7 ENERGY – "BE GREEN"

A renewable energy feasibility exercise has been carried out in order to determine the feasible renewable energy option(s).

The study is summarised in Table 14 below. The viable technology option (solar thermal) is presented below.

SOLAR THERMAL

Technical Overview

Solar thermal water heating is a well-established renewable energy system. Solar hot water can be successfully applied to a range of domestic and non-domestic building types which have high demands for hot water.

There are some maintenance requirements although in general the quality of the installations has been strengthened in recent years by advancements in manufacturing and installer training and accreditation as supported by the Microgeneration Certification Scheme (MCS).

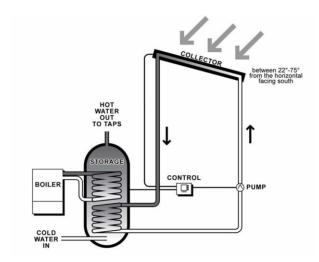


Figure 10: Solar thermal schematic

Applicability to the Proposed Scheme

Solar thermal is applicable to the proposed scheme. As a large house it has a significant hot water demand. Furthermore, the small flat roof area provides a possible location for the installation.



Figure 11: Example solar thermal "flat plate" collector

TECHNOLOGY FEASIBILITY STUDY SUMMARY

The overall summary of the feasibility exercise is presented below.

Technology		Assessment / Viability
Wind Power	Wind turbine installed on the roof of the development.	Due to the neighbouring residential areas, the high cost per kW for smaller building-mounted turbines and the impacts in terms of visual noise and shadow flicker, wind turbines are not considered a viable technology for the development. CONCLUSION: NOT CONSIDERED FEASIBLE
Ground Source Heat Pumps	Open or closed loop GSHP system requiring extraction of ground water and / or deep boreholes.	Minimal maintenance and no external visual and low noise impact. However, there are space restrictions and significant investment is required especially for schemes employing bore holes.
		CONCLUSION: NOT CONSIDERED FEASIBLE
Air Source Heat Pumps	Electric powered external plant serving each unit	The carbon offsetting potential for an ASHP is very low therefore is not recommended.
	providing heating and cooling	CONCLUSION: NOT CONSIDERED FEASIBLE
Solar Thermal Collectors	Roof-mounted solar thermal panels providing hot water heating	The small flat roof area has good potential for a domestic solar thermal energy collection (4m²). Solar hot water collectors would provide a significant proportion of domestic hot water demand of the development (~50%).
		CONCLUSION: CONSIDERED FEASIBLE
Solar Photovoltaic Panels	Roof mounted Photovoltaic panels (PV) provide electricity directly to the development, exporting any surplus production to the grid.	The flat roof areas is too small for PV. It is only capable of housing 2 panels which is not enough for a viable system. The SE facing pitch roof is heavily overshadowed. The NW pitch roof will not receive a high amount of solar irradiation and is also not recommended. Therefore solar PV is not considered feasible for this project.
		CONCLUSION: NOT CONSIDERED FEASIBLE
Biomass Heating	Biomass-fired community heating system.	Biomass heating is an established technology but has high maintenance requirements, fuel storage and delivery issues and is a source of increase in pollution, notably particulates (PM10), SO ₂ and NO _X emissions.
		CONCLUSION: NOT CONSIDERED FEASIBLE

Table 13: Summary of Low and Zero Carbon Study Analysis Results

"Be Green" Total Carbon Emissions

The CO₂ emission associated with regulated energy consumption are given below.

Ref	Bedrooms	DER (kg.CO ₂ /m²/yr.)
House	6 bed	10.14
Total "Be Gr	een"	10.14

Table 14: Be Green Regulated Carbon Emissions

The CO_2 emission associated with unregulated energy consumption are the same as calculated for the baseline scenario. Therefore, the total "Be Green" CO_2 emissions associated with regulated and unregulated energy consumption is summarised below.

Ref	Bedrooms	Regulated Carbon Emissions (kg.CO ₂ /yr.)	Unregulated Carbon Emissions (kg.CO₂/yr.)	Total Carbon Emissions (kg.CO ₂ /yr.)
House	6 bed	5,048	6,656	11,704
Total "Be Gr	een" Emissions	5,048	6,656	11,704

Table 15: Be Green Total Carbon Emissions

8 SUMMARY

The predicted total annual regulated CO₂ emissions of the proposed development, following the introduction of energy efficiency measures, passive and active design (Be Lean) and renewable energy systems (Be Green), is summarised below.

Carbon Emissions Summary (Be Green)

Target	Regulated Carbon Emissions (kg.CO ₂ /yr.)	Percentage Improvement	Total Carbon Emissions (kg.CO ₂ /yr.)	Percentage Improvement (regulated & unregulated)
Baseline Emissions: Part L 2013	6,241	N/A	12,897	N/A
Be Lean	5,310	14.9%	11,965	7.2%
Be Clean	5,310	14.9%	11,965	7.2%
Be Green	5,048	19.1%	11,704	9.3%

Table 16: Summary of "Be Green" Carbon Emissions and Baseline Comparison



Figure 12: Summary of CO2 savings.

Sustainability Credentials

The scheme will create a large modern home based on a highly efficient, air tight thermal envelope, making use of a central glazed atrium to provide excellent natural ventilation and night cooling as well as daylight access into the core of the building.

The scheme will feature solar thermal collectors and water saving devices. The site has excellent links to low energy public transportation.

APPENDIX A: OVERHEATING CHECKLISTS

Section 1 - Site features affecting vuln	erability to overheating	Yes or No
Site location	Urban – within central London or in a high-density conurbation	Yes
	Peri-urban – on the suburban fringes of London	No
Air quality and/or Noise sensitivity –	Busy roads / A roads	No
are any of the following in the vicinity of buildings?	Railways / Overground / DLR	No
	Airport / Flight path	No
	Industrial uses / waste facility	No
Proposed building use	Will any buildings be occupied by vulnerable people (e.g. elderly, disabled, young children)?	
	Are residents likely to be at home during the day (e.g. students)?	Yes
Dwelling aspect	Are there any single aspect units?	No
Glazing ratio	Is the glazing ratio (glazing: internal floor area) greater than 25%?	No
	If yes, is this to allow acceptable levels of daylighting?	NA
	Single storey ground floor units	No
Security - Are there any security issues	Vulnerable areas identified by the Police Architectural Liaison Officer	No
that could limit opening of windows for ventilation?	Other	No

Table A1: Domestic Overheating Checklist Section 1 (GLA Guidance on preparing Overheating Checklist)

