
GROUND MOVEMENT ASSESSMENT REPORT

Royal Academy of Dramatic
Arts
16-18 Cheries Street
London WC1E 7EX

Client: Royal Academy of Dramatic Arts




J15215

October 2018



GEA Geotechnical &
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Associates

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1.0 INTRODUCTION

Geotechnical and Environmental Associates (GEA) has been commissioned by Sinclair Johnston and Partners (SJ&P), on behalf of the Royal Academy of Dramatic Art (RADA), to update a ground movement assessment for the proposed extension of an existing basement at RADA's site at 16-18 Chenies Street, London, WC1E 7EX.

A Site Investigation and Basement Impact Assessment has previously been carried out by GEA (report ref J15215A, October 2018) and the findings of this report, along with an additional borehole by others, have been used in the derivation of parameters for use in this assessment.

A Ground Movement Assessment was undertaken for the previous scheme and developed through three issues between December 2015 and March 2016 under direction from Price and Myers as the consulting engineer. These formed part of a planning application and in 2016 the final issue received approval from Campbell Reith who were acting as auditors on behalf of the London Borough of Camden.

The purpose of this assessment has been to develop the previous assessment in respect of any effects of the proposed basement construction upon nearby sensitive structures.

1.1 Proposed Development

It is proposed to extend the existing single-storey basement that is present beneath the Drill Hall at No 16 Chenies Street as well as extending an existing basement beneath No 18 Chenies Street. The extension below No 16 is already at about 1.9 m depth and will be extended laterally by some 7 m and deepened by approximately 0.9 m. Further to the previous GMA, a 3.65 m deep corridor has been extended. The existing basement at No 18 Chenies Street will be extended by some 5 m laterally. The basement extensions will be the same depth as the existing, of 2.8 m below ground level but involving excavation to 3.33 m depth.

This report is specific to the proposed development and the advice herein should be reviewed if the development proposals are amended.

1.2 Limitations

The conclusions and recommendations made in this report are limited to those that can be made on the basis of the investigation. The results of the work should be viewed in the context of the range of data sources consulted, the number of locations where the ground was sampled and the number of soil, gas or groundwater samples tested; no liability can be accepted for information in other data sources or conditions not revealed by the sampling or testing. Any comments made on the basis of information obtained from the client or other third parties are given in good faith on the assumption that the information is accurate; no independent validation of such information has been made by GEA.

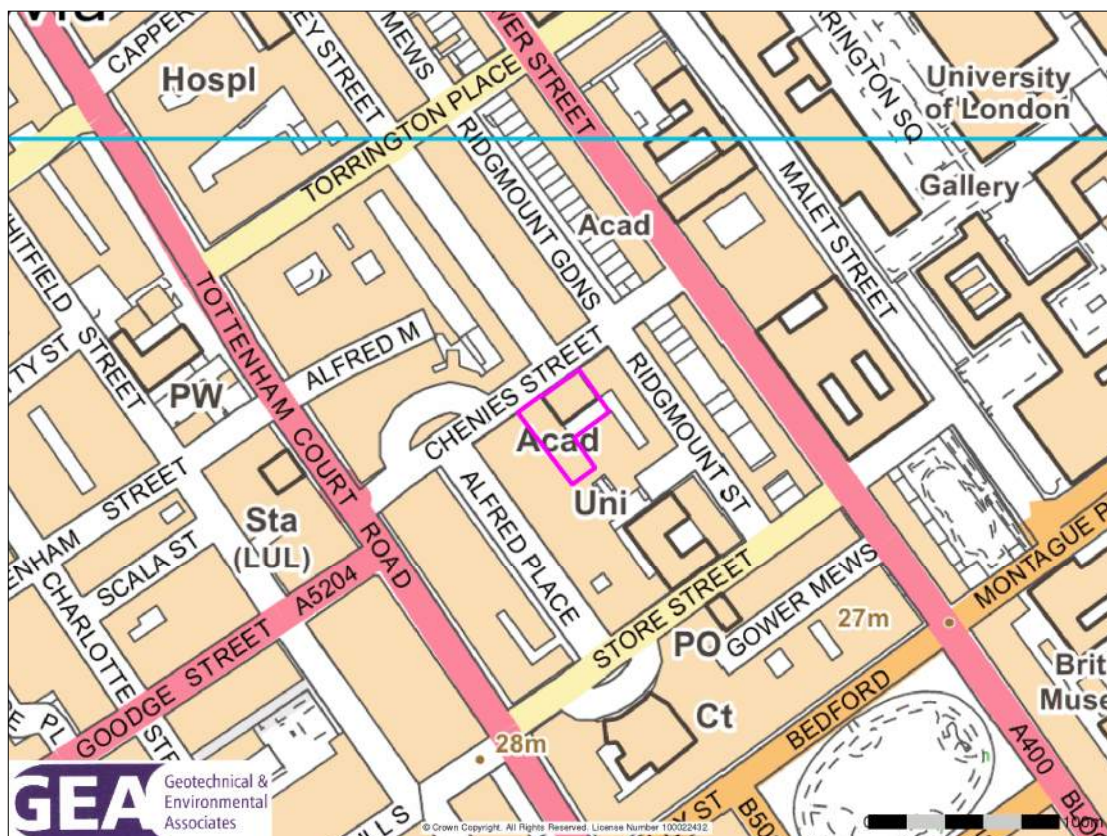
2.0 THE SITE

2.1 Site Description

The site is located in the London Borough of Camden, approximately 150 m northwest of the British Museum. It is bounded to the north by Chenies Street with access to the rear of the building via Ridgmount Street to the east and by five-storey and seven-storey buildings to the

east and west respectively. It may be additionally located by National Grid Reference 529670, 181850 and is shown on the map extract overleaf.

The site is accessed at the front of the building, and is roughly L shaped, measuring approximately 45 m by 40 m; it is occupied by the Royal Academy of Dramatic Arts (RADA), a three-storey Victorian brick building with a single level basement. The site is devoid of vegetation and sensibly levelled.



3.0 SUMMARY OF GROUND CONDITIONS

The previous site investigation has been supplemented by additional investigation points and confirmed the findings of the previous work in that, based on all of the borehole data, the updated ground model for the site generally comprises a significant thickness of made ground, overlying the Lynch Hill Gravel, which is in turn underlain by the London Clay and at depth the Lambeth Group.

The made ground generally comprised brownish grey clay with fragments of brick, concrete, mortar and ash and extended to depths of between 0.80 m and 5.50 m (23.78 m OD and 22.48 m OD). The Lynch Hill Gravel extended to depths of between 3.00 m and 9.60 m (21.00 m OD and 19.01 m OD) and generally comprised an upper clay horizon, overlying varying proportions of sand and gravel with pockets and bands of clay locally encountered. The London Clay comprised an upper thin horizon of weathered brown silty sandy clay, overlying an unweathered stiff becoming very stiff dark grey silty fissured clay with varying proportions of silt and sand, shell fragments, grey burrows and speckles of mica. This stratum was found to extend to depths of 22.60 m (3.90 m OD) and 24.70 m (4.10 m OD). The Lambeth Group comprised very stiff locally water softened multi-coloured silty sandy clay with rare fragments of mudstone and was proved to a depth of 33.00 m (-3.50 m OD).

Groundwater is present within the Lynch Hill Gravel at levels of between 21.03 m OD and 20.32 m OD.

A borehole record from the adjacent Alfred Street building indicates that the London Clay extends to a depth of 26.0 m whereupon the soils of the Lambeth Group (listed as the Woolwich and Reading Beds) were encountered and underlain in turn by Thanet Sand at 38.1 m and ultimately chalk at 42.2 m.

Groundwater was not encountered in the boreholes during drilling, but subsequent monitoring of standpipes has measured water at a depth of 5.45 m.

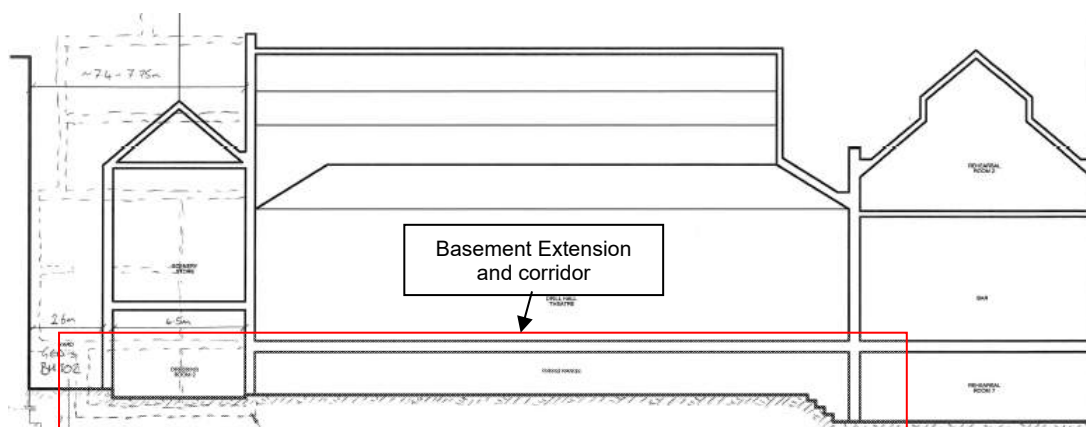
3.1 Surrounding Structures

This assessment of ground movements has been undertaken to determine the potential for damage to No 16 Chenies Street and for No 18 Chenies Street as well as the University of Law building and its infill building that abuts No 16 Chenies Street.

4.0 CONSTRUCTION SEQUENCE

4.1 16 Chenies Street

A section through the proposed building at No 16 Chenies Street including its basement is included below.



For the purposes of the ground movement assessment, the existing external ground level has been taken as 0.0 m and the proposed basement will be formed at depths between 1.25 m and 3.65 m deeper than at present; the greater depth representing a new corridor running parallel to the existing basement. The underpinning of the external walls will be through traditional methods and will deepen their foundations by around 0.9 m to bear at a depth 2.8 m from the existing ground level.

The new structure that is to be formed within the basement extension is to be supported upon piled foundations and will be completely independent of the existing structure. The drawings within the Construction Method Statement (CMS) show that the piles are relatively widely spaced and therefore can be deemed to act singly. On this basis the loading of the piles will not affect the existing building but the limited unloading due to the basement deepening will cause a minor degree of heave. SJ&P have provided drawings that indicate the unloading

effects of the development and also the reloading information for the remaining parts of the building. The reloading occurs where new spread foundations are to be cast or where existing walls are to support additional load. For the purpose of this analysis, the unloading and subsequent loading at basement level will be applied at depth of generally 2.80 m below existing ground level, although as deep as 3.65 m beneath the new corridor. The appended results graphs show the movements at 2.8 m below existing ground level, the level of the new foundations.

The construction sequence has been modelled at three stages. These are short term unloading only, short term unloading and reloading and then unloading and reloading in the long term when reversion to drained soil parameters has been assumed to take place.

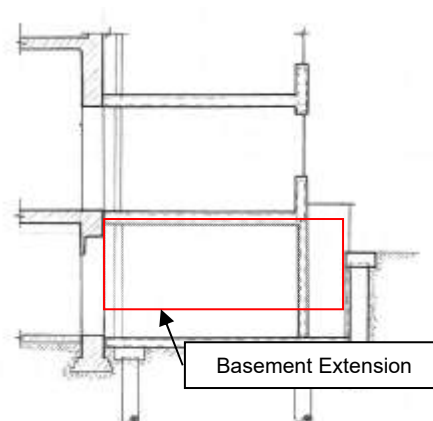
4.2 18 Chenies Street

A section through the proposed building at No 18 Chenies Street including its basement is included below.

The section, right, shows the location of a small length of bored pile wall which enables the lateral extension of the existing basement by 5.0 m.

The wall is to retain approximately 3.3 m of soil and will initially act as a cantilever with propping force provided in the long term by the basement slab and ground beams.

For such a retained height it is considered that a bored pile wall of 450 mm diameter contiguous piles should be sufficient and that with a ratio of embedded length to exposed length of roughly 2:1 for a cantilevered wall, the pile lengths may be expected to be about 9.0 m.



5.0 GROUND MOVEMENTS

An assessment of ground movements within and surrounding the excavation has been undertaken using the X_Disp and P_Disp computer programs licensed from the OASYS suite of geotechnical modelling software from Arup. These programs are commonly used within the ground engineering industry and are considered to be appropriate tools for this analysis.

The X_Disp program has been used to predict ground movements likely to arise from the construction of the proposed basement. This includes the settlement of the ground (vertical movement) and the lateral movement of soil behind the proposed retaining walls (horizontal movement) which occur due to the installation of piling and underpinning together and subsequent excavation.

The analysis of potential ground movements within the excavation, as a result of unloading of the underlying soils and subsequent reloading as the building is constructed, has been carried out using the Oasys P_Disp Version 19.4 software package and is based on the assumption that the soils behave elastically, which provides a reasonable approximation to soil behaviour at small strains.

For the purpose of these analyses, the corners have been defined by x and y coordinates, with the x-direction roughly perpendicular to Chenies Street and the y-direction parallel with the same road. Vertical movement is in the z-direction.

The output movement contour plots are included within the appendix along with the full data set of results and line graphs for the walls analysed.

5.1 Movements Surrounding the Excavations

5.1.1 Model Used

For the X-Disp analysis, the soil movement relationships used for the embedded retaining walls are based on the default values CIRIA report C760¹. The C760 movements were derived from a number of historic case studies of the short term movements that result from wall installation and basement excavation.

Given the limited extent of the mass concrete underpinning it is deemed appropriate to adopt the ground movement curves for ‘no horizontal and vertical movement’ for this analysis.

On the basis of the notes in Section 4.2 above, a pile length of 9.0 m has been assumed along with a maximum basement excavation depth of 3.3 m. Groundwater has not been encountered within the proposed basement depth and therefore a contiguous bored pile wall is deemed appropriate; a lining wall will provide long term water-tightness. The piled wall, which will act as a cantilever, falls into the low stiffness category in C760.

5.1.2 Results

The X-Disp analysis has been used to estimate the movements behind the walls resulting from pile installation and basement excavation. This includes the settlement of the ground (vertical movement) and the lateral movement of soil behind the wall (horizontal movement). The contour graphs of these movement predictions are appended for the piling phase together with the total movement prediction which combined the effects. For clarity the graphs show the movements at a depth of 2.8 m below existing ground level, the level of the new foundations.

The following values of vertical and horizontal movement are those occurring immediately behind the piled wall and reduce to zero at the distance noted as the maximum lateral influence.

Phase of Works (CIRIA C760 Movement Curve)	Maximum Movements at Existing Ground Level of 0.0 m	
	Vertical Settlement (mm) [Maximum lateral influence (m)]	Horizontal Movement (mm) [Maximum lateral influence (m)]
Piling Phase (C760 Contiguous Bored Pile Wall)	<4 [18.0]	<4 [13.5]
Combined Piling and Basement Excavation Phases (Excavation in front of a low stiffness wall)	10 [12.0]	10 to 16 [12.0]

¹ Gaba, A, Hardy S, Doughty, L, Powrie, W and Selemetas, D (2017) *Guidance on Embedded Retaining Wall Design*. CIRIA Report C760.

5.2 Movements within the Excavations

5.2.1 Model Used

At this site the loading configurations supplied by SJ&P indicate that the various walls and slab areas will be subject to unloading and different walls and areas will be reloaded. The annotated drawings indicate the imposed load increases are relatively modest and the maximum unloading is 60 kN/m². Where there is a net unloading of the London Clay, there will be a reduction in vertical stress in the short term that will cause heave to take place. Undrained soil parameters have been used to estimate the potential short term movements, which include the “immediate” or elastic movements as a result of the basement excavation. Drained parameters have been used to provide an estimate of the total long-term movement.

The elastic analysis requires values of soil stiffness at various levels to calculate displacements. Values of stiffness for the soils at this site are readily available from published data and well-established methods have been used to provide our estimates. These relate values of E_u and E' , the undrained and drained stiffness respectively, to values of undrained cohesion, as described by Padfield and Sharrock² and Butler³ and more recently by O’Brien and Sharp⁴. Relationships of $E_u = 500 C_u$ and $E' = 300 C_u$ for the cohesive soils have been used to obtain values of Young’s modulus. More recent published data⁵ indicates stiffness values of 750 x C_u for the London Clay and a ratio of E' to E_u of 0.75 but it is considered that the use of the more conservative values provides a sensible approach for this site at this stage in the design.

The soil parameters used in this assessment are tabulated below.

Stratum	Depth range (m)	E_u (MPa)	E' (MPa)
Made Ground	G/L to 3.3	25	15
Firm Clay	3.3 – 4.1	37.5	22.5
Lynch Hill Gravel	4.1 – 6.3	54	54
London Clay	6.3 – 20	55 – 108	33 – 64.8
London Clay	20 – 26	55	108

It is noted that the made ground extended to a depth of 5.0 m in Borehole No 1 beyond the end of the building. This thickness of made ground is considered to derive from the Dallas House building that stood on that part of the site, but was demolished following World War II, such that it is not considered to be representative of the typical conditions beneath the site. The ground conditions in the table above are based on GEA Borehole Nos 101 and 103 to 106 which are essentially consistent with the findings of LBH Borehole No 1 and therefore considered to be a reliable representation of the ground conditions on the wider site.

² Padfield CJ and Sharrock MJ (1983) *Settlement of structures on clay soils*. CIRIA Special Publication 27

³ Butler FG (1974) *Heavily overconsolidated clays: a state of the art review*. Proc Conf Settlement of Structures, Cambridge, 531-578, Pentech Press, Lond

⁴ O’Brien AS and Sharp P (2001) *Settlement and heave of overconsolidated clays - a simplified non-linear method*. Part Two, Ground Engineering, Nov 2001, 48-53

⁵ Burland JB, Standing, JR, and Jardine, FM (2001) *Building response to tunnelling, case studies from construction of the Jubilee Line Extension*. CIRIA Special Publication 200

A rigid boundary for the analysis has been set within the Lambeth Group at a depth of 26.0 m below existing ground level. Below this depth the soils are considered essentially incompressible.

5.2.2 Results

The P-Disp analysis indicates that, by the time the basement construction is complete, less than 8 mm of heave is likely to have taken place at the centre of the proposed extension, whilst settlement is not shown to be dominant. This ties in with the fact that new vertical loading will be very limited since it is to be largely carried on piles.

Following completion of the basement construction and application of new loads, the heave is predicted to be less than 10 mm, settlement under subsequent reloading is not predicted for the external walls. For clarity the appended graphs show the movements at a depth of 2.8 m below existing ground level, the level of the new foundations.

