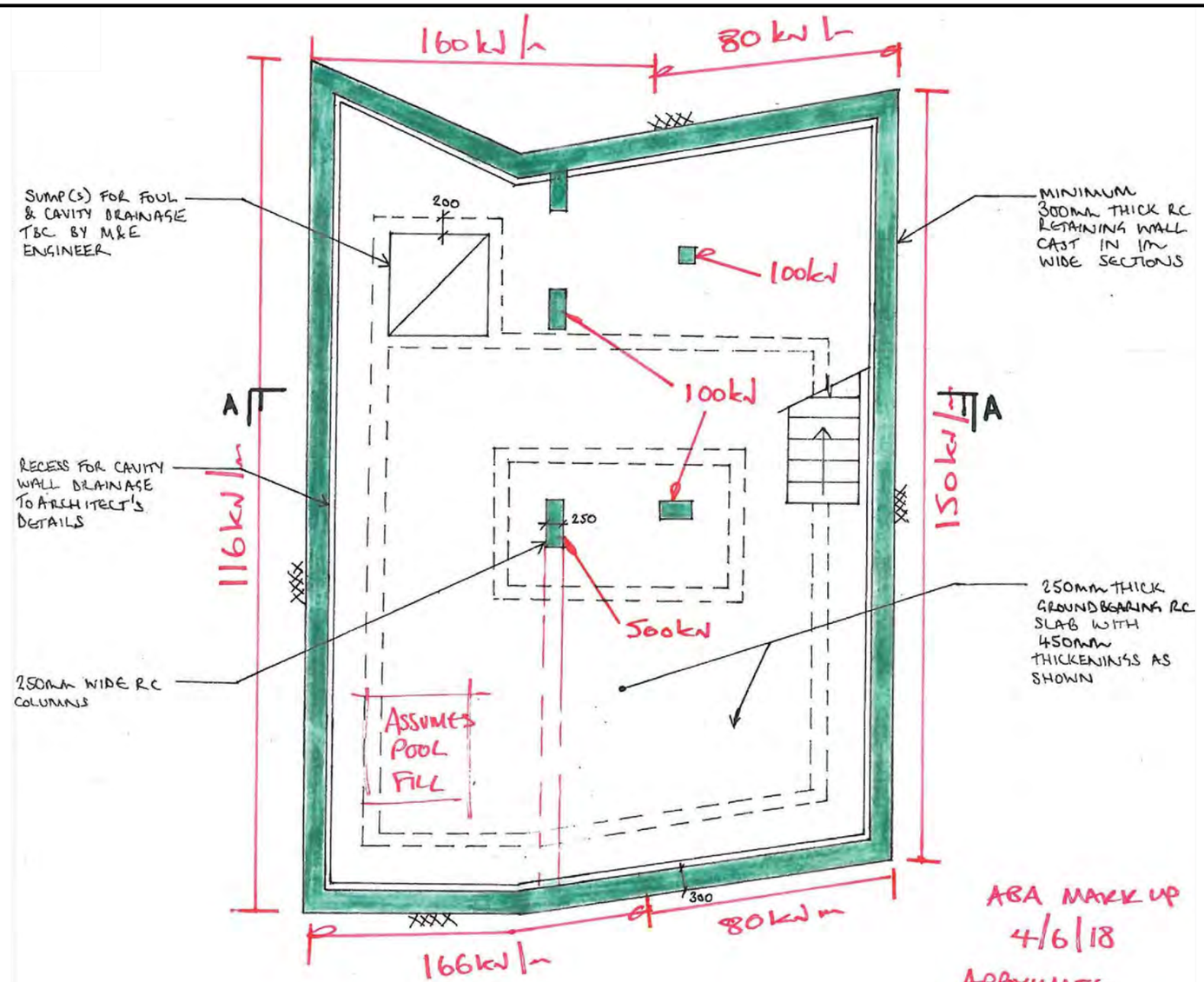
Client: MR. MARK GOLINSKY

Project Title: 6 ALBERT TERRACE MEWS, PRIMROSE HILL, LONDON

Drawing Title: PROPOSED CONSTRUCTION SEQUENCE

Project No.	Drawing File
29841 - R02 (00)	29841 (R02-00) App A.8.dwg

Scale	Orig Size	Dimensions	Drawing No.	Rev.
NTS	A3	m	APPENDIX A.8	P1



ABA MARK UP
4/6/18
APPROXIMATE
DL+LL @
FOUNDATION
LEVEL

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Rev.	Date	Amendment	Drawn	Chkd.	Appd.

Drawn	Date	Checked	Date	Approved	Date
ASC	19.06.18	ST	19.06.18	ST	19.06.18

Client: MR. MARK GOLINSKY

Project Title: 6 ALBERT TERRACE MEWS, PRIMROSE HILL, LONDON

Drawing Title: PROPOSED LOADING SCHEDULE

Project No.	Drawing File
29841 - R01 (00)	29841 (R02-00) App A.9.dwg

Scale	Orig Size	Dimensions	Drawing No.	Rev.
NTS	A3	m	APPENDIX A.9	P1

APPENDIX B
DETERMINATION OF HORIZONTAL TENSILE STRAINS AND DEFLECTION RATIOS USING CIRIA C760 APPROACH – RESULTS FROM XDISP ANALYSIS

Problem Type

Problem Type : Tunnelling and Embedded Wall Excavations

Displacement Data

Type	Name	Direction of extrusion	Point/Line/Line for extrusion						No. of intervals across extrusion/line	Extrusion depth	No. of intervals along extrusion	Calculate	Surface type for tunnels
			First point			Second point							
			X [m]	Y [m]	Z(level) [m]	X [m]	Y [m]	Z(level) [m]		[m]			
Line	No.5 Albert Terrace Mews	-	8.08000	6.15000	32.67000	18.08000	6.15000	32.67000	10	-	-	Yes	Surface
Grid	Proposed Basement	Global X	-20.00000	-20.00000	29.43000	-	30.00000	29.43000	25	50.00000	25	No	Surface
Line	No.4 Albert Terrace Mews	-	18.08000	6.15000	32.67000	28.08000	6.15000	32.67000	10	-	-	Yes	Surface

Vertical Ground Movement Curves (Excavations)

Curve Name: **Installation of planar diaphragm wall in stiff clay_amended**

Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.100][0.050,0.000,0.094][0.100,0.000,0.086][0.150,0.000,0.080]
[0.200,0.000,0.074][0.250,0.000,0.068][0.300,0.000,0.062][0.350,0.000,0.056]
[0.400,0.000,0.050][0.450,0.000,0.044][0.500,0.000,0.040][0.550,0.000,0.036]
[0.600,0.000,0.032][0.650,0.000,0.028][0.700,0.000,0.024][0.750,0.000,0.020]
[0.800,0.000,0.016][0.850,0.000,0.014][0.900,0.000,0.012][0.950,0.000,0.010]
[1.000,0.000,0.008][1.050,0.000,0.006][1.100,0.000,0.006][1.150,0.000,0.004]
[1.200,0.000,0.004][1.250,0.000,0.002][1.300,0.000,0.002][1.350,0.000,0.002]
[1.400,0.000,0.002][1.450,0.000,0.000][1.500,0.000,0.000]

Curve Fitting Method: Polynomial
x Order: 4
y Order: 0
Polynomial: z = $-2.2677E-2x^4 + 6.3043E-2x^3 + 6.8712E-4x^2 - 1.3292E-1x + 9.9991E-2$
Coeff. of Determination: 9.9969E-1

Curve Name: **Excavation in front of high stiffness wall in stiff clay_amended**

Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.078][0.100,0.000,0.098][0.200,0.000,0.112][0.300,0.000,0.124]
[0.400,0.000,0.134][0.500,0.000,0.140][0.600,0.000,0.144][0.700,0.000,0.146]
[0.800,0.000,0.146][0.900,0.000,0.144][1.000,0.000,0.140][1.100,0.000,0.136]
[1.200,0.000,0.130][1.300,0.000,0.122][1.400,0.000,0.116][1.500,0.000,0.108]
[1.600,0.000,0.100][1.700,0.000,0.092][1.800,0.000,0.084][1.900,0.000,0.076]
[2.000,0.000,0.068][2.100,0.000,0.060][2.200,0.000,0.054][2.300,0.000,0.046]
[2.400,0.000,0.040][2.500,0.000,0.034][2.600,0.000,0.028][2.700,0.000,0.024]
[2.800,0.000,0.020][2.900,0.000,0.016][3.000,0.000,0.014][3.100,0.000,0.010]
[3.200,0.000,0.008][3.300,0.000,0.008][3.400,0.000,0.006][3.500,0.000,0.004]
[3.600,0.000,0.004][3.700,0.000,0.004][3.800,0.000,0.002][3.900,0.000,0.002]
[4.000,0.000,0.000]

Curve Fitting Method: Polynomial
x Order: 4
y Order: 0
Polynomial: z = $-5.2909E-3x^4 + 5.6989E-2x^3 - 2.0101E-1x^2 + 2.1138E-1x + 7.7980E-2$
Coeff. of Determination: 9.9991E-1

Horizontal Ground Movement Curves (Excavations)

Curve Name: **Installation of planar diaphragm wall in stiff clay_amended**

Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.000][1.500,0.000,0.000]

Curve Fitting Method: Polynomial
x Order: 1
y Order: 0
Polynomial: z = 0.0x + 0.0
Coeff. of Determination: -2147483648.E+2147483647

Curve Name: **Excavation in front of high stiffness wall in stiff clay_amended**

Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.180][4.000,0.000,0.000]

Curve Fitting Method: Polynomial
x Order: 1
y Order: 0
Polynomial: z = -4.50E-2x + 1.80E-1
Coeff. of Determination: 1.00

Polygonal Excavations

Excavation Name: **Basement underpinning**
Surface level [m]: 33.430
Contribution: Positive
Enabled: Yes
Surface movement curves which are selected are applied between surface and [m]: 28.930

Corner	x [m]	y [m]	Base Level [m]	Stiffened	Previous Side d [m]	Previous Side p1 [%]	Previous Side p2* [%]	Next Side d [m]	Next Side p1 [%]	Next Side p2* [%]
1	0.0	0.0	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
2	4.7900	0.29000	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
3	8.0800	0.80000	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
4	8.0800	11.500	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
5	0.0	11.800	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000

Side	Corner 1 x [m]	Corner 1 y [m]	Corner 2 x [m]	Corner 2 y [m]	Ground Movement Curve: Vertical	Ground Movement Curve: Horizontal
1	0.0	0.0	4.7900	0.29000	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
2	4.7900	0.29000	8.0800	0.80000	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
3	8.0800	0.80000	8.0800	11.500	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
4	8.0800	11.500	0.0	11.800	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
5	0.0	11.800	0.0	0.0	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended

Side	Corner 1 x [m]	Corner 1 y [m]	Corner 2 x [m]	Corner 2 y [m]	Ground Movement Curve Vertical	Ground Movement Curve Horizontal
1	0.0	0.0	4.7900	0.29000	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
2	4.7900	0.29000	8.0800	0.80000	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
3	8.0800	0.80000	8.0800	11.500	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
4	8.0800	11.500	0.0	11.800	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
5	0.0	11.800	0.0	0.0	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended

Excavation Name: Basement Excavation
Surface level [m]: 33.430
Contribution: Positive
Enabled: Yes
Surface movement curves which are selected are applied between surface and [m]: 29.430

Corner	x [m]	y [m]	Base Level [m]	Stiffened	Previous Side d [m]	Previous Side p1 [%]	Previous Side p2* [%]	Next Side d [m]	Next Side p1 [%]	Next Side p2* [%]
1	0.0	0.0	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
2	4.7900	0.29000	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
3	8.0800	0.80000	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
4	8.0800	11.500	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
5	0.0	11.800	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000

Damage Category Strains

Name	0 (Negligible) to 1 (Very Slight)	1 (Very Slight) to 2 (Slight)	2 (Slight) to 3 (Moderate)	3 (Moderate) to 4 (Severe)
Burland Strain Limits	0.0	500.00E-6	750.00E-6	0.0015000

Specific Structures - Geometry

Structure Name	Sub-Structure Name	Displacement Line	Start Distance Along Line [m]	End Distance Along Line [m]	Vertical Offsets from Line for Vertical Movement Calculations [m]	Vertical Displacement Limit Sensitivity [mm]	Damage Category Strains	Poisson's Ratio	E/G
No.5 Albert Terrace Mews	No.5 Albert Terrace Mews	No.5 Albert Terrace Mews	0.00000	9.99900	0.0	0.10000	Burland Strain Limits	0.20000	2.6000
No.4 Albert Terrace Mews	No.4 Albert Terrace Mews	No.4 Albert Terrace Mews	0.00000	10.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000

Specific Structures - Bending Parameters

Structure Name	Sub-Structure Name	Height [m]	Default Properties	Hogging 2nd Moment of Area (per unit width) [m³]	Hogging Distance of Bending Strain from N.A. [m]	Hogging Distance of N.A. from Edge of Beam in Tension [m]	Sagging 2nd Moment of Area (per unit width) [m³]	Sagging Distance of Bending Strain from N.A. [m]	Sagging Distance of N.A. from Edge of Beam in Tension [m]
No.5 Albert Terrace Mews	No.5 Albert Terrace Mews	6.0000	Yes	72.000	6.0000	6.0000	18.000	3.0000	3.0000
No.4 Albert Terrace Mews	No.4 Albert Terrace Mews	6.0000	Yes	72.000	6.0000	6.0000	18.000	3.0000	3.0000

Building Segment Combinations

Structure Name	Sub-Structure Name	Vertical Offset from Line for Vertical Movement Calculations [m]	Segment	Start Length [m]	Curvature [m]	Combined Segment

No structures have segments combined.

Utility Strain Calculation Options

Neglect beneficial contribution of axial strains : No

Warnings

1 Multiple excavations have been specified. The displacements resulting from these excavations are calculated by summing the displacements resulting from each individual excavation. No account has been taken of the interactions between excavations (e.g. overlapping zones of influence or 'shielding' of one excavation by another).

Errors

None

Displacement and Strain Results

Type/No. Name	Dist. [m]	Coordinates x [m]	y [m]	z [m]	Displacements x [mm]	y [mm]	z [mm]	Horizontal displacement along Line [mm]	Horizontal displacement perpendicular to Line [mm]	Angle of Line to x Axis [°]
No.5 Albert Terrace Mews	Line 1	8.08000	6.15000	32.67000	-7.1640	0.0	7.5332	-7.1640	0.0	0.0
	1.0000	9.08000	6.15000	32.67000	-6.7140	0.0	7.8790	-6.7140	0.0	0.0
	2.0000	10.08000	6.15000	32.67000	-6.2640	0.0	7.5781	-6.2640	0.0	0.0
	3.0000	11.08000	6.15000	32.67000	-5.8140	0.0	6.9150	-5.8140	0.0	0.0
	4.0000	12.08000	6.15000	32.67000	-5.3640	0.0	6.0916	-5.3640	0.0	0.0
	5.0000	13.08000	6.15000	32.67000	-4.9140	0.0	5.2267	-4.9140	0.0	0.0
	6.0000	14.08000	6.15000	32.67000	-4.4640	0.0	4.3567	-4.4640	0.0	0.0
	7.0000	15.08000	6.15000	32.67000	-4.0140	0.0	3.4780	-4.0140	0.0	0.0
	8.0000	16.08000	6.15000	32.67000	-3.5640	0.0	2.6737	-3.5640	0.0	0.0
	9.0000	17.08000	6.15000	32.67000	-3.1140	0.0	1.9400	-3.1140	0.0	0.0
	10.000	18.08000	6.15000	32.67000	-2.6640	0.0	1.3215	-2.6640	0.0	0.0
No.4 Albert Terrace Mews	Line 2	18.08000	6.15000	32.67000	-2.6640	0.0	1.3215	-2.6640	0.0	0.0
	1.0000	19.08000	6.15000	32.67000	-2.2140	0.0	0.84274	-2.2140	0.0	0.0

Name	Type/No. Dist.	Coordinates x	y	z	Displacements x	y	z	Horizontal displacement	Horizontal displacement	Angle of Line to x Axis
	2.0000	20.08000	6.15000	32.67000	-1.7640	0.0	0.50816	-1.7640	0.0	0.0
	3.0000	21.08000	6.15000	32.67000	-1.3140	0.0	0.30196	-1.3140	0.0	0.0
	4.0000	22.08000	6.15000	32.67000	-0.86400	0.0	0.18824	-0.86400	0.0	0.0
	5.0000	23.08000	6.15000	32.67000	-0.41400	0.0	0.11093	-0.41400	0.0	0.0
	6.0000	24.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	0.0	0.0
	7.0000	25.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	0.0	0.0
	8.0000	26.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	0.0	0.0
	9.0000	27.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	0.0	0.0
	10.000	28.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	0.0	0.0

Specific Building Damage Results - Horizontal Displacements

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements x	y	Horizontal displacement along the Line	Horizontal displacement perpendicular to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	8.08000	6.15000	32.67000	-7.1640	0.0	-7.1640	0.0
1.0000	9.08000	6.15000	32.67000	-6.7140	0.0	-6.7140	0.0
2.0000	10.08000	6.15000	32.67000	-6.2640	0.0	-6.2640	0.0
3.0000	11.08000	6.15000	32.67000	-5.8140	0.0	-5.8140	0.0
4.0000	12.08000	6.15000	32.67000	-5.3640	0.0	-5.3640	0.0
5.0000	13.08000	6.15000	32.67000	-4.9140	0.0	-4.9140	0.0
6.0000	14.08000	6.15000	32.67000	-4.4640	0.0	-4.4640	0.0
7.0000	15.08000	6.15000	32.67000	-4.0140	0.0	-4.0140	0.0
8.0000	16.08000	6.15000	32.67000	-3.5640	0.0	-3.5640	0.0
9.0000	17.08000	6.15000	32.67000	-3.1140	0.0	-3.1140	0.0
10.000	18.08000	6.15000	32.67000	-2.6640	0.0	-2.6640	0.0

Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements x	y	Horizontal displacement along the Line	Horizontal displacement perpendicular to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	18.08000	6.15000	32.67000	-2.6640	0.0	-2.6640	0.0
1.0000	19.08000	6.15000	32.67000	-2.2140	0.0	-2.2140	0.0
2.0000	20.08000	6.15000	32.67000	-1.7640	0.0	-1.7640	0.0
3.0000	21.08000	6.15000	32.67000	-1.3140	0.0	-1.3140	0.0
4.0000	22.08000	6.15000	32.67000	-0.86400	0.0	-0.86400	0.0
5.0000	23.08000	6.15000	32.67000	-0.41400	0.0	-0.41400	0.0
6.0000	24.08000	6.15000	32.67000	0.0	0.0	0.0	0.0
7.0000	25.08000	6.15000	32.67000	0.0	0.0	0.0	0.0
8.0000	26.08000	6.15000	32.67000	0.0	0.0	0.0	0.0
9.0000	27.08000	6.15000	32.67000	0.0	0.0	0.0	0.0
10.000	28.08000	6.15000	32.67000	0.0	0.0	0.0	0.0

Specific Building Damage Results - Vertical Displacements

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements z
[m]	[m]	[m]	[m]	[mm]
Vertical Offset 1				
0.0	8.08000	6.15000	32.67000	7.5332
1.0000	9.08000	6.15000	32.67000	7.8790
2.0000	10.08000	6.15000	32.67000	7.5781
3.0000	11.08000	6.15000	32.67000	6.9150
4.0000	12.08000	6.15000	32.67000	6.0916
5.0000	13.08000	6.15000	32.67000	5.2267
6.0000	14.08000	6.15000	32.67000	4.3567
7.0000	15.08000	6.15000	32.67000	3.4780
8.0000	16.08000	6.15000	32.67000	2.6737
9.0000	17.08000	6.15000	32.67000	1.9400
10.000	18.08000	6.15000	32.67000	1.3215

Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements z
[m]	[m]	[m]	[m]	[mm]
Vertical Offset 1				
0.0	18.08000	6.15000	32.67000	1.3215
1.0000	19.08000	6.15000	32.67000	0.84274
2.0000	20.08000	6.15000	32.67000	0.50816
3.0000	21.08000	6.15000	32.67000	0.30196
4.0000	22.08000	6.15000	32.67000	0.18824
5.0000	23.08000	6.15000	32.67000	0.11093
6.0000	24.08000	6.15000	32.67000	0.0
7.0000	25.08000	6.15000	32.67000	0.0
8.0000	26.08000	6.15000	32.67000	0.0
9.0000	27.08000	6.15000	32.67000	0.0
10.000	28.08000	6.15000	32.67000	0.0

Specific Building Damage Results - All Segments

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
[m]		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	5.5373	Sagging	0.018857	0.045000	0.066974	-449.80E-6	869.64E-6	1394.4	1 (Very Slight)
	2	5.5373	4.4617	Hogging	0.0042065	0.045000	0.047324	-449.80E-6	878.25E-6	7913.5	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
[m]		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	5.0000	Hogging	0.0065643	0.045000	0.049029	-449.80E-6	478.51E-6	6759.0	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Specific Building Damage Results - Critical Values for All Segments within Each Sub-Structure

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Vertical	Deflection	Average	Max Slope	Max	Max	Max Gradient	Max Gradient	Min	Min	Damage Category

Offset from Line for Vertical Movement Calculations	Ratio	Horizontal Strain		Settlement	Tensile Strain	of Horizontal Displacement Curve	of Vertical Displacement Curve	Radius of Curvature (Hogging)	Radius of Curvature (Sagging)	
[m]	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.018857	0.045000	878.25E-6	7.8769	0.066974	-449.80E-6	878.25E-6	7913.5	1394.4	1 (Very Slight)

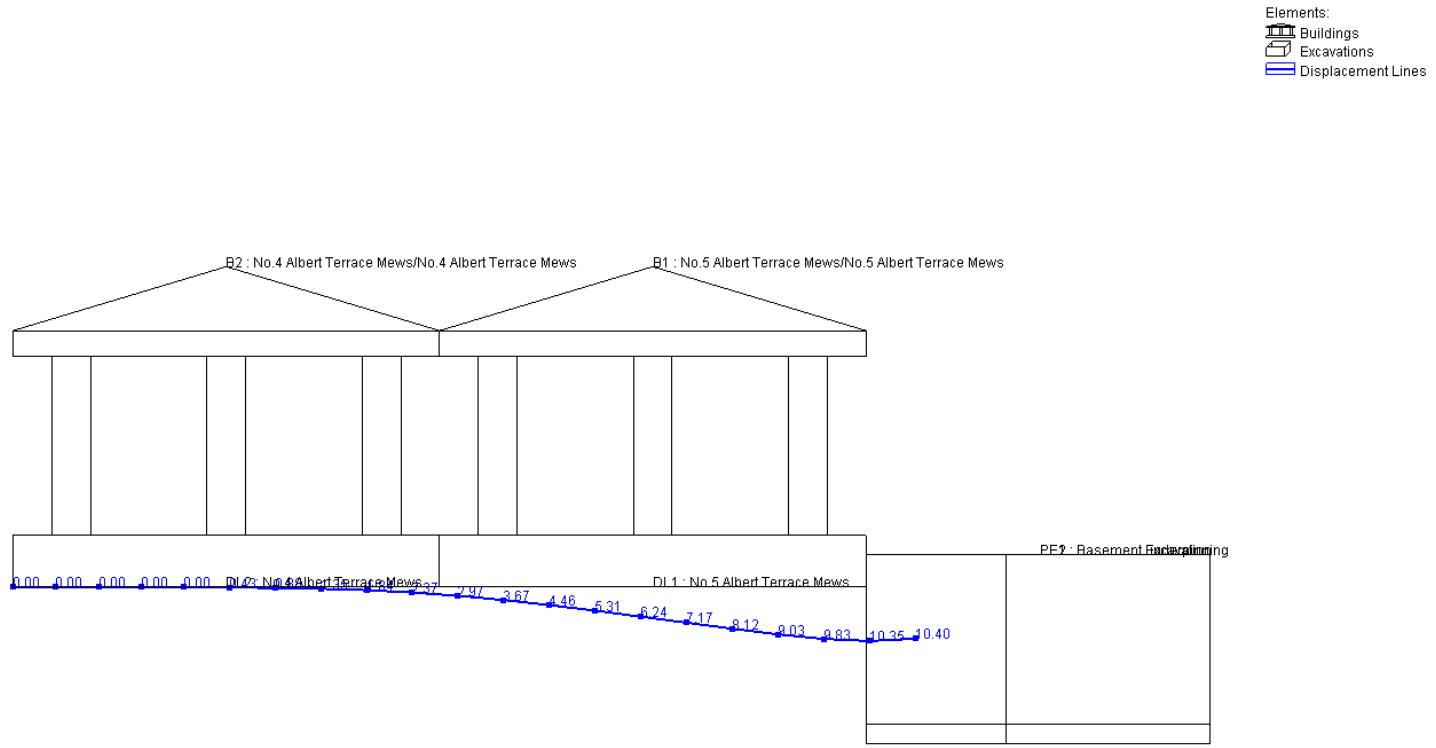
Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.0065643	0.045000	478.51E-6	1.3215	0.049029	-449.80E-6	478.51E-6	6759.0	-	0 (Negligible)

Specific Building Damage Results - Critical Segments within Each Structure

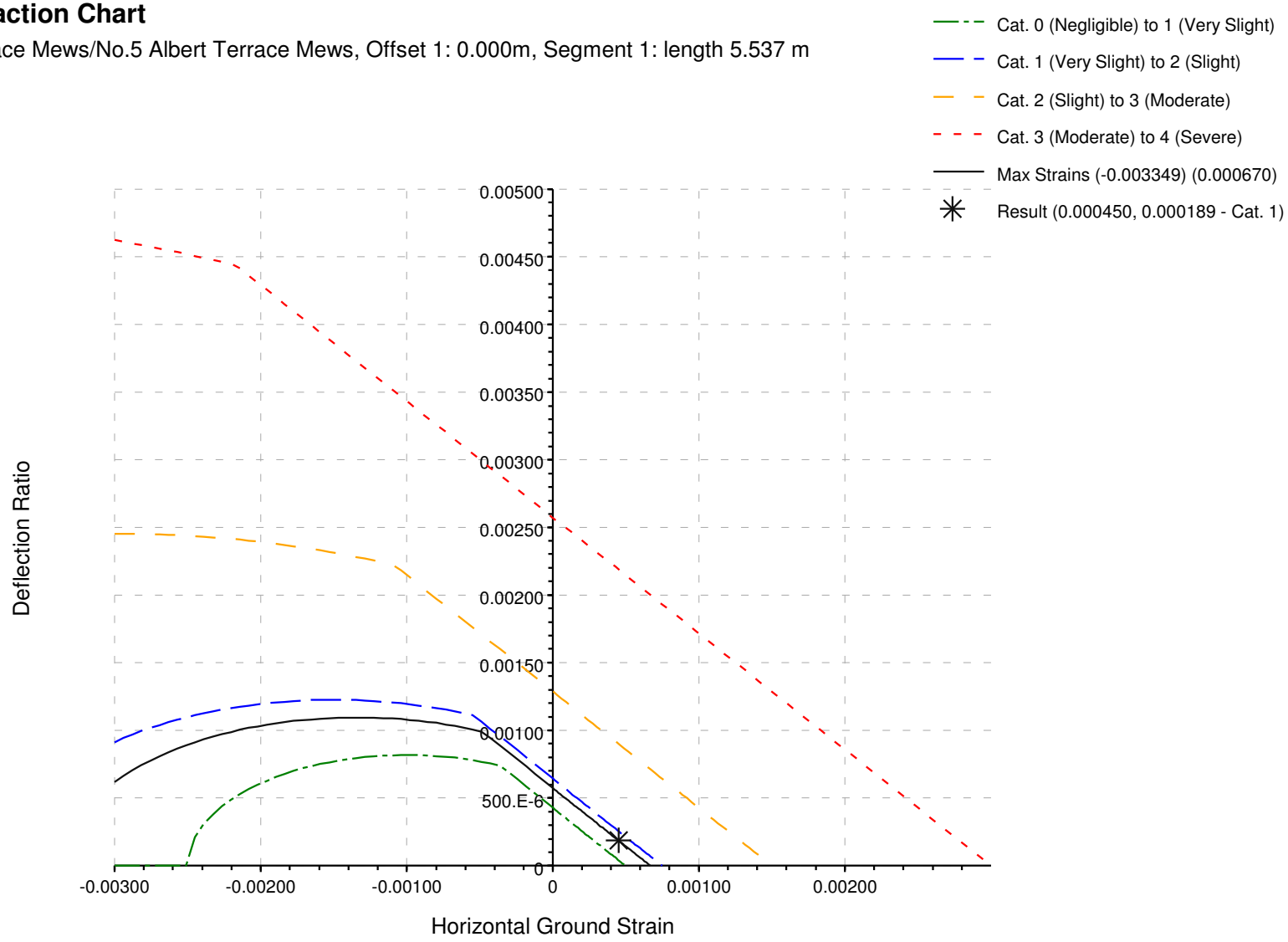
Structure Name	Parameter	Critical Sub-Structure	Critical Segment	Start	End	Curvature	Max Slope	Max Settlement	Max Tensile Strain	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
				[m]	[m]			[mm]	[%]	[m]	[m]	
No.5 Albert Terrace Mews	Max Slope	No.5 Albert Terrace Mews	2	5.5373	9.9990	Hogging	**878.25E-6**	4.7592	0.047324	7913.5	-	0 (Negligible)
	Max Settlement	No.5 Albert Terrace Mews	1	0.0	5.5373	Sagging	869.64E-6	**7.8769**	0.066974	-	1394.4	1 (Very Slight)
	Max Tensile Strain	No.5 Albert Terrace Mews	1	0.0	5.5373	Sagging	869.64E-6	7.8769	**0.066974**	-	1394.4	1 (Very Slight)
	Min Radius of Curvature (Hogging)	No.5 Albert Terrace Mews	2	5.5373	9.9990	Hogging	878.25E-6	4.7592	0.047324	**7913.5**	-	0 (Negligible)
	Min Radius of Curvature (Sagging)	No.5 Albert Terrace Mews	1	0.0	5.5373	Sagging	869.64E-6	7.8769	0.066974	-	**1394.4**	1 (Very Slight)
No.4 Albert Terrace Mews	Max Slope	No.4 Albert Terrace Mews	1	0.0	5.0000	Hogging	**478.51E-6**	1.3215	0.049029	6759.0	-	0 (Negligible)
	Max Settlement	No.4 Albert Terrace Mews	1	0.0	5.0000	Hogging	478.51E-6	**1.3215**	0.049029	6759.0	-	0 (Negligible)
	Max Tensile Strain	No.4 Albert Terrace Mews	1	0.0	5.0000	Hogging	478.51E-6	1.3215	**0.049029**	6759.0	-	0 (Negligible)
	Min Radius of Curvature (Hogging)	No.4 Albert Terrace Mews	1	0.0	5.0000	Hogging	478.51E-6	1.3215	0.049029	**6759.0**	-	0 (Negligible)
	Min Radius of Curvature (Sagging)		-	-	-	-	-	-	-	-	-	-

Graphics Display



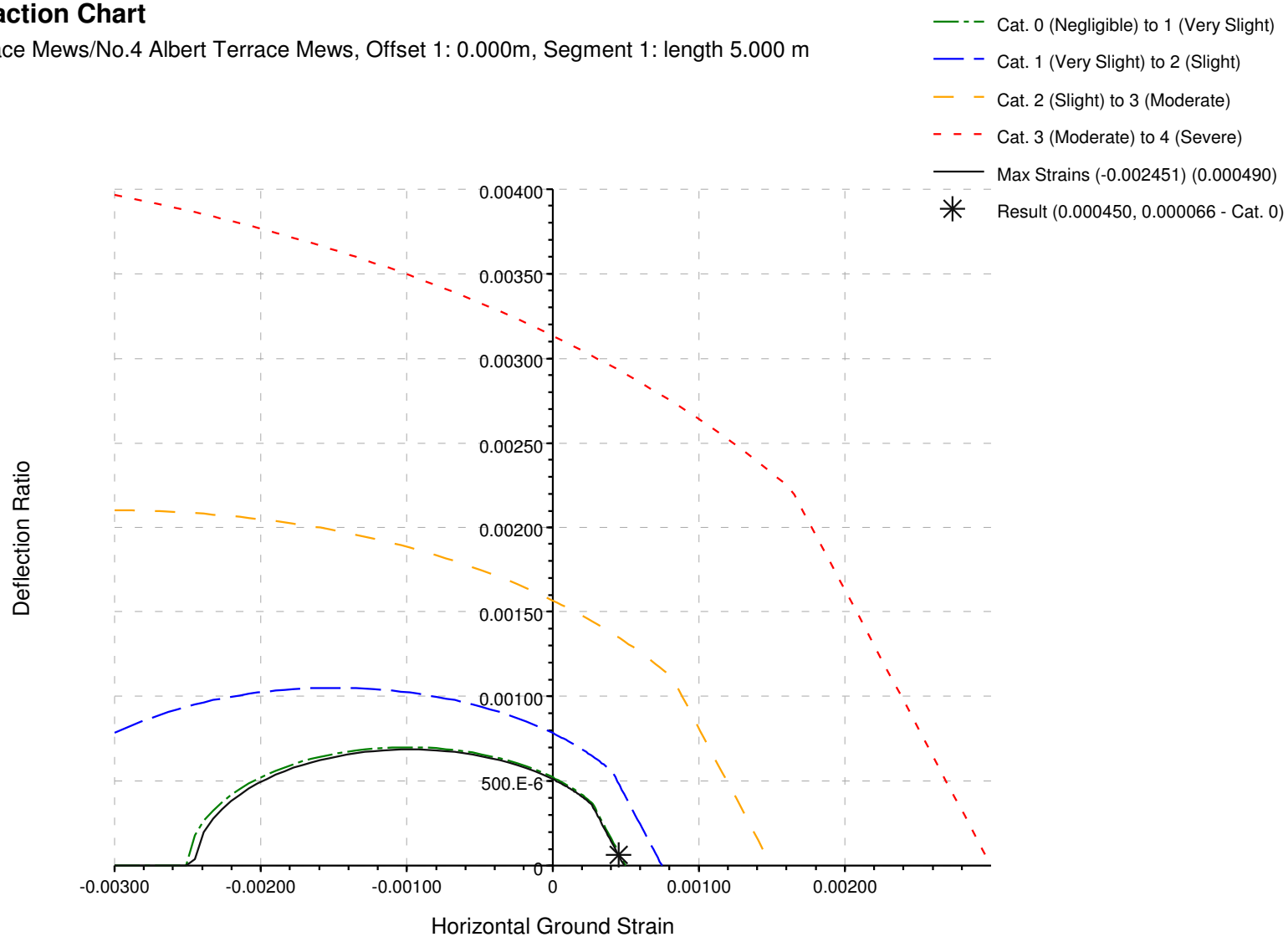
Building Damage Interaction Chart

Structure 1: No.5 Albert Terrace Mews/No.5 Albert Terrace Mews, Offset 1: 0.000m, Segment 1: length 5.537 m



Building Damage Interaction Chart

Structure 2: No.4 Albert Terrace Mews/No.4 Albert Terrace Mews, Offset 1: 0.000m, Segment 1: length 5.000 m



Problem Type

Problem Type : Tunnelling and Embedded Wall Excavations

Displacement Data

Type	Name	Direction of extrusion	Point/Line/Line for extrusion						No. of intervals across extrusion/line	Extrusion depth	No. of intervals along extrusion	Calculate	Surface type for tunnels
			First point			Second point							
			X [m]	Y [m]	Z(level) [m]	X [m]	Y [m]	Z(level) [m]		[m]			
Line	No.5 Albert Terrace Mews	-	8.08000	6.15000	32.67000	18.08000	6.15000	32.67000	10	-	-	Yes	Surface
Grid	Proposed Basement	Global X	-20.00000	-20.00000	29.43000	-	30.00000	29.43000	25	50.00000	25	No	Surface
Line	No.4 Albert Terrace Mews	-	18.08000	6.15000	32.67000	28.08000	6.15000	32.67000	10	-	-	Yes	Surface

Imported Displacements

The following data points and displacements were found in the import file Long Term.csv.

Ref.	Coordinates			Displacements			
	x [m]	y [m]	z [m]	x [mm]	y [mm]	z [mm]	
1	8.08000	6.15000	32.67000	0.00000	0.00000	-2.18761	1,2,6
2	9.08000	6.15000	32.67000	0.00000	0.00000	-1.74049	1,2,6
3	10.08000	6.15000	32.67000	0.00000	0.00000	-1.36657	1,2,6
4	11.08000	6.15000	32.67000	0.00000	0.00000	-1.09848	1,2,6
5	12.08000	6.15000	32.67000	0.00000	0.00000	-0.90247	1,2,6
6	13.08000	6.15000	32.67000	0.00000	0.00000	-0.75450	1,2,6
7	14.08000	6.15000	32.67000	0.00000	0.00000	-0.63962	1,2,6
8	15.08000	6.15000	32.67000	0.00000	0.00000	-0.54833	1,2,6
9	16.08000	6.15000	32.67000	0.00000	0.00000	-0.47440	1,2,6
10	17.08000	6.15000	32.67000	0.00000	0.00000	-0.41359	1,2,6
11	18.08000	6.15000	32.67000	0.00000	0.00000	-0.36293	1,2,6
12	19.08000	6.15000	32.67000	0.00000	0.00000	-0.32029	1,2,6
13	20.08000	6.15000	32.67000	0.00000	0.00000	-0.28408	1,2,6
14	21.08000	6.15000	32.67000	0.00000	0.00000	-0.25309	1,2,6
15	22.08000	6.15000	32.67000	0.00000	0.00000	-0.22641	1,2,6
16	23.08000	6.15000	32.67000	0.00000	0.00000	-0.20330	1,2,6
17	24.08000	6.15000	32.67000	0.00000	0.00000	-0.18318	1,2,6
18	25.08000	6.15000	32.67000	0.00000	0.00000	-0.16559	1,2,6
19	26.08000	6.15000	32.67000	0.00000	0.00000	-0.15014	1,2,6
20	27.08000	6.15000	32.67000	0.00000	0.00000	-0.13652	1,2,6
21	28.08000	6.15000	32.67000	0.00000	0.00000	-0.12447	1,2,6

1 - Data point coincident with displacement data. Its displacement has been added to those calculated by Xdisp.
2 - Data point coincident with horizontal movement calculation point for a specific building. Its displacement has been added before performing building damage calculations.
6 - Data point coincident with vertical movement calculation point for a specific building. Its displacement has been added before performing building damage calculations.

Vertical Ground Movement Curves (Excavations)

Curve Name: **Installation of planar diaphragm wall in stiff clay_amended**
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.100][0.050,0.000,0.094][0.100,0.000,0.086][0.150,0.000,0.080]
[0.200,0.000,0.074][0.250,0.000,0.068][0.300,0.000,0.062][0.350,0.000,0.056]
[0.400,0.000,0.050][0.450,0.000,0.044][0.500,0.000,0.040][0.550,0.000,0.036]
[0.600,0.000,0.032][0.650,0.000,0.028][0.700,0.000,0.024][0.750,0.000,0.020]
[0.800,0.000,0.016][0.850,0.000,0.014][0.900,0.000,0.012][0.950,0.000,0.010]
[1.000,0.000,0.008][1.050,0.000,0.006][1.100,0.000,0.006][1.150,0.000,0.004]
[1.200,0.000,0.004][1.250,0.000,0.002][1.300,0.000,0.002][1.350,0.000,0.002]
[1.400,0.000,0.002][1.450,0.000,0.000][1.500,0.000,0.000]
Curve Fitting Method: Polynomial
x Order: 4
y Order: 0
Polynomial: z = $-2.2677E-2x^4 + 6.3043E-2x^3 + 6.8712E-4x^2 - 1.3292E-1x + 9.9991E-2$
Coeff. of Determination: 9.9969E-1

Curve Name: **Excavation in front of high stiffness wall in stiff clay_amended**
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.078][0.100,0.000,0.098][0.200,0.000,0.112][0.300,0.000,0.124]
[0.400,0.000,0.134][0.500,0.000,0.140][0.600,0.000,0.144][0.700,0.000,0.146]
[0.800,0.000,0.146][0.900,0.000,0.144][1.000,0.000,0.140][1.100,0.000,0.136]
[1.200,0.000,0.130][1.300,0.000,0.122][1.400,0.000,0.116][1.500,0.000,0.108]
[1.600,0.000,0.100][1.700,0.000,0.092][1.800,0.000,0.084][1.900,0.000,0.076]
[2.000,0.000,0.068][2.100,0.000,0.060][2.200,0.000,0.054][2.300,0.000,0.046]
[2.400,0.000,0.040][2.500,0.000,0.034][2.600,0.000,0.028][2.700,0.000,0.024]
[2.800,0.000,0.020][2.900,0.000,0.016][3.000,0.000,0.014][3.100,0.000,0.010]
[3.200,0.000,0.008][3.300,0.000,0.008][3.400,0.000,0.006][3.500,0.000,0.004]
[3.600,0.000,0.004][3.700,0.000,0.004][3.800,0.000,0.002][3.900,0.000,0.002]
[4.000,0.000,0.000]
Curve Fitting Method: Polynomial
x Order: 4
y Order: 0
Polynomial: z = $-5.2909E-3x^4 + 5.6989E-2x^3 - 2.0101E-1x^2 + 2.1138E-1x + 7.7980E-2$
Coeff. of Determination: 9.9991E-1

Horizontal Ground Movement Curves (Excavations)

Curve Name: **Installation of planar diaphragm wall in stiff clay_amended**
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.000][1.500,0.000,0.000]
Curve Fitting Method: Polynomial
x Order: 1
y Order: 0
Polynomial: z = 0.0x + 0.0
Coeff. of Determination: -2147483648.E+2147483647

Curve Name: **Excavation in front of high stiffness wall in stiff clay_amended**
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z)(%)]
[0.000,0.000,0.180][4.000,0.000,0.000]
Curve Fitting Method: Polynomial
x Order: 1
y Order: 0
Polynomial: z = -4.50E-2x + 1.80E-1
Coeff. of Determination: 1.00

Polygonal Excavations

Excavation Name: **Basement underpinning**
Surface level [m]: 33.430
Contribution: Positive

Ref.	Coordinates x [m]	y [m]	z [m]	Displacements x [mm]	y [mm]	z [mm]

Enabled: Yes
Surface movement curves which are selected are applied between surface and [m]: 28.930

Corner	x	y	Base Level	Stiffened	Previous Side d [m]	p1 [%]	p2* [%]	Next Side d [m]	p1 [%]	p2* [%]
1	0.0	0.0	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
2	4.7900	0.29000	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
3	8.0800	0.80000	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
4	8.0800	11.500	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
5	0.0	11.800	29.000	Yes	0.0	67.000	25.000	0.0	67.000	25.000

Side	Corner 1 x [m]	y [m]	Corner 2 x [m]	y [m]	Ground Movement Curve Vertical	Horizontal
1	0.0	0.0	4.7900	0.29000	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
2	4.7900	0.29000	8.0800	0.80000	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
3	8.0800	0.80000	8.0800	11.500	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
4	8.0800	11.500	0.0	11.800	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended
5	0.0	11.800	0.0	0.0	Installation of planar diaphragm wall in stiff clay_amended	Installation of planar diaphragm wall in stiff clay_amended

Excavation Name: Basement Excavation
Surface level [m]: 33.430
Contribution: Positive
Enabled: Yes
Surface movement curves which are selected are applied between surface and [m]: 29.430

Corner	x	y	Base Level	Stiffened	Previous Side d [m]	p1 [%]	p2* [%]	Next Side d [m]	p1 [%]	p2* [%]
1	0.0	0.0	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
2	4.7900	0.29000	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
3	8.0800	0.80000	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
4	8.0800	11.500	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000
5	0.0	11.800	29.450	Yes	0.0	67.000	25.000	0.0	67.000	25.000

Side	Corner 1 x [m]	y [m]	Corner 2 x [m]	y [m]	Ground Movement Curve Vertical	Horizontal
1	0.0	0.0	4.7900	0.29000	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
2	4.7900	0.29000	8.0800	0.80000	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
3	8.0800	0.80000	8.0800	11.500	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
4	8.0800	11.500	0.0	11.800	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended
5	0.0	11.800	0.0	0.0	Excavation in front of high stiffness wall in stiff clay_amended	Excavation in front of high stiffness wall in stiff clay_amended

Damage Category Strains

Name	0 (Negligible) to 1 (Very Slight)	1 (Very Slight) to 2 (Slight)	2 (Slight) to 3 (Moderate)	3 (Moderate) to 4 (Severe)
Burland Strain Limits	0.0	500.00E-6	750.00E-6	0.0015000

Specific Structures - Geometry

Structure Name	Sub-Structure Name	Displacement Line	Start Distance Along Line [m]	End Distance Along Line [m]	Vertical Offsets from Line for Vertical Movement Calculations [m]	Vertical Displacement Limit Sensitivity [mm]	Damage Category Strains	Poisson's Ratio	E/G
No.5 Albert Terrace Mews	No.5 Albert Terrace Mews	No.5 Albert Terrace Mews	0.00000	9.99900	0.0	0.10000	Burland Strain Limits	0.20000	2.6000
No.4 Albert Terrace Mews	No.4 Albert Terrace Mews	No.4 Albert Terrace Mews	0.00000	10.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000

Specific Structures - Bending Parameters

Structure Name	Sub-Structure Name	Height [m]	Default Properties	Hogging 2nd Moment of Area (per unit width) [m³]	Hogging Distance of Bending Strain from N.A. [m]	Hogging Distance of N.A. from Edge of Beam in Tension [m]	Sagging 2nd Moment of Area (per unit width) [m³]	Sagging Distance of Bending Strain from N.A. [m]	Sagging Distance of N.A. from Edge of Beam in Tension [m]
No.5 Albert Terrace Mews	No.5 Albert Terrace Mews	6.0000	Yes	72.000	6.0000	6.0000	18.000	3.0000	3.0000
No.4 Albert Terrace Mews	No.4 Albert Terrace Mews	6.0000	Yes	72.000	6.0000	6.0000	18.000	3.0000	3.0000

Building Segment Combinations

Structure Name	Sub-Structure Name	Vertical Offset from Line for Vertical Movement Calculations [m]	Segment Start [m]	Length [m]	Curvature	Combined Segment

No structures have segments combined.

Utility Strain Calculation Options

Neglect beneficial contribution of axial strains : No

Warnings

1 Multiple excavations have been specified. The displacements resulting from these excavations are calculated by summing the displacements resulting from each individual excavation. No account has been taken of the interactions between excavations (e.g. overlapping zones of influence or 'shielding' of one excavation by another).