Section 2 - Design fea	atures implemented to mitigate overheating risks	Response
Landscaping	Will deciduous trees be provided for summer shading (to windows and pedestrian routes)?	Yes
	Will green roofs be provided?	Yes (see Figure 5)
	Will other green or blue infrastructure be provided around buildings for evaporative cooling?	Landscaping
Materials	Have high albedo (light colour) materials been specified?	TBC
Dwelling aspect	% of total units that are single aspect	0%
	% single aspect with N / NE / NW orientation	0%
	% single aspect with S / SE / SW orientation	0%
	% single aspect with W orientation	0%
Glazing ratio -	N . NE . NW	TBC
(glazing; internal floor area)	E	TBC
	S / SE / SW	TBC
	W	TBC
Daylighting	What is the average daylight factor range?	TBC
Window opening	Window opening	All windows are openable
	What is the average percentage of openable area for the windows?	TBC
Window opening -	Fully openable	Yes
What is the extent of the opening?	Limited (e.g. for security, safety, wind loading reasons)	Yes low level "night cooling" openings are secure.
Security	Where there are security issues (e.g. ground floor flats) has an alternative night time natural ventilation method been provided (e.g. ventilation grates)?	NA
Shading	Is there any external shading?	No
	Is there any internal shading?	Yes internal blinds
Glazing specification	Is there any solar control glazing	see G-value specification in main body of report
Ventilation - What is the ventilation	Natural – background	Yes
strategy?	Natural – purge	Yes
	Mechanical – background (e.g. MVHR)	Yes MHVR
	Mechanical – purge	Yes the option for mechanical ventilation boost is possible and a heat recovery bypass is specified.
	What is the average design air change rate	4, Air changes per hour during hot weather
Heating system	Is communal heating present?	No
	What is the flow/return temperature?	N/A
	Have horizontal pipe runs been minimised?	N/A
	Do the specifications include insulation levels in line with the London Heat Network Manual	N/A

Table A2: Domestic Overheating Checklist Section 2 (GLA Guidance on preparing Overheating Checklist)

APPENDIX B: SAP CALCULATION (BE GREEN) WORKSHEET

DER WorkSheet: New dwelling design stage

) i	User Details:					
Assessor Name: Software Name:	Stroma FSAP 2012	Softv	na Num vare Ve	rsion:	Versio	on: 1.0.4.9	
Address :	30, Glenilla Road, LONDON,	perty Addres NW3 4AN	s: Glenilla	a Road			
Overall dwelling dimensions		INVO TAIN					
		Area(m²)		Av. Height	(m)	Volume(m³	·)
Basement		161.8	(1a) x	2.7	(2a) =	436.86	(3a)
Ground floor		135.55	(1b) x	2.7	(2b) =	365.99	(3b)
First floor		96.89	(1c) x	2.7	(2c) =	261.6	(3c)
Second floor		58.8	(1d) x	2.7	(2d) =	158.76	(3d)
Third floor		44.57	(1e) x	2.7	(2e) =	120.34	(3e)
Total floor area TFA = (1a)	+(1b)+(1c)+(1d)+(1e)+(1n)	497.61	(4)				
Dwelling volume		N-	(3a)+(3b)+(3c)+(3d)+(3e)+(3n) =	1343.55	(5)
2. Ventilation rate:							
	main secondary heating heating	other		total		m³ per hou	ır
Number of chimneys	0 + 0	+ 0	= [0	x 40 =	0	(6a)
Number of open flues	0 + 0	+ 0	=	0	x 20 =	0	(6b)
Number of intermittent fans				0	x 10 =	0	(7a)
Number of passive vents				0	x 10 =	0	(7b)
Number of flueless gas fire	s	7		0	x 40 =	0	(7c)
					Air ch	anges per ho	our
Infiltration due to chimneys	, flues and fans = (6a)+(6b)+(7a))+(7b)+(7c) =	Γ	0	÷ (5) =	0	(8)
If a pressurisation test has bee	n carried out or is intended, proceed t	to (17), otherwise	e continue fr	om (9) to (16)			2000
Number of storeys in the	dwelling (ns)					0	(9)
Additional infiltration					[(9)-1]x0.1 =	0	(10)
	5 for steel or timber frame or 0		- A	ruction		0	(11)
if both types of wall are pres deducting areas of opening.	sent, use the value corresponding to these; if equal user 0.35	he greater wall a	rea (after				
	or, enter 0.2 (unsealed) or 0.1	(sealed), else	e enter 0		03	0	(12)
If no draught lobby, ente	r 0.05, else enter 0					0	(13)
Percentage of windows	and doors draught stripped				× ×	0	(14)
Window infiltration		0.25 - [0	.2 x (14) + 1	00] =	Ĭ	0	(15)
Infiltration rate		(8) + (10	0) + (11) + (1	12) + (13) + (15)	E.	0	(16)
Air permeability value, q	50, expressed in cubic metres	per hour per	square m	etre of envel	ope area	4	(17)
and the second of the second o	value, then (18) = [(17) + 20]+(8),					0.2	(18)
	f a pressurisation test has been done	or a degree air p	ermeability	is being used	· ·		-
Number of sides sheltered Shelter factor		(20) = 1	- [0.075 x (1	19)1 =		2	(19)
Infiltration rate incorporating	a shalter factor	20.000 m	8) x (20) =	-41		0.85	(20)
audi rate incorporatin	g chanci idoloi	\-·/ (·				0.17	(21)