The results of the P-Disp analysis can be used to indicate the likely impact of the proposed basement construction beyond the site boundaries. At a distance of about 5.0 m away from the basement extension excavation, the total movements reduce to roughly 2.0 mm of heave and at a similar distance from the external walls. Movements outside the excavation will be constrained to a certain extent by the presence of the new retaining walls and off-set to a large extent by the movements during pile and underpin installation. The estimated movements obtained from the analysis may therefore not occur in practice.

Basement Location	Movement (mm) Heave -ve / Settlement +ve		
	Short-term Heave (Unloading / excavation phase)	Short-term Heave / Settlement (Post-construction)	Total Heave / Settlement
16 Chenies Street	-5 to -8	-5 to -8	-5 to -10
18 Chenies Street	-5 to -8	-5 to -8	-5 to -10

A void or layer of compressible material may need to be incorporated into the design to accommodate these potential long term movements. This analysis suggests that if such a compressible material is to be used beneath the slab, it will need to be designed to be able to resist the limited potential uplift forces generated by the ground movements and relating to less than 10 mm of total uplift movement.

6.0 DAMAGE ASSESSMENT

In addition to the above assessment of the likely movements that will result from the proposed development, the neighbouring buildings are considered to be sensitive structures, requiring Building Damage Assessments, on the basis of the classification given in C760¹.

All structures are shown on the appended site plan.

6.1 Damage to Neighbouring Structures

The movements resulting from the construction of the basement extension have been considered with the infill wall to the Law Building taken as being sensitive to the ground movements as well as the four main walls of No 16 Chenies Street, the retained wall at No 18 Chenies Street and the nearest two walls of the University of law building.

A building damage assessment is included within the X-Disp analysis and indicates that all walls other than one segment in each of the Eastern wall of 16 Chenies Street and the Infill Building will suffer movement equivalent to Damage Category 0 – ‘Negligible’ or Category 1 – ‘Very Slight’. The other two segments are indicated to be Category 2 – ‘Slight’. However consideration of the wall as a whole, where individual segments of hogging or sagging, are combined to give a more realistic pattern of movement indicates that the effect will be Category 0 – ‘Negligible’.

Analysis of the line plot for the wall to the Law Building Infill and 16 Chenies St East taken from the P-Disp analysis shows that the total movement will generate ‘negligible’ damage with the deflection ratios shown as much less than 1 in 1000 through either the ‘hogging’ heave movements or ‘sagging’ settlements.

6.2 Monitoring of Ground Movements

The predictions of ground movement based on the ground movement analysis should be checked by monitoring of the adjacent properties and structures and following confirmation of the foundation arrangements. The structures to be monitored during the construction stages should include the neighbouring structures. Condition surveys of the above existing structures should be carried out before and after the proposed works.

However, it should be remembered that the context is that this is a small extension to an existing basement and that the movements predicted are relatively small.

The precise monitoring strategy will be developed at a later stage and it will be subject to discussions and agreements with the owners of the adjacent structures under the obligations of the Party Wall Act. Contingency measures will be implemented if movements of the adjacent structures exceed predefined trigger levels. Both contingency measures and trigger levels will need to be developed within a future monitoring specification for the works.

7.0 CONCLUSIONS

The analysis has concluded that the predicted damage to the neighbouring properties from the construction of the basement extension would generally be ‘Negligible’ or ‘very slight’ for which the damage that would occur would fall within the acceptable limits. It is recommended that movement monitoring is carried out on all structures prior to and during the proposed basement construction.

The separate phases of work, including excavation of the proposed basement, will in practice be separated by a number of weeks during which time construction of permanent supports, basement slab and retaining wall curing will take place. This will provide an opportunity for the ground movements during and immediately after underpin construction to be measured and the data acquired can be fed back into the design and compared with the predicted values. Such a comparison will allow the ground model to be reviewed and the predicted wall movements to be reassessed prior to the main excavation taking place so that propping arrangements can be adjusted if required.

APPENDICES

X-DISP ANALYSIS

Pile and Underpinning Installation Movement
Contour Plots and Tabular Data

Excavation Movement Contour Plots
and Tabular Data

P-DISP ANALYSIS

Short Term Movement Contour Plots – Unloading

Short Term Movement Contour Plots – Reloading

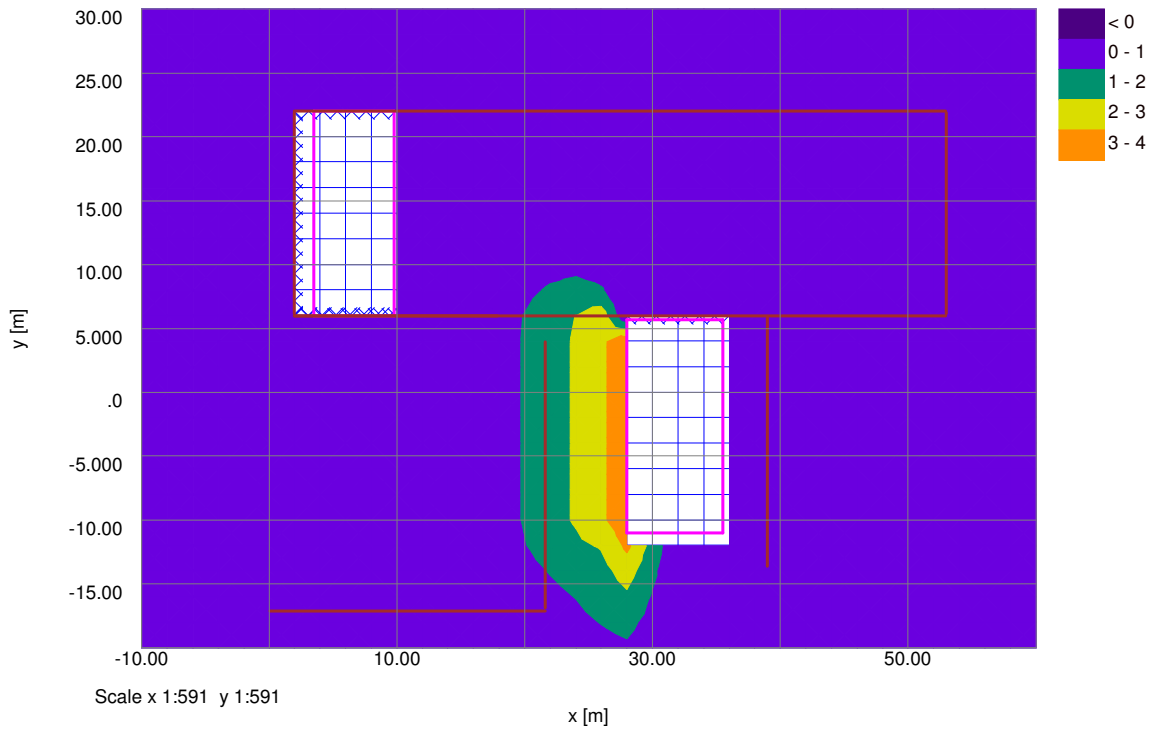
Total Movement Contour Plots

Cross Section Line Plots

Basement Plan and Loading
Information

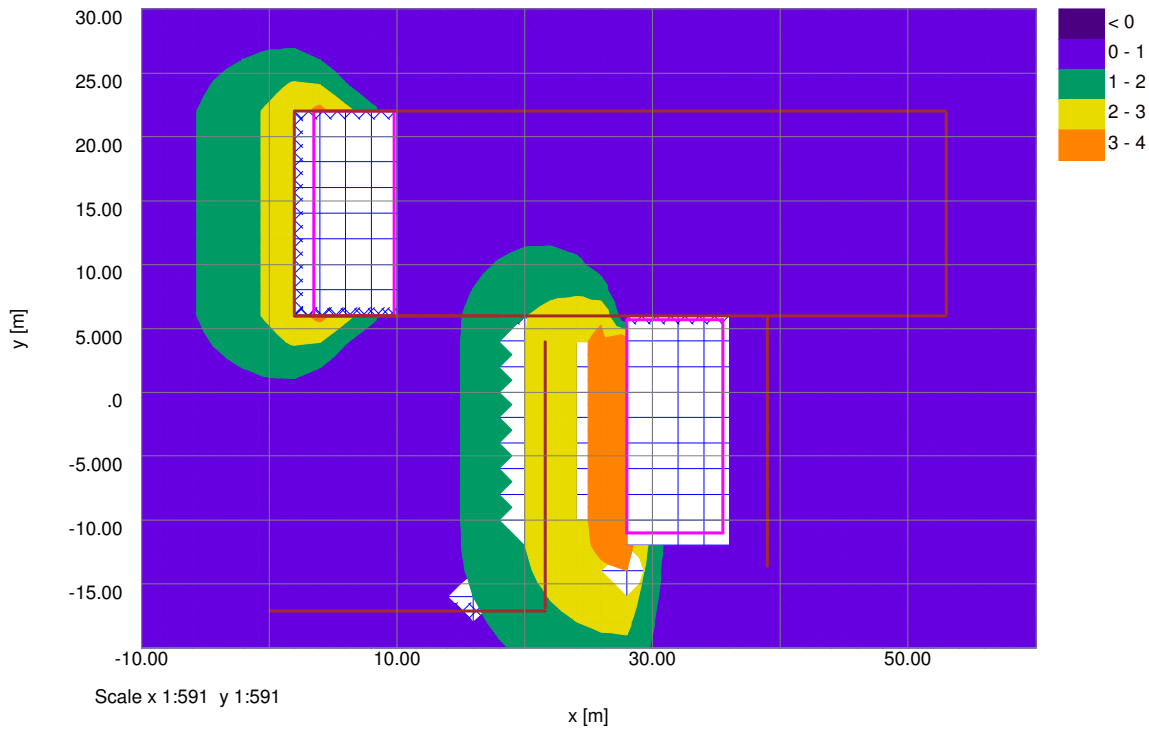
Job No.	Sheet No.	Rev.
J15215		
Drg. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Horizontal Displacement Contours: Grid 1 (level -2.800m) Interval 1mm



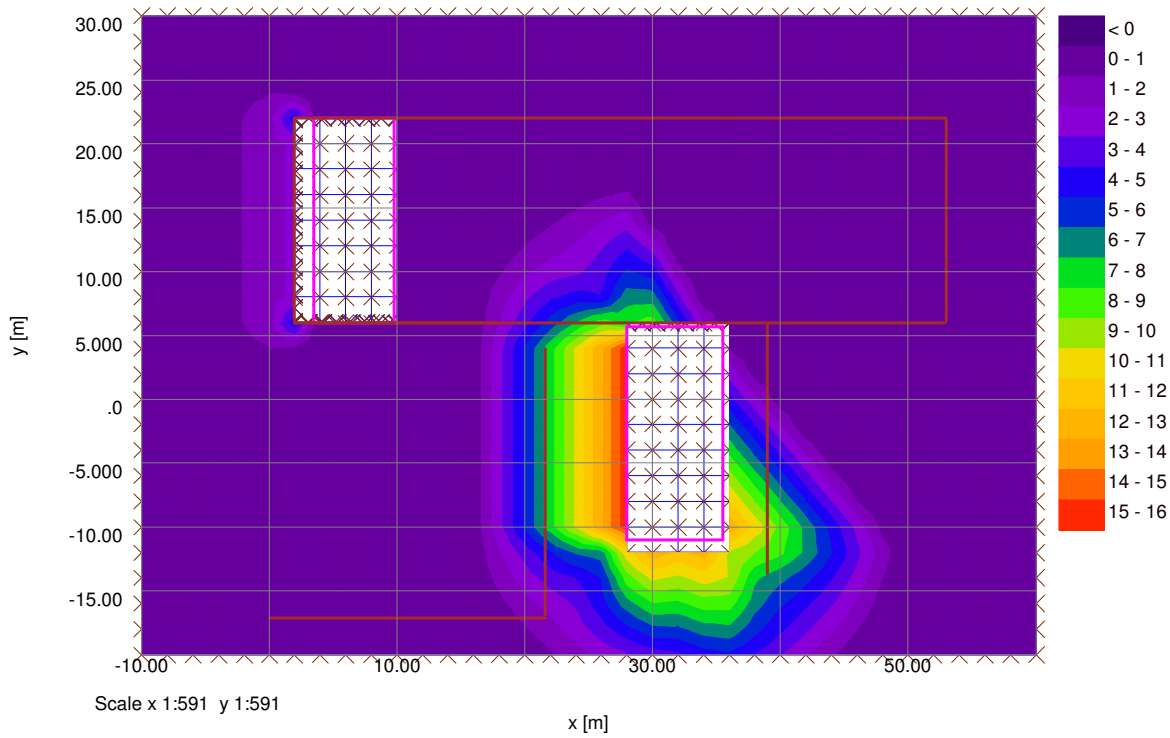
Job No.	Sheet No.	Rev.
J15215		
Dr. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Vertical Settlement Contours: Grid 1 (level -2.800m) (Interval 1mm)



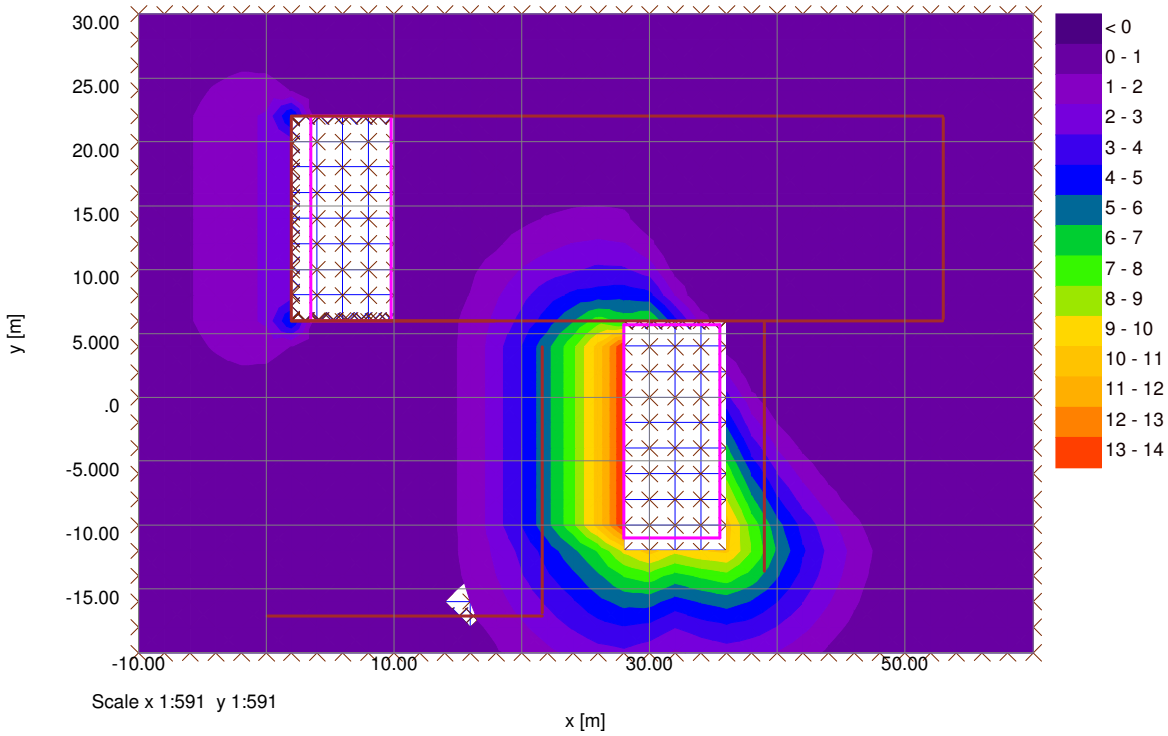
Job No.	Sheet No.	Rev.
J15215		
Drg. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Horizontal Displacement Contours: Grid 1 (level -2.800m) Interval 1mm



Job No.	Sheet No.	Rev.
J15215		
Drg. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Vertical Settlement Contours: Grid 1 (level -2.800m) (Interval 1mm)





Royal Academy of Dramatic Arts
16-18 Chenies Street Development
Run 4 Excavation and imported Installation

Job No.	Sheet No.	Rev.
J15215		
Drg. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Problem Type

Problem Type : Tunnelling and Embedded Wall Excavations

Displacement Data

Type	Name	Direction of extrusion	Point/Line/Line for extrusion						No. of intervals across extrusion/line	Extrusion depth [m]	No. of intervals along extrusion	Calculate	Surface type for tunnels
			First point			Second point							
			X [m]	Y [m]	Z (level) [m]	X [m]	Y [m]	Z (level) [m]					
Grid	Grid 1	Global X	-10.00000	-20.00000	-2.80000	-	30.00000	-2.80000	25	70.00000	35	Yes	Surface
Line	Law Bdg Infill	-	2.00000	6.00000	-1.50000	18.00000	6.00000	-1.50000	15	-	-	Yes	Surface
Line	16 Chenies Wst	-	2.00000	22.00000	-2.80000	53.00000	22.00000	-2.80000	45	-	-	Yes	Surface
Line	16 Chenies Sth	-	2.00000	21.90000	-2.80000	2.00000	6.10000	-2.80000	15	-	-	Yes	Surface
Line	16 Chenies Est	-	2.00000	6.00000	-2.80000	53.00000	6.00000	-2.80000	45	-	-	Yes	Surface
Line	16 Chenies Nth	-	53.00000	21.90000	-2.80000	53.00000	6.10000	-2.80000	15	-	-	Yes	Surface
Line	18 Chenies	-	39.00000	-13.60000	-3.50000	39.00000	6.00000	-3.50000	20	-	-	Yes	Surface
Line	Retained Wall	-	21.60000	4.00000	-2.80000	21.60000	-17.00000	-2.80000	20	-	-	Yes	Surface
Line	Law Bdg Est	-	21.60000	-17.10000	-2.80000	0.00000	-17.10000	-2.80000	20	-	-	Yes	Surface

Imported Displacements

The following data points and displacements were found in the import file Xdispl Run 4 Installation.csv.

