

# LMB GEOSOLUTIONS LTD

# **GROUND INVESTIGATION & ASSESSMENT**

ROCHESTER SQUARE SPIRITUALIST TEMPLE, ROCHESTER SQUARE, LONDON NW1

December 2016

#### **DOCUMENT RECORD**

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# Executive Summary

Site Details	Rochester Square Spiritualist Temple, Rochester Square, London NW1 9RY
Proposed Development	The development proposals include demolition of the existing structure and construction of a new mixed use four storey structure that will include a single storey basement.
Ground & Groundwater Conditions	Made Ground overlying Head Deposits and the London Clay Formation. Groundwater was recorded during monitoring and is considered to form a thin but laterally continuous aquifer unit within the Head Deposits over the area of the site.
Geotechnical Advice	For traditional spread or raft foundations placed on the competent firm to stiff clay at a depth of 4.00m to 4.50m bgl (i.e. approximate formation level) a net safe bearing pressure of 140kN/m2 should be available.
	However, should a piled foundation solution be considered, a preliminary assessment indicates that for a 10m pile (founded on the London Clay Formation) safe working loads of 263kN and 371kN are estimated for 450mm and 600mm pile diameters respectively.
	The above advice assumes that the proposed basement development and in particular foundations would not be within the influence of any trees or tree routes.
	Given the size of the excavation, the adjacent and nearby structures and the presence of shallow groundwater it is considered likely that temporary or permanent support (sheet/secant piles or similar) will be needed for construction.
	Coefficient of active earth pressure: Made Ground: 0.35. Head Deposits 0.30.London Clay Formation: 0.40.
	Coefficient of passive earth resistance: Made Ground: 3.5. Head Deposits 4.0.London Clay Formation: 2.5.
	Buried concrete: Made Ground: DS-1, AC-1s. Head Deposits DS-1, AC-1s. London Clay Formation: DS-2, AC-2.
Recommendations	<ul> <li>The full set of recommendations should be reviewed but in summary the following are provided:</li> <li>The preliminary pile assessment should be confirmed and/or amended by a competent piling contractor.</li> <li>It is recommended that additional groundwater and ground gas monitoring be undertaken.</li> </ul>
This executive summary in including conclusions and	is not a stand alone document and should be read in conjunction with the full report text, recommendations.

# INTRODUCTION

### Introduction

#### AUTHORISATION

LMB Geosolutions Ltd (LMB) was instructed by Spacelab (Architects) on behalf of Camden Land Partnership Ltd (the Client) in November 2016 to undertake ground investigation and assessment works in relation to the proposed development at Rochester Square Spiritualist Temple, Rochester Square, London NW1 9RY (the Site).

#### PROJECT AND SITE DETAILS

Site Address	Rochester Square Spiritualist Temple, Rochester Square, London NW1 9RY (the Site). A Site Location Plan is provided as <b>Figure 1</b> .
Proposed Development	<ul> <li>The site currently comprises a former temple that is occupied by live in security. The main entrance is via gate located on the southern side of Rochester Square with the rear garden accessed from a gate on the northern side of Rochester Square.</li> <li>Information provided by the Architects and Symmetrys Ltd (Consultant Engineers) indicates that the proposed development involves demolition of the existing structure and construction of a new mixed use four storey structure that will include a single storey basement.</li> <li>Based on the information provided, the following assumptions have been made:</li> <li>The development will comprise demolition of the existing building and construction of commercial space and residential flats;</li> <li>The basement will comprise a single storey structure;</li> <li>The basement will occupy most the footprint of the development (326m<sup>2</sup> of</li> </ul>
	<ul> <li>426m<sup>2</sup>); and</li> <li>The basement will be utilised for office space (front) and residential units (rear).</li> </ul>
Background	<ul> <li>The scope of works and requirements of this report were based on the information provided by Symmetrys (Consultant Engineers) within the following documents:</li> <li>Specification for Geotechnical Site Investigation for 110 Rochester Square, London NW1 (ref. 2016061, 3<sup>rd</sup> November 2016); &amp;</li> <li>Borehole Location Plan (ref. SI01).</li> </ul>

### INTRODUCTION

#### AIMS & OBJECTIVES

This report aims to provide information sufficient to meet the requirements of the specification provided by the Consultant Engineers.

