

PROJECT:	PAGE: 1 OF 26
St John's Wood Park	DATE: JAN. 19
PROJECT NO: 5006835	BY: ML CHK'D: RL

Partnership House  
 Moorside Road  
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GROUND MOVEMENT ASSESSMENT TO CIRIA C760

NEIGHBOURING PROPERTY - 1 St John's Wood Park.

BUILDING WIDTH,  $L = 12600\text{mm}$   
 DISTANCE TO CLOSEST POINT FROM EXCAVATION & INSTAURATION,  $L_1 = 2900\text{mm}$   
 DISTANCE TO FURTHEST POINT FROM EXCAVATION & INSTAURATION,  $L_2 = 15500\text{mm}$

HEIGHT,  $H = 9000\text{mm}$

$L/H = 1.4$

MAX EXCAVATION DEPTH,  $H_b = 6.0\text{m}$   
 PILE WASH DEPTH,  $D = 13.25\text{m}$

- POTENTIAL MOVEMENT DUE TO INSTAURATION OF WASH (USING PARAMETERS FROM TABLE 6.1 & FIGURE 6.8)

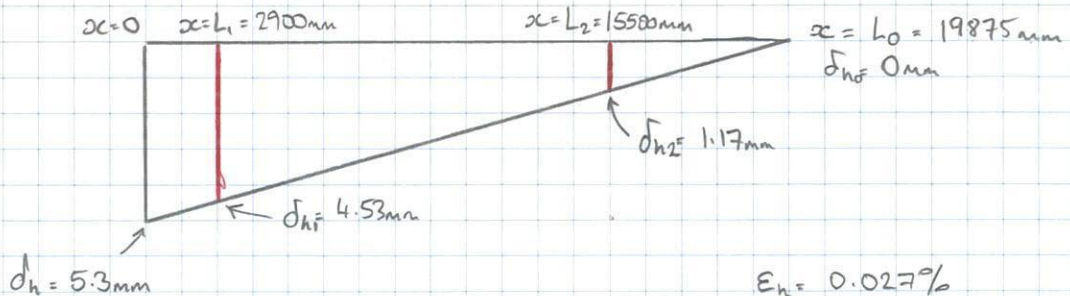
HORIZONTAL SURFACE MOVEMENT AT WASH (% OF WASH DEPTH) = 0.04%

$\therefore \text{MAX } \delta_h = (0.04/100) \times 13250\text{mm} = 5.3\text{mm}$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WASH DEPTH) = 1.5

$\therefore L_0 = 13.25\text{m} \times 1.5 = 19.875\text{m}$

HORIZONTAL MOVEMENT GRADIENT DUE TO INSTAURATION



PROJECT:	PAGE: 2 OF 26
St John's Wood Park	DATE: JAN 19
PROJECT NO: 5006835	BY: ML CHK'D: RL

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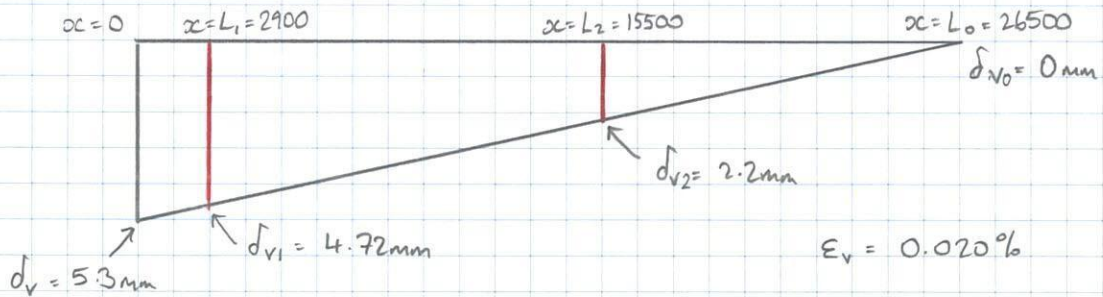
VERTICAL SURFACE MOVEMENT AT W/AU (% OF W/AU DEPTH) = 0.04%

$\therefore \text{MAX } \delta_v = (0.04/100) \times 13250\text{mm} = 5.3\text{mm}$

DISTANCE BEHIND W/AU TO NEGLIGIBLE MOVEMENT (MULTIPLE OF W/AU DEPTH) = 2.0

$\therefore L_0 = 13.25\text{m} \times 2.0 = 26.5\text{m}$

VERTICAL MOVEMENT GRADIENT DUE TO INSTAURATION



- POTENTIAL MOVEMENT DUE TO EXCAVATION OF GROUND IN FRONT OF W/AU. (USING PARAMETERS FROM TABLE 6.3 & FIGURE 6.15)

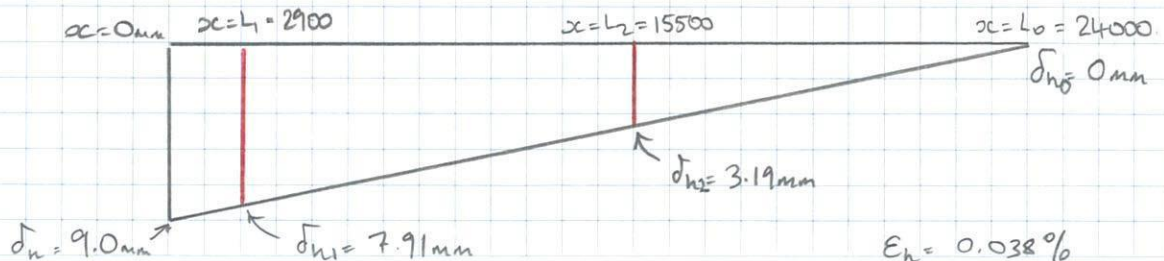
HORIZONTAL SURFACE MOVEMENT AT W/AU (% OF EXCAVATION DEPTH) = 0.15%

$\therefore \text{MAX } \delta_h = (0.15/100) \times 6000 = 9.0\text{mm}$

DISTANCE BEHIND W/AU TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAVATION DEPTH) = 4

$\therefore L_0 = 6\text{m} \times 4 = 24\text{m}$

HORIZONTAL MOVEMENT GRADIENT DUE TO EXCAVATION.



PROJECT:	PAGE: 3 OF 26
St John's Wood Park	DATE: JAN 19
PROJECT NO: 5006835	BY: ML CHK'D: RL

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VERTICAL SURFACE MOVEMENT AT WALL: [USE FIGURE 6.15b]

DISTANCE BEHIND WALL TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAV. DEPTH) = 3.5

$\therefore L_0 = 6.0 \times 3.5 = 21.0m$

INTERPRETATION OF FIGURE 6.15b :

→ @  $x = 0 \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.04%

→ @ POINT OF MAX SETTLEMENT

↳ SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.075%

↳ DISTANCE FROM WALL / MAX EXCAVATION DEPTH = 0.64

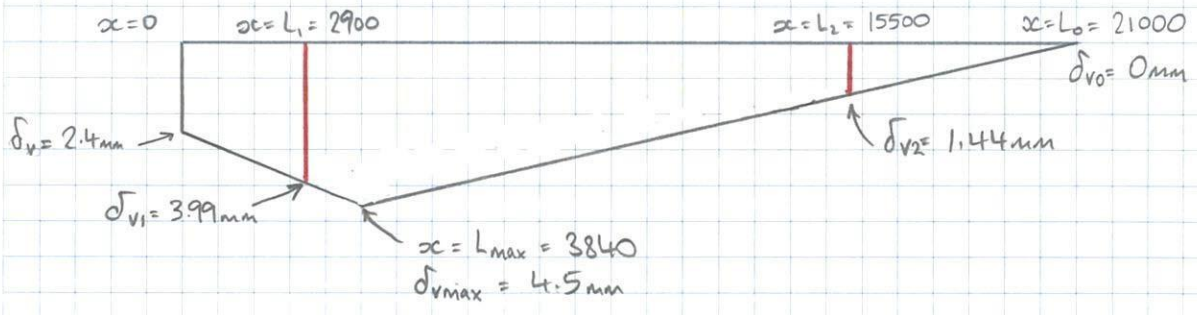
→ @  $x = 21.0m \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0%

@  $x = 0$  VERTICAL MOVEMENT =  $(0.04 / 100) \times 6000 = 2.4mm$

@  $\delta_v$  (MAX) VERTICAL MOVEMENT =  $(0.075 / 100) \times 6000 = 4.5mm$

@  $\delta_v$  (MAX) DISTANCE FROM WALL =  $0.64 \times 6000 = 3840mm$

$\therefore$  SIMPLIFIED VERTICAL MOVEMENT GRADIENT:



PROJECT:	PAGE: 4 OF 26
St John's Wood Park	DATE: JAN 19
PROJECT NO: 5006835	BY: ML. CHKD: RL

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- COMBINED POTENTIAL MOVEMENTS DUE TO INSTANTATION & EXCAVATION.