Ref.	Coordinates			Displacements		
	x [m]	y [m]	z [m]	x [mm]	y [mm]	z [mm]
1	-10.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
2	-8.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
3	-6.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
4	-4.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
5	-2.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
6	0.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
7	2.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
8	4.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
9	6.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
10	8.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
11	10.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
12	12.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
13	14.00000	-20.00000	-2.80000	0.00000	0.00000	0.27134
14	16.00000	-20.00000	-2.80000	0.00000	0.00000	0.60000
15	18.00000	-20.00000	-2.80000	0.00550	0.00481	0.90928
16	20.00000	-20.00000	-2.80000	0.12054	0.14003	1.19168
17	22.00000	-20.00000	-2.80000	0.18143	0.30325	1.43667
18	24.00000	-20.00000	-2.80000	0.17848	0.49188	1.63023
19	26.00000	-20.00000	-2.80000	0.11090	0.68577	1.75609
20	28.00000	-20.00000	-2.80000	0.00000	0.84195	1.80000
21	30.00000	-20.00000	-2.80000	0.00000	0.42098	0.90000
22	32.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
23	34.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
24	36.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
25	38.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
26	40.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
27	42.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
28	44.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
29	46.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
30	48.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
31	50.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
32	52.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
33	54.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
34	56.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
35	58.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
36	60.00000	-20.00000	-2.80000	0.00000	0.00000	0.00000
37	-10.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
38	-8.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
39	-6.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
40	-4.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
41	-2.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
42	0.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
43	2.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
44	4.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
45	6.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
46	8.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
47	10.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
48	12.00000	-18.00000	-2.80000	0.00000	0.00000	0.10715
49	14.00000	-18.00000	-2.80000	0.00000	0.00000	0.46950
50	16.00000	-18.00000	-2.80000	0.00000	0.00000	0.82151
51	18.00000	-18.00000	-2.80000	0.14121	0.08983	1.15869
52	20.00000	-18.00000	-2.80000	0.28191	0.23785	1.47397
53	22.00000	-18.00000	-2.80000	0.35940	0.43727	1.75609
54	24.00000	-18.00000	-2.80000	0.34484	0.69856	1.98755
55	26.00000	-18.00000	-2.80000	0.21665	1.00616	2.14398
56	28.00000	-18.00000	-2.80000	0.00000	1.28988	2.20000
57	30.00000	-18.00000	-2.80000	0.00000	0.64494	1.10000
58	32.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
59	34.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
60	36.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
61	38.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
62	40.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
63	42.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
64	44.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
65	46.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
66	48.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
67	50.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
68	52.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
69	54.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
70	56.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
71	58.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
72	60.00000	-18.00000	-2.80000	0.00000	0.00000	0.00000
73	-10.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
74	-8.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
75	-6.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
76	-4.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
77	-2.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
78	0.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
79	2.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
80	4.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
81	6.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
82	8.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
83	10.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
84	12.00000	-16.00000	-2.80000	0.00000	1.81942	2.60000
85	14.00000	-16.00000	-2.80000	0.00000	0.00000	0.62679
86	16.00000	-16.00000	-2.80000	0.06757	0.02268	1.00000
87	18.00000	-16.00000	-2.80000	0.29397	0.12311	1.36393
88	20.00000	-16.00000	-2.80000	0.48527	0.26781	1.71320
89	22.00000	-16.00000	-2.80000	0.61348	0.48651	2.03795
90	24.00000	-16.00000	-2.80000	0.61779	0.82043	2.31938
91	26.00000	-16.00000	-2.80000	0.11421	1.29571	2.52297
92	28.00000	-16.00000	-2.80000	0.00000	1.81942	2.60000
93	30.00000	-16.00000	-2.80000	0.00000	0.90971	1.30000
94	32.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
95	34.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000
96	36.00000	-16.00000	-2.80000	0.00000	0.00000	0.00000



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Ref.	Coordinates			Displacements		
	x [m]	y [m]	z [m]	x [mm]	y [mm]	z [mm]
1121	19.44000	-17.10000	-2.80000	0.32856	0.21376	1.49778
1122	18.36000	-17.10000	-2.80000	0.24050	0.13479	1.31843
1123	17.28000	-17.10000	-2.80000	0.13969	0.06860	1.13319
1124	16.20000	-17.10000	-2.80000	0.02805	0.01224	0.94331
1125	15.12000	-17.10000	-2.80000	0.00000	0.00000	0.74971
1126	14.04000	-17.10000	-2.80000	0.00000	0.00000	0.55309
1127	12.96000	-17.10000	-2.80000	0.00000	0.00000	0.35401
1128	11.88000	-17.10000	-2.80000	0.00000	0.00000	0.15289
1129	10.80000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1130	9.72000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1131	8.64000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1132	7.56000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1133	6.48000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1134	5.40000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1135	4.32000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1136	3.24000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1137	2.16000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1138	1.08000	-17.10000	-2.80000	0.00000	0.00000	0.00000
1139	0.00000	-17.10000	-2.80000	0.00000	0.00000	0.00000

- 1 - Data point coincident with displacement data. Its displacement has been added to those calculated by Xdisp.
- 2 - Data point coincident with horizontal movement calculation point for a specific building. Its displacement has been added before performing building damage calculations.
- 6 - Data point coincident with vertical movement calculation point for a specific building. Its displacement has been added before performing building damage calculations.

Vertical Ground Movement Curves (Excavations)

Curve Name: No vertical ground movement
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (%)]
 [0.000,0.000,0.000][1.000,0.000,0.000][0.000,1.000,0.000][1.000,1.000,0.000]
Curve Fitting Polynomial
Method:
 x Order: 1
 y Order: 0
 Polynomial: z = 0.0x + 0.0
 Coeff. of -2147483648.E+2147483647
Determination:

Curve Name: Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (%)]
 [0.000,0.000,0.039][0.100,0.000,0.049][0.200,0.000,0.056][0.300,0.000,0.062]
 [0.400,0.000,0.067][0.500,0.000,0.070][0.600,0.000,0.072][0.700,0.000,0.073]
 [0.800,0.000,0.073][0.900,0.000,0.072][1.000,0.000,0.070][1.100,0.000,0.068]
 [1.200,0.000,0.065][1.300,0.000,0.061][1.400,0.000,0.058][1.500,0.000,0.054]
 [1.600,0.000,0.050][1.700,0.000,0.046][1.800,0.000,0.042][1.900,0.000,0.038]
 [2.000,0.000,0.034][2.100,0.000,0.030][2.200,0.000,0.027][2.300,0.000,0.023]
 [2.400,0.000,0.019][2.500,0.000,0.017][2.600,0.000,0.014][2.700,0.000,0.012]
 [2.800,0.000,0.010][2.900,0.000,0.008][3.000,0.000,0.007][3.100,0.000,0.005]
 [3.200,0.000,0.004][3.300,0.000,0.004][3.400,0.000,0.003][3.500,0.000,0.002]
 [3.600,0.000,0.002][3.700,0.000,0.002][3.800,0.000,0.001][3.900,0.000,0.001]
 [4.000,0.000,0.000]
Curve Fitting Polynomial
Method:
 x Order: 4
 y Order: 0
 Polynomial: z = -2.6455E-3x⁴ + 2.8495E-2x³ - 1.0051E-1x² + 1.0569E-1x + 3.8990E-2
 Coeff. of 9.9999E-1
Determination:

Curve Name: Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (%)]
 [0.000,0.000,0.345][0.100,0.000,0.327][0.200,0.000,0.311][0.300,0.000,0.294]
 [0.400,0.000,0.279][0.500,0.000,0.264][0.600,0.000,0.250][0.700,0.000,0.237]
 [0.800,0.000,0.224][0.900,0.000,0.212][1.000,0.000,0.200][1.100,0.000,0.189]
 [1.200,0.000,0.178][1.300,0.000,0.168][1.400,0.000,0.158][1.500,0.000,0.149]
 [1.600,0.000,0.140][1.700,0.000,0.132][1.800,0.000,0.124][1.900,0.000,0.116]
 [2.000,0.000,0.109][2.100,0.000,0.101][2.200,0.000,0.095][2.300,0.000,0.088]
 [2.400,0.000,0.082][2.500,0.000,0.076][2.600,0.000,0.070][2.700,0.000,0.065]
 [2.800,0.000,0.059][2.900,0.000,0.054][3.000,0.000,0.049][3.100,0.000,0.044]
 [3.200,0.000,0.039][3.300,0.000,0.034][3.400,0.000,0.029][3.500,0.000,0.025]
 [3.600,0.000,0.020][3.700,0.000,0.015][3.800,0.000,0.010][3.900,0.000,0.005]
 [4.000,0.000,0.000]
Curve Fitting Polynomial
Method:
 x Order: 3
 y Order: 0
 Polynomial: z = -3.5383E-3x³ + 3.7194E-2x² - 1.7831E-1x + 3.4467E-1
 Coeff. of 9.9999E-1
Determination:

Horizontal Ground Movement Curves (Excavations)

Curve Name: No horizontal ground movement
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (%)]
 [0.000,0.000,0.000][1.000,0.000,0.000][0.000,1.000,0.000][1.000,1.000,0.000]
Curve Fitting Polynomial
Method:
 x Order: 0
 y Order: 0
 Polynomial: z = 0.0
 Coeff. of -2147483648.E+2147483647
Determination:

Curve Name: Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (%)]
 [0.000,0.000,0.150][4.000,0.000,0.000]
Curve Fitting Polynomial
Method:
 x Order: 1
 y Order: 0
 Polynomial: z = -3.75E-2x + 1.50E-1
 Coeff. of 1.00
Determination:

Curve Name: Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
Coordinates: [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (%)]
 [0.000,0.000,0.400][4.000,0.000,0.000]
Curve Fitting Polynomial
Method:
 x Order: 1
 y Order: 0
 Polynomial: z = -10.E-2x + 4.0E-1
 Coeff. of 1.0
Determination:

Polygonal Excavations

Excavation Name: 16 Chenies Underpinning
Surface level [m]: -1.9000
Contribution: Positive
Enabled: Yes
 Surface movement curves which are selected are applied between -2.8000



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Ref.	Coordinates			Displacements		
	x [m]	y [m]	z [m]	x [mm]	y [mm]	z [mm]
surface and [m]:						
Corner	x	y	Base Level	Stiffened	Previous Side	Next Side
	[m]	[m]	[m]	d	p1	p2*
	[m]	[m]	[m]	[m]	[%]	[%]
1	3.5000	6.0000	-2.8000	No	-	-
2	3.5000	22.0000	-2.8000	No	-	-
3	9.8000	22.0000	-2.8000	No	-	-
4	9.8000	6.0000	-2.8000	No	-	-

Side	Corner 1		Corner 2		Ground Movement Curve	
	x [m]	y [m]	x [m]	y [m]	Vertical	Horizontal
1	3.5000	6.0000	3.5000	22.0000	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))	Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
2	3.5000	22.0000	9.8000	22.0000	No vertical ground movement	No horizontal ground movement
3	9.8000	22.0000	9.8000	6.0000	No vertical ground movement	No horizontal ground movement
4	9.8000	6.0000	3.5000	6.0000	No vertical ground movement	No horizontal ground movement

Excavation Name: 18 Chenies Piling
Surface level [m]: 0.0
Contribution: Positive
Enabled: Yes
Surface movement curves which are selected are applied between surface and [m]: -3.0000

Corner	x [m]	y [m]	Base Level [m]	Stiffened	Previous Side		Next Side			
					d	p1	d	p1		
					[m]	[%]	[m]	[%]		
1	28.000	5.7000	-3.0000	Yes	0.0	67.000	25.000	0.0	67.000	25.000
2	35.500	5.7000	0.0	No	-	-	-	-	-	-
3	35.500	-11.000	-3.5000	No	-	-	-	-	-	-
4	30.000	-11.000	-3.0000	No	-	-	-	-	-	-
5	28.000	-11.000	-3.0000	Yes	0.0	67.000	25.000	0.0	67.000	25.000

Side	Corner 1		Corner 2		Ground Movement Curve	
	x [m]	y [m]	x [m]	y [m]	Vertical	Horizontal
1	28.000	5.7000	35.500	5.7000	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
2	35.500	5.7000	35.500	-11.000	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
3	35.500	-11.000	30.000	-11.000	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
4	30.000	-11.000	28.000	-11.000	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))
5	28.000	-11.000	28.000	5.7000	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))	Excavation in front of low stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))

Damage Category Strains

Name	0 (Negligible) to 1 (Very Slight)	1 (Very Slight) to 2 (Slight)	2 (Slight) to 3 (Moderate)	3 (Moderate) to 4 (Severe)
Burland Strain Limits	0.0	500.00E-6	750.00E-6	0.0015000

Specific Structures - Geometry

Structure Name	Sub-Structure Name	Displacement Line	Start Distance Along Line [m]	End Distance Along Line [m]	Vertical Offsets from Line for Vertical Movement Calculations [m]	Vertical Displacement Limit Sensitivity [mm]	Damage Category	Strains	Poisson's Ratio	E/G
Law Building	Infill	Law Bdg Infill	0.00000	15.90000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
16 Chenies	West	16 Chenies Wst	0.00000	15.70000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
16 Chenies	South	16 Chenies Sth	0.00000	15.70000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
16 Chenies	East	16 Chenies Est	0.00000	50.90000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
16 Chenies	North	16 Chenies Nth	0.00000	15.70000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
18 Chenies	Retained Wall	18 Chenies Retained Wall	0.00000	19.50000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Law Building	North	Law Bdg Nth	0.00000	20.90000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Law Building	East	Law Bdg Est	0.00000	21.50000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	

Specific Structures - Bending Parameters

Structure Name	Sub-Structure Name	Height [m]	Default Properties	Hogging			Sagging		
				2nd Moment of Area (per unit width) [m ³]	Distance of Bending Strain from N.A. [m]	Distance of N.A. from Edge of Beam in Tension [m]	2nd Moment of Area (per unit width) [m ³]	Distance of Bending Strain from N.A. [m]	Distance of N.A. from Edge of Beam in Tension [m]
Law Building	Infill	10.000	Yes	333.33	10.000	10.000	83.333	5.0000	5.0000
16 Chenies	West	16.000	Yes	1365.3	16.000	16.000	341.33	8.0000	8.0000
16 Chenies	South	16.000	Yes	1365.3	16.000	16.000	341.33	8.0000	8.0000
16 Chenies	East	16.000	Yes	1365.3	16.000	16.000	341.33	8.0000	8.0000
16 Chenies	North	16.000	Yes	1365.3	16.000	16.000	341.33	8.0000	8.0000
18 Chenies	Retained Wall	22.000	Yes	3549.3	22.000	22.000	887.33	11.000	11.000
Law Building	North	22.000	Yes	3549.3	22.000	22.000	887.33	11.000	11.000
Law Building	East	22.000	Yes	3549.3	22.000	22.000	887.33	11.000	11.000

Building Segment Combinations

Structure Name	Sub-Structure Name	Vertical Offset from Line for Vertical Movement Calculations [m]	Segment	Start [m]	Length [m]	Curvature	Combined Segment
Law Building	Infill	0.0	1	0.0	1.8443	Sagging	1
			2	1.8443	2.4224	Hogging	1
			3	4.2667	1.0667	None	1
			4	5.3333	5.3153	Hogging	1
			5	10.649	1.0927	Sagging	1
			6	11.741	3.9318	Hogging	1
			7	15.673	0.22695	None	1
16 Chenies	East	0.0	0	0.0	0.88703	Hogging	1
			2	0.88703	3.6463	Hogging	1
			3	4.5333	1.1333	None	1
			4	5.6667	5.4783	Hogging	1
			5	11.145	0.19946	Sagging	1
			6	11.344	10.989	Hogging	1
			7	22.333	0.51468	Hogging	1
			8	22.848	1.2945	Sagging	1
			9	24.142	4.1884	Sagging	1
			10	28.331	4.5358	Hogging	1

Utility Strain Calculation Options

Neglect beneficial contribution of axial strains : No



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Structure Name	Sub-Structure Name	Vertical Offset from Line for Vertical	Segment	Start	Length	Curvature	Combined Segment
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Warnings

- Multiple excavations have been specified. The displacements resulting from these excavations are calculated by summing the displacements resulting from each individual excavation. No account has been taken of the interactions between excavations (e.g. overlapping zones of influence or 'shielding' of one excavation by another).
- If an embedded wall excavation is assigned a 'surface' ground movement curve and if the 'allow movement calculation to level' option is checked for the excavation then displacements induced by it are calculated for points at the surface, and points below the surface to the level specified. Others are ignored. An example of such a combination, for which displacements will not be calculated is Excavation XP1/Side 1/Line 1/Vertical. This is an example only. There are 13 others.
- If an embedded wall excavation is assigned a 'sub-surface' ground movement curve then displacements induced by it can only be calculated for those points that are level with or below the embedded wall excavation's 'surface level'. Others are ignored. An example of such a combination, for which displacements will not be calculated is Excavation XP1/Side 2/Line 1/Vertical. This is an example only. There are 5 others.