#### SCOPE OF WORKS

The following scope of works has been completed:

- Site set up including liaison with Consultant Engineers, Client and appointment of sub-contractors;
- Mobilisation to site and transport of the rig to the proposed location;
- Completion of 2No 'cut down' cable percussive boreholes to depths of 15.00m bgl (or refusal) with insitu SPTs and collection of disturbed and undisturbed samples for laboratory testing;
- Supervision and geological logging of the soil arisings in accordance with BS5930 by an appropriately experienced geo-environmental engineer;
- Installation of two monitoring wells to depths of 4.0m and 8.0m below ground level and return monitoring of groundwater levels on 1no. occasion;
- Geotechnical laboratory testing of the soil samples for an appropriate suite of determinands (including pH, sulphate, atterberg limits, and moisture content);
- Chemical analysis of 1no. sample of Made Ground, including Waste Acceptance Criteria (WAC);
- Completion of a factual and interpretive report that includes;
  - Details of the ground and groundwater conditions encountered;
  - Presentation of chemical analytical results;
  - Geotechnical laboratory testing and provision of advice on the material properties of the shallow soil horizon including parameters to aid in retaining wall design and foundation options; &
  - Conclusions and recommendations.

#### LIMITATIONS

LMB has prepared this report solely for the use of the named Client and those parties with whom a warranty agreement and/or assignment has been agreed. Should any third party wish to use or rely upon the contents of the report, written approval must be sought from LMB and the Client.

LMB accepts no responsibility or liability for:

a) the consequences of this document being used for any purpose or project other than for which it was commissioned, and

b) issue of this document to any third party with whom an agreement has not been executed.

The risk assessment and opinions provided, among other things, take in to consideration currently available guidance and best available techniques relating to acceptable contamination concentrations and

# INTRODUCTION

interpretation of these values. No liability can be accepted for the retrospective effects of any future changes or amendments to these value.

### GROUND INVESTIGATION & FINDINGS

### Ground Investigation & Findings

#### INTRODUCTION

The ground investigation works were undertaken between 21<sup>st</sup> and 22<sup>nd</sup> November 2016 and comprised the progression of two 'cut down' cable percussive boreholes to 15.0m bgl with sampling of soil for laboratory testing (see **Figure 2**).

Groundwater monitoring was undertaken following completion of the fieldworks on 30<sup>th</sup> November 2016.

Details of the ground investigation completed, along with the findings of the investigation, are provided in the following sections. The exploratory hole logs and laboratory results are presented in **Appendix A**, **B** and **C** respectively.

#### **Guidance Documents**

Details of the best practice guidance documents and reference information used in undertaking the ground investigation and assessment are provided at the end of this report (see REFERENCES & GUIDANCE).

#### INVESTIGATION STRATEGY

The ground investigation was designed based on the requirements of the Consultant Engineers set out in the Specification for Geotechnical Site Investigation for 110 Rochester Square, London NW1 (ref. 2016061, 3rd November 2016).

#### **Soil Chemical Analysis & Laboratory Testing**

Soil samples were submitted to the UKAS and MCERTS accredited laboratories of i2 Analytical for chemical analysis and geotechnical testing.

The results of the geotechnical and chemical analysis (including waste acceptance criteria testing) are presented in **Appendix B** and **C** respectively.

#### **GROUND & GROUNDWATER CONDITIONS**

#### **Ground Conditions**

The table below provides a summary of ground conditions encountered with full descriptions provided in the associated exploratory hole logs provided in **Appendix A**:

# **GROUND INVESTIGATION & FINDINGS**

Strata	Depth Range to Top (m bgl)	Depth Range to (Base (m bgl)	Summary Description
Made Ground	Ground Level	0.50 - 0.80	In BH1 (frontage) the ground surface was found to comprise concrete.
			The Made Ground soils were generally found to comprise an upper layer (0.15m) of slightly sandy clay with rootlets over clay with brick gravel.
			In BH1 the base of the Made Ground included broken tile and brick.
Head Deposits	0.50 - 0.80	3.65 - 3.75	Soils interpreted as Head Deposits were found to comprise an upper horizon (approx. 1m) of soft becoming firm clay overlying gravelly clay.
London Clay Formation	3.65 - 3.75	15.00(1)	The London Clay was found to comprise firm becoming stiff very closely fissured clay.

(1) Base of the London Clay was not determined.