Structure Name	Sub-Structure Name	Vertical Offset from Line for Vertical	Segment Start	Length	Curvature	Combined Segment

Errors

None

Displacement and Strain Results

Type/No. Name	Dist.	Coordinates x	y	z	Displacements x	y	z	Horizontal displacement along Line	Horizontal displacement perpendicular to Line	Angle of Line to x Axis
	[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]	[mm]	[°]
No.5 Albert Terrace Mews	Line 1	8.08000	6.15000	32.67000	-7.1640	0.0	5.3456	-7.1640	0.0	0.0 *
	1.0000	9.08000	6.15000	32.67000	-6.7140	0.0	6.1385	-6.7140	0.0	0.0 *
	2.0000	10.08000	6.15000	32.67000	-6.2640	0.0	6.2115	-6.2640	0.0	0.0 *
	3.0000	11.08000	6.15000	32.67000	-5.8140	0.0	5.8166	-5.8140	0.0	0.0 *
	4.0000	12.08000	6.15000	32.67000	-5.3640	0.0	5.1891	-5.3640	0.0	0.0 *
	5.0000	13.08000	6.15000	32.67000	-4.9140	0.0	4.4722	-4.9140	0.0	0.0 *
	6.0000	14.08000	6.15000	32.67000	-4.4640	0.0	3.7170	-4.4640	0.0	0.0 *
	7.0000	15.08000	6.15000	32.67000	-4.0140	0.0	2.9297	-4.0140	0.0	0.0 *
	8.0000	16.08000	6.15000	32.67000	-3.5640	0.0	2.1993	-3.5640	0.0	0.0 *
	9.0000	17.08000	6.15000	32.67000	-3.1140	0.0	1.5264	-3.1140	0.0	0.0 *
	10.000	18.08000	6.15000	32.67000	-2.6640	0.0	0.95853	-2.6640	0.0	0.0 *
No.4 Albert Terrace Mews	Line 2	18.08000	6.15000	32.67000	-2.6640	0.0	0.95853	-2.6640	0.0	0.0 *
	1.0000	19.08000	6.15000	32.67000	-2.2140	0.0	0.52245	-2.2140	0.0	0.0 *
	2.0000	20.08000	6.15000	32.67000	-1.7640	0.0	0.22409	-1.7640	0.0	0.0 *
	3.0000	21.08000	6.15000	32.67000	-1.3140	0.0	0.048872	-1.3140	0.0	0.0 *
	4.0000	22.08000	6.15000	32.67000	-0.86400	0.0	-0.038171	-0.86400	0.0	0.0 *
	5.0000	23.08000	6.15000	32.67000	-0.41400	0.0	-0.092363	-0.41400	0.0	0.0 *
	6.0000	24.08000	6.15000	32.67000	0.0	0.0	-0.18318	0.0	0.0	0.0 *
	7.0000	25.08000	6.15000	32.67000	0.0	0.0	-0.16559	0.0	0.0	0.0 *
	8.0000	26.08000	6.15000	32.67000	0.0	0.0	-0.15014	0.0	0.0	0.0 *
	9.0000	27.08000	6.15000	32.67000	0.0	0.0	-0.13652	0.0	0.0	0.0 *
	10.000	28.08000	6.15000	32.67000	0.0	0.0	-0.12447	0.0	0.0	0.0 *

* Result includes imported displacement(s).

Specific Building Damage Results - Horizontal Displacements

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements x	y	Horizontal displacement along the Line	Horizontal displacement perpendicular to Line	
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]	
0.0	8.08000	6.15000	32.67000	-7.1640	0.0	-7.1640	0.0	d
1.0000	9.08000	6.15000	32.67000	-6.7140	0.0	-6.7140	0.0	d
2.0000	10.08000	6.15000	32.67000	-6.2640	0.0	-6.2640	0.0	d
3.0000	11.08000	6.15000	32.67000	-5.8140	0.0	-5.8140	0.0	d
4.0000	12.08000	6.15000	32.67000	-5.3640	0.0	-5.3640	0.0	d
5.0000	13.08000	6.15000	32.67000	-4.9140	0.0	-4.9140	0.0	d
6.0000	14.08000	6.15000	32.67000	-4.4640	0.0	-4.4640	0.0	d
7.0000	15.08000	6.15000	32.67000	-4.0140	0.0	-4.0140	0.0	d
8.0000	16.08000	6.15000	32.67000	-3.5640	0.0	-3.5640	0.0	d
9.0000	17.08000	6.15000	32.67000	-3.1140	0.0	-3.1140	0.0	d
10.000	18.08000	6.15000	32.67000	-2.6640	0.0	-2.6640	0.0	d

d - Displacements include imported displacements.

Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements x	y	Horizontal displacement along the Line	Horizontal displacement perpendicular to Line	
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]	
0.0	18.08000	6.15000	32.67000	-2.6640	0.0	-2.6640	0.0	d
1.0000	19.08000	6.15000	32.67000	-2.2140	0.0	-2.2140	0.0	d
2.0000	20.08000	6.15000	32.67000	-1.7640	0.0	-1.7640	0.0	d
3.0000	21.08000	6.15000	32.67000	-1.3140	0.0	-1.3140	0.0	d
4.0000	22.08000	6.15000	32.67000	-0.86400	0.0	-0.86400	0.0	d
5.0000	23.08000	6.15000	32.67000	-0.41400	0.0	-0.41400	0.0	d
6.0000	24.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	d
7.0000	25.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	d
8.0000	26.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	d
9.0000	27.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	d
10.000	28.08000	6.15000	32.67000	0.0	0.0	0.0	0.0	d

d - Displacements include imported displacements.

Specific Building Damage Results - Vertical Displacements

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements z	
[m]	[m]	[m]	[m]	[mm]	
Vertical Offset 1					
0.0	8.08000	6.15000	32.67000	5.3456	d
1.0000	9.08000	6.15000	32.67000	6.1385	d
2.0000	10.08000	6.15000	32.67000	6.2115	d
3.0000	11.08000	6.15000	32.67000	5.8166	d
4.0000	12.08000	6.15000	32.67000	5.1891	d
5.0000	13.08000	6.15000	32.67000	4.4722	d
6.0000	14.08000	6.15000	32.67000	3.7170	d
7.0000	15.08000	6.15000	32.67000	2.9297	d
8.0000	16.08000	6.15000	32.67000	2.1993	d
9.0000	17.08000	6.15000	32.67000	1.5264	d
10.000	18.08000	6.15000	32.67000	0.95853	d

d - Displacements include imported displacements.

Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Dist.	Coordinates x	y	z	Displacements z	
[m]	[m]	[m]	[m]	[mm]	
Vertical Offset 1					
0.0	18.08000	6.15000	32.67000	0.95853	d
1.0000	19.08000	6.15000	32.67000	0.52245	d
2.0000	20.08000	6.15000	32.67000	0.22409	d
3.0000	21.08000	6.15000	32.67000	0.048872	d
4.0000	22.08000	6.15000	32.67000	-0.038171	d
5.0000	23.08000	6.15000	32.67000	-0.092363	d
6.0000	24.08000	6.15000	32.67000	-0.18318	d
7.0000	25.08000	6.15000	32.67000	-0.16559	d
8.0000	26.08000	6.15000	32.67000	-0.15014	d
9.0000	27.08000	6.15000	32.67000	-0.13652	d
10.000	28.08000	6.15000	32.67000	-0.12447	d

d - Displacements include imported displacements.

Dist.	Coordinates x	y	z	Displacements z
[m]	[m]	[m]	[m]	[mm]

Specific Building Damage Results - All Segments

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
[m]		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	6.2471	Sagging	0.023162	0.045000	0.074032	-449.80E-6	-792.55E-6	1278.5	1 (Very Slight)
	2	6.2471	3.7519	Hogging	0.0033376	0.045000	0.046566	-449.80E-6	787.00E-6	8550.3	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
[m]		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	7.9327	Hogging	0.0061583	0.033582	0.039214	-449.80E-6	435.88E-6	7080.7	0 (Negligible)
	2	7.9327	2.0673	Sagging	42.011E-6	0.0	40.805E-6	0.0	-15.449E-6	543470.	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Specific Building Damage Results - Critical Values for All Segments within Each Sub-Structure

Structure: No.5 Albert Terrace Mews | Sub-structure: No.5 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.023162	0.045000	-792.55E-6	6.2083	0.074032	-449.80E-6	-792.55E-6	8550.3	1278.5	1 (Very Slight)

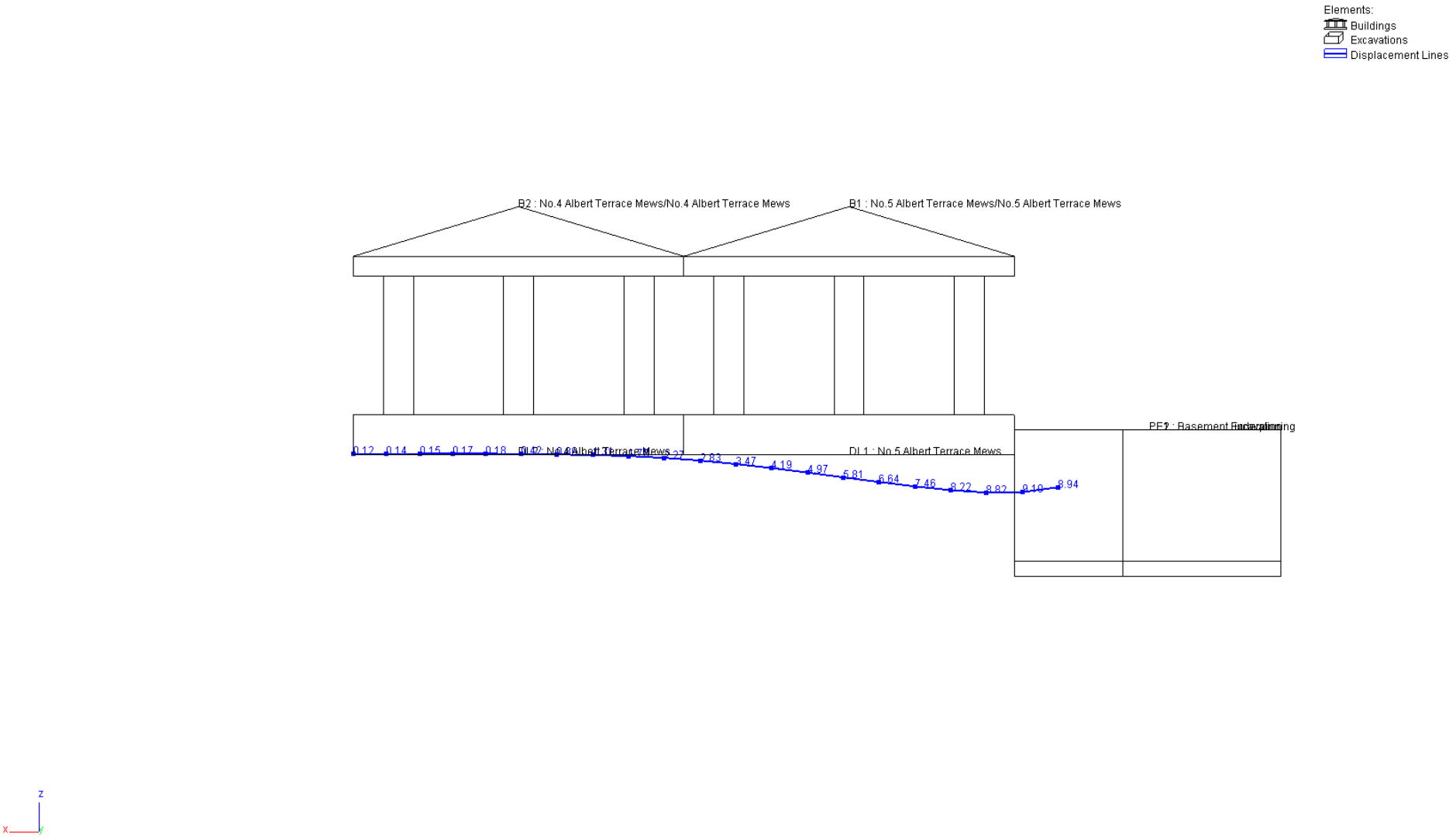
Structure: No.4 Albert Terrace Mews | Sub-structure: No.4 Albert Terrace Mews

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.0061583	0.033582	435.88E-6	0.95853	0.039214	-449.80E-6	435.88E-6	7080.7	543470.	0 (Negligible)

Specific Building Damage Results - Critical Segments within Each Structure

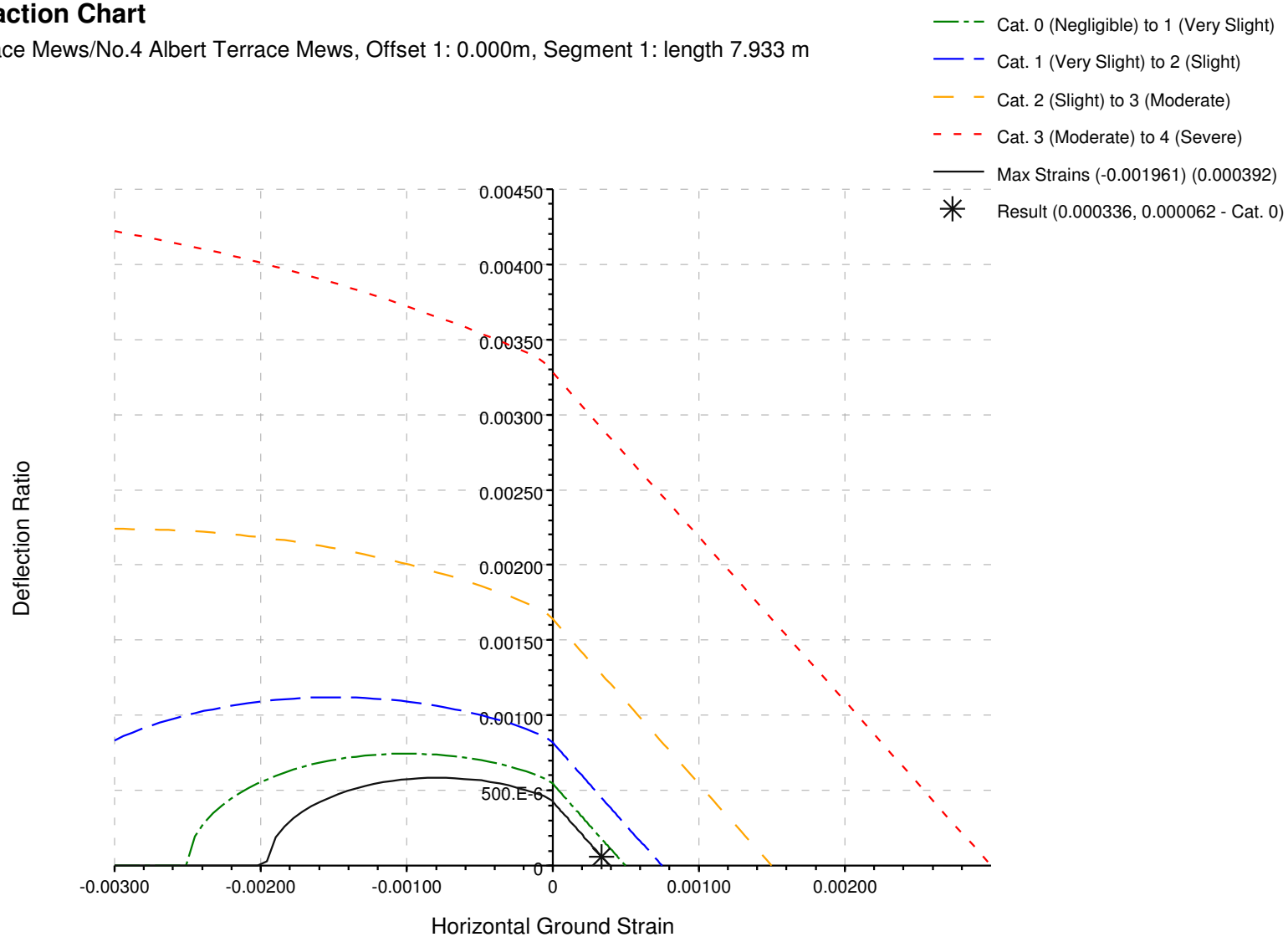
Structure Name	Parameter	Critical Sub-Structure	Critical Segment	Start	End	Curvature	Max Slope	Max Settlement	Max Tensile Strain	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
				[m]	[m]			[mm]	[%]	[m]	[m]	
No.5 Albert Terrace Mews	Max Slope	No.5 Albert Terrace Mews	1	0.0	6.2471	Sagging	**792.55E-6**	6.2083	0.074032	-	1278.5	1 (Very Slight)
	Max Settlement	No.5 Albert Terrace Mews	1	0.0	6.2471	Sagging	792.55E-6	**6.2083**	0.074032	-	1278.5	1 (Very Slight)
	Max Tensile Strain	No.5 Albert Terrace Mews	1	0.0	6.2471	Sagging	792.55E-6	6.2083	**0.074032**	-	1278.5	1 (Very Slight)
	Min Radius of Curvature (Hogging)	No.5 Albert Terrace Mews	2	6.2471	9.9990	Hogging	787.00E-6	3.5225	0.046566	**8550.3**	-	0 (Negligible)
	Min Radius of Curvature (Sagging)	No.5 Albert Terrace Mews	1	0.0	6.2471	Sagging	792.55E-6	6.2083	0.074032	-	**1278.5**	1 (Very Slight)
No.4 Albert Terrace Mews	Max Slope	No.4 Albert Terrace Mews	1	0.0	7.9327	Hogging	**435.88E-6**	0.95853	0.039214	7080.7	-	0 (Negligible)
	Max Settlement	No.4 Albert Terrace Mews	1	0.0	7.9327	Hogging	435.88E-6	**0.95853**	0.039214	7080.7	-	0 (Negligible)
	Max Tensile Strain	No.4 Albert Terrace Mews	1	0.0	7.9327	Hogging	435.88E-6	0.95853	**0.039214**	7080.7	-	0 (Negligible)
	Min Radius of Curvature (Hogging)	No.4 Albert Terrace Mews	1	0.0	7.9327	Hogging	435.88E-6	0.95853	0.039214	**7080.7**	-	0 (Negligible)
	Min Radius of Curvature (Sagging)	No.4 Albert Terrace Mews	2	7.9327	10.000	Sagging	15.449E-6	0.15118	40.805E-6	-	**543470.**	0 (Negligible)

Graphics Display



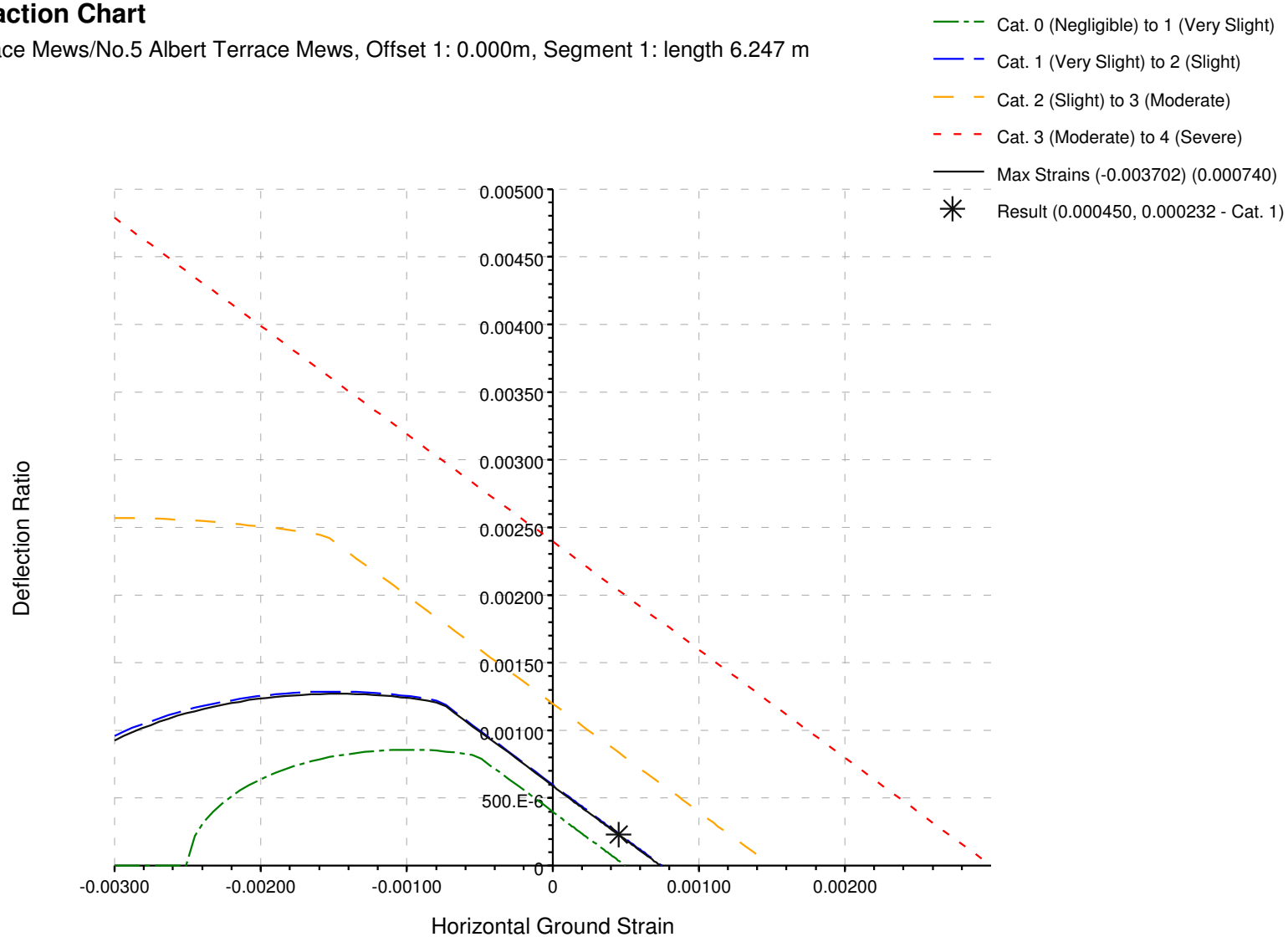
Building Damage Interaction Chart

Structure 2: No.4 Albert Terrace Mews/No.4 Albert Terrace Mews, Offset 1: 0.000m, Segment 1: length 7.933 m



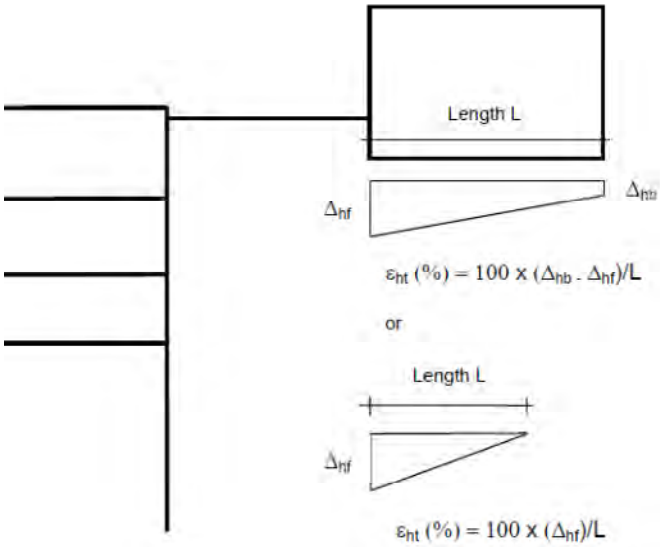
Building Damage Interaction Chart

Structure 1: No.5 Albert Terrace Mews/No.5 Albert Terrace Mews, Offset 1: 0.000m, Segment 1: length 6.247 m



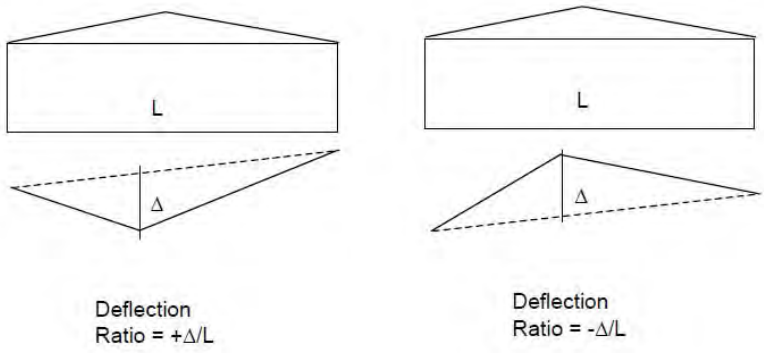
Horizontal Tensile Strain ε_{ht}

To determine the resulting horizontal tensile strain that will develop in the adjacent properties, the lateral displacement to the rear of the property (Δ_{hb}) is subtracted from the lateral displacement at the front of the property (Δ_{hf}). The resulting differential lateral displacement is then divided by the length of the property perpendicular to the basement wall to determine the horizontal tensile strain. Where the lateral displacement is zero at the rear of the property the lateral displacement at the front of the property is divided by the distance from the front of the property to the point of zero lateral displacement to determine the lateral strain. This approach is illustrated below and has been adopted for both the lateral displacements caused by wall installation and excavation.



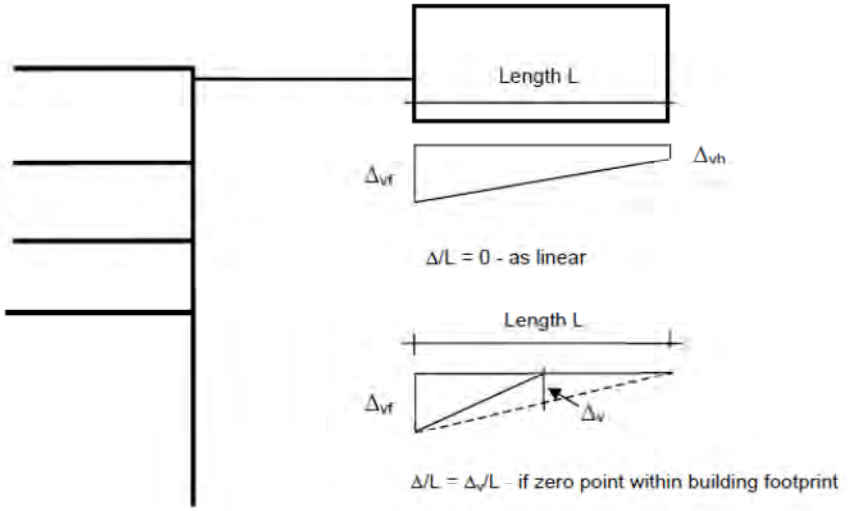
Deflection Ratio Δ/L

The deflection ratio is defined as the off linear vertical displacement across a structure as illustrated below.



A negative deflection ratio will result in greater damage to a property, as tension will be developed in the superstructure. Conversely with a positive deflection ratio compression will develop within the superstructure, which can be more easily resisted.

In the case of properties adjacent to a basement excavation the deflection ratio will depend on the distribution of vertical ground movement across its footprint. Reference to Figure 2.8 of CIRIA 580 in fact indicates a linear distribution of settlement due to wall installation with distance from the wall. As such the Deflection Ratio will be zero unless the point at which settlement ceases is within the footprint of the building as illustrated below.



Reference to Figure 2.11 of CIRIA 580 also indicates that the pattern of ground settlement due to basement excavation is relatively linear. As such the resulting Deflection Ratio is likely to be small. Within one excavation depth of the basement wall some non linearity is indicated however this would tend to result in a positive Deflection Ratio and as such be less likely to cause damage.

From the above discussion it is apparent that based on the empirical approach the vertical movements resulting from basement construction will only have a small influence on the damage to adjacent property compared to the lateral movements.

APPENDIX C
DEFINITION OF DAMAGE CATEGORIES

Table 2.5 *Classification of visible damage to walls (after Burland et al, 1977, Boscardin and Cording, 1989; and Burland, 2001)*

Category of damage	Description of typical damage (ease of repair is underlined)	Approximate crack width (mm)	Limiting tensile strain ε_{lim} (per cent)
0 Negligible	Hairline cracks of less than about 0.1 mm are classed as negligible.	< 0.1	0.0–0.05
1 Very slight	Fine cracks that can easily be treated during normal decoration. Perhaps isolated slight fracture in building. Cracks in external brickwork visible on inspection.	< 1	0.05–0.075
2 Slight	Cracks easily filled. Redecoration probably required. Several slight fractures showing inside of building. Cracks are visible externally and some repointing may be required externally to ensure weathertightness. Doors and windows may stick slightly.	< 5	0.075–0.15
3 Moderate	The cracks require some opening up and can be patched by a mason. Recurrent cracks can be masked by suitable linings. Repointing of external brickwork and possibly a small amount of brickwork to be replaced. Doors and windows sticking. Service pipes may fracture. Weathertightness often impaired.	5–15 or a number of cracks > 3	0.15–0.3
4 Severe	Extensive repair work involving breaking-out and replacing sections of walls, especially over doors and windows. Windows and frames distorted, floor sloping noticeably. Walls leaning or bulging noticeably, some loss of bearing in beams. Service pipes disrupted.	15–25 but also depends on number of cracks	> 0.3
5 Very severe	This requires a major repair involving partial or complete rebuilding. Beams lose bearings, walls lean badly and require shoring. Windows broken with distortion. Danger of instability.	usually > 25 but depends on number of cracks.	

Notes

1. In assessing the degree of damage, account must be taken of its location in the building or structure.
2. Crack width is only one aspect of damage and should not be used on its own as a direct measure of it.

APPENDIX D
DETERMINATION OF VERTICAL ELASTIC DISPLACEMENTS – RESULTS FROM PDISP ANALYSIS

Analysis Options

Analysis: Boussinesq
Global Poisson's ratio: 0.50
Maximum allowable ratio between values of E: 1.5
Horizontal rigid boundary level: -15.00 [m OD]
Stiffness for horizontal displacement calculations: Weighted average
Using legacy heave correction factor: No
Displacements at load centroids: Yes

Soil ProfilesSoil Profile 1

Layer	Level at top	Number of intermediate displacement levels	Youngs Modulus Top	Youngs Modulus Btm	Poissons ratio	Non-linear curve
	[mOD]		[kN/m²]	[kN/m²]		
1	35.000	5	9600.0	9600.0	0.50000	None
2	32.500	5	20000.	31000.	0.50000	None
3	29.000	5	31000.	42000.	0.50000	None
4	25.500	5	42000.	53000.	0.50000	None
5	22.000	5	53000.	64000.	0.50000	None
6	18.500	5	64000.	75000.	0.50000	None
7	15.000	10	75000.	2.5000E+6	0.50000	None

Soil Zones

Zone	Name	X coordinates min [m]	X coordinates max [m]	Y coordinates min [m]	Y coordinates max [m]	Profile
1	Soil Zone 1	-20.00000	30.00000	-20.00000	30.00000	Soil Profile 1

Load Data

Load ref.	Name	Shape	Orientation of Plane	Centre of load (Global) X [m]	Y [m]	Z (level) [m]	Load position Angle of local x from [Degrees]	Width x or Radius [m]	Length y [m]	Polygon Coordinates [m]	Rectangle tolerance [%]	Number of rectangles	Load value Normal (local z) [kN/m²]	Tangential (local x) [kN/m²]	(local y) [kN/m²]
1	Proposed Basement Excavation (including lowering of ground floor)	Polygonal	Horizontal	N/A	N/A	29.43000	N/A	N/A	N/A	(0,0) (3,0) (4.79,0.29) (8.08,0.8) (8.08,11.5) (4.79,10.9) (3,10.5) (0,11.8) (0,0)	10.000	3	-82.650	N/A	N/A

Polygonal Loads' Rectangles

No.	Centre of load X [m]	Centre of load Y [m]	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
Load 1 : Proposed Basement Excavation (including lowering of ground floor)					
(Edge 1 optimal)					
1	1.50000	5.57250	0.0	3.0000	11.145
2	3.89500	5.41250	0.0	1.7900	10.535
3	6.43500	5.86500	0.0	3.2900	10.640

Displacement Data

Ref.	Type	Name	Direction of Extrusion	Line/Line for extrusion First point X [m]	First point Y [m]	First point Z(level) [m]	Second point X [m]	Second point Y [m]	Second point Z(level) [m]	No. of intrvls across extrusion/line	Extrusion Depth [m]	No. of intrvls along extrusion	Calculate	Show Detailed results
1	Grid	Proposed Basement Level	Global X	-20.00000	-20.00000	29.43000	N/A	30.00000	29.43000	25	50.00000	25	Yes	Yes
2	Line	No. 8 Albert Terrace Mews	N/A	8.08000	6.15000	34.25000	18.08000	6.15000	34.25000	10	N/A	N/A	Yes	Yes

RESULTS FOR GRIDS

Analysis: Boussinesq
Global Poisson's ratio: 0.50
Horizontal rigid boundary level: -15.00 [m OD]

The maximum displacement difference between the Boussinesq method (-5.2054mm) and the Mindlin method (-3.7780mm) occurs at point X = 8.08000m, Y = 6.15000m, level = 34.250mOD, and is 1.4274mm.

Name	Location X [m]	Location Y [m]	Location Z[Level] [mOD]	Displacement Z [mm]	Stresses Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
Proposed Basement Excavation (including lowering of ground floor)	3.98649	5.65795	29.43000	-9.3319	29.215	-82.643	-237.45	-172.77E-6
Proposed Basement Level	-20.00000	-20.00000	29.43000	0.056118	29.215	0.0	-0.017630	0.0
	-18.00000	-20.00000	29.43000	0.060595	29.215	0.0	-0.019879	0.0
	-16.00000	-20.00000	29.43000	0.065213	29.215	-1.0472E-6	-0.022388	0.0
	-14.00000	-20.00000	29.43000	0.069896	29.215	-1.2771E-6	-0.025153	0.0
	-12.00000	-20.00000	29.43000	0.074545	29.215	-1.5480E-6	-0.028153	0.0
	-10.00000	-20.00000	29.43000	0.079046	29.215	-1.8591E-6	-0.031335	0.0
	-8.00000	-20.00000	29.43000	0.083271	29.215	-2.2045E-6	-0.034613	0.0
	-6.00000	-20.00000	29.43000	0.087090	29.215	-2.5708E-6	-0.037862	0.0
	-4.00000	-20.00000	29.43000	0.090382	29.215	-2.9362E-6	-0.040915	0.0
	-2.00000	-20.00000	29.43000	0.093043	29.215	-3.2709E-6	-0.043579	0.0
	0.00000	-20.00000	29.43000	0.094995	29.215	-3.5410E-6	-0.045653	0.0
	2.00000	-20.00000	29.43000	0.096185	29.215	-3.7145E-6	-0.046961	0.0
	4.00000	-20.00000	29.43000	0.096581	29.215	-3.7693E-6	-0.047384	0.0
	6.00000	-20.00000	29.43000	0.096174	29.215	-3.6982E-6	-0.046882	0.0
	8.00000	-20.00000	29.43000	0.094972	29.215	-3.5114E-6	-0.045506	0.0
	10.00000	-20.00000	29.43000	0.093002	29.215	-3.2332E-6	-0.043384	0.0
	12.00000	-20.00000	29.43000	0.090320	29.215	-2.8957E-6	-0.040694	0.0
	14.00000	-20.00000	29.43000	0.087006	29.215	-2.5320E-6	-0.037636	0.0
	16.00000	-20.00000	29.43000	0.083168	29.215	-2.1700E-6	-0.034398	0.0
	18.00000	-20.00000	29.43000	0.078929	29.215	-1.8303E-6	-0.031140	0.0
	20.00000	-20.00000	29.43000	0.074420	29.215	-1.5249E-6	-0.027982	0.0
	22.00000	-20.00000	29.43000	0.069768	29.215	-1.2592E-6	-0.025009	0.0
	24.00000	-20.00000	29.43000	0.065088	29.215	-1.0335E-6	-0.022267	0.0
	26.00000	-20.00000	29.43000	0.060476	29.215	0.0	-0.019780	0.0
	28.00000	-20.00000	29.43000	0.056008	29.215	0.0	-0.017549	0.0
	30.00000	-20.00000	29.43000	0.051738	29.215	0.0	-0.015566	0.0
	-20.00000	-18.00000	29.43000	0.060878	29.215	0.0	-0.020008	0.0
	-18.00000	-18.00000	29.43000	0.066004	29.215	-1.0793E-6	-0.022812	0.0
	-16.00000	-18.00000	29.43000	0.071311	29.215	-1.3489E-6	-0.026002	0.0
	-14.00000	-18.00000	29.43000	0.076705	29.215	-1.6824E-6	-0.029593	0.0
	-12.00000	-18.00000	29.43000	0.082058	29.215	-2.0883E-6	-0.033577	0.0
	-10.00000	-18.00000	29.43000	0.087224	29.215	-2.5711E-6	-0.037903	0.0
	-8.00000	-18.00000	29.43000	0.092039	29.215	-3.1262E-6	-0.042470	0.0
	-6.00000	-18.00000	29.43000	0.096344	29.215	-3.7358E-6	-0.047103	0.0
	-4.00000	-18.00000	29.43000	0.099999	29.215	-4.3638E-6	-0.051555	0.0
	-2.00000	-18.00000	29.43000	0.10291	29.215	-4.9555E-6	-0.055516	0.0
	0.00000	-18.00000	29.43000	0.10500	29.215	-5.4433E-6	-0.058647	0.0
	2.00000	-18.00000	29.43000	0.10627	29.215	-5.7609E-6	-0.060641	0.0
	4.00000	-18.00000	29.43000	0.10670	29.215	-5.8604E-6	-0.061283	1.0103E-6
	6.00000	-18.00000	29.43000	0.10628	29.215	-5.7269E-6	-0.060504	0.0
	8.00000	-18.00000	29.43000	0.10502	29.215	-5.3830E-6	-0.058398	0.0