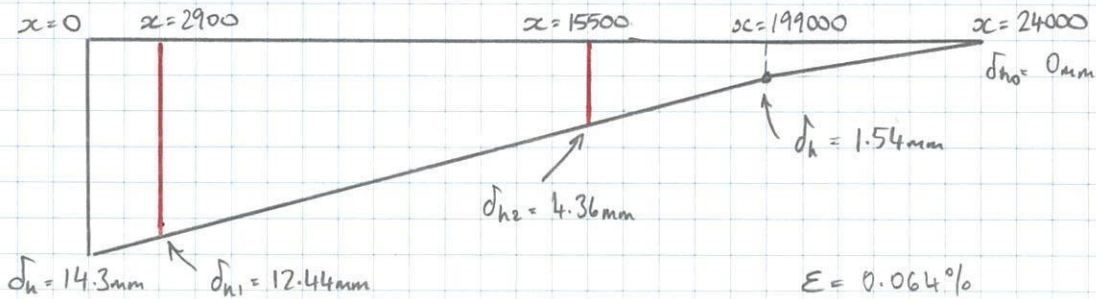
HORIZONTAL MOVEMENT:

INSTANTATION:  $\delta_h = 5.3 \text{ mm}$ ,  $\delta_{h1} = 4.53 \text{ mm}$ ,  $\delta_{h2} = 1.17 \text{ mm}$ ,  $L_0 = 19900 \text{ mm}$

EXCAVATION:  $\delta_h = 9.0 \text{ mm}$ ,  $\delta_{h1} = 7.91 \text{ mm}$ ,  $\delta_{h2} = 3.19 \text{ mm}$ ,  $L_0 = 24000 \text{ mm}$

FIND MOVEMENT DUE TO EXCAV. @ 19900mm.

$$\delta_h = \tan\left(\tan^{-1}\left(\frac{9.0}{24000}\right)\right) \times (24000 - 19900) = 1.54 \text{ mm}$$



VERTICAL MOVEMENT:

INSTANTATION:  $\delta_v = 5.3 \text{ mm}$ ,  $\delta_{v1} = 4.72 \text{ mm}$ ,  $\delta_{v2} = 2.2 \text{ mm}$ ,  $L_0 = 26500$

EXCAVATION:  $\delta_v = 2.4 \text{ mm}$ ,  $\delta_{v1} = 3.99 \text{ mm}$ ,  $\delta_{v2} = 1.44 \text{ mm}$ ,  $L_0 = 21000$ ,  $\delta_{vmax} = 4.5 \text{ mm}$   
 $L_{max} = 3840 \text{ mm}$

FIND MOVEMENT DUE TO INSTANTATION @ 21000

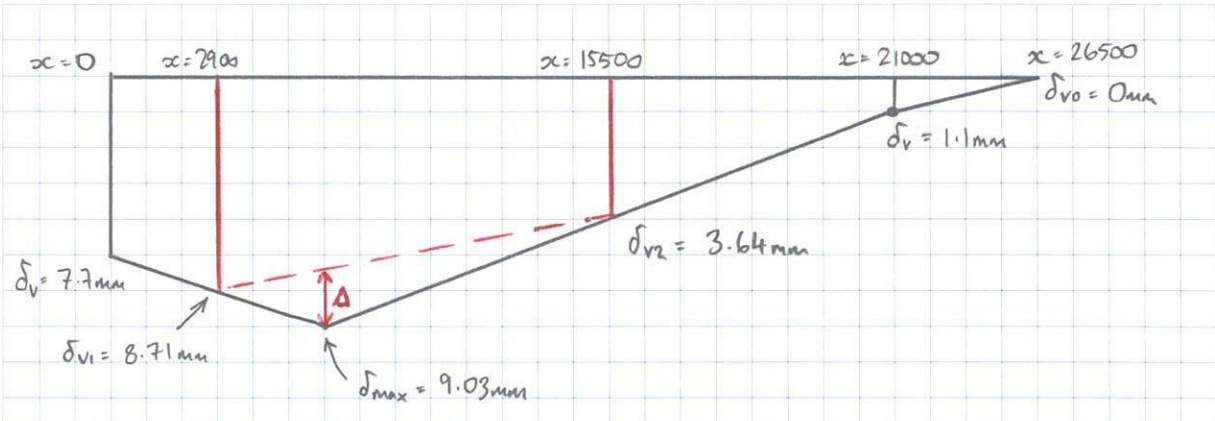
$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 21000) = 1.1 \text{ mm}$$

FIND MOVEMENT DUE TO INSTANTATION @ 3840 +  $\delta_{vmax}$

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 3840) + 4.5 = 9.03 \text{ mm}$$

PROJECT:	St John's Wood Park	PAGE:	5 OF 26
PROJECT NO:	5006835	DATE:	JAN 19
		BY:	ML
		CHK'D:	RL

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∴ RELATIVE VERTICAL MOVEMENT WITHIN BUILDING :

$$\Delta = 9.03 - \left[ \tan \left( \tan^{-1} \left( \frac{d_{v1} - d_{v2}}{L_2 - L_1} \right) \right) \times (L_2 - L_{max}) \right] + d_{v2}$$

$$= 2.90 \text{ mm}$$

• CALCULATION OF DAMAGE CATEGORY (USING FIGURE 6.27 & TABLE 6.4)

CAMDEN COUNCIL REQUIRES A DAMAGE CATEGORY NOT EXCEEDING CATEGORY 1 'VERY SLIGHT' ON THE BURLAND SCALE.

∴  $E_{lim} = 0.075\%$

$E_k = 0.064\%$

$\Delta/L = 2.90 / 12600 \times 100 = 0.023\%$

CONSERVATIVELY USE LINE 'L/H = 1.5' ⇒ EQ. OF LINE =  $y = 1 - x$

$y = \Delta/L = 0.023$  ,  $x = E_k = 0.064$

∴ TOTAL TENSILE STRAIN,  $E = 0.023 + 0.064 = 0.087\%$

∴ MOVEMENT WITHIN DAMAGE CATEGORY 2 'SLIGHT'

MITIGATION MEASURES WILL THEREFORE BE REQUIRED, SEE OVER.

PROJECT:	PAGE: 6 OF 26
St John's Wood Park	DATE: JAN 19
PROJECT NO: 5006835	BY: ML CHK'D: RL

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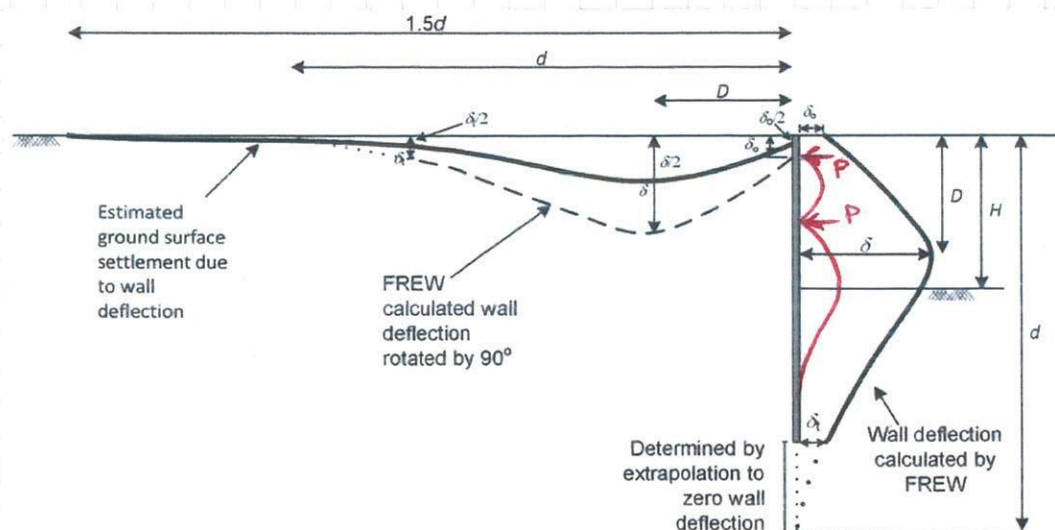
FIGURE 6.17 SHOWS THE RELATIONSHIP BETWEEN ANALYSED LATERAL (PROPPED) WALL DEFLECTIONS AND PREDICTED GROUND SURFACE SETTLEMENTS IN STIFF GROUND

THE FIGURE SHOWS THAT THE ESTIMATED GROUND SURFACE SETTLEMENT DUE TO WALL DEFLECTION IS CIRCA 1/2 THE DEFLECTION EXPERIENCED BY THE WALL.

THEREFORE, LIMITING THE DEFLECTION OF THE WALL WILL REDUCE THE TOTAL TENSIVE STRAIN,  $\epsilon$ .

THE WALL DEFLECTION WILL THEREFORE BE LIMITED DURING CONSTRUCTION AS PER APPENDIX H.

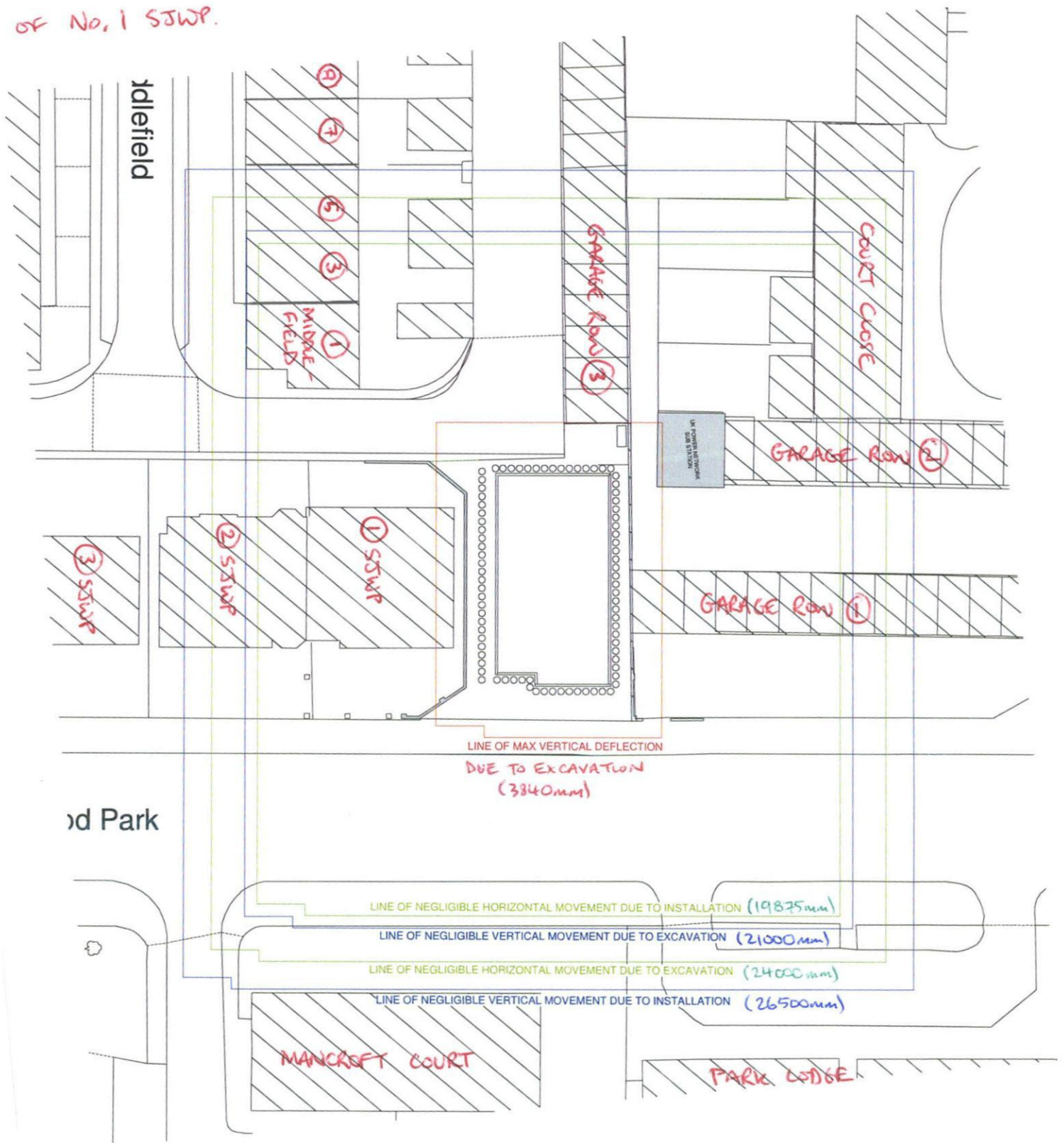
FINAL PROPPING SCHEME IS TO BE DECIDED BY THE CONTRACTOR, HOWEVER, WE WOULD RECOMMEND THAT THEY CONSIDER A SECONDARY LINE OF PROPPING AT MID-HEIGHT OF THE EXCAVATION DEPTH. A MARK-UP OF FIGURE 6.17 SHOWS HOW THIS WOULD AFFECT THE DEFLECTION OF THE WALL.