Infiltration rate	modified for	or monthly	wina spee	d								
Jan	Feb	Mar A	pr May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Monthly avera	ge wind sp	eed from	Γable 7									
(22)m= 5.1	5	4.9 4.	4 4.3	3.8	3.8	3.7	4	4.3	4.5	4.7		
\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	20 \ (00											
Wind Factor (2 (22a)m= 1.27	T 1	2)m ÷ 4 1.23 1.	1 1.08	0.95	0.95	0.92	1	1.08	1.12	1.18		
(224)11-1.27	1.20	1.20	1.00	0.55	0.55	0.52	s	1.00	1.12	1.10		
Adjusted infiltr	The second of th		NO DESCRIPTIONS			(21a) x	(22a)m			r		
0.22 Calculate effe		0.21 0.		0.16	0.16	0.16	0.17	0.18	0.19	0.2		
If mechanic			тог тте арри	cable cas	.6					1	0.5	(23a)
If exhaust air h	eat pump usin	g Appendix	N, (23b) = (23	a) × Fmv (e	quation (N	5)) , other	wise (23b)) = (23a)		Ī	0.5	(23b)
If balanced with	n heat recover	y: efficiency	in % allowing	for in-use fa	ctor (from	Table 4h)	=			Ī	74.8	(23c)
a) If balance	ed mechani	cal ventila	tion with he	at recove	ry (MVH	IR) (24a)m = (22	2b)m + (2	23b) × [1	1 – (23c)	÷ 100]	
(24a)m= 0.34	0.34	0.33 0.3	31 0.31	0.29	0.29	0.28	0.3	0.31	0.32	0.33		(24a)
b) If balance	ed mechani	cal ventila	tion without	heat rec	overy (M	1 V) (24b)m = (22	2b)m + (2	23b)			
(24b)m= 0	0	0 (0	0	0	0	0	0	0	0		(24b)
c) If whole h	1720-100-100-100-100-100-100-100-100-100-1	A STATE OF THE STA	Activities to the second		and the second second	A SALES OF THE SAL		- 1001				
	$n < 0.5 \times (2)$	3b), then	(24c) = (23)	b); otherw	ise (24c	e) = (22b	0) m + 0.	100	0	0		(24c)
								0	U	0		(240)
d) If natural if (22b)r			(22b)m oth	The second secon	The state of the s	17	The second second	0.5]				
(24d)m= 0	0	0 (0	0	0	0	0	0	0	0		(24d)
Effective air	change rat	e - enter	24a) or (24	b) or (24c) or (24c	d) in box	(25)					
(25)m= 0.34	0.34	0.33	0.31	0.29	0.29	0.28	0.3	0.31	0.32	0.33		(25)
3. Heat losse	s and heat	loss para	meter:									
ELEMENT	Gross		enings	Net Are	22							
	area (m	²)	m2		,u	U-valu	ie	AXU		k-value		AXk
Doors Type 1			m²	A ,m) ²	U-valu W/m2	K	(W/I	<)	k-value kJ/m²·k		kJ/K
D T 0			m	2.1		W/m2 1	к] = [(W/F 2.1	<) 			kJ/K (26)
Doors Type 2			III.	2.1	1 ²	W/m2 1	K = [= [2.1 2.1	<) 			kJ/K (26) (26)
Windows Type			m	2.1 2.1 5.13	1 ²	W/m2 1 1 [1/(1.4)+	K = [2.1 2.1 6.8	<) 			kJ/K (26) (26) (27)
Windows Type	e 2		m-	2.1 2.1 5.13 9.45	12 x [W/m2 1 1 [1/(1.4)+ [1/(1.4)+	K = [2.1 2.1 6.8 12.53	<) 			kJ/K (26) (26) (27) (27)
Windows Type Windows Type Windows Type	e 2 e 3		m	2.1 2.1 5.13	x [x1/[x1/[W/m2 1 1 [1/(1.4)+ [1/(1.4)+		2.1 2.1 6.8	<) 			(26) (26) (27) (27) (27)
Windows Type Windows Type Windows Type Windows Type	e 2 e 3 e 4		HI-	2.1 2.1 5.13 9.45	x x x x x x x x x x	W/m2 1 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+		2.1 2.1 6.8 12.53	<) 			(26) (26) (27) (27) (27) (27)
Windows Type Windows Type Windows Type Windows Type Windows Type	e 2 e 3 e 4 e 5		III-	2.1 2.1 5.13 9.45 2.7 3.51 4.2	x x x x x x x x x x	W/m2 1 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+	$ \begin{array}{ccc} K & & & \\ & & = & \\ & & = & \\ & 0.04] & = & \\ & 0.04] & = & \\ & 0.04] & = & \\ & 0.04] & = & \\ & 0.04] & = & \\ \end{array} $	2.1 2.1 6.8 12.53 3.58 4.65 5.57				(26) (26) (27) (27) (27) (27) (27)
Windows Type Windows Type Windows Type Windows Type Windows Type Windows Type	2 2 3 4 4 5 5 6 6		III-	2.1 2.1 5.13 9.45 2.7 3.51		W/m2 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+	$ \begin{array}{ccc} K \\ $	2.1 2.1 6.8 12.53 3.58 4.65	<)			(26) (26) (27) (27) (27) (27)
Windows Type	e 2 e 3 e 4 e 5 e 6 e 7		III-	2.1 2.1 5.13 9.45 2.7 3.51 4.2		W/m2 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+	$ \begin{array}{ccc} K \\ $	2.1 2.1 6.8 12.53 3.58 4.65 5.57	<)			(26) (26) (27) (27) (27) (27) (27)
Windows Type	e 2 e 3 e 4 e 5 e 6 e 7			2.1 2.1 5.13 9.45 2.7 3.51 4.2 2.88		W/m2 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+	$ \begin{array}{ccc} K \\ $	(W/H 2.1 2.1 6.8 12.53 3.58 4.65 5.57 3.82	<)			kJ/K (26) (26) (27) (27) (27) (27) (27) (27)
Windows Type	e 2 e 3 e 4 e 5 e 6 e 7 e 8			2.1 2.1 5.13 9.45 2.7 3.51 4.2 2.88 2.08	2	W/m2 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+	$ \begin{array}{ccc} K & = & \begin{bmatrix} & & & \\ & $	(W/H 2.1 2.1 6.8 12.53 3.58 4.65 5.57 3.82 2.76	<)			kJ/K (26) (27) (27) (27) (27) (27) (27) (27) (27
Windows Type	2 2 3 4 4 5 5 6 6 7 6 8 8 9 9 6 10			2.1 2.1 5.13 9.45 2.7 3.51 4.2 2.88 2.08 3.51	2	W/m2 1 [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+ [1/(1.4)+	$ \begin{array}{ccc} K & = & \begin{bmatrix} & & & \\ & $	(W/H 2.1 2.1 6.8 12.53 3.58 4.65 5.57 3.82 2.76 4.65	<)			(26) (26) (27) (27) (27) (27) (27) (27) (27) (27

