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Project **KXB**

## LOAD AND CAPACITY FACTORS

### Philosophy

S1061 Existing elements to the TfL demise are validated to TfL report S1061 A5.

### Load combinations

cl. 3.3.4.2 QA = assessment load =  $\gamma_f \times QK$   
 QK = nominal load  
 $\gamma_f = \gamma_{f1} \times \gamma_{f2} \times \gamma_{f3}$   
 (b)  $\gamma_{f3} = 1.15, \quad \gamma_{f2} = 1.0$

We note that by inspection, wind loading is not critical for the girders.

Table 13

Type	Beneficial	Adverse
DL	0.85	1.15
LL	0	1.35

→  $\gamma_{f1}$

← Chosen conservatively from table 14

$$\gamma_f = 1.32G + 1.55Q$$

Standard BS factors will instead be employed conservatively:

$$\gamma_f = 1.4G + 1.6Q$$

### Assessment of Resistance

cl. 3.3.5.2 RA = assessment resistance =  $FC \times RA^*$   
 RA\* = calculated resistance  
 FC = condition factor

cl. 3.3.5.3 RA\* = function ( $f_k / \gamma_M$ )

table 15

Material	Steel	RC	Masonry	RC reinf.
$\gamma_M$	1.05	1.5	1.0	1.15

cl. 3.2.6.3 RA\* = function ( $230 / 1.05$ ) = function (219)  
 FC = 0.9 -> web and top flange uncertainty for girders  
 RA = function ( $219 \times 0.9$ ) = function (197).

cl. 3.3.10.2 Alternatively, grade 46 (s275) steel can be used for the calculation and the resulting capacities multiplied by 230/275. The FC factor will in these instances still be applied to the results --> utilisation  $\leq 100\% \times 230/275 \times 0.9 = 75\%$