THE SECONDARY LINE OF PROPPING WILL SIGNIFICANTLY REDUCE WALL DEFLECTIONS, AND SUBSEQUENTLY LIMIT GROUND MOVEMENT TO WITHIN THE ACCEPTABLE  $\epsilon$  LIMIT BY INSPECTION.

THE RESIDUAL IMPACTS TO THE NEIGHBOURING BUILDING WILL BE POSSIBLE FINE CRACKING THAT CAN EASILY BE TREATED DURING NORMAL DECORATION [DAMAGE CATEGORY 1 - VERY SLIGHT]

PLAN SHOWING LINES OF INFLUENCE OF HORIZONTAL & VERTICAL GROUND MOVEMENTS DUE TO INSTALLATION OF WALL & EXCAVATION. IN THE CONSTRUCTION OF THE PROPOSED BASEMENT. LINES PLOTTED FROM RESULTS OBTAINED IN ASSESSMENT OF NO. 1 SJWP.



PROJECT:	St John's Wood Park.	PAGE:	8	OF	26
PROJECT NO:	5006835	DATE:	JAN 19		
		BY:	ML.	CHK'D:	RL

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### NEIGHBOURING PROPERTY - 2 St John's Wood Park.

BUILDING CONSTRUCTION AND DIMENSIONS ARE IDENTICAL TO No. 1 SJWP.

BY INSPECTION OF THE LINE OF INFLUENCE DIAGRAM IT CAN BE SEEN THAT THE STRUCTURE IS NOT NEAR TO THE LINE OF MAX VERTICAL DEFLECTION & THE LINES OF NEGLIGIBLE MOVEMENT, BOTH HORIZONTAL & VERTICAL, DUE TO INSTALLATION AND EXCAVATION ARE WITHIN THE BUILDING ENVELOPE.

∴ THE BUILDING WILL EXPERIENCE VERY LOW DEFLECTIONS & STRAIN RESULTING IN A SIGNIFICANTLY LOWER RISK OF DAMAGE & CAN BE CONSIDERED ACCEPTABLE BY INSPECTION OF PREVIOUS CALCULATIONS.

### NEIGHBOURING PROPERTY - 3 St John's Wood Park.

BY INSPECTION OF LINE OF INFLUENCE DIAGRAM THE ENTIRE STRUCTURE LIES OUTSIDE THE LINES OF NEGLIGENT DEFLECTION FOR BOTH VERTICAL & HORIZONTAL MOVEMENT DUE TO INSTALLATION + EXCAVATION.

### MANCROFT COURT

AS PER No. 3 SJWP

### PARK LODGE

AS PER No. 3 SJWP.



PROJECT:

St John's Wood Park

PAGE: 9 OF 26

DATE: JAN. 19

PROJECT NO: 5006835

BY: ML CHK'D: RL

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GROUND MOVEMENT ASSESSMENT TO CIRIA C760

NEIGHBOURING PROPERTY - 1 MIDDLEFIELD

BUILDING WIDTH,  $L = 10200 \text{ mm}$

DISTANCE TO CLOSEST POINT FROM EXCAVATION & INSTAURATION,  $L_1 = 10800 \text{ mm}$

DISTANCE TO FURTHEST POINT FROM EXCAVATION & INSTAURATION,  $L_2 = 21000 \text{ mm}$

HEIGHT,  $H = 9000 \text{ mm}$

$L/H = 1.13$

MAX EXCAVATION DEPTH,  $H_b = 6.0 \text{ m}$

PILE WASH DEPTH,  $D = 13.25 \text{ m}$

- POTENTIAL MOVEMENT DUE TO INSTAURATION OF WASH (USING PARAMETERS FROM TABLE 6.1 & FIGURE 6.8)

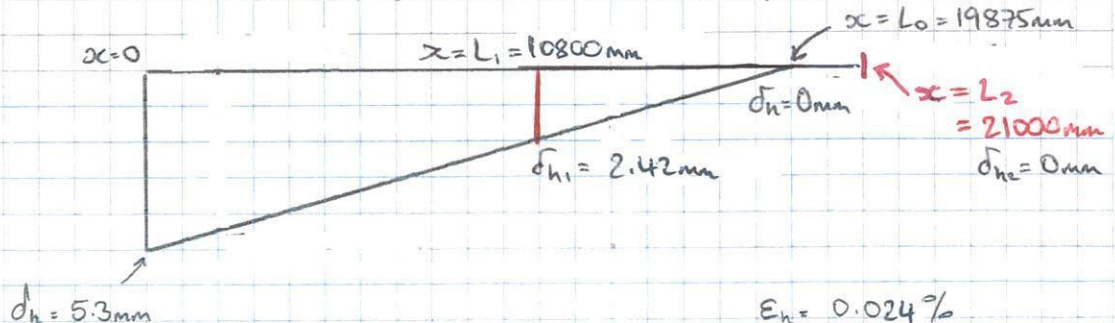
HORIZONTAL SURFACE MOVEMENT AT WASH (% OF WASH DEPTH) = 0.04%

$\therefore \text{MAX } \delta_h = (0.04/100) \times 13250 \text{ mm} = 5.3 \text{ mm}$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WASH DEPTH) = 1.5

$\therefore L_0 = 13.25 \text{ m} \times 1.5 = 19.875 \text{ m}$

HORIZONTAL MOVEMENT GRADIENT DUE TO INSTAURATION



PROJECT:

St John's Wood Park

PROJECT NO:

5006835

PAGE: 10 OF 26

DATE: JAN 19

BY: ML CHK'D: RL

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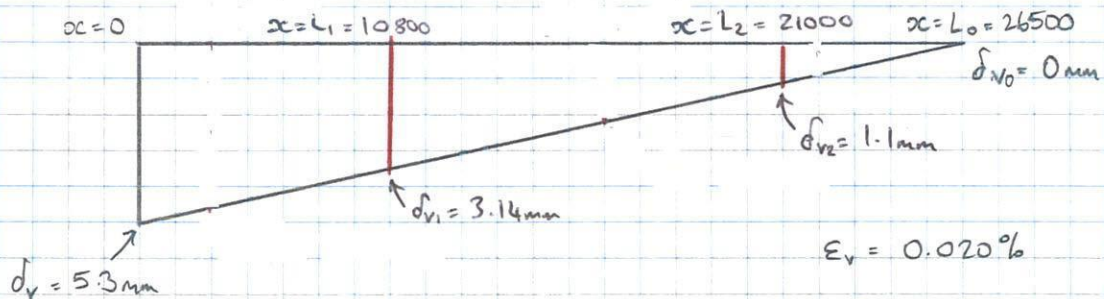
VERTICAL SURFACE MOVEMENT AT WASH (% OF WASH DEPTH) = 0.04%

$$\therefore \text{MAX } \delta_v = (0.04/100) \times 13250\text{mm} = 5.3\text{mm}$$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WASH DEPTH) = 2.0

$$\therefore L_0 = 13.25\text{m} \times 2.0 = 26.5\text{m}$$

VERTICAL MOVEMENT GRADIENT DUE TO INSTALLATION



- POTENTIAL MOVEMENT DUE TO EXCAVATION OF GROUND IN FRONT OF WASH (USING PARAMETERS FROM TABLE 6.3 & FIGURE 6.15)

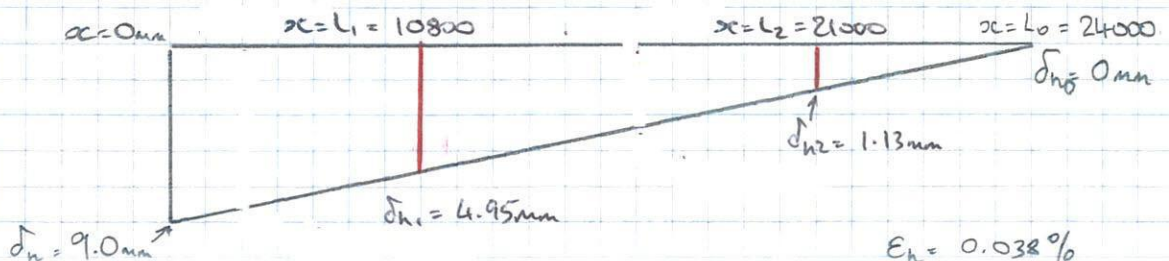
HORIZONTAL SURFACE MOVEMENT AT WASH (% OF EXCAVATION DEPTH) = 0.15%

$$\therefore \text{MAX } \delta_h = (0.15/100) \times 6000 = 9.0\text{mm}$$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAVATION DEPTH) = 4

$$\therefore L_0 = 6\text{m} \times 4 = 24\text{m}$$

HORIZONTAL MOVEMENT GRADIENT DUE TO EXCAVATION.