Errors

None

Displacement and Strain Results

Type/No.	Coordinates	Displacements	Angle of Line to x Axis
Name	Dist. x y z	x y z Horizontal displacement along Line Horizontal displacement perpendicular to Line	[°]
Grid 1	[m]	[mm]	
Grid 1	-10.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	-8.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	-6.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	-4.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	-2.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	0.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	2.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	4.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	6.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	8.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	10.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	12.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	14.00000 -20.00000 -2.80000	0.0 0.0 0.27134	-
	16.00000 -20.00000 -2.80000	0.0 0.0 0.60000	-
	18.00000 -20.00000 -2.80000	0.0054992 0.0048090 0.90928	-
	20.00000 -20.00000 -2.80000	0.12054 0.14003 1.1917	-
	22.00000 -20.00000 -2.80000	0.40291 0.72400 1.7533	-
	24.00000 -20.00000 -2.80000	0.46485 1.4520 2.2382	-
	26.00000 -20.00000 -2.80000	0.30444 2.2235 2.6020	-
	28.00000 -20.00000 -2.80000	0.0 2.8520 2.7842	-
	30.00000 -20.00000 -2.80000	0.0 3.4210 2.3689	-
	32.00000 -20.00000 -2.80000	0.0 3.7273 1.8399	-
	34.00000 -20.00000 -2.80000	0.0 4.4545 2.2228	-
	36.00000 -20.00000 -2.80000	-0.17617 4.8100 2.5101	-
	38.00000 -20.00000 -2.80000	-0.80367 3.8556 2.3262	-
	40.00000 -20.00000 -2.80000	-1.1623 2.7754 1.9387	-
	42.00000 -20.00000 -2.80000	-1.1541 1.7444 1.4234	-
	44.00000 -20.00000 -2.80000	-0.78082 0.83976 0.79604	-
	46.00000 -20.00000 -2.80000	-0.093684 0.077000 0.089232	-
	48.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	50.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	52.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	54.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	56.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	58.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	60.00000 -20.00000 -2.80000	0.0 0.0 0.0	-
	-10.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	-8.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	-6.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	-4.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	-2.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	0.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	2.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	4.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	6.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	8.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	10.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	12.00000 -18.00000 -2.80000	0.0 0.0 0.10715	-
	14.00000 -18.00000 -2.80000	0.0 0.0 0.46950	-
	16.00000 -18.00000 -2.80000	0.0 0.0 0.82151	-
	18.00000 -18.00000 -2.80000	0.14121 0.089825 1.1587	-
	20.00000 -18.00000 -2.80000	0.67314 0.55129 1.8202	-
	22.00000 -18.00000 -2.80000	0.98657 1.2465 2.4579	-
	24.00000 -18.00000 -2.80000	0.99555 2.2437 3.0822	-
	26.00000 -18.00000 -2.80000	0.63476 3.4661 3.6155	-
	28.00000 -18.00000 -2.80000	0.0 4.6399 3.9321	-
	30.00000 -18.00000 -2.80000	0.0 5.6449 3.6952	-
	32.00000 -18.00000 -2.80000	0.0 5.7273 3.0145	-
	34.00000 -18.00000 -2.80000	0.0 6.4545 3.4577	-
	36.00000 -18.00000 -2.80000	-0.31696 6.6652 3.7857	-
	38.00000 -18.00000 -2.80000	-1.4341 5.1329 3.4951	-
	40.00000 -18.00000 -2.80000	-2.0654 3.6130 2.9200	-
	42.00000 -18.00000 -2.80000	-2.1189 2.3286 2.2101	-
	44.00000 -18.00000 -2.80000	-1.6779 1.3108 1.4582	-
	46.00000 -18.00000 -2.80000	-0.86378 0.51679 0.68075	-
	48.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	50.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	52.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	54.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	56.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	58.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	60.00000 -18.00000 -2.80000	0.0 0.0 0.0	-
	-10.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	-8.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	-6.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	-4.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	-2.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	0.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	2.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	4.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	6.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	8.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	10.00000 -16.00000 -2.80000	0.0 0.0 0.0	-
	12.00000 -16.00000 -2.80000	0.0 0.0 0.24739	-
	14.00000 -16.00000 -2.80000	0.0 0.0 0.62679	-
	16.00000 -16.00000 -2.80000	0.067574 0.022685 1.0000	-
	18.00000 -16.00000 -2.80000	0.63992 0.24408 1.5953	-
	20.00000 -16.00000 -2.80000	1.4380 0.72406 2.4007	-
	22.00000 -16.00000 -2.80000	1.8640 1.4130 3.1311	-
	24.00000 -16.00000 -2.80000	1.8199 2.5508 3.8776	-
	26.00000 -16.00000 -2.80000	1.2154 4.3817 4.7087	-
	28.00000 -16.00000 -2.80000	0.0 6.6509 5.3021	-
	30.00000 -16.00000 -2.80000	0.0 7.9097 5.3329	-
	32.00000 -16.00000 -2.80000	0.0 7.7273 4.5371	-
	34.00000 -16.00000 -2.80000	0.0 8.4545 5.0517	-
	36.00000 -16.00000 -2.80000	-0.56948 8.4056 5.4206	-
	38.00000 -16.00000 -2.80000	-2.44823 5.9215 4.9122	-
	40.00000 -16.00000 -2.80000	-3.3931 3.8801 3.9987	-
	42.00000 -16.00000 -2.80000	-3.3786 2.4208 2.9949	-
	44.00000 -16.00000 -2.80000	-2.7376 1.4009 2.0443	-
	46.00000 -16.00000 -2.80000	-1.6397 0.67062 1.1565	-
	48.00000 -16.00000 -2.80000	-0.40658 0.13010 0.27135	-
	50.00000 -16.00000 -2.80000	0.0 0.0 0.0	-

Type/No.		Coordinates			Displacements			Angle of Line	
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement
		28.00000	16.00000	-2.80000	0.0	-1.1390	0.55714	-	-
		30.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		32.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		34.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		36.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		38.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		40.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		42.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		44.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		46.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		48.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		50.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		52.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		54.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		56.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		58.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		60.00000	16.00000	-2.80000	0.0	0.0	0.0	-	-
		-10.00000	18.00000	-2.80000	0.0	0.0	0.14000	-	-
		-8.00000	18.00000	-2.80000	0.0	0.0	0.54000	-	-
		-6.00000	18.00000	-2.80000	0.20546	0.0	0.94000	-	-
		-4.00000	18.00000	-2.80000	0.58248	0.0	1.34000	-	-
		-2.00000	18.00000	-2.80000	1.0230	0.0	1.74000	-	-
		0.00000	18.00000	-2.80000	1.5673	0.0	2.14000	-	-
		2.00000	18.00000	-2.80000	2.2561	0.0	2.54000	-	-
		4.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		6.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		8.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		10.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		12.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		14.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		16.00000	18.00000	-2.80000	0.0	0.0	0.080317	-	-
		18.00000	18.00000	-2.80000	0.0	0.0	0.18668	-	-
		20.00000	18.00000	-2.80000	0.0	0.0	0.24429	-	-
		22.00000	18.00000	-2.80000	0.0	0.0	0.24932	-	-
		24.00000	18.00000	-2.80000	0.020396	0.0	0.20280	-	-
		26.00000	18.00000	-2.80000	0.019045	0.0	0.11367	-	-
		28.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		30.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		32.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		34.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		36.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		38.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		40.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		42.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		44.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		46.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		48.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		50.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		52.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		54.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		56.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		58.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		60.00000	18.00000	-2.80000	0.0	0.0	0.0	-	-
		-10.00000	20.00000	-2.80000	0.0	0.0	0.14000	-	-
		-8.00000	20.00000	-2.80000	0.0	0.0	0.54000	-	-
		-6.00000	20.00000	-2.80000	0.20546	0.0	0.94000	-	-
		-4.00000	20.00000	-2.80000	0.58248	0.0	1.34000	-	-
		-2.00000	20.00000	-2.80000	1.0230	0.0	1.74000	-	-
		0.00000	20.00000	-2.80000	1.5673	0.0	2.14000	-	-
		2.00000	20.00000	-2.80000	2.2561	0.0	2.54000	-	-
		4.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		6.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		8.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		10.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		12.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		14.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		16.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		18.00000	20.00000	-2.80000	0.0	0.0	0.042763	-	-
		20.00000	20.00000	-2.80000	0.0	0.0	0.10484	-	-
		22.00000	20.00000	-2.80000	0.0	0.0	0.12406	-	-
		24.00000	20.00000	-2.80000	0.0	0.0	0.10943	-	-
		26.00000	20.00000	-2.80000	0.0	0.0	0.063001	-	-
		28.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		30.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		32.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		34.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		36.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		38.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		40.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		42.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		44.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		46.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		48.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		50.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		52.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		54.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		56.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		58.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		60.00000	20.00000	-2.80000	0.0	0.0	0.0	-	-
		-10.00000	22.00000	-2.80000	0.0	0.0	0.14000	-	-
		-8.00000	22.00000	-2.80000	0.0	0.0	0.54000	-	-
		-6.00000	22.00000	-2.80000	0.20546	0.0	0.94000	-	-
		-4.00000	22.00000	-2.80000	0.58248	0.0	1.34000	-	-
		-2.00000	22.00000	-2.80000	1.0230	0.0	1.74000	-	-
		0.00000	22.00000	-2.80000	1.5673	0.0	2.14000	-	-
		2.00000	22.00000	-2.80000	4.5122	0.0	5.08000	-	-
		4.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		6.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		8.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		10.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		12.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		14.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		16.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		18.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		20.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		22.00000	22.00000	-2.80000	0.0	0.0	0.028327	-	-
		24.00000	22.00000	-2.80000	0.0	0.0	0.037269	-	-
		26.00000	22.00000	-2.80000	0.0	0.0	0.024526	-	-
		28.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		30.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		32.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		34.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		36.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		38.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		40.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		42.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		44.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		46.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		48.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		50.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		52.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		54.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		56.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		58.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		60.00000	22.00000	-2.80000	0.0	0.0	0.0	-	-
		-10.00000	24.00000	-2.80000	0.0	0.0	0.10018	-	-
		-8.00000	24.00000	-2.80000	0.0	0.0	0.45007	-	-
		-6.00000	24.00000	-2.80000	0.14600	0.0	0.77968	-	-
		-4.00000	24.00000	-2.80000	0.44235	0.0	1.07400	-	-
		-2.00000	24.00000	-2.80000	0.73048	0.0	1.2988	-	-
		0.00000	24.00000	-2.80000	0.94424	0.0	1.3616	-	-
		2.00000	24.00000	-2.80000	0.77474	0.0	0.95862	-	-
		4.00000	24.00000	-2.80000	0.0	0.0	0.0	-	-
		6.00000	24.00000	-2.80000	0.0	0.0	0.0	-	-
		8.00000	24.00000	-2.80000	0.0	0.0	0.0	-	-
		10.00000	24.00000	-2.80000	0.0	0.0	0.0	-	-
		12.00000	24.00000	-2.80000	0.0	0.0	0.0	-	-



Royal Academy of Dramatic Arts
16-18 Cheries Street Development
Run 4 Excavation and imported Installation

Job No.	Sheet No.	Rev.
J15215		
Drq. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Type/No.	Coordinates			Displacements				Angle of Line		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
	12.800	14.80000	6.00000	-1.50000	0.053600	0.0	0.94544	0.053600	0.0	0.0 *
	13.867	15.86667	6.00000	-1.50000	0.23963	0.0	1.1541	0.23963	0.0	0.0 *
	14.933	16.93333	6.00000	-1.50000	1.0389	-0.0080166	1.6681	1.0389	-0.0080166	0.0 *
	16.000	18.00000	6.00000	-1.50000	1.9326	-0.019050	2.2147	1.9326	-0.019050	0.0 *
16 Cheries Line 2	2.00000	22.00000	-2.80000	4.5122	0.0	5.0800	4.5122	0.0	0.0 *	
Wst										
	1.1333	3.13333	22.00000	-2.80000	2.7258	0.0	2.7667	2.7258	0.0	0.0 *
	2.2667	4.26667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	3.4000	5.40000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	4.5333	6.53333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	5.6667	7.66667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	6.8000	8.80000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	7.9333	9.93333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	9.0667	11.06667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	10.2000	12.20000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	11.3333	13.33333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	12.4667	14.46667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	13.6000	15.60000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	14.7333	16.73333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	15.8667	17.86667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	17.0000	19.00000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	18.1333	20.13333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	19.2667	21.26667	22.00000	-2.80000	0.0	0.018156	0.0	0.0	0.0	0.0 *
	20.4000	22.40000	22.00000	-2.80000	0.0	0.032227	0.0	0.0	0.0	0.0 *
	21.5333	23.53333	22.00000	-2.80000	0.0	0.037429	0.0	0.0	0.0	0.0 *
	22.6667	24.66667	22.00000	-2.80000	0.0	0.034948	0.0	0.0	0.0	0.0 *
	23.8000	25.80000	22.00000	-2.80000	0.0	0.026514	0.0	0.0	0.0	0.0 *
	24.9333	26.93333	22.00000	-2.80000	0.0	0.013854	0.0	0.0	0.0	0.0 *
	26.0667	28.06667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	27.2000	29.20000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	28.3333	30.33333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	29.4667	31.46667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	30.6000	32.60000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	31.7333	33.73333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	32.8667	34.86667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	34.0000	36.00000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	35.1333	37.13333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	36.2667	38.26667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	37.4000	39.40000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	38.5333	40.53333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	39.6667	41.66667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	40.8000	42.80000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	41.9333	43.93333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	43.0667	45.06667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	44.2000	46.20000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	45.3333	47.33333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	46.4667	48.46667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	47.6000	49.60000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	48.7333	50.73333	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	49.8667	51.86667	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	51.0000	53.00000	22.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
16 Cheries Line 3	2.00000	21.90000	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0	0.0 *
Sth										
	1.0533	2.00000	20.84667	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	2.1067	2.00000	19.79333	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	3.1600	2.00000	18.74000	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	4.2133	2.00000	17.68667	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	5.2667	2.00000	16.63333	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	6.3200	2.00000	15.58000	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	7.3733	2.00000	14.52667	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	8.4267	2.00000	13.47333	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	9.4800	2.00000	12.42000	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	10.5333	2.00000	11.36667	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	11.5867	2.00000	10.31333	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	12.6400	2.00000	9.26000	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	13.6933	2.00000	8.20667	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	14.7467	2.00000	7.15333	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
	15.8000	2.00000	6.10000	-2.80000	2.2561	0.0	2.5400	2.2561	270.00	0.0 *
16 Cheries Line 4	2.00000	6.00000	-2.80000	4.5122	0.0	5.0800	4.5122	0.0	0.0	0.0 *
Est										
	1.1333	3.13333	6.00000	-2.80000	2.7258	0.0	2.7667	2.7258	0.0	0.0 *
	2.2667	4.26667	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	3.4000	5.40000	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	4.5333	6.53333	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	5.6667	7.66667	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	6.8000	8.80000	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	7.9333	9.93333	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	9.0667	11.06667	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	10.2000	12.20000	6.00000	-2.80000	0.0	0.43412	0.0	0.0	0.0	0.0 *
	11.3333	13.33333	6.00000	-2.80000	0.0	0.0	0.0	0.0	0.0	0.0 *
	12.4667	14.46667	6.00000	-2.80000	0.0	0.0	0.88007	0.0	0.0	0.0 *
	13.6000	15.60000	6.00000	-2.80000	0.19288	0.0	1.1020	0.19288	0.0	0.0 *
	14.7333	16.73333	6.00000	-2.80000	0.87194	-0.0061802	1.5649	0.87194	-0.0061802	0.0 *
	15.8667	17.86667	6.00000	-2.80000	1.8206	-0.017544	2.1464	1.8206	-0.017544	0.0 *
	17.0000	19.00000	6.00000	-2.80000	2.7764	-0.031766	2.7327	2.7764	-0.031766	0.0 *
	18.1333	20.13333	6.00000	-2.80000	3.7410	-0.050081	3.3453	3.7410	-0.050081	0.0 *
	19.2667	21.26667	6.00000	-2.80000	4.7141	-0.074548	4.0046	4.7141	-0.074548	0.0 *
	20.4000	22.40000	6.00000	-2.80000	5.6918	-0.10889	4.7290	5.6918	-0.10889	0.0 *
	21.5333	23.53333	6.00000	-2.80000	6.6611	-0.16060	5.5322	6.6611	-0.16060	0.0 *
	22.6667	24.66667	6.00000	-2.80000	7.5854	-0.24723	6.4155	7.5854	-0.24723	0.0 *
	23.8000	25.80000	6.00000	-2.80000	8.3455	-0.42189	7.3358	8.3455	-0.42189	0.0 *
	24.9333	26.93333	6.00000	-2.80000	8.3246	-0.95054	7.9862	8.3246	-0.95054	0.0 *
	26.0667	28.06667	6.00000	-2.80000	0.0	-11.593	9.7245	0.0	-11.593	0.0 *
	27.2000	29.20000	6.00000	-2.80000	0.0	-9.7800	8.1640	0.0	-9.7800	0.0 *
	28.3333	30.33333	6.00000	-2.80000	0.0	-7.9667	6.6043	0.0	-7.9667	0.0 *
	29.4667	31.46667	6.00000	-2.80000	0.0	-6.1533	5.0462	0.0	-6.1533	0.0 *
	30.6000	32.60000	6.00000	-2.80000	0.0	-4.3400	3.4914	0.0	-4.3400	0.0 *
	31.7333	33.73333	6.00000	-2.80000	0.0	-2.5267	1.9			



Royal Academy of Dramatic Arts
16-18 Cheries Street Development
Run 4 Excavation and imported Installation

Job No.	Sheet No.	Rev.
J15215		
Drq. Ref.		
Made by	Date	Checked
MC	04-Jul-2017	

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
46.467	48.46667	22.00000	-2.80000	0.0	0.0	0.0
47.600	49.60000	22.00000	-2.80000	0.0	0.0	0.0
48.733	50.73333	22.00000	-2.80000	0.0	0.0	0.0
49.867	51.86667	22.00000	-2.80000	0.0	0.0	0.0
51.000	53.00000	22.00000	-2.80000	0.0	0.0	0.0

d - Displacements include imported displacements.

Structure: 16 Cheries | Sub-structure: South

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]
0.0	2.00000	21.90000	-2.80000	2.2561	0.0	0.0
1.0533	2.00000	20.84667	-2.80000	2.2561	0.0	0.0
2.1067	2.00000	19.79333	-2.80000	2.2561	0.0	0.0
3.1600	2.00000	18.74000	-2.80000	2.2561	0.0	0.0
4.2133	2.00000	17.68667	-2.80000	2.2561	0.0	0.0
5.2667	2.00000	16.63333	-2.80000	2.2561	0.0	0.0
6.3200	2.00000	15.58000	-2.80000	2.2561	0.0	0.0
7.3733	2.00000	14.52667	-2.80000	2.2561	0.0	0.0
8.4267	2.00000	13.47333	-2.80000	2.2561	0.0	0.0
9.4800	2.00000	12.42000	-2.80000	2.2561	0.0	0.0
10.533	2.00000	11.36667	-2.80000	2.2561	0.0	0.0
11.587	2.00000	10.31333	-2.80000	2.2561	0.0	0.0
12.640	2.00000	9.26000	-2.80000	2.2561	0.0	0.0
13.693	2.00000	8.20667	-2.80000	2.2561	0.0	0.0
14.747	2.00000	7.15333	-2.80000	2.2561	0.0	0.0
15.800	2.00000	6.10000	-2.80000	2.2561	0.0	0.0

d - Displacements include imported displacements.