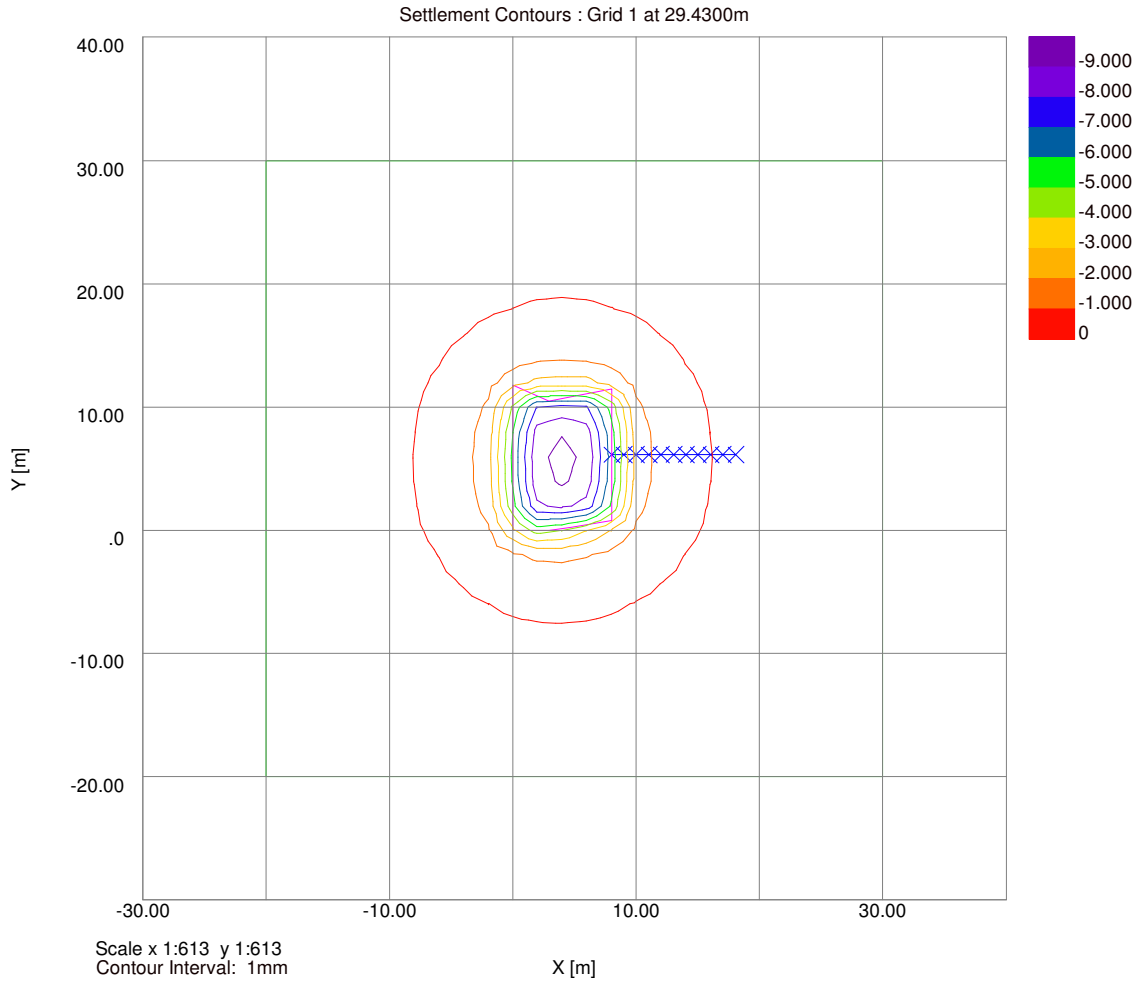
Name	Location			Displacement	Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	10.00000	-18.00000	29.43000	0.10291	29.215	-4.8809E-6	-0.055194	0.0
	12.00000	-18.00000	29.43000	0.099978	29.215	-4.2869E-6	-0.051202	0.0
	14.00000	-18.00000	29.43000	0.096290	29.215	-3.6653E-6	-0.046754	0.0
	16.00000	-18.00000	29.43000	0.091954	29.215	-3.0667E-6	-0.042149	0.0
	18.00000	-18.00000	29.43000	0.087113	29.215	-2.5237E-6	-0.037623	0.0
	20.00000	-18.00000	29.43000	0.081931	29.215	-2.0522E-6	-0.033341	0.0
	22.00000	-18.00000	29.43000	0.076570	29.215	-1.6555E-6	-0.029400	0.0
	24.00000	-18.00000	29.43000	0.071176	29.215	-1.3293E-6	-0.025846	0.0
	26.00000	-18.00000	29.43000	0.065874	29.215	-1.0651E-6	-0.022687	0.0
	28.00000	-18.00000	29.43000	0.060758	29.215	0.0	-0.019909	0.0
	30.00000	-18.00000	29.43000	0.055894	29.215	0.0	-0.017483	0.0
	-20.00000	-16.00000	29.43000	0.065855	29.215	-1.0683E-6	-0.022701	0.0
	-18.00000	-16.00000	29.43000	0.071681	29.215	-1.3633E-6	-0.026198	0.0
	-16.00000	-16.00000	29.43000	0.077726	29.215	-1.7439E-6	-0.030263	0.0
	-14.00000	-16.00000	29.43000	0.083863	29.215	-2.2312E-6	-0.034949	0.0
	-12.00000	-16.00000	29.43000	0.089926	29.215	-2.8475E-6	-0.040283	0.0
	-10.00000	-16.00000	29.43000	0.095711	29.215	-3.6106E-6	-0.046239	0.0
	-8.00000	-16.00000	29.43000	0.10100	29.215	-4.5264E-6	-0.052708	0.0
	-6.00000	-16.00000	29.43000	0.10560	29.215	-5.5759E-6	-0.059464	0.0
	-4.00000	-16.00000	29.43000	0.10935	29.215	-6.7021E-6	-0.066139	1.0904E-6
	-2.00000	-16.00000	29.43000	0.11220	29.215	-7.8017E-6	-0.072226	1.1907E-6
	0.00000	-16.00000	29.43000	0.11415	29.215	-8.7339E-6	-0.077133	1.2716E-6
	2.00000	-16.00000	29.43000	0.11529	29.215	-9.3506E-6	-0.080295	1.3237E-6
	4.00000	-16.00000	29.43000	0.11569	29.215	-9.5419E-6	-0.081309	1.3404E-6
	6.00000	-16.00000	29.43000	0.11536	29.215	-9.2742E-6	-0.080048	1.3196E-6
	8.00000	-16.00000	29.43000	0.11427	29.215	-8.6018E-6	-0.076691	1.2643E-6
	10.00000	-16.00000	29.43000	0.11231	29.215	-7.6449E-6	-0.071671	1.1816E-6
	12.00000	-16.00000	29.43000	0.10944	29.215	-6.5486E-6	-0.065554	1.0807E-6
	14.00000	-16.00000	29.43000	0.10563	29.215	-5.4432E-6	-0.058911	0.0
	16.00000	-16.00000	29.43000	0.10097	29.215	-4.4210E-6	-0.052222	0.0
	18.00000	-16.00000	29.43000	0.095629	29.215	-3.5316E-6	-0.045834	0.0
	20.00000	-16.00000	29.43000	0.089810	29.215	-2.7904E-6	-0.039956	0.0
	22.00000	-16.00000	29.43000	0.083729	29.215	-2.1910E-6	-0.034691	0.0
	24.00000	-16.00000	29.43000	0.077586	29.215	-1.7159E-6	-0.030062	0.0
	26.00000	-16.00000	29.43000	0.071544	29.215	-1.3440E-6	-0.026042	0.0
	28.00000	-16.00000	29.43000	0.065726	29.215	-1.0550E-6	-0.022581	0.0
	30.00000	-16.00000	29.43000	0.060218	29.215	0.0	-0.019615	0.0
	-20.00000	-14.00000	29.43000	0.070979	29.215	-1.3184E-6	-0.025720	0.0
	-18.00000	-14.00000	29.43000	0.077539	29.215	-1.7211E-6	-0.030074	0.0
	-16.00000	-14.00000	29.43000	0.084342	29.215	-2.2586E-6	-0.035257	0.0
	-14.00000	-14.00000	29.43000	0.091211	29.215	-2.9743E-6	-0.041392	0.0
	-12.00000	-14.00000	29.43000	0.097905	29.215	-3.9195E-6	-0.048582	0.0
	-10.00000	-14.00000	29.43000	0.10413	29.215	-5.1476E-6	-0.056874	0.0
	-8.00000	-14.00000	29.43000	0.10958	29.215	-6.6995E-6	-0.066199	1.0914E-6
	-6.00000	-14.00000	29.43000	0.11397	29.215	-8.5758E-6	-0.076292	1.2577E-6
	-4.00000	-14.00000	29.43000	0.11716	29.215	-10.697E-6	-0.086621	1.4279E-6
	-2.00000	-14.00000	29.43000	0.11918	29.215	-12.867E-6	-0.096344	1.5882E-6
	0.00000	-14.00000	29.43000	0.12028	29.215	-14.774E-6	-0.10439	1.7207E-6
	2.00000	-14.00000	29.43000	0.12079	29.215	-16.062E-6	-0.10965	1.8075E-6
	4.00000	-14.00000	29.43000	0.12100	29.215	-16.456E-6	-0.11133	1.8351E-6
	6.00000	-14.00000	29.43000	0.12100	29.215	-15.873E-6	-0.10917	1.7996E-6
	8.00000	-14.00000	29.43000	0.12063	29.215	-14.459E-6	-0.10355	1.7070E-6
	10.00000	-14.00000	29.43000	0.11957	29.215	-12.513E-6	-0.095340	1.5716E-6
	12.00000	-14.00000	29.43000	0.11748	29.215	-10.373E-6	-0.085615	1.4114E-6
	14.00000	-14.00000	29.43000	0.11418	29.215	-8.3161E-6	-0.075393	1.2429E-6
	16.00000	-14.00000	29.43000	0.10966	29.215	-6.5083E-6	-0.065453	1.0791E-6
	18.00000	-14.00000	29.43000	0.10412	29.215	-5.0143E-6	-0.056284	0.0
	20.00000	-14.00000	29.43000	0.097824	29.215	-3.8295E-6	-0.048129	0.0
	22.00000	-14.00000	29.43000	0.091090	29.215	-2.9146E-6	-0.041050	0.0
	24.00000	-14.00000	29.43000	0.084204	29.215	-2.2192E-6	-0.035001	0.0
	26.00000	-14.00000	29.43000	0.077399	29.215	-1.6951E-6	-0.029883	0.0
	28.00000	-14.00000	29.43000	0.070845	29.215	-1.3012E-6	-0.025577	0.0
	30.00000	-14.00000	29.43000	0.064655	29.215	-1.0050E-6	-0.021962	0.0
	-20.00000	-12.00000	29.43000	0.076158	29.215	-1.6193E-6	-0.029060	0.0
	-18.00000	-12.00000	29.43000	0.083462	29.215	-2.1657E-6	-0.034460	0.0
	-16.00000	-12.00000	29.43000	0.091000	29.215	-2.9227E-6	-0.041052	0.0
	-14.00000	-12.00000	29.43000	0.098513	29.215	-3.9748E-6	-0.049087	0.0
	-12.00000	-12.00000	29.43000	0.10564	29.215	-5.4347E-6	-0.058823	0.0
	-10.00000	-12.00000	29.43000	0.11190	29.215	-7.4419E-6	-0.070481	1.1620E-6
	-8.00000	-12.00000	29.43000	0.11681	29.215	-10.143E-6	-0.084150	1.3872E-6
	-6.00000	-12.00000	29.43000	0.11993	29.215	-13.638E-6	-0.099622	1.6422E-6
	-4.00000	-12.00000	29.43000	0.12109	29.215	-17.868E-6	-0.11619	1.9152E-6
	-2.00000	-12.00000	29.43000	0.12057	29.215	-22.474E-6	-0.13246	2.1833E-6
	0.00000	-12.00000	29.43000	0.11914	29.215	-26.724E-6	-0.14638	2.4127E-6
	2.00000	-12.00000	29.43000	0.11783	29.215	-29.672E-6	-0.15568	2.5659E-6
	4.00000	-12.00000	29.43000	0.11749	29.215	-30.550E-6	-0.15863	2.6144E-6
	6.00000	-12.00000	29.43000	0.11839	29.215	-29.147E-6	-0.15467	2.5493E-6
	8.00000	-12.00000	29.43000	0.12005	29.215	-25.891E-6	-0.14468	2.3847E-6
	10.00000	-12.00000	29.43000	0.12154	29.215	-21.605E-6	-0.13053	2.1515E-6
	12.00000	-12.00000	29.43000	0.12190	29.215	-17.143E-6	-0.11439	1.8855E-6
	14.00000	-12.00000	29.43000	0.12049	29.215	-13.110E-6	-0.098123	1.6175E-6
	16.00000	-12.00000	29.43000	0.11712	29.215	-9.7898E-6	-0.082991	1.3681E-6
	18.00000	-12.00000	29.43000	0.11202	29.215	-7.2161E-6	-0.069623	1.1478E-6
	20.00000	-12.00000	29.43000	0.10562	29.215	-5.2938E-6	-0.058201	0.0
	22.00000	-12.00000	29.43000	0.098424	29.215	-3.8874E-6	-0.048640	0.0
	24.00000	-12.00000	29.43000	0.090873	29.215	-2.8683E-6	-0.040732	0.0
	26.00000	-12.00000	29.43000	0.083323	29.215	-2.1315E-6	-0.034230	0.0
	28.00000	-12.00000	29.43000	0.076023	29.215	-1.5976E-6	-0.028893	0.0
	30.00000	-12.00000	29.43000	0.069130	29.215	-1.2085E-6	-0.024510	0.0
	-20.00000	-10.00000	29.43000	0.081277	29.215	-1.9738E-6	-0.032690	0.0
	-18.00000	-10.00000	29.43000	0.089297	29.215	-2.7075E-6	-0.039338	0.0
	-16.00000	-10.00000	29.43000	0.097494	29.215	-3.7648E-6	-0.047677	0.0
	-14.00000	-10.00000	29.43000	0.10547	29.215	-5.3044E-6	-0.058165	0.0
	-12.00000	-10.00000	29.43000	0.11263	29.215	-7.5628E-6	-0.071356	1.1764E-6
	-10.00000	-10.00000	29.43000	0.11820	29.215	-10.879E-6	-0.087854	1.4483E-6
	-8.00000	-10.00000	29.43000	0.12125	29.215	-15.698E-6	-0.10819	1.7834E-6
	-6.00000	-10.00000	29.43000	0.12099	29.215	-22.499E-6	-0.13255	2.1847E-6
	-4.00000	-10.00000	29.43000	0.11709	29.215	-31.521E-6	-0.16023	2.6408E-6
	-2.00000	-10.00000	29.43000	0.11027	29.215	-42.237E-6	-0.18902	3.1150E-6
	0.00000	-10.00000	29.43000	0.10251	29.215	-52.817E-6	-0.21485	3.5405E-6
	2.00000	-10.00000	29.43000	0.096590	29.215	-60.407E-6	-0.23260	3.8328E-6
	4.00000	-10.00000	29.43000	0.094857	29.215	-62.561E-6	-0.23811	3.9237E-6
	6.00000	-10.00000	29.43000	0.097993	29.215	-58.701E-6	-0.23021	3.7935E-6
	8.00000	-10.00000	29.43000	0.10472	29.215	-50.292E-6	-0.21106	3.4781E-6
	10.00000	-10.00000	29.43000	0.11254	29.215	-39.869E-6	-0.18504	3.0496E-6
	12.00000	-10.00000	29.43000	0.11893	29.215	-29.779E-6	-0.15685	2.5851E-6
	14.00000	-10.00000	29.43000	0.12223	29.215	-21.385E-6	-0.12999	2.1427E-6
	16.00000	-10.00000	29.43000	0.12197	29.215	-15.038E-6	-0.10639	1.7537E-6
	18.00000	-10.00000	29.43000	0.11853	29.215	-10.500E-6	-0.086618	1.4279E-6
	20.00000	-10.00000	29.43000	0.11273	29.215	-7.3466E-6	-0.070518	1.1626E-6
	22.00000	-10.00000	29.43000	0.10543	29.215	-5.1800E-6	-0.057596	0.0
	24.00000	-10.00000	29.43000	0.097390	29.215	-3.6921E-6	-0.047287	0.0
	26.00000	-10.00000	29.43000	0.089168	29.215	-2.6641E-6	-0.039068	0.0
	28.00000	-10.00000	29.43000	0.081145	29.215	-1.9473E-6	-0.032500	0.0
	30.00000	-10.00000	29.43000	0.073552	29.215	-1.4419E-6	-0.027226	0.0
	-20.00000	-8.00000	29.43000	0.086203	29.215	-2.3794E-6	-0.036538	0.0
	-18.00000	-8.00000	29.43000	0.094876	29.215	-3.3495E-6	-0.044637	0.0
	-16.00000	-8.00000	29.43000	0.10359	29.215	-4.8049E-6	-0.055080	0.0
	-14.00000	-8.00000	29.43000	0.11173	29.215	-7.0312E-6	-0.068662	1.1320E-6
	-12.00000	-8.00000	29.43000	0.11832	29.215	-10.501E-6	-0.086448	1.4251E-6
	-10.00000	-8.00000	29.43000	0.12198	29.215	-15.991E-6	-0.10982	1.8102E-6
	-8.00000	-8.00000	29.43000	0.12097	29.215	-24.746E-6	-0.14039	2.3140E-6
	-6.00000	-8.00000	29.43000	0.11346	29.215	-38.561E-6	-0.17970	2.9615E-6
	-4.00000	-8.00000	29.43000	0.098481	29.215	-59.380E-6	-0.22811	3.7589E-6
	-2.00000	-8.00000	29.43000	0.077233	29.215	-87.477E-6	-0.28276	4.6587E-6
	0.00000	-8.00000	29.43000	0.054377	29.215	-118.14E-6	-0.33526	5.5229E-6
	2.00000	-8.00000	29.43000	0.037214	29.215	-141.09E-6	-0.37269	6.1390E-6
	4.00000	-8.00000	29.43000	0.032110	29.215	-146.94E-6	-0.38392	6.3239E-6
	6.00000	-8.00000	29.43000	0.040811	29.215	-134.25E-6	-0.36616	6.0317E-6
	8.00000	-8.00000	29.43000	0.059761	29.215	-109.01E-6	-0.32571	5.3660E-6
	10.00000	-8.00000	29.43000	0.082363	29.215	-80.157E-6	-0.27388	4.5126E-6
	12.00000	-8.00000	29.43000	0.10230	29.215	-54.892E-6	-0.22151	3.6502E-6
	14.00000	-8.00000	29.43000	0.11589	29.215	-36.157E-6	-0.17532	2.8894E-6
	16.00000	-8.00000	29.43000	0.12231	29.215	-23.524E-6	-0.13762	2.2683E-6
	18.00000	-8.00000	29.43000	0.12264	29.215	-15.373E-6	-0.10808	1.7816E-6
	20.00000	-8.00000	29.43000	0.11857	29.215	-10.182E-6	-0.085357	1.4071E-6
	22.00000	-8.00000	29.43000	0.11176	29.215	-6.8620E-6	-0.067963	1.1204E-6
	24.00000	-8.00000	29.43000	0.10352	29.215	-4.7121E-6	-0.054624	0.0
	26.00000	-8.00000	29.43000	0.094761	29.215	-3.2969E-6	-0.044333	0.0
	28.00000	-8.00000	29.43000	0.086077	29.215	-2.3487E-6	-0.036330	0.0
	30.00000	-8.00000	29.43000	0.077814	29.215	-1.7019E-6	-0.030052	0.0

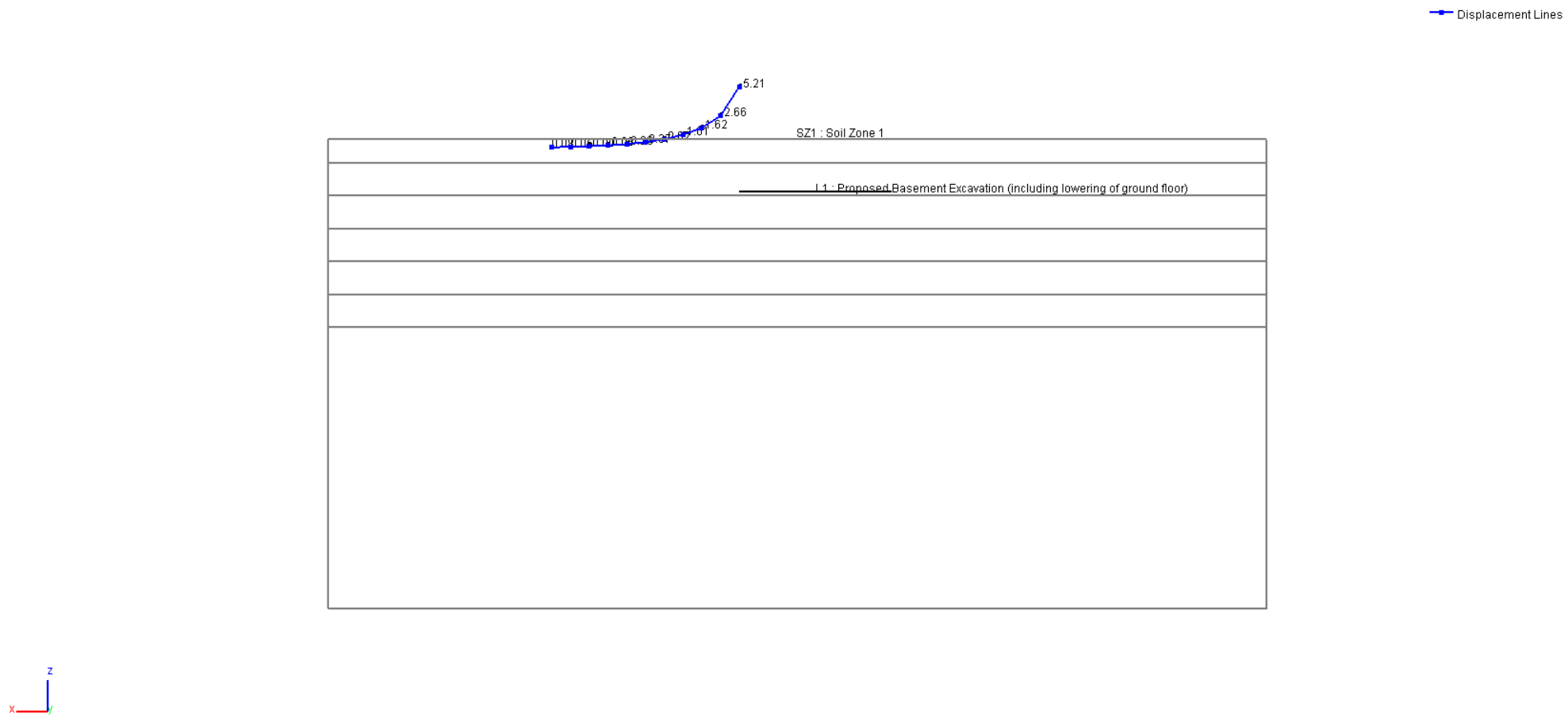
Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]	
	-20.00000	-6.00000	29.43000	0.090792	29.215	-2.8263E-6	-0.040490	0.0	
	-18.00000	-6.00000	29.43000	0.10002	29.215	-4.0813E-6	-0.050211	0.0	
	-16.00000	-6.00000	29.43000	0.10905	29.215	-6.0411E-6	-0.063095	1.0402E-6	
	-14.00000	-6.00000	29.43000	0.11695	29.215	-9.1921E-6	-0.080432	1.3260E-6	
	-12.00000	-6.00000	29.43000	0.12215	29.215	-14.423E-6	-0.10412	1.7163E-6	
	-10.00000	-6.00000	29.43000	0.12222	29.215	-23.411E-6	-0.13696	2.2574E-6	
	-8.00000	-6.00000	29.43000	0.11373	29.215	-39.375E-6	-0.18299	3.0158E-6	
	-6.00000	-6.00000	29.43000	0.092496	29.215	-68.429E-6	-0.24764	4.0804E-6	
	-4.00000	-6.00000	29.43000	0.054948	29.215	-120.91E-6	-0.33651	5.5435E-6	
	-2.00000	-6.00000	29.43000	0.0016910	29.215	-207.66E-6	-0.45001	7.4109E-6	
	0.00000	-6.00000	29.43000	-0.057286	29.215	-319.41E-6	-0.57143	9.4078E-6	
	2.00000	-6.00000	29.43000	-0.10232	29.215	-407.28E-6	-0.66234	10.903E-6	
	4.00000	-6.00000	29.43000	-0.11541	29.215	-424.00E-6	-0.68721	11.312E-6	
	6.00000	-6.00000	29.43000	-0.092438	29.215	-370.26E-6	-0.64040	10.543E-6	
	8.00000	-6.00000	29.43000	-0.043736	29.215	-277.02E-6	-0.54316	8.9437E-6	
	10.00000	-6.00000	29.43000	0.013096	29.215	-181.12E-6	-0.42821	7.0527E-6	
	12.00000	-6.00000	29.43000	0.062434	29.215	-108.59E-6	-0.32324	5.3252E-6	
	14.00000	-6.00000	29.43000	0.096768	29.215	-63.265E-6	-0.24023	3.9585E-6	
	16.00000	-6.00000	29.43000	0.11595	29.215	-37.208E-6	-0.17890	2.9484E-6	
	18.00000	-6.00000	29.43000	0.12327	29.215	-22.461E-6	-0.13465	2.2194E-6	
	20.00000	-6.00000	29.43000	0.12258	29.215	-13.984E-6	-0.10277	1.6942E-6	
	22.00000	-6.00000	29.43000	0.11707	29.215	-8.9769E-6	-0.079620	1.3126E-6	
	24.00000	-6.00000	29.43000	0.10902	29.215	-5.9302E-6	-0.062588	1.0319E-6	
	26.00000	-6.00000	29.43000	0.099921	29.215	-4.0215E-6	-0.049885	0.0	
	28.00000	-6.00000	29.43000	0.090677	29.215	-2.7926E-6	-0.040274	0.0	
	30.00000	-6.00000	29.43000	0.081800	29.215	-1.9813E-6	-0.032903	0.0	
	-20.00000	-4.00000	29.43000	0.094902	29.215	-3.2945E-6	-0.044381	0.0	
	-18.00000	-4.00000	29.43000	0.10455	29.215	-4.8733E-6	-0.055824	0.0	
	-16.00000	-4.00000	29.43000	0.11369	29.215	-7.4332E-6	-0.071396	1.1770E-6	
	-14.00000	-4.00000	29.43000	0.12091	29.215	-11.750E-6	-0.093051	1.5339E-6	
	-12.00000	-4.00000	29.43000	0.12377	29.215	-19.378E-6	-0.12391	2.0425E-6	
	-10.00000	-4.00000	29.43000	0.11822	29.215	-33.628E-6	-0.16914	2.7876E-6	
	-8.00000	-4.00000	29.43000	0.097819	29.215	-62.103E-6	-0.23747	3.9130E-6	
	-6.00000	-4.00000	29.43000	0.053167	29.215	-123.67E-6	-0.34405	5.6677E-6	
	-4.00000	-4.00000	29.43000	-0.027314	29.215	-267.43E-6	-0.51423	8.4670E-6	
	-2.00000	-4.00000	29.43000	-0.15101	29.215	-605.20E-6	-0.77968	12.828E-6	
	0.00000	-4.00000	29.43000	-0.30127	29.215	-0.0012117	-1.1257	18.504E-6	
	2.00000	-4.00000	29.43000	-0.42027	29.215	-0.0017161	-1.4017	23.030E-6	
	4.00000	-4.00000	29.43000	-0.45165	29.215	-0.0017309	-1.4569	23.940E-6	
	6.00000	-4.00000	29.43000	-0.38911	29.215	-0.0013913	-1.3006	21.379E-6	
	8.00000	-4.00000	29.43000	-0.26447	29.215	-917.36E-6	-1.0193	16.764E-6	
	10.00000	-4.00000	29.43000	-0.12601	29.215	-486.97E-6	-0.72034	11.855E-6	
	12.00000	-4.00000	29.43000	-0.013846	29.215	-232.76E-6	-0.48779	8.0327E-6	
	14.00000	-4.00000	29.43000	0.059830	29.215	-113.31E-6	-0.33231	5.4745E-6	
	16.00000	-4.00000	29.43000	0.10097	29.215	-58.633E-6	-0.23191	3.8216E-6	
	18.00000	-4.00000	29.43000	0.11964	29.215	-32.319E-6	-0.16632	2.7412E-6	
	20.00000	-4.00000	29.43000	0.12435	29.215	-18.832E-6	-0.12239	2.0174E-6	
	22.00000	-4.00000	29.43000	0.12108	29.215	-11.502E-6	-0.092180	1.5196E-6	
	24.00000	-4.00000	29.43000	0.11368	29.215	-7.3124E-6	-0.070874	1.1684E-6	
	26.00000	-4.00000	29.43000	0.10448	29.215	-4.8109E-6	-0.055499	0.0	
	28.00000	-4.00000	29.43000	0.094801	29.215	-3.2605E-6	-0.044170	0.0	
	30.00000	-4.00000	29.43000	0.085392	29.215	-2.2678E-6	-0.035665	0.0	
	-20.00000	-2.00000	29.43000	0.098406	29.215	-3.7539E-6	-0.048000	0.0	
	-18.00000	-2.00000	29.43000	0.10835	29.215	-5.6729E-6	-0.061155	1.0082E-6	
	-16.00000	-2.00000	29.43000	0.11737	29.215	-8.8894E-6	-0.079482	1.3103E-6	
	-14.00000	-2.00000	29.43000	0.12353	29.215	-14.549E-6	-0.10574	1.7431E-6	
	-12.00000	-2.00000	29.43000	0.12327	29.215	-25.125E-6	-0.14465	2.3842E-6	
	-10.00000	-2.00000	29.43000	0.11024	29.215	-46.466E-6	-0.20472	3.3738E-6	
	-8.00000	-2.00000	29.43000	0.073415	29.215	-94.211E-6	-0.30242	4.9826E-6	
	-6.00000	-2.00000	29.43000	-0.0061477	29.215	-217.94E-6	-0.47279	7.7860E-6	
	-4.00000	-2.00000	29.43000	-0.16011	29.215	-618.09E-6	-0.80034	13.168E-6	
	-2.00000	-2.00000	29.43000	-0.43632	29.215	-0.0024010	-1.5163	24.888E-6	
	0.00000	-2.00000	29.43000	-0.85401	29.215	-0.010470	-3.0392	49.601E-6	
	2.00000	-2.00000	29.43000	-1.2045	29.215	-0.017678	-4.3571	70.979E-6	
	4.00000	-2.00000	29.43000	-1.2665	29.215	-0.015137	-4.3269	70.607E-6	
	6.00000	-2.00000	29.43000	-1.0769	29.215	-0.0099195	-3.5154	57.482E-6	
	8.00000	-2.00000	29.43000	-0.73812	29.215	-0.0054768	-2.4033	39.362E-6	
	10.00000	-2.00000	29.43000	-0.38508	29.215	-0.0017373	-1.3437	22.073E-6	
	12.00000	-2.00000	29.43000	-0.13960	29.215	-532.66E-6	-0.75393	12.407E-6	
	14.00000	-2.00000	29.43000	0.0024695	29.215	-201.04E-6	-0.45696	7.5258E-6	
	16.00000	-2.00000	29.43000	0.077128	29.215	-89.662E-6	-0.29596	4.8763E-6	
	18.00000	-2.00000	29.43000	0.11182	29.215	-44.960E-6	-0.20173	3.3245E-6	
	20.00000	-2.00000	29.43000	0.12389	29.215	-24.548E-6	-0.14313	2.3592E-6	
	22.00000	-2.00000	29.43000	0.12373	29.215	-14.302E-6	-0.10491	1.7294E-6	
	24.00000	-2.00000	29.43000	0.11738	29.215	-8.7739E-6	-0.078998	1.3023E-6	
	26.00000	-2.00000	29.43000	0.10828	29.215	-5.6150E-6	-0.060859	1.0034E-6	
	28.00000	-2.00000	29.43000	0.098318	29.215	-3.7230E-6	-0.047811	0.0	
	30.00000	-2.00000	29.43000	0.088478	29.215	-2.5442E-6	-0.038202	0.0	
	-20.00000	0.00000	29.43000	0.10120	29.215	-4.1657E-6	-0.051109	0.0	
	-18.00000	0.00000	29.43000	0.11131	29.215	-6.4071E-6	-0.065815	1.0851E-6	
	-16.00000	0.00000	29.43000	0.12008	29.215	-10.266E-6	-0.086705	1.4294E-6	
	-14.00000	0.00000	29.43000	0.12499	29.215	-17.293E-6	-0.11739	1.9350E-6	
	-12.00000	0.00000	29.43000	0.12123	29.215	-31.026E-6	-0.16435	2.7087E-6	
	-10.00000	0.00000	29.43000	0.099851	29.215	-60.480E-6	-0.24007	3.9560E-6	
	-8.00000	0.00000	29.43000	0.044063	29.215	-132.46E-6	-0.37103	6.1122E-6	
	-6.00000	0.00000	29.43000	-0.078390	29.215	-347.67E-6	-0.62207	10.242E-6	
	-4.00000	0.00000	29.43000	-0.33407	29.215	-0.0012708	-1.1947	19.638E-6	
	-2.00000	0.00000	29.43000	-0.88963	29.215	-0.010590	-3.1172	50.882E-6	
	0.00000	0.00000	29.43000	-2.7491	29.215	-20.662	-60.581	-23.180E-6	
	2.00000	0.00000	29.43000	-4.4851	29.215	-41.300	-117.34	-108.12E-6	
	4.00000	0.00000	29.43000	-4.0463	29.215	-13.462	-71.145	507.23E-6	
	6.00000	0.00000	29.43000	-3.0660	29.215	-0.91259	-25.565	376.45E-6	
	8.00000	0.00000	29.43000	-1.9650	29.215	-0.52154	-14.723	217.00E-6	
	10.00000	0.00000	29.43000	-0.81808	29.215	-0.0083765	-2.7884	45.570E-6	
	12.00000	0.00000	29.43000	-0.31234	29.215	-0.0011580	-1.1419	18.773E-6	
	14.00000	0.00000	29.43000	-0.070214	29.215	-330.42E-6	-0.60682	9.9908E-6	
	16.00000	0.00000	29.43000	0.047373	29.215	-128.32E-6	-0.36530	6.0178E-6	
	18.00000	0.00000	29.43000	0.10120	29.215	-59.193E-6	-0.23753	3.9143E-6	
	20.00000	0.00000	29.43000	0.12174	29.215	-30.553E-6	-0.16310	2.6882E-6	
	22.00000	0.00000	29.43000	0.12514	29.215	-17.096E-6	-0.11672	1.9240E-6	
	24.00000	0.00000	29.43000	0.12008	29.215	-10.175E-6	-0.086320	1.4230E-6	
	26.00000	0.00000	29.43000	0.11125	29.215	-6.3622E-6	-0.065581	1.0812E-6	
	28.00000	0.00000	29.43000	0.10112	29.215	-4.1419E-6	-0.050960	0.0	
	30.00000	0.00000	29.43000	0.090956	29.215	-2.7894E-6	-0.040363	0.0	
	-20.00000	2.00000	29.43000	0.10319	29.215	-4.4884E-6	-0.053470	0.0	
	-18.00000	2.00000	29.43000	0.11339	29.215	-6.9927E-6	-0.069402	1.1442E-6	
	-16.00000	2.00000	29.43000	0.12188	29.215	-11.388E-6	-0.092357	1.5225E-6	
	-14.00000	2.00000	29.43000	0.12562	29.215	-19.588E-6	-0.12669	2.0883E-6	
	-12.00000	2.00000	29.43000	0.11870	29.215	-36.114E-6	-0.18047	2.9744E-6	
	-10.00000	2.00000	29.43000	0.089750	29.215	-72.996E-6	-0.26990	4.4474E-6	
	-8.00000	2.00000	29.43000	0.016506	29.215	-167.95E-6	-0.43111	7.1013E-6	
	-6.00000	2.00000	29.43000	-0.14632	29.215	-472.45E-6	-0.75832	12.482E-6	
	-4.00000	2.00000	29.43000	-0.50020	29.215	-0.0019158	-1.5701	25.799E-6	
	-2.00000	2.00000	29.43000	-1.3318	29.215	-0.018776	-4.6955	76.506E-6	
	0.00000	2.00000	29.43000	-4.6365	29.215	-41.314	-118.13	-95.881E-6	
	2.00000	2.00000	29.43000	-7.8221	29.215	-82.608	-231.23	-273.65E-6	
	4.00000	2.00000	29.43000	-8.2274	29.215	-82.615	-232.86	-247.05E-6	
	6.00000	2.00000	29.43000	-7.6479	29.215	-82.582	-229.56	-299.96E-6	
	8.00000	2.00000	29.43000	-4.8896	29.215	-59.266	-144.75	-544.95E-6	
	10.00000	2.00000	29.43000	-1.3073	29.215	-0.020028	-4.6946	76.428E-6	
	12.00000	2.00000	29.43000	-0.48960	29.215	-0.0019090	-1.5513	25.489E-6	
	14.00000	2.00000	29.43000	-0.14202	29.215	-467.38E-6	-0.75114	12.364E-6	
	16.00000	2.00000	29.43000	0.018254	29.215	-166.31E-6	-0.42814	7.0522E-6	
	18.00000	2.00000	29.43000	0.090438	29.215	-72.424E-6	-0.26852	4.4247E-6	
	20.00000	2.00000	29.43000	0.11894	29.215	-35.889E-6	-0.17977	2.9628E-6	
	22.00000	2.00000	29.43000	0.12566	29.215	-19.489E-6	-0.12630	2.0818E-6	
	24.00000	2.00000	29.43000	0.12185	29.215	-11.341E-6	-0.092126	1.5187E-6	
	26.00000	2.00000	29.43000	0.11333	29.215	-6.9685E-6	-0.069258	1.1418E-6	
	28.00000	2.00000	29.43000	0.10313	29.215	-4.4752E-6	-0.053375	0.0	
	30.00000	2.00000	29.43000	0.092746	29.215	-2.9813E-6	-0.042001	0.0	
	-20.00000	4.00000	29.43000	0.10435	29.215	-4.6852E-6	-0.054883	0.0	
	-18.00000	4.00000	29.43000	0.11458	29.215	-7.3537E-6	-0.071568	1.1799E-6	
	-16.00000	4.00000	29.43000	0.12286	29.215	-12.089E-6	-0.095804	1.5793E-6	
	-14.00000	4.00000	29.43000	0.12582	29.215	-21.043E-6	-0.13243	2.1829E-6	
	-12.00000	4.00000	29.43000	0.11682	29.215	-39.391E-6	-0.19058	3.1409E-6	
	-10.00000	4.00000	29.43000	0.082862	29.215	-81.156E-6	-0.28891	4.7604E-6	
	-8.00000	4.00000	29.43000	-0.0019188	29.215	-191.00E-6	-0.46986	7.7391E-6	
	-6.00000	4.00000	29.43000	-0.19111	29.215	-549.23E-6	-0.84565	13.919E-6	
	-4.00000	4.00000	29.43000	-0.60550	29.215	-0.0022346	-1.7928	29.454E-6	
	-2.00000	4.00000	29.43000	-1.5742	29.215	-0.020528	-5.3443	87.118E-6	
	0.00000	4.00000	29.43000	-5.1387	29.215	-41.323	-119.96	-66.118E-6	

Name	Location			Displacement		Stresses		
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	2.00000	4.00000	29.43000	-8.5890	29.215	-82.625	-234.34	-223.24E-6
	4.00000	4.00000	29.43000	-9.1522	29.215	-82.642	-236.93	-181.25E-6
	6.00000	4.00000	29.43000	-8.5904	29.215	-82.627	-234.43	-221.74E-6
	8.00000	4.00000	29.43000	-5.5396	29.215	-59.293	-147.85	-495.15E-6
	10.00000	4.00000	29.43000	-1.5985	29.215	-0.023056	-5.5672	90.669E-6
	12.00000	4.00000	29.43000	-0.61025	29.215	-0.0023339	-1.8159	29.831E-6
	14.00000	4.00000	29.43000	-0.19235	29.215	-559.87E-6	-0.84963	13.984E-6
	16.00000	4.00000	29.43000	-0.0023589	29.215	-192.80E-6	-0.47068	7.7525E-6
	18.00000	4.00000	29.43000	0.082649	29.215	-81.549E-6	-0.28906	4.7628E-6
	20.00000	4.00000	29.43000	0.11668	29.215	-39.491E-6	-0.19057	3.1408E-6
	22.00000	4.00000	29.43000	0.12572	29.215	-21.070E-6	-0.13239	2.1822E-6
	24.00000	4.00000	29.43000	0.12278	29.215	-12.095E-6	-0.095759	1.5786E-6
	26.00000	4.00000	29.43000	0.11452	29.215	-7.3544E-6	-0.071529	1.1792E-6
	28.00000	4.00000	29.43000	0.10429	29.215	-4.6843E-6	-0.054852	0.0
	30.00000	4.00000	29.43000	0.093791	29.215	-3.1003E-6	-0.042994	0.0
	-20.00000	6.00000	29.43000	0.10463	29.215	-4.7319E-6	-0.055221	0.0
	-18.00000	6.00000	29.43000	0.11487	29.215	-7.4394E-6	-0.072085	1.1884E-6
	-16.00000	6.00000	29.43000	0.12311	29.215	-12.255E-6	-0.096629	1.5929E-6
	-14.00000	6.00000	29.43000	0.12588	29.215	-21.389E-6	-0.13381	2.2056E-6
	-12.00000	6.00000	29.43000	0.11638	29.215	-40.172E-6	-0.19300	3.1809E-6
	-10.00000	6.00000	29.43000	0.081233	29.215	-83.096E-6	-0.29347	4.8355E-6
	-8.00000	6.00000	29.43000	-0.0063023	29.215	-196.40E-6	-0.47912	7.8916E-6
	-6.00000	6.00000	29.43000	-0.20170	29.215	-566.23E-6	-0.86612	14.255E-6
	-4.00000	6.00000	29.43000	-0.62967	29.215	-0.0022941	-1.8415	30.255E-6
	-2.00000	6.00000	29.43000	-1.6255	29.215	-0.020736	-5.4615	89.040E-6
	0.00000	6.00000	29.43000	-5.2327	29.215	-41.324	-120.20	-62.141E-6
	2.00000	6.00000	29.43000	-8.7279	29.215	-82.626	-234.72	-216.99E-6
	4.00000	6.00000	29.43000	-9.3236	29.215	-82.643	-237.43	-173.16E-6
	6.00000	6.00000	29.43000	-8.7662	29.215	-82.629	-234.97	-213.03E-6
	8.00000	6.00000	29.43000	-5.6740	29.215	-59.294	-148.24	-488.76E-6
	10.00000	6.00000	29.43000	-1.6734	29.215	-0.023452	-5.7533	93.718E-6
	12.00000	6.00000	29.43000	-0.64516	29.215	-0.0024359	-1.8888	31.028E-6
	14.00000	6.00000	29.43000	-0.20754	29.215	-586.76E-6	-0.87863	14.461E-6
	16.00000	6.00000	29.43000	-0.0087025	29.215	-200.86E-6	-0.48325	7.9595E-6
	18.00000	6.00000	29.43000	0.080184	29.215	-84.325E-6	-0.29504	4.8614E-6
	20.00000	6.00000	29.43000	0.11590	29.215	-40.571E-6	-0.19366	3.1917E-6
	22.00000	6.00000	29.43000	0.12564	29.215	-21.535E-6	-0.13410	2.2105E-6
	24.00000	6.00000	29.43000	0.12299	29.215	-12.314E-6	-0.096768	1.5952E-6
	26.00000	6.00000	29.43000	0.11480	29.215	-7.4645E-6	-0.072152	1.1895E-6
	28.00000	6.00000	29.43000	0.10459	29.215	-4.7432E-6	-0.055253	0.0
	30.00000	6.00000	29.43000	0.094058	29.215	-3.1334E-6	-0.043261	0.0
	-20.00000	8.00000	29.43000	0.10403	29.215	-4.6225E-6	-0.054452	0.0
	-18.00000	8.00000	29.43000	0.11427	29.215	-7.2374E-6	-0.070900	1.1689E-6
	-16.00000	8.00000	29.43000	0.12263	29.215	-11.860E-6	-0.094729	1.5616E-6
	-14.00000	8.00000	29.43000	0.12587	29.215	-20.562E-6	-0.13062	2.1530E-6
	-12.00000	8.00000	29.43000	0.11760	29.215	-38.294E-6	-0.18734	3.0875E-6
	-10.00000	8.00000	29.43000	0.085357	29.215	-78.395E-6	-0.28272	4.6585E-6
	-8.00000	8.00000	29.43000	0.0044950	29.215	-183.17E-6	-0.45708	7.5287E-6
	-6.00000	8.00000	29.43000	-0.17582	29.215	-523.61E-6	-0.81668	13.442E-6
	-4.00000	8.00000	29.43000	-0.57034	29.215	-0.0021364	-1.7205	28.267E-6
	-2.00000	8.00000	29.43000	-1.4970	29.215	-0.020111	-5.1532	83.987E-6
	0.00000	8.00000	29.43000	-4.9915	29.215	-41.322	-119.51	-73.409E-6
	2.00000	8.00000	29.43000	-8.3752	29.215	-82.623	-233.61	-235.11E-6
	4.00000	8.00000	29.43000	-8.9279	29.215	-82.638	-236.13	-194.30E-6
	6.00000	8.00000	29.43000	-8.4265	29.215	-82.625	-233.91	-230.35E-6
	8.00000	8.00000	29.43000	-5.4457	29.215	-59.292	-147.59	-499.44E-6
	10.00000	8.00000	29.43000	-1.5533	29.215	-0.022850	-5.4622	88.947E-6
	12.00000	8.00000	29.43000	-0.59049	29.215	-0.0022866	-1.7761	29.177E-6
	14.00000	8.00000	29.43000	-0.18404	29.215	-547.31E-6	-0.83316	13.713E-6
	16.00000	8.00000	29.43000	941.33E-6	29.215	-188.81E-6	-0.46311	7.6278E-6
	18.00000	8.00000	29.43000	0.083775	29.215	-80.082E-6	-0.28523	4.6999E-6
	20.00000	8.00000	29.43000	0.11688	29.215	-38.882E-6	-0.18849	3.1064E-6
	22.00000	8.00000	29.43000	0.12555	29.215	-20.791E-6	-0.13118	2.1623E-6
	24.00000	8.00000	29.43000	0.12249	29.215	-11.958E-6	-0.095020	1.5664E-6
	26.00000	8.00000	29.43000	0.11420	29.215	-7.2820E-6	-0.071057	1.1715E-6
	28.00000	8.00000	29.43000	0.10400	29.215	-4.6441E-6	-0.054540	0.0
	30.00000	8.00000	29.43000	0.093537	29.215	-3.0769E-6	-0.042781	0.0
	-20.00000	10.00000	29.43000	0.10257	29.215	-4.3711E-6	-0.052649	0.0
	-18.00000	10.00000	29.43000	0.11276	29.215	-6.7771E-6	-0.068140	1.1234E-6
	-16.00000	10.00000	29.43000	0.12139	29.215	-10.969E-6	-0.090343	1.4893E-6
	-14.00000	10.00000	29.43000	0.12562	29.215	-18.718E-6	-0.12333	2.0329E-6
	-12.00000	10.00000	29.43000	0.11998	29.215	-34.155E-6	-0.17455	2.8768E-6
	-10.00000	10.00000	29.43000	0.094030	29.215	-68.101E-6	-0.25874	4.2636E-6
	-8.00000	10.00000	29.43000	0.027672	29.215	-153.90E-6	-0.40822	6.7245E-6
	-6.00000	10.00000	29.43000	-0.11926	29.215	-423.10E-6	-0.70561	11.615E-6
	-4.00000	10.00000	29.43000	-0.43487	29.215	-0.0016721	-1.4252	23.420E-6
	-2.00000	10.00000	29.43000	-1.1647	29.215	-0.016444	-4.1456	67.552E-6
	0.00000	10.00000	29.43000	-4.1889	29.215	-41.269	-115.10	-143.59E-6
	2.00000	10.00000	29.43000	-7.0699	29.215	-82.506	-225.12	-369.31E-6
	4.00000	10.00000	29.43000	-7.3193	29.215	-82.197	-221.58	-412.44E-6
	6.00000	10.00000	29.43000	-7.1502	29.215	-82.524	-225.95	-356.52E-6
	8.00000	10.00000	29.43000	-4.6424	29.215	-59.240	-143.20	-569.31E-6
	10.00000	10.00000	29.43000	-1.2168	29.215	-0.018949	-4.4243	72.024E-6
	12.00000	10.00000	29.43000	-0.45413	29.215	-0.0018005	-1.4755	24.244E-6
	14.00000	10.00000	29.43000	-0.12758	29.215	-444.15E-6	-0.72164	11.879E-6
	16.00000	10.00000	29.43000	0.023907	29.215	-159.28E-6	-0.41458	6.8290E-6
	18.00000	10.00000	29.43000	0.092303	29.215	-69.828E-6	-0.26159	4.3104E-6
	20.00000	10.00000	29.43000	0.11919	29.215	-34.797E-6	-0.17593	2.8996E-6
	22.00000	10.00000	29.43000	0.12527	29.215	-18.983E-6	-0.12404	2.0447E-6
	24.00000	10.00000	29.43000	0.12125	29.215	-11.087E-6	-0.090734	1.4958E-6
	26.00000	10.00000	29.43000	0.11271	29.215	-6.8334E-6	-0.068362	1.1270E-6
	28.00000	10.00000	29.43000	0.10255	29.215	-4.3994E-6	-0.052779	0.0
	30.00000	10.00000	29.43000	0.092247	29.215	-2.9368E-6	-0.041591	0.0
	-20.00000	12.00000	29.43000	0.10027	29.215	-4.0078E-6	-0.049971	0.0
	-18.00000	12.00000	29.43000	0.11036	29.215	-6.1217E-6	-0.064089	1.0566E-6
	-16.00000	12.00000	29.43000	0.11929	29.215	-9.7225E-6	-0.087993	1.3847E-6
	-14.00000	12.00000	29.43000	0.12477	29.215	-16.190E-6	-0.11295	1.8618E-6
	-12.00000	12.00000	29.43000	0.12253	29.215	-28.607E-6	-0.15669	2.5827E-6
	-10.00000	12.00000	29.43000	0.10472	29.215	-54.602E-6	-0.22604	3.7249E-6
	-8.00000	12.00000	29.43000	0.057010	29.215	-115.98E-6	-0.34309	5.6522E-6
	-6.00000	12.00000	29.43000	-0.046977	29.215	-289.78E-6	-0.55926	9.2084E-6
	-4.00000	12.00000	29.43000	-0.25778	29.215	-961.42E-6	-1.0205	16.781E-6
	-2.00000	12.00000	29.43000	-0.68154	29.215	-0.0059076	-2.3212	37.987E-6
	0.00000	12.00000	29.43000	-1.5283	29.215	-0.12899	-8.3925	132.02E-6
	2.00000	12.00000	29.43000	-2.2639	29.215	-0.24127	-13.722	214.36E-6
	4.00000	12.00000	29.43000	-2.3571	29.215	-0.10511	-11.308	181.28E-6
	6.00000	12.00000	29.43000	-2.3356	29.215	-0.28273	-14.774	229.66E-6
	8.00000	12.00000	29.43000	-1.6025	29.215	-0.16379	-9.3174	145.55E-6
	10.00000	12.00000	29.43000	-0.71343	29.215	-0.0067196	-2.4517	40.098E-6
	12.00000	12.00000	29.43000	-0.27197	29.215	-0.0010322	-1.0539	17.329E-6
	14.00000	12.00000	29.43000	-0.053711	29.215	-304.02E-6	-0.57170	9.4130E-6
	16.00000	12.00000	29.43000	0.053766	29.215	-120.11E-6	-0.34858	5.7425E-6
	18.00000	12.00000	29.43000	0.10317	29.215	-56.061E-6	-0.22870	3.7688E-6
	20.00000	12.00000	29.43000	0.12181	29.215	-29.192E-6	-0.15808	2.6055E-6
	22.00000	12.00000	29.43000	0.12446	29.215	-16.447E-6	-0.11371	1.8743E-6
	24.00000	12.00000	29.43000	0.11917	29.215	-9.8431E-6	-0.084426	1.3918E-6
	26.00000	12.00000	29.43000	0.11033	29.215	-6.1817E-6	-0.064345	1.0608E-6
	28.00000	12.00000	29.43000	0.10028	29.215	-4.0391E-6	-0.050127	0.0
	30.00000	12.00000	29.43000	0.090227	29.215	-2.7284E-6	-0.039786	0.0
	-20.00000	14.00000	29.43000	0.097210	29.215	-3.5724E-6	-0.046638	0.0
	-18.00000	14.00000	29.43000	0.10708	29.215	-5.3523E-6	-0.059125	0.0
	-16.00000	14.00000	29.43000	0.11622	29.215	-8.2955E-6	-0.076358	1.2588E-6
	-14.00000	14.00000	29.43000	0.12292	29.215	-13.385E-6	-0.10076	1.6609E-6
	-12.00000	14.00000	29.43000	0.12410	29.215	-22.678E-6	-0.13635	2.2474E-6
	-10.00000	14.00000	29.43000	0.11444	29.215	-40.841E-6	-0.19013	3.1334E-6
	-8.00000	14.00000	29.43000	0.085011	29.215	-79.598E-6	-0.27496	4.5305E-6
	-6.00000	14.00000	29.43000	0.021412	29.215	-172.57E-6	-0.41606	6.8528E-6
	-4.00000	14.00000	29.43000	-0.097718	29.215	-432.49E-6	-0.66581	10.959E-6
	-2.00000	14.00000	29.43000	-0.29630	29.215	-0.0012723	-1.1281	18.541E-6
	0.00000	14.00000	29.43000	-0.56439	29.215	-0.0034840	-1.8731	30.717E-6
	2.00000	14.00000	29.43000	-0.79023	29.215	-0.0053105	-2.5000	40.965E-6
	4.00000	14.00000	29.43000	-0.87290	29.215	-0.0054441	-2.6824	43.966E-6
	6.00000	14.00000	29.43000	-0.80628	29.215	-0.0056336	-2.5639	42.003E-6
	8.00000	14.00000	29.43000	-0.58423	29.215	-0.0037649	-1.9406	31.816E-6
	10.00000	14.00000	29.43000	-0.31076	29.215	-0.0013704	-1.1657	19.156E-6
	12.00000	14.00000	29.43000	-0.10616	29.215	-457.59E-6	-0.68290	11.239E-6
	14.00000	14.00000	29.43000	0.016831	29.215	-180.06E-6	-0.42417	6.9861E-6
	16.00000	14.00000	29.43000	0.082626	29.215	-82.247E-6	-0.27907	4.5982E-6
	18.00000	14.00000	29.43000	0.11325	29.215	-41.904E-6	-0.19233	3.1696E-6
	20.00000	14.00000	29.43000	0.12354	29.215	-23.146E-6	-0.13758	2.2677E-6
	22.00000	14.00000	29.43000	0.12268	29.215	-13.605E-6	-0.10147	1.6727E-6

Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	24.00000	14.00000	29.43000	0.11615	29.215	-8.4052E-6	-0.076786	1.2659E-6
	26.00000	14.00000	29.43000	0.10708	29.215	-5.4095E-6	-0.059388	0.0
	28.00000	14.00000	29.43000	0.097238	29.215	-3.6034E-6	-0.046805	0.0
	30.00000	14.00000	29.43000	0.087545	29.215	-2.4720E-6	-0.037496	0.0
	-20.00000	16.00000	29.43000	0.093469	29.215	-3.1060E-6	-0.042892	0.0
	-18.00000	16.00000	29.43000	0.10300	29.215	-4.5496E-6	-0.053650	0.0
	-16.00000	16.00000	29.43000	0.11217	29.215	-6.8539E-6	-0.068135	1.1233E-6
	-14.00000	16.00000	29.43000	0.11979	29.215	-10.664E-6	-0.088011	1.4509E-6
	-12.00000	16.00000	29.43000	0.12381	29.215	-17.220E-6	-0.11585	1.9097E-6
	-10.00000	16.00000	29.43000	0.12091	29.215	-29.038E-6	-0.15572	2.5665E-6
	-8.00000	16.00000	29.43000	0.10610	29.215	-51.474E-6	-0.21406	3.5276E-6
	-6.00000	16.00000	29.43000	0.072556	29.215	-96.371E-6	-0.30100	4.9590E-6
	-4.00000	16.00000	29.43000	0.012950	29.215	-189.26E-6	-0.43066	7.0927E-6
	-2.00000	16.00000	29.43000	-0.075302	29.215	-372.09E-6	-0.61447	10.115E-6
	0.00000	16.00000	29.43000	-0.17889	29.215	-648.22E-6	-0.83299	13.705E-6
	2.00000	16.00000	29.43000	-0.26385	29.215	-883.30E-6	-1.0111	16.631E-6
	4.00000	16.00000	29.43000	-0.29774	29.215	-968.24E-6	-1.0804	17.769E-6
	6.00000	16.00000	29.43000	-0.26893	29.215	-908.27E-6	-1.0233	16.830E-6
	8.00000	16.00000	29.43000	-0.18609	29.215	-676.45E-6	-0.84892	13.966E-6
	10.00000	16.00000	29.43000	-0.081693	29.215	-389.55E-6	-0.62720	10.324E-6
	12.00000	16.00000	29.43000	0.0084792	29.215	-197.27E-6	-0.43877	7.2260E-6
	14.00000	16.00000	29.43000	0.069816	29.215	-99.792E-6	-0.30579	5.0378E-6
	16.00000	16.00000	29.43000	0.10456	29.215	-52.977E-6	-0.21687	3.5738E-6
	18.00000	16.00000	29.43000	0.12011	29.215	-29.734E-6	-0.15738	2.5939E-6
	20.00000	16.00000	29.43000	0.12343	29.215	-17.559E-6	-0.11686	1.9262E-6
	22.00000	16.00000	29.43000	0.11965	29.215	-10.836E-6	-0.088631	1.4611E-6
	24.00000	16.00000	29.43000	0.11215	29.215	-6.9453E-6	-0.068525	1.1297E-6
	26.00000	16.00000	29.43000	0.10303	29.215	-4.5997E-6	-0.053901	0.0
	28.00000	16.00000	29.43000	0.093516	29.215	-3.1344E-6	-0.043056	0.0
	30.00000	16.00000	29.43000	0.084286	29.215	-2.1901E-6	-0.034872	0.0
	-20.00000	18.00000	29.43000	0.089166	29.215	-2.6442E-6	-0.038962	0.0
	-18.00000	18.00000	29.43000	0.098222	29.215	-3.7785E-6	-0.048030	0.0
	-16.00000	18.00000	29.43000	0.10721	29.215	-5.5205E-6	-0.059916	0.0
	-14.00000	18.00000	29.43000	0.11532	29.215	-8.2632E-6	-0.075690	1.2478E-6
	-12.00000	18.00000	29.43000	0.12127	29.215	-12.696E-6	-0.096869	1.5969E-6
	-10.00000	18.00000	29.43000	0.12314	29.215	-20.045E-6	-0.12558	2.0700E-6
	-8.00000	18.00000	29.43000	0.11828	29.215	-32.493E-6	-0.16467	2.7136E-6
	-6.00000	18.00000	29.43000	0.10372	29.215	-53.734E-6	-0.21750	3.5842E-6
	-4.00000	18.00000	29.43000	0.077210	29.215	-89.010E-6	-0.28674	4.7242E-6
	-2.00000	18.00000	29.43000	0.039692	29.215	-142.04E-6	-0.37060	6.1046E-6
	0.00000	18.00000	29.43000	-0.0019407	29.215	-206.02E-6	-0.45719	7.5294E-6
	2.00000	18.00000	29.43000	-0.035331	29.215	-259.02E-6	-0.52411	8.6304E-6
	4.00000	18.00000	29.43000	-0.048725	29.215	-280.40E-6	-0.55039	9.0628E-6
	6.00000	18.00000	29.43000	-0.037200	29.215	-263.03E-6	-0.52763	8.6882E-6
	8.00000	18.00000	29.43000	-0.0048086	29.215	-211.40E-6	-0.46245	7.6159E-6
	10.00000	18.00000	29.43000	0.036850	29.215	-146.42E-6	-0.37566	6.1879E-6
	12.00000	18.00000	29.43000	0.074987	29.215	-91.742E-6	-0.29066	4.7888E-6
	14.00000	18.00000	29.43000	0.10223	29.215	-55.243E-6	-0.22024	3.6293E-6
	16.00000	18.00000	29.43000	0.11740	29.215	-33.294E-6	-0.16648	2.7439E-6
	18.00000	18.00000	29.43000	0.12267	29.215	-20.470E-6	-0.12677	2.0895E-6
	20.00000	18.00000	29.43000	0.12106	29.215	-12.925E-6	-0.097642	1.6096E-6
	22.00000	18.00000	29.43000	0.11526	29.215	-8.3897E-6	-0.076197	1.2562E-6
	24.00000	18.00000	29.43000	0.10722	29.215	-5.5920E-6	-0.060252	0.0
	26.00000	18.00000	29.43000	0.098272	29.215	-3.8199E-6	-0.048255	0.0
	28.00000	18.00000	29.43000	0.089227	29.215	-2.6687E-6	-0.039114	0.0
	30.00000	18.00000	29.43000	0.080555	29.215	-1.9030E-6	-0.032063	0.0
	-20.00000	20.00000	29.43000	0.084436	29.215	-2.2129E-6	-0.035041	0.0
	-18.00000	20.00000	29.43000	0.092896	29.215	-3.0821E-6	-0.042553	0.0
	-16.00000	20.00000	29.43000	0.10147	29.215	-4.3643E-6	-0.052131	0.0
	-14.00000	20.00000	29.43000	0.10965	29.215	-6.2854E-6	-0.064420	1.0621E-6
	-12.00000	20.00000	29.43000	0.11663	29.215	-9.2032E-6	-0.080250	1.3230E-6
	-10.00000	20.00000	29.43000	0.12133	29.215	-13.674E-6	-0.10063	1.6588E-6
	-8.00000	20.00000	29.43000	0.12238	29.215	-20.522E-6	-0.12664	2.0875E-6
	-6.00000	20.00000	29.43000	0.11848	29.215	-30.808E-6	-0.15912	2.6225E-6
	-4.00000	20.00000	29.43000	0.10895	29.215	-45.471E-6	-0.19783	3.2603E-6
	-2.00000	20.00000	29.43000	0.094677	29.215	-64.261E-6	-0.24025	3.9589E-6
	0.00000	20.00000	29.43000	0.078790	29.215	-84.280E-6	-0.28046	4.6209E-6
	2.00000	20.00000	29.43000	0.066077	29.215	-100.06E-6	-0.31001	5.1075E-6
	4.00000	20.00000	29.43000	0.060965	29.215	-106.37E-6	-0.32135	5.2941E-6
	6.00000	20.00000	29.43000	0.065340	29.215	-101.01E-6	-0.31131	5.1288E-6
	8.00000	20.00000	29.43000	0.077606	29.215	-85.704E-6	-0.28256	4.6554E-6
	10.00000	20.00000	29.43000	0.093825	29.215	-65.621E-6	-0.24252	3.9962E-6
	12.00000	20.00000	29.43000	0.10790	29.215	-46.498E-6	-0.19983	3.2931E-6
	14.00000	20.00000	29.43000	0.11774	29.215	-31.486E-6	-0.16068	2.6483E-6
	16.00000	20.00000	29.43000	0.12193	29.215	-20.940E-6	-0.12780	2.1065E-6
	18.00000	20.00000	29.43000	0.12110	29.215	-13.925E-6	-0.10145	1.6723E-6
	20.00000	20.00000	29.43000	0.11655	29.215	-9.3518E-6	-0.080823	1.3324E-6
	22.00000	20.00000	29.43000	0.10965	29.215	-6.3740E-6	-0.064818	1.0686E-6
	24.00000	20.00000	29.43000	0.10152	29.215	-4.4176E-6	-0.052407	0.0
	26.00000	20.00000	29.43000	0.092963	29.215	-3.1146E-6	-0.042746	0.0
	28.00000	20.00000	29.43000	0.084508	29.215	-2.2330E-6	-0.035177	0.0
	30.00000	20.00000	29.43000	0.076468	29.215	-1.6269E-6	-0.029201	0.0
	-20.00000	22.00000	29.43000	0.079423	29.215	-1.9278E-6	-0.031274	0.0
	-18.00000	22.00000	29.43000	0.087199	29.215	-2.4812E-6	-0.037416	0.0
	-16.00000	22.00000	29.43000	0.095190	29.215	-3.4076E-6	-0.045036	0.0
	-14.00000	22.00000	29.43000	0.10306	29.215	-4.7305E-6	-0.054500	0.0
	-12.00000	22.00000	29.43000	0.11034	29.215	-6.6263E-6	-0.066227	1.0918E-6
	-10.00000	22.00000	29.43000	0.11637	29.215	-9.3337E-6	-0.080638	1.3294E-6
	-8.00000	22.00000	29.43000	0.12045	29.215	-13.143E-6	-0.098049	1.6163E-6
	-6.00000	22.00000	29.43000	0.12194	29.215	-18.326E-6	-0.11845	1.9524E-6
	-4.00000	22.00000	29.43000	0.12058	29.215	-24.956E-6	-0.14113	2.3261E-6
	-2.00000	22.00000	29.43000	0.11680	29.215	-32.607E-6	-0.16431	2.7081E-6
	0.00000	22.00000	29.43000	0.11192	29.215	-40.110E-6	-0.18503	3.0494E-6
	2.00000	22.00000	29.43000	0.10778	29.215	-45.747E-6	-0.19966	3.2904E-6
	4.00000	22.00000	29.43000	0.10607	29.215	-47.945E-6	-0.20514	3.3806E-6
	6.00000	22.00000	29.43000	0.10749	29.215	-46.036E-6	-0.20022	3.2996E-6
	8.00000	22.00000	29.43000	0.11143	29.215	-40.574E-6	-0.18598	3.0651E-6
	10.00000	22.00000	29.43000	0.11627	29.215	-33.100E-6	-0.16542	2.7264E-6
	12.00000	22.00000	29.43000	0.12012	29.215	-25.379E-6	-0.14219	2.3437E-6
	14.00000	22.00000	29.43000	0.12162	29.215	-18.643E-6	-0.11936	1.9675E-6
	16.00000	22.00000	29.43000	0.12026	29.215	-13.362E-6	-0.098781	1.6283E-6
	18.00000	22.00000	29.43000	0.11629	29.215	-9.4790E-6	-0.081196	1.3386E-6
	20.00000	22.00000	29.43000	0.11034	29.215	-6.7203E-6	-0.066642	1.0987E-6
	22.00000	22.00000	29.43000	0.10311	29.215	-4.7907E-6	-0.054804	0.0
	24.00000	22.00000	29.43000	0.095260	29.215	-3.4460E-6	-0.045257	0.0
	26.00000	22.00000	29.43000	0.087277	29.215	-2.5059E-6	-0.037576	0.0
	28.00000	22.00000	29.43000	0.079501	29.215	-1.8437E-6	-0.031391	0.0
	30.00000	22.00000	29.43000	0.072141	29.215	-1.3728E-6	-0.026392	0.0
	-20.00000	24.00000	29.43000	0.074268	29.215	-1.4953E-6	-0.027756	0.0
	-18.00000	24.00000	29.43000	0.081311	29.215	-1.9800E-6	-0.032732	0.0
	-16.00000	24.00000	29.43000	0.088602	29.215	-2.6415E-6	-0.038746	0.0
	-14.00000	24.00000	29.43000	0.095924	29.215	-3.5448E-6	-0.045992	0.0
	-12.00000	24.00000	29.43000	0.10297	29.215	-4.7730E-6	-0.054657	0.0
	-10.00000	24.00000	29.43000	0.10935	29.215	-6.4227E-6	-0.064882	1.0697E-6
	-8.00000	24.00000	29.43000	0.11465	29.215	-8.5872E-6	-0.076680	1.2641E-6
	-6.00000	24.00000	29.43000	0.11851	29.215	-11.314E-6	-0.089818	1.4806E-6
	-4.00000	24.00000	29.43000	0.12074	29.215	-14.536E-6	-0.10368	1.7090E-6
	-2.00000	24.00000	29.43000	0.12149	29.215	-17.987E-6	-0.11715	1.9310E-6
	0.00000	24.00000	29.43000	0.12122	29.215	-21.175E-6	-0.12868	2.1211E-6
	2.00000	24.00000	29.43000	0.12062	29.215	-23.476E-6	-0.13658	2.2512E-6
	4.00000	24.00000	29.43000	0.12029	29.215	-24.353E-6	-0.13948	2.2990E-6
	6.00000	24.00000	29.43000	0.12051	29.215	-23.580E-6	-0.13685	2.2557E-6
	8.00000	24.00000	29.43000	0.12104	29.215	-21.351E-6	-0.12916	2.1289E-6
	10.00000	24.00000	29.43000	0.12129	29.215	-18.188E-6	-0.11773	1.9407E-6
	12.00000	24.00000	29.43000	0.12057	29.215	-14.724E-6	-0.10428	1.7189E-6
	14.00000	24.00000	29.43000	0.11839	29.215	-11.469E-6	-0.090367	1.4897E-6
	16.00000	24.00000	29.43000	0.11460	29.215	-8.7046E-6	-0.077147	1.2718E-6
	18.00000	24.00000	29.43000	0.10936	29.215	-6.5072E-6	-0.065261	1.0759E-6
	20.00000	24.00000	29.43000	0.10302	29.215	-4.8318E-6	-0.054955	0.0
	22.00000	24.00000	29.43000	0.095995	29.215	-3.5850E-6	-0.046220	0.0
	24.00000	24.00000	29.43000	0.088684	29.215	-2.6687E-6	-0.038919	0.0
	26.00000	24.00000	29.43000	0.081394	29.215	-1.9983E-6	-0.032863	0.0
	28.00000	24.00000	29.43000	0.074348	29.215	-1.5076E-6	-0.027855	0.0
	30.00000	24.00000	29.43000	0.067690	29.215	-1.1469E-6	-0.023715	0.0
	-20.00000	26.00000	29.43000	0.069099	29.215	-1.2154E-6	-0.024542	0.0
	-18.00000	26.00000	29.43000	0.075396	29.215	-1.5721E-6	-0.028550	0.0
	-16.00000	26.00000	29.43000	0.081934	29.215	-2.0417E-6	-0.033276	0.0
	-14.00000	26.00000	29.43000	0.088561	29.215	-2.6572E-6	-0.038814	0.0
	-12.00000	26.00000	29.43000	0.095070	29.215	-3.4559E-6	-0.045232	0.0
	-10.00000	26.00000	29.43000	0.10121	29.215	-4.4742E-6	-0.052543	0.0
	-8.00000	26.00000	29.43000	0.10671	29.215	-5.7356E-6	-0.060661	1.0001E-6

Name	Location X [m]	Location Y [m]	Z[Level] [mOD]	Displacement Z [mm]	Calc Level [mOD]	Stresses Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	-6.00000	26.00000	29.43000	0.11132	29.215	-7.2315E-6	-0.069343	1.1432E-6
	-4.00000	26.00000	29.43000	0.11488	29.215	-8.8953E-6	-0.078136	1.2881E-6
	-2.00000	26.00000	29.43000	0.11736	29.215	-10.582E-6	-0.086364	1.4237E-6
	0.00000	26.00000	29.43000	0.11888	29.215	-12.071E-6	-0.093187	1.5362E-6
	2.00000	26.00000	29.43000	0.11966	29.215	-13.113E-6	-0.097751	1.6114E-6
	4.00000	26.00000	29.43000	0.11987	29.215	-13.502E-6	-0.099404	1.6386E-6
	6.00000	26.00000	29.43000	0.11962	29.215	-13.155E-6	-0.097893	1.6137E-6
	8.00000	26.00000	29.43000	0.11883	29.215	-12.146E-6	-0.093444	1.5404E-6
	10.00000	26.00000	29.43000	0.11730	29.215	-10.671E-6	-0.086691	1.4291E-6
	12.00000	26.00000	29.43000	0.11484	29.215	-8.9847E-6	-0.078487	1.2939E-6
	14.00000	26.00000	29.43000	0.11131	29.215	-7.3106E-6	-0.069681	1.1488E-6
	16.00000	26.00000	29.43000	0.10673	29.215	-5.8001E-6	-0.060965	1.0051E-6
	18.00000	26.00000	29.43000	0.10126	29.215	-4.5238E-6	-0.052802	0.0
	20.00000	26.00000	29.43000	0.095142	29.215	-3.4927E-6	-0.045444	0.0
	22.00000	26.00000	29.43000	0.088644	29.215	-2.6837E-6	-0.038984	0.0
	24.00000	26.00000	29.43000	0.082020	29.215	-2.0606E-6	-0.033411	0.0
	26.00000	26.00000	29.43000	0.075479	29.215	-1.5854E-6	-0.028655	0.0
	28.00000	26.00000	29.43000	0.069176	29.215	-1.2248E-6	-0.024624	0.0
	30.00000	26.00000	29.43000	0.063215	29.215	0.0	-0.021218	0.0
	-20.00000	28.00000	29.43000	0.064022	29.215	0.0	-0.021653	0.0
	-18.00000	28.00000	29.43000	0.069593	29.215	-1.2455E-6	-0.024871	0.0
	-16.00000	28.00000	29.43000	0.075375	29.215	-1.5784E-6	-0.028581	0.0
	-14.00000	28.00000	29.43000	0.081254	29.215	-1.9989E-6	-0.032820	0.0
	-12.00000	28.00000	29.43000	0.087082	29.215	-2.5228E-6	-0.037598	0.0
	-10.00000	28.00000	29.43000	0.092681	29.215	-3.1616E-6	-0.042880	0.0
	-8.00000	28.00000	29.43000	0.097856	29.215	-3.9164E-6	-0.048560	0.0
	-6.00000	28.00000	29.43000	0.10242	29.215	-4.7693E-6	-0.054439	0.0
	-4.00000	28.00000	29.43000	0.10622	29.215	-5.6745E-6	-0.060205	0.0
	-2.00000	28.00000	29.43000	0.10917	29.215	-6.5539E-6	-0.065446	1.0790E-6
	0.00000	28.00000	29.43000	0.11124	29.215	-7.3041E-6	-0.069686	1.1488E-6
	2.00000	28.00000	29.43000	0.11245	29.215	-7.8157E-6	-0.072471	1.1948E-6
	4.00000	28.00000	29.43000	0.11285	29.215	-8.0039E-6	-0.073469	1.2112E-6
	6.00000	28.00000	29.43000	0.11245	29.215	-7.8349E-6	-0.072551	1.1961E-6
	8.00000	28.00000	29.43000	0.11124	29.215	-7.3385E-6	-0.069833	1.1513E-6
	10.00000	28.00000	29.43000	0.10918	29.215	-6.5970E-6	-0.065638	1.0821E-6
	12.00000	28.00000	29.43000	0.10624	29.215	-5.7196E-6	-0.060419	0.0
	14.00000	28.00000	29.43000	0.10246	29.215	-4.8115E-6	-0.054653	0.0
	16.00000	28.00000	29.43000	0.097912	29.215	-3.9528E-6	-0.048760	0.0
	18.00000	28.00000	29.43000	0.092752	29.215	-3.1912E-6	-0.043058	0.0
	20.00000	28.00000	29.43000	0.087162	29.215	-2.5459E-6	-0.037750	0.0
	22.00000	28.00000	29.43000	0.081337	29.215	-2.0165E-6	-0.032946	0.0
	24.00000	28.00000	29.43000	0.075458	29.215	-1.5915E-6	-0.028684	0.0
	26.00000	28.00000	29.43000	0.069672	29.215	-1.2551E-6	-0.024954	0.0
	28.00000	28.00000	29.43000	0.064095	29.215	0.0	-0.021719	0.0
	30.00000	28.00000	29.43000	0.058804	29.215	0.0	-0.018930	0.0
	-20.00000	30.00000	29.43000	0.059120	29.215	0.0	-0.019085	0.0
	-18.00000	30.00000	29.43000	0.064008	29.215	0.0	-0.021667	0.0
	-16.00000	30.00000	29.43000	0.069065	29.215	-1.2234E-6	-0.024583	0.0
	-14.00000	30.00000	29.43000	0.074205	29.215	-1.5124E-6	-0.027840	0.0
	-12.00000	30.00000	29.43000	0.079315	29.215	-1.8599E-6	-0.031423	0.0
	-10.00000	30.00000	29.43000	0.084259	29.215	-2.2678E-6	-0.035283	0.0
	-8.00000	30.00000	29.43000	0.088889	29.215	-2.7314E-6	-0.039325	0.0
	-6.00000	30.00000	29.43000	0.093056	29.215	-3.2351E-6	-0.043398	0.0
	-4.00000	30.00000	29.43000	0.096624	29.215	-3.7501E-6	-0.047292	0.0
	-2.00000	30.00000	29.43000	0.099486	29.215	-4.2342E-6	-0.050750	0.0
	0.00000	30.00000	29.43000	0.10157	29.215	-4.6360E-6	-0.053496	0.0
	2.00000	30.00000	29.43000	0.10283	29.215	-4.9048E-6	-0.055274	0.0
	4.00000	30.00000	29.43000	0.10326	29.215	-5.0025E-6	-0.055905	0.0
	6.00000	30.00000	29.43000	0.10284	29.215	-4.9142E-6	-0.055321	0.0
	8.00000	30.00000	29.43000	0.10159	29.215	-4.6531E-6	-0.053584	0.0
	10.00000	30.00000	29.43000	0.099515	29.215	-4.2562E-6	-0.050868	0.0
	12.00000	30.00000	29.43000	0.096666	29.215	-3.7741E-6	-0.047427	0.0
	14.00000	30.00000	29.43000	0.093111	29.215	-3.2585E-6	-0.043537	0.0
	16.00000	30.00000	29.43000	0.088955	29.215	-2.7525E-6	-0.039460	0.0
	18.00000	30.00000	29.43000	0.084333	29.215	-2.2858E-6	-0.035407	0.0
	20.00000	30.00000	29.43000	0.079393	29.215	-1.8746E-6	-0.031532	0.0
	22.00000	30.00000	29.43000	0.074285	29.215	-1.5240E-6	-0.027934	0.0
	24.00000	30.00000	29.43000	0.069143	29.215	-1.2324E-6	-0.024662	0.0
	26.00000	30.00000	29.43000	0.064081	29.215	0.0	-0.021732	0.0
	28.00000	30.00000	29.43000	0.059187	29.215	0.0	-0.019139	0.0
	30.00000	30.00000	29.43000	0.054526	29.215	0.0	-0.016860	0.0
No. 8 Albert Terrace Mews	8.08000	6.15000	34.25000	-5.2054	34.031	0.0	0.0	0.0
	9.08000	6.15000	34.25000	-2.6567	34.031	0.0	0.0	0.0
	10.08000	6.15000	34.25000	-1.6162	34.031	0.0	0.0	0.0
	11.08000	6.15000	34.25000	-1.0077	34.031	0.0	0.0	0.0
	12.08000	6.15000	34.25000	-0.62170	34.031	0.0	0.0	0.0
	13.08000	6.15000	34.25000	-0.36755	34.031	0.0	0.0	0.0
	14.08000	6.15000	34.25000	-0.19708	34.031	0.0	0.0	0.0
	15.08000	6.15000	34.25000	-0.081869	34.031	0.0	0.0	0.0
	16.08000	6.15000	34.25000	-0.0040899	34.031	0.0	0.0	0.0
	17.08000	6.15000	34.25000	0.047922	34.031	0.0	0.0	0.0
	18.08000	6.15000	34.25000	0.082018	34.031	0.0	0.0	0.0


Settlement Contours : Grid 1 at 29.4300m
40.00
30.00
20.00
10.00
.0
-10.00
-20.00
Y [m]
-30.00
-10.00
10.00
30.00
X [m]
-9.000
-8.000
-7.000
-6.000
-5.000
-4.000
-3.000
-2.000
-1.000
0
Scale x 1:613 y 1:613
Contour Interval: 1mm


Displacement Lines
5.21
2.66
1.62
SZ1 : Soil Zone 1
L1 : Proposed Basement Excavation (including lowering of ground floor)
Z
X
Y

Analysis Options

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Maximum allowable ratio between values of E: 1.5
Horizontal rigid boundary level: -15.00 [m OD]
Stiffness for horizontal displacement calculations: Weighted average
Using legacy heave correction factor: No
Displacements at load centroids: Yes

Soil ProfilesSoil Profile 1

Layer	Level at top	Number of intermediate displacement levels	Youngs Modulus Top	Youngs Modulus Btm	Poissons ratio	Non-linear curve
	[mOD]		[kN/m²]	[kN/m²]		
1	35.000	5	7680.0	7680.0	0.20000	None
2	32.500	5	16000.	24800.	0.20000	None
3	29.000	5	24800.	33600.	0.20000	None
4	25.500	5	33600.	42400.	0.20000	None
5	22.000	5	42400.	51200.	0.20000	None
6	18.500	5	51200.	60000.	0.20000	None
7	15.000	10	60000.	2.5000E+6	0.20000	None

Soil Zones

Zone	Name	X coordinates min [m]	X coordinates max [m]	Y coordinates min [m]	Y coordinates max [m]	Profile
1	Soil Zone 1	-20.00000	30.00000	-20.00000	30.00000	Soil Profile 1

Load Data

Load ref.	Name	Shape	Orientation of Plane	Centre of load (Global) X [m]	Y [m]	Z (level) [m]	Load position Angle of local x from [Degrees]	Width x or Radius [m]	Length y [m]	Polygon Coordinates [m]	Rectangle tolerance [%]	Number of rectangles	Load value Normal (local z) [kN/m²]	Tangential (local x) [kN/m²]	(local y) [kN/m²]
1	Proposed Basement Excavation (including lowering of ground floor)	Polygonal	Horizontal	N/A	N/A	29.43000	N/A	N/A	N/A	(0,0) (3,0) (4.79,0.29) (8.08,0.8) (8.08,11.5) (4.79,10.9) (3,10.5) (0,11.8) (0,0)	10.000	3	-82.650	N/A	N/A

Polygonal Loads' Rectangles

No.	Centre of load X [m]	Centre of load Y [m]	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
Load 1 : Proposed Basement Excavation (including lowering of ground floor)					
(Edge 1 optimal)					
1	1.50000	5.57250	0.0	3.0000	11.145
2	3.89500	5.41250	0.0	1.7900	10.535
3	6.43500	5.86500	0.0	3.2900	10.640

Displacement Data

Ref.	Type	Name	Direction of Extrusion	Line/Line for extrusion First point X [m]	First point Y [m]	First point Z(level) [m]	Second point X [m]	Second point Y [m]	Second point Z(level) [m]	No. of intrvls across extrusion/line	Extrusion Depth [m]	No. of intrvls along extrusion	Calculate	Show Detailed results
1	Grid	Proposed Basement Level	Global X	-20.00000	-20.00000	29.43000	N/A	30.00000	29.43000	25	50.00000	25	Yes	Yes
2	Line	No. 8 Albert Terrace Mews	N/A	8.08000	6.15000	34.25000	18.08000	6.15000	34.25000	10	N/A	N/A	Yes	Yes

RESULTS FOR GRIDS

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Horizontal rigid boundary level: -15.00 [m OD]

The maximum displacement difference between the Boussinesq method (-10.441mm) and the Mindlin method (-6.0162mm) occurs at point X = 8.08000m, Y = 6.15000m, level = 34.250mOD, and is 4.4245mm.

Name	Location X [m]	Location Y [m]	Location Z[Level] [mOD]	Displacement Z [mm]	Stresses Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
Proposed Basement Excavation (including lowering of ground floor)	3.98649	5.65795	29.43000	-17.363	29.215	-82.643	-189.96	-0.0025223
Proposed Basement Level	-20.00000	-20.00000	29.43000	0.0050443	29.215	0.0	-0.014104	0.0
	-18.00000	-20.00000	29.43000	0.0039933	29.215	0.0	-0.015903	0.0
	-16.00000	-20.00000	29.43000	0.0025920	29.215	-1.0472E-6	-0.017910	0.0
	-14.00000	-20.00000	29.43000	801.97E-6	29.215	-1.2771E-6	-0.020123	0.0
	-12.00000	-20.00000	29.43000	-0.0013938	29.215	-1.5480E-6	-0.022522	0.0
	-10.00000	-20.00000	29.43000	-0.0039762	29.215	-1.8591E-6	-0.025068	0.0
	-8.00000	-20.00000	29.43000	-0.0068749	29.215	-2.2045E-6	-0.027691	0.0
	-6.00000	-20.00000	29.43000	-0.0099558	29.215	-2.5708E-6	-0.030290	0.0
	-4.00000	-20.00000	29.43000	-0.013018	29.215	-2.9362E-6	-0.032732	0.0
	-2.00000	-20.00000	29.43000	-0.015806	29.215	-3.2709E-6	-0.034863	0.0
	0.00000	-20.00000	29.43000	-0.018042	29.215	-3.5410E-6	-0.036523	0.0
	2.00000	-20.00000	29.43000	-0.019474	29.215	-3.7145E-6	-0.037569	0.0
	4.00000	-20.00000	29.43000	-0.019931	29.215	-3.7693E-6	-0.037907	0.0
	6.00000	-20.00000	29.43000	-0.019355	29.215	-3.6982E-6	-0.037506	0.0
	8.00000	-20.00000	29.43000	-0.017822	29.215	-3.5114E-6	-0.036405	0.0
	10.00000	-20.00000	29.43000	-0.015519	29.215	-3.2332E-6	-0.034707	0.0
	12.00000	-20.00000	29.43000	-0.012701	29.215	-2.8957E-6	-0.032556	0.0
	14.00000	-20.00000	29.43000	-0.0096409	29.215	-2.5320E-6	-0.030109	0.0
	16.00000	-20.00000	29.43000	-0.0065859	29.215	-2.1700E-6	-0.027518	0.0
	18.00000	-20.00000	29.43000	-0.0037263	29.215	-1.8303E-6	-0.024912	0.0
	20.00000	-20.00000	29.43000	-0.0011878	29.215	-1.5249E-6	-0.022386	0.0
	22.00000	-20.00000	29.43000	965.47E-6	29.215	-1.2592E-6	-0.020007	0.0
	24.00000	-20.00000	29.43000	0.0027179	29.215	-1.0335E-6	-0.017814	0.0
	26.00000	-20.00000	29.43000	0.0040878	29.215	0.0	-0.015824	0.0
	28.00000	-20.00000	29.43000	0.0051136	29.215	0.0	-0.014039	0.0
	30.00000	-20.00000	29.43000	0.0058431	29.215	0.0	-0.012453	0.0
	-20.00000	-18.00000	29.43000	0.0039485	29.215	0.0	-0.016007	0.0
	-18.00000	-18.00000	29.43000	0.0023610	29.215	-1.0793E-6	-0.018250	0.0
	-16.00000	-18.00000	29.43000	240.48E-6	29.215	-1.3489E-6	-0.020802	0.0
	-14.00000	-18.00000	29.43000	-0.0024913	29.215	-1.6824E-6	-0.023675	0.0
	-12.00000	-18.00000	29.43000	-0.0058863	29.215	-2.0883E-6	-0.026861	0.0
	-10.00000	-18.00000	29.43000	-0.0099444	29.215	-2.5711E-6	-0.030323	0.0
	-8.00000	-18.00000	29.43000	-0.014582	29.215	-3.1262E-6	-0.033976	0.0
	-6.00000	-18.00000	29.43000	-0.019605	29.215	-3.7358E-6	-0.037682	0.0
	-4.00000	-18.00000	29.43000	-0.024686	29.215	-4.3638E-6	-0.041244	0.0
	-2.00000	-18.00000	29.43000	-0.029386	29.215	-4.9555E-6	-0.044413	0.0
	0.00000	-18.00000	29.43000	-0.033204	29.215	-5.4433E-6	-0.046918	0.0
	2.00000	-18.00000	29.43000	-0.035671	29.215	-5.7609E-6	-0.048512	0.0
	4.00000	-18.00000	29.43000	-0.036456	29.215	-5.8604E-6	-0.049026	0.0
	6.00000	-18.00000	29.43000	-0.035455	29.215	-5.7269E-6	-0.048403	0.0
	8.00000	-18.00000	29.43000	-0.032813	29.215	-5.3830E-6	-0.046719	0.0

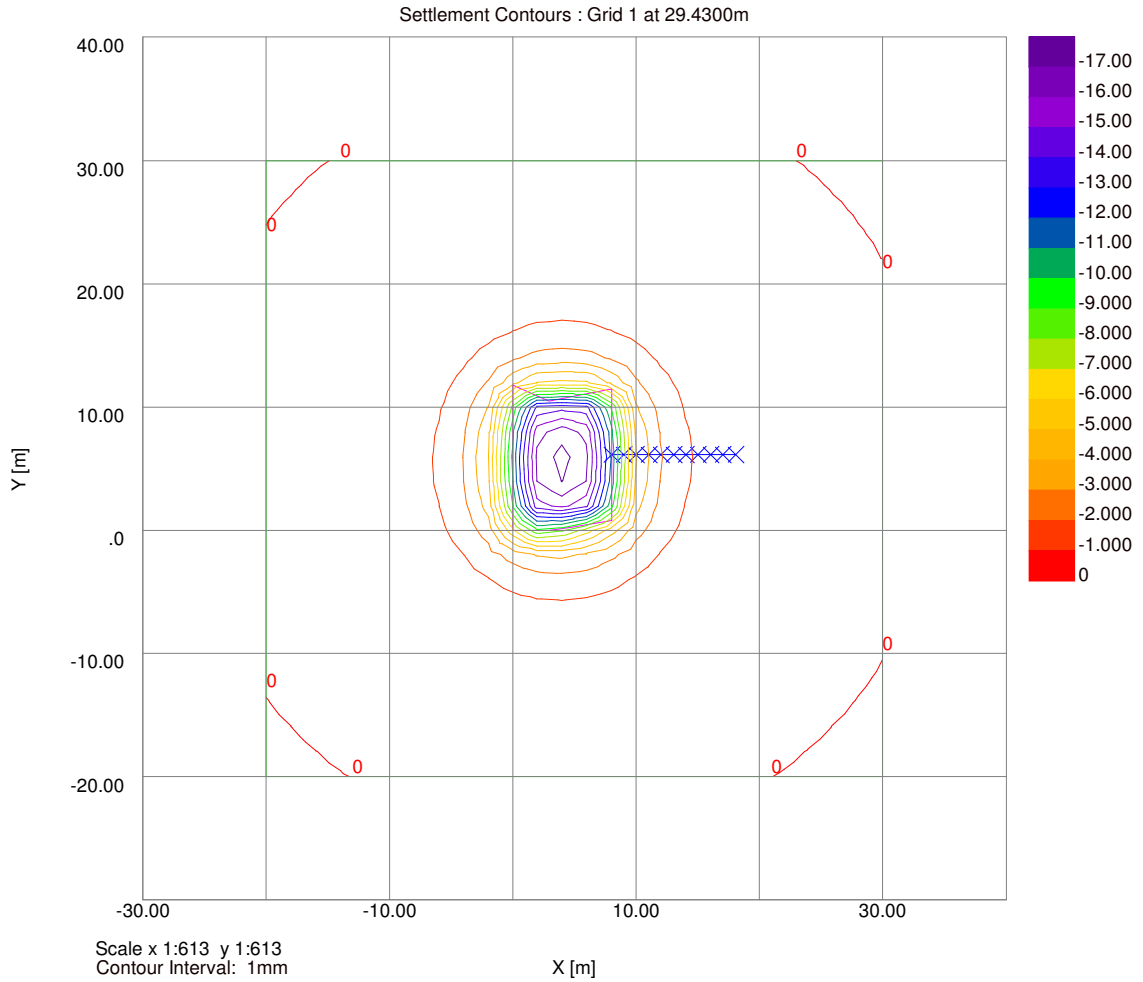
Name	Location			Displacement	Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	10.00000	-18.00000	29.43000	-0.028885	29.215	-4.8809E-6	-0.044155	0.0
	12.00000	-18.00000	29.43000	-0.024146	29.215	-4.2869E-6	-0.040961	0.0
	14.00000	-18.00000	29.43000	-0.019084	29.215	-3.6653E-6	-0.037403	0.0
	16.00000	-18.00000	29.43000	-0.014120	29.215	-3.0667E-6	-0.033719	0.0
	18.00000	-18.00000	29.43000	-0.0095576	29.215	-2.5237E-6	-0.030099	0.0
	20.00000	-18.00000	29.43000	-0.0055775	29.215	-2.0522E-6	-0.026673	0.0
	22.00000	-18.00000	29.43000	-0.0022535	29.215	-1.6555E-6	-0.023520	0.0
	24.00000	-18.00000	29.43000	418.45E-6	29.215	-1.3293E-6	-0.020677	0.0
	26.00000	-18.00000	29.43000	0.0024912	29.215	-1.0651E-6	-0.018150	0.0
	28.00000	-18.00000	29.43000	0.0040420	29.215	0.0	-0.015927	0.0
	30.00000	-18.00000	29.43000	0.0051560	29.215	0.0	-0.013986	0.0
	-20.00000	-16.00000	29.43000	0.0024567	29.215	-1.0683E-6	-0.018161	0.0
	-18.00000	-16.00000	29.43000	136.32E-6	29.215	-1.3633E-6	-0.020958	0.0
	-16.00000	-16.00000	29.43000	-0.0029911	29.215	-1.7439E-6	-0.024210	0.0
	-14.00000	-16.00000	29.43000	-0.0070787	29.215	-2.2312E-6	-0.027960	0.0
	-12.00000	-16.00000	29.43000	-0.012253	29.215	-2.8475E-6	-0.032227	0.0
	-10.00000	-16.00000	29.43000	-0.018572	29.215	-3.6106E-6	-0.036991	0.0
	-8.00000	-16.00000	29.43000	-0.025963	29.215	-4.5264E-6	-0.042166	0.0
	-6.00000	-16.00000	29.43000	-0.034160	29.215	-5.5759E-6	-0.047571	0.0
	-4.00000	-16.00000	29.43000	-0.042644	29.215	-6.7021E-6	-0.052911	0.0
	-2.00000	-16.00000	29.43000	-0.050654	29.215	-7.8017E-6	-0.057780	0.0
	0.00000	-16.00000	29.43000	-0.057267	29.215	-8.7339E-6	-0.061706	0.0
	2.00000	-16.00000	29.43000	-0.061583	29.215	-9.3506E-6	-0.064236	0.0
	4.00000	-16.00000	29.43000	-0.062956	29.215	-9.5419E-6	-0.065047	0.0
	6.00000	-16.00000	29.43000	-0.061181	29.215	-9.2742E-6	-0.064038	0.0
	8.00000	-16.00000	29.43000	-0.056550	29.215	-8.6018E-6	-0.061353	0.0
	10.00000	-16.00000	29.43000	-0.049760	29.215	-7.6449E-6	-0.057337	0.0
	12.00000	-16.00000	29.43000	-0.041711	29.215	-6.5486E-6	-0.052443	0.0
	14.00000	-16.00000	29.43000	-0.033293	29.215	-5.4432E-6	-0.047129	0.0
	16.00000	-16.00000	29.43000	-0.025223	29.215	-4.4210E-6	-0.041778	0.0
	18.00000	-16.00000	29.43000	-0.017976	29.215	-3.5316E-6	-0.036667	0.0
	20.00000	-16.00000	29.43000	-0.011795	29.215	-2.7904E-6	-0.031965	0.0
	22.00000	-16.00000	29.43000	-0.0067379	29.215	-2.1910E-6	-0.027753	0.0
	24.00000	-16.00000	29.43000	-0.0027440	29.215	-1.7159E-6	-0.024049	0.0
	26.00000	-16.00000	29.43000	312.04E-6	29.215	-1.3440E-6	-0.020834	0.0
	28.00000	-16.00000	29.43000	0.0025797	29.215	-1.0550E-6	-0.018065	0.0
	30.00000	-16.00000	29.43000	0.0042076	29.215	0.0	-0.015692	0.0
	-20.00000	-14.00000	29.43000	509.37E-6	29.215	-1.3184E-6	-0.020576	0.0
	-18.00000	-14.00000	29.43000	-0.0027910	29.215	-1.7211E-6	-0.024060	0.0
	-16.00000	-14.00000	29.43000	-0.0073028	29.215	-2.2586E-6	-0.028206	0.0
	-14.00000	-14.00000	29.43000	-0.013313	29.215	-2.9743E-6	-0.033113	0.0
	-12.00000	-14.00000	29.43000	-0.021100	29.215	-3.9195E-6	-0.038866	0.0
	-10.00000	-14.00000	29.43000	-0.030862	29.215	-5.1476E-6	-0.045500	0.0
	-8.00000	-14.00000	29.43000	-0.042612	29.215	-6.6995E-6	-0.052959	0.0
	-6.00000	-14.00000	29.43000	-0.056031	29.215	-8.5758E-6	-0.061034	0.0
	-4.00000	-14.00000	29.43000	-0.070328	29.215	-10.697E-6	-0.069297	0.0
	-2.00000	-14.00000	29.43000	-0.084179	29.215	-12.867E-6	-0.077075	0.0
	0.00000	-14.00000	29.43000	-0.095852	29.215	-14.774E-6	-0.083509	0.0
	2.00000	-14.00000	29.43000	-0.10357	29.215	-16.062E-6	-0.087720	0.0
	4.00000	-14.00000	29.43000	-0.10602	29.215	-16.456E-6	-0.089064	0.0
	6.00000	-14.00000	29.43000	-0.10280	29.215	-15.873E-6	-0.087337	0.0
	8.00000	-14.00000	29.43000	-0.094499	29.215	-14.459E-6	-0.082841	0.0
	10.00000	-14.00000	29.43000	-0.082545	29.215	-12.513E-6	-0.076272	0.0
	12.00000	-14.00000	29.43000	-0.068693	29.215	-10.373E-6	-0.068492	0.0
	14.00000	-14.00000	29.43000	-0.054580	29.215	-8.3161E-6	-0.060314	0.0
	16.00000	-14.00000	29.43000	-0.041428	29.215	-6.5083E-6	-0.052362	0.0
	18.00000	-14.00000	29.43000	-0.029952	29.215	-5.0143E-6	-0.045028	0.0
	20.00000	-14.00000	29.43000	-0.020430	29.215	-3.8295E-6	-0.038503	0.0
	22.00000	-14.00000	29.43000	-0.012834	29.215	-2.9146E-6	-0.032840	0.0
	24.00000	-14.00000	29.43000	-0.0069674	29.215	-2.2192E-6	-0.028001	0.0
	26.00000	-14.00000	29.43000	-0.0025597	29.215	-1.6951E-6	-0.023906	0.0
	28.00000	-14.00000	29.43000	666.96E-6	29.215	-1.3012E-6	-0.020461	0.0
	30.00000	-14.00000	29.43000	0.0029661	29.215	-1.0050E-6	-0.017570	0.0
	-20.00000	-12.00000	29.43000	-0.0019366	29.215	-1.6193E-6	-0.023248	0.0
	-18.00000	-12.00000	29.43000	-0.0065147	29.215	-2.1657E-6	-0.027568	0.0
	-16.00000	-12.00000	29.43000	-0.012887	29.215	-2.9227E-6	-0.032842	0.0
	-14.00000	-12.00000	29.43000	-0.021571	29.215	-3.9748E-6	-0.039269	0.0
	-12.00000	-12.00000	29.43000	-0.033131	29.215	-5.4347E-6	-0.047058	0.0
	-10.00000	-12.00000	29.43000	-0.048082	29.215	-7.4419E-6	-0.056385	0.0
	-8.00000	-12.00000	29.43000	-0.066705	29.215	-10.143E-6	-0.067320	0.0
	-6.00000	-12.00000	29.43000	-0.088757	29.215	-13.638E-6	-0.079698	0.0
	-4.00000	-12.00000	29.43000	-0.11311	29.215	-17.868E-6	-0.092952	0.0
	-2.00000	-12.00000	29.43000	-0.13750	29.215	-22.474E-6	-0.10597	0.0
	0.00000	-12.00000	29.43000	-0.15860	29.215	-26.724E-6	-0.11710	0.0
	2.00000	-12.00000	29.43000	-0.17279	29.215	-29.672E-6	-0.12455	1.0255E-6
	4.00000	-12.00000	29.43000	-0.17729	29.215	-30.550E-6	-0.12690	1.0449E-6
	6.00000	-12.00000	29.43000	-0.17123	29.215	-29.147E-6	-0.12374	1.0188E-6
	8.00000	-12.00000	29.43000	-0.15595	29.215	-25.891E-6	-0.11575	0.0
	10.00000	-12.00000	29.43000	-0.13443	29.215	-21.605E-6	-0.10442	0.0
	12.00000	-12.00000	29.43000	-0.11021	29.215	-17.143E-6	-0.091508	0.0
	14.00000	-12.00000	29.43000	-0.086322	29.215	-13.110E-6	-0.078498	0.0
	16.00000	-12.00000	29.43000	-0.064828	29.215	-9.7898E-6	-0.066393	0.0
	18.00000	-12.00000	29.43000	-0.046715	29.215	-7.2161E-6	-0.055698	0.0
	20.00000	-12.00000	29.43000	-0.032172	29.215	-5.2938E-6	-0.046561	0.0
	22.00000	-12.00000	29.43000	-0.020915	29.215	-3.8874E-6	-0.038912	0.0
	24.00000	-12.00000	29.43000	-0.012445	29.215	-2.8683E-6	-0.032586	0.0
	26.00000	-12.00000	29.43000	-0.0062197	29.215	-2.1315E-6	-0.027384	0.0
	28.00000	-12.00000	29.43000	-0.0017412	29.215	-1.5976E-6	-0.023115	0.0
	30.00000	-12.00000	29.43000	0.0014120	29.215	-1.2085E-6	-0.019608	0.0
	-20.00000	-10.00000	29.43000	-0.0048920	29.215	-1.9738E-6	-0.026152	0.0
	-18.00000	-10.00000	29.43000	-0.011086	29.215	-2.7075E-6	-0.031471	0.0
	-16.00000	-10.00000	29.43000	-0.019886	29.215	-3.7648E-6	-0.038141	0.0
	-14.00000	-10.00000	29.43000	-0.032190	29.215	-5.3044E-6	-0.046532	0.0
	-12.00000	-10.00000	29.43000	-0.049078	29.215	-7.5628E-6	-0.057085	0.0
	-10.00000	-10.00000	29.43000	-0.071711	29.215	-10.879E-6	-0.070283	0.0
	-8.00000	-10.00000	29.43000	-0.10106	29.215	-15.698E-6	-0.086553	0.0
	-6.00000	-10.00000	29.43000	-0.13738	29.215	-22.499E-6	-0.10604	0.0
	-4.00000	-10.00000	29.43000	-0.17934	29.215	-31.521E-6	-0.12818	1.0554E-6
	-2.00000	-10.00000	29.43000	-0.22317	29.215	-42.237E-6	-0.15121	1.2448E-6
	0.00000	-10.00000	29.43000	-0.26245	29.215	-52.817E-6	-0.17188	1.4146E-6
	2.00000	-10.00000	29.43000	-0.28942	29.215	-60.407E-6	-0.18608	1.5313E-6
	4.00000	-10.00000	29.43000	-0.29794	29.215	-62.561E-6	-0.19049	1.5676E-6
	6.00000	-10.00000	29.43000	-0.28610	29.215	-58.701E-6	-0.18417	1.5157E-6
	8.00000	-10.00000	29.43000	-0.25703	29.215	-50.292E-6	-0.16885	1.3898E-6
	10.00000	-10.00000	29.43000	-0.21728	29.215	-39.869E-6	-0.14804	1.2187E-6
	12.00000	-10.00000	29.43000	-0.17412	29.215	-29.779E-6	-0.12548	1.0332E-6
	14.00000	-10.00000	29.43000	-0.13332	29.215	-21.385E-6	-0.10400	0.0
	16.00000	-10.00000	29.43000	-0.098141	29.215	-15.038E-6	-0.085110	0.0
	18.00000	-10.00000	29.43000	-0.069711	29.215	-10.500E-6	-0.069295	0.0
	20.00000	-10.00000	29.43000	-0.047749	29.215	-7.3466E-6	-0.056415	0.0
	22.00000	-10.00000	29.43000	-0.031322	29.215	-5.1800E-6	-0.046077	0.0
	24.00000	-10.00000	29.43000	-0.019324	29.215	-3.6921E-6	-0.037829	0.0
	26.00000	-10.00000	29.43000	-0.010724	29.215	-2.6641E-6	-0.031255	0.0
	28.00000	-10.00000	29.43000	-0.0046589	29.215	-1.9473E-6	-0.026000	0.0
	30.00000	-10.00000	29.43000	-452.40E-6	29.215	-1.4419E-6	-0.021781	0.0
	-20.00000	-8.00000	29.43000	-0.0083167	29.215	-2.3794E-6	-0.029230	0.0
	-18.00000	-8.00000	29.43000	-0.016478	29.215	-3.3495E-6	-0.035710	0.0
	-16.00000	-8.00000	29.43000	-0.028331	29.215	-4.8049E-6	-0.044064	0.0
	-14.00000	-8.00000	29.43000	-0.045364	29.215	-7.0312E-6	-0.054929	0.0
	-12.00000	-8.00000	29.43000	-0.069530	29.215	-10.501E-6	-0.069158	0.0
	-10.00000	-8.00000	29.43000	-0.10322	29.215	-15.991E-6	-0.087852	0.0
	-8.00000	-8.00000	29.43000	-0.14898	29.215	-24.746E-6	-0.11231	0.0
	-6.00000	-8.00000	29.43000	-0.20865	29.215	-38.561E-6	-0.14376	1.1835E-6
	-4.00000	-8.00000	29.43000	-0.28166	29.215	-59.380E-6	-0.18249	1.5018E-6
	-2.00000	-8.00000	29.43000	-0.36236	29.215	-87.477E-6	-0.22621	1.8609E-6
	0.00000	-8.00000	29.43000	-0.43814	29.215	-118.14E-6	-0.26821	2.2057E-6
	2.00000	-8.00000	29.43000	-0.49166	29.215	-141.09E-6	-0.29815	2.4514E-6
	4.00000	-8.00000	29.43000	-0.50836	29.215	-146.94E-6	-0.30713	2.5252E-6
	6.00000	-8.00000	29.43000	-0.48405	29.215	-134.25E-6	-0.29293	2.4087E-6
	8.00000	-8.00000	29.43000	-0.42646	29.215	-109.01E-6	-0.26057	2.1432E-6
	10.00000	-8.00000	29.43000	-0.35069	29.215	-80.157E-6	-0.21910	1.8027E-6
	12.00000	-8.00000	29.43000	-0.27229	29.215	-54.892E-6	-0.17721	1.4585E-6
	14.00000	-8.00000	29.43000	-0.20201	29.215	-36.157E-6	-0.14025	1.1547E-6
	16.00000	-8.00000	29.43000	-0.14458	29.215	-23.524E-6	-0.11010	0.0
	18.00000	-8.00000	29.43000	-0.10041	29.215	-15.373E-6	-0.086466	0.0
	20.00000	-8.00000	29.43000	-0.067772	29.215	-10.182E-6	-0.068285	0.0
	22.00000	-8.00000	29.43000	-0.044271	29.215	-6.8620E-6	-0.054370	0.0
	24.00000	-8.00000	29.43000	-0.027652	29.215	-4.7121E-6	-0.043699	0.0
	26.00000	-8.00000	29.43000	-0.016054	29.215	-3.2969E-6	-0.035466	0.0
	28.00000	-8.00000	29.43000	-0.0080518	29.215	-2.3487E-6	-0.029064	0.0
	30.00000	-8.00000	29.43000	-0.0025934	29.215	-1.7019E-6	-0.024041	0.0