PROJECT:

St John's Wood Park

PROJECT NO:

5006835

PAGE: 11 OF 26

DATE: JAN 19

BY: ML CHK'D: RL

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VERTICAL SURFACE MOVEMENT AT WALL: [USE FIGURE 6.15b]

DISTANCE BEHIND WALL TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAV. DEPTH) = 3.5

$$\therefore L_0 = 6.0 \times 3.5 = 21.0\text{m}$$

INTERPRETATION OF FIGURE 6.15b:

→ @  $x = 0 \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.04%

→ @ POINT OF MAX SETTLEMENT

↳ SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.075%

↳ DISTANCE FROM WALL / MAX EXCAVATION DEPTH = 0.64

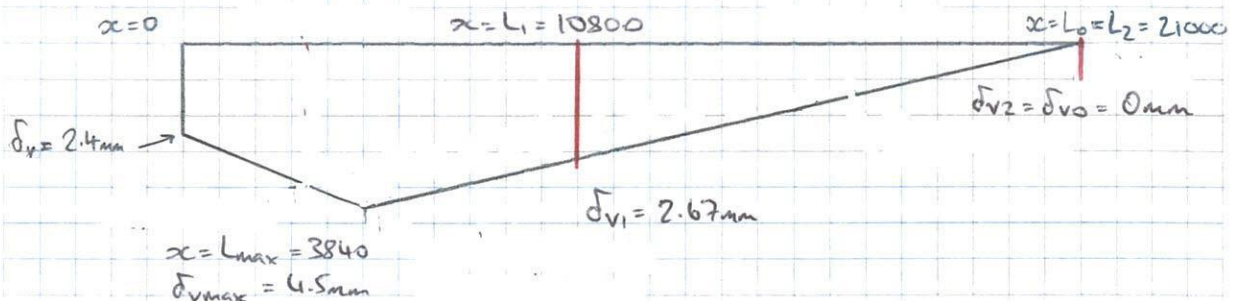
→ @  $x = 21.0\text{m} \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0%

@  $x = 0$  VERTICAL MOVEMENT =  $(0.04 / 100) \times 6000 = 2.4\text{mm}$

@  $\delta_v$  (MAX) VERTICAL MOVEMENT =  $(0.075 / 100) \times 6000 = 4.5\text{mm}$

@  $\delta_v$  (MAX) DISTANCE FROM WALL =  $0.64 \times 6000 = 3840\text{mm}$

$\therefore$  SIMPLIFIED VERTICAL MOVEMENT GRADIENT:



PROJECT:	PAGE: 12 OF 26
St John's Wood Park	DATE: JAN 19
PROJECT NO: 5006885	BY: ML. CHK'D: RL

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- COMBINED POTENTIAL MOVEMENTS DUE TO INSTANTATION & EXCAVATION.

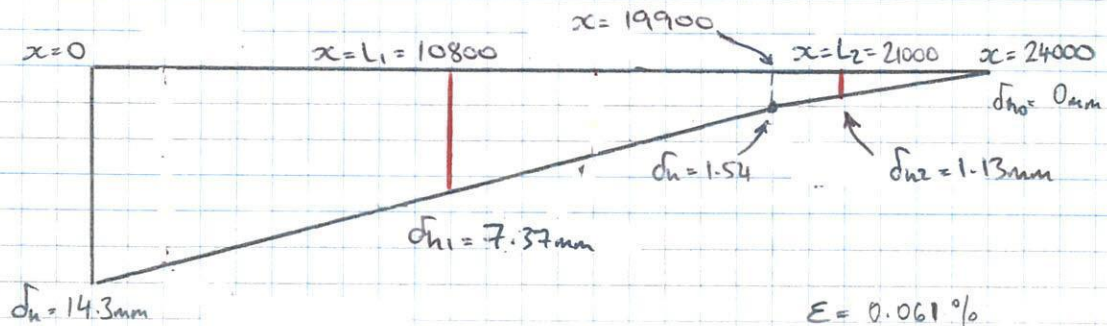
HORIZONTAL MOVEMENT:

INSTANTATION:  $\delta_h = 5.3\text{mm}$ ,  $\delta_{h1} = 2.42\text{mm}$ ,  $\delta_{h2} = 0\text{mm}$ ,  $L_0 = 19900\text{mm}$

EXCAVATION:  $\delta_h = 9.0\text{mm}$ ,  $\delta_{h1} = 4.95\text{mm}$ ,  $\delta_{h2} = 1.13\text{mm}$ ,  $L_0 = 24000\text{mm}$

FIND MOVEMENT DUE TO EXCAV. @ 19900mm

$$\delta_h = \tan\left(\tan^{-1}\left(\frac{9.0}{24000}\right)\right) \times (24000 - 19900) = 1.54\text{mm}$$



VERTICAL MOVEMENT:

INSTANTATION:  $\delta_v = 5.3\text{mm}$ ,  $\delta_{v1} = 3.14\text{mm}$ ,  $\delta_{v2} = 1.1\text{mm}$ ,  $L_0 = 26500$

EXCAVATION:  $\delta_v = 2.4\text{mm}$ ,  $\delta_{v1} = 2.67\text{mm}$ ,  $\delta_{v2} = 0\text{mm}$ ,  $L_0 = 21000$ ,  $\delta_{v\text{max}} = 4.5\text{mm}$   
 $L_{\text{max}} = 3840\text{mm}$

FIND MOVEMENT DUE TO INSTANTATION @ 21000

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 21000) = 1.1\text{mm}$$

FIND MOVEMENT DUE TO INSTANTATION @ 3840 +  $\delta_{v\text{max}}$

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 3840) + 4.5 = 9.03\text{mm}$$

PROJECT:

St John's Wood Park

PAGE: 13 OF 26

DATE: JAN 19

PROJECT NO:

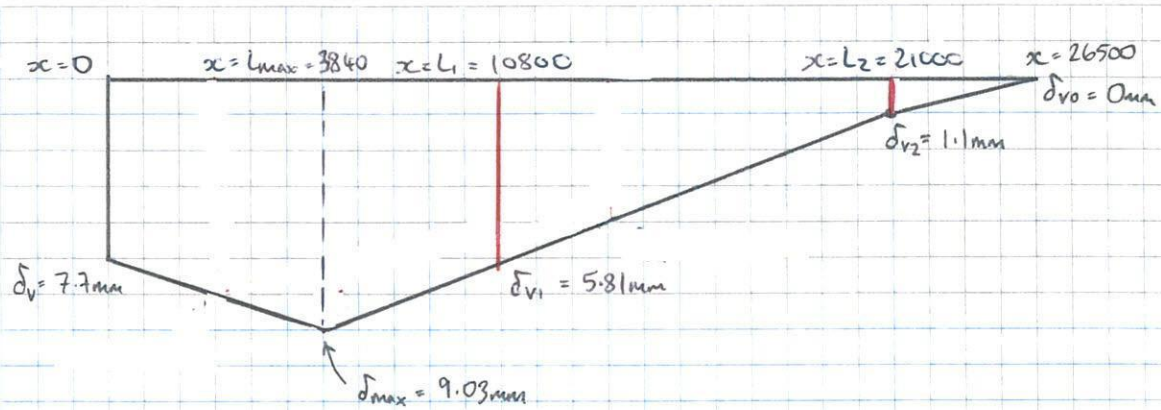
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∴ RELATIVE VERTICAL MOVEMENT WITHIN BUILDING :

$$\Delta = 0\text{mm}$$

BUILDING EXPERIENCES NEGLECTABLE RELATIVE VERTICAL MOVEMENT.

- CALCULATION OF DAMAGE CATEGORY (USING FIGURE 6.27 & TABLE 6.4)

CAMDEN COUNCIL REQUIRES A DAMAGE CATEGORY NOT EXCEEDING CATEGORY 1 'VERY SLIGHT' ON THE BURLAND SCALE.