Structure: 16 Cheries | Sub-structure: East

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]
0.0	2.00000	6.00000	-2.80000	4.5122	0.0	0.0
1.1333	3.13333	6.00000	-2.80000	2.7258	0.0	0.0
2.2667	4.26667	6.00000	-2.80000	0.0	0.0	0.0
3.4000	5.40000	6.00000	-2.80000	0.0	0.0	0.0
4.5333	6.53333	6.00000	-2.80000	0.0	0.0	0.0
5.6667	7.66667	6.00000	-2.80000	0.0	0.0	0.0
6.8000	8.80000	6.00000	-2.80000	0.0	0.0	0.0
7.9333	9.93333	6.00000	-2.80000	0.0	0.0	0.0
9.0667	11.06667	6.00000	-2.80000	0.0	0.0	0.0
10.2000	12.20000	6.00000	-2.80000	0.0	0.0	0.0
11.3333	13.33333	6.00000	-2.80000	0.0	0.0	0.0
12.4667	14.46667	6.00000	-2.80000	0.0	0.0	0.0
13.6000	15.60000	6.00000	-2.80000	0.19288	0.0	0.0
14.7333	16.73333	6.00000	-2.80000	0.87194	-0.0061802	0.87194
15.867	17.86667	6.00000	-2.80000	1.8206	-0.017544	1.8206
17.0000	19.00000	6.00000	-2.80000	2.7764	-0.031766	2.7764
18.1333	20.13333	6.00000	-2.80000	3.7410	-0.050081	3.7410
19.2667	21.26667	6.00000	-2.80000	4.7141	-0.074548	4.7141
20.4000	22.40000	6.00000	-2.80000	5.6918	-0.10889	5.6918
21.5333	23.53333	6.00000	-2.80000	6.6611	-0.16060	6.6611
22.6667	24.66667	6.00000	-2.80000	7.5854	-0.24723	7.5854
23.8000	25.80000	6.00000	-2.80000	8.3455	-0.42189	8.3455
24.9333	26.93333	6.00000	-2.80000	8.3246	-0.95054	8.3246
26.067	28.06667	6.00000	-2.80000	0.0	-11.593	0.0
27.2000	29.20000	6.00000	-2.80000	0.0	-9.7800	0.0
28.3333	30.33333	6.00000	-2.80000	0.0	-7.9667	0.0
29.4667	31.46667	6.00000	-2.80000	0.0	-6.1533	0.0
30.6000	32.60000	6.00000	-2.80000	0.0	-4.3400	0.0
31.7333	33.73333	6.00000	-2.80000	0.0	-2.5267	0.0
32.867	34.86667	6.00000	-2.80000	0.0	-0.71333	0.0
34.0000	36.00000	6.00000	-2.80000	0.0	0.0	0.0
35.1333	37.13333	6.00000	-2.80000	0.0	0.0	0.0
36.267	38.26667	6.00000	-2.80000	0.0	0.0	0.0
37.4000	39.40000	6.00000	-2.80000	0.0	0.0	0.0
38.5333	40.53333	6.00000	-2.80000	0.0	0.0	0.0
39.667	41.66667	6.00000	-2.80000	0.0	0.0	0.0
40.8000	42.80000	6.00000	-2.80000	0.0	0.0	0.0
41.9333	43.93333	6.00000	-2.80000	0.0	0.0	0.0
43.067	45.06667	6.00000	-2.80000	0.0	0.0	0.0
44.2000	46.20000	6.00000	-2.80000	0.0	0.0	0.0
45.3333	47.33333	6.00000	-2.80000	0.0	0.0	0.0
46.467	48.46667	6.00000	-2.80000	0.0	0.0	0.0
47.6000	49.60000	6.00000	-2.80000	0.0	0.0	0.0
48.7333	50.73333	6.00000	-2.80000	0.0	0.0	0.0
49.867	51.86667	6.00000	-2.80000	0.0	0.0	0.0
51.0000	53.00000	6.00000	-2.80000	0.0	0.0	0.0

d - Displacements include imported displacements.

Structure: 16 Cheries | Sub-structure: North

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]
0.0	53.00000	21.90000	-2.80000	0.0	0.0	0.0
1.0533	53.00000	20.84667	-2.80000	0.0	0.0	0.0
2.1067	53.00000	19.79333	-2.80000	0.0	0.0	0.0
3.1600	53.00000	18.74000	-2.80000	0.0	0.0	0.0
4.2133	53.00000	17.68667	-2.80000	0.0	0.0	0.0
5.2667	53.00000	16.63333	-2.80000	0.0	0.0	0.0
6.3200	53.00000	15.58000	-2.80000	0.0	0.0	0.0
7.3733	53.00000	14.52667	-2.80000	0.0	0.0	0.0
8.4267	53.00000	13.47333	-2.80000	0.0	0.0	0.0
9.4800	53.00000	12.42000	-2.80000	0.0	0.0	0.0
10.533	53.00000	11.36667	-2.80000	0.0	0.0	0.0
11.587	53.00000	10.31333	-2.80000	0.0	0.0	0.0
12.640	53.00000	9.26000	-2.80000	0.0	0.0	0.0
13.693	53.00000	8.20667	-2.80000	0.0	0.0	0.0
14.747	53.00000	7.15333	-2.80000	0.0	0.0	0.0
15.800	53.00000	6.10000	-2.80000	0.0	0.0	0.0

d - Displacements include imported displacements.

Structure: 18 Cheries | Sub-structure: Retained Wall

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]
0.0	39.00000	-13.60000	-3.50000	0.0	0.0	0.0
0.98000	39.00000	-12.62000	-3.50000	0.0	0.0	0.0
1.96000	39.00000	-11.64000	-3.50000	0.0	0.0	0.0
2.94000	39.00000	-10.66000	-3.50000	0.0	0.0	0.0
3.92000	39.00000	-9.68000	-3.50000	0.0	0.0	0.0
4.90000	39.00000	-8.70000	-3.50000	0.0	0.0	0.0
5.88000	39.00000	-7.72000	-3.50000	0.0	0.0	0.0
6.86000	39.00000	-6.74000	-3.50000	0.0	0.0	0.0
7.84000	39.00000	-5.76000	-3.50000	0.0	0.0	0.0
8.82000	39.00000	-4.78000	-3.50000	0.0	0.0	0.0
9.80000	39.00000	-3.80000	-3.50000	0.0	0.0	0.0
10.78000	39.00000	-2.82000	-3.50000	0.0	0.0	0.0

Job No.	Sheet No.	Rev.
J15215		
Dr. Ref.		
Made by MC	Date 04-Jul-2017	Checked

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
11.760	39.00000	-1.84000	-3.50000	0.0	0.0	0.0
12.740	39.00000	-0.86000	-3.50000	0.0	0.0	0.0
13.720	39.00000	0.12000	-3.50000	0.0	0.0	0.0
14.700	39.00000	1.10000	-3.50000	0.0	0.0	0.0
15.680	39.00000	2.08000	-3.50000	0.0	0.0	0.0
16.660	39.00000	3.06000	-3.50000	0.0	0.0	0.0
17.640	39.00000	4.04000	-3.50000	0.0	0.0	0.0
18.620	39.00000	5.02000	-3.50000	0.0	0.0	0.0
19.600	39.00000	6.00000	-3.50000	0.0	0.0	0.0

Structure: Law Building | Sub-structure: North

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	21.60000	4.00000	-2.80000	7.0390	0.0	0.0
1.050	21.60000	2.95000	-2.80000	7.0390	0.0	0.0
2.100	21.60000	1.90000	-2.80000	7.0390	0.0	0.0
3.150	21.60000	0.85000	-2.80000	7.0390	0.0	0.0
4.200	21.60000	-0.20000	-2.80000	7.0390	0.0	0.0
5.250	21.60000	-1.25000	-2.80000	7.0390	0.0	0.0
6.300	21.60000	-2.30000	-2.80000	7.0390	0.0	0.0
7.350	21.60000	-3.35000	-2.80000	7.0390	0.0	0.0
8.400	21.60000	-4.40000	-2.80000	7.0390	0.0	0.0
9.450	21.60000	-5.45000	-2.80000	7.0390	0.0	0.0
10.500	21.60000	-6.50000	-2.80000	7.0390	0.0	0.0
11.550	21.60000	-7.55000	-2.80000	7.0390	0.0	0.0
12.600	21.60000	-8.60000	-2.80000	7.0390	0.0	0.0
13.650	21.60000	-9.65000	-2.80000	7.0390	0.0	0.0
14.700	21.60000	-10.70000	-2.80000	7.0390	0.0	0.0
15.750	21.60000	-11.75000	-2.80000	4.6979	0.31236	-0.31236
16.800	21.60000	-12.80000	-2.80000	3.9371	0.70727	-0.70727
17.850	21.60000	-13.85000	-2.80000	3.1720	1.0096	-1.0096
18.900	21.60000	-14.90000	-2.80000	2.4640	1.1934	-1.1934
19.950	21.60000	-15.95000	-2.80000	1.8453	1.2538	-1.2538
21.000	21.60000	-17.00000	-2.80000	1.3255	1.2002	-1.2002

Structure: Law Building | Sub-structure: East

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	21.60000	-17.10000	-2.80000	1.2811	1.1897	-1.1897
1.080	20.52000	-17.10000	-2.80000	1.1146	0.82026	-1.1146
2.160	19.44000	-17.10000	-2.80000	0.83315	0.50719	-0.83315
3.240	18.36000	-17.10000	-2.80000	0.45858	0.24113	-0.45858
4.320	17.28000	-17.10000	-2.80000	0.13969	0.068598	-0.13969
5.400	16.20000	-17.10000	-2.80000	0.028048	0.012236	-0.028048
6.480	15.12000	-17.10000	-2.80000	0.0	0.0	0.0
7.560	14.04000	-17.10000	-2.80000	0.0	0.0	0.0
8.640	12.96000	-17.10000	-2.80000	0.0	0.0	0.0
9.720	11.88000	-17.10000	-2.80000	0.0	0.0	0.0
10.800	10.80000	-17.10000	-2.80000	0.0	0.0	0.0
11.880	9.72000	-17.10000	-2.80000	0.0	0.0	0.0
12.960	8.64000	-17.10000	-2.80000	0.0	0.0	0.0
14.040	7.56000	-17.10000	-2.80000	0.0	0.0	0.0
15.120	6.48000	-17.10000	-2.80000	0.0	0.0	0.0
16.200	5.40000	-17.10000	-2.80000	0.0	0.0	0.0
17.280	4.32000	-17.10000	-2.80000	0.0	0.0	0.0
18.360	3.24000	-17.10000	-2.80000	0.0	0.0	0.0
19.440	2.16000	-17.10000	-2.80000	0.0	0.0	0.0
20.520	1.08000	-17.10000	-2.80000	0.0	0.0	0.0
21.600	0.00000	-17.10000	-2.80000	0.0	0.0	0.0

Specific Building Damage Results - Vertical Displacements

Structure: Law Building | Sub-structure: Infill

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	2.00000	6.00000	-1.50000	2.9672	0.0	0.0
1.0667	3.06667	6.00000	-1.50000	3.3799	0.0	0.0
2.1333	4.13333	6.00000	-1.50000	0.0	0.0	0.0
3.2000	5.20000	6.00000	-1.50000	0.0	0.0	0.0
4.2667	6.26667	6.00000	-1.50000	0.0	0.0	0.0
5.3333	7.33333	6.00000	-1.50000	0.0	0.0	0.0
6.4000	8.40000	6.00000	-1.50000	0.0	0.0	0.0
7.4667	9.46667	6.00000	-1.50000	0.0	0.0	0.0
8.5333	10.53333	6.00000	-1.50000	0.10499	0.0	0.0
9.6000	11.60000	6.00000	-1.50000	0.31573	0.0	0.0
10.667	12.66667	6.00000	-1.50000	0.52611	0.0	0.0
11.733	13.73333	6.00000	-1.50000	0.73605	0.0	0.0
12.800	14.80000	6.00000	-1.50000	0.94544	0.0	0.0
13.867	15.86667	6.00000	-1.50000	1.1541	0.0	0.0
14.933	16.93333	6.00000	-1.50000	1.6681	0.0	0.0
16.000	18.00000	6.00000	-1.50000	2.2147	0.0	0.0

Structure: 16 Cheries | Sub-structure: West

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	2.00000	22.00000	-2.80000	5.0800	0.0	0.0
1.1333	3.13333	22.00000	-2.80000	2.7667	0.0	0.0
2.2667	4.26667	22.00000	-2.80000	0.0	0.0	0.0
3.4000	5.40000	22.00000	-2.80000	0.0	0.0	0.0
4.5333	6.53333	22.00000	-2.80000	0.0	0.0	0.0
5.6667	7.66667	22.00000	-2.80000	0.0	0.0	0.0
6.8000	8.80000	22.00000	-2.80000	0.0	0.0	0.0
7.9333	9.93333	22.00000	-2.80000	0.0	0.0	0.0
9.0667	11.06667	22.00000	-2.80000	0.0	0.0	0.0
10.2000	12.20000	22.00000	-2.80000	0.0	0.0	0.0
11.3333	13.33333	22.00000	-2.80000	0.0	0.0	0.0
12.4667	14.46667	22.00000	-2.80000	0.0	0.0	0.0
13.6000	15.60000	22.00000	-2.80000	0.0	0.0	0.0
14.7333	16.73333	22.00000	-2.80000	0.0	0.0	0.0
15.8667	17.86667	22.00000	-2.80000	0.0	0.0	0.0
17.0000	19.00000	22.00000	-2.80000	0.0	0.0	0.0
18.1333	20.13333	22.00000	-2.80000	0.0	0.0	0.0
19.2667	21.26667	22.00000	-2.80000	0.038156	0.0	0.0
20.4000	22.40000	22.00000	-2.80000	0.032227	0.0	0.0
21.5333	23.53333	22.00000	-2.80000	0.037429	0.0	0.0
22.6667	24.66667	22.00000	-2.80000	0.034998	0.0	0.0
23.8000	25.80000	22.00000	-2.80000	0.026514	0.0	0.0
24.9333	26.93333	22.00000	-2.80000	0.033854	0.0	0.0
26.0667	28.06667	22.00000	-2.80000	0.0	0.0	0.0
27.2000	29.20000	22.00000	-2.80000	0.0	0.0	0.0
28.3333	30.33333	22.00000	-2.80000	0.0	0.0	0.0
29.4667	31.46667	22.00000	-2.80000	0.0	0.0	0.0



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Dist.	Coordinates			Displacements	
[m]	x [m]	y [m]	z [m]	z [mm]	

30.600	32.60000	22.00000	-2.80000	0.0	d
31.733	33.73333	22.00000	-2.80000	0.0	d
32.867	34.86667	22.00000	-2.80000	0.0	d
34.000	36.00000	22.00000	-2.80000	0.0	d
35.133	37.13333	22.00000	-2.80000	0.0	d
36.267	38.26667	22.00000	-2.80000	0.0	d
37.400	39.40000	22.00000	-2.80000	0.0	d
38.533	40.53333	22.00000	-2.80000	0.0	d
39.667	41.66667	22.00000	-2.80000	0.0	d
40.800	42.80000	22.00000	-2.80000	0.0	d
41.933	43.93333	22.00000	-2.80000	0.0	d
43.067	45.06667	22.00000	-2.80000	0.0	d
44.200	46.20000	22.00000	-2.80000	0.0	d
45.333	47.33333	22.00000	-2.80000	0.0	d
46.467	48.46667	22.00000	-2.80000	0.0	d
47.600	49.60000	22.00000	-2.80000	0.0	d
48.733	50.73333	22.00000	-2.80000	0.0	d
49.867	51.86667	22.00000	-2.80000	0.0	d
51.000	53.00000	22.00000	-2.80000	0.0	d

d - Displacements include imported displacements.

Structure: 16 Cheries | Sub-structure: South

Dist.	Coordinates			Displacements	
[m]	x [m]	y [m]	z [m]	z [mm]	

Vertical Offset 1

0.0	2.00000	21.90000	-2.80000	2.5400	d
1.0533	2.00000	20.84667	-2.80000	2.5400	d
2.1067	2.00000	19.79333	-2.80000	2.5400	d
3.1600	2.00000	18.74000	-2.80000	2.5400	d
4.2133	2.00000	17.68667	-2.80000	2.5400	d
5.2667	2.00000	16.63333	-2.80000	2.5400	d
6.3200	2.00000	15.58000	-2.80000	2.5400	d
7.3733	2.00000	14.52667	-2.80000	2.5400	d
8.4267	2.00000	13.47333	-2.80000	2.5400	d
9.4800	2.00000	12.42000	-2.80000	2.5400	d
10.5333	2.00000	11.36667	-2.80000	2.5400	d
11.5867	2.00000	10.31333	-2.80000	2.5400	d
12.6400	2.00000	9.26000	-2.80000	2.5400	d
13.6933	2.00000	8.20667	-2.80000	2.5400	d
14.7467	2.00000	7.15333	-2.80000	2.5400	d
15.8000	2.00000	6.10000	-2.80000	2.5400	d

d - Displacements include imported displacements.

Structure: 16 Cheries | Sub-structure: East

Dist.	Coordinates			Displacements	
[m]	x [m]	y [m]	z [m]	z [mm]	

Vertical Offset 1

0.0	2.00000	6.00000	-2.80000	5.0800	d
1.1333	3.13333	6.00000	-2.80000	2.7622	d
2.2667	4.26667	6.00000	-2.80000	0.0	d
3.4000	5.40000	6.00000	-2.80000	0.0	d
4.5333	6.53333	6.00000	-2.80000	0.0	d
5.6667	7.66667	6.00000	-2.80000	0.0	d
6.8000	8.80000	6.00000	-2.80000	0.0	d
7.9333	9.93333	6.00000	-2.80000	0.0	d
9.0667	11.06667	6.00000	-2.80000	0.21040	d
10.2000	12.20000	6.00000	-2.80000	0.43412	d
11.3333	13.33333	6.00000	-2.80000	0.65738	d
12.4667	14.46667	6.00000	-2.80000	0.88007	d
13.6000	15.60000	6.00000	-2.80000	1.1020	d
14.7333	16.73333	6.00000	-2.80000	1.5649	d
15.8667	17.86667	6.00000	-2.80000	2.1464	d
17.0000	19.00000	6.00000	-2.80000	2.7327	d
18.1333	20.13333	6.00000	-2.80000	3.3453	d
19.2667	21.26667	6.00000	-2.80000	4.0046	d
20.4000	22.40000	6.00000	-2.80000	4.7290	d
21.5333	23.53333	6.00000	-2.80000	5.5322	d
22.6667	24.66667	6.00000	-2.80000	6.4155	d
23.8000	25.80000	6.00000	-2.80000	7.3358	d
24.9333	26.93333	6.00000	-2.80000	7.9862	d
26.0667	28.06667	6.00000	-2.80000	9.7245	d
27.2000	29.20000	6.00000	-2.80000	8.1640	d
28.3333	30.33333	6.00000	-2.80000	6.6043	d
29.4667	31.46667	6.00000	-2.80000	5.0462	d
30.6000	32.60000	6.00000	-2.80000	3.4914	d
31.7333	33.73333	6.00000	-2.80000	1.9462	d
32.8667	34.86667	6.00000	-2.80000	0.45550	d
34.0000	36.00000	6.00000	-2.80000	0.0	d
35.1333	37.13333	6.00000	-2.80000	0.0	d
36.2667	38.26667	6.00000	-2.80000	0.0	d
37.4000	39.40000	6.00000	-2.80000	0.0	d
38.5333	40.53333	6.00000	-2.80000	0.0	d
39.6667	41.66667	6.00000	-2.80000	0.0	d
40.8000	42.80000	6.00000	-2.80000	0.0	d
41.9333	43.93333	6.00000	-2.80000	0.0	d
43.0667	45.06667	6.00000	-2.80000	0.0	d
44.2000	46.20000	6.00000	-2.80000	0.0	d
45.3333	47.33333	6.00000	-2.80000	0.0	d
46.4667	48.46667	6.00000	-2.80000	0.0	d
47.6000	49.60000	6.00000	-2.80000	0.0	d
48.7333	50.73333	6.00000	-2.80000	0.0	d
49.8667	51.86667	6.00000	-2.80000	0.0	d
51.0000	53.00000	6.00000	-2.80000	0.0	d

d - Displacements include imported displacements.

Structure: 16 Cheries | Sub-structure: North

Dist.	Coordinates			Displacements	
[m]	x [m]	y [m]	z [m]	z [mm]	

Vertical Offset 1

0.0	53.00000	21.90000	-2.80000	0.0	d
1.0533	53.00000	20.84667	-2.80000	0.0	d
2.1067	53.00000	19.79333	-2.80000	0.0	d
3.1600	53.00000	18.74000	-2.80000	0.0	d
4.2133	53.00000	17.68667	-2.80000	0.0	d
5.2667	53.00000	16.63333	-2.80000	0.0	d
6.3200	53.00000	15.58000	-2.80000	0.0	d
7.3733	53.00000	14.52667	-2.80000	0.0	d
8.4267	53.00000	13.47333	-2.80000	0.0	d
9.4800	53.00000	12.42000	-2.80000	0.0	d
10.5333	53.00000	11.36667	-2.80000	0.0	d
11.5867	53.00000	10.31333	-2.80000	0.0	d
12.6400	53.00000	9.26000	-2.80000	0.0	d
13.6933	53.00000	8.20667	-2.80000	0.0	d
14.7467	53.00000	7.15333	-2.80000	0.0	d
15.8000	53.00000	6.10000	-2.80000	0.0	d

d - Displacements include imported displacements.

Structure: 18 Cheries | Sub-structure: Retained Wall

Dist.	Coordinates			Displacements	
[m]	x [m]	y [m]	z [m]	z [mm]	

Vertical Offset 1

0.0	39.00000	-13.60000	-3.50000	0.0	d
0.98000	39.00000	-12.62000	-3.50000	0.0	d
1.96000	39.00000	-11.64000	-3.50000	0.0	d



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Dist.	Coordinates			Displacements	
	x [m]	y [m]	z [m]	z [mm]	
2.9400	39.00000	-10.66000	-3.50000	0.0	d
3.9200	39.00000	-9.68000	-3.50000	0.0	d
4.9000	39.00000	-8.70000	-3.50000	0.0	d
5.8800	39.00000	-7.72000	-3.50000	0.0	d
6.8600	39.00000	-6.74000	-3.50000	0.0	d
7.8400	39.00000	-5.76000	-3.50000	0.0	d
8.8200	39.00000	-4.78000	-3.50000	0.0	d
9.8000	39.00000	-3.80000	-3.50000	0.0	d
10.7800	39.00000	-2.82000	-3.50000	0.0	d
11.7600	39.00000	-1.84000	-3.50000	0.0	d
12.7400	39.00000	-0.86000	-3.50000	0.0	d
13.7200	39.00000	0.12000	-3.50000	0.0	d
14.7000	39.00000	1.10000	-3.50000	0.0	d
15.6800	39.00000	2.08000	-3.50000	0.0	d
16.6600	39.00000	3.06000	-3.50000	0.0	d
17.6400	39.00000	4.04000	-3.50000	0.0	d
18.6200	39.00000	5.02000	-3.50000	0.0	d
19.6000	39.00000	6.00000	-3.50000	0.0	d

d - Displacements include imported displacements.

Structure: Law Building | Sub-structure: North

Dist.	Coordinates			Displacements	
	x [m]	y [m]	z [m]	z [mm]	
Vertical Offset 1					
0.0	21.60000	4.00000	-2.80000	5.2962	d
1.0500	21.60000	2.95000	-2.80000	5.2962	d
2.1000	21.60000	1.90000	-2.80000	5.2962	d
3.1500	21.60000	0.85000	-2.80000	5.2962	d
4.2000	21.60000	-0.20000	-2.80000	5.2962	d
5.2500	21.60000	-1.25000	-2.80000	5.2962	d
6.3000	21.60000	-2.30000	-2.80000	5.2962	d
7.3500	21.60000	-3.35000	-2.80000	5.2962	d
8.4000	21.60000	-4.40000	-2.80000	5.2962	d
9.4500	21.60000	-5.45000	-2.80000	5.2962	d
10.5000	21.60000	-6.50000	-2.80000	5.2962	d
11.5500	21.60000	-7.55000	-2.80000	5.2962	d
12.6000	21.60000	-8.60000	-2.80000	5.2962	d
13.6500	21.60000	-9.65000	-2.80000	5.2962	d
14.7000	21.60000	-10.70000	-2.80000	5.2962	d
15.7500	21.60000	-11.75000	-2.80000	4.2110	d
16.8000	21.60000	-12.80000	-2.80000	3.9866	d
17.8500	21.60000	-13.85000	-2.80000	3.6944	d
18.9000	21.60000	-14.90000	-2.80000	3.3617	d
19.9500	21.60000	-15.95000	-2.80000	3.0090	d
21.0000	21.60000	-17.00000	-2.80000	2.6491	d

d - Displacements include imported displacements.

Structure: Law Building | Sub-structure: East

Dist.	Coordinates			Displacements	
	x [m]	y [m]	z [m]	z [mm]	
Vertical Offset 1					
0.0	21.60000	-17.10000	-2.80000	2.6146	d
1.0800	20.52000	-17.10000	-2.80000	2.2672	d
2.1600	19.44000	-17.10000	-2.80000	1.8992	d
3.2400	18.36000	-17.10000	-2.80000	1.4812	d
4.3200	17.28000	-17.10000	-2.80000	1.1332	d
5.4000	16.20000	-17.10000	-2.80000	0.94331	d
6.4800	15.12000	-17.10000	-2.80000	0.74971	d
7.5600	14.04000	-17.10000	-2.80000	0.55309	d
8.6400	12.96000	-17.10000	-2.80000	0.35401	d
9.7200	11.88000	-17.10000	-2.80000	0.15289	d
10.8000	10.80000	-17.10000	-2.80000	0.0	d
11.8800	9.72000	-17.10000	-2.80000	0.0	d
12.9600	8.64000	-17.10000	-2.80000	0.0	d
14.0400	7.56000	-17.10000	-2.80000	0.0	d
15.1200	6.48000	-17.10000	-2.80000	0.0	d
16.2000	5.40000	-17.10000	-2.80000	0.0	d
17.2800	4.32000	-17.10000	-2.80000	0.0	d
18.3600	3.24000	-17.10000	-2.80000	0.0	d
19.4400	2.16000	-17.10000	-2.80000	0.0	d
20.5200	1.08000	-17.10000	-2.80000	0.0	d
21.6000	0.00000	-17.10000	-2.80000	0.0	d

d - Displacements include imported displacements.

Specific Building Damage Results - All Segments

Structure: Law Building | Sub-structure: Infill

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	1.8443	Sagging	0.086364	-0.10796	0.064177	0.0036545	0.0031802	202.59	1 (Very Slight)
	2	1.8443	2.4224	Hogging	0.033244	-0.043452	0.024769	0.0036545	0.0031802	1340.6	0 (Negligible)
	3	4.2667	1.0667	None	0.0	0.0	0.0	0.0	0.0	-	0 (Negligible)
	4	5.3333	5.3153	Hogging	0.0039458	0.0	0.0038756	0.0	-197.57E-6	14397.	0 (Negligible)
	5	10.649	1.0927	Sagging	0.0	36.630E-6	36.728E-6	-50.248E-6	-197.23E-6	1.9991E+6	0 (Negligible)
	6	11.741	3.9318	Hogging	0.0073329	0.042177	0.044373	-837.12E-6	-512.01E-6	7129.7	0 (Negligible)
	7	15.673	0.22695	None	0.0	0.083782	0.083782	-837.12E-6	-512.01E-6	37662.2	2 (Slight)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 16 Cheries | Sub-structure: West

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	0.88703	Hogging	0.0	-0.15762	0.031524	0.0015787	0.0020444	1014.5	0 (Negligible)
	2	0.88703	0.24630	None	0.0	-0.15762	0.031524	0.0024110	0.0024471	3653.6	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 16 Cheries | Sub-structure: South

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	15.700	None	0.0	0.0	0.0	0.0	0.0	-	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 16 Cheries | Sub-structure: East



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Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	0.88703	Hogging	0.0	-0.15762	0.031524	0.0015787	0.0020444	1014.5	0 (Negligible)
	2	0.88703	3.6463	Hogging	0.055295	-0.085403	0.041091	0.0024110	0.0024471	1017.2	0 (Negligible)
	3	4.5333	1.1333	None	0.0	0.0	0.0	0.0	0.0	-	0 (Negligible)
	4	5.6667	5.4783	Hogging	0.0046819	0.0	0.0046469	0.0	-197.40E-6	11845.	0 (Negligible)
	5	11.145	0.19946	Sagging	2.6301E-6	0.0	2.6107E-6	0.0	-197.00E-6	2.1895E+6	0 (Negligible)
	6	11.344	10.989	Hogging	0.0071686	0.066554	0.070230	-861.90E-6	-778.69E-6	8696.3	1 (Very Slight)
	7	22.333	0.51468	Hogging	747.85E-6	0.076458	0.076477	-814.97E-6	-811.55E-6	44796.2	2 (Slight)
	8	22.848	1.2945	Sagging	0.0045915	0.048839	0.049409	-670.21E-6	-811.55E-6	8565.2	0 (Negligible)
	9	24.142	4.1884	Sagging	0.061910	-0.19910	0.054421	0.0073996	-0.0015451	936.44	1 (Very Slight)
	10	28.331	4.5358	Hogging	0.0010230	0.0	0.0010178	0.0	0.0013762	1991.1	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 16 Chenies | Sub-structure: North

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0											

All settlements are less than the Settlement Trough Limit Sensitivity.
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 18 Chenies | Sub-structure: Retained Wall

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0											

All settlements are less than the Settlement Trough Limit Sensitivity.
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: Law Building | Sub-structure: North

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	12.600	None	0.0	0.0	0.0	0.0	0.0	-	0 (Negligible)
	2	12.600	2.8320	Sagging	0.019699	-0.0076890	0.017075	297.57E-6	0.0010338	3373.2	0 (Negligible)
	3	15.432	2.2106	Hogging	0.0096362	-0.033120	0.0088344	376.25E-6	0.0010338	6441.5	0 (Negligible)
	4	17.643	3.2574	Sagging	675.60E-6	-0.0078406	0.0016159	288.05E-6	342.82E-6	26426.	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: Law Building | Sub-structure: East

Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature	Damage Category
Calculations		[m]	[m]		[%]	[%]	[%]			[m]	
0.0	1	0.0	2.2779	Sagging	772.00E-6	0.021460	0.021583	-346.70E-6	377.62E-6	38013.	0 (Negligible)
	2	2.2779	4.1194	Hogging	0.0042649	0.019180	0.019942	-346.70E-6	377.62E-6	12549.	0 (Negligible)
	3	6.3973	1.3714	Sagging	31.871E-6	156.65E-6	161.90E-6	-25.969E-6	184.33E-6	381350.	0 (Negligible)
	4	7.7687	1.9513	Sagging	46.416E-6	0.0	46.313E-6	0.0	186.22E-6	18865.	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Specific Building Damage Results - Critical Values for All Segments within Each Sub-Structure

Structure: Law Building | Sub-structure: Infill

Vertical Offset from Line for Vertical Movement	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
Calculations	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.086364	-0.10796	0.0031802	3.3773	0.083782	0.0036545	0.0031802	1340.6	202.59	2 (Slight)

Structure: 16 Chenies | Sub-structure: West

Vertical Offset from Line for Vertical Movement	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
Calculations	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.0	-0.15762	0.0024471	5.0800	0.031524	0.0024110	0.0024471	1014.5	-0	(Negligible)

Structure: 16 Chenies | Sub-structure: South

Vertical Offset from Line for Vertical Movement	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
Calculations	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.0	0.0	0.0	2.5400	0.0	0.0	0.0	-	-0	(Negligible)

Structure: 16 Chenies | Sub-structure: East

Vertical Offset from Line for Vertical Movement	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement	Max Gradient of Vertical Displacement	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
Calculations	[%]	[%]		[mm]	[%]			[m]	[m]	
0.0	0.0	0.0	0.0	2.5400	0.0	0.0	0.0	-	-0	(Negligible)



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Movement Calculations

[m]	[%]	[%]	[mm]	[%]	[m]	[m]
0.0	0.061910	-0.19910	0.0024471	9.7000	0.076477	0.0073996

Structure: 16 Chenies | Sub-structure: North

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]	[mm]	[%]	[%]	[m]	[m]	[m]	[m]	

Structure: 18 Chenies | Sub-structure: Retained Wall

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]	[mm]	[%]	[%]	[m]	[m]	[m]	[m]	

Structure: Law Building | Sub-structure: North

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]	[mm]	[%]	[%]	[m]	[m]	[m]	[m]	
0.0	0.019699	-0.033120	0.0010338	5.2962	0.017075	376.25E-6	0.0010338	6441.5	3373.2	0 (Negligible)

Structure: Law Building | Sub-structure: East

Vertical Offset from Line for Vertical Movement Calculations	Deflection Ratio	Average Horizontal Strain	Max Slope	Max Settlement	Max Tensile Strain	Max Gradient of Horizontal Displacement Curve	Max Gradient of Vertical Displacement Curve	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
[m]	[%]	[%]	[mm]	[%]	[%]	[m]	[m]	[m]	[m]	
0.0	0.0042649	0.021460	377.62E-6	2.6146	0.021583	-346.70E-6	377.62E-6	12549.	18865.	0 (Negligible)

Specific Building Damage Results - Critical Segments within Each Structure

Structure Name	Parameter	Critical Sub-Structure	Critical Segment	Start	End	Curvature	Max Slope	Max Settlement	Max Tensile Strain	Min Radius of Curvature (Hogging)	Min Radius of Curvature (Sagging)	Damage Category
Law Building	Max Slope	Infill	1	0.0	1.8443	Sagging	0.0031802	3.3773	0.064177	-	202.59	1 (Very Slight)
Law Building	Max Settlement	North	1	0.0	12.600	Sagging	0.0	5.2962	0.0	-	-	0 (Negligible)
Law Building	Max Tensile Strain	Infill	7	15.673	15.900	Sagging	512.01E-6	2.1635	0.083782	-	37662.	2 (Slight)
Law Building	Min Radius of Curvature (Hogging)	Infill	2	1.8443	4.2667	Hogging	0.0031802	0.91597	0.024769	1340.6	-	0 (Negligible)
Law Building	Min Radius of Curvature (Sagging)	Infill	1	0.0	1.8443	Sagging	0.0031802	3.3773	0.064177	-	202.59	1 (Very Slight)
16 Chenies	Max Slope	West	2	0.88703	1.1333	Sagging	0.0024471	3.2694	0.031524	-	3653.6	0 (Negligible)
16 Chenies	Max Settlement	East	9	24.142	28.331	Sagging	0.0015451	9.7000	0.054421	-	936.44	1 (Very Slight)
16 Chenies	Max Tensile Strain	East	7	22.333	22.848	Hogging	811.55E-6	6.5626	0.076477	44796.	-	2 (Slight)
16 Chenies	Min Radius of Curvature (Hogging)	West	1	0.0	0.88703	Hogging	0.0020444	5.0800	0.031524	1014.5	-	0 (Negligible)
16 Chenies	Min Radius of Curvature (Sagging)	East	9	24.142	28.331	Sagging	0.0015451	9.7000	0.054421	-	936.44	1 (Very Slight)
18 Chenies	All settlements are less than the Settlement Trough Limit Sensitivity.											
18 Chenies	All settlements are less than the Settlement Trough Limit Sensitivity.											
18 Chenies	All settlements are less than the Settlement Trough Limit Sensitivity.											
18 Chenies	All settlements are less than the Settlement Trough Limit Sensitivity.											

Specific Building Damage Results - All Combined Segments

Structure: Law Building | Sub-structure: Infill

Vertical Offset from Line for Vertical Movement Calculations	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
[m]	[m]	[m]	[m]	[%]	[%]	[%]	[%]	
0.0	1	0.0	15.900	Hogging	0.017948	-0.0075142	0.013084	0 (Negligible)

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 16 Chenies | Sub-structure: West

Vertical Offset from Line for Vertical Movement Calculations	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
[m]	[m]	[m]	[m]	[%]	[%]	[%]	[%]	
No structures have segments combined.								

Structure: 16 Chenies | Sub-structure: South

Vertical Offset from Line for Vertical Movement Calculations	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
[m]	[m]	[m]	[m]	[%]	[%]	[%]	[%]	
No structures have segments combined.								

Structure: 16 Chenies | Sub-structure: East

Vertical Offset from Line for Vertical Movement Calculations	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
[m]	[m]	[m]	[m]	[%]	[%]	[%]	[%]	
0.0	1	0.0	32.867	Hogging	0.024687	-0.013729	0.016975	0 (Negligible)



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Vertical Offset from Line for Vertical	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
----------------------------------------	------------------	-------	--------	-----------	------------------	---------------------------	--------------------	-----------------

Tensile horizontal strains are +ve, compressive horizontal strains are -ve.

Structure: 16 Cheries | Sub-structure: North

Vertical Offset from Line for Vertical Movement	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
-------------------------------------------------	------------------	-------	--------	-----------	------------------	---------------------------	--------------------	-----------------

Calculations [m] [m] [%] [%] [%]
 No structures have segments combined.

Structure: 18 Cheries | Sub-structure: Retained Wall

Vertical Offset from Line for Vertical Movement	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
-------------------------------------------------	------------------	-------	--------	-----------	------------------	---------------------------	--------------------	-----------------

Calculations [m] [m] [%] [%] [%]
 No structures have segments combined.

Structure: Law Building | Sub-structure: North

Vertical Offset from Line for Vertical Movement	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
-------------------------------------------------	------------------	-------	--------	-----------	------------------	---------------------------	--------------------	-----------------

Calculations [m] [m] [%] [%] [%]
 No structures have segments combined.