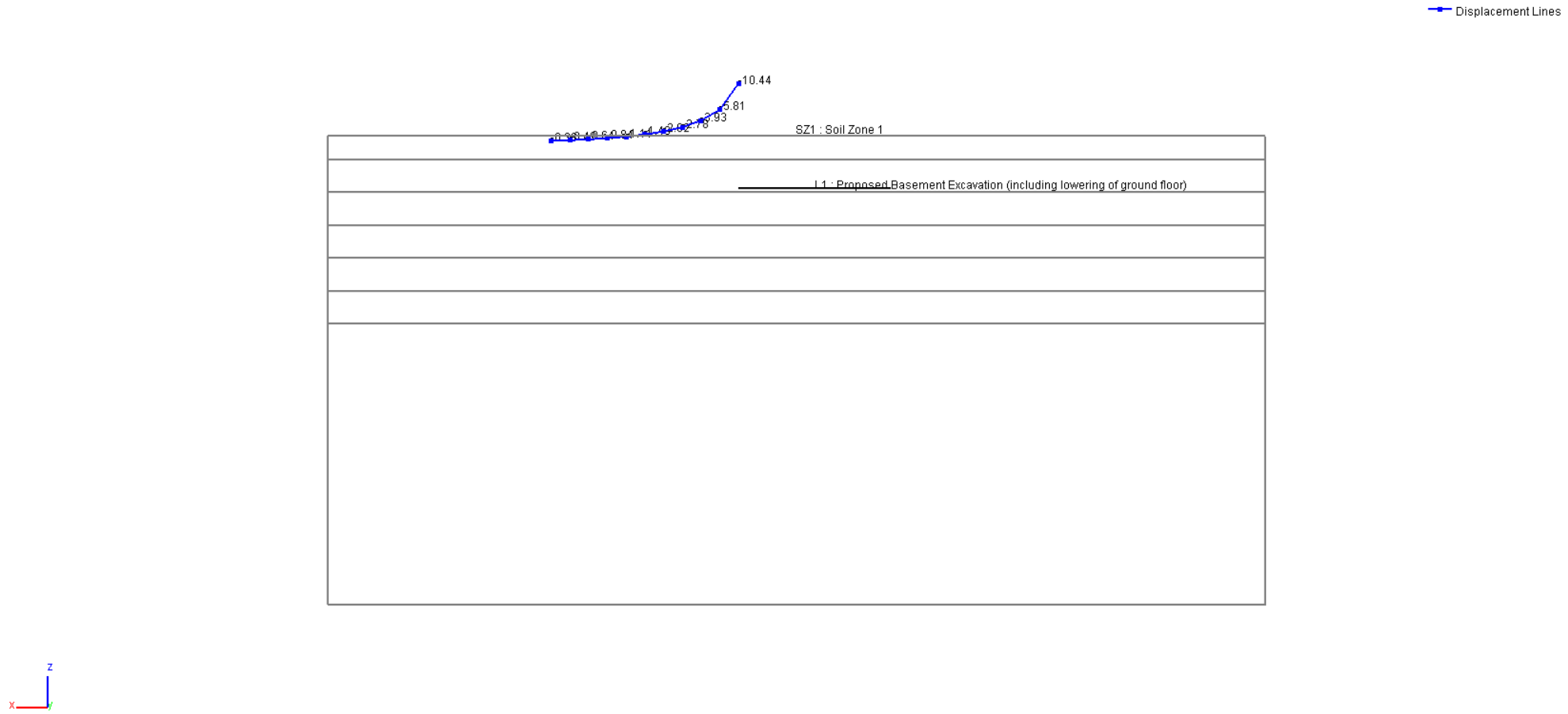
Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	-20.00000	-6.00000	29.43000	-0.012101	29.215	-2.8263E-6	-0.032392	0.0
	-18.00000	-6.00000	29.43000	-0.022547	29.215	-4.0813E-6	-0.040169	0.0
	-16.00000	-6.00000	29.43000	-0.038062	29.215	-6.0411E-6	-0.050476	0.0
	-14.00000	-6.00000	29.43000	-0.060985	29.215	-9.1921E-6	-0.064345	0.0
	-12.00000	-6.00000	29.43000	-0.094639	29.215	-14.423E-6	-0.083296	0.0
	-10.00000	-6.00000	29.43000	-0.14357	29.215	-23.411E-6	-0.10957	0.0
	-8.00000	-6.00000	29.43000	-0.21351	29.215	-39.375E-6	-0.14639	1.2051E-6
	-6.00000	-6.00000	29.43000	-0.31057	29.215	-68.429E-6	-0.19811	1.6301E-6
	-4.00000	-6.00000	29.43000	-0.43827	29.215	-120.91E-6	-0.26921	2.2138E-6
	-2.00000	-6.00000	29.43000	-0.59086	29.215	-207.66E-6	-0.36001	2.9582E-6
	0.00000	-6.00000	29.43000	-0.74423	29.215	-319.41E-6	-0.45715	3.7536E-6
	2.00000	-6.00000	29.43000	-0.85658	29.215	-407.28E-6	-0.52987	4.3489E-6
	4.00000	-6.00000	29.43000	-0.89062	29.215	-424.00E-6	-0.54977	4.5122E-6
	6.00000	-6.00000	29.43000	-0.83725	29.215	-370.26E-6	-0.51232	4.2060E-6
	8.00000	-6.00000	29.43000	-0.71718	29.215	-277.02E-6	-0.43453	3.5693E-6
	10.00000	-6.00000	29.43000	-0.56717	29.215	-181.12E-6	-0.34257	2.8157E-6
	12.00000	-6.00000	29.43000	-0.42169	29.215	-108.59E-6	-0.25859	2.1269E-6
	14.00000	-6.00000	29.43000	-0.30014	29.215	-63.265E-6	-0.19218	1.5815E-6
	16.00000	-6.00000	29.43000	-0.20725	29.215	-37.208E-6	-0.14312	1.1783E-6
	18.00000	-6.00000	29.43000	-0.13987	29.215	-22.461E-6	-0.10772	0.0
	20.00000	-6.00000	29.43000	-0.092460	29.215	-13.984E-6	-0.082220	0.0
	22.00000	-6.00000	29.43000	-0.059694	29.215	-8.9769E-6	-0.063696	0.0
	24.00000	-6.00000	29.43000	-0.037291	29.215	-5.9302E-6	-0.050071	0.0
	26.00000	-6.00000	29.43000	-0.022082	29.215	-4.0215E-6	-0.039908	0.0
	28.00000	-6.00000	29.43000	-0.011818	29.215	-2.7926E-6	-0.032219	0.0
	30.00000	-6.00000	29.43000	-0.0049371	29.215	-1.9813E-6	-0.026322	0.0
	-20.00000	-4.00000	29.43000	-0.016056	29.215	-3.2945E-6	-0.035505	0.0
	-18.00000	-4.00000	29.43000	-0.029004	29.215	-4.8733E-6	-0.044660	0.0
	-16.00000	-4.00000	29.43000	-0.048650	29.215	-7.4332E-6	-0.057117	0.0
	-14.00000	-4.00000	29.43000	-0.078463	29.215	-11.750E-6	-0.074441	0.0
	-12.00000	-4.00000	29.43000	-0.12372	29.215	-19.378E-6	-0.099131	0.0
	-10.00000	-4.00000	29.43000	-0.19234	29.215	-33.628E-6	-0.13531	1.1140E-6
	-8.00000	-4.00000	29.43000	-0.29584	29.215	-62.103E-6	-0.18997	1.5634E-6
	-6.00000	-4.00000	29.43000	-0.44983	29.215	-123.67E-6	-0.27524	2.2634E-6
	-4.00000	-4.00000	29.43000	-0.67180	29.215	-267.43E-6	-0.41138	3.3789E-6
	-2.00000	-4.00000	29.43000	-0.96883	29.215	-605.20E-6	-0.62375	5.1132E-6
	0.00000	-4.00000	29.43000	-1.3021	29.215	-0.0012117	-0.90057	7.3658E-6
	2.00000	-4.00000	29.43000	-1.5585	29.215	-0.0017161	-1.1213	9.1611E-6
	4.00000	-4.00000	29.43000	-1.6295	29.215	-0.0017309	-1.1655	9.5245E-6
	6.00000	-4.00000	29.43000	-1.5009	29.215	-0.0013913	-1.0404	8.5103E-6
	8.00000	-4.00000	29.43000	-1.2330	29.215	-917.36E-6	-0.81546	6.6785E-6
	10.00000	-4.00000	29.43000	-0.92013	29.215	-486.97E-6	-0.57628	4.7276E-6
	12.00000	-4.00000	29.43000	-0.64395	29.215	-232.76E-6	-0.39023	3.2062E-6
	14.00000	-4.00000	29.43000	-0.43477	29.215	-113.31E-6	-0.26584	2.1864E-6
	16.00000	-4.00000	29.43000	-0.28772	29.215	-58.633E-6	-0.18553	1.5269E-6
	18.00000	-4.00000	29.43000	-0.18790	29.215	-32.319E-6	-0.13305	1.0955E-6
	20.00000	-4.00000	29.43000	-0.12125	29.215	-18.832E-6	-0.097912	0.0
	22.00000	-4.00000	29.43000	-0.077066	29.215	-11.502E-6	-0.073744	0.0
	24.00000	-4.00000	29.43000	-0.047844	29.215	-7.3124E-6	-0.056699	0.0
	26.00000	-4.00000	29.43000	-0.028531	29.215	-4.8109E-6	-0.044399	0.0
	28.00000	-4.00000	29.43000	-0.015774	29.215	-3.2605E-6	-0.035336	0.0
	30.00000	-4.00000	29.43000	-0.0073651	29.215	-2.2678E-6	-0.028532	0.0
	-20.00000	-2.00000	29.43000	-0.019911	29.215	-3.7539E-6	-0.038400	0.0
	-18.00000	-2.00000	29.43000	-0.035403	29.215	-5.6729E-6	-0.048924	0.0
	-16.00000	-2.00000	29.43000	-0.059362	29.215	-8.8894E-6	-0.063586	0.0
	-14.00000	-2.00000	29.43000	-0.096602	29.215	-14.549E-6	-0.084594	0.0
	-12.00000	-2.00000	29.43000	-0.15487	29.215	-25.125E-6	-0.11572	0.0
	-10.00000	-2.00000	29.43000	-0.24670	29.215	-46.466E-6	-0.16378	1.3481E-6
	-8.00000	-2.00000	29.43000	-0.39248	29.215	-94.211E-6	-0.24194	1.9902E-6
	-6.00000	-2.00000	29.43000	-0.62532	29.215	-217.94E-6	-0.37823	3.1079E-6
	-4.00000	-2.00000	29.43000	-0.99843	29.215	-618.09E-6	-0.64027	5.2488E-6
	-2.00000	-2.00000	29.43000	-1.5887	29.215	-0.0024010	-1.2131	9.8838E-6
	0.00000	-2.00000	29.43000	-2.4147	29.215	-0.010470	-2.4313	19.530E-6
	2.00000	-2.00000	29.43000	-3.0945	29.215	-0.017678	-3.4857	27.867E-6
	4.00000	-2.00000	29.43000	-3.2270	29.215	-0.015137	-3.4615	27.793E-6
	6.00000	-2.00000	29.43000	-2.8693	29.215	-0.0099195	-2.8123	22.698E-6
	8.00000	-2.00000	29.43000	-2.2071	29.215	-0.0054768	-1.9226	15.582E-6
	10.00000	-2.00000	29.43000	-1.4932	29.215	-0.0017373	-1.0750	8.7776E-6
	12.00000	-2.00000	29.43000	-0.95781	29.215	-532.66E-6	-0.60314	4.9469E-6
	14.00000	-2.00000	29.43000	-0.60673	29.215	-201.04E-6	-0.36556	3.0043E-6
	16.00000	-2.00000	29.43000	-0.38341	29.215	-89.662E-6	-0.23677	1.9479E-6
	18.00000	-2.00000	29.43000	-0.24207	29.215	-44.960E-6	-0.16138	1.3285E-6
	20.00000	-2.00000	29.43000	-0.15242	29.215	-24.548E-6	-0.11450	0.0
	22.00000	-2.00000	29.43000	-0.095261	29.215	-14.302E-6	-0.083927	0.0
	24.00000	-2.00000	29.43000	-0.058609	29.215	-8.7739E-6	-0.063198	0.0
	26.00000	-2.00000	29.43000	-0.034970	29.215	-5.6150E-6	-0.048687	0.0
	28.00000	-2.00000	29.43000	-0.019657	29.215	-3.7230E-6	-0.038249	0.0
	30.00000	-2.00000	29.43000	-0.0097174	29.215	-2.5442E-6	-0.030562	0.0
	-20.00000	0.00000	29.43000	-0.023343	29.215	-4.1657E-6	-0.040887	0.0
	-18.00000	0.00000	29.43000	-0.041179	29.215	-6.4071E-6	-0.052652	0.0
	-16.00000	0.00000	29.43000	-0.069199	29.215	-10.266E-6	-0.069364	0.0
	-14.00000	0.00000	29.43000	-0.11362	29.215	-17.293E-6	-0.093911	0.0
	-12.00000	0.00000	29.43000	-0.18487	29.215	-31.026E-6	-0.13148	1.0826E-6
	-10.00000	0.00000	29.43000	-0.30080	29.215	-60.480E-6	-0.19205	1.5806E-6
	-8.00000	0.00000	29.43000	-0.49278	29.215	-132.46E-6	-0.29683	2.4410E-6
	-6.00000	0.00000	29.43000	-0.81845	29.215	-347.67E-6	-0.49766	4.0863E-6
	-4.00000	0.00000	29.43000	-1.3932	29.215	-0.0012708	-0.95573	7.8177E-6
	-2.00000	0.00000	29.43000	-2.4995	29.215	-0.010590	-2.4938	20.039E-6
	0.00000	0.00000	29.43000	-5.7690	29.215	-20.662	-48.464	-622.61E-6
	2.00000	0.00000	29.43000	-8.7882	29.215	-41.300	-93.875	-0.0012692
	4.00000	0.00000	29.43000	-8.1988	29.215	-13.462	-56.916	-196.72E-6
	6.00000	0.00000	29.43000	-6.4782	29.215	-0.91259	-20.452	123.49E-6
	8.00000	0.00000	29.43000	-4.4801	29.215	-0.52154	-11.779	71.319E-6
	10.00000	0.00000	29.43000	-2.3692	29.215	-0.0083765	-2.2307	17.979E-6
	12.00000	0.00000	29.43000	-1.3509	29.215	-0.0011580	-0.91349	7.4750E-6
	14.00000	0.00000	29.43000	-0.80108	29.215	-330.42E-6	-0.48546	3.9865E-6
	16.00000	0.00000	29.43000	-0.48482	29.215	-128.32E-6	-0.29224	2.4033E-6
	18.00000	0.00000	29.43000	-0.29689	29.215	-59.193E-6	-0.19003	1.5640E-6
	20.00000	0.00000	29.43000	-0.18285	29.215	-30.553E-6	-0.13048	1.0744E-6
	22.00000	0.00000	29.43000	-0.11254	29.215	-17.096E-6	-0.093374	0.0
	24.00000	0.00000	29.43000	-0.068603	29.215	-10.175E-6	-0.069056	0.0
	26.00000	0.00000	29.43000	-0.040840	29.215	-6.3622E-6	-0.052465	0.0
	28.00000	0.00000	29.43000	-0.023146	29.215	-4.1419E-6	-0.040768	0.0
	30.00000	0.00000	29.43000	-0.011806	29.215	-2.7894E-6	-0.032290	0.0
	-20.00000	2.00000	29.43000	-0.026015	29.215	-4.4884E-6	-0.042776	0.0
	-18.00000	2.00000	29.43000	-0.045725	29.215	-6.9927E-6	-0.055522	0.0
	-16.00000	2.00000	29.43000	-0.077044	29.215	-11.388E-6	-0.073886	0.0
	-14.00000	2.00000	29.43000	-0.12741	29.215	-19.588E-6	-0.10135	0.0
	-12.00000	2.00000	29.43000	-0.20964	29.215	-36.114E-6	-0.14438	1.1887E-6
	-10.00000	2.00000	29.43000	-0.34649	29.215	-72.996E-6	-0.21592	1.7768E-6
	-8.00000	2.00000	29.43000	-0.57980	29.215	-167.95E-6	-0.34489	2.8355E-6
	-6.00000	2.00000	29.43000	-0.99119	29.215	-472.45E-6	-0.60666	4.9789E-6
	-4.00000	2.00000	29.43000	-1.7583	29.215	-0.0019158	-1.2561	10.263E-6
	-2.00000	2.00000	29.43000	-3.3721	29.215	-0.018776	-3.7564	30.045E-6
	0.00000	2.00000	29.43000	-9.0884	29.215	-41.314	-94.502	-0.0012647
	2.00000	2.00000	29.43000	-14.556	29.215	-82.608	-184.98	-0.0025616
	4.00000	2.00000	29.43000	-15.304	29.215	-82.615	-186.29	-0.0025512
	6.00000	2.00000	29.43000	-14.252	29.215	-82.582	-183.65	-0.0025713
	8.00000	2.00000	29.43000	-9.4284	29.215	-59.266	-115.80	-0.0019772
	10.00000	2.00000	29.43000	-3.3251	29.215	-0.020028	-3.7557	29.977E-6
	12.00000	2.00000	29.43000	-1.7370	29.215	-0.0019090	-1.2411	10.139E-6
	14.00000	2.00000	29.43000	-0.98168	29.215	-467.38E-6	-0.60092	4.9318E-6
	16.00000	2.00000	29.43000	-0.57532	29.215	-166.31E-6	-0.34251	2.8160E-6
	18.00000	2.00000	29.43000	-0.34427	29.215	-72.424E-6	-0.21482	1.7677E-6
	20.00000	2.00000	29.43000	-0.20849	29.215	-35.889E-6	-0.14381	1.1840E-6
	22.00000	2.00000	29.43000	-0.12678	29.215	-19.489E-6	-0.10104	0.0
	24.00000	2.00000	29.43000	-0.076696	29.215	-11.341E-6	-0.073700	0.0
	26.00000	2.00000	29.43000	-0.045526	29.215	-6.9685E-6	-0.055406	0.0
	28.00000	2.00000	29.43000	-0.025898	29.215	-4.4752E-6	-0.042700	0.0
	30.00000	2.00000	29.43000	-0.013439	29.215	-2.9813E-6	-0.033601	0.0
	-20.00000	4.00000	29.43000	-0.027637	29.215	-4.6852E-6	-0.043907	0.0
	-18.00000	4.00000	29.43000	-0.048504	29.215	-7.3537E-6	-0.057254	0.0
	-16.00000	4.00000	29.43000	-0.081880	29.215	-12.089E-6	-0.076644	0.0
	-14.00000	4.00000	29.43000	-0.13599	29.215	-21.043E-6	-0.10595	0.0
	-12.00000	4.00000	29.43000	-0.22524	29.215	-39.391E-6	-0.15246	1.2552E-6
	-10.00000	4.00000	29.43000	-0.37564	29.215	-81.156E-6	-0.23113	1.9018E-6
	-8.00000	4.00000	29.43000	-0.63594	29.215	-191.00E-6	-0.37589	3.0900E-6
	-6.00000	4.00000	29.43000	-1.1031	29.215	-549.23E-6	-0.67652	5.5511E-6
	-4.00000	4.00000	29.43000	-1.9895	29.215	-0.0022346	-1.4342	11.715E-6
	-2.00000	4.00000	29.43000	-3.8600	29.215	-0.020528	-4.2754	34.238E-6
	0.00000	4.00000	29.43000	-10.048	29.215	-41.323	-95.968	-0.0012531

Name	Location			Displacement	Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	2.00000	4.00000	29.43000	-15.991	29.215	-82.625	-187.47	-0.0025420
	4.00000	4.00000	29.43000	-17.021	29.215	-82.642	-189.55	-0.0025256
	6.00000	4.00000	29.43000	-15.992	29.215	-82.627	-187.55	-0.0025414
	8.00000	4.00000	29.43000	-10.646	29.215	-59.293	-118.28	-0.0019581
	10.00000	4.00000	29.43000	-3.9008	29.215	-0.023056	-4.4538	35.583E-6
	12.00000	4.00000	29.43000	-1.9971	29.215	-0.0023339	-1.4527	11.863E-6
	14.00000	4.00000	29.43000	-1.1047	29.215	-559.87E-6	-0.67970	5.5768E-6
	16.00000	4.00000	29.43000	-0.63626	29.215	-192.80E-6	-0.37654	3.0953E-6
	18.00000	4.00000	29.43000	-0.37565	29.215	-81.549E-6	-0.23125	1.9027E-6
	20.00000	4.00000	29.43000	-0.22519	29.215	-39.491E-6	-0.15246	1.2551E-6
	22.00000	4.00000	29.43000	-0.13593	29.215	-21.070E-6	-0.10591	0.0
	24.00000	4.00000	29.43000	-0.081835	29.215	-12.095E-6	-0.076607	0.0
	26.00000	4.00000	29.43000	-0.048471	29.215	-7.3544E-6	-0.057223	0.0
	28.00000	4.00000	29.43000	-0.027615	29.215	-4.6843E-6	-0.043881	0.0
	30.00000	4.00000	29.43000	-0.014451	29.215	-3.1003E-6	-0.034395	0.0
	-20.00000	6.00000	29.43000	-0.028022	29.215	-4.7319E-6	-0.044177	0.0
	-18.00000	6.00000	29.43000	-0.049164	29.215	-7.4394E-6	-0.057668	0.0
	-16.00000	6.00000	29.43000	-0.083031	29.215	-12.255E-6	-0.077303	0.0
	-14.00000	6.00000	29.43000	-0.13804	29.215	-21.389E-6	-0.10705	0.0
	-12.00000	6.00000	29.43000	-0.22898	29.215	-40.172E-6	-0.15440	1.2712E-6
	-10.00000	6.00000	29.43000	-0.38263	29.215	-83.096E-6	-0.23478	1.9317E-6
	-8.00000	6.00000	29.43000	-0.64943	29.215	-196.40E-6	-0.38330	3.1508E-6
	-6.00000	6.00000	29.43000	-1.1298	29.215	-566.23E-6	-0.69290	5.6853E-6
	-4.00000	6.00000	29.43000	-2.0433	29.215	-0.0022941	-1.4732	12.034E-6
	-2.00000	6.00000	29.43000	-3.9655	29.215	-0.020736	-4.3692	35.001E-6
	0.00000	6.00000	29.43000	-10.233	29.215	-41.324	-96.162	-0.0011515
	2.00000	6.00000	29.43000	-16.259	29.215	-82.626	-187.78	-0.0025395
	4.00000	6.00000	29.43000	-17.347	29.215	-82.643	-189.94	-0.0025225
	6.00000	6.00000	29.43000	-16.326	29.215	-82.629	-187.97	-0.0025380
	8.00000	6.00000	29.43000	-10.904	29.215	-59.294	-118.60	-0.0019556
	10.00000	6.00000	29.43000	-4.0504	29.215	-0.023452	-4.6026	36.791E-6
	12.00000	6.00000	29.43000	-2.0716	29.215	-0.0024359	-1.5110	12.339E-6
	14.00000	6.00000	29.43000	-1.1409	29.215	-586.76E-6	-0.70291	5.7668E-6
	16.00000	6.00000	29.43000	-0.65414	29.215	-200.86E-6	-0.38660	3.1778E-6
	18.00000	6.00000	29.43000	-0.38477	29.215	-84.325E-6	-0.23603	1.9420E-6
	20.00000	6.00000	29.43000	-0.23000	29.215	-40.571E-6	-0.15493	1.2755E-6
	22.00000	6.00000	29.43000	-0.13854	29.215	-21.535E-6	-0.10728	0.0
	24.00000	6.00000	29.43000	-0.083287	29.215	-12.314E-6	-0.077414	0.0
	26.00000	6.00000	29.43000	-0.049298	29.215	-7.4645E-6	-0.057722	0.0
	28.00000	6.00000	29.43000	-0.028093	29.215	-4.7432E-6	-0.044202	0.0
	30.00000	6.00000	29.43000	-0.014732	29.215	-3.1334E-6	-0.034609	0.0
	-20.00000	8.00000	29.43000	-0.027123	29.215	-4.6225E-6	-0.043562	0.0
	-18.00000	8.00000	29.43000	-0.047620	29.215	-7.2374E-6	-0.056720	0.0
	-16.00000	8.00000	29.43000	-0.080334	29.215	-11.860E-6	-0.075783	0.0
	-14.00000	8.00000	29.43000	-0.13323	29.215	-20.562E-6	-0.10449	0.0
	-12.00000	8.00000	29.43000	-0.22019	29.215	-38.294E-6	-0.14987	1.2339E-6
	-10.00000	8.00000	29.43000	-0.36612	29.215	-78.395E-6	-0.22618	1.8611E-6
	-8.00000	8.00000	29.43000	-0.61749	29.215	-183.17E-6	-0.36566	3.0060E-6
	-6.00000	8.00000	29.43000	-1.0662	29.215	-523.61E-6	-0.65335	5.3613E-6
	-4.00000	8.00000	29.43000	-1.9137	29.215	-0.0021364	-1.3764	11.243E-6
	-2.00000	8.00000	29.43000	-3.7056	29.215	-0.020111	-4.1225	32.998E-6
	0.00000	8.00000	29.43000	-9.7656	29.215	-41.322	-95.611	-0.0012560
	2.00000	8.00000	29.43000	-15.589	29.215	-82.623	-186.89	-0.0025466
	4.00000	8.00000	29.43000	-16.600	29.215	-82.638	-188.91	-0.0025308
	6.00000	8.00000	29.43000	-15.680	29.215	-82.625	-187.13	-0.0025448
	8.00000	8.00000	29.43000	-10.461	29.215	-59.292	-118.07	-0.0019598
	10.00000	8.00000	29.43000	-3.8067	29.215	-0.022850	-4.3697	34.901E-6
	12.00000	8.00000	29.43000	-1.9516	29.215	-0.0022866	-1.4209	11.603E-6
	14.00000	8.00000	29.43000	-1.0824	29.215	-547.31E-6	-0.66652	5.4688E-6
	16.00000	8.00000	29.43000	-0.62498	29.215	-188.81E-6	-0.37048	3.0455E-6
	18.00000	8.00000	29.43000	-0.36975	29.215	-80.082E-6	-0.22819	1.8776E-6
	20.00000	8.00000	29.43000	-0.22201	29.215	-38.882E-6	-0.15079	1.2414E-6
	22.00000	8.00000	29.43000	-0.13417	29.215	-20.791E-6	-0.10494	0.0
	24.00000	8.00000	29.43000	-0.080835	29.215	-11.958E-6	-0.076016	0.0
	26.00000	8.00000	29.43000	-0.047894	29.215	-7.2820E-6	-0.056846	0.0
	28.00000	8.00000	29.43000	-0.027276	29.215	-4.6441E-6	-0.043632	0.0
	30.00000	8.00000	29.43000	-0.014251	29.215	-3.0769E-6	-0.034225	0.0
	-20.00000	10.00000	29.43000	-0.025049	29.215	-4.3711E-6	-0.042119	0.0
	-18.00000	10.00000	29.43000	-0.044073	29.215	-6.7771E-6	-0.054512	0.0
	-16.00000	10.00000	29.43000	-0.074176	29.215	-10.969E-6	-0.072275	0.0
	-14.00000	10.00000	29.43000	-0.12233	29.215	-18.718E-6	-0.098661	0.0
	-12.00000	10.00000	29.43000	-0.21044	29.215	-34.155E-6	-0.13964	1.1497E-6
	-10.00000	10.00000	29.43000	-0.32935	29.215	-68.101E-6	-0.20699	1.7034E-6
	-8.00000	10.00000	29.43000	-0.54681	29.215	-153.90E-6	-0.32658	2.6852E-6
	-6.00000	10.00000	29.43000	-0.92506	29.215	-423.10E-6	-0.56449	4.6336E-6
	-4.00000	10.00000	29.43000	-1.6179	29.215	-0.0016721	-1.1401	9.3183E-6
	-2.00000	10.00000	29.43000	-3.0449	29.215	-0.016444	-3.3165	26.533E-6
	0.00000	10.00000	29.43000	-8.2673	29.215	-41.269	-92.079	-0.0012825
	2.00000	10.00000	29.43000	-13.203	29.215	-82.506	-180.10	-0.0025968
	4.00000	10.00000	29.43000	-13.689	29.215	-82.197	-177.27	-0.0026049
	6.00000	10.00000	29.43000	-13.344	29.215	-82.524	-180.76	-0.0025923
	8.00000	10.00000	29.43000	-8.9621	29.215	-59.240	-114.56	-0.0019862
	10.00000	10.00000	29.43000	-3.1393	29.215	-0.018949	-3.5394	28.247E-6
	12.00000	10.00000	29.43000	-1.6549	29.215	-0.0018005	-1.1804	9.6443E-6
	14.00000	10.00000	29.43000	-0.94204	29.215	-444.15E-6	-0.57732	4.7383E-6
	16.00000	10.00000	29.43000	-0.55514	29.215	-159.28E-6	-0.33166	2.7269E-6
	18.00000	10.00000	29.43000	-0.33359	29.215	-69.828E-6	-0.20927	1.7221E-6
	20.00000	10.00000	29.43000	-0.20266	29.215	-34.797E-6	-0.14075	1.1588E-6
	22.00000	10.00000	29.43000	-0.12353	29.215	-18.983E-6	-0.099235	0.0
	24.00000	10.00000	29.43000	-0.074834	29.215	-11.087E-6	-0.072587	0.0
	26.00000	10.00000	29.43000	-0.044443	29.215	-6.8334E-6	-0.054690	0.0
	28.00000	10.00000	29.43000	-0.025260	29.215	-4.3994E-6	-0.042223	0.0
	30.00000	10.00000	29.43000	-0.013060	29.215	-2.9368E-6	-0.033273	0.0
	-20.00000	12.00000	29.43000	-0.022033	29.215	-4.0078E-6	-0.039977	0.0
	-18.00000	12.00000	29.43000	-0.038963	29.215	-6.1217E-6	-0.051271	0.0
	-16.00000	12.00000	29.43000	-0.065398	29.215	-9.7225E-6	-0.067194	0.0
	-14.00000	12.00000	29.43000	-0.10699	29.215	-16.190E-6	-0.090357	0.0
	-12.00000	12.00000	29.43000	-0.17306	29.215	-28.607E-6	-0.12536	1.0322E-6
	-10.00000	12.00000	29.43000	-0.27924	29.215	-54.602E-6	-0.18083	1.4883E-6
	-8.00000	12.00000	29.43000	-0.45222	29.215	-115.98E-6	-0.27447	2.2574E-6
	-6.00000	12.00000	29.43000	-0.73889	29.215	-289.78E-6	-0.44740	3.6748E-6
	-4.00000	12.00000	29.43000	-1.2261	29.215	-961.42E-6	-0.81639	6.6840E-6
	-2.00000	12.00000	29.43000	-2.0919	29.215	-0.0059076	-1.8570	15.020E-6
	0.00000	12.00000	29.43000	-3.6768	29.215	-0.12899	-6.7140	48.979E-6
	2.00000	12.00000	29.43000	-5.0375	29.215	-0.24127	-10.978	78.583E-6
	4.00000	12.00000	29.43000	-5.2392	29.215	-0.10511	-9.0463	69.392E-6
	6.00000	12.00000	29.43000	-5.1627	29.215	-0.28273	-11.819	83.470E-6
	8.00000	12.00000	29.43000	-3.8081	29.215	-0.16379	-7.4539	53.359E-6
	10.00000	12.00000	29.43000	-2.1512	29.215	-0.0067196	-1.9613	15.840E-6
	12.00000	12.00000	29.43000	-1.2542	29.215	-0.0010322	-0.84312	6.9010E-6
	14.00000	12.00000	29.43000	-0.75320	29.215	-304.02E-6	-0.45736	3.7562E-6
	16.00000	12.00000	29.43000	-0.45980	29.215	-120.11E-6	-0.27886	2.2934E-6
	18.00000	12.00000	29.43000	-0.28334	29.215	-56.061E-6	-0.18296	1.5059E-6
	20.00000	12.00000	29.43000	-0.17532	29.215	-29.192E-6	-0.12647	1.0413E-6
	22.00000	12.00000	29.43000	-0.10825	29.215	-16.447E-6	-0.090964	0.0
	24.00000	12.00000	29.43000	-0.066117	29.215	-9.8431E-6	-0.067541	0.0
	26.00000	12.00000	29.43000	-0.039378	29.215	-6.1817E-6	-0.051476	0.0
	28.00000	12.00000	29.43000	-0.022276	29.215	-4.0391E-6	-0.040101	0.0
	30.00000	12.00000	29.43000	-0.011286	29.215	-2.7284E-6	-0.031829	0.0
	-20.00000	14.00000	29.43000	-0.018392	29.215	-3.5724E-6	-0.037310	0.0
	-18.00000	14.00000	29.43000	-0.032869	29.215	-5.3523E-6	-0.047300	0.0
	-16.00000	14.00000	29.43000	-0.055088	29.215	-8.2955E-6	-0.061086	0.0
	-14.00000	14.00000	29.43000	-0.089298	29.215	-13.385E-6	-0.080606	0.0
	-12.00000	14.00000	29.43000	-0.14219	29.215	-22.678E-6	-0.10908	0.0
	-10.00000	14.00000	29.43000	-0.22426	29.215	-40.841E-6	-0.15210	1.2521E-6
	-8.00000	14.00000	29.43000	-0.35188	29.215	-79.598E-6	-0.21997	1.8098E-6
	-6.00000	14.00000	29.43000	-0.54990	29.215	-172.57E-6	-0.33285	2.7360E-6
	-4.00000	14.00000	29.43000	-0.85322	29.215	-432.49E-6	-0.53264	4.3706E-6
	-2.00000	14.00000	29.43000	-1.2974	29.215	-0.0012723	-0.90248	7.3785E-6
	0.00000	14.00000	29.43000	-1.8532	29.215	-0.0034840	-1.4985	12.183E-6
	2.00000	14.00000	29.43000	-2.3098	29.215	-0.0053105	-2.0000	16.228E-6
	4.00000	14.00000	29.43000	-2.4776	29.215	-0.0054441	-2.1459	17.425E-6
	6.00000	14.00000	29.43000	-2.3395	29.215	-0.0056336	-2.0511	16.634E-6
	8.00000	14.00000	29.43000	-1.8905	29.215	-0.0037649	-1.5525	12.615E-6
	10.00000	14.00000	29.43000	-1.3257	29.215	-0.0013704	-0.93256	7.6217E-6
	12.00000	14.00000	29.43000	-0.87076	29.215	-457.59E-6	-0.54632	4.4821E-6
	14.00000	14.00000	29.43000	-0.56022	29.215	-180.06E-6	-0.33934	2.7891E-6
	16.00000	14.00000	29.43000	-0.35788	29.215	-82.247E-6	-0.22326	1.8368E-6
	18.00000	14.00000	29.43000	-0.22773	29.215	-41.904E-6	-0.15386	1.2666E-6
	20.00000	14.00000	29.43000	-0.14420	29.215	-23.146E-6	-0.11006	0.0
	22.00000	14.00000	29.43000	-0.090480	29.215	-13.605E-6	-0.081178	0.0