$$\therefore E_{lim} = 0.075\%$$

$$E_n = 0.064\%$$

$$\Delta/L = 0 / 12600 \times 100 = 0.0\%$$

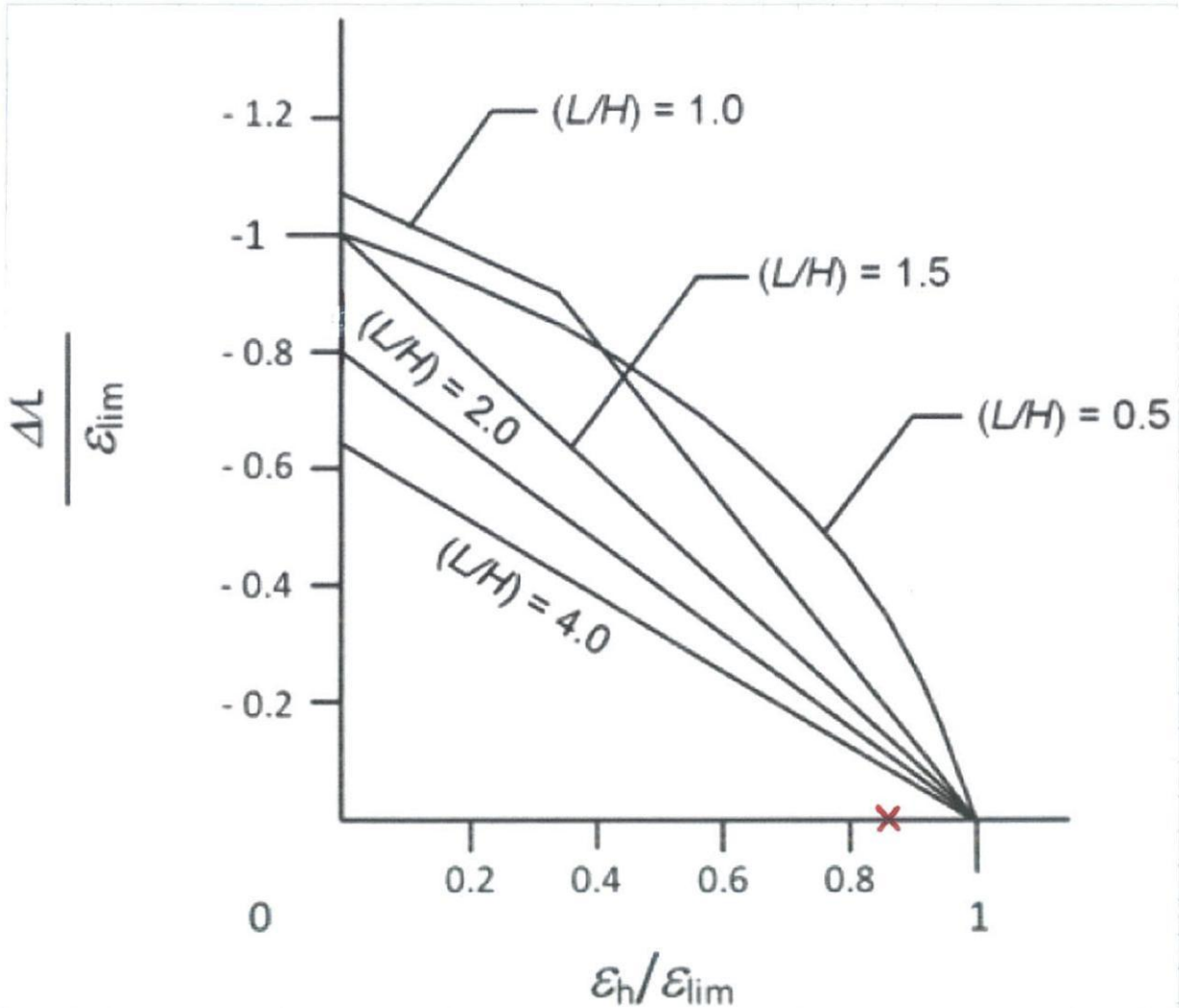
$$E_n/E_{lim} = 0.86$$

$$\Delta/L/E_{lim} = 0.00$$

SEE OVER FOR PLOT ONTO FIGURE 6.27

PROJECT:	SE John's Wood Park	PAGE:	14	OF	26
PROJECT NO:	5006835	DATE:	JAN 19		
		BY:	MU	CHK'D:	RL

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∴ GROUND MOVEMENT LIES WITHIN THE ACCEPTED LIMITS TO RESTRICT DAMAGE CATEGORY TO 1 - VERY SLIGHT.

THE PROPPING PROPOSED IN THE ISJWP CALCULATION WILL FURTHER RESTRICT THIS GROUND MOVEMENT.

No 1. MIDDLEFIELD IS THE WORST CASE OF AN BUILDING ON MIDDLEFIELD THE CONSTRUCTION AND DIMENSIONS ARE SIMILAR & THIS IS THE CLOSEST TO THE BASEMENT.

∴ BY INSPECTION THE OTHER BUILDINGS WILL BE IN DAMAGE CATEGORY 1 'VERY SLIGHT' OR LESS.

PROJECT:	PAGE: 15 OF 26
St John's Wood Park.	DATE: JAN 19
PROJECT NO: 5006835	BY: ML. CHK'D: RL

Partnership House  
Moorside Road  
Winchester  
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BY INSPECTION OF THE RESULTS FROM THE G.M.A OF 1 MIDDLEFIELD THE VALUE OF  $E_h$  DOES NOT EXCEED 0.064%, REDUCING IF BUILDING IS LOCATED OUTSIDE OF THE LINES OF INFLUENCE AND  $\Delta$  IS ONLY PRESENT IF THE LINE OF MAX VERTICAL DEFLECTION LIES WITHIN THE BUILDING ENVELOPE.

- ∴ BY INSPECTION OF THE MARKED-UP FIGURE 6.27 ALL STRUCTURES IN THE VICINITY THAT DO NOT CONTAIN THE LINE OF MAX VERTICAL DEFLECTION DUE TO EXCAVATION WILL HAVE A 'VERY SLIGHT' DAMAGE CATEGORY [1] OR LESS. [REGARD LESS OF L/H AS ALL PASS X AXIS @ 1.0].
- ∴ COURT CLOSE, GARAGE ROW (3), GARAGE ROW (2) ALL IN DAMAGE CATEGORY 1 - 'VERY SLIGHT' BY INSPECTION.

TUBE TUNNELS ARE ALSO PRESENT & RUN UNDER ST JOHN'S WOOD PARK (ROAD) THESE TUNNELS ARE ALSO OUTSIDE THE LINE OF MAX VERTICAL DEFLECTION. CIRIA C760 GROUND SURFACE MOVEMENTS & AS SUCH ARE NOT REPRESENTATIVE OF THE GROUND MOVEMENT ON SUBTERRANEAN STRUCTURES, WHICH WILL BE LOWER THAN THAT EXPERIENCED ON THE SURFACE. CONSULTATION WITH LUL (ASSET OWNER) SHALL BE CARRIED OUT & MAINTAINED DURING THE DETAILED DESIGN + CONSTRUCTION PHASES TO LIMIT & CONTROL GROUND MOVEMENTS & THE EFFECTS ON THE TUNNELS.

PROJECT: St John's Wood Park  
 PAGE: 16 OF 26  
 DATE: JAN. 19  
 PROJECT NO: 5006835  
 BY: ML  
 CHK'D: RL

Partnership House  
 Moorside Road  
 Winchester  
 SO23 7RX

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GROUND MOVEMENT ASSESSMENT TO CIRIA C760

NEIGHBOURING PROPERTY - SUBSTATION

BUILDING WIDTH,  $L = 6000$

DISTANCE TO CLOSEST POINT FROM EXCAVATION & INSTAURATION,  $L_1 = 3400$

DISTANCE TO FURTHEST POINT FROM EXCAVATION & INSTAURATION,  $L_2 = 9400$

HEIGHT,  $H = 3000 \text{ mm}$

$L/H = 2.0$

MAX EXCAVATION DEPTH,  $H_b = 6.0 \text{ m}$

PILE WASH DEPTH,  $D = 13.25 \text{ m}$

- POTENTIAL MOVEMENT DUE TO INSTAURATION OF WASH  
 (USING PARAMETERS FROM TABLE 6.1 & FIGURE 6.8)

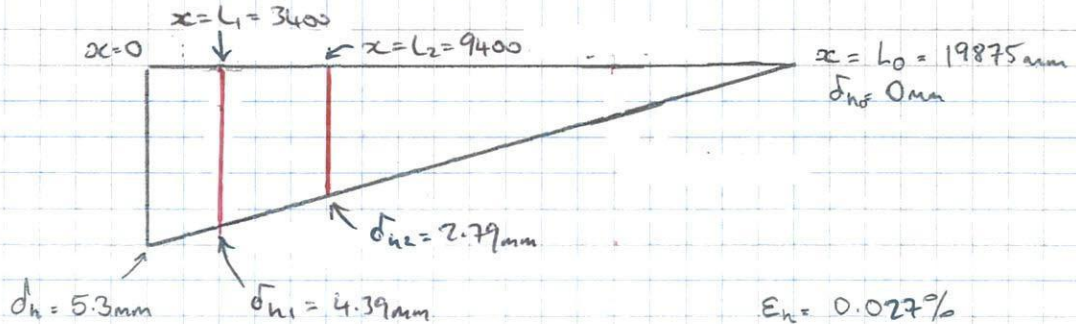
HORIZONTAL SURFACE MOVEMENT AT WASH (% OF WASH DEPTH) = 0.04%

$\therefore \text{MAX } \delta_h = (0.04/100) \times 13250 \text{ mm} = 5.3 \text{ mm}$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WASH DEPTH) = 1.5

$\therefore L_0 = 13.25 \text{ m} \times 1.5 = 19.875 \text{ m}$

HORIZONTAL MOVEMENT GRADIENT DUE TO INSTAURATION





PROJECT:

St John's Wood Park

PROJECT NO:

5006835

PAGE: 17 OF 26

DATE: JAN 19

BY: ML CHK'D: RL

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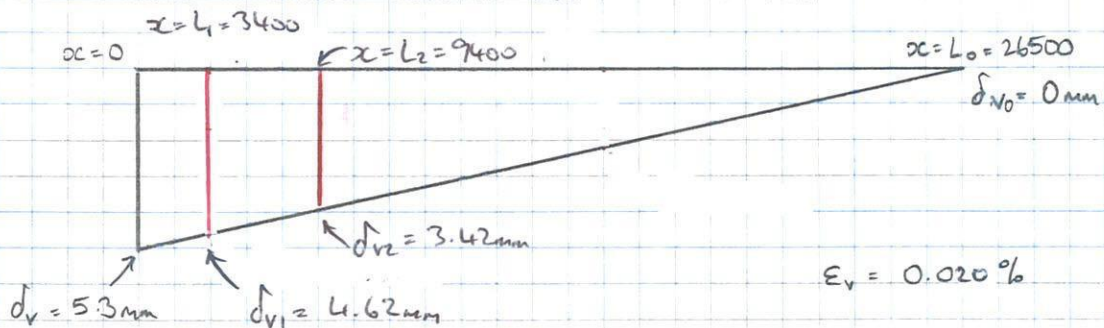
VERTICAL SURFACE MOVEMENT AT WASH (% OF WASH DEPTH) = 0.04%

$$\therefore \text{MAX } \delta_v = (0.04/100) \times 13250\text{mm} = 5.3\text{mm}$$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WASH DEPTH) = 2.0

$$\therefore L_0 = 13.25\text{m} \times 2.0 = 26.5\text{m}$$

VERTICAL MOVEMENT GRADIENT DUE TO INSTAURATION



- POTENTIAL MOVEMENT DUE TO EXCAVATION OF GROUND IN FRONT OF WASH (USING PARAMETERS FROM TABLE 6.3 & FIGURE 6.15)