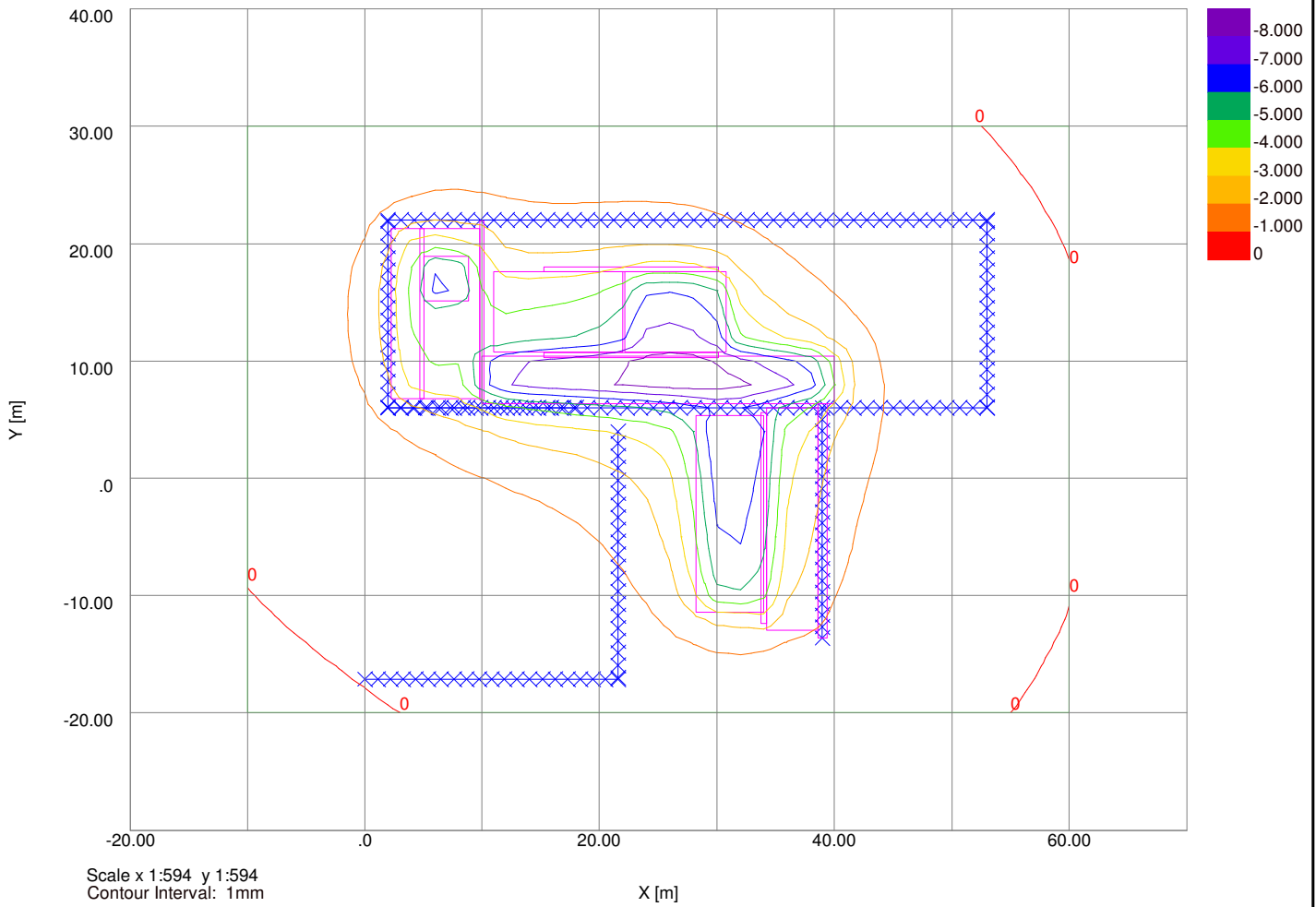
Structure: Law Building | Sub-structure: East

Vertical Offset from Line for Vertical Movement	Combined Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max Tensile Strain	Damage Category
-------------------------------------------------	------------------	-------	--------	-----------	------------------	---------------------------	--------------------	-----------------

Calculations [m] [m] [%] [%] [%]
 No structures have segments combined.

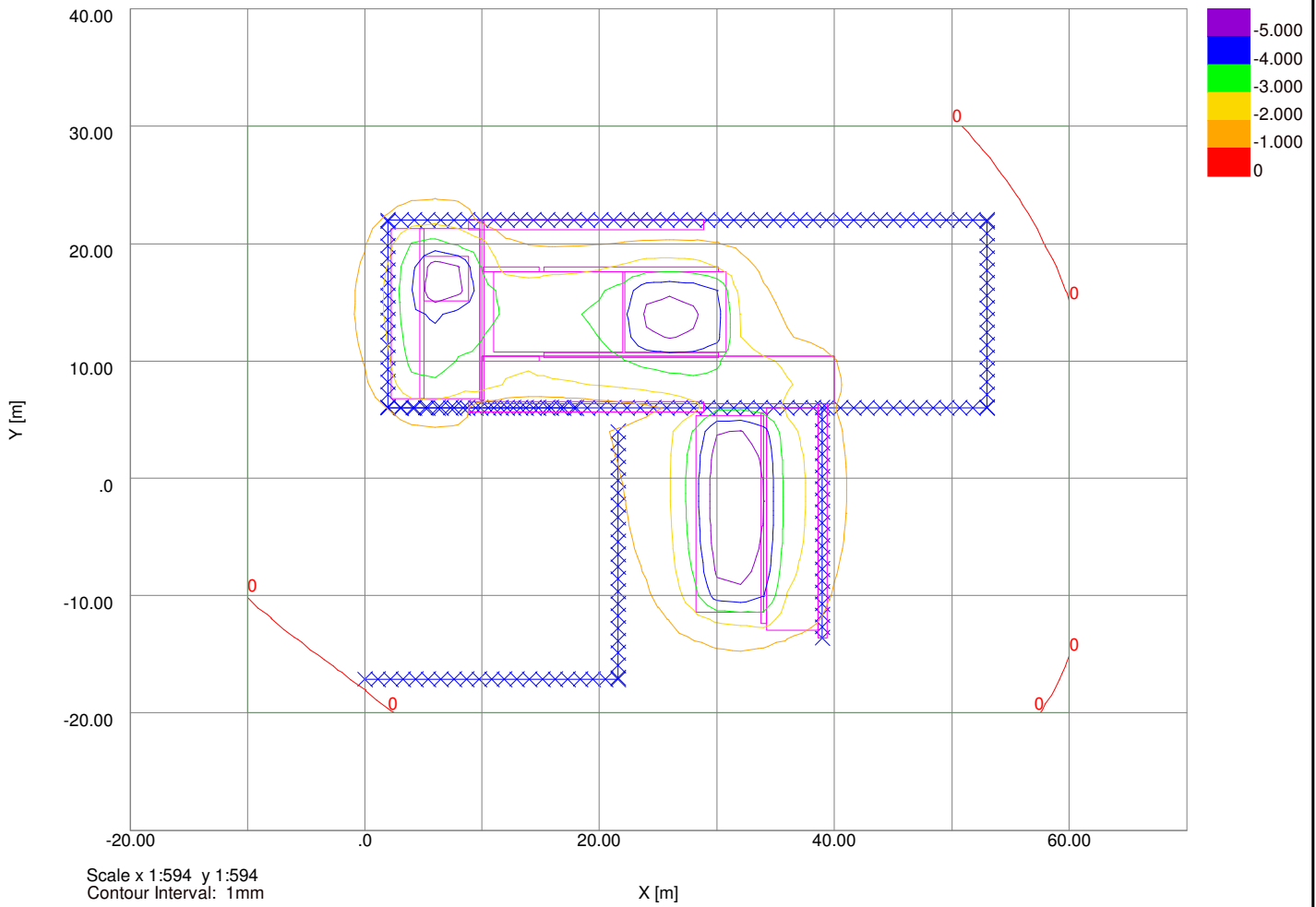
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Settlement Contours : Grid 1 at -2.8000m



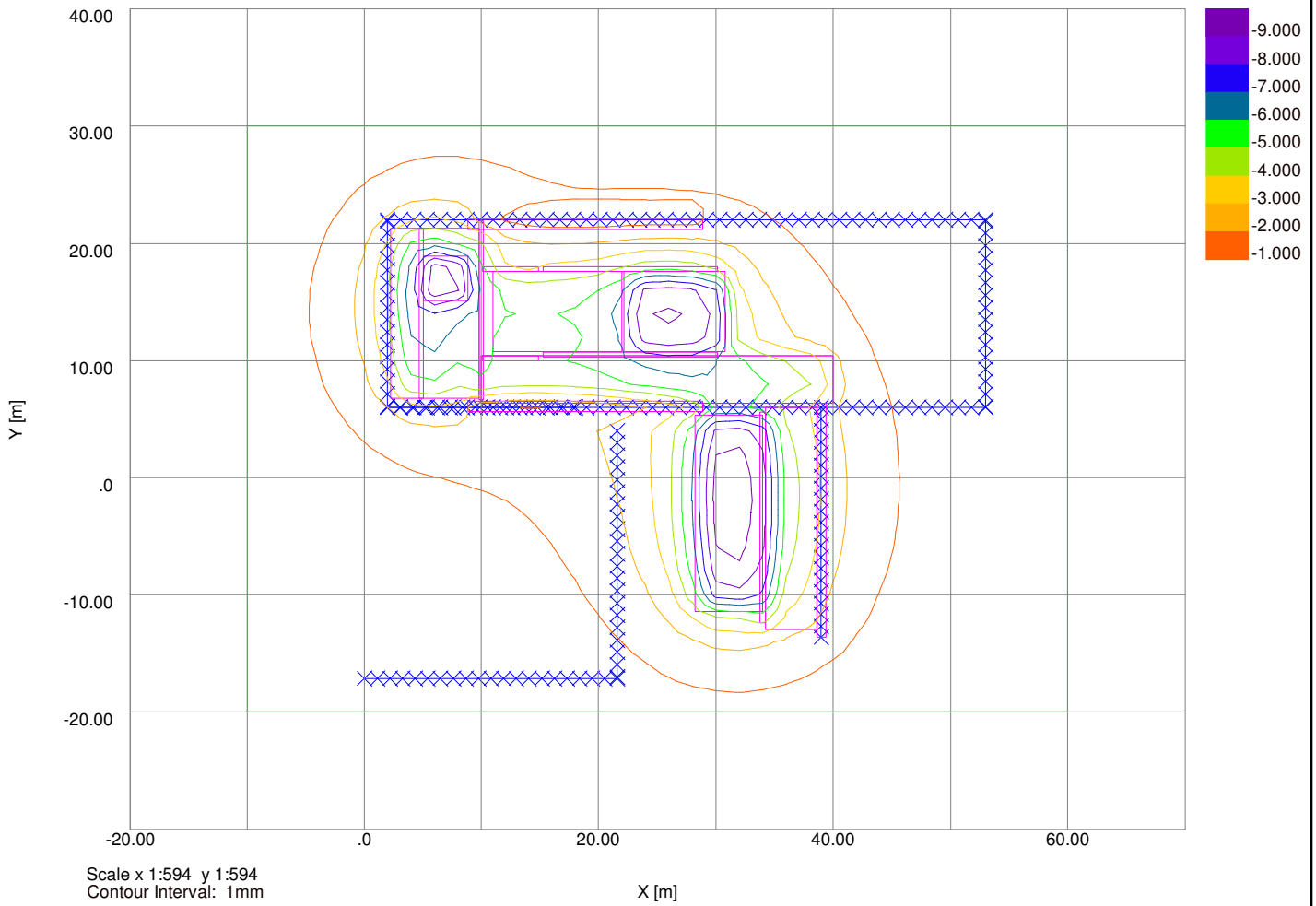
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Drg. Ref.		
Made by MC	Date	Checked

Settlement Contours : Grid 1 at -2.8000m



Job No.	Sheet No.	Rev.
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Drg. Ref.		
Made by MC	Date	Checked

Settlement Contours : Grid 1 at -2.8000m



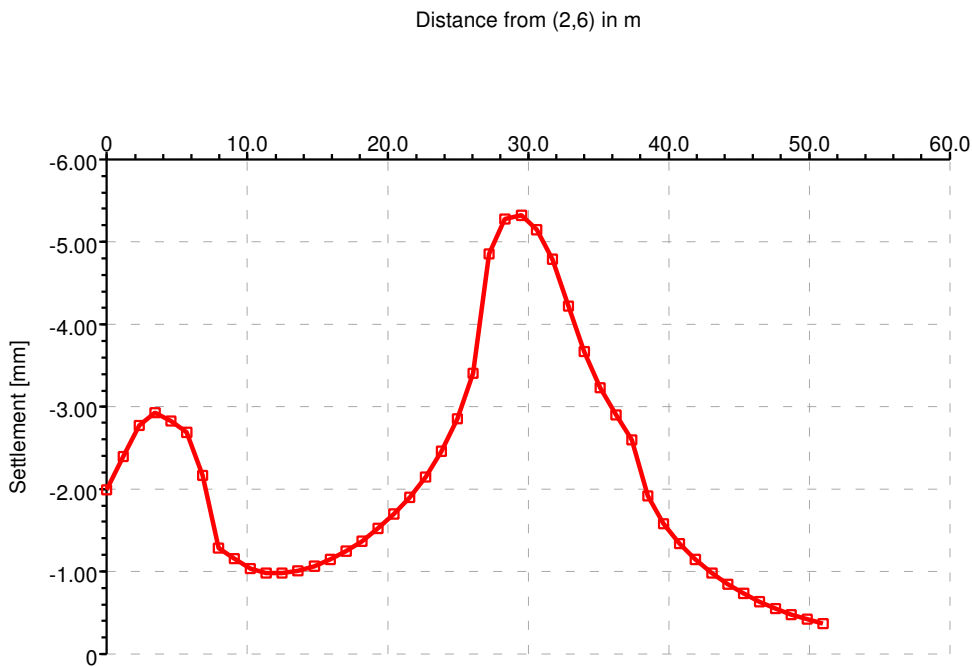
Scale x 1:594 y 1:594
Contour Interval: 1mm

X [m]

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Displacement for 16 Cheries Est

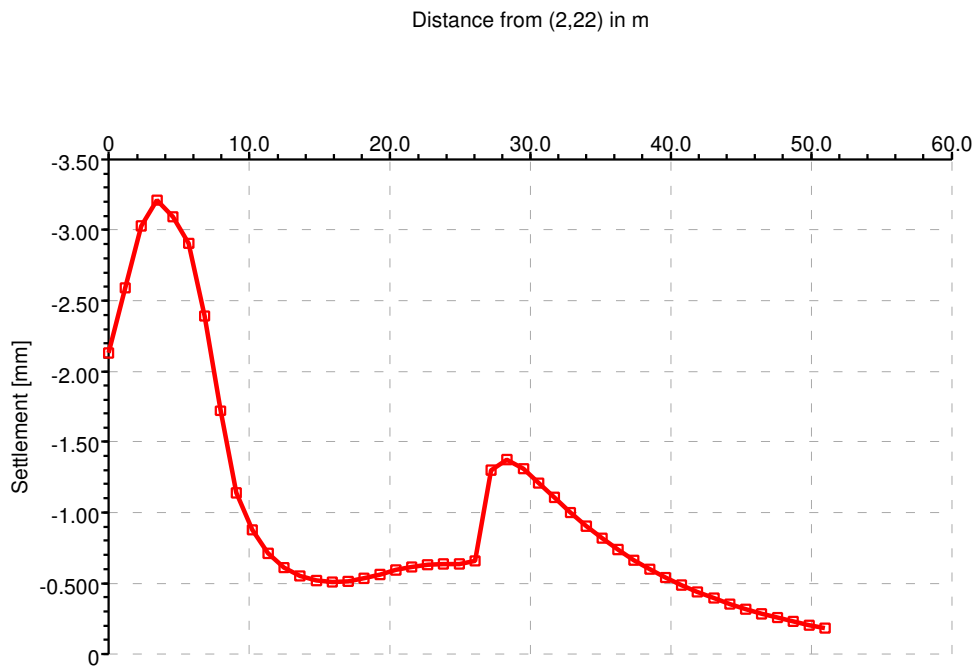
—■— Line Displacement



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J15215		
Drg. Ref.		
Made by MC	Date	Checked

Displacement for 16 Cheries Wst

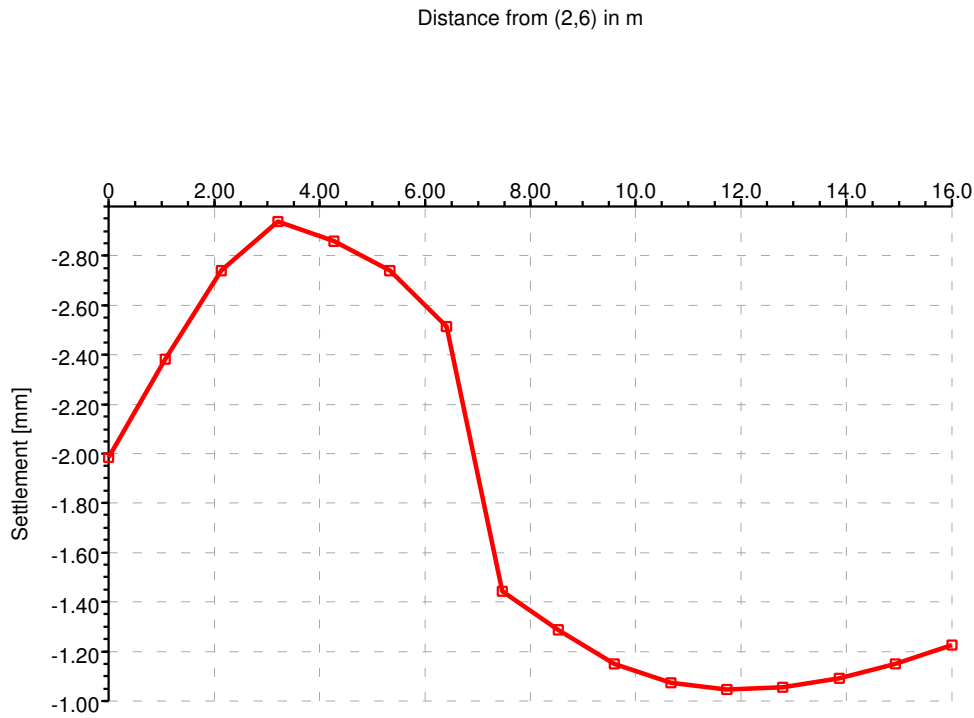
—■— Line Displacement



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Made by MC	Date	Checked

Displacement for Law Bdg Infill

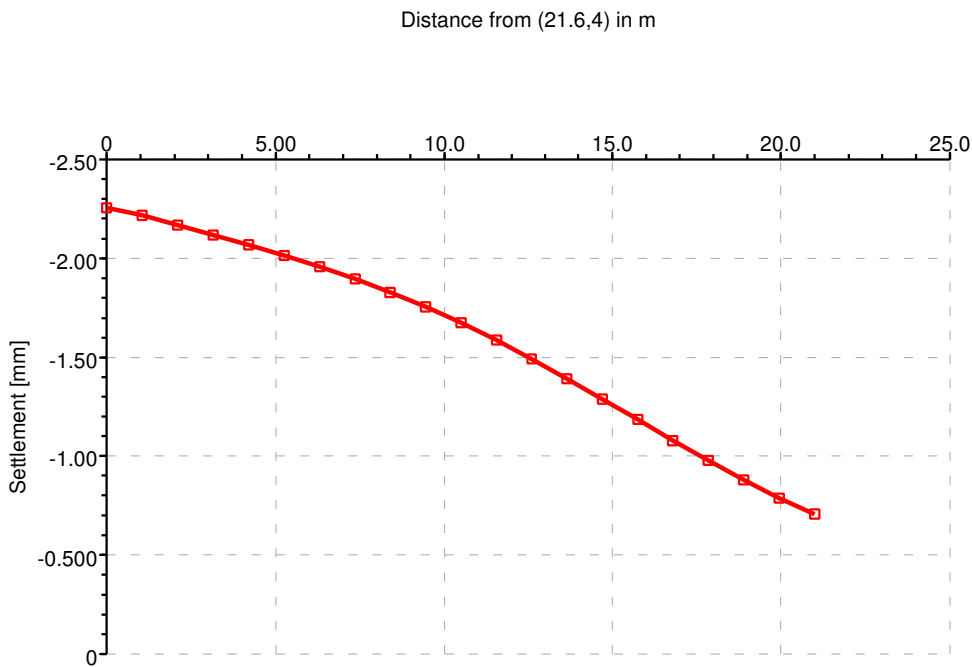
—■— Line Displacement



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Dr. Ref.		
Made by	Date	Checked
MC		