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Windows Type 12		2.88	x1/[1/(1.4)+ 0.04] = 3.82	(27)
Windows Type 13		2.08	$x^{1/[1/(1.4) + 0.04]} = 2.76$	(27)
Windows Type 14		3.51	x1/[1/(1.4) + 0.04] = 4.65	(27)
Windows Type 15		2.72	$x^{1/[1/(1.4) + 0.04]} = 3.61$	(27)
Windows Type 16		2.4	$x^{1/[1/(1.4) + 0.04]} = 3.18$	(27)
Windows Type 17		3.51	x1/[1/(1.4) + 0.04] = 4.65	(27)
Windows Type 18		2.7	$x^{1/[1/(1.4) + 0.04]} = 3.58$	(27)
Rooflights Type 1		2	$x^{1/[1/(1.4) + 0.04]} = 2.8$	(27b)
Rooflights Type 2		3	$x^{1/[1/(1.4) + 0.04]} = 4.2$	(27b)
Rooflights Type 3		7.5	$\times 1/[1/(1.4) + 0.04] = 10.5$	(27b)
Floor		161.8	x 0.12 = 19.416	(28)
Walls Type1 24.3	0	24.3	x 0.16 = 3.89	(29)
Walls Type2 55.35	0	55.35	x 0.16 = 8.86	(29)
Walls Type3 24.3	0	24.3	x 0.16 = 3.89	(29)
Walls Type4 55.35	0	55.35	x 0.16 = 8.86	(29)
Walls Type5 20.25	14.58	5.67	x 0.16 = 0.91	(29)
Walls Type6 55.35	8.31	47.04	x 0.16 = 7.53	(29)
Walls Type7 20.25	6.3	13.95	x 0.16 = 2.23	(29)
Wal <mark>ls Typ</mark> e8 55.35	2.7	52.65	x 0.16 = 8.42	(29)
Walls Type9 20.52	4.96	15.56	x 0.16 = 2.49	(29)
Wal <mark>ls Type10 37.26</mark>	3.51	33.75	x 0.16 = 5.4	(29)
Walls Type11 20.52	4.96	15.56	x 0.16 = 2.49	(29)
Walls Type12 37.26	1.3	35.96	x 0.16 = 5.75	(29)
Walls Type13 18.9	4.96	13.94	x 0.16 = 2.23	(29)
Walls Type14 22.68	3.51	19.17	x 0.16 = 3.07	(29)
Walls Type15 22.68	0	22.68	x 0.16 = 3.63	(29)
Walls Type16 18.09	0	18.09	x 0.16 = 2.89	(29)
Walls Type17 22.41	3.51	18.9	x 0.16 = 3.02	(29)
Walls Type18 18.09	0	18.09	x 0.16 = 2.89	(29)
Walls Type19 22.41	0	22.41	x 0.16 = 3.59	(29)
Walls Type20 18.9	5.12	13.78	x 0.16 = 2.2	(29)
Roof Type1 108.73	11.5	97.23	x 0.12 = 11.67	(30)
Roof Type2 83.83	3	80.83	x 0.12 = 9.7	(30)
Total area of elements, m ²		944.58		(31)
* for windows and roof windows, use e ** include the areas on both sides of in			ısing formula 1/[(1/U-value)+0.04] as given in paragraph 3.2	
Fabric heat loss, W/K = S (A x		same(3856997	(26)(30) + (32) = 227.36	(33)
WEST 1991 - DOWN SCHOOL STREET STREET				=

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = (27.36) (33) Heat capacity Cm = S(A x k) ((28)...(30) + (32) + (32a)...(32e) = (34) Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Medium (35) (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

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Energy lost from water storage, kWh/year $(47) \times (51) \times (52)$ Enter (50) or (54) in (55)	2) x (53) = 4.62 (54) 4.62 (55)
Water storage loss calculated for each month $((56)m = (55) \times$	
(56)m= 143.35 129.48 143.35 138.73 143.35 138.73 143.35 143.35 138.	
If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) – (H11)] + (50), else (57)m =	
(57)m= 143.35 129.48 143.35 138.73 143.35 138.73 143.35 143.35 138.	No. Control
Primary circuit loss (annual) from Table 3	0 (58)
Primary circuit loss calculated for each month (59)m = $(58) \div 365 \times (41)$ m	
(modified by factor from Table H5 if there is solar water heating and a cylin	
(59)m= 0 0 0 0 0 0 0 0 0	0 0 0 (59)
Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m	
(61)m= 1.29 1.13 1.17 1.02 0.97 0.84 0.78 0.89 0.8	9 1.05 1.15 1.25 (61)
Total heat required for water heating calculated for each month (62)m = 0.85	5 × (45)m + (46)m + (57)m + (59)m + (61)m
(62)m= 331.72 294.23 313.36 286.95 285.57 261.45 257.07 273.85 270.	.78 297.25 306.72 325.78 (62)
Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no	solar contribution to water heating)
(add additional lines if FGHRS and/or WWHRS applies, see Appendix G)	
(63)m= -31.28 -53.63 -94.5 -130.25 -163.29 -161.33 -158.88 -137.37 -105	.18 -69.48 -37.4 -25.97 (63)
Output from water heater	
(64)m= 300.44 240.61 218.86 156.7 122.28 100.12 98.2 136.48 165	5.6 227.78 269.32 299.81
Output from	m water heater (annual) ₁₁₂ 2336.21 (64)
Heat gains from water heating, kWh/month 0.25 [0.85 × (45)m + (61)m] + 0	0.8 x [(46)m + (57)m + (59)m]
(65)m= 177.21 158.27 171.11 160.18 161.89 151.72 152.43 158 154.	
(65)m= 177.21 158.27 171.11 160.18 161.89 151.72 152.43 158 154	.82 165.77 166.75 175.24 (65)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or ho	
include (57)m in calculation of (65)m only if cylinder is in the dwelling or ho	
include (57)m in calculation of (65)m only if cylinder is in the dwelling or house. 5. Internal gains (see Table 5 and 5a): Metabolic gains (Table 5), Watts	
include (57)m in calculation of (65)m only if cylinder is in the dwelling or house. 5. Internal gains (see Table 5 and 5a): Metabolic gains (Table 5), Watts	ot water is from community heating
include (57)m in calculation of (65)m only if cylinder is in the dwelling or house. 5. Internal gains (see Table 5 and 5a): Metabolic gains (Table 5), Watts Jan Feb Mar Apr May Jun Jul Aug Se	ep Oct Nov Dec .44 169.44 169.44 169.44 (66)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or ho 5. Internal gains (see Table 5 and 5a): Metabolic gains (Table 5), Watts Jan Feb Mar Apr May Jun Jul Aug Sc (66)m= 169.44	ep Oct Nov Dec .44 169.44 169.44 169.44 (66)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or hold of the color o	ep Oct Nov Dec
include (57)m in calculation of (65)m only if cylinder is in the dwelling or house the following of the control	ep Oct Nov Dec .44 169.44 169.44 169.44 (66) e 5 78 46.7 54.51 58.11 (67) Table 5
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the control	ep Oct Nov Dec .44 169.44 169.44 169.44 (66) e 5 78 46.7 54.51 58.11 (67) Table 5 .2 494.81 537.23 577.11 (68)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the color o	ep Oct Nov Dec (66) 44 169.44 169.44 (66) 65 78 46.7 54.51 58.11 (67) Table 5 (68) 68 5 (68) 68 5 (68) 68 5 (68) 68 5 (68) 68 68 68 68 68 68 68 68 68 68 68 68 68
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec (66) 44 169.44 169.44 (66) 65 78 46.7 54.51 58.11 (67) Table 5 (68) 68 5 (68) 68 5 (68) 68 5 (68) 68 5 (68) 68 68 68 68 68 68 68 68 68 68 68 68 68
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec .44 169.44 169.44 169.44 (66) e 5 78 46.7 54.51 58.11 (67) Table 5 .2 494.81 537.23 577.11 (68) able 5 .94 39.94 39.94 39.94 (69)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec .44 169.44 169.44 169.44 (66) e 5 78 46.7 54.51 58.11 (67) Table 5 .2 494.81 537.23 577.11 (68) able 5 .94 39.94 39.94 39.94 (69)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the color o	ep Oct Nov Dec
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec 44 169.44 169.44 169.44 (66) 5 5 78 46.7 54.51 58.11 (67) Table 5 2 494.81 537.23 577.11 (68) able 5 94 39.94 39.94 39.94 (69) 5 3 3 3 3 (70) 5 5 -135.55 -135.55 -135.55 (71)
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec
include (57)m in calculation of (65)m only if cylinder is in the dwelling or home of the content	ep Oct Nov Dec