#### **Visual and Olfactory Observations**

No visual or olfactory evidence of contamination was observed during the ground investigation works. However, Made Ground soils were encountered in all exploratory hole locations and can be indicative of the presence of contaminants.

#### **Groundwater Conditions**

Groundwater strikes were recorded during the ground investigation works within BH1 (0.70m and 7.0m). In BH2 no groundwater strikes were observed during drilling, but groundwater was recorded the following morning within the open hole (3.40m).

#### Return Monitoring

Groundwater and ground gas levels were monitored on Wednesday 30<sup>th</sup> November 2016 and the results are summarised in the table below:

Location	Strata	Groundwater Depth (m bgl)	VOC (ppm)	CH4 (% v/v)	CO2 (% v/v)	02 (% v/v)	Flow Rate (l/hr)	Gas Screening Value (l/hr)
BH1	London Clay	6.58	0.7	0.10	1.40	18.2	0.2	0.0028
BH2	Head Deposits	1.64	-	-	-	-	-	-

# **GROUND INVESTIGATION & FINDINGS**

#### **Characteristic Values of Soil Parameters**

A summary of the geotechnical properties of the strata based on the field and laboratory testing is provided in the table below.

Soil Property	Stratum					
	Made Ground	Head Deposits	London Clay			
SPT 'N' Value	-	10 -25	18 – 26			
Undrained Shear Strength (kN/m <sup>2</sup> )	-	-	51 - 82			
Bulk Density (mg/m <sup>3</sup> )	1.70(1)	1.80(1)	1.96 - 2.03			
Moisture Content (%)	15 - 20	12	19 – 29			
Plasticity Index (%)	-	-	44			
pH	7.2	8.4	8.3			
Sulphate (g/l)	0.018	0.065	0.55			

(1) Value based on BS8002

A plot of SPT 'N' value against depth is provided in **Appendix D.** 

The plot indicates that there is a fairly uniform correlation between depth and relative density (SPT N Value).

### Geotechnical Advice

#### INTRODUCTION

The temple currently comprises a main building of approximately three storey height with a rear single storey height extension. It is understood that the proposed development will comprise demolition of the existing structure and construction of a new mixed use four storey structure that will include a single storey basement.

On this basis, it the following assumptions have been made:

- The finished floor level of the basement will be -2.80m.
- The load from the existing structure will be in the region of 10-15kN/m<sup>2</sup> (rear extension) to 30-40KN/m<sup>2</sup> (main building).
- For the existing structure (including the roof) the wall load is estimated at approximately 60-80kN/m run.
- The new development will comprise a four-storey structure that will include a single storey basement. Assuming a weight from the new development of 12.5kN/m<sup>2</sup> / per storey (Tomlison, MJ 2001) that will equate to approximately 62.5kN/m<sup>2</sup>.
- There will be no significant changes in elevation over the proposed basement development.
- Foundations will not be eccentrically loaded.

#### GROUND CONDITIONS SUMMARY AND ENGINEERING PARAMETERS

The ground conditions encountered in the exploratory holes comprise Made Ground overlying firm clay and gravelly clay (interpreted as Head Deposits), which rest on the firm becoming stiff London Clay.

Groundwater associated with the Head Deposits was recorded at a depth of approximately 1.64m bgl during monitoring. The groundwater is considered to form a thin but laterally continuous aquifer unit within the Head Deposits.

#### FOUNDATION DESIGN

#### **Non-piled Foundations**

Based on the information supplied, the finished floor level is at 2.80m bgl and it has been estimated that this would equate to a formation level of approximately 3.30m bgl. However, the presence of shallow groundwater within the Head Deposits is likely to preclude formation of foundations at this depth.

As such it has been assumed that formation level for foundations will be extended through the Head Deposits to the top of the underlying London Clay Formation at a depth of c.4.50m bgl.

Based on the findings of the ground investigation and the subsequent laboratory testing it has been concluded that for a traditional spread or raft foundations placed within the London Clay at the assumed formation level (4.50m bgl) a net safe bearing pressure of 140kN/m<sup>2</sup> should be available. The bearing pressure is based on a factor of safety of 3 to ensure that settlement remains within normally acceptable limits.

Foundations should be placed on the firm to stiff cohesive London Clay deposits present at the site and it is recommended that the undrained shear strength of soils at formation level be confirmed using a hand shear vane and should exceed 60kN/m<sup>2</sup>.