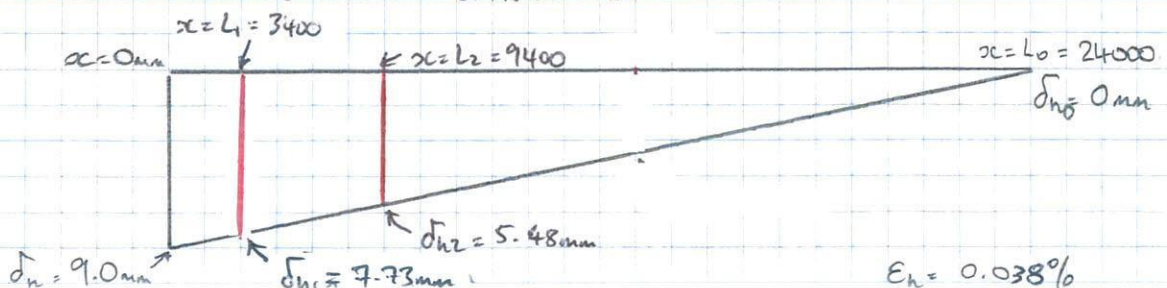
HORIZONTAL SURFACE MOVEMENT AT WASH (% OF EXCAVATION DEPTH) = 0.15%

$$\therefore \text{MAX } \delta_h = (0.15/100) \times 6000 = 9.0\text{mm}$$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAVATION DEPTH) = 4

$$\therefore L_0 = 6\text{m} \times 4 = 24\text{m}$$

HORIZONTAL MOVEMENT GRADIENT DUE TO EXCAVATION.



PROJECT:

St John's Wood Park

PROJECT NO:

5006835

PAGE: 18 OF 26

DATE: JAN 19

BY: ML CHK'D: RL

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VERTICAL SURFACE MOVEMENT AT WAU: [USE FIGURE 6.15b]

DISTANCE BEHIND WAU TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAV. DEPTH) = 3.5

$$\therefore L_0 = 6.0 \times 3.5 = 21.0\text{m}$$

INTERPRETATION OF FIGURE 6.15b:

→ @  $x = 0 \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.04%

→ @ POINT OF MAX SETTLEMENT

↳ SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.075%

↳ DISTANCE FROM WAU / MAX EXCAVATION DEPTH = 0.64

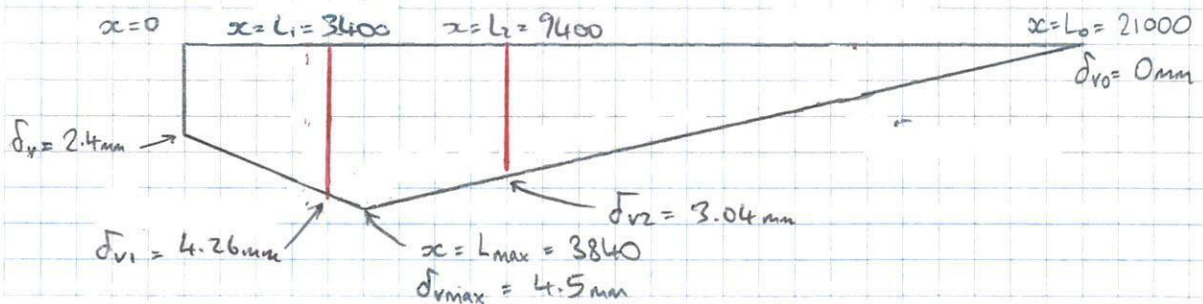
→ @  $x = 21.0\text{m} \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0%

@  $x = 0$  VERTICAL MOVEMENT =  $(0.04 / 100) \times 6000 = 2.4\text{mm}$

@  $\delta_v$  (MAX) VERTICAL MOVEMENT =  $(0.075 / 100) \times 6000 = 4.5\text{mm}$

@  $\delta_v$  (MAX) DISTANCE FROM WAU =  $0.64 \times 6000 = 3840\text{mm}$

$\therefore$  SIMPLIFIED VERTICAL MOVEMENT GRADIENT:



PROJECT:	St John's Wood Park	PAGE:	19 OF 26
PROJECT NO:	5006835	DATE:	JAN 19
		BY:	ML.
		CHK'D:	PL

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• COMBINED POTENTIAL MOVEMENTS DUE TO INSTANTATION & EXCAVATION.

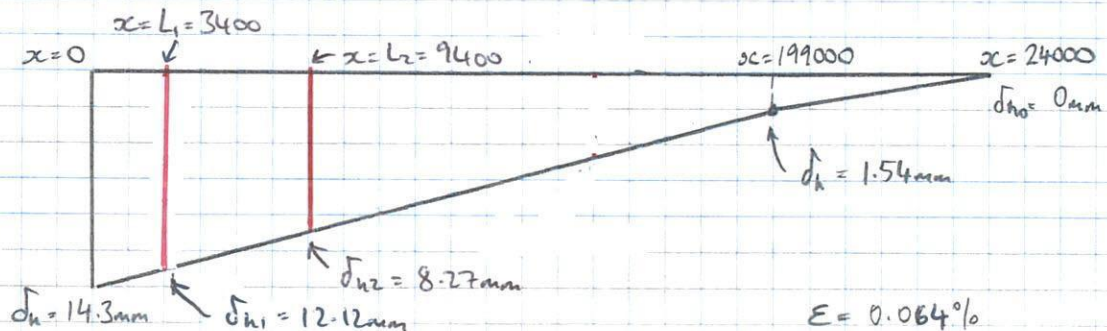
HORIZONTAL MOVEMENT:

INSTANTATION:  $\delta_h = 5.3\text{mm}$ ,  $\delta_{h1} = 4.39\text{mm}$ ,  $\delta_{h2} = 2.79\text{mm}$ ,  $L_0 = 19900\text{mm}$

EXCAVATION:  $\delta_h = 9.0\text{mm}$ ,  $\delta_{h1} = 7.73\text{mm}$ ,  $\delta_{h2} = 5.48\text{mm}$ ,  $L_0 = 24000\text{mm}$

FIND MOVEMENT DUE TO EXCAV. @ 19900mm

$$\delta_h = \tan\left(\tan^{-1}\left(\frac{9.0}{24000}\right)\right) \times (24000 - 19900) = 1.54\text{mm}$$



VERTICAL MOVEMENT:

INSTANTATION:  $\delta_v = 5.3\text{mm}$ ,  $\delta_{v1} = 4.62\text{mm}$ ,  $\delta_{v2} = 3.42\text{mm}$ ,  $L_0 = 26500$

EXCAVATION:  $\delta_v = 2.4\text{mm}$ ,  $\delta_{v1} = 4.26\text{mm}$ ,  $\delta_{v2} = 3.04\text{mm}$ ,  $L_0 = 21000$ ,  $\delta_{v\text{max}} = 4.5\text{mm}$   
 $L_{\text{max}} = 3840\text{mm}$

FIND MOVEMENT DUE TO INSTANTATION @ 21000

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 21000) = 1.1\text{mm}$$

FIND MOVEMENT DUE TO INSTANTATION @ 3840 +  $\delta_{v\text{max}}$

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 3840) + 4.5 = 9.03\text{mm}$$

PROJECT:

St John's Wood Park

PAGE: 20 OF 26

DATE: JAN 19

PROJECT NO:

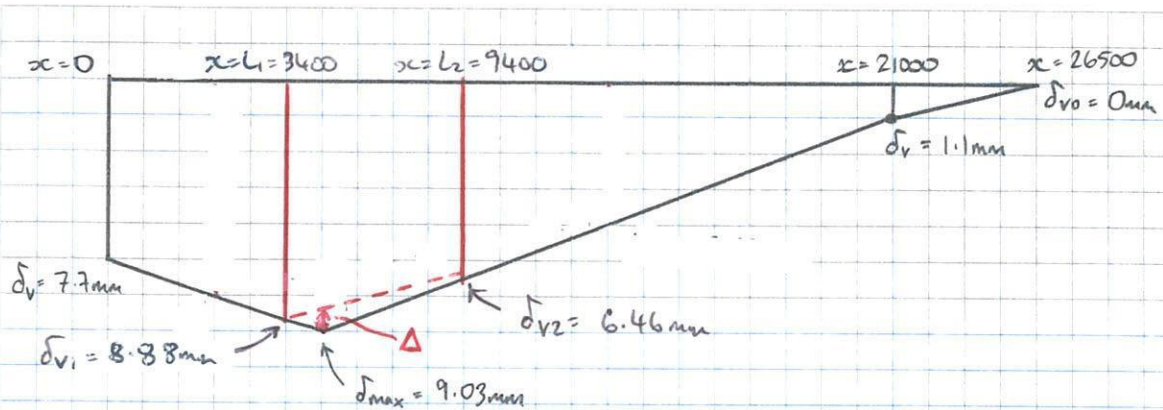
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∴ RELATIVE VERTICAL MOVEMENT WITHIN BUILDING :

$$\Delta = 9.03 - \left[ \tan \left( \tan^{-1} \left( \frac{dv_1 - dv_2}{L_2 - L_1} \right) \right) \times (L_2 - L_{max}) \right] + dv_2$$

$$= 0.33 \text{ mm}$$

• CALCULATION OF DAMAGE CATEGORY  
(USING FIGURE 6.27 & TABLE 6.4)

CAMDEN COUNCIL REQUIRES A DAMAGE CATEGORY NOT EXCEEDING  
CATEGORY 1 'VERY SLIGHT' ON THE BURLAND SCALE.

$$\therefore E_{lim} = 0.075\%$$

$$E_n = 0.064\%$$

$$\Delta/L = 0.33 / 6000 \times 100 = 0.005\%$$

CONSERVATIVELY USE LINE 'L/H = 1.5' ⇒ EQ. OF LINE =  $y = 1 - x$

$$y = \Delta/L = 0.005, \quad x = E_n = 0.064$$

$$\therefore \text{TOTAL TENSILE STRAIN, } E = 0.005 + 0.064 = 0.069\%$$

∴ MOVEMENT WITHIN DAMAGE CATEGORY 1 - 'VERY SLIGHT'

∴ GROUNDS MOVEMENT WITHIN ACCEPTABLE LIMITS.

PROJECT:

St John's Wood Park

PAGE: 21 OF 26

DATE: JAN. 19

Partnership House  
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PROJECT NO:

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GROUND MOVEMENT ASSESSMENT TO CIRIA C760

NEIGHBOURING PROPERTY - GARAGE ROW 1

BUILDING WIDTH,  $L = 38700$

DISTANCE TO CLOSEST POINT FROM EXCAVATION & INSTALLATION,  $L_1 = 1200$

DISTANCE TO FURTHEST POINT FROM EXCAVATION & INSTALLATION,  $L_2 = 39900$

HEIGHT,  $H = 3000$

$L/H = 12.9$

MAX EXCAVATION DEPTH,  $H_b = 6.0m$

PILE WASH DEPTH,  $D = 13.25m$

- POTENTIAL MOVEMENT DUE TO INSTALLATION OF WASH  
(USING PARAMETERS FROM TABLE 6.1 & FIGURE 6.8)

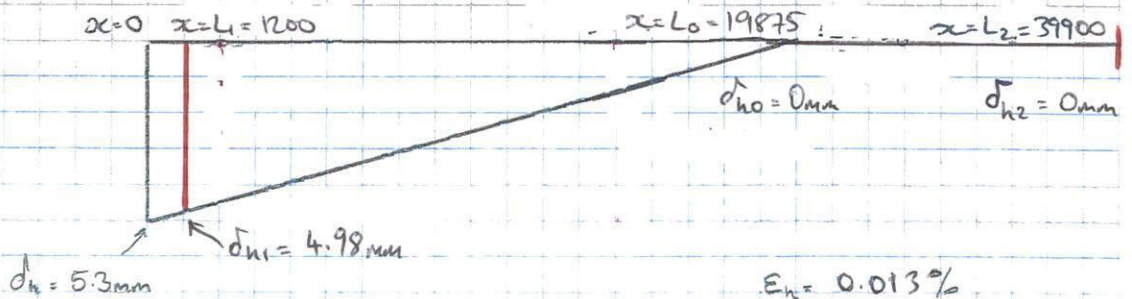
HORIZONTAL SURFACE MOVEMENT AT WASH (% OF WASH DEPTH) = 0.04%

$\therefore \text{MAX } \delta_h = (0.04/100) \times 13250mm = 5.3mm$

DISTANCE BEHIND WASH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WASH DEPTH) = 1.5

$\therefore L_0 = 13.25m \times 1.5 = 19.875m$

HORIZONTAL MOVEMENT GRADIENT DUE TO INSTALLATION



PROJECT:

St John's Wood Park

PROJECT NO:

5006835

PAGE: 22 OF 26

DATE: JAN 19

BY: ML CHK'D: RL

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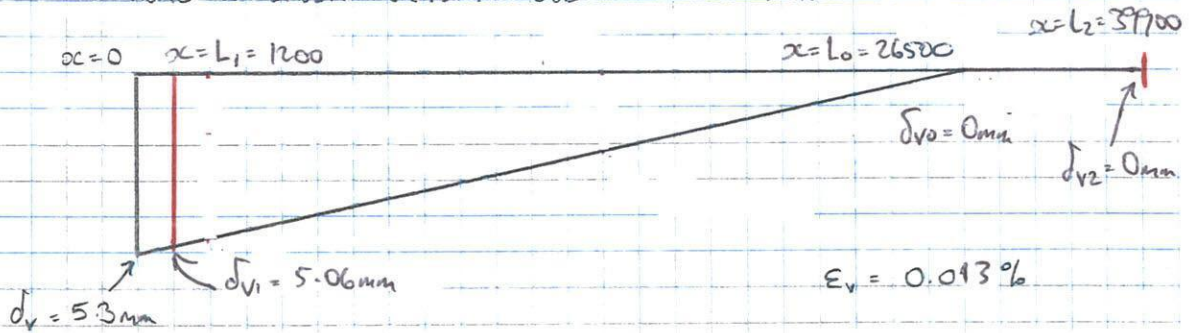
VERTICAL SURFACE MOVEMENT AT WAH (% OF WAH DEPTH) = 0.04%

$\therefore \text{MAX } \delta_v = (0.04/100) \times 13250\text{mm} = 5.3\text{mm}$

DISTANCE BEHIND WAH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF WAH DEPTH) = 2.0

$\therefore L_0 = 13.25\text{m} \times 2.0 = 26.5\text{m}$

VERTICAL MOVEMENT GRADIENT DUE TO INSTAURATION



- POTENTIAL MOVEMENT DUE TO EXCAVATION OF GROUND IN FRONT OF WAH (USING PARAMETERS FROM TABLE 6.3 & FIGURE 6.15)

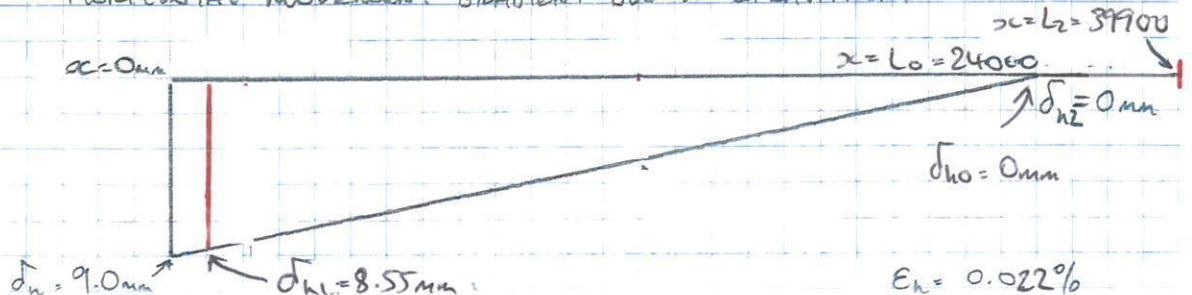
HORIZONTAL SURFACE MOVEMENT AT WAH (% OF EXCAVATION DEPTH) = 0.15%

$\therefore \text{MAX } \delta_h = (0.15/100) \times 6000 = 9.0\text{mm}$

DISTANCE BEHIND WAH TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAVATION DEPTH) = 4

$\therefore L_0 = 6\text{m} \times 4 = 24\text{m}$

HORIZONTAL MOVEMENT GRADIENT DUE TO EXCAVATION



PROJECT:

St John's Wood Park

PROJECT NO:

5006835

PAGE: 23 OF 26

DATE: JAN 19

BY: ML CHK'D: RL

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VERTICAL SURFACE MOVEMENT AT WALL: [USE FIGURE 6.15b]

DISTANCE BEHIND WALL TO NEGLIGIBLE MOVEMENT (MULTIPLE OF EXCAV. DEPTH) = 3.5

$\therefore L_0 = 6.0 \times 3.5 = 21.0m$

INTERPRETATION OF FIGURE 6.15b:

→ @  $x = 0 \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.04%

→ @ POINT OF MAX SETTLEMENT

↳ SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0.075%

↳ DISTANCE FROM WALL / MAX EXCAVATION DEPTH = 0.64

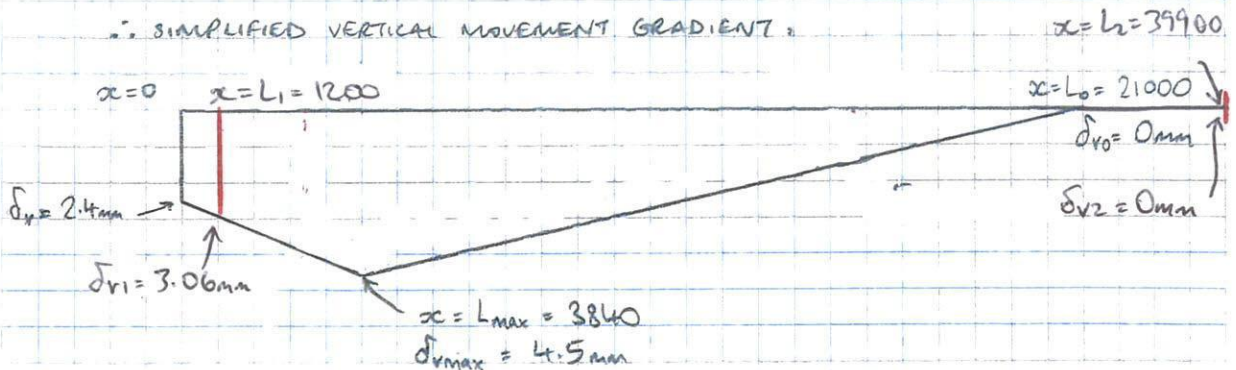
→ @  $x = 21.0m \Rightarrow$  SETTLEMENT / MAX EXCAVATION DEPTH (%) = 0%

@  $x = 0$  VERTICAL MOVEMENT =  $(0.04 / 100) \times 6000 = 2.4mm$

@  $\delta_v$  (MAX) VERTICAL MOVEMENT =  $(0.075 / 100) \times 6000 = 4.5mm$

@  $\delta_v$  (MAX) DISTANCE FROM WALL =  $0.64 \times 6000 = 3840mm$

$\therefore$  SIMPLIFIED VERTICAL MOVEMENT GRADIENT:



PROJECT:

St John's Wood Park

PROJECT NO:

5006885

PAGE: 24 OF 26

DATE: JAN 19

BY: ML. CHK'D: R1

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• COMBINED POTENTIAL MOVEMENTS DUE TO INSTANTATION & EXCAVATION.