Name	Location			Displacement	Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	24.00000	14.00000	29.43000	-0.055785	29.215	-8.4052E-6	-0.061429	0.0
	26.00000	14.00000	29.43000	-0.033284	29.215	-5.4095E-6	-0.047511	0.0
	28.00000	14.00000	29.43000	-0.018643	29.215	-3.6034E-6	-0.037444	0.0
	30.00000	14.00000	29.43000	-0.0091050	29.215	-2.4720E-6	-0.029997	0.0
	-20.00000	16.00000	29.43000	-0.014464	29.215	-3.1060E-6	-0.034314	0.0
	-18.00000	16.00000	29.43000	-0.026392	29.215	-4.5496E-6	-0.042920	0.0
	-16.00000	16.00000	29.43000	-0.044335	29.215	-6.8539E-6	-0.054508	0.0
	-14.00000	16.00000	29.43000	-0.071273	29.215	-10.664E-6	-0.070409	0.0
	-12.00000	16.00000	29.43000	-0.11162	29.215	-17.220E-6	-0.092682	0.0
	-10.00000	16.00000	29.43000	-0.17176	29.215	-29.038E-6	-0.12457	1.0257E-6
	-8.00000	16.00000	29.43000	-0.26051	29.215	-51.474E-6	-0.17125	1.4095E-6
	-6.00000	16.00000	29.43000	-0.38879	29.215	-96.371E-6	-0.24080	1.9808E-6
	-4.00000	16.00000	29.43000	-0.56666	29.215	-189.26E-6	-0.34453	2.8315E-6
	-2.00000	16.00000	29.43000	-0.79334	29.215	-372.09E-6	-0.49158	4.0349E-6
	0.00000	16.00000	29.43000	-1.0373	29.215	-648.22E-6	-0.66639	5.4627E-6
	2.00000	16.00000	29.43000	-1.2294	29.215	-883.30E-6	-0.80889	6.6261E-6
	4.00000	16.00000	29.43000	-1.3047	29.215	-968.24E-6	-0.86433	7.0790E-6
	6.00000	16.00000	29.43000	-1.2394	29.215	-908.27E-6	-0.81860	6.7049E-6
	8.00000	16.00000	29.43000	-1.0519	29.215	-676.45E-6	-0.67914	5.5664E-6
	10.00000	16.00000	29.43000	-0.80677	29.215	-389.55E-6	-0.50176	4.1180E-6
	12.00000	16.00000	29.43000	-0.57668	29.215	-197.27E-6	-0.35101	2.8845E-6
	14.00000	16.00000	29.43000	-0.39552	29.215	-99.792E-6	-0.24463	2.0122E-6
	16.00000	16.00000	29.43000	-0.26481	29.215	-52.977E-6	-0.17349	1.4279E-6
	18.00000	16.00000	29.43000	-0.17444	29.215	-29.734E-6	-0.12590	1.0367E-6
	20.00000	16.00000	29.43000	-0.11327	29.215	-17.559E-6	-0.093486	0.0
	22.00000	16.00000	29.43000	-0.072286	29.215	-10.836E-6	-0.070904	0.0
	24.00000	16.00000	29.43000	-0.044956	29.215	-6.9453E-6	-0.054820	0.0
	26.00000	16.00000	29.43000	-0.026775	29.215	-4.5997E-6	-0.043120	0.0
	28.00000	16.00000	29.43000	-0.014702	29.215	-3.1344E-6	-0.034445	0.0
	30.00000	16.00000	29.43000	-0.0067109	29.215	-2.1901E-6	-0.027897	0.0
	-20.00000	18.00000	29.43000	-0.010554	29.215	-2.6442E-6	-0.031170	0.0
	-18.00000	18.00000	29.43000	-0.020054	29.215	-3.7785E-6	-0.038424	0.0
	-16.00000	18.00000	29.43000	-0.034037	29.215	-5.5205E-6	-0.047933	0.0
	-14.00000	18.00000	29.43000	-0.054467	29.215	-8.2632E-6	-0.060552	0.0
	-12.00000	18.00000	29.43000	-0.084050	29.215	-12.696E-6	-0.077495	0.0
	-10.00000	18.00000	29.43000	-0.12634	29.215	-20.045E-6	-0.10046	0.0
	-8.00000	18.00000	29.43000	-0.18554	29.215	-32.493E-6	-0.13173	1.0846E-6
	-6.00000	18.00000	29.43000	-0.26566	29.215	-53.734E-6	-0.17400	1.4321E-6
	-4.00000	18.00000	29.43000	-0.36805	29.215	-89.010E-6	-0.22939	1.8870E-6
	-2.00000	18.00000	29.43000	-0.48693	29.215	-142.04E-6	-0.29648	2.4376E-6
	0.00000	18.00000	29.43000	-0.60462	29.215	-206.02E-6	-0.36575	3.0056E-6
	2.00000	18.00000	29.43000	-0.69340	29.215	-259.02E-6	-0.41929	3.4445E-6
	4.00000	18.00000	29.43000	-0.72784	29.215	-280.40E-6	-0.44032	3.6168E-6
	6.00000	18.00000	29.43000	-0.69742	29.215	-263.03E-6	-0.42210	3.4675E-6
	8.00000	18.00000	29.43000	-0.61097	29.215	-211.40E-6	-0.36996	3.0401E-6
	10.00000	18.00000	29.43000	-0.49353	29.215	-146.42E-6	-0.30053	2.4708E-6
	12.00000	18.00000	29.43000	-0.37362	29.215	-91.742E-6	-0.23253	1.9128E-6
	14.00000	18.00000	29.43000	-0.26982	29.215	-55.243E-6	-0.17619	1.4501E-6
	16.00000	18.00000	29.43000	-0.18844	29.215	-33.294E-6	-0.13319	1.0966E-6
	18.00000	18.00000	29.43000	-0.12827	29.215	-20.470E-6	-0.10141	0.0
	20.00000	18.00000	29.43000	-0.085313	29.215	-12.925E-6	-0.078114	0.0
	22.00000	18.00000	29.43000	-0.055279	29.215	-8.3897E-6	-0.060957	0.0
	24.00000	18.00000	29.43000	-0.034557	29.215	-5.5920E-6	-0.048201	0.0
	26.00000	18.00000	29.43000	-0.020385	29.215	-3.8199E-6	-0.038604	0.0
	28.00000	18.00000	29.43000	-0.010765	29.215	-2.6687E-6	-0.031292	0.0
	30.00000	18.00000	29.43000	-0.0042874	29.215	-1.9030E-6	-0.025650	0.0
	-20.00000	20.00000	29.43000	-0.0068985	29.215	-2.2129E-6	-0.028033	0.0
	-18.00000	20.00000	29.43000	-0.014237	29.215	-3.0821E-6	-0.034042	0.0
	-16.00000	20.00000	29.43000	-0.024801	29.215	-4.3643E-6	-0.041705	0.0
	-14.00000	20.00000	29.43000	-0.039816	29.215	-6.2854E-6	-0.051536	0.0
	-12.00000	20.00000	29.43000	-0.060837	29.215	-9.2032E-6	-0.064200	0.0
	-10.00000	20.00000	29.43000	-0.089687	29.215	-13.674E-6	-0.080504	0.0
	-8.00000	20.00000	29.43000	-0.12816	29.215	-20.522E-6	-0.10132	0.0
	-6.00000	20.00000	29.43000	-0.17733	29.215	-30.808E-6	-0.12729	1.0481E-6
	-4.00000	20.00000	29.43000	-0.23625	29.215	-45.471E-6	-0.15827	1.3028E-6
	-2.00000	20.00000	29.43000	-0.30030	29.215	-64.261E-6	-0.19220	1.5816E-6
	0.00000	20.00000	29.43000	-0.36023	29.215	-84.280E-6	-0.22437	1.8459E-6
	2.00000	20.00000	29.43000	-0.40384	29.215	-100.06E-6	-0.24801	2.0400E-6
	4.00000	20.00000	29.43000	-0.42045	29.215	-106.37E-6	-0.25708	2.1145E-6
	6.00000	20.00000	29.43000	-0.40564	29.215	-101.01E-6	-0.24905	2.0485E-6
	8.00000	20.00000	29.43000	-0.36322	29.215	-85.704E-6	-0.22605	1.8596E-6
	10.00000	20.00000	29.43000	-0.30365	29.215	-65.621E-6	-0.19401	1.5965E-6
	12.00000	20.00000	29.43000	-0.23933	29.215	-46.498E-6	-0.15986	1.3159E-6
	14.00000	20.00000	29.43000	-0.17983	29.215	-31.486E-6	-0.12855	1.0584E-6
	16.00000	20.00000	29.43000	-0.13004	29.215	-20.940E-6	-0.10224	0.0
	18.00000	20.00000	29.43000	-0.091022	29.215	-13.925E-6	-0.081160	0.0
	20.00000	20.00000	29.43000	-0.061757	29.215	-9.3518E-6	-0.064659	0.0
	22.00000	20.00000	29.43000	-0.040436	29.215	-6.3740E-6	-0.051855	0.0
	24.00000	20.00000	29.43000	-0.025214	29.215	-4.4176E-6	-0.041926	0.0
	26.00000	20.00000	29.43000	-0.014510	29.215	-3.1146E-6	-0.034197	0.0
	28.00000	20.00000	29.43000	-0.0070781	29.215	-2.2330E-6	-0.028141	0.0
	30.00000	20.00000	29.43000	-0.0019852	29.215	-1.6269E-6	-0.023360	0.0
	-20.00000	22.00000	29.43000	-0.0036552	29.215	-1.8278E-6	-0.025019	0.0
	-18.00000	22.00000	29.43000	-0.0091690	29.215	-2.4812E-6	-0.029933	0.0
	-16.00000	22.00000	29.43000	-0.016938	29.215	-3.4076E-6	-0.036029	0.0
	-14.00000	22.00000	29.43000	-0.027691	29.215	-4.7305E-6	-0.043600	0.0
	-12.00000	22.00000	29.43000	-0.042274	29.215	-6.6263E-6	-0.052981	0.0
	-10.00000	22.00000	29.43000	-0.061548	29.215	-9.3337E-6	-0.064510	0.0
	-8.00000	22.00000	29.43000	-0.086165	29.215	-13.143E-6	-0.078440	0.0
	-6.00000	22.00000	29.43000	-0.11615	29.215	-18.326E-6	-0.094756	0.0
	-4.00000	22.00000	29.43000	-0.15029	29.215	-24.956E-6	-0.11290	0.0
	-2.00000	22.00000	29.43000	-0.18563	29.215	-32.607E-6	-0.13145	1.0823E-6
	0.00000	22.00000	29.43000	-0.21735	29.215	-40.110E-6	-0.14803	1.2186E-6
	2.00000	22.00000	29.43000	-0.23978	29.215	-45.747E-6	-0.15973	1.3148E-6
	4.00000	22.00000	29.43000	-0.24818	29.215	-47.945E-6	-0.16411	1.3508E-6
	6.00000	22.00000	29.43000	-0.24064	29.215	-46.036E-6	-0.16018	1.3185E-6
	8.00000	22.00000	29.43000	-0.21884	29.215	-40.574E-6	-0.14879	1.2248E-6
	10.00000	22.00000	29.43000	-0.18738	29.215	-33.100E-6	-0.13234	1.0896E-6
	12.00000	22.00000	29.43000	-0.15201	29.215	-25.379E-6	-0.11375	0.0
	14.00000	22.00000	29.43000	-0.11763	29.215	-18.643E-6	-0.095489	0.0
	16.00000	22.00000	29.43000	-0.087351	29.215	-13.362E-6	-0.079025	0.0
	18.00000	22.00000	29.43000	-0.062441	29.215	-9.4790E-6	-0.064957	0.0
	20.00000	22.00000	29.43000	-0.042921	29.215	-6.7203E-6	-0.053314	0.0
	22.00000	22.00000	29.43000	-0.028148	29.215	-4.7907E-6	-0.043844	0.0
	24.00000	22.00000	29.43000	-0.017254	29.215	-3.4460E-6	-0.036206	0.0
	26.00000	22.00000	29.43000	-0.0093849	29.215	-2.5059E-6	-0.030061	0.0
	28.00000	22.00000	29.43000	-0.0038016	29.215	-1.8437E-6	-0.025112	0.0
	30.00000	22.00000	29.43000	88.746E-6	29.215	-1.3728E-6	-0.021114	0.0
	-20.00000	24.00000	29.43000	-903.13E-6	29.215	-1.4953E-6	-0.022205	0.0
	-18.00000	24.00000	29.43000	-0.0049413	29.215	-1.9800E-6	-0.026186	0.0
	-16.00000	24.00000	29.43000	-0.010522	29.215	-2.6415E-6	-0.030997	0.0
	-14.00000	24.00000	29.43000	-0.018060	29.215	-3.5448E-6	-0.036793	0.0
	-12.00000	24.00000	29.43000	-0.027990	29.215	-4.7730E-6	-0.043726	0.0
	-10.00000	24.00000	29.43000	-0.040683	29.215	-6.4227E-6	-0.051906	0.0
	-8.00000	24.00000	29.43000	-0.056301	29.215	-8.5872E-6	-0.061344	0.0
	-6.00000	24.00000	29.43000	-0.074576	29.215	-11.314E-6	-0.071854	0.0
	-4.00000	24.00000	29.43000	-0.094562	29.215	-14.536E-6	-0.082942	0.0
	-2.00000	24.00000	29.43000	-0.11447	29.215	-17.987E-6	-0.093720	0.0
	0.00000	24.00000	29.43000	-0.13179	29.215	-21.175E-6	-0.10295	0.0
	2.00000	24.00000	29.43000	-0.14376	29.215	-23.476E-6	-0.10926	0.0
	4.00000	24.00000	29.43000	-0.14818	29.215	-24.353E-6	-0.11159	0.0
	6.00000	24.00000	29.43000	-0.14419	29.215	-23.580E-6	-0.10948	0.0
	8.00000	24.00000	29.43000	-0.13256	29.215	-21.351E-6	-0.10333	0.0
	10.00000	24.00000	29.43000	-0.11542	29.215	-18.188E-6	-0.094187	0.0
	12.00000	24.00000	29.43000	-0.095532	29.215	-14.724E-6	-0.083421	0.0
	14.00000	24.00000	29.43000	-0.075460	29.215	-11.469E-6	-0.072293	0.0
	16.00000	24.00000	29.43000	-0.057043	29.215	-8.7046E-6	-0.061718	0.0
	18.00000	24.00000	29.43000	-0.041270	29.215	-6.5072E-6	-0.052209	0.0
	20.00000	24.00000	29.43000	-0.028434	29.215	-4.8318E-6	-0.043964	0.0
	22.00000	24.00000	29.43000	-0.018386	29.215	-3.5850E-6	-0.036976	0.0
	24.00000	24.00000	29.43000	-0.010756	29.215	-2.6687E-6	-0.031136	0.0
	26.00000	24.00000	29.43000	-0.0051068	29.215	-1.9983E-6	-0.026290	0.0
	28.00000	24.00000	29.43000	-0.0010186	29.215	-1.5076E-6	-0.022284	0.0
	30.00000	24.00000	29.43000	0.0018717	29.215	-1.1469E-6	-0.018972	0.0
	-20.00000	26.00000	29.43000	0.0013402	29.215	-1.2154E-6	-0.019634	0.0
	-18.00000	26.00000	29.43000	-0.0015452	29.215	-1.5721E-6	-0.022840	0.0
	-16.00000	26.00000	29.43000	-0.0054677	29.215	-2.0417E-6	-0.026621	0.0
	-14.00000	26.00000	29.43000	-0.010655	29.215	-2.6572E-6	-0.031051	0.0
	-12.00000	26.00000	29.43000	-0.017318	29.215	-3.4559E-6	-0.036185	0.0
	-10.00000	26.00000	29.43000	-0.025593	29.215	-4.4742E-6	-0.042035	0.0
	-8.00000	26.00000	29.43000	-0.035458	29.215	-5.7356E-6	-0.048529	0.0

Name	Location X [m]	Location Y [m]	Z[Level] [mOD]	Displacement Z [mm]	Calc Level [mOD]	Stresses Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	-6.00000	26.00000	29.43000	-0.046627	29.215	-7.2315E-6	-0.055474	0.0
	-4.00000	26.00000	29.43000	-0.058449	29.215	-8.8953E-6	-0.062509	0.0
	-2.00000	26.00000	29.43000	-0.069879	29.215	-10.582E-6	-0.069092	0.0
	0.00000	26.00000	29.43000	-0.079576	29.215	-12.071E-6	-0.074550	0.0
	2.00000	26.00000	29.43000	-0.086158	29.215	-13.113E-6	-0.078200	0.0
	4.00000	26.00000	29.43000	-0.088566	29.215	-13.502E-6	-0.079523	0.0
	6.00000	26.00000	29.43000	-0.086388	29.215	-13.155E-6	-0.078314	0.0
	8.00000	26.00000	29.43000	-0.079990	29.215	-12.146E-6	-0.074755	0.0
	10.00000	26.00000	29.43000	-0.070403	29.215	-10.671E-6	-0.069353	0.0
	12.00000	26.00000	29.43000	-0.059005	29.215	-8.9847E-6	-0.062789	0.0
	14.00000	26.00000	29.43000	-0.047155	29.215	-7.3106E-6	-0.055745	0.0
	16.00000	26.00000	29.43000	-0.035920	29.215	-5.8001E-6	-0.048772	0.0
	18.00000	26.00000	29.43000	-0.025974	29.215	-4.5238E-6	-0.042241	0.0
	20.00000	26.00000	29.43000	-0.017619	29.215	-3.4927E-6	-0.036355	0.0
	22.00000	26.00000	29.43000	-0.010884	29.215	-2.6837E-6	-0.031187	0.0
	24.00000	26.00000	29.43000	-0.0056378	29.215	-2.0606E-6	-0.026728	0.0
	26.00000	26.00000	29.43000	-0.0016690	29.215	-1.5854E-6	-0.022924	0.0
	28.00000	26.00000	29.43000	0.0012515	29.215	-1.2248E-6	-0.019699	0.0
	30.00000	26.00000	29.43000	0.0033394	29.215	0.0	-0.016975	0.0
	-20.00000	28.00000	29.43000	0.0031005	29.215	0.0	-0.017322	0.0
	-18.00000	28.00000	29.43000	0.0010906	29.215	-1.2455E-6	-0.019897	0.0
	-16.00000	28.00000	29.43000	-0.0016087	29.215	-1.5784E-6	-0.022865	0.0
	-14.00000	28.00000	29.43000	-0.0051177	29.215	-1.9989E-6	-0.026256	0.0
	-12.00000	28.00000	29.43000	-0.0095309	29.215	-2.5228E-6	-0.030078	0.0
	-10.00000	28.00000	29.43000	-0.014881	29.215	-3.1616E-6	-0.034304	0.0
	-8.00000	28.00000	29.43000	-0.021096	29.215	-3.9164E-6	-0.038848	0.0
	-6.00000	28.00000	29.43000	-0.027944	29.215	-4.7693E-6	-0.043551	0.0
	-4.00000	28.00000	29.43000	-0.035005	29.215	-5.6745E-6	-0.048164	0.0
	-2.00000	28.00000	29.43000	-0.041672	29.215	-6.5539E-6	-0.052357	0.0
	0.00000	28.00000	29.43000	-0.047218	29.215	-7.3041E-6	-0.055749	0.0
	2.00000	28.00000	29.43000	-0.050929	29.215	-7.8157E-6	-0.057977	0.0
	4.00000	28.00000	29.43000	-0.052276	29.215	-8.0039E-6	-0.058775	0.0
	6.00000	28.00000	29.43000	-0.051054	29.215	-7.8349E-6	-0.058041	0.0
	8.00000	28.00000	29.43000	-0.047447	29.215	-7.3385E-6	-0.055866	0.0
	10.00000	28.00000	29.43000	-0.041969	29.215	-6.5970E-6	-0.052510	0.0
	12.00000	28.00000	29.43000	-0.035329	29.215	-5.7196E-6	-0.048335	0.0
	14.00000	28.00000	29.43000	-0.028262	29.215	-4.8115E-6	-0.043723	0.0
	16.00000	28.00000	29.43000	-0.021384	29.215	-3.9528E-6	-0.039008	0.0
	18.00000	28.00000	29.43000	-0.015128	29.215	-3.1912E-6	-0.034446	0.0
	20.00000	28.00000	29.43000	-0.0097320	29.215	-2.5459E-6	-0.030200	0.0
	22.00000	28.00000	29.43000	-0.0052761	29.215	-2.0165E-6	-0.026357	0.0
	24.00000	28.00000	29.43000	-0.0017298	29.215	-1.5915E-6	-0.022947	0.0
	26.00000	28.00000	29.43000	999.94E-6	29.215	-1.2551E-6	-0.019963	0.0
	28.00000	28.00000	29.43000	0.0030339	29.215	0.0	-0.017375	0.0
	30.00000	28.00000	29.43000	0.0044968	29.215	0.0	-0.015144	0.0
	-20.00000	30.00000	29.43000	0.0044286	29.215	0.0	-0.015268	0.0
	-18.00000	30.00000	29.43000	0.0030684	29.215	0.0	-0.017334	0.0
	-16.00000	30.00000	29.43000	0.0012532	29.215	-1.2234E-6	-0.019666	0.0
	-14.00000	30.00000	29.43000	-0.0010783	29.215	-1.5124E-6	-0.022272	0.0
	-12.00000	30.00000	29.43000	-0.0039633	29.215	-1.8599E-6	-0.025138	0.0
	-10.00000	30.00000	29.43000	-0.0073946	29.215	-2.2678E-6	-0.028226	0.0
	-8.00000	30.00000	29.43000	-0.011297	29.215	-2.7314E-6	-0.031460	0.0
	-6.00000	30.00000	29.43000	-0.015506	29.215	-3.2351E-6	-0.034718	0.0
	-4.00000	30.00000	29.43000	-0.019756	29.215	-3.7501E-6	-0.037834	0.0
	-2.00000	30.00000	29.43000	-0.023694	29.215	-4.2342E-6	-0.040600	0.0
	0.00000	30.00000	29.43000	-0.026920	29.215	-4.6360E-6	-0.042796	0.0
	2.00000	30.00000	29.43000	-0.029054	29.215	-4.9048E-6	-0.044219	0.0
	4.00000	30.00000	29.43000	-0.029824	29.215	-5.0025E-6	-0.044724	0.0
	6.00000	30.00000	29.43000	-0.029124	29.215	-4.9142E-6	-0.044257	0.0
	8.00000	30.00000	29.43000	-0.027049	29.215	-4.6531E-6	-0.042867	0.0
	10.00000	30.00000	29.43000	-0.023866	29.215	-4.2562E-6	-0.040695	0.0
	12.00000	30.00000	29.43000	-0.019948	29.215	-3.7741E-6	-0.037941	0.0
	14.00000	30.00000	29.43000	-0.015699	29.215	-3.2585E-6	-0.034830	0.0
	16.00000	30.00000	29.43000	-0.011478	29.215	-2.7525E-6	-0.031568	0.0
	18.00000	30.00000	29.43000	-0.0075535	29.215	-2.2858E-6	-0.028325	0.0
	20.00000	30.00000	29.43000	-0.0040969	29.215	-1.8746E-6	-0.025226	0.0
	22.00000	30.00000	29.43000	-0.0011866	29.215	-1.5240E-6	-0.022347	0.0
	24.00000	30.00000	29.43000	0.0011680	29.215	-1.2324E-6	-0.019729	0.0
	26.00000	30.00000	29.43000	0.0030031	29.215	0.0	-0.017386	0.0
	28.00000	30.00000	29.43000	0.0043795	29.215	0.0	-0.015311	0.0
	30.00000	30.00000	29.43000	0.0053678	29.215	0.0	-0.013488	0.0
No. 8 Albert Terrace Mews	8.08000	6.15000	34.25000	-10.441	34.031	0.0	0.0	0.0
	9.08000	6.15000	34.25000	-5.8142	34.031	0.0	0.0	0.0
	10.08000	6.15000	34.25000	-3.9323	34.031	0.0	0.0	0.0
	11.08000	6.15000	34.25000	-2.7825	34.031	0.0	0.0	0.0
	12.08000	6.15000	34.25000	-2.0194	34.031	0.0	0.0	0.0
	13.08000	6.15000	34.25000	-1.4908	34.031	0.0	0.0	0.0
	14.08000	6.15000	34.25000	-1.1144	34.031	0.0	0.0	0.0
	15.08000	6.15000	34.25000	-0.84120	34.031	0.0	0.0	0.0
	16.08000	6.15000	34.25000	-0.63985	34.031	0.0	0.0	0.0
	17.08000	6.15000	34.25000	-0.48974	34.031	0.0	0.0	0.0
	18.08000	6.15000	34.25000	-0.37672	34.031	0.0	0.0	0.0


Settlement Contours : Grid 1 at 29.4300m
40.00
30.00
20.00
10.00
.0
-10.00
-20.00
Y [m]
-30.00
-10.00
10.00
30.00
X [m]
0
-17.00
-16.00
-15.00
-14.00
-13.00
-12.00
-11.00
-10.00
-9.000
-8.000
-7.000
-6.000
-5.000
-4.000
-3.000
-2.000
-1.000
0
Scale x 1:613 y 1:613
Contour Interval: 1mm


Displacement Lines
10.44
9.81
9.93
SZ1 : Soil Zone 1
L1 : Proposed Basement Excavation (including lowering of ground floor)
Z
X
Y

Analysis Options

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Maximum allowable ratio between values of E: 1.5
Horizontal rigid boundary level: -15.00 [m OD]
Stiffness for horizontal displacement calculations: Weighted average
Using legacy heave correction factor: No
Displacements at load centroids: Yes

Soil ProfilesSoil Profile 1

Layer	Level at top	Number of intermediate displacement levels	Youngs Modulus Top	Youngs Modulus Btm	Poissons ratio	Non-linear curve
	[mOD]		[kN/m²]	[kN/m²]		
1	35.000	5	7680.0	7680.0	0.20000	None
2	32.500	5	16000.	24800.	0.20000	None
3	29.000	5	24800.	33600.	0.20000	None
4	25.500	5	33600.	42400.	0.20000	None
5	22.000	5	42400.	51200.	0.20000	None
6	18.500	5	51200.	60000.	0.20000	None
7	15.000	10	60000.	2.5000E+6	0.20000	None

Soil Zones

Zone	Name	X coordinates min [m]	X coordinates max [m]	Y coordinates min [m]	Y coordinates max [m]	Profile
1	Soil Zone 1	-20.00000	30.00000	-20.00000	30.00000	Soil Profile 1

Load Data

Load ref.	Name	Shape	Orientation of Plane	Centre of load (Global) X [m]	Y [m]	Z (level) [m]	Load position Angle of local x from [Degrees]	Width x or Radius [m]	Length y [m]	Polygon Coordinates [m]	Rectangle tolerance [%]	Number of rectangles	Load value Normal (local z) [kN/m²]	Tangential (local x) [kN/m²]	Tangential (local y) [kN/m²]
1	UDL at basement level	Polygonal	Horizontal	N/A	N/A	29.43000	N/A	N/A	N/A	(0,0) (3,0) (4.79,0.29) (8.08,0.8) (8.08,11.5) (4.79,10.9) (3,10.5) (0,11.8) (0,0)	10.000	3	10.000	N/A	N/A
2	Underpinning load 1	Rectangular	Horizontal	1.50000	0.00000	29.43000	0.0	3.0000	0.50000	N/A	N/A	1	110.67	0.0	0.0
3	Underpinning load 2	Rectangular	Horizontal	3.90000	0.14000	29.43000	9.2000	1.8200	0.50000	N/A	N/A	1	182.42	0.0	0.0
4	Underpinning load 3	Rectangular	Horizontal	6.43000	0.55000	29.43000	9.2000	3.3700	0.50000	N/A	N/A	1	47.480	0.0	0.0
5	Underpinning load 4	Rectangular	Horizontal	8.08000	6.15000	29.43000	0.0	0.50000	10.700	N/A	N/A	1	28.040	0.0	0.0
6	Underpinning load 5	Rectangular	Horizontal	0.00000	5.90000	29.43000	0.0	0.50000	11.800	N/A	N/A	1	19.660	0.0	0.0
7	Underpinning load 6	Rectangular	Horizontal	1.50000	11.15000	29.43000	-23.420	3.2800	0.50000	N/A	N/A	1	97.560	0.0	0.0
8	Underpinning load 7	Rectangular	Horizontal	3.90000	10.68000	29.43000	11.240	1.8200	0.50000	N/A	N/A	1	175.82	0.0	0.0
9	Underpinning load 8	Rectangular	Horizontal	6.43000	11.19000	29.43000	11.240	3.3700	0.50000	N/A	N/A	1	47.480	0.0	0.0
10	Proposed Basement Excavation (including lowering of ground floor)	Polygonal	Horizontal	N/A	N/A	29.43000	N/A	N/A	N/A	(0,0) (3,0) (4.79,0.29) (8.08,0.8) (8.08,11.5) (4.79,10.9) (3,10.5) (0,11.8) (0,0)	10.000	3	-82.650	N/A	N/A

Polygonal Loads' Rectangles

No.	Centre of load X [m]	Centre of load Y [m]	Angle of local x from global X [Degrees]	Width x [m]	Depth y [m]
Load 1 : UDL at basement level					
(Edge 1 optimal)					
1	1.50000	5.57250	0.0	3.0000	11.145
2	3.89500	5.41250	0.0	1.7900	10.535
3	6.43500	5.86500	0.0	3.2900	10.640
Load 10 : Proposed Basement Excavation (including lowering of ground floor)					
(Edge 1 optimal)					
1	1.50000	5.57250	0.0	3.0000	11.145
2	3.89500	5.41250	0.0	1.7900	10.535
3	6.43500	5.86500	0.0	3.2900	10.640

Displacement Data

Ref.	Type	Name	Direction of Extrusion	Line/Line for extrusion First point X [m]	First point Y [m]	First point Z(level) [m]	Second point X [m]	Second point Y [m]	Second point Z(level) [m]	No. of intrvls across extrusion/line	Extrusion Depth [m]	No. of intrvls along extrusion	Calculate	Show Detailed results
1	Grid	Proposed Basement Level	Global X	-20.00000	-20.00000	29.43000	N/A	30.00000	29.43000	25	50.00000	25	Yes	Yes
2	Line	No. 8 Albert Terrace Mews	N/A	8.08000	6.15000	34.25000	18.08000	6.15000	34.25000	10	N/A	N/A	Yes	Yes

RESULTS FOR GRIDS

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Horizontal rigid boundary level: -15.00 [m OD]

The maximum displacement difference between the Boussinesq method (-7.3930mm) and the Mindlin method (-4.6323mm) occurs at point X = 8.08000m, Y = 6.15000m, level = 34.250mOD, and is 2.7607mm.

Name	Location X [m]	Location Y [m]	Displacement Z[Level] [mOD]	Displacement Z [mm]	Stresses Calc Level [mOD]	Stresses Vert Stress [kN/m²]	Stresses Sum Princ [kN/m²]	Stresses Vert Strain [-]
UDL at basement level	3.98649	5.65795	29.43000	-14.602	29.215	-72.643	-166.42	-0.0022217
Underpinning load 1	1.50000	0.00000	29.43000	-2.5584	29.215	59.160	63.420	0.0024039
Underpinning load 2	3.90000	0.14000	29.43000	-1.1721	29.215	121.98	153.11	0.0047720
Underpinning load 3	6.43000	0.55000	29.43000	-5.3436	29.215	3.5780	-20.843	348.88E-6
Underpinning load 4	8.08000	6.15000	29.43000	-7.3863	29.215	-12.138	-47.442	-209.30E-6
Underpinning load 5	0.00000	5.90000	29.43000	-7.7331	29.215	-19.366	-58.430	-476.30E-6
Underpinning load 6	1.50000	11.15000	29.43000	-2.9383	29.215	48.940	48.151	0.0020242
Underpinning load 7	3.90000	10.68000	29.43000	-2.2963	29.215	115.09	139.52	0.0045433
Underpinning load 8	6.43000	11.19000	29.43000	-4.8842	29.215	5.7402	-17.363	427.16E-6
Proposed Basement Excavation (including	3.98649	5.65795	29.43000	-14.602	29.215	-72.643	-166.42	-0.0022217

Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]	
lowering of ground floor) Proposed Basement Level	-20.00000	-20.00000	29.43000	0.0038125	29.215	0.0	-0.010171	0.0	
	-18.00000	-20.00000	29.43000	0.0031007	29.215	0.0	-0.011451	0.0	
	-16.00000	-20.00000	29.43000	0.0021521	29.215	0.0	-0.012873	0.0	
	-14.00000	-20.00000	29.43000	943.06E-6	29.215	0.0	-0.014435	0.0	
	-12.00000	-20.00000	29.43000	-535.11E-6	29.215	-1.0767E-6	-0.016121	0.0	
	-10.00000	-20.00000	29.43000	-0.0022671	29.215	-1.2852E-6	-0.017901	0.0	
	-8.00000	-20.00000	29.43000	-0.0042041	29.215	-1.5146E-6	-0.019728	0.0	
	-6.00000	-20.00000	29.43000	-0.0062567	29.215	-1.7559E-6	-0.021530	0.0	
	-4.00000	-20.00000	29.43000	-0.0082942	29.215	-1.9950E-6	-0.023220	0.0	
	-2.00000	-20.00000	29.43000	-0.010152	29.215	-2.2136E-6	-0.024694	0.0	
	0.00000	-20.00000	29.43000	-0.011654	29.215	-2.3910E-6	-0.025847	0.0	
	2.00000	-20.00000	29.43000	-0.012638	29.215	-2.5078E-6	-0.026586	0.0	
	4.00000	-20.00000	29.43000	-0.012988	29.215	-2.5497E-6	-0.026847	0.0	
	6.00000	-20.00000	29.43000	-0.012662	29.215	-2.5115E-6	-0.026604	0.0	
	8.00000	-20.00000	29.43000	-0.011699	29.215	-2.3978E-6	-0.025881	0.0	
	10.00000	-20.00000	29.43000	-0.010211	29.215	-2.2223E-6	-0.024740	0.0	
	12.00000	-20.00000	29.43000	-0.0083597	29.215	-2.0044E-6	-0.023275	0.0	
	14.00000	-20.00000	29.43000	-0.0063222	29.215	-1.7650E-6	-0.021589	0.0	
	16.00000	-20.00000	29.43000	-0.0042647	29.215	-1.5230E-6	-0.019788	0.0	
	18.00000	-20.00000	29.43000	-0.0023200	29.215	-1.2926E-6	-0.017961	0.0	
	20.00000	-20.00000	29.43000	-578.97E-6	29.215	-1.0830E-6	-0.016178	0.0	
	22.00000	-20.00000	29.43000	908.31E-6	29.215	0.0	-0.014488	0.0	
	24.00000	-20.00000	29.43000	0.0021259	29.215	0.0	-0.012923	0.0	
	26.00000	-20.00000	29.43000	0.0030820	29.215	0.0	-0.011497	0.0	
	28.00000	-20.00000	29.43000	0.0038004	29.215	0.0	-0.010213	0.0	
	30.00000	-20.00000	29.43000	0.0043121	29.215	0.0	-0.0090685	0.0	
	-20.00000	-18.00000	29.43000	0.0030494	29.215	0.0	-0.011541	0.0	
	-18.00000	-18.00000	29.43000	0.0019656	29.215	0.0	-0.013135	0.0	
	-16.00000	-18.00000	29.43000	521.85E-6	29.215	0.0	-0.014941	0.0	
	-14.00000	-18.00000	29.43000	-0.0013307	29.215	-1.1735E-6	-0.016965	0.0	
	-12.00000	-18.00000	29.43000	-0.0036218	29.215	-1.4466E-6	-0.019197	0.0	
	-10.00000	-18.00000	29.43000	-0.0063454	29.215	-1.7673E-6	-0.021608	0.0	
	-8.00000	-18.00000	29.43000	-0.0094413	29.215	-2.1316E-6	-0.024136	0.0	
	-6.00000	-18.00000	29.43000	-0.012778	29.215	-2.5268E-6	-0.026687	0.0	
	-4.00000	-18.00000	29.43000	-0.016144	29.215	-2.9302E-6	-0.029129	0.0	
	-2.00000	-18.00000	29.43000	-0.019259	29.215	-3.3084E-6	-0.031297	0.0	
	0.00000	-18.00000	29.43000	-0.021807	29.215	-3.6218E-6	-0.033019	0.0	
	2.00000	-18.00000	29.43000	-0.023490	29.215	-3.8313E-6	-0.034134	0.0	
	4.00000	-18.00000	29.43000	-0.024093	29.215	-3.9075E-6	-0.034530	0.0	
	6.00000	-18.00000	29.43000	-0.023534	29.215	-3.8390E-6	-0.034163	0.0	
	8.00000	-18.00000	29.43000	-0.021887	29.215	-3.6355E-6	-0.033072	0.0	
	10.00000	-18.00000	29.43000	-0.019363	29.215	-3.3253E-6	-0.031368	0.0	
	12.00000	-18.00000	29.43000	-0.016256	29.215	-2.9476E-6	-0.029210	0.0	
	14.00000	-18.00000	29.43000	-0.012888	29.215	-2.5430E-6	-0.026772	0.0	
	16.00000	-18.00000	29.43000	-0.0095407	29.215	-2.1456E-6	-0.024220	0.0	
	18.00000	-18.00000	29.43000	-0.0064304	29.215	-1.7790E-6	-0.021688	0.0	
	20.00000	-18.00000	29.43000	-0.0036913	29.215	-1.4561E-6	-0.019272	0.0	
	22.00000	-18.00000	29.43000	-0.0013854	29.215	-1.1812E-6	-0.017034	0.0	
	24.00000	-18.00000	29.43000	480.41E-6	29.215	0.0	-0.015004	0.0	
	26.00000	-18.00000	29.43000	0.0019355	29.215	0.0	-0.013192	0.0	
	28.00000	-18.00000	29.43000	0.0030288	29.215	0.0	-0.011592	0.0	
	30.00000	-18.00000	29.43000	0.0038164	29.215	0.0	-0.010190	0.0	
	-20.00000	-16.00000	29.43000	0.0020019	29.215	0.0	-0.013093	0.0	
	-18.00000	-16.00000	29.43000	407.99E-6	29.215	0.0	-0.015081	0.0	
	-16.00000	-16.00000	29.43000	-0.0017317	29.215	-1.2222E-6	-0.017381	0.0	
	-14.00000	-16.00000	29.43000	-0.0045133	29.215	-1.5524E-6	-0.020017	0.0	
	-12.00000	-16.00000	29.43000	-0.0080121	29.215	-1.9643E-6	-0.022997	0.0	
	-10.00000	-16.00000	29.43000	-0.012254	29.215	-2.4665E-6	-0.026300	0.0	
	-8.00000	-16.00000	29.43000	-0.017180	29.215	-3.0592E-6	-0.029858	0.0	
	-6.00000	-16.00000	29.43000	-0.022604	29.215	-3.7273E-6	-0.033545	0.0	
	-4.00000	-16.00000	29.43000	-0.028191	29.215	-4.4337E-6	-0.037163	0.0	
	-2.00000	-16.00000	29.43000	-0.033459	29.215	-5.1173E-6	-0.040451	0.0	
	0.00000	-16.00000	29.43000	-0.037835	29.215	-5.6986E-6	-0.043110	0.0	
	2.00000	-16.00000	29.43000	-0.040758	29.215	-6.0947E-6	-0.044856	0.0	
	4.00000	-16.00000	29.43000	-0.041813	29.215	-6.2414E-6	-0.045481	0.0	
	6.00000	-16.00000	29.43000	-0.040841	29.215	-6.1126E-6	-0.044905	0.0	
	8.00000	-16.00000	29.43000	-0.037983	29.215	-5.7291E-6	-0.043199	0.0	
	10.00000	-16.00000	29.43000	-0.033645	29.215	-5.1531E-6	-0.040565	0.0	
	12.00000	-16.00000	29.43000	-0.028386	29.215	-4.4683E-6	-0.037289	0.0	
	14.00000	-16.00000	29.43000	-0.022788	29.215	-3.7572E-6	-0.033671	0.0	
	16.00000	-16.00000	29.43000	-0.017341	29.215	-3.0834E-6	-0.029978	0.0	
	18.00000	-16.00000	29.43000	-0.012388	29.215	-2.4854E-6	-0.026410	0.0	
	20.00000	-16.00000	29.43000	-0.0081194	29.215	-1.9788E-6	-0.023097	0.0	
	22.00000	-16.00000	29.43000	-0.0045966	29.215	-1.5636E-6	-0.020107	0.0	
	24.00000	-16.00000	29.43000	-0.0017945	29.215	-1.2309E-6	-0.017461	0.0	
	26.00000	-16.00000	29.43000	362.14E-6	29.215	0.0	-0.015152	0.0	
	28.00000	-16.00000	29.43000	0.0019698	29.215	0.0	-0.013156	0.0	
	30.00000	-16.00000	29.43000	0.0031279	29.215	0.0	-0.011440	0.0	
	-20.00000	-14.00000	29.43000	624.59E-6	29.215	0.0	-0.014837	0.0	
	-18.00000	-14.00000	29.43000	-0.0016552	29.215	-1.2134E-6	-0.017313	0.0	
	-16.00000	-14.00000	29.43000	-0.0047564	29.215	-1.5815E-6	-0.020243	0.0	
	-14.00000	-14.00000	29.43000	-0.0088611	29.215	-2.0650E-6	-0.023690	0.0	
	-12.00000	-14.00000	29.43000	-0.014138	29.215	-2.6933E-6	-0.027697	0.0	
	-10.00000	-14.00000	29.43000	-0.020694	29.215	-3.4938E-6	-0.032274	0.0	
	-8.00000	-14.00000	29.43000	-0.028511	29.215	-4.4832E-6	-0.037366	0.0	
	-6.00000	-14.00000	29.43000	-0.037354	29.215	-5.6513E-6	-0.042816	0.0	
	-4.00000	-14.00000	29.43000	-0.046702	29.215	-6.9425E-6	-0.048335	0.0	
	-2.00000	-14.00000	29.43000	-0.055725	29.215	-8.2422E-6	-0.053495	0.0	
	0.00000	-14.00000	29.43000	-0.063364	29.215	-9.3834E-6	-0.057767	0.0	
	2.00000	-14.00000	29.43000	-0.068540	29.215	-10.181E-6	-0.060623	0.0	
	4.00000	-14.00000	29.43000	-0.070427	29.215	-10.483E-6	-0.061658	0.0	
	6.00000	-14.00000	29.43000	-0.068701	29.215	-10.227E-6	-0.060714	0.0	
	8.00000	-14.00000	29.43000	-0.063645	29.215	-9.4594E-6	-0.057928	0.0	
	10.00000	-14.00000	29.43000	-0.056063	29.215	-8.3252E-6	-0.053692	0.0	
	12.00000	-14.00000	29.43000	-0.047043	29.215	-7.0163E-6	-0.048539	0.0	
	14.00000	-14.00000	29.43000	-0.037661	29.215	-5.7094E-6	-0.043009	0.0	
	16.00000	-14.00000	29.43000	-0.028769	29.215	-4.5261E-6	-0.037540	0.0	
	18.00000	-14.00000	29.43000	-0.020902	29.215	-3.5248E-6	-0.032428	0.0	
	20.00000	-14.00000	29.43000	-0.014300	29.215	-2.7156E-6	-0.027831	0.0	
	22.00000	-14.00000	29.43000	-0.0089847	29.215	-2.0814E-6	-0.023806	0.0	
	24.00000	-14.00000	29.43000	-0.0048486	29.215	-1.5937E-6	-0.020345	0.0	
	26.00000	-14.00000	29.43000	-0.0017224	29.215	-1.2226E-6	-0.017401	0.0	
	28.00000	-14.00000	29.43000	577.09E-6	29.215	0.0	-0.014914	0.0	
	30.00000	-14.00000	29.43000	0.0022217	29.215	0.0	-0.012819	0.0	
	-20.00000	-12.00000	29.43000	-0.0011178	29.215	-1.1490E-6	-0.016771	0.0	
	-18.00000	-12.00000	29.43000	-0.0042980	29.215	-1.5277E-6	-0.019843	0.0	
	-16.00000	-12.00000	29.43000	-0.0086997	29.215	-2.0463E-6	-0.023573	0.0	
	-14.00000	-12.00000	29.43000	-0.014655	29.215	-2.7562E-6	-0.028084	0.0	
	-12.00000	-12.00000	29.43000	-0.022513	29.215	-3.7225E-6	-0.033500	0.0	
	-10.00000	-12.00000	29.43000	-0.032569	29.215	-5.0193E-6	-0.039909	0.0	
	-8.00000	-12.00000	29.43000	-0.044944	29.215	-6.7143E-6	-0.047318	0.0	
	-6.00000	-12.00000	29.43000	-0.059415	29.215	-8.8343E-6	-0.055571	0.0	
	-4.00000	-12.00000	29.43000	-0.075212	29.215	-11.312E-6	-0.064266	0.0	
	-2.00000	-12.00000	29.43000	-0.090911	29.215	-13.934E-6	-0.072696	0.0	
	0.00000	-12.00000	29.43000	-0.10453	29.215	-16.329E-6	-0.079891	0.0	
	2.00000	-12.00000	29.43000	-0.11392	29.215	-18.055E-6	-0.084810	0.0	
	4.00000	-12.00000	29.43000	-0.11738	29.215	-18.735E-6	-0.086627	0.0	
	6.00000	-12.00000	29.43000	-0.11424	29.215	-18.196E-6	-0.085003	0.0	
	8.00000	-12.00000	29.43000	-0.10508	29.215	-16.546E-6	-0.080213	0.0	
	10.00000	-12.00000	29.43000	-0.091543	29.215	-14.149E-6	-0.073062	0.0	
	12.00000	-12.00000	29.43000	-0.075812	29.215	-11.483E-6	-0.064615	0.0	
	14.00000	-12.00000	29.43000	-0.059926	29.215	-8.9531E-6	-0.055875	0.0	
	16.00000	-12.00000	29.43000	-0.045353	29.215	-6.7926E-6	-0.047574	0.0	
	18.00000	-12.00000	29.43000	-0.032885	29.215	-5.0706E-6	-0.040124	0.0	
	20.00000	-12.00000	29.43000	-0.022753	29.215	-3.7568E-6	-0.033680	0.0	
	22.00000	-12.00000	29.43000	-0.014834	29.215	-2.7799E-6	-0.028236	0.0	
	24.00000	-12.00000	29.43000	-0.0088315	29.215	-2.0632E-6	-0.023701	0.0	
	26.00000	-12.00000	29.43000	-0.0043934	29.215	-1.5402E-6	-0.019953	0.0	
	28.00000	-12.00000	29.43000	-0.0011854	29.215	-1.1583E-6	-0.016864	0.0	
	30.00000	-12.00000	29.43000	0.0010815	29.215	0.0	-0.014320	0.0	
	-20.00000	-10.00000	29.43000	-0.0032387	29.215	-1.4027E-6	-0.018878	0.0	
	-18.00000	-10.00000	29.43000	-0.0075669	29.215	-1.9127E-6	-0.022667	0.0	
	-16.00000	-10.00000	29.43000	-0.013681	29.215	-2.6387E-6	-0.027391	0.0	
	-14.00000	-10.00000	29.43000	-0.022164	29.215	-3.6787E-6	-0.033285	0.0	
	-12.00000	-10.00000	29.43000	-0.033696	29.215	-5.1710E-6	-0.040619	0.0	
	-10.00000	-10.00000	29.43000	-0.048965	29.215	-7.2992E-6	-0.049663	0.0	
	-8.00000	-10.00000	29.43000	-0.068481	29.215	-10.277E-6	-0.060610	0.0	
	-6.00000	-10.00000	29.43000	-0.092232	29.215	-14.282E-6	-0.073429	0.0	

Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	-4.00000	-10.00000	29.43000	-0.11922	29.215	-19.314E-6	-0.087636	0.0
	-2.00000	-10.00000	29.43000	-0.14704	29.215	-24.984E-6	-0.10208	0.0
	0.00000	-10.00000	29.43000	-0.17191	29.215	-30.422E-6	-0.11489	0.0
	2.00000	-10.00000	29.43000	-0.18944	29.215	-34.486E-6	-0.12391	1.0200E-6
	4.00000	-10.00000	29.43000	-0.19603	29.215	-36.183E-6	-0.12734	1.0482E-6
	6.00000	-10.00000	29.43000	-0.19015	29.215	-35.005E-6	-0.12439	1.0239E-6
	8.00000	-10.00000	29.43000	-0.17305	29.215	-31.154E-6	-0.11563	0.0
	10.00000	-10.00000	29.43000	-0.14825	29.215	-25.620E-6	-0.10282	0.0
	12.00000	-10.00000	29.43000	-0.12028	29.215	-19.743E-6	-0.088268	0.0
	14.00000	-10.00000	29.43000	-0.093074	29.215	-14.536E-6	-0.073923	0.0
	16.00000	-10.00000	29.43000	-0.069116	29.215	-10.421E-6	-0.060992	0.0
	18.00000	-10.00000	29.43000	-0.049435	29.215	-7.3835E-6	-0.049963	0.0
	20.00000	-10.00000	29.43000	-0.034042	29.215	-5.2230E-6	-0.040860	0.0
	22.00000	-10.00000	29.43000	-0.022418	29.215	-3.7127E-6	-0.033482	0.0
	24.00000	-10.00000	29.43000	-0.013865	29.215	-2.6621E-6	-0.027553	0.0
	26.00000	-10.00000	29.43000	-0.0076991	29.215	-1.9294E-6	-0.022803	0.0
	28.00000	-10.00000	29.43000	-0.0033321	29.215	-1.4148E-6	-0.018992	0.0
	30.00000	-10.00000	29.43000	-292.87E-6	29.215	-1.0501E-6	-0.015923	0.0
	-20.00000	-8.00000	29.43000	-0.0057156	29.215	-1.6949E-6	-0.021121	0.0
	-18.00000	-8.00000	29.43000	-0.011455	29.215	-2.3723E-6	-0.025748	0.0
	-16.00000	-8.00000	29.43000	-0.019746	29.215	-3.3763E-6	-0.031679	0.0
	-14.00000	-8.00000	29.43000	-0.031570	29.215	-4.8864E-6	-0.039330	0.0
	-12.00000	-8.00000	29.43000	-0.048181	29.215	-7.1843E-6	-0.049235	0.0
	-10.00000	-8.00000	29.43000	-0.071038	29.215	-10.700E-6	-0.062039	0.0
	-8.00000	-8.00000	29.43000	-0.10157	29.215	-16.046E-6	-0.078416	0.0
	-6.00000	-8.00000	29.43000	-0.14056	29.215	-23.940E-6	-0.098831	0.0
	-4.00000	-8.00000	29.43000	-0.18715	29.215	-34.846E-6	-0.12301	1.0126E-6
	-2.00000	-8.00000	29.43000	-0.23748	29.215	-48.182E-6	-0.14919	1.2278E-6
	0.00000	-8.00000	29.43000	-0.28424	29.215	-61.677E-6	-0.17363	1.4286E-6
	2.00000	-8.00000	29.43000	-0.31810	29.215	-72.107E-6	-0.19145	1.5750E-6
	4.00000	-8.00000	29.43000	-0.33109	29.215	-76.935E-6	-0.19850	1.6330E-6
	6.00000	-8.00000	29.43000	-0.31979	29.215	-74.567E-6	-0.19286	1.5866E-6
	8.00000	-8.00000	29.43000	-0.28675	29.215	-64.748E-6	-0.17560	1.4447E-6
	10.00000	-8.00000	29.43000	-0.23989	29.215	-50.389E-6	-0.15090	1.2418E-6
	12.00000	-8.00000	29.43000	-0.18903	29.215	-36.027E-6	-0.12423	1.0225E-6
	14.00000	-8.00000	29.43000	-0.14192	29.215	-24.497E-6	-0.099645	0.0
	16.00000	-8.00000	29.43000	-0.10252	29.215	-16.309E-6	-0.078980	0.0
	18.00000	-8.00000	29.43000	-0.071717	29.215	-10.835E-6	-0.062452	0.0
	20.00000	-8.00000	29.43000	-0.048667	29.215	-7.2608E-6	-0.049554	0.0
	22.00000	-8.00000	29.43000	-0.031920	29.215	-4.9340E-6	-0.039583	0.0
	24.00000	-8.00000	29.43000	-0.019997	29.215	-3.4080E-6	-0.031884	0.0
	26.00000	-8.00000	29.43000	-0.011634	29.215	-2.3943E-6	-0.025916	0.0
	28.00000	-8.00000	29.43000	-0.0058415	29.215	-1.7106E-6	-0.021259	0.0
	30.00000	-8.00000	29.43000	-0.0018787	29.215	-1.2421E-6	-0.017596	0.0
	-20.00000	-6.00000	29.43000	-0.0084754	29.215	-2.0194E-6	-0.023435	0.0
	-18.00000	-6.00000	29.43000	-0.015873	29.215	-2.9012E-6	-0.029007	0.0
	-16.00000	-6.00000	29.43000	-0.026808	29.215	-4.2628E-6	-0.036354	0.0
	-14.00000	-6.00000	29.43000	-0.042856	29.215	-6.4170E-6	-0.046162	0.0
	-12.00000	-6.00000	29.43000	-0.066200	29.215	-9.9092E-6	-0.059412	0.0
	-10.00000	-6.00000	29.43000	-0.099700	29.215	-15.695E-6	-0.077465	0.0
	-8.00000	-6.00000	29.43000	-0.14674	29.215	-25.415E-6	-0.10211	0.0
	-6.00000	-6.00000	29.43000	-0.21040	29.215	-41.615E-6	-0.13536	1.1141E-6
	-4.00000	-6.00000	29.43000	-0.29146	29.215	-67.129E-6	-0.17843	1.4679E-6
	-2.00000	-6.00000	29.43000	-0.38468	29.215	-101.77E-6	-0.22928	1.8855E-6
	0.00000	-6.00000	29.43000	-0.47571	29.215	-137.95E-6	-0.27993	2.3013E-6
	2.00000	-6.00000	29.43000	-0.54365	29.215	-165.30E-6	-0.31812	2.6149E-6
	4.00000	-6.00000	29.43000	-0.57050	29.215	-181.25E-6	-0.33429	2.7475E-6
	6.00000	-6.00000	29.43000	-0.54831	29.215	-182.08E-6	-0.32372	2.6602E-6
	8.00000	-6.00000	29.43000	-0.48181	29.215	-155.50E-6	-0.28654	2.3550E-6
	10.00000	-6.00000	29.43000	-0.38959	29.215	-111.13E-6	-0.23376	1.9220E-6
	12.00000	-6.00000	29.43000	-0.29471	29.215	-70.639E-6	-0.18085	1.4877E-6
	14.00000	-6.00000	29.43000	-0.21248	29.215	-42.821E-6	-0.13668	1.1249E-6
	16.00000	-6.00000	29.43000	-0.14811	29.215	-25.869E-6	-0.10292	0.0
	18.00000	-6.00000	29.43000	-0.10065	29.215	-15.899E-6	-0.078023	0.0
	20.00000	-6.00000	29.43000	-0.066865	29.215	-10.017E-6	-0.059828	0.0
	22.00000	-6.00000	29.43000	-0.043330	29.215	-6.4819E-6	-0.046485	0.0
	24.00000	-6.00000	29.43000	-0.027145	29.215	-4.3049E-6	-0.036609	0.0
	26.00000	-6.00000	29.43000	-0.016111	29.215	-2.9298E-6	-0.029212	0.0
	28.00000	-6.00000	29.43000	-0.0086415	29.215	-2.0395E-6	-0.023601	0.0
	30.00000	-6.00000	29.43000	-0.0036227	29.215	-1.4493E-6	-0.019289	0.0
	-20.00000	-4.00000	29.43000	-0.011383	29.215	-2.3625E-6	-0.025725	0.0
	-18.00000	-4.00000	29.43000	-0.020620	29.215	-3.4800E-6	-0.032312	0.0
	-16.00000	-4.00000	29.43000	-0.034583	29.215	-5.2754E-6	-0.041235	0.0
	-14.00000	-4.00000	29.43000	-0.055663	29.215	-8.2618E-6	-0.053565	0.0
	-12.00000	-4.00000	29.43000	-0.087418	29.215	-13.426E-6	-0.070960	0.0
	-10.00000	-4.00000	29.43000	-0.13502	29.215	-22.747E-6	-0.096034	0.0
	-8.00000	-4.00000	29.43000	-0.20560	29.215	-40.320E-6	-0.13290	1.0938E-6
	-6.00000	-4.00000	29.43000	-0.30783	29.215	-74.547E-6	-0.18774	1.5444E-6
	-4.00000	-4.00000	29.43000	-0.44910	29.215	-139.69E-6	-0.26814	2.2041E-6
	-2.00000	-4.00000	29.43000	-0.62646	29.215	-238.56E-6	-0.37603	3.0888E-6
	0.00000	-4.00000	29.43000	-0.81198	29.215	-311.54E-6	-0.49131	4.0357E-6
	2.00000	-4.00000	29.43000	-0.95409	29.215	-326.49E-6	-0.57690	4.7407E-6
	4.00000	-4.00000	29.43000	-1.0117	29.215	-380.87E-6	-0.61723	5.0706E-6
	6.00000	-4.00000	29.43000	-0.97006	29.215	-532.66E-6	-0.61040	5.0068E-6
	8.00000	-4.00000	29.43000	-0.82905	29.215	-478.44E-6	-0.52231	4.2830E-6
	10.00000	-4.00000	29.43000	-0.63658	29.215	-290.58E-6	-0.38961	3.1982E-6
	12.00000	-4.00000	29.43000	-0.45427	29.215	-150.26E-6	-0.27286	2.2425E-6
	14.00000	-4.00000	29.43000	-0.31075	29.215	-76.871E-6	-0.18971	1.5605E-6
	16.00000	-4.00000	29.43000	-0.20745	29.215	-41.004E-6	-0.13399	1.1028E-6
	18.00000	-4.00000	29.43000	-0.13629	29.215	-23.025E-6	-0.096762	0.0
	20.00000	-4.00000	29.43000	-0.088309	29.215	-13.570E-6	-0.071494	0.0
	22.00000	-4.00000	29.43000	-0.056293	29.215	-8.3478E-6	-0.053972	0.0
	24.00000	-4.00000	29.43000	-0.035027	29.215	-5.3307E-6	-0.041552	0.0
	26.00000	-4.00000	29.43000	-0.020930	29.215	-3.5171E-6	-0.032561	0.0
	28.00000	-4.00000	29.43000	-0.011598	29.215	-2.3879E-6	-0.025923	0.0
	30.00000	-4.00000	29.43000	-0.0054374	29.215	-1.6628E-6	-0.020934	0.0
	-20.00000	-2.00000	29.43000	-0.014242	29.215	-2.7022E-6	-0.027867	0.0
	-18.00000	-2.00000	29.43000	-0.025371	29.215	-4.0718E-6	-0.035472	0.0
	-16.00000	-2.00000	29.43000	-0.042548	29.215	-6.3525E-6	-0.046036	0.0
	-14.00000	-2.00000	29.43000	-0.069160	29.215	-10.325E-6	-0.061105	0.0
	-12.00000	-2.00000	29.43000	-0.11059	29.215	-17.629E-6	-0.083268	0.0
	-10.00000	-2.00000	29.43000	-0.17536	29.215	-31.968E-6	-0.11705	0.0
	-8.00000	-2.00000	29.43000	-0.27682	29.215	-62.495E-6	-0.17073	1.4047E-6
	-6.00000	-2.00000	29.43000	-0.43515	29.215	-134.18E-6	-0.26021	2.1390E-6
	-4.00000	-2.00000	29.43000	-0.67774	29.215	-316.66E-6	-0.41593	3.4139E-6
	-2.00000	-2.00000	29.43000	-1.0259	29.215	-596.73E-6	-0.67351	5.5239E-6
	0.00000	-2.00000	29.43000	-1.4275	29.215	0.0029030	-0.87873	7.3893E-6
	2.00000	-2.00000	29.43000	-1.7359	29.215	0.0072852	-0.95769	8.2572E-6
	4.00000	-2.00000	29.43000	-1.8467	29.215	0.0079469	-0.98557	8.5197E-6
	6.00000	-2.00000	29.43000	-1.8162	29.215	-0.0016596	-1.4013	11.473E-6
	8.00000	-2.00000	29.43000	-1.4905	29.215	-0.0025267	-1.1774	9.5834E-6
	10.00000	-2.00000	29.43000	-1.0446	29.215	-981.49E-6	-0.71831	5.8744E-6
	12.00000	-2.00000	29.43000	-0.68433	29.215	-341.17E-6	-0.42315	3.4722E-6
	14.00000	-2.00000	29.43000	-0.43874	29.215	-137.36E-6	-0.26263	2.1587E-6
	16.00000	-2.00000	29.43000	-0.27921	29.215	-63.312E-6	-0.17208	1.4158E-6
	18.00000	-2.00000	29.43000	-0.17703	29.215	-32.312E-6	-0.11797	0.0
	20.00000	-2.00000	29.43000	-0.11177	29.215	-17.816E-6	-0.083947	0.0
	22.00000	-2.00000	29.43000	-0.069989	29.215	-10.438E-6	-0.061616	0.0
	24.00000	-2.00000	29.43000	-0.043125	29.215	-6.4245E-6	-0.046426	0.0
	26.00000	-2.00000	29.43000	-0.025770	29.215	-4.1192E-6	-0.035772	0.0
	28.00000	-2.00000	29.43000	-0.014514	29.215	-2.7341E-6	-0.028101	0.0
	30.00000	-2.00000	29.43000	-0.0072024	29.215	-1.8695E-6	-0.022449	0.0
	-20.00000	0.00000	29.43000	-0.016806	29.215	-3.0097E-6	-0.029717	0.0
	-18.00000	0.00000	29.43000	-0.029701	29.215	-4.6220E-6	-0.038255	0.0
	-16.00000	0.00000	29.43000	-0.049950	29.215	-7.3884E-6	-0.050367	0.0
	-14.00000	0.00000	29.43000	-0.082020	29.215	-12.398E-6	-0.068122	0.0
	-12.00000	0.00000	29.43000	-0.13337	29.215	-22.098E-6	-0.095192	0.0
	-10.00000	0.00000	29.43000	-0.21663	29.215	-42.565E-6	-0.13854	1.1402E-6
	-8.00000	0.00000	29.43000	-0.35361	29.215	-91.079E-6	-0.21249	1.7476E-6
	-6.00000	0.00000	29.43000	-0.58294	29.215	-227.41E-6	-0.35023	2.8766E-6
	-4.00000	0.00000	29.43000	-0.97610	29.215	-730.64E-6	-0.64344	5.2694E-6
	-2.00000	0.00000	29.43000	-1.6736	29.215	-0.0032794	-1.4154	11.509E-6
	0.00000	0.00000	29.43000	-1.9977	29.215	38.046	43.139	0.0015266
	2.00000	0.00000	29.43000	-2.6992	29.215	59.191	63.725	0.0024029
	4.00000	0.00000	29.43000	-0.75649	29.215	120.83	154.11	0.0047071
	6.00000	0.00000	29.43000	-3.9113	29.215	2.9987	0.93752	140.63E-6
	8.00000	0.00000	29.43000	-2.9829	29.215	-0.10967	-5.2878	38.175E-6
	10.00000	0.00000	29.43000	-1.6839	29.215	-0.0041073	-1.4572	11.812E-6
	12.00000	0.00000	29.43000	-0.98136	29.215	-744.59E-6	-0.64770	5.3039E-6
	14.00000	0.00000	29.43000	-0.58703	29.215	-229.35E-6	-0.35252	2.8954E-6
	16.00000	0.00000	29.43000	-0.35669	29.215	-91.849E-6	-0.21412	1.7610E-6

Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]	
	18.00000	0.00000	29.43000	-0.21886	29.215	-42.981E-6	-0.13972	1.1500E-6	
	20.00000	0.00000	29.43000	-0.13494	29.215	-22.343E-6	-0.096059	0.0	
	22.00000	0.00000	29.43000	-0.083105	29.215	-12.547E-6	-0.068761	0.0	
	24.00000	0.00000	29.43000	-0.050691	29.215	-7.4819E-6	-0.050843	0.0	
	26.00000	0.00000	29.43000	-0.030204	29.215	-4.6821E-6	-0.038613	0.0	
	28.00000	0.00000	29.43000	-0.017144	29.215	-3.0492E-6	-0.029991	0.0	
	30.00000	0.00000	29.43000	-0.0087746	29.215	-2.0536E-6	-0.023743	0.0	
	-20.00000	2.00000	29.43000	-0.018814	29.215	-3.2525E-6	-0.031129	0.0	
	-18.00000	2.00000	29.43000	-0.033135	29.215	-5.0657E-6	-0.040410	0.0	
	-16.00000	2.00000	29.43000	-0.055914	29.215	-8.2459E-6	-0.053786	0.0	
	-14.00000	2.00000	29.43000	-0.092585	29.215	-14.171E-6	-0.073797	0.0	
	-12.00000	2.00000	29.43000	-0.15254	29.215	-26.085E-6	-0.10515	0.0	
	-10.00000	2.00000	29.43000	-0.25243	29.215	-52.544E-6	-0.15723	1.2939E-6	
	-8.00000	2.00000	29.43000	-0.42286	29.215	-119.98E-6	-0.25088	2.0627E-6	
	-6.00000	2.00000	29.43000	-0.72326	29.215	-331.89E-6	-0.43961	3.6084E-6	
	-4.00000	2.00000	29.43000	-1.2816	29.215	-0.0012955	-0.89981	7.3554E-6	
	-2.00000	2.00000	29.43000	-2.4461	29.215	-0.011423	-2.6008	20.880E-6	
	0.00000	2.00000	29.43000	-6.4578	29.215	-19.347	-56.117	-494.43E-6	
	2.00000	2.00000	29.43000	-11.588	29.215	-72.585	-160.03	-0.0022715	
	4.00000	2.00000	29.43000	-12.165	29.215	-72.578	-160.71	-0.0022655	
	6.00000	2.00000	29.43000	-11.418	29.215	-72.551	-158.83	-0.0022797	
	8.00000	2.00000	29.43000	-6.5831	29.215	-28.803	-65.099	-888.23E-6	
	10.00000	2.00000	29.43000	-2.4384	29.215	-0.010555	-2.5509	20.512E-6	
	12.00000	2.00000	29.43000	-1.2868	29.215	-0.0012808	-0.90013	7.3587E-6	
	14.00000	2.00000	29.43000	-0.72884	29.215	-332.52E-6	-0.44228	3.6304E-6	
	16.00000	2.00000	29.43000	-0.42718	29.215	-120.90E-6	-0.25306	2.0807E-6	
	18.00000	2.00000	29.43000	-0.25548	29.215	-53.120E-6	-0.15881	1.3069E-6	
	20.00000	2.00000	29.43000	-0.15462	29.215	-26.424E-6	-0.10626	0.0	
	22.00000	2.00000	29.43000	-0.093988	29.215	-14.372E-6	-0.074593	0.0	
	24.00000	2.00000	29.43000	-0.056849	29.215	-8.3669E-6	-0.054361	0.0	
	26.00000	2.00000	29.43000	-0.033756	29.215	-5.1409E-6	-0.040832	0.0	
	28.00000	2.00000	29.43000	-0.019225	29.215	-3.3006E-6	-0.031444	0.0	
	30.00000	2.00000	29.43000	-0.010006	29.215	-2.1979E-6	-0.024726	0.0	
	-20.00000	4.00000	29.43000	-0.020039	29.215	-3.4014E-6	-0.031977	0.0	
	-18.00000	4.00000	29.43000	-0.035246	29.215	-5.3413E-6	-0.041717	0.0	
	-16.00000	4.00000	29.43000	-0.059618	29.215	-8.7875E-6	-0.055886	0.0	
	-14.00000	4.00000	29.43000	-0.099229	29.215	-15.315E-6	-0.077337	0.0	
	-12.00000	4.00000	29.43000	-0.16478	29.215	-28.721E-6	-0.11148	0.0	
	-10.00000	4.00000	29.43000	-0.27572	29.215	-59.325E-6	-0.16943	1.3941E-6	
	-8.00000	4.00000	29.43000	-0.46890	29.215	-140.08E-6	-0.27662	2.2739E-6	
	-6.00000	4.00000	29.43000	-0.81848	29.215	-403.83E-6	-0.50076	4.1091E-6	
	-4.00000	4.00000	29.43000	-1.4894	29.215	-0.0016327	-1.0696	8.7390E-6	
	-2.00000	4.00000	29.43000	-2.9259	29.215	-0.013771	-3.1778	25.521E-6	
	0.00000	4.00000	29.43000	-7.5276	29.215	-19.365	-58.180	-478.32E-6	
	2.00000	4.00000	29.43000	-13.302	29.215	-72.623	-163.88	-0.0022416	
	4.00000	4.00000	29.43000	-14.225	29.215	-72.641	-165.89	-0.0022259	
	6.00000	4.00000	29.43000	-13.305	29.215	-72.624	-163.90	-0.0022415	
	8.00000	4.00000	29.43000	-7.7846	29.215	-28.856	-68.118	-865.93E-6	
	10.00000	4.00000	29.43000	-2.9405	29.215	-0.013372	-3.1782	25.544E-6	
	12.00000	4.00000	29.43000	-1.5020	29.215	-0.0016334	-1.0763	8.7940E-6	
	14.00000	4.00000	29.43000	-0.82784	29.215	-406.89E-6	-0.50573	4.1499E-6	
	16.00000	4.00000	29.43000	-0.47530	29.215	-141.81E-6	-0.27991	2.3010E-6	
	18.00000	4.00000	29.43000	-0.27994	29.215	-60.232E-6	-0.17158	1.4118E-6	
	20.00000	4.00000	29.43000	-0.16752	29.215	-29.204E-6	-0.11291	0.0	
	22.00000	4.00000	29.43000	-0.10100	29.215	-15.582E-6	-0.078313	0.0	
	24.00000	4.00000	29.43000	-0.060766	29.215	-8.9413E-6	-0.056567	0.0	
	26.00000	4.00000	29.43000	-0.035991	29.215	-5.4334E-6	-0.042204	0.0	
	28.00000	4.00000	29.43000	-0.020523	29.215	-3.4585E-6	-0.032332	0.0	
	30.00000	4.00000	29.43000	-0.010770	29.215	-2.2875E-6	-0.025321	0.0	
	-20.00000	6.00000	29.43000	-0.020330	29.215	-3.4367E-6	-0.032180	0.0	
	-18.00000	6.00000	29.43000	-0.035749	29.215	-5.4068E-6	-0.042031	0.0	
	-16.00000	6.00000	29.43000	-0.060502	29.215	-8.9164E-6	-0.056390	0.0	
	-14.00000	6.00000	29.43000	-0.10082	29.215	-15.588E-6	-0.078188	0.0	
	-12.00000	6.00000	29.43000	-0.16773	29.215	-29.354E-6	-0.11301	0.0	
	-10.00000	6.00000	29.43000	-0.28137	29.215	-60.966E-6	-0.17238	1.4184E-6	
	-8.00000	6.00000	29.43000	-0.48012	29.215	-144.95E-6	-0.28289	2.3254E-6	
	-6.00000	6.00000	29.43000	-0.84173	29.215	-420.69E-6	-0.51556	4.2303E-6	
	-4.00000	6.00000	29.43000	-1.5393	29.215	-0.0017003	-1.1085	9.0557E-6	
	-2.00000	6.00000	29.43000	-3.0319	29.215	-0.014050	-3.2832	26.377E-6	
	0.00000	6.00000	29.43000	-7.7270	29.215	-19.366	-58.422	-476.36E-6	
	2.00000	6.00000	29.43000	-13.599	29.215	-72.625	-164.27	-0.0022385	
	4.00000	6.00000	29.43000	-14.581	29.215	-72.643	-166.38	-0.0022220	
	6.00000	6.00000	29.43000	-13.650	29.215	-72.626	-164.39	-0.0022376	
	8.00000	6.00000	29.43000	-8.0338	29.215	-28.857	-68.448	-863.27E-6	
	10.00000	6.00000	29.43000	-3.0736	29.215	-0.013776	-3.3177	26.675E-6	
	12.00000	6.00000	29.43000	-1.5643	29.215	-0.0017237	-1.1261	9.1998E-6	
	14.00000	6.00000	29.43000	-0.85685	29.215	-428.93E-6	-0.52447	4.3033E-6	
	16.00000	6.00000	29.43000	-0.48930	29.215	-148.15E-6	-0.28779	2.3657E-6	
	18.00000	6.00000	29.43000	-0.28697	29.215	-62.364E-6	-0.17526	1.4421E-6	
	20.00000	6.00000	29.43000	-0.17119	29.215	-30.023E-6	-0.11480	0.0	
	22.00000	6.00000	29.43000	-0.10298	29.215	-15.932E-6	-0.079350	0.0	
	24.00000	6.00000	29.43000	-0.061859	29.215	-9.1049E-6	-0.057174	0.0	
	26.00000	6.00000	29.43000	-0.036611	29.215	-5.5156E-6	-0.042578	0.0	
	28.00000	6.00000	29.43000	-0.020881	29.215	-3.5023E-6	-0.032572	0.0	
	30.00000	6.00000	29.43000	-0.010979	29.215	-2.3121E-6	-0.025481	0.0	
	-20.00000	8.00000	29.43000	-0.019651	29.215	-3.3537E-6	-0.031719	0.0	
	-18.00000	8.00000	29.43000	-0.034573	29.215	-5.2517E-6	-0.041315	0.0	
	-16.00000	8.00000	29.43000	-0.058429	29.215	-8.6087E-6	-0.055230	0.0	
	-14.00000	8.00000	29.43000	-0.097080	29.215	-14.931E-6	-0.076213	0.0	
	-12.00000	8.00000	29.43000	-0.16079	29.215	-27.822E-6	-0.10943	0.0	
	-10.00000	8.00000	29.43000	-0.26805	29.215	-56.982E-6	-0.16541	1.3611E-6	
	-8.00000	8.00000	29.43000	-0.45361	29.215	-133.12E-6	-0.26801	2.2033E-6	
	-6.00000	8.00000	29.43000	-0.78669	29.215	-379.54E-6	-0.48021	3.9408E-6	
	-4.00000	8.00000	29.43000	-1.4206	29.215	-0.0015307	-1.0143	8.2874E-6	
	-2.00000	8.00000	29.43000	-2.7741	29.215	-0.013274	-3.0139	24.194E-6	
	0.00000	8.00000	29.43000	-7.2170	29.215	-19.363	-57.726	-481.96E-6	
	2.00000	8.00000	29.43000	-12.797	29.215	-72.617	-162.94	-0.0022490	
	4.00000	8.00000	29.43000	-13.673	29.215	-72.632	-164.77	-0.0022347	
	6.00000	8.00000	29.43000	-12.939	29.215	-72.620	-163.30	-0.0022463	
	8.00000	8.00000	29.43000	-7.5947	29.215	-28.855	-67.883	-867.82E-6	
	10.00000	8.00000	29.43000	-2.8506	29.215	-0.013157	-3.0937	24.859E-6	
	12.00000	8.00000	29.43000	-1.4605	29.215	-0.0015855	-1.0460	8.5468E-6	
	14.00000	8.00000	29.43000	-0.80816	29.215	-394.66E-6	-0.49378	4.0520E-6	
	16.00000	8.00000	29.43000	-0.46560	29.215	-138.09E-6	-0.27463	2.2577E-6	
	18.00000	8.00000	29.43000	-0.27497	29.215	-58.911E-6	-0.16900	1.3906E-6	
	20.00000	8.00000	29.43000	-0.16488	29.215	-28.673E-6	-0.11154	0.0	
	22.00000	8.00000	29.43000	-0.099561	29.215	-15.346E-6	-0.077533	0.0	
	24.00000	8.00000	29.43000	-0.059958	29.215	-8.8272E-6	-0.056098	0.0	
	26.00000	8.00000	29.43000	-0.035529	29.215	-5.3743E-6	-0.041909	0.0	
	28.00000	8.00000	29.43000	-0.020254	29.215	-3.4262E-6	-0.032139	0.0	
	30.00000	8.00000	29.43000	-0.010611	29.215	-2.2689E-6	-0.025191	0.0	
	-20.00000	10.00000	29.43000	-0.018087	29.215	-3.1637E-6	-0.030640	0.0	
	-18.00000	10.00000	29.43000	-0.031884	29.215	-4.9008E-6	-0.039653	0.0	
	-16.00000	10.00000	29.43000	-0.053724	29.215	-7.9214E-6	-0.052567	0.0	
	-14.00000	10.00000	29.43000	-0.088669	29.215	-13.487E-6	-0.071736	0.0	
	-12.00000	10.00000	29.43000	-0.14535	29.215	-24.512E-6	-0.10145	0.0	
	-10.00000	10.00000	29.43000	-0.23884	29.215	-48.514E-6	-0.15014	1.2356E-6	
	-8.00000	10.00000	29.43000	-0.39619	29.215	-108.05E-6	-0.23593	1.9400E-6	
	-6.00000	10.00000	29.43000	-0.66837	29.215	-288.13E-6	-0.40388	3.3160E-6	
	-4.00000	10.00000	29.43000	-1.1605	29.215	-0.0010646	-0.79596	6.5105E-6	
	-2.00000	10.00000	29.43000	-2.1446	29.215	-0.0089043	-2.1633	17.397E-6	
	0.00000	10.00000	29.43000	-5.5826	29.215	-19.284	-53.070	-516.47E-6	
	2.00000	10.00000	29.43000	-9.6290	29.215	-71.853	-146.54	-0.0023465	
	4.00000	10.00000	29.43000	-9.3746	29.215	-69.331	-128.31	-0.0023720	
	6.00000	10.00000	29.43000	-10.349	29.215	-72.397	-154.03	-0.0023117	
	8.00000	10.00000	29.43000	-6.1423	29.215	-28.790	-64.017	-896.49E-6	
	10.00000	10.00000	29.43000	-2.2671	29.215	-0.0094468	-2.3394	18.822E-6	
	12.00000	10.00000	29.43000	-1.2137	29.215	-0.0011709	-0.84365	6.8984E-6	
	14.00000	10.00000	29.43000	-0.69454	29.215	-310.19E-6	-0.42130	3.4585E-6	
	16.00000	10.00000	29.43000	-0.41008	29.215	-114.43E-6	-0.24376	2.0043E-6	
	18.00000	10.00000	29.43000	-0.24659	29.215	-50.818E-6	-0.15419	1.2689E-6	
	20.00000	10.00000	29.43000	-0.14984	29.215	-25.484E-6	-0.10376	0.0	
	22.00000	10.00000	29.43000	-0.091344	29.215	-13.946E-6	-0.073150	0.0	
	24.00000	10.00000	29.43000	-0.055352	29.215	-8.1581E-6	-0.053483	0.0	
	26.00000	10.00000	29.43000	-0.032892	29.215	-5.0315E-6	-0.040274	0.0	
	28.00000	10.00000	29.43000	-0.018719	29.215	-3.2400E-6	-0.031075	0.0	
	30.00000	10.00000	29.43000	-0.0097073	29.215	-2.1628E-6	-0.024475	0.0	
	-20.00000	12.00000	29.43000	-0.015826	29.215	-2.8912E-6	-0.029043	0.0	
	-18.00000	12.00000	29.43000	-0.028035	29.215	-4.4061E-6	-0.037226	0.0	
	-16.00000	12.00000	29.43000	-0.047077	29.215	-6.9736E-6	-0.048740	0.0	
	-14.00000	12.00000	29.43000	-0.076976	29.215	-11.548E-6	-0.065433	0.0	

Name	Location			Displacement		Stresses			
	X [m]	Y [m]	Z[Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m²]	Sum Princ [kN/m²]	Vert Strain [-]
	-12.00000	12.00000	29.43000	-0.12432	29.215	-20.214E-6	-0.090516	0.0
	-10.00000	12.00000	29.43000	-0.19997	29.215	-37.935E-6	-0.12987	1.0690E-6
	-8.00000	12.00000	29.43000	-0.32198	29.215	-77.978E-6	-0.19502	1.6042E-6
	-6.00000	12.00000	29.43000	-0.52038	29.215	-181.24E-6	-0.31054	2.5516E-6
	-4.00000	12.00000	29.43000	-0.84400	29.215	-486.78E-6	-0.53308	4.3714E-6
	-2.00000	12.00000	29.43000	-1.3535	29.215	158.86E-6	-0.92550	7.6391E-6
	0.00000	12.00000	29.43000	-1.2109	29.215	19.779	36.823	674.92E-6
	2.00000	12.00000	29.43000	-2.7076	29.215	0.16940	-0.87686	15.611E-6
	4.00000	12.00000	29.43000	-2.9611	29.215	0.098191	-1.2411	15.092E-6
	6.00000	12.00000	29.43000	-3.2347	29.215	0.048912	-4.3878	38.599E-6
	8.00000	12.00000	29.43000	-2.2905	29.215	1.6267	3.4545	51.994E-6
	10.00000	12.00000	29.43000	-1.4919	29.215	-0.0019358	-1.1839	9.6664E-6
	12.00000	12.00000	29.43000	-0.89897	29.215	-616.69E-6	-0.58455	4.7895E-6
	14.00000	12.00000	29.43000	-0.54693	29.215	-204.70E-6	-0.32841	2.6978E-6
	16.00000	12.00000	29.43000	-0.33601	29.215	-84.526E-6	-0.20296	1.6693E-6
	18.00000	12.00000	29.43000	-0.20778	29.215	-40.272E-6	-0.13395	1.1025E-6
	20.00000	12.00000	29.43000	-0.12883	29.215	-21.194E-6	-0.092837	0.0
	22.00000	12.00000	29.43000	-0.079663	29.215	-12.011E-6	-0.066853	0.0
	24.00000	12.00000	29.43000	-0.048711	29.215	-7.2114E-6	-0.049659	0.0
	26.00000	12.00000	29.43000	-0.029046	29.215	-4.5373E-6	-0.037848	0.0
	28.00000	12.00000	29.43000	-0.016459	29.215	-2.9676E-6	-0.029479	0.0
	30.00000	12.00000	29.43000	-0.0083662	29.215	-2.0056E-6	-0.023391	0.0
	-20.00000	14.00000	29.43000	-0.013115	29.215	-2.5674E-6	-0.027066	0.0
	-18.00000	14.00000	29.43000	-0.023486	29.215	-3.8326E-6	-0.034272	0.0
	-16.00000	14.00000	29.43000	-0.039359	29.215	-5.9074E-6	-0.044183	0.0
	-14.00000	14.00000	29.43000	-0.063695	29.215	-9.4502E-6	-0.058135	0.0
	-12.00000	14.00000	29.43000	-0.10108	29.215	-15.788E-6	-0.078302	0.0
	-10.00000	14.00000	29.43000	-0.15851	29.215	-27.751E-6	-0.10831	0.0
	-8.00000	14.00000	29.43000	-0.24642	29.215	-51.707E-6	-0.15435	1.2701E-6
	-6.00000	14.00000	29.43000	-0.37916	29.215	-102.00E-6	-0.22692	1.8660E-6
	-4.00000	14.00000	29.43000	-0.57262	29.215	-198.57E-6	-0.34088	2.8009E-6
	-2.00000	14.00000	29.43000	-0.82955	29.215	-127.69E-6	-0.49112	4.0432E-6
	0.00000	14.00000	29.43000	-1.1158	29.215	0.0016574	-0.60118	5.0391E-6
	2.00000	14.00000	29.43000	-1.4011	29.215	-181.47E-6	-0.90995	7.4941E-6
	4.00000	14.00000	29.43000	-1.5538	29.215	-0.0013592	-1.1105	9.0897E-6
	6.00000	14.00000	29.43000	-1.5201	29.215	-0.0020296	-1.1592	9.4579E-6
	8.00000	14.00000	29.43000	-1.2605	29.215	-0.0011030	-0.90673	7.4220E-6
	10.00000	14.00000	29.43000	-0.91253	29.215	-616.52E-6	-0.59943	4.9122E-6
	12.00000	14.00000	29.43000	-0.61459	29.215	-272.04E-6	-0.37613	3.0880E-6
	14.00000	14.00000	29.43000	-0.40139	29.215	-118.96E-6	-0.24123	1.9832E-6
	16.00000	14.00000	29.43000	-0.25874	29.215	-56.994E-6	-0.16119	1.3263E-6
	18.00000	14.00000	29.43000	-0.16558	29.215	-29.758E-6	-0.11198	0.0
	20.00000	14.00000	29.43000	-0.10524	29.215	-16.663E-6	-0.080445	0.0
	22.00000	14.00000	29.43000	-0.066206	29.215	-9.8732E-6	-0.059470	0.0
	24.00000	14.00000	29.43000	-0.040901	29.215	-6.1290E-6	-0.045057	0.0
	26.00000	14.00000	29.43000	-0.024447	29.215	-3.9563E-6	-0.034868	0.0
	28.00000	14.00000	29.43000	-0.013721	29.215	-2.6402E-6	-0.027487	0.0
	30.00000	14.00000	29.43000	-0.0067242	29.215	-1.8133E-6	-0.022021	0.0
	-20.00000	16.00000	29.43000	-0.010213	29.215	-2.2239E-6	-0.024855	0.0
	-18.00000	16.00000	29.43000	-0.018698	29.215	-3.2419E-6	-0.031038	0.0
	-16.00000	16.00000	29.43000	-0.031408	29.215	-4.8495E-6	-0.039323	0.0
	-14.00000	16.00000	29.43000	-0.050376	29.215	-7.4650E-6	-0.050609	0.0
	-12.00000	16.00000	29.43000	-0.078541	29.215	-11.856E-6	-0.066240	0.0
	-10.00000	16.00000	29.43000	-0.12001	29.215	-19.462E-6	-0.088227	0.0
	-8.00000	16.00000	29.43000	-0.18009	29.215	-32.955E-6	-0.11948	0.0
	-6.00000	16.00000	29.43000	-0.26462	29.215	-56.816E-6	-0.16382	1.3479E-6
	-4.00000	16.00000	29.43000	-0.37733	29.215	-95.318E-6	-0.22462	1.8474E-6
	-2.00000	16.00000	29.43000	-0.51427	29.215	-140.65E-6	-0.30065	2.4721E-6
	0.00000	16.00000	29.43000	-0.65878	29.215	-191.67E-6	-0.38516	3.1664E-6
	2.00000	16.00000	29.43000	-0.78125	29.215	-310.93E-6	-0.46846	3.8474E-6
	4.00000	16.00000	29.43000	-0.84277	29.215	-418.20E-6	-0.51869	4.2562E-6
	6.00000	16.00000	29.43000	-0.81782	29.215	-442.35E-6	-0.51053	4.1877E-6
	8.00000	16.00000	29.43000	-0.70855	29.215	-349.49E-6	-0.43830	3.5968E-6
	10.00000	16.00000	29.43000	-0.55453	29.215	-219.19E-6	-0.33607	2.7603E-6
	12.00000	16.00000	29.43000	-0.40354	29.215	-122.14E-6	-0.24308	1.9983E-6
	14.00000	16.00000	29.43000	-0.28058	29.215	-65.987E-6	-0.17331	1.4258E-6
	16.00000	16.00000	29.43000	-0.18969	29.215	-36.448E-6	-0.12464	1.0260E-6
	18.00000	16.00000	29.43000	-0.12581	29.215	-20.950E-6	-0.091216	0.0
	20.00000	16.00000	29.43000	-0.082088	29.215	-12.554E-6	-0.068073	0.0
	22.00000	16.00000	29.43000	-0.052570	29.215	-7.8195E-6	-0.051788	0.0
	24.00000	16.00000	29.43000	-0.032782	29.215	-5.0417E-6	-0.040114	0.0
	26.00000	16.00000	29.43000	-0.019566	29.215	-3.3519E-6	-0.031587	0.0
	28.00000	16.00000	29.43000	-0.010767	29.215	-2.2900E-6	-0.025248	0.0
	30.00000	16.00000	29.43000	-0.0049303	29.215	-1.6027E-6	-0.020455	0.0
	-20.00000	18.00000	29.43000	-0.0073486	29.215	-1.8871E-6	-0.022548	0.0
	-18.00000	18.00000	29.43000	-0.014060	29.215	-2.6815E-6	-0.027741	0.0
	-16.00000	18.00000	29.43000	-0.023888	29.215	-3.8868E-6	-0.034510	0.0
	-14.00000	18.00000	29.43000	-0.038144	29.215	-5.7514E-6	-0.043420	0.0
	-12.00000	18.00000	29.43000	-0.058590	29.215	-8.6881E-6	-0.055243	0.0
	-10.00000	18.00000	29.43000	-0.087435	29.215	-13.373E-6	-0.070994	0.0
	-8.00000	18.00000	29.43000	-0.12713	29.215	-20.853E-6	-0.091893	0.0
	-6.00000	18.00000	29.43000	-0.17964	29.215	-32.516E-6	-0.11911	0.0
	-4.00000	18.00000	29.43000	-0.24502	29.215	-49.517E-6	-0.15305	1.2595E-6
	-2.00000	18.00000	29.43000	-0.31922	29.215	-71.720E-6	-0.19213	1.5806E-6
	0.00000	18.00000	29.43000	-0.39263	29.215	-98.330E-6	-0.23199	1.9080E-6
	2.00000	18.00000	29.43000	-0.45062	29.215	-126.64E-6	-0.26522	2.1807E-6
	4.00000	18.00000	29.43000	-0.47762	29.215	-145.99E-6	-0.28221	2.3198E-6
	6.00000	18.00000	29.43000	-0.46423	29.215	-145.40E-6	-0.27604	2.2689E-6
	8.00000	18.00000	29.43000	-0.41302	29.215	-122.73E-6	-0.24730	2.0331E-6
	10.00000	18.00000	29.43000	-0.33876	29.215	-89.238E-6	-0.20539	1.6891E-6
	12.00000	18.00000	29.43000	-0.26006	29.215	-58.728E-6	-0.16216	1.3342E-6
	14.00000	18.00000	29.43000	-0.19004	29.215	-36.845E-6	-0.12485	1.0276E-6
	16.00000	18.00000	29.43000	-0.13396	29.215	-22.882E-6	-0.095457	0.0
	18.00000	18.00000	29.43000	-0.091838	29.215	-14.363E-6	-0.073251	0.0
	20.00000	18.00000	29.43000	-0.061407	29.215	-9.1971E-6	-0.056715	0.0
	22.00000	18.00000	29.43000	-0.039949	29.215	-6.0271E-6	-0.044410	0.0
	24.00000	18.00000	29.43000	-0.025047	29.215	-4.0434E-6	-0.035195	0.0
	26.00000	18.00000	29.43000	-0.014808	29.215	-2.7744E-6	-0.028229	0.0
	28.00000	18.00000	29.43000	-0.0078330	29.215	-1.9443E-6	-0.022903	0.0
	30.00000	18.00000	29.43000	-0.0031231	29.215	-1.3894E-6	-0.018785	0.0
	-20.00000	20.00000	29.43000	-0.0046931	29.215	-1.5752E-6	-0.020257	0.0
	-18.00000	20.00000	29.43000	-0.0098441	29.215	-2.1808E-6	-0.024548	0.0
	-16.00000	20.00000	29.43000	-0.017218	29.215	-3.0630E-6	-0.029985	0.0
	-14.00000	20.00000	29.43000	-0.027620	29.215	-4.3620E-6	-0.036906	0.0
	-12.00000	20.00000	29.43000	-0.042043	29.215	-6.2877E-6	-0.045721	0.0
	-10.00000	20.00000	29.43000	-0.061595	29.215	-9.1412E-6	-0.056897	0.0
	-8.00000	20.00000	29.43000	-0.087280	29.215	-13.315E-6	-0.070874	0.0
	-6.00000	20.00000	29.43000	-0.11955	29.215	-19.221E-6	-0.087873	0.0
	-4.00000	20.00000	29.43000	-0.15756	29.215	-27.084E-6	-0.10756	0.0
	-2.00000	20.00000	29.43000	-0.19844	29.215	-36.646E-6	-0.12864	1.0589E-6
	0.00000	20.00000	29.43000	-0.23688	29.215	-46.939E-6	-0.14860	1.2229E-6
	2.00000	20.00000	29.43000	-0.26586	29.215	-56.033E-6	-0.16392	1.3488E-6
	4.00000	20.00000	29.43000	-0.27865	29.215	-61.136E-6	-0.17097	1.4067E-6
	6.00000	20.00000	29.43000	-0.27159	29.215	-60.003E-6	-0.16753	1.3784E-6
	8.00000	20.00000	29.43000	-0.24607	29.215	-52.629E-6	-0.15419	1.2688E-6
	10.00000	20.00000	29.43000	-0.20820	29.215	-41.637E-6	-0.13427	1.1051E-6
	12.00000	20.00000	29.43000	-0.16597	29.215	-30.449E-6	-0.11215	0.0
	14.00000	20.00000	29.43000	-0.12597	29.215	-21.202E-6	-0.091233	0.0
	16.00000	20.00000	29.43000	-0.091865	29.215	-14.422E-6	-0.073223	0.0
	18.00000	20.00000	29.43000	-0.064743	29.215	-9.7564E-6	-0.058521	0.0
	20.00000	20.00000	29.43000	-0.044161	29.215	-6.6357E-6	-0.046851	0.0
	22.00000	20.00000	29.43000	-0.029030	29.215	-4.5643E-6	-0.037703	0.0
	24.00000	20.00000	29.43000	-0.018153	29.215	-3.1843E-6	-0.030558	0.0
	26.00000	20.00000	29.43000	-0.010462	29.215	-2.2558E-6	-0.024967	0.0
	28.00000	20.00000	29.43000	-0.0051006	29.215	-1.6229E-6	-0.020569	0.0
	30.00000	20.00000	29.43000	-0.0014148	29.215	-1.1853E-6	-0.017088	0.0
	-20.00000	22.00000	29.43000	-0.0023555	29.215	-1.2987E-6	-0.018066	0.0
	-18.00000	22.00000	29.43000	-0.0062032	29.215	-1.7525E-6	-0.021567	0.0
	-16.00000	22.00000	29.43000	-0.011595	29.215	-2.3879E-6	-0.025886	0.0
	-14.00000	22.00000	29.43000	-0.019003	29.215	-3.2809E-6	-0.031209	0.0
	-12.00000	22.00000	29.43000	-0.028960	29.215	-4.5337E-6	-0.037739	0.0
	-10.00000	22.00000	29.43000	-0.041979	29.215	-6.2747E-6	-0.045663	0.0
	-8.00000	22.00000	29.43000	-0.058404	29.215	-8.6424E-6	-0.055089	0.0
	-6.00000	22.00000	29.43000	-0.078158	29.215	-11.741E-6	-0.065937	0.0
	-4.00000	22.00000	29.43000	-0.10041	29.215	-15.558E-6	-0.077792	0.0
	-2.00000	22.00000	29.43000	-0.12333	29.215	-19.862E-6	-0.089773	0.0
	0.00000	22.00000	29.43000	-0.14405	29.215	-24.131E-6	-0.10051	0.0
	2.00000	22.00000	29.43000	-0.15914	29.215	-27.561E-6	-0.10832	0.0
	4.00000	22.00000	29.43000	-0.16555	29.215	-29.264E-6	-0.11168	0.0
	6.00000	22.00000	29.43000	-0.16176	29.215	-28.654E-6	-0.10977	0.0
	8.00000	22.00000	29.43000	-0.14846	29.215	-25.821E-6	-0.10289	0.0