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation: Ac	cess Factor ble 6d		Area m²		Flux Table 6a		g_ Table 6b		FF Table 6c		Gains (W)	
Northeast _{0.9x}	0.77	x	4.2	x	11.28	×	0.63	x	0.7	=	14.48	(75)
Northeast _{0.9x}	0.77	x	2.08	×	11.28	×	0.63	×	0.7	=	7.17	(75)
Northeast _{0.9x}	0.77	x	2.88	×	11.28	×	0.63	×	0.7	=	9.93	(75)
Northeast _{0.9x}	0.77	x	2.72	×	11.28	×	0.63	×	0.7	=	9.38	(75)
Northeast 0.9x	0.77	x	2.4	×	11.28	×	0.63	×	0.7	=	8.28	(75)
Northeast _{0.9x}	0.77	x	4.2	×	22.97	×	0.63	×	0.7] =	29.48	(75)
Northeast _{0.9x}	0.77	x	2.08	×	22.97	×	0.63	×	0.7] =	14.6	(75)
Northeast _{0.9x}	0.77	x	2.88	×	22.97	x	0.63	×	0.7	=	20.21	(75)
Northeast _{0.9x}	0.77	x	2.72	×	22.97	×	0.63	×	0.7	=	19.09	(75)
Northeast _{0.9x}	0.77	x	2.4	×	22.97	×	0.63	×	0.7] =	16.85	(75)
Northeast _{0.9x}	0.77	x	4.2	×	41.38	×	0.63	×	0.7] =	53.11	(75)
Northeast _{0.9x}	0.77	x	2.08	×	41.38	×	0.63	×	0.7	=	26.3	(75)
Northeast _{0.9x}	0.77	x	2.88	×	41.38	×	0.63	×	0.7] =	36.42	(75)
Northeast _{0.9x}	0.77	x	2.72	x	41.38	х	0.63	×	0.7] =	34.4	(75)
Northeast _{0.9x}	0.77	x	2.4	x	41.38	×	0.63	×	0.7] =	30.35	(75)
Northeast 0.9x	0.77	x	4.2	×	67.96	×	0.63	×	0.7] =	87.23	(75)
Northeast 0.9x	0.77	x	2.08	×	67.96	×	0.63	×	0.7] =	43.2	(75)
Northeast _{0.9x}	0.77	x	2.88	×	67.96	×	0.63	×	0.7] =	59,81	(75)
Northeast _{0.9x}	0.77	x	2.72	×	67.96	×	0.63	×	0.7] =	56.49	(75)
Northeast 0.9x	0.77	x	2.4	×	67.96	×	0.63	×	0.7] =	49.84	(75)
Northeast _{0.9x}	0.77	x	4.2	×	91.35	×	0.63	×	0.7	=	117.25	(75)
Northeast 0.9x	0.77	x	2.08	×	91.35	x	0.63	×	0.7] =	58.07	(75)
Northeast _{0.9x}	0.77	x	2.88	×	91.35	x	0.63	x	0.7] =	80.4	(75)
Northeast _{0.9x}	0.77	X	2.72	×	91.35	×	0.63	×	0.7	=-	75.93	(75)
Northeast _{0.9x}	0.77	X	2.4	×	91.35	x	0.63	x	0.7] =	67	(75)
Northeast _{0.9x}	0.77	x	4.2	×	97.38	×	0.63	×	0.7] =	125	(75)
Northeast _{0.9x}	0.77	X	2.08	×	97.38	×	0.63	×	0.7	=	61.9	(75)
Northeast _{0.9x}	0.77	X	2.88	×	97.38	×	0.63	×	0.7	=	85.71	(75)
Northeast _{0.9x}	0.77	X	2.72	×	97.38	×	0.63	×	0.7	=	80.95	(75)
Northeast _{0.9x}	0.77	X	2.4	x	97.38	×	0.63	×	0.7	=	71.43	(75)
Northeast _{0.9x}	0.77	X	4.2	×	91.1	×	0.63	×	0.7	=	116.94	(75)
Northeast _{0.9x}	0.77	X	2.08	×	91.1	×	0.63	×	0.7	=	57.91	(75)
Northeast _{0.9x}	0.77	X	2.88	×	91.1	X	0.63	X	0.7	=	80.18	(75)
Northeast _{0.9x}	0.77	X	2.72	×	91.1	×	0.63	×	0.7	=	75.73	(75)
Northeast _{0.9x}	0.77	X	2.4	×	91.1	×	0.63	×	0.7	=	66.82	(75)
Northeast _{0.9x}	0.77	X	4.2	×	72.63	×	0.63	x	0.7	=	93.22	(75)
Northeast _{0.9x}	0.77	x	2.08	×	72.63	×	0.63	x	0.7	=	46.17	(75)
Northeast _{0.9x}	0.77	X	2.88	х	72.63	×	0.63	X	0.7] =	63.92	(75)
Northeast _{0.9x}	0.77	X	2.72	X	72.63	×	0.63	X	0.7	=	60.37	(75)