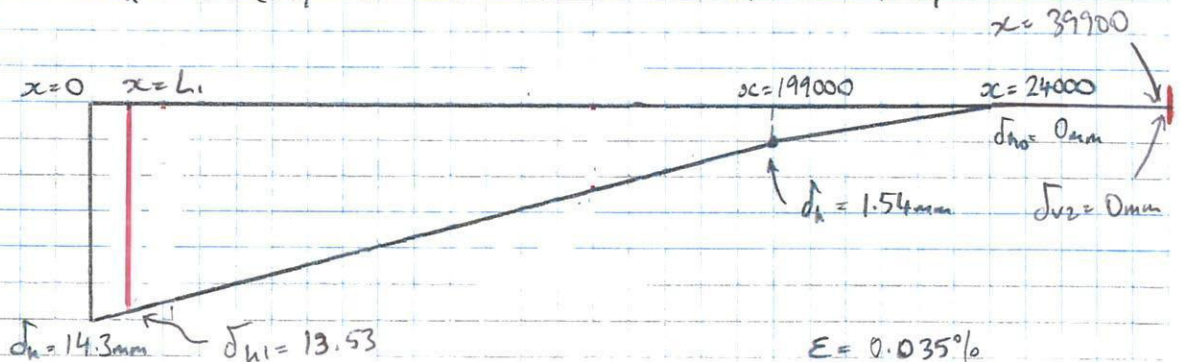
HORIZONTAL MOVEMENT:

INSTANTATION:  $\delta_h = 5.3\text{mm}$ ,  $\delta_{h1} =$ ,  $\delta_{h2} =$ ,  $L_0 = 19900\text{mm}$

EXCAVATION:  $\delta_h = 9.0\text{mm}$ ,  $\delta_{h1} =$ ,  $\delta_{h2} =$ ,  $L_0 = 24000\text{mm}$

FIND MOVEMENT DUE TO EXCAV. @ 19900mm

$$\delta_h = \tan\left(\tan^{-1}\left(\frac{9.0}{24000}\right)\right) \times (24000 - 19900) = 1.54\text{mm}$$



VERTICAL MOVEMENT:

INSTANTATION:  $\delta_v = 5.3\text{mm}$ ,  $\delta_{v1} = 4.98\text{mm}$ ,  $\delta_{v2} = 0\text{mm}$ ,  $L_0 = 26500$

EXCAVATION:  $\delta_v = 2.4\text{mm}$ ,  $\delta_{v1} = 8.55\text{mm}$ ,  $\delta_{v2} = 0\text{mm}$ ,  $L_0 = 21000$ ,  $\delta_{v\text{max}} = 4.5\text{mm}$   
 $L_{\text{max}} = 3840\text{mm}$

FIND MOVEMENT DUE TO INSTANTATION @ 21000

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 21000) = 1.1\text{mm}$$

FIND MOVEMENT DUE TO INSTANTATION @ 3840 +  $\delta_{v\text{max}}$

$$\delta_v = \tan\left(\tan^{-1}\left(\frac{5.3}{26500}\right)\right) \times (26500 - 3840) + 4.5 = 9.03\text{mm}$$



PROJECT:

St John's Wood Park

PAGE: 25 OF 26

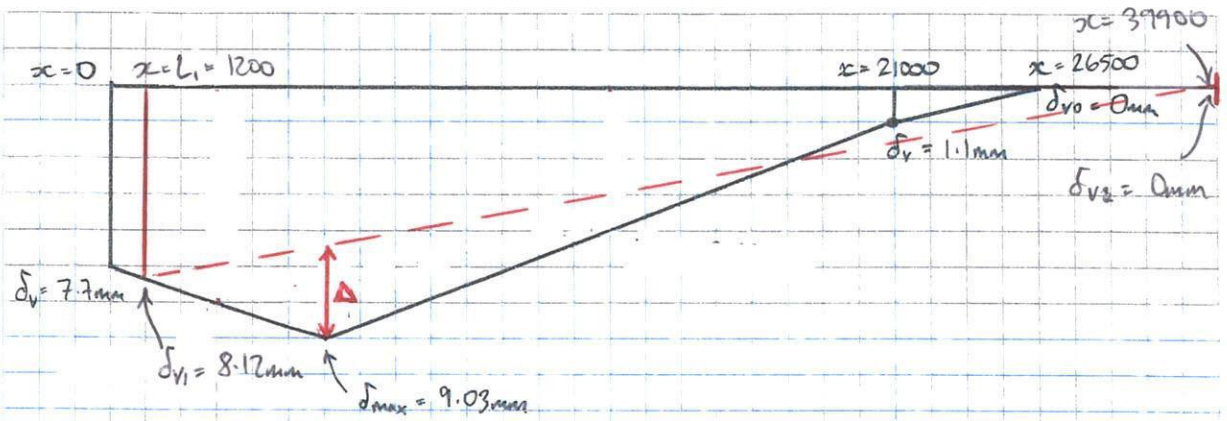
DATE: JAN 19

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PROJECT NO: 5006835

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∴ RELATIVE VERTICAL MOVEMENT WITHIN BUILDING:

$$\Delta = 9.03 - \left[ \tan \left( \tan^{-1} \left( \frac{dv_1 - dv_2}{L_2 - L_1} \right) \right) \times (L_2 - L_{max}) \right] + dv_2$$

$$= 1.47 \text{ mm}$$

• CALCULATION OF DAMAGE CATEGORY  
(USING FIGURE 6.27 & TABLE 6.4)

CAMDEN COUNCIL REQUIRES A DAMAGE CATEGORY NOT EXCEEDING  
CATEGORY 1 'VERY SLIGHT' ON THE BURLAND SCALE.

$$\therefore \epsilon_{lim} = 0.075\%$$

$$\epsilon_n = 0.035\%$$

$$\Delta/L = 1.47/38700 \times 100 = 0.004\%$$

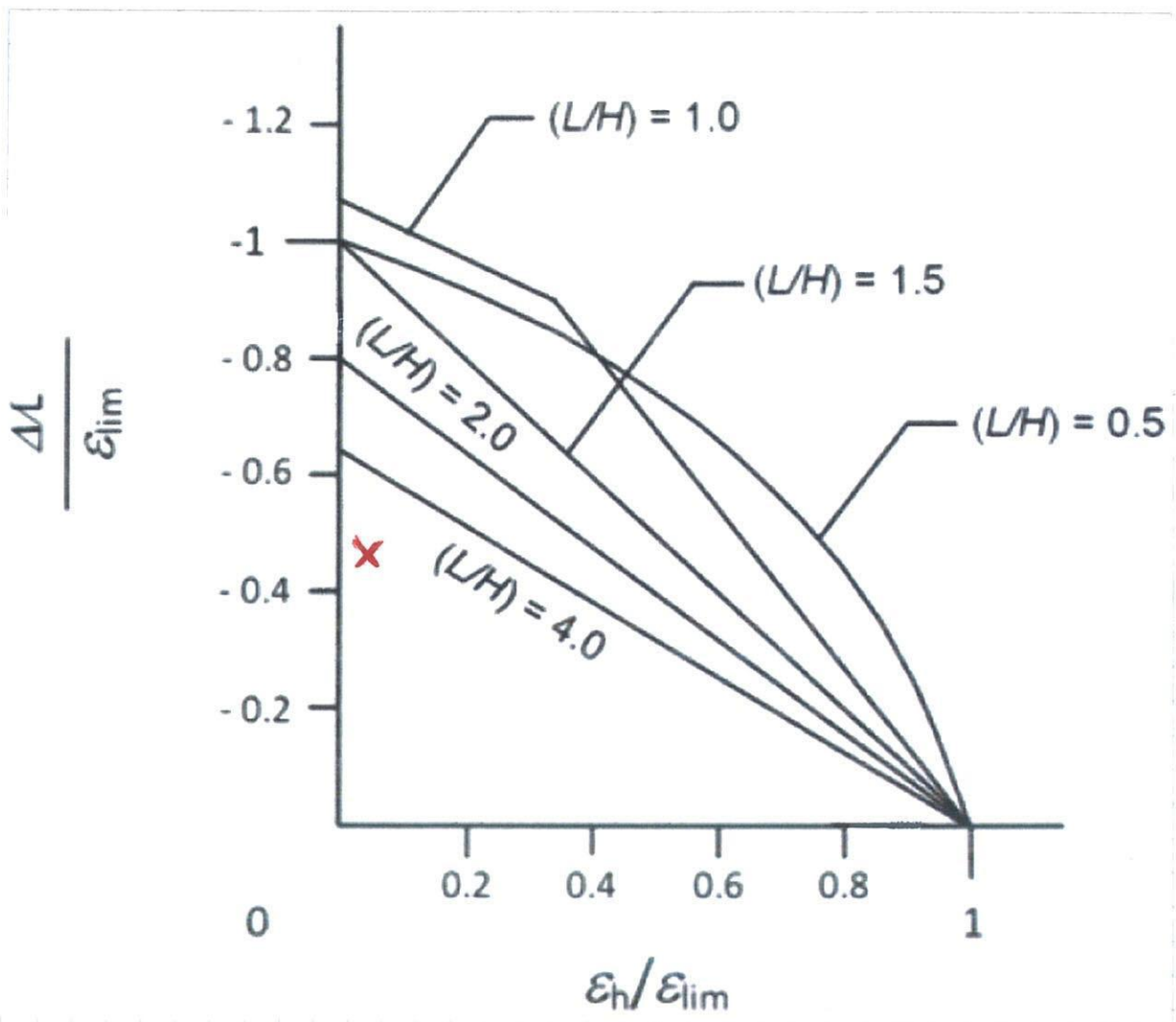
$$\epsilon_n/\epsilon_{lim} = 0.47$$

$$\Delta/L/\epsilon_{lim} = 0.05$$

SEE OVER FOR PLOT ONTO FIGURE 6.27.

PROJECT: <i>SE John's Wood Park</i>	PAGE: <i>26</i> OF <i>26</i>
PROJECT NO: <i>5006835</i>	DATE: <i>JAN 19</i>
	BY: <i>ML</i> CHK'D: <i>EL</i>

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∴ GROUND MOVEMENT LIES WITHIN THE ACCEPTED LIMITS TO RESTRICT DAMAGE CATEGORY TO 1 - VERY SLIGHT.  
 THE PROPPING PROPOSED IN THE ISJWP CALCULATION WILL FURTHER RESTRICT THIS GROUND MOVEMENT.