Name	Location X [m]	Location Y [m]	Displacement Z[Level] [mOD]	Displacement Z [mm]	Stresses Calc Level [mOD]	Stresses Vert Stress [kN/m²]	Stresses Sum Princ [kN/m²]	Stresses Vert Strain [-]
	10.00000	22.00000	29.43000	-0.12836	29.215	-21.551E-6	-0.092425	0.0
	12.00000	22.00000	29.43000	-0.10510	29.215	-16.894E-6	-0.080214	0.0
	14.00000	22.00000	29.43000	-0.082032	29.215	-12.664E-6	-0.067916	0.0
	16.00000	22.00000	29.43000	-0.061369	29.215	-9.2349E-6	-0.056611	0.0
	18.00000	22.00000	29.43000	-0.044138	29.215	-6.6436E-6	-0.046801	0.0
	20.00000	22.00000	29.43000	-0.030485	29.215	-4.7621E-6	-0.038581	0.0
	22.00000	22.00000	29.43000	-0.020061	29.215	-3.4234E-6	-0.031833	0.0
	24.00000	22.00000	29.43000	-0.012319	29.215	-2.4783E-6	-0.026351	0.0
	26.00000	22.00000	29.43000	-0.0066944	29.215	-1.8108E-6	-0.021918	0.0
	28.00000	22.00000	29.43000	-0.0026862	29.215	-1.3371E-6	-0.018334	0.0
	30.00000	22.00000	29.43000	116.41E-6	29.215	0.0	-0.015429	0.0
	-20.00000	24.00000	29.43000	-386.48E-6	29.215	-1.0613E-6	-0.016026	0.0
	-18.00000	24.00000	29.43000	-0.0031896	29.215	-1.3974E-6	-0.018860	0.0
	-16.00000	24.00000	29.43000	-0.0070435	29.215	-1.8508E-6	-0.022266	0.0
	-14.00000	24.00000	29.43000	-0.012215	29.215	-2.4612E-6	-0.026342	0.0
	-12.00000	24.00000	29.43000	-0.018975	29.215	-3.2765E-6	-0.031176	0.0
	-10.00000	24.00000	29.43000	-0.027538	29.215	-4.3483E-6	-0.036822	0.0
	-8.00000	24.00000	29.43000	-0.037974	29.215	-5.7205E-6	-0.043261	0.0
	-6.00000	24.00000	29.43000	-0.050075	29.215	-7.4056E-6	-0.050346	0.0
	-4.00000	24.00000	29.43000	-0.063219	29.215	-9.3530E-6	-0.057741	0.0
	-2.00000	24.00000	29.43000	-0.076293	29.215	-11.416E-6	-0.064887	0.0
	0.00000	24.00000	29.43000	-0.087748	29.215	-13.341E-6	-0.071031	0.0
	2.00000	24.00000	29.43000	-0.095874	29.215	-14.797E-6	-0.075338	0.0
	4.00000	24.00000	29.43000	-0.099238	29.215	-15.464E-6	-0.077107	0.0
	6.00000	24.00000	29.43000	-0.097158	29.215	-15.160E-6	-0.075998	0.0
	8.00000	24.00000	29.43000	-0.089975	29.215	-13.936E-6	-0.072170	0.0
	10.00000	24.00000	29.43000	-0.078954	29.215	-12.066E-6	-0.066243	0.0
	12.00000	24.00000	29.43000	-0.065853	29.215	-9.9271E-6	-0.059082	0.0
	14.00000	24.00000	29.43000	-0.052389	29.215	-7.8508E-6	-0.051535	0.0
	16.00000	24.00000	29.43000	-0.039851	29.215	-6.0394E-6	-0.044248	0.0
	18.00000	24.00000	29.43000	-0.028979	29.215	-4.5668E-6	-0.037610	0.0
	20.00000	24.00000	29.43000	-0.020040	29.215	-3.4230E-6	-0.031792	0.0
	22.00000	24.00000	29.43000	-0.012982	29.215	-2.5589E-6	-0.026820	0.0
	24.00000	24.00000	29.43000	-0.0075858	29.215	-1.9162E-6	-0.022637	0.0
	26.00000	24.00000	29.43000	-0.0035674	29.215	-1.4416E-6	-0.019148	0.0
	28.00000	24.00000	29.43000	-646.26E-6	29.215	-1.0915E-6	-0.016252	0.0
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	-16.00000	26.00000	29.43000	-0.0034830	29.215	-1.4317E-6	-0.019126	0.0
	-14.00000	26.00000	29.43000	-0.0070307	29.215	-1.8488E-6	-0.022245	0.0
	-12.00000	26.00000	29.43000	-0.011558	29.215	-2.3823E-6	-0.025834	0.0
	-10.00000	26.00000	29.43000	-0.017140	29.215	-3.0512E-6	-0.029891	0.0
	-8.00000	26.00000	29.43000	-0.023746	29.215	-3.8653E-6	-0.034356	0.0
	-6.00000	26.00000	29.43000	-0.031178	29.215	-4.8143E-6	-0.039093	0.0
	-4.00000	26.00000	29.43000	-0.039013	29.215	-5.8557E-6	-0.043858	0.0
	-2.00000	26.00000	29.43000	-0.046591	29.215	-6.9058E-6	-0.048306	0.0
	0.00000	26.00000	29.43000	-0.053070	29.215	-7.8415E-6	-0.052010	0.0
	2.00000	26.00000	29.43000	-0.057572	29.215	-8.5194E-6	-0.054538	0.0
	4.00000	26.00000	29.43000	-0.059399	29.215	-8.8135E-6	-0.055544	0.0
	6.00000	26.00000	29.43000	-0.058230	29.215	-8.6586E-6	-0.054872	0.0
	8.00000	26.00000	29.43000	-0.054238	29.215	-8.0791E-6	-0.052605	0.0
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No. 8 Albert Terrace Mews	8.08000	6.15000	34.25000	-7.3930	34.031	0.0	0.0	0.0
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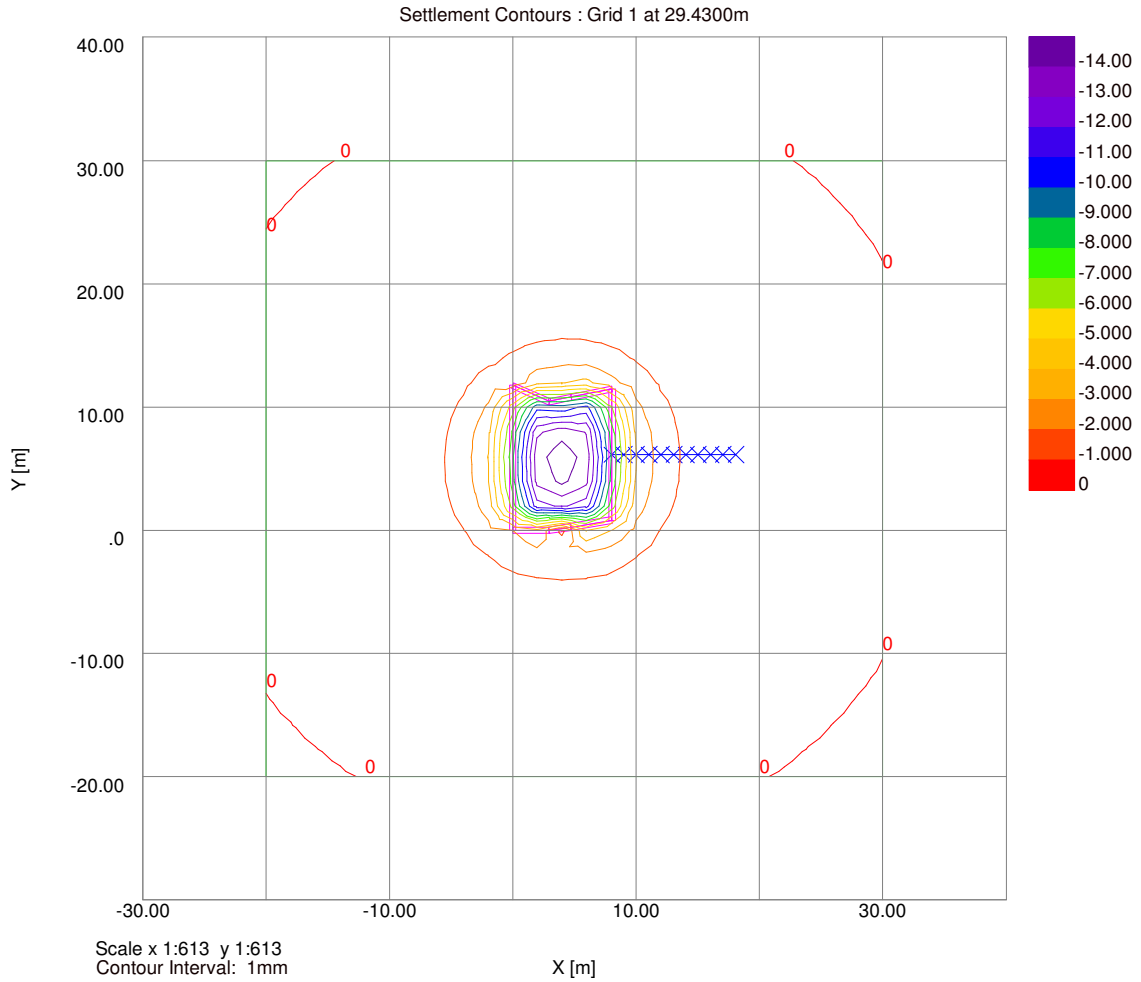
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30.00
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Y [m]
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-10.00
10.00
30.00
X [m]
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-12.00
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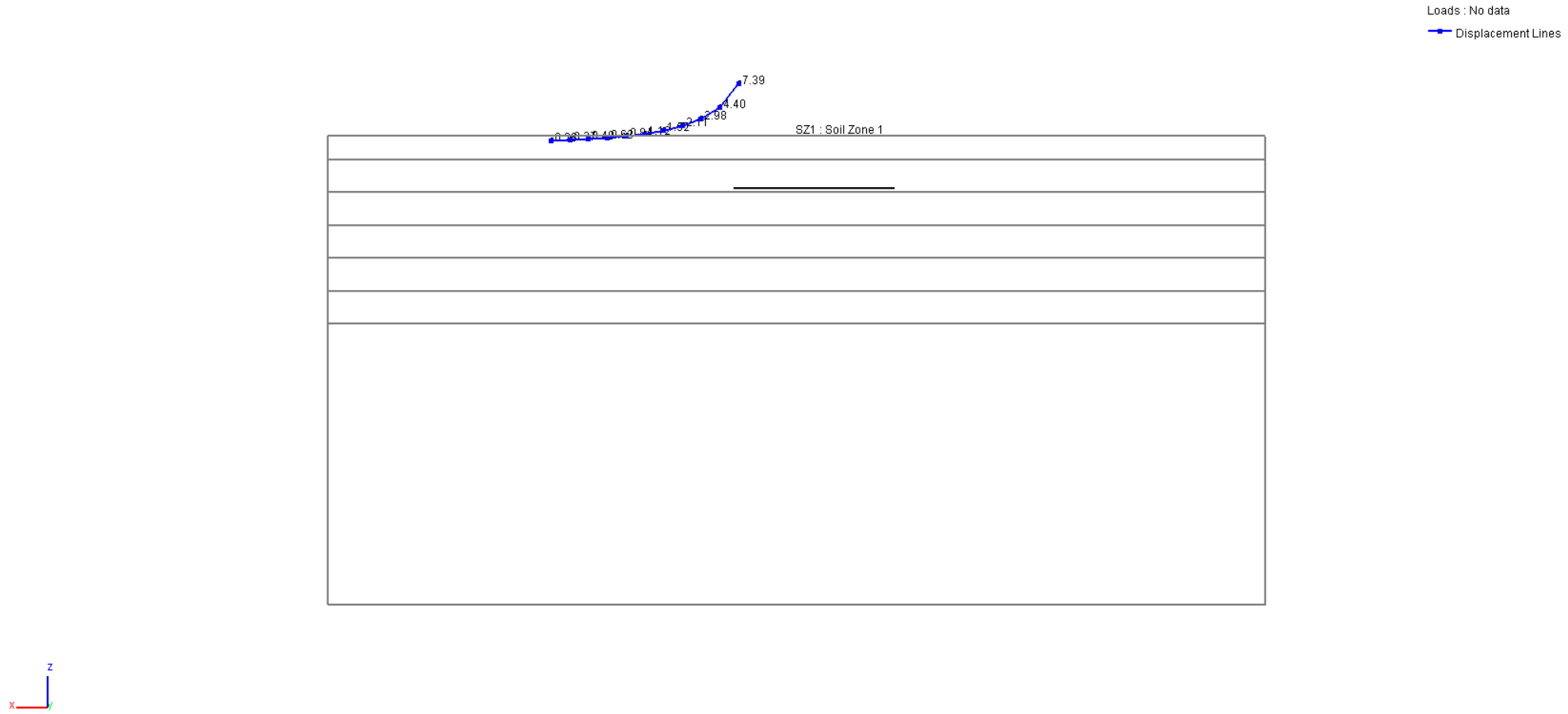
Contour Interval: 1mm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Displacement Lines
7.39
4.40
2.98
SZ1 : Soil Zone 1
Z
X
Y

APPENDIX E
SITE INVESTIGATION INFORMATION – COPIES OF BOREHOLE AND TRIAL PIT LOGS

LEGEND

- Borehole location
- Trial pit location

Rev.	Date	Amendment	Drawn	Chkd.	Appd.
P1	19.03.18	FIRST ISSUE	AP	JG	JG

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Client

MR. MARK GOLINSKY

Project Title

6 ALBERT TERRACE MEWS

Drawing Title

EXPLORATORY HOLE
LOCATION PLAN
ALBERT TERRACE MEWS

Drawn	Date	Checked	Date	Approved	Date
AP	19.03.18	JG	19.03.18	JG	19.03.18

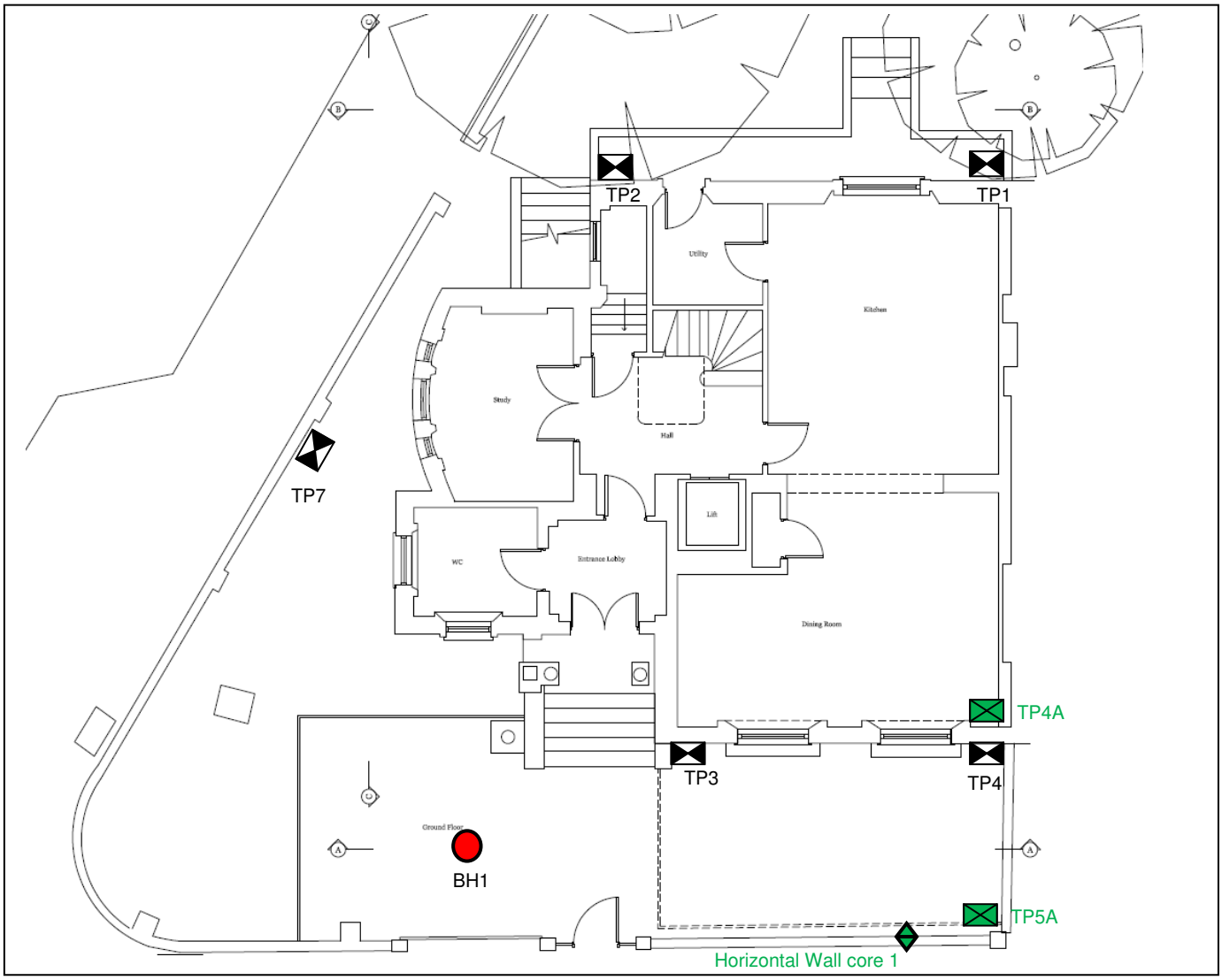
Scale	Orig Size	Dimensions
1:100	A3	m

Project No.	Drawing File
29841 - R01(00)	29841 - (R01-00) Fig 2.dwg

Drawing No.	Rev.
FIGURE 2	P1

Scale

0 1 2 3 4 5m



RSK Site investigation intrusive investigation work between 27th February and 3rd March 2017 and presented in RSK report reference 29123 R01 (01).

RSK Site investigation intrusive investigation work between 12th and 13th March 2018 and presented in RSK report reference 29123 R01 (02).

RSK	**Exploratory Hole Location Plan**	**Client: Alan Baxter Ltd**	**App E1**
		Site: 6 Albert Terrace	**Job No: 29123**
		Scale: Not to scale	**Source:**

DRAFT

BOREHOLE LOG

Contract:	Client:	Borehole:
6 Albert Terrace	Alan Baxter	BH1

Contract Ref:	Start: 03.02.17	Ground Level (m AOD):	National Grid Co-ordinate:	Sheet:
29123	End: 03.06.17	34.00	E:528066.0 N:183765.0	1 of 3

Samples and In-situ Tests				Water	Backfill & Instru-mentation	Description of Strata	Depth (Thick ness)	Material Graphic Legend
Depth	No	Type	Results					
						Made Ground: Concrete slab at surface.	0.15	
						(MADE GROUND)	0.25	
0.50	1	D				Made Ground: Medium to coarse sandy, sub rounded to subangular fine to medium gravel. (type 1 subase material) (MADE GROUND)		
1.00	2	D				Made Ground: Soft to firm orangeish brown mottled grey slightly sandy gravelly CLAY. Sand is fine to coarse. Gravel is angular to subangular flint, brick and concrete with occasional chalk fragments. (MADE GROUND)	(2.25)	
1.50-1.95	1	SPT	N=5					
1.50-1.95	3	D						
2.00	4	D						
							2.50	
2.50-2.95	5	U				Firm medium strength brown silty CLAY. (LONDON CLAY FORMATION)		
3.00	6	U						
3.50-3.95	2	SPT	N=12					
3.50-3.95	7	D						
4.00	8	D						
4.50-4.95	9	U						
5.00	10	U						
6.00-6.45	3	SPT	N=20			. . . High strength mottled grey silty CLAY at 6.00m bgl.		
6.00-6.45	11	D						
6.75	12	D					(8.70)	
7.50-7.95	13	U						
8.00	14	U						

Boring Progress and Water Observations

Date	Time	Borehole Depth	Casing Depth	Borehole Diameter (mm)	Water Depth
02/03/17		10.00	2.00	150	
06/03/17		20.00	2.00	150	

Chiselling / Slow Progress

From	To	Duration (hh:mm)

General Remarks

1. Inspection pit hand dug to 1.20m depth.
2. Water added to aid drilling.
3. No groundwater encountered.
4. On completion, borehole backfilled with arisings to 10.0m, with a gravel response zone to 1.0m bgl and 1.0m of bentonite to ground level.

All dimensions in metres | Scale: 1:50

Method Used:	Plant Used:	Drilled By:	Logged By:	Checked By:
Inspection pit + Cable percussion	Dando 2000 Mark2	???	JHowourth	AG

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_016 PrjVersion: v8_06 - Core+Logs - 002 | Log CABLE PERCUSSION LOG - A4P | 29123_6 ALBERT TERRACE.GPJ - v8_06.
RSK Environment Ltd, 18 Frogmore Road, Hemel Hempstead, Hertfordshire, HP3 9RT. Tel: 01442 437550, Fax: 01442 437500, Web: www.rsk.co.uk. | 03/17/17 - 10:01 | JH8 |

DRAFT

BOREHOLE LOG

Contract:	Client:	Borehole:
6 Albert Terrace	**Alan Baxter**	**BH1**

Contract Ref:	Start:	Ground Level (m AOD):	National Grid Co-ordinate:	Sheet:
29123	**03.02.17** End: **03.06.17**	**34.00**	**E:528066.0 N:183765.0**	**2** of **3**

Samples and In-situ Tests				Water	Backfill & Instru-mentation	Description of Strata	Depth (Thick ness)	Material Graphic Legend
Depth	No	Type	Results					
9.00-9.45	4	SPT	N=22			Firm medium strength brown silty CLAY. (LONDON CLAY FORMATION) *(stratum copied from 2.50m from previous sheet)*		
9.00-9.45	15	D						
9.75	16	D						
10.50-10.95	17	U						
11.00	18	U					11.20	
						Firm to stiff high strengthdark grey, fissured silty CLAY. (LONDON CLAY FORMATION)		
12.00-12.45	5	SPT	N=26					
12.00-12.45	19	D						
12.75	20	D						
13.50-13.95	21	U						
14.00	22	U						
15.00-15.45	6	SPT	N=31				(8.80)	
15.00-15.45	23	D						
15.75	24	D						
16.50-16.95	25	U						
17.00	26	U						

Boring Progress and Water Observations					
Date	Time	Borehole Depth	Casing Depth	Borehole Diameter (mm)	Water Depth

Chiselling / Slow Progress		
From	To	Duration (hh:mm)

General Remarks

All dimensions in metres | Scale: **1:50**

Method Used:	Plant Used:	Drilled By:	Logged By:	Checked By:
Inspection pit + Cable percussion	**Dando 2000 Mark2**	**???**	**JHowourth**	AG

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_016 PrjVersion: v8_06 - Core+Logs - 002 | Log CABLE PERCUSSION LOG - A4P | 29123_6 ALBERT TERRACE.GPJ - v8_06.
RSK Environment Ltd, 18 Frogmore Road, Hemel Hempstead, Hertfordshire, HP3 9RT. Tel: 01442 437500, Fax: 01442 437550, Web: www.rsk.co.uk. | 03/17/17 - 10:01 | JH8 |

DRAFT

BOREHOLE LOG

Contract:	Client:	Borehole:
6 Albert Terrace	**Alan Baxter**	**BH1**

Contract Ref:	Start:	Ground Level (m AOD):	National Grid Co-ordinate:	Sheet:
29123	**03.02.17** End: **03.06.17**	**34.00**	**E:528066.0 N:183765.0**	**3** of **3**

Samples and In-situ Tests				Water	Backfill & Instru-mentation	Description of Strata	Depth (Thick ness)	Material Graphic Legend
Depth	No	Type	Results					
18.00-18.45	7	SPT	N=35			Firm to stiff high strengthdark grey, fissured silty CLAY. (LONDON CLAY FORMATION)		
18.00-18.45	27	D				*(stratum copied from 11.20m from previous sheet)*		
18.75	28	D				. . . Slight claystone from 19.00m bgl.		
19.50-19.95	29	U						
20.00	30	U				Borehole terminated at 20.00m bgl.	20.00	

Boring Progress and Water Observations					
Date	Time	Borehole Depth	Casing Depth	Borehole Diameter (mm)	Water Depth

Chiselling / Slow Progress		
From	To	Duration (hh:mm)

General Remarks

All dimensions in metres | Scale: **1:50**

Method Used:	Plant Used:	Drilled By:	Logged By:	Checked By:
Inspection pit + Cable percussion	**Dando 2000 Mark2**	**???**	**JHowourth**	AG

AGS

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_016 PrjVersion: v8_06 - Core+Logs - 002 | Log CABLE PERCUSSION LOG - A4P | 29123_6 ALBERT TERRACE.GPJ - v8_06.
RSK Environment Ltd, 18 Frogmore Road, Hemel Hempstead, Hertfordshire, HP3 9RT. Tel: 01442 437500, Fax: 01442 437550, Web: www.rsk.co.uk. | 03/17/17 - 10:01 | JH8 |

WINDOW SAMPLE LOG

Contract:	Client:	Window Sample:
6 Albert Terrace Mews	**Mr. Mark Golinsky**	**BH1A**

Contract Ref:	Start:	Ground Level:	Co-ordinates:	Sheet:
29841	**12.03.18**	**---**	**---**	**1** of **2**
	End: **12.03.18**			

Progress	Samples / Tests				Water	Backfill & Instru-mentation	Description of Strata	Depth (Thick ness)	Material Graphic Legend
Window Run	Depth	No	Type	Results					
	0.20	1	ES	1xT1xV1xJ			TOPSOIL: Dark brown slightly sandy CLAY with frequent rootlets and roots (5mm in diameter) and grass cover.	(0.30) 0.30	
							MADE GROUND: Yellowish brown gravelly SAND. Sand is fine to coarse. Gravel is angular fine of flints occasional shell fragments.	0.40	
	0.50-1.00	2	ES	1xT1xJ1xV			MADE GROUND: Dark brown slightly clayey gravelly SAND. Sand is angular to subrounded fine to coarse of brick clinker flint and sandstone with occasional shell fragments.	(0.90)	
	1.00-1.45	1	SPT	N=10			1.00m : at 1.00m occasional cobbles of brick and flint 8-10cm.	1.30	
							MADE GROUND: Light yellow SAND and GRAVEL. Sand is fine to coarse. Gravel is possible concrete screed.	1.40	
	1.50	3	ES	1xT1xV1xJ			MADE GROUND: Stiff mottled grey and black slightly gravelly CLAY. Gravel is angular to rounded fine to coarse of flint brick clinker and occasional granite. Occasional rootlets 1-2mm diameter.	(0.80)	
	2.00 2.00-2.45 2.00	1 2	D SPT V	 N=12 c_u=70				2.20	
	2.30	4	ES				MADE GROUND: Reworked firm to stiff mottled grey and brown silty CLAY with occasional rootlets. (REWORKED LONDON CLAY FORMATION)	(0.30) 2.50	
							Initially firm becoming stiff mottled grey and brown silty CLAY with occasional rootlets. (LONDON CLAY FORMATION)		
	3.00 3.00-3.45 3.00	2 3	D SPT V	 N=12 c_u=90				(1.20) 3.70	
							Bluish grey fine to coarse angular to subrounded CLAYSTONE. (LONDON CLAY FORMATION)	3.80	
	4.00 4.00-4.45 4.00	3 4	D SPT V	 N=14 c_u=135			Stiff to very stiff high to very high strength mottled bluish grey and brown silty CLAY. (LONDON CLAY FORMATION)		

Drilling Progress and Water Observations

Date	Time	Borehole Depth (m)	Casing Depth (m)	Borehole Diameter (mm)	Water Depth (m)

General Remarks

1. Inspection pit to 1.20m.
2. Borehole remained stable.
3. Groundwater encountered at 3.80m within a claystone band.
4. Borehole terminated at 6.45mbgl.
5. Borehole installed with 3.00m plain, 3.00m slotted 25mm pipe to base.

All dimensions in metres | Scale: **1:25**

Method Used:	Plant Used:	Drilled By:	Logged By:	Checked By:
Tracked window sampling	**Archway Competitor**	**GEH**	**JGriffin**	

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_018 PrjVersion: v8_06 - Core+Logs - 002 | Log WINDOW SAMPLE LOG - A4P | 29841_6_ALBERT_TERRACE.GPJ - v8_06. | 16/05/18 - 12:09 | JG9 |

WINDOW SAMPLE LOG

Contract:	Client:	Window Sample:
6 Albert Terrace Mews	**Mr. Mark Golinsky**	**BH1A**

Contract Ref:	Start:	Ground Level:	Co-ordinates:	Sheet:
29841	**12.03.18**	**---**	**---**	**2** of **2**
	End: **12.03.18**			

Progress	Samples / Tests				Water	Backfill & Instru-mentation	Description of Strata	Depth (Thick ness)	Material Graphic Legend
Window Run	Depth	No	Type	Results					
	5.00 5.00-5.45 5.00	4 5	D SPT V	N=19 c_u=180			Stiff to very stiff high to very high strength mottled bluish grey and brown silty CLAY. (LONDON CLAY FORMATION) *(stratum copied from 3.80m from previous sheet)* 4.80m : at 4.80m gypsum crystals present.	(2.65)	
	6.00 6.00-6.45 6.00	5 6	D SPT V	N=16 c_u=192				6.45	
							Window sample hole terminated at 6.45m depth.		

Drilling Progress and Water Observations

Date	Time	Borehole Depth (m)	Casing Depth (m)	Borehole Diameter (mm)	Water Depth (m)

General Remarks

All dimensions in metres | Scale: **1:25**

Method Used:	Plant Used:	Drilled By:	Logged By:	Checked By:
Tracked window sampling	**Archway Competitor**	**GEH**	**JGriffin**	

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_018 PrjVersion: v8_06 - Core+Logs - 002 | Log WINDOW SAMPLE LOG - A4P | 29841_6_ALBERT_TERRACE.GPJ - v8_06.
| 16/05/18 - 12:09 | JG9 |

TRIAL PIT LOG

Contract:	Client:	Trial Pit:
6 Albert Terrace Mews	**Mr. Mark Golinsky**	**TP1A**

Contract Ref:	Start: **12.03.18**	Ground Level:	Co-ordinates:	Sheet:
29841	End: **13.03.18**	**---**	**---**	**1** of **1**

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
						MADE GROUND: Concrete screed.	0.05	
						MADE GROUND: Dark brown very clayey SAND and GRAVEL. Gravel is of brick concrete and flints with medium cobble content of brick and concrete.	(0.95)	
						Trial pit terminated at 1.00m depth due to a concrete slab. Slab broken out and determined to a depth of 1.18mbgl.	1.00	

General Remarks

1. Trial pit remained dry and stable.
2. Trial pit terminated at 1.00mbgl on concrete slab. This was broken out and proven to extend to 1.18mbgl using a road pin.
3. Trial pit backfilled with arisings.

All dimensions in metres | Scale: **1:25**

Method Used:	Plant Used:	Logged By:	Checked By:
Hand dug	**Hand tools**	**CJBall**	

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_018 PrjVersion: v8_06 - Core+Logs - 002 | Log TRIAL PIT LOG - NO PLAN - A4P | 29841_6_ALBERT_TERRACE.GPJ - v8_06. | 16/05/18 - 12:13 | JG9 |

TRIAL PIT LOG

Contract:	Client:	Trial Pit:
6 Albert Terrace Mews	**Mr. Mark Golinsky**	**TP2A**

Contract Ref:	Start:	Ground Level:	Co-ordinates:	Sheet:
29841	**12.03.18**	**---**	**---**	**1** of **1**
	End: **12.03.18**			

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
						MADE GROUND: Brick cobbles.	0.08	
						MADE GROUND: Orange medium to coarse SAND (sub-base).	0.10	
0.50	1	ES	1xT1xV1xJ			MADE GROUND: Light brown slightly sandy gravelly CLAY. Sand is fine to coarse. Gravel is angular to subrounded fine to coarse of brick and flints with frequent roots and rootlets throughout. Occasional cobble of brick (15cm). 0.41m : at 0.41m very large cobble of brick 10cm in diameter. 0.54m : at 0.54m very large root 5cm in diameter.	(0.80)	
						Trial pit terminated at 0.90m depth.	0.90	

General Remarks

1. Trial pit remained dry and stable.
2. Trial pit terminated at 0.90mbgl.
3. Trial pit backfilled with arisings and finished in brick paving.

All dimensions in metres | Scale: **1:25**

Method Used:	Plant Used:	Logged By:	Checked By:
Hand dug	**Hand tools**	**JGriffin**	

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_018 PrjVersion: v8_06 - Core+Logs - 002 | Log TRIAL PIT LOG - NO PLAN - A4P | 29841_6_ALBERT_TERRACE.GPJ - v8_06. | 16/05/18 - 12:14 | JG9 |

TRIAL PIT LOG

Contract:	Client:	Trial Pit:
6 Albert Terrace Mews	**Mr. Mark Golinsky**	**TP3A**

Contract Ref:	Start:	Ground Level:	Co-ordinates:	Sheet:
29841	**12.03.18**	**---**	**---**	**1** of **1**
	End: **12.03.18**			

Samples and In-situ Tests				Water	Backfill	Description of Strata	Depth (Thickness)	Material Graphic Legend
Depth	No	Type	Results					
						MADE GROUND: Concrete.	0.08	
						MADE GROUND: Dark brown very clayey SAND and GRAVEL. Sand is fine to coarse. Gravel is fine of brick concrete and ceramic.	(0.72)	
							0.80	
						Orange SAND and GRAVEL. Sand is medium to coarse. Gravel is fine to coarse flints. 0.80m : at 0.80m layers of concrete 300/400/600mm	1.00	
						Trial pit terminated at 1.00m depth.		

General Remarks

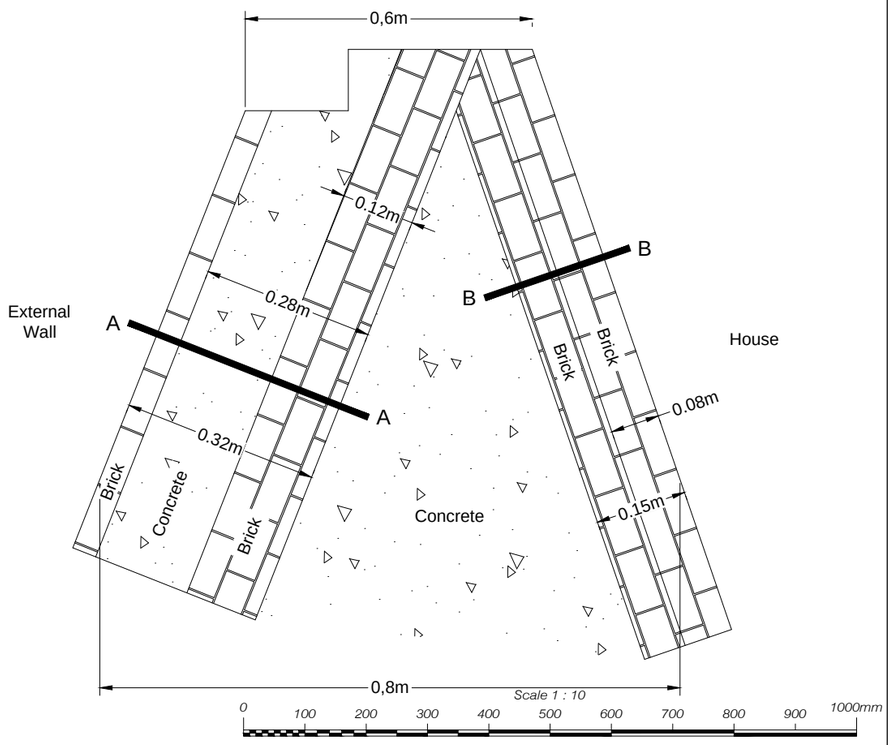
1. Trial pit remained dry and stable.
2. Trial pit terminated at 1.00mbgl.
3. Trial pit backfilled with arisings and finished with concrete.

All dimensions in metres | Scale: **1:25**

Method Used:	Plant Used:	Logged By:	Checked By:
Hand dug	**Hand tools**	**CJBall**	

GINT_LIBRARY_V8_06.GLB LibVersion: v8_06_018 PrjVersion: v8_06 - Core+Logs - 002 | Log TRIAL PIT LOG - NO PLAN - A4P | 29841_6_ALBERT_TERRACE.GPJ - v8_06. | 16/05/18 - 12:14 | JG9 |

Plan view:
(1:10)



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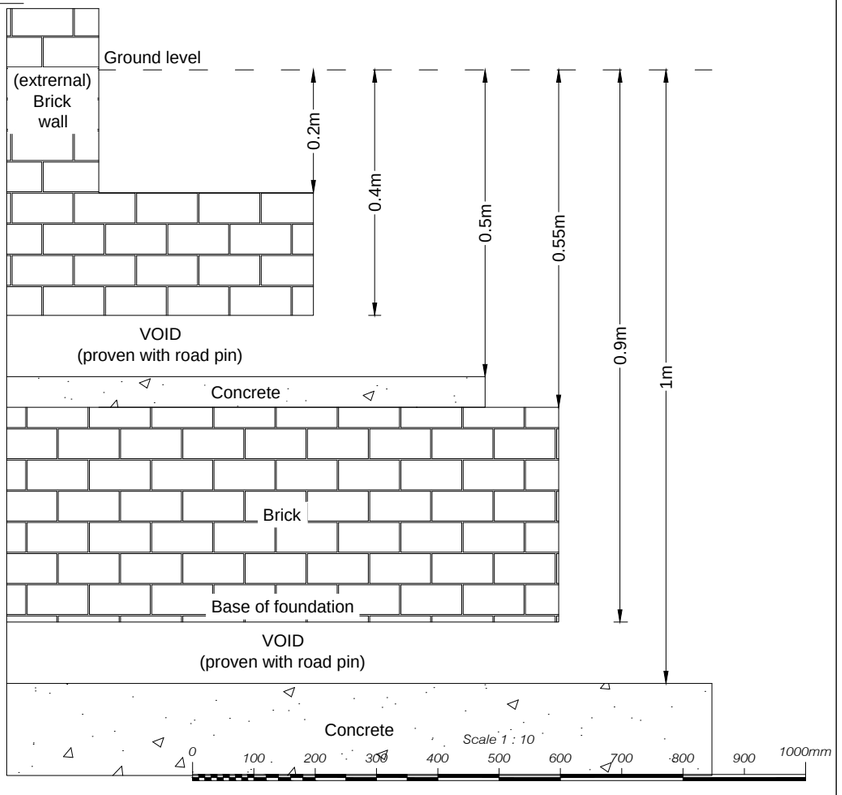

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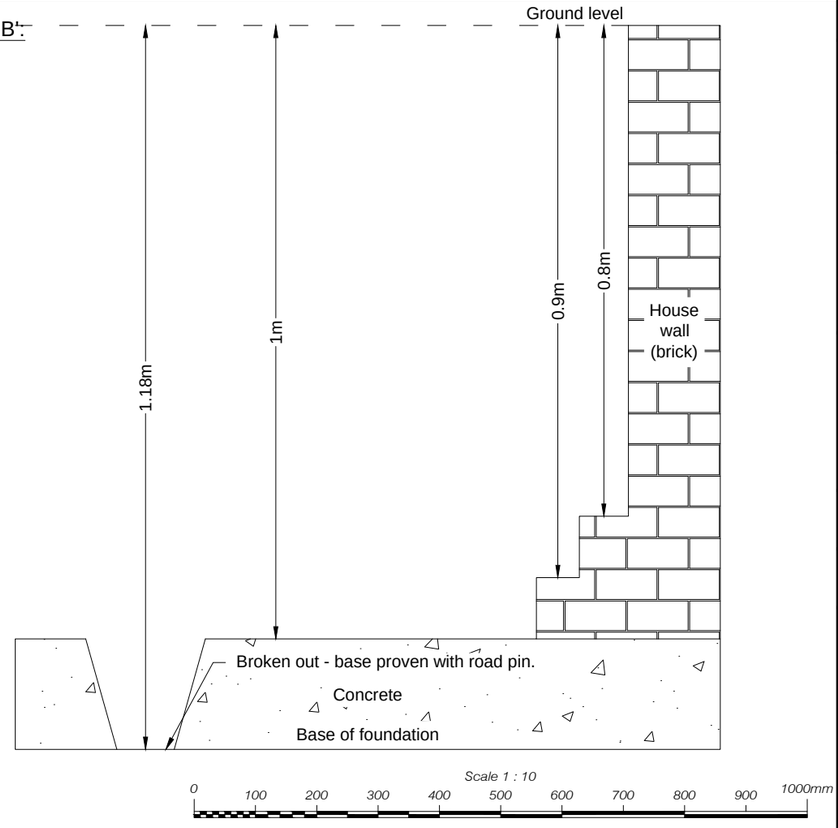

LEGEND

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Client

MR. MARK GOLINSKY

Project Title

6 ALBERT TERRACE MEWS

Drawing Title

FOUNDATION INSPECTION PIT TP1A

Drawn	Date	Checked	Date	Approved	Date
AP	19.03.18	JG	19.03.18	JG	19.03.18

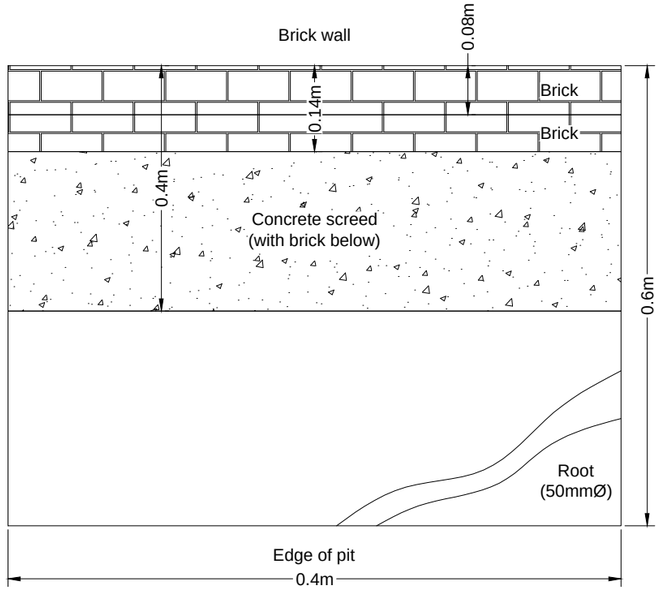
Scale	Orig Size	Dimensions
AS SHOWN	A3	m

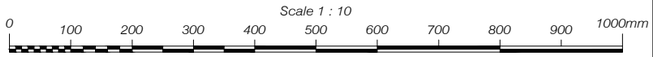
Project No.	Drawing File
29841 - R01(00)	29841 - (R01-00) TP.dwg

Drawing No.	Rev.
FIGURE TP1A	P1

Scale 1 : 10
0 0.1 0.2 0.3 0.4 0.5m

Plan view:
(1:10)





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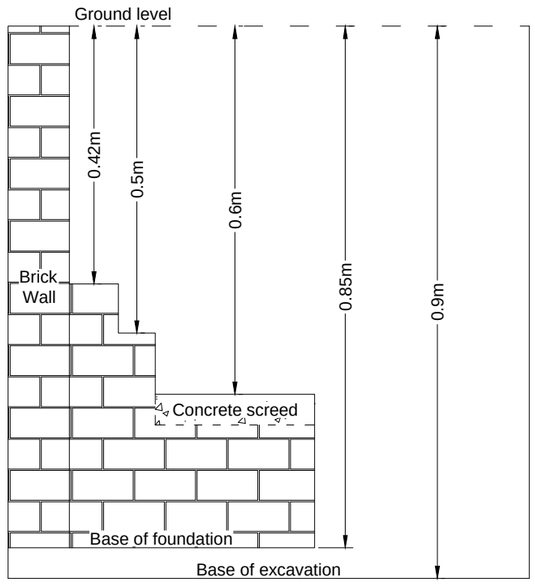

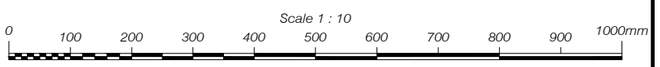

LEGEND

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Client
MR. MARK GOLINSKY

Project Title
6 ALBERT TERRACE MEWS

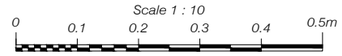
Drawing Title
FOUNDATION INSPECTION PIT TP2A

Drawn	Date	Checked	Date	Approved	Date
AP	19.03.18	JG	19.03.18	JG	19.03.18

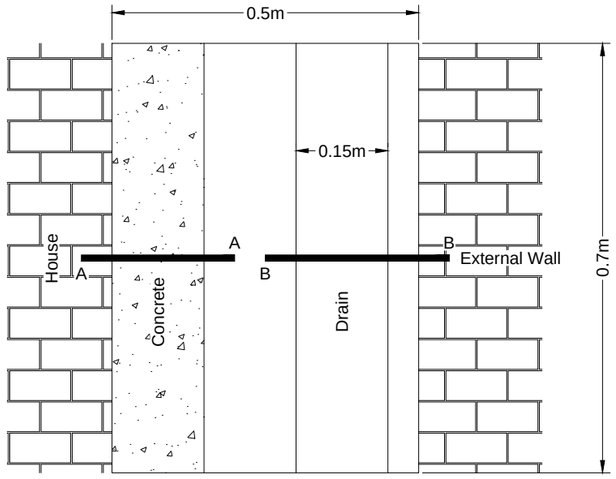
Scale	Orig Size	Dimensions
AS SHOWN	A3	m

Project No.	Drawing File
29841 - R01(00)	29841 - (R01-00) TP.dwg

Drawing No.	Rev.
FIGURE TP2A	P1



Plan view:
(1:10)



Scale 1 : 10

0 100 200 300 400 500 600 700 800 900 1000mm

LEGEND

Rev.	Date	Amendment	Drawn	Chkd.	Appd.

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Client

MR. MARK GOLINSKY

Project Title

6 ALBERT TERRACE MEWS

Drawing Title

FOUNDATION INSPECTION PIT TP3A

Drawn	Date	Checked	Date	Approved	Date
AP	19.03.18	JG	19.03.18	JG	19.03.18

Scale	Orig Size	Dimensions
AS SHOWN	A3	m

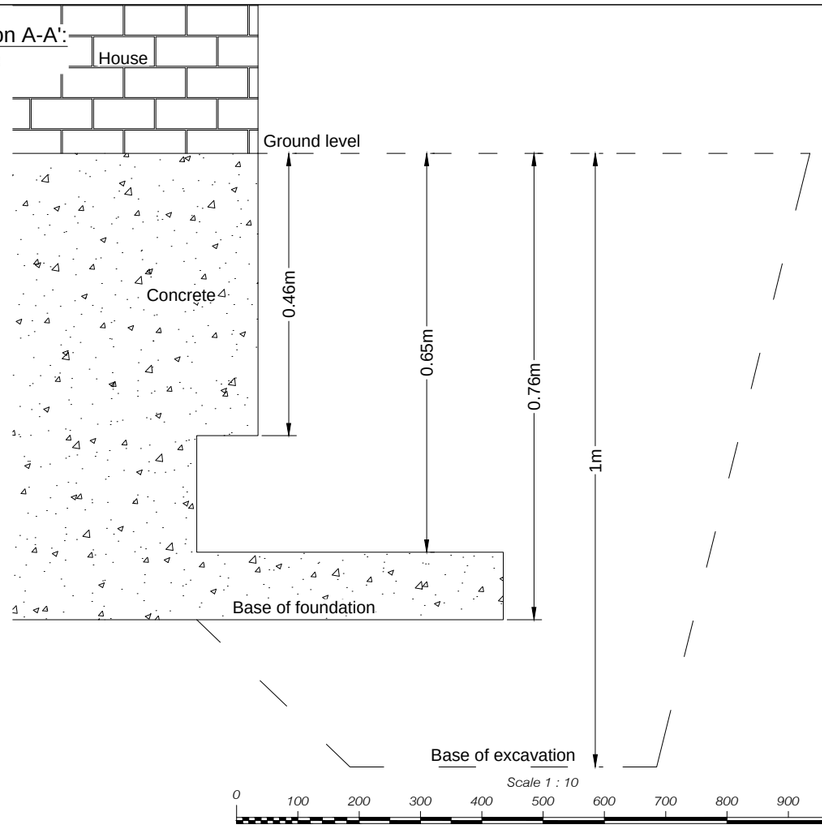
Project No.	Drawing File
29841 - R01(00)	29841 - (R01-00) TP.dwg

Drawing No.	Rev.
FIGURE TP3A	P1

Scale 1 : 10

0 0.1 0.2 0.3 0.4 0.5m

Section A-A':
(1:10)



Scale 1 : 10

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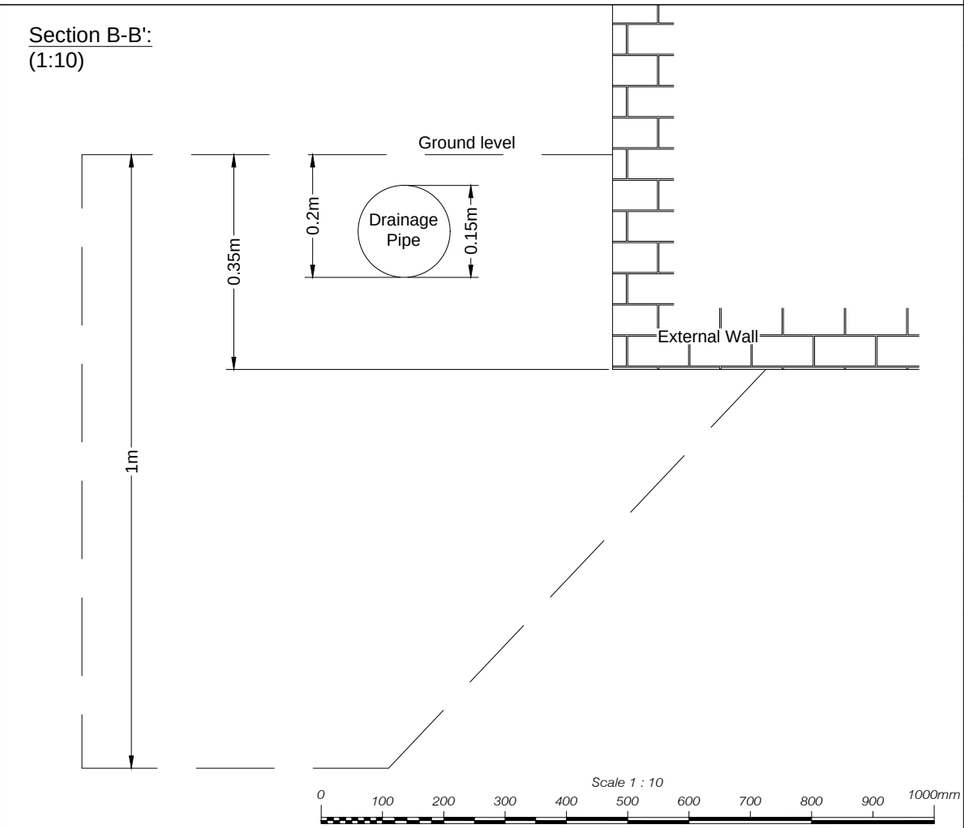
Section B-B':
(1:10)



Scale 1 : 10

0 100 200 300 400 500 600 700 800 900 1000mm

IN-SITU WATER MONITORING RESULTS

	Weather	Ground Conditions	Wind Conditions	Air Temperature (°C)	Equipment Used & Remarks
Round 1	Sunny	Dry	Light	20	Dipmeter

Exploratory Position ID	Pipe Ref	Pipe Diameter	Monitoring Round / Test Number	Reported Installation Depth (m)	Measured Installation Depth (mbgl)	Response Zone	Date & Time of Monitoring	Water Depth (mbgl)	Remarks
BH1A	1	25	1 / 1	6.00	6.20	3.00 to 6.00	04/05/2018	1.90	

Key: NDA denotes 'no data available'.

Compiled By	Date	Checked By	Date	Contract Ref:
	16/05/18			29841
Contract: 6 Albert Terrace Mews				Page: 1 of 1