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Northeast 0.9x 0.77 x 2.4 x 72.63 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.28 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.24	0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7		53.27 (7 64.72 (7 32.05 (7 44.38 (7 41.91 (7 36.98 (7 36.03 (7 17.84 (7 24.7 (7 23.33 (7 20.59 (7 18.22 (7
Northeast 0.9x 0.77 x 2.08 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.08	0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7		32.05 (7 44.38 (7 41.91 (7 36.98 (7 36.03 (7 17.84 (7 24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 2.88 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.24 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.08	0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7		44.38 (7 41.91 (7 36.98 (7 36.03 (7 17.84 (7 24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x	0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7		41.91 (7 36.98 (7 36.03 (7 17.84 (7 24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 2.4 x 50.42 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7 0.7 0.7 0.7 0.7 0.7 0.7 0.7		36.98 (7 36.03 (7 17.84 (7 24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 4.2 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7 0.7 0.7 0.7 0.7 0.7 0.7		36.03 (7 17.84 (7 24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 2.08 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7 0.7 0.7 0.7 0.7 0.7 0.7		17.84 (7 24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 2.88 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.72 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7 0.7 0.7 0.7 0.7		24.7 (7 23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 2.72 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7 0.7 0.7 0.7		23.33 (7 20.59 (7
Northeast 0.9x 0.77 x 2.4 x 28.07 x 0.63 x Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7 0.7 0.7		20.59 (7
Northeast 0.9x 0.77 x 4.2 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.08 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7		***************************************
Northeast 0.9x 0.77 x 2.08 x 14.2 x 0.63 x Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x	0.7	<u> </u>	18.22 (7
Northeast 0.9x 0.77 x 2.88 x 14.2 x 0.63 x		=	
	0.7		9.02 (7
North cost a c	- Constant	= [12.5 (7
Northeast 0.9x 0.77 x 2.72 x 14.2 x 0.63 x	0.7	= [11.8 (7
Northeast 0.9x 0.77 x 2.4 x 14.2 x 0.63 x	0.7		10.41 (7
Northeast 0.9x 0.77 x 4.2 x 9.21 x 0.63 x	0.7	=[11.83 (7
Northeast 0.9x 0.77 x 2.08 x 9.21 x 0.63 x	0.7	=[5.86 (7
Northeast 0.9x 0.77 x 2.88 x 9.21 x 0.63 x	0.7	= [8.11 (7
Northeast 0.9x 0.77 x 2.72 x 9.21 x 0.63 x	0.7	=[7.66 (7
Northeast 0.9x 0.77 x 2.4 x 9.21 x 0.63 x	0.7	- [6.76 (7
Southeast 0.9x 0.77 x 3.51 x 36.79 x 0.63 x	0.7	3	39.47 (7
Southeast 0.9x 0.77 x 3.51 x 36.79 x 0.63 x	0.7	= [39.47 (7
Southeast 0.9x 0.77 x 3.51 x 36.79 x 0.63 x	0.7	[39.47 (7
Southeast 0.9x 0.77 x 3.51 x 36.79 x 0.63 x	0.7	= [39.47 (7
Southeast 0.9x 0.77 x 2.7 x 36.79 x 0.63 x	0.7	= [30.36 (7
Southeast 0.9x 0.77 x 3.51 x 62.67 x 0.63 x	0.7	= [67.23 (7
Southeast 0.9x 0.77 x 3.51 x 62.67 x 0.63 x	0.7	= [67.23 (7
Southeast 0.9x 0.77 x 3.51 x 62.67 x 0.63 x	0.7	= _	67.23 (7
Southeast 0.9x 0.77 x 3.51 x 62.67 x 0.63 x	0.7	=	67.23 (7
Southeast 0.9x 0.77 x 2.7 x 62.67 x 0.63 x	0.7	= _	51.72 (7
Southeast 0.9x 0.77 x 3.51 x 85.75 x 0.63 x	0.7		91.99 (7
Southeast 0.9x 0.77 x 3.51 x 85.75 x 0.63 x	0.7	= _	91.99 (7
Southeast 0.9x 0.77 x 3.51 x 85.75 x 0.63 x	0.7	= _	91.99 (7
Southeast 0.9x 0.77 x 3.51 x 85.75 x 0.63 x	0.7	= _	91.99 (7
Southeast 0.9x 0.77 x 2.7 x 85.75 x 0.63 x	0.7		70.76 (7
Southeast 0.9x 0.77 x 3.51 x 106.25 x 0.63 x	0.7	= _	113.98 (7
Southeast 0.9x 0.77 x 3.51 x 106.25 x 0.63 x	0.7	= _	113.98 (7
Southeast 0.9x 0.77 x 3.51 x 106.25 x 0.63 x	0.7	= _	113.98 (7
Southeast 0.9x 0.77 x 3.51 x 106.25 x 0.63 x	0.7	-	113.98 (7
Southeast 0.9x 0.77 x 2.7 x 106.25 x 0.63 x	0.7	= _	87.67 (7