The above advice assumes that the proposed basement development and in particular foundations would not be within the influence of any trees or tree routes.

#### **Piled Foundations**

Based on the proposed basement development and the ground conditions encountered it is possible that a piled foundation would be an economic and feasible solution.

At present, there is no information regarding the actual loads for the proposed building and at this stage the assessment of the likely pile capacities has been undertaken purely as an illustration of the feasibility of a piled solution and possible pile capacities.

A factor of safety (FOS) of 2.5 has been adopted in the following preliminary pile design. A lower FOS may be adopted but this will require preliminary and working pile tests and the approval of the local District Surveyor.

Based on the ground investigation data the following preliminary pile design is provided and should be confirmed and/or amended by a competent piling contractor.

Founding De	epth (m)	Pile Diameter (mm)	Safe Working Load (kN)	Founding Stratum
10		450	263	Stiff London Clay Formation.
		600	371	

The actual pile design will depend on a number of factors including the particular details of the piling system to be adopted. The advice of a specialist piling contractor should be sought such that the final design of the piles can be undertaken and the suitability of the particular piling system can be considered. All information relating to the site should be provided to the piling contractor. The piling contractor should review all information available for the site and confirm that the information is adequate to complete the design of the piles or undertake further investigation as required.

The specialist piling contractor should consider noise and vibration and confirm the technique proposed is acceptable for the site and any impact on adjacent structures.

In addition, it is likely that due to the presence of groundwater, the retaining wall will need to be formed by the use of sheet piling or a secant pile wall and this is discussed in the further sections.

#### **GROUND STABILITY & RETAINING STRUCTURES**

The boreholes remained stable during the investigation but in BH2 there was some collapse following removal of casing and walls constructed in open cut are unlikely to be feasible for this situation. The instability is believed to be related to groundwater ingress from the Head Deposits.

The groundwater is considered to form a thin but laterally continuous aquifer unit within the Head Deposits and sustained inflows would be anticipated into any open excavations taken through the aquifer unit. This is supported by anecdotal information from site personnel at the adjacent site

To prevent inflow of groundwater and to enable construction of the basement and retaining wall it is recommended that consideration is given to the following:

- Use of temporary or permanent sheet piles that would be carried through the Head Deposits and 'keyed' into the firm to stiff London Clay below formation level.
- Use of a secant piles for formation of the basement retaining wall that would be carried through the Head Deposits and 'keyed' into the firm to stiff London Clay below formation level.

A discussion of potential heave, settlement and inward yielding is provided in the next section, however it is likely that any excavations will need to be trimmed back following heave of clay at formation level.

In addition, zones loosened by the removal of existing and relict construction may be particularly unpredictable and liable to collapse.

It would be beneficial to install the basement retaining wall and floor slab sequentially to provide propping and/or lateral restraint, which could help to minimise deflections.

Safe working conditions should be ensured where persons are required to work in excavations. It is recommended that reference be made to CIRIA Report No. 97,"Trenching Practice" 1992.

Strata	Depth Range (m bgl)		Effective Angle of Shear Resistance <sup>(2)</sup>	Coefficient of Active Earth Pressure (Ka) <sup>(2)</sup>	Coefficient of Earth Pressure at rest (Kr) <sup>(3)</sup>	Coefficient of Passive Earth Resistance (Kp)	Bulk Density
	Тор	Base				(2)	
Made Ground	Ground Level	0.50 – 0.80	28	0.35	0.75	3.5	1.70(1)
Head Deposits	0.50 – 0.80	3.65 - 3.75	30	0.30	0.75	4.0	1.80 <sup>(1)</sup>
London Clay Formation	3.65 – 3.75	15.00	22	0.40	1.0	2.5	1.96 - 2.03

The parameters presented in the table below may be considered within the design of retaining walls.

(1) Assumed value based on literature information.

- (2) Based on soil properties and reference to BS8002 & Tomlinson, M.J. (1986) for a free standing wall.
- (3) Based on soil properties and reference to BS8002 & Tomlinson, M.J. (1986) for an embedded wall.

#### **BURIED CONCRETE**

In accordance with BRE Special Digest 1 (2005), the results indicate that the following design sulphate classes and Aggressive Chemical Environment for Concrete (ACEC) classes would apply:

Strata	Design Sulphate Class	ACEC Class
Made Ground	DS-1	AC-1s
Head Deposits	DS-1	AC-1s
London Clay Formation	DS-2	AC-2

#### ADDITIONAL CONSIDERATIONS

#### **Existing Structures**

It is recommended that any existing buried construction that will underlie the new development is broken out and removed. However, if buried construction (such as existing foundations) are to remain close to the new structure then care should be taken to avoid interaction i.e. to prevent the slab 'breaking its back' over the existing construction.

#### **Potential for Heave, Settlement & Inward Yielding**

Although the laboratory testing on the Head Deposits suggests that it is not high plasticity, the London Clay near assumed formation level is known to have high plasticity indices with a high volume change potential.

The removal of the overburden during the excavation of the basement is likely to result in heave and inward yielding of the London Clay soils at formation level and possibly a subsequent settlement of the soils outside the excavation. Based on the ground investigation data, the London Clay at formation level is anticipated to comprise firm to stiff clay and so the potential effects maybe limited by their relatively low compressibility (as compared to soft clay soils). Inward yielding in firm to stiff clays is typically in the range of 5-40mm (Tomlinson, M.J. (1986).

The total uplift will be a function of the soil heave pressure and water pressure, it is anticipated that almost half of this will be immediate upon excavation, while the remainder would be long term. The estimated depth of excavation is between 3.50m and 4.50m below current ground level, assuming an unsaturated unit weight of 20kN/m<sup>3</sup> and accounting for groundwater within the Head Deposits, the estimated unload due to the excavation would be in the order of 60kN/m<sup>2</sup> to 80kN/m<sup>2</sup>

It is anticipated that following excavation and construction of the basement, the load imposed by the new substructure will be less than the overburden pressure at formation prior to excavation.

However, it is anticipated the basement slab would not be loaded if strip footings are adopted. In this case a suspended basement floor slab would be appropriate, constructed with suitable compressible void formers that can accommodate the expected ground heave.

As outlined, the basement is estimated to extend beneath the majority of the footprint of the site but there will be areas outside the basement. As such, there will be a difference in load at formation level between the area inside and outside the basement, which could result in differential heave over the long term.

This means there is the potential for longer term heave of the London Clay soils at formation level following basement construction.

#### Groundwater

As outlined, groundwater was encountered during the ground investigation works and recorded in the Head Deposits at approximately 1.64m bgl during monitoring.

The groundwater is considered to form a laterally continuous aquifer unit that is possibly confined and it is considered prudent to adopt a conservative approach in relation to the basement design and account for groundwater at a depth of approximately 1.00m bgl.

Based on the information presented above it is recommended that the basement design takes into account the following:

- The potential for short term and long term heave and inward yielding during construction and following construction.
- The potential for differential heave that will occur in the areas of the basement and areas where the basement doesn't extend.
- The potential for groundwater to cause both lateral and uplift pressure.
- The potential for groundwater ingress into the basement following construction.

#### **Management of Formation Level**

Should pockets of inferior material be present during the inspection of the foundation excavation, they should be removed and replaced with well graded, well compacted hardcore or lean mix concrete. The excavated surface should be protected from deterioration and a blinding layer of concrete used where foundations are not completed without delay. Any surface or perched water should not be allowed to collect in the base of excavations since the clay is prone to rapid deterioration in the presence of water, with loss of their favourable bearing properties.

#### **Groundwater Management**

It is presumed that the retaining wall would be constructed to act as a 'cut-off' to groundwater ingress. However, some dewatering should be anticipated during the construction of the basement and foundations. Assuming the retaining wall is installed prior to excavation then inflow of groundwater is likely to be dealt with by pumping from sumps. Should this not be the case then a larger dewatering system is likely to be required.

#### **Potential Project Risk**

It should be noted that the excavation of the basement may undermine the adjacent property and could lead to settlement in gardens and damage to buildings and below ground services. It is recommended that the principle contractor should allow for suitable mitigation measures that may include:

- A survey of existing ground levels and buildings;
- A survey of existing below ground services,
- Monitoring of adjacent buildings during construction
- Monitoring of adjacent ground levels during construction.
- Careful construction planning to deal with the above potential issues and potential groundwater ingress during construction.

### **REFERENCES & GUIDANCE**

### **REFERENCES & GUIDANCE**

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 $<sup>^1</sup>$  This document has been withdrawn but is considered to remain useful in proving technical background for designing ground investigation works.