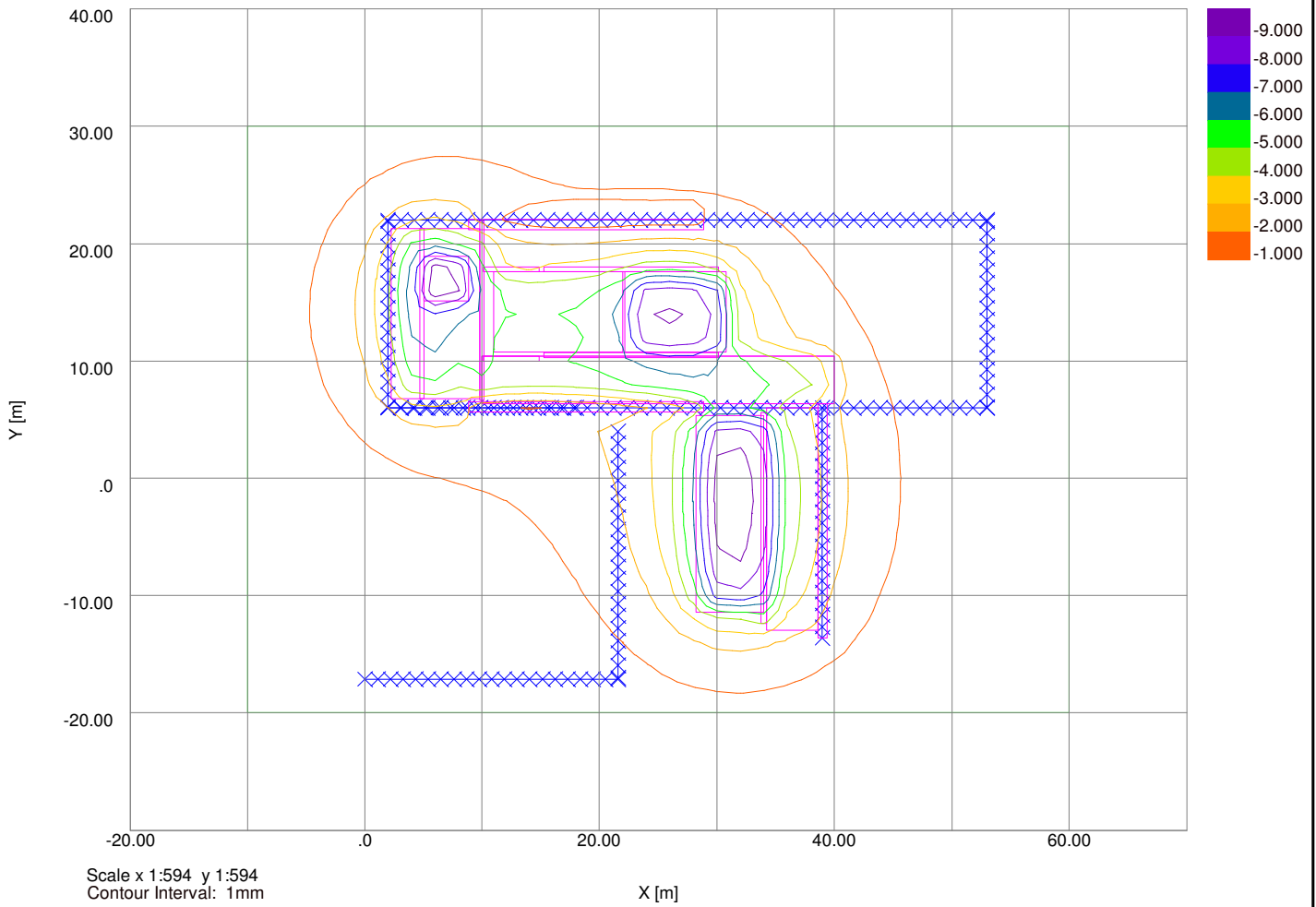
Displacement for Law Bdg Nth

—■— Line Displacement



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Made by MC	Date	Checked

Settlement Contours : Grid 1 at -2.8000m



BASEMENT PLAN AS PROPOSED
STRUCTURAL ALTERATIONS TO THEATRE

1:100 @ A3

NO 16-CHELVES STREET
 RADA - "THE RICHARD ATTENBOROUGH
 THEATRE REDEVELOPMENT"





EXISTING LOADS
 DL 72.5 kN/m
 LL 24.5 kN/m

PROPOSED LOADS
 DL 92 kN/m
 LL 37 kN/m

900mm WIDTHS
 OF MASS CONCRETE
 UNDERPIPS

700mm RC GROUND SLAB
 (OVER) - PILED

KEY LEGENDS:

- (-) DENOTES UNLOADING
-  RC STRUCTURE
-  MASS CONCRETE STRUCTURE
-  PILE FOUNDATION UNDER
-  MASS CONCRETE UNDERPIN WIDTHS

- EXCAVATION DEPTH: 2.760m
 - EXCAVATION DEPTH: 3.650m
 - EXCAVATION DEPTH: 1.250m

EXISTING LOADS: DL=72.5 kN/m
 LL=24.5 kN/m

PROPOSED LOADS: DL 92 kN/m
 LL 37 kN/m

DL=41.5 kN/m²
 LL=12.5 kN/m²

NOTE ALL UNDERPIPS TO REACH
 DEPTH OF LYCII BLUE GRAVEL
 FORMATION (7.0m ON SITE)
 (APPROX @ 22.5m OD LEVEL)

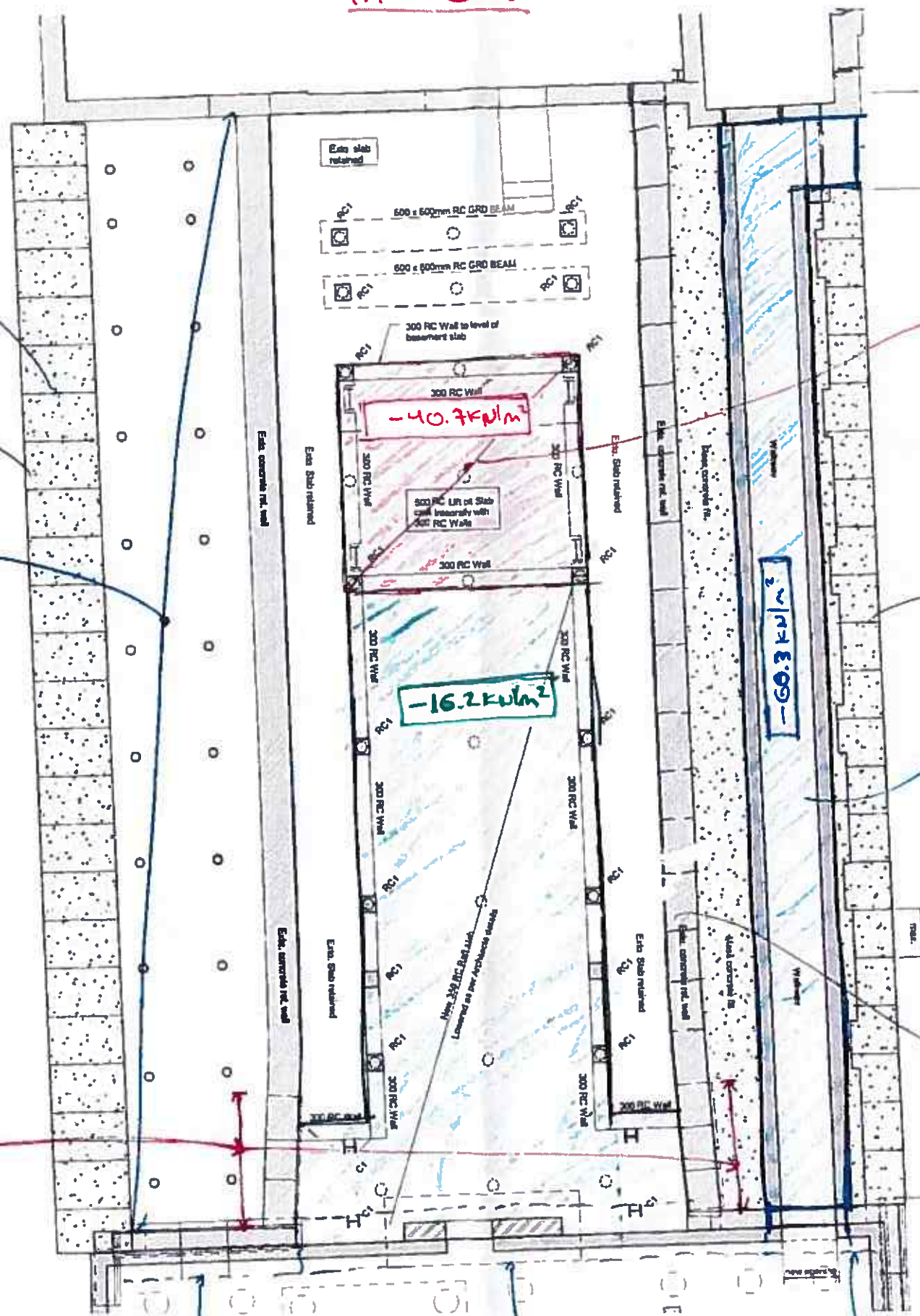
EXIST RETAINING WALLS WILL
 ONLY CARRY SELFWEIGHT

EXIST RETAINING
 WALLS UNDERPINNED
 LOCALLY FOR NEW
 750 RC RAFT SLAB

900mm WIDTHS
 OF MASS CONCRETE
 UNDERPIPS

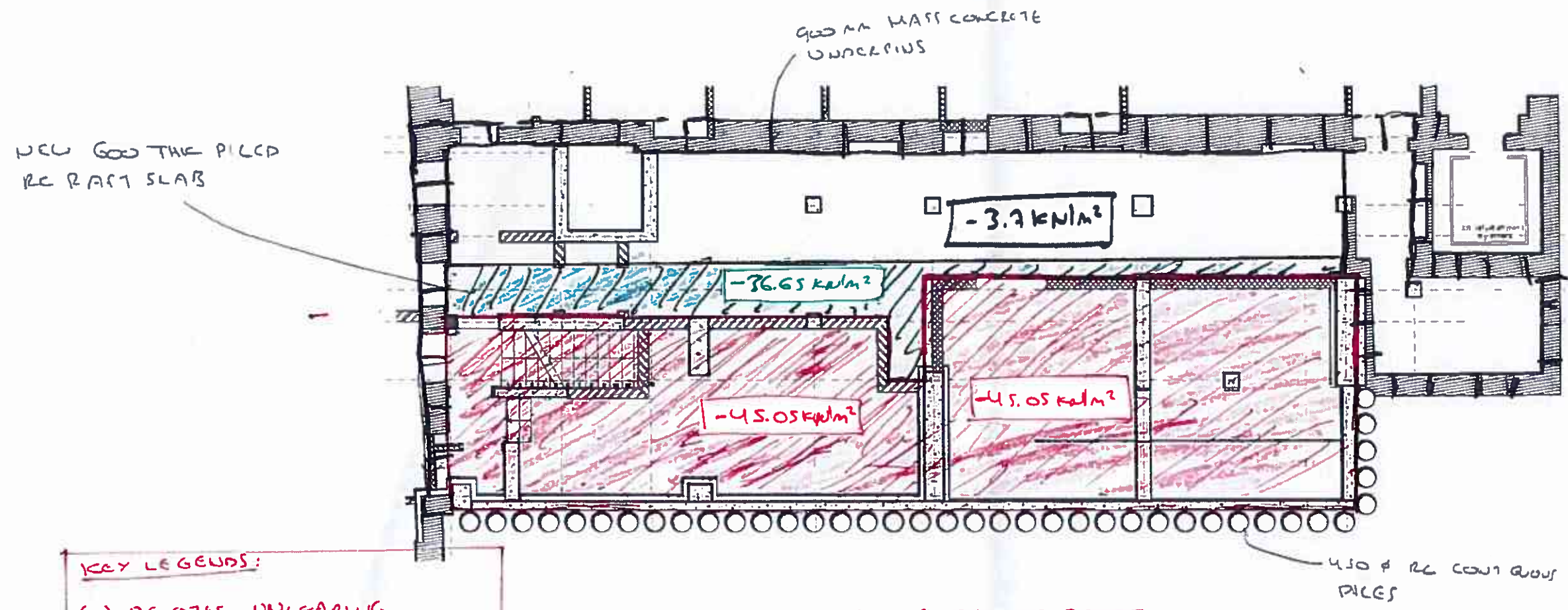
NEW FOOTING -
 WIDTH TO MATCH
 EXISTING FOOTINGS

900mm WIDTHS OF
 MASS CONCRETE
 UNDERPIPS



No 10 CHEMIST STREET
 RADA - 'THE RICHARD ATTENBOROUGH'
 THEATRE REDEVELOPMENT

NOTE ALL UNDERPINS TO REACH
 DEPTH OF LYXCH HILL GRAVEL
 FORMATION TBC ON SITE
 (APPROX OD LEVEL 22.8m)



KEY LEGENDS:
 (-) DELOTT'S UNLOADING
 [Dotted Box] NEW RC CONCRETE STRUCTURE
 [Hatched Box] EXISTING W/AH STRUCTURE

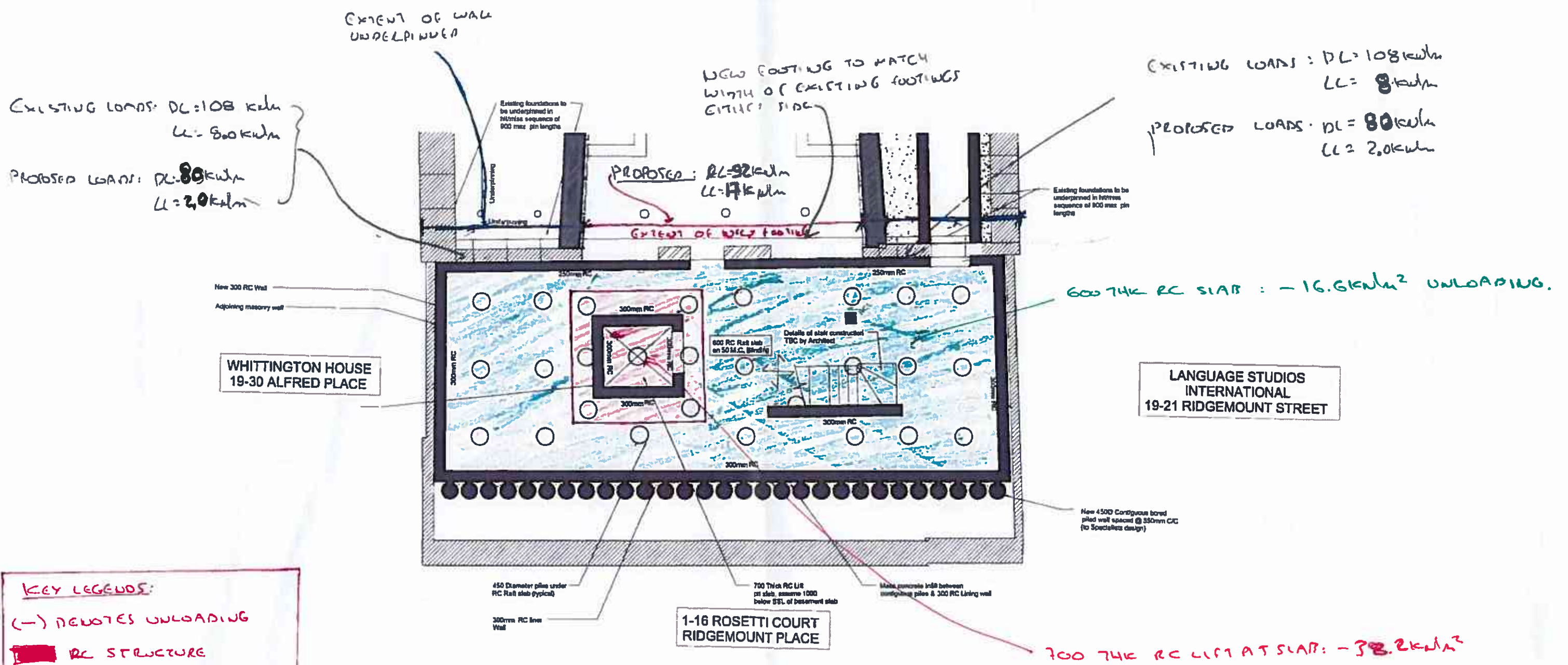
- EXCAVATION DEPTH: 3.33m
 - EXCAVATION DEPTH: 2.82m
 - EXCAVATION DEPTH: 0.27m

No 18 CHEMIST STREET
 REAR EXTENSION
 1:100 @ A3

UNLOADING - UNFACTORED

BASEMENT PLAN AS PROPOSED

No 16 CHEVIES STREET
RADA - 'THE RICHER ATTENTION' THEATRE REDEVELOPMENT



EXISTING LOADS: DL=108 kN/m²
LL=80 kN/m²
PROPOSED LOADS: DL=80 kN/m²
LL=20 kN/m²

EXISTING LOADS: DL=108 kN/m²
LL=80 kN/m²
PROPOSED LOADS: DL=80 kN/m²
LL=20 kN/m²

KEY LEGENDS:
(-) DENOTES UNLOADING
[Solid Box] RC STRUCTURE
[Hatched Box] EXISTING MASONRY
[Dotted Box] NEW MASONRY

- EXCAVATION DEPTH: 2.87m
- EXCAVATION DEPTH: 1.57m

BASEMENT PLAN AS PROPOSED
STRUCTURAL ALTERATIONS TO REAL-
NEW LIBRARY & OFFICE BUILDING
1:100 @ A3

Geotechnical & Environmental Associates (GEA) is an engineer-led and client-focused independent specialist providing a complete range of geotechnical and contaminated land investigation, analytical and consultancy services to the property and construction industries.

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