Southeast _{0.9x}	0.77	x	3.51	x	119.01	x	0.63	x	0.7	=	127.66	(77)
Southeast _{0.9x}	0.77	×	3.51	×	119.01	×	0.63	×	0.7	=	127.66	(77)
Southeast _{0.9x}	0.77	×	3.51	×	119.01	×	0.63	×	0.7	=	127.66	(77)
Southeast _{0.9x}	0.77	×	3.51	×	119.01	×	0.63	×	0.7	=	127.66	(77)
Southeast _{0.9x}	0.77	×	2.7	×	119.01	×	0.63	×	0.7	=	98.2	(77)
Southeast _{0.9x}	0.77	×	3.51	×	118.15	×	0.63	×	0.7	=	126.74	(77)
Southeast _{0.9x}	0.77	×	3.51	×	118.15	×	0.63	×	0.7	=	126.74	(77)
Southeast _{0.9x}	0.77	×	3.51	×	118.15	×	0.63	×	0.7	=	126.74	(77)
Southeast _{0.9x}	0.77	×	3.51	×	118.15	×	0.63	x	0.7	=	126.74	(77)
Southeast _{0.9x}	0.77	×	2.7	×	118.15	×	0.63	×	0.7] = [97.49	(77)
Southeast _{0.9x}	0.77	×	3.51	×	113.91	×	0.63	×	0.7	=	122.19	(77)
Southeast _{0.9x}	0.77	×	3.51	×	113.91	×	0.63	×	0.7	=	122.19	(77)
Southeast _{0.9x}	0.77	×	3.51	×	113.91	×	0.63	×	0.7] =	122.19	(77)
Southeast _{0.9x}	0.77	×	3.51	×	113.91	x	0.63	×	0.7	=	122.19	(77)
Southeast _{0.9x}	0.77	×	2.7	×	113.91	x	0.63	x	0.7	=	93.99	(77)
Southeast _{0.9x}	0.77	×	3.51	×	104.39	×	0.63	X	0.7	=	111.98	(77)
Southeast _{0.9x}	0.77	×	3.51	x	104.39	x	0.63	x	0.7		111.98	(77)
Southeast 0.9x	0.77	×	3.51	×	104.39	×	0.63	X	0.7] =	111.98	(77)
Southeast 0.9x	0.77	×	3.51	×	104.39	×	0.63	×	0.7] =	111.98	(77)
Southeast 0.9x	0.77	×	2.7	×	104.39	x	0.63	×	0.7] = [86.14	(77)
Southeast 0.9x	0.77	×	3.51	x	92.85	x	0.63	×	0.7] =	99.6	(77)
Southeast _{0.9x}	0.77	×	3.51	x	92.85	×	0.63	×	0.7] =	99.6	(77)
Southeast _{0.9x}	0.77	×	3.51	×	92.85	×	0.63	×	0.7] =	99.6	(77)
Sout <mark>heast _{0.9x}</mark>	0.77	×	3.51	×	92.85	×	0.63	×	0.7	=	99.6	(77)
Southeast _{0.9x}	0.77	×	2.7	×	92.85	x	0.63	x	0.7	=	76.62	(77)
Southeast _{0.9x}	0.77	×	3.51	×	69.27	×	0.63	×	0.7] =	74.3	(77)
Southeast _{0.9x}	0.77	×	3.51	×	69.27	×	0.63	×	0.7	=	74.3	(77)
Southeast _{0.9x}	0.77	×	3.51	×	69.27	×	0.63	×	0.7	=	74.3	(77)
Southeast _{0.9x}	0.77	×	3.51	×	69.27	×	0.63	×	0.7	=	74.3	(77)
Southeast _{0.9x}	0.77	×	2.7	×	69.27	×	0.63	×	0.7	=	57.16	(77)
Southeast _{0.9x}	0.77	×	3.51	×	44.07	×	0.63	×	0.7	=	47.27	(77)
Southeast _{0.9x}	0.77	×	3.51	×	44.07	×	0.63	X	0.7	=	47.27	(77)
Southeast _{0.9x}	0.77	×	3.51	X	44.07	×	0.63	X	0.7	=	47.27	(77)
Southeast _{0.9x}	0.77	×	3.51	×	44.07	×	0.63	×	0.7	=	47.27	(77)
Southeast _{0.9x}	0.77	×	2.7	×	44.07	×	0.63	×	0.7	=	36.37	(77)
Southeast _{0.9x}	0.77	×	3.51	×	31.49	×	0.63	×	0.7	=	33.78	(77)
Southeast 0.9x	0.77	×	3.51	×	31.49	×	0.63	×	0.7	=	33.78	(77)
Southeast _{0.9x}	0.77	×	3.51	×	31.49	X	0.63	×	0.7	=	33.78	(77)
Southeast _{0.9x}	0.77	×	3.51	×	31.49	×	0.63	×	0.7	=	33.78	(77)
Southeast 0.9x	0.77	×	2.7	×	31.49	×	0.63	×	0.7	=	25.98	(77)
Southwest _{0.9x}	0.77	×	5.13	X	36.79		0.63	X	0.7	=	57.69	(79)

Southwest _{0.9x}	0.77	x	9.45	x	36.79		0.63	×	0.7	=	106.26	(79)
Southwest _{0.9x}	0.77	×	2.88	×	36.79		0.63	×	0.7	=	32.38	(79)
Southwest _{0.9x}	0.77	×	2.08	×	36.79		0.63	×	0.7	=	23.39	(79)
Southwest _{0.9x}	0.77	×	2.88	×	36.79		0.63	×	0.7	=	32.38	(79)
Southwest _{0.9x}	0.77	×	2.08	x	36.79		0.63	×	0.7	=	23.39	(79)
Southwest _{0.9x}	0.77	×	5.13	×	62.67		0.63	×	0.7] =	98.26	(79)
Southwest _{0.9x}	0.77	×	9.45	×	62.67		0.63	×	0.7] =	181	(79)
Southwest _{0.9x}	0.77	×	2.88	×	62.67		0.63	×	0.7	=	55.16	(79)
Southwest _{0.9x}	0.77	×	2.08	×	62.67		0.63	×	0.7	=	39.84	(79)
Southwest _{0.9x}	0.77	×	2.88	×	62.67		0.63	×	0.7] =	55.16	(79)
Southwest _{0.9x}	0.77	×	2.08	×	62.67		0.63	×	0.7	=	39.84	(79)
Southwest _{0.9x}	0.77	×	5.13	×	85.75		0.63	×	0.7	=	134.44	(79)
Southwest _{0.9x}	0.77	×	9.45	×	85.75		0.63	×	0.7	=	247.66	(79)
Southwest _{0.9x}	0.77	x	2.88	×	85.75		0.63	×	0.7] =	75.48	(79)
Southwest _{0.9x}	0.77	x	2.08	x	85.75		0.63	X	0.7	=	54.51	(79)
Southwest _{0.9x}	0.77	×	2.88	×	85.75		0.63	×	0.7	=	75.48	(79)
Southwest _{0.9x}	0.77	X	2.08	x	85.75		0.63	X	0.7	=	54.51	(79)
Southwest _{0.9x}	0.77	×	5.13	×	106.25		0.63	×	0.7] =	166.58	(79)
Southwest _{0.9x}	0.77	×	9.45	×	106.25	Λ	0.63	×	0.7] =	306.86	(79)
Southwest _{0.9x}	0.77	×	2.88	×	106.25		0.63	×	0.7	=	93.52	(79)
Southwest _{0.9x}	0.77	×	2.08	X	106.25		0.63	×	0.7	=	67.54	(79)
Southwest _{0.9x}	0.77	x	2.88	×	106,25		0.63	×	0.7	_ =	93.52	(79)
Southwest _{0.9x}	0.77	×	2.08	×	106.25		0.63	×	0.7	_ =	67.54	(79)
Southwest _{0.9x}	0.77	×	5.13	×	119.01		0.63	×	0.7	=	186.58	(79)
Southwest _{0.9x}	0.77	X	9.45	X	119.01	* *	0.63	X	0.7] =	343.71	(79)
Southwest _{0.9x}	0.77	X	2.88	X	119.01		0.63	X	0.7	=	104.75	(79)
Southwest _{0.9x}	0.77	×	2.08	×	119.01		0.63	×	0.7	=	75.65	(79)
Southwest _{0.9x}	0.77	×	2.88	×	119.01		0.63	×	0.7	=	104.75	(79)
Southwest _{0.9x}	0.77	×	2.08	×	119.01		0.63	×	0.7	=	75.65	(79)
Southwest _{0.9x}	0.77	×	5.13	×	118.15		0.63	×	0.7	=	185.23	(79)
Southwest _{0.9x}	0.77	×	9.45	X	118.15		0.63	×	0.7] =	341.22	(79)
Southwest _{0.9x}	0.77	×	2.88	×	118.15		0.63	×	0.7	-	103.99	(79)
Southwest _{0.9x}	0.77	X	2.08	X	118.15	8 8	0.63	X	0.7	=	75.11	(79)
Southwest _{0.9x}	0.77	X	2.88	×	118.15		0.63	×	0.7	_ =	103.99	(79)
Southwest _{0.9x}	0.77	×	2.08	×	118.15		0.63	×	0.7	_ =	75.11	(79)
Southwesto s	0.77	X	5.13	×	113.91		0.63	×	0.7	=	178.59	(79)
Southwesto.9x	0.77	X	9.45	×	113.91		0.63	X	0.7	=	328.97	(79)
Southwests a	0.77	Х	2.88	×	113.91		0.63	×	0.7	_ =	100.26	(79)
Southwesto.o.	0.77	X	2.08	×	113.91		0.63	X	0.7] =	72.41	(79)
Southwest _{0.9x}	0.77	X	2.88	×	113.91		0.63	X	0.7	-	100.26	(79)
Southwest0.9x	0.77	X	2.08	X	113.91	. s	0.63	X	0.7	_ =	72.41	(79)

Southwest _{0.9x}	0.77	×	5.13	x	104.39	Ī	0.63	x	0.7	=	163.66	(79)
Southwest _{0.9x}	0.77	×	9.45	×	104.39	ĺ	0.63	×	0.7	=	301.48	(79)
Southwest _{0.9x}	0.77	×	2.88	×	104.39	Ì	0.63	×	0.7	=	91.88	(79)
Southwest _{0.9x}	0.77	×	2.08	×	104.39		0.63	×	0.7	=	66.36	(79)
Southwest _{0.9x}	0.77	×	2.88	x	104.39	Ì	0.63	×	0.7	=	91.88	(79)
Southwest _{0.9x}	0.77	×	2.08	×	104.39	Ì	0.63	×	0.7] = [66.36	(79)
Southwest _{0.9x}	0.77	×	5.13	×	92.85]	0.63	×	0.7	=	145.57	(79)
Southwest _{0.9x}	0.77	×	9.45	×	92.85		0.63	×	0.7	=	268.16	(79)
Southwest _{0.9x}	0.77	×	2.88	×	92.85		0.63	×	0.7	=	81.73	(79)
Southwest _{0.9x}	0.77	×	2.08	×	92.85]	0.63	×	0.7	=	59.02	(79)
Southwest _{0.9x}	0.77	×	2.88	×	92.85		0.63	×	0.7	=	81.73	(79)
Southwest _{0.9x}	0.77	×	2.08	×	92.85	l	0.63	×	0.7] =	59.02	(79)
Southwest _{0.9x}	0.77	×	5.13	×	69.27		0.63	×	0.7] =	108.6	(79)
Southwest _{0.9x}	0.77	×	9.45	×	69.27]	0.63	×	0.7	=	200.05	(79)
Southwest _{0.9x}	0.77	×	2.88	×	69.27		0.63	×	0.7	=	60.97	(79)
Southwest _{0.9x}	0.77	×	2.08	×	69.27	l	0.63	X	0.7	=	44.03	(79)
Southwest _{0.9x}	0.77	×	2.88	X	69.27		0.63	X	0.7	=	60.97	(79)
Southwest _{0.9x}	0.77	×	2.08	×	69.27		0.63	×	0.7] =	44.03	(79)
Southwest _{0.9x}	0.77	×	5.13	×	44.07		0.63	×	0.7] = [69.09	(79)
Southwest _{0.9x}	0.77	×	9.45	×	44.07		0.63	×	0.7	=	127.28	(79)
Southwest _{0.9x}	0.77	×	2.88	X	44.07		0.63	×	0.7	=	38.79	(79)
Southwest _{0.9x}	0.77	×	2.08	×	44.07		0.63	×	0.7	=	28.01	(79)
Southwest _{0.9x}	0.77	×	2.88	×	44.07		0.63	×	0.7	=	38.79	(79)
Southwest _{0.9x}	0.77	×	2.08	×	44.07	ļ	0.63	×	0.7	=	28.01	(79)
Southwest _{0,9x}	0.77	X	5.13	X	31.49		0.63	X	0.7	=	49.37	(79)
Southwest _{0.9x}	0.77	×	9.45	×	31.49		0.63	×	0.7	=	90.94	(79)
Southwest _{0.9x}	0.77	×	2.88	×	31.49	ļ	0.63	×	0.7	=	27.71	(79)
Southwest _{0.9x}	0.77	×	2.08	×	31.49	ļ	0.63	×	0.7	=	20.02	(79)
Southwest _{0.9x}	0.77	×	2.88	X	31.49		0.63	×	0.7	=	27.71	(79)
Southwest _{0.9x}	0.77	×	2.08	×	31.49		0.63	×	0.7	=	20.02	(79)
Northwest 0.9x	0.77	×	2.7	×	11.28	×	0.63	×	0.7	= :	9.31	(81)
Northwest _{0.9x}	0.77	×	1.3	×	11.28	×	0.63	×	0.7	-	4.48	(81)
Northwest _{0.9x}	0.77	×	2.7	X	22.97	X	0.63	X	0.7	=	18.95	(81)
Northwest _{0.9x}	0.77	×	1.3	×	22.97	×	0.63	×	0.7	=	9.12	(81)
Northwest _{0.9x}	0.77	×	2.7	×	41.38	×	0.63	×	0.7	=	34.14	(81)
Northwest 0.9x	0.77	×	1.3	×	41.38	×	0.63	×	0.7	=	16.44	(81)
Northwest 0.9x	0.77	X	2.7	×	67.96	×	0.63	X	0.7	=	56.07	(81)
Northwest 0.9x	0.77	X	1.3	×	67.96	X	0.63	×	0.7	= =	27	(81)
Northwest 0.9x	0.77	X	2.7	×	91.35	×	0.63	×	0.7	= .	75.37	(81)
Northwest 0.9x	0.77	X	1.3	×	91.35	×	0.63	X	0.7	=	36.29	(81)
Northwest _{0.9x}	0.77	X	2.7	X	97.38	X	0.63	X	0.7	=	80.36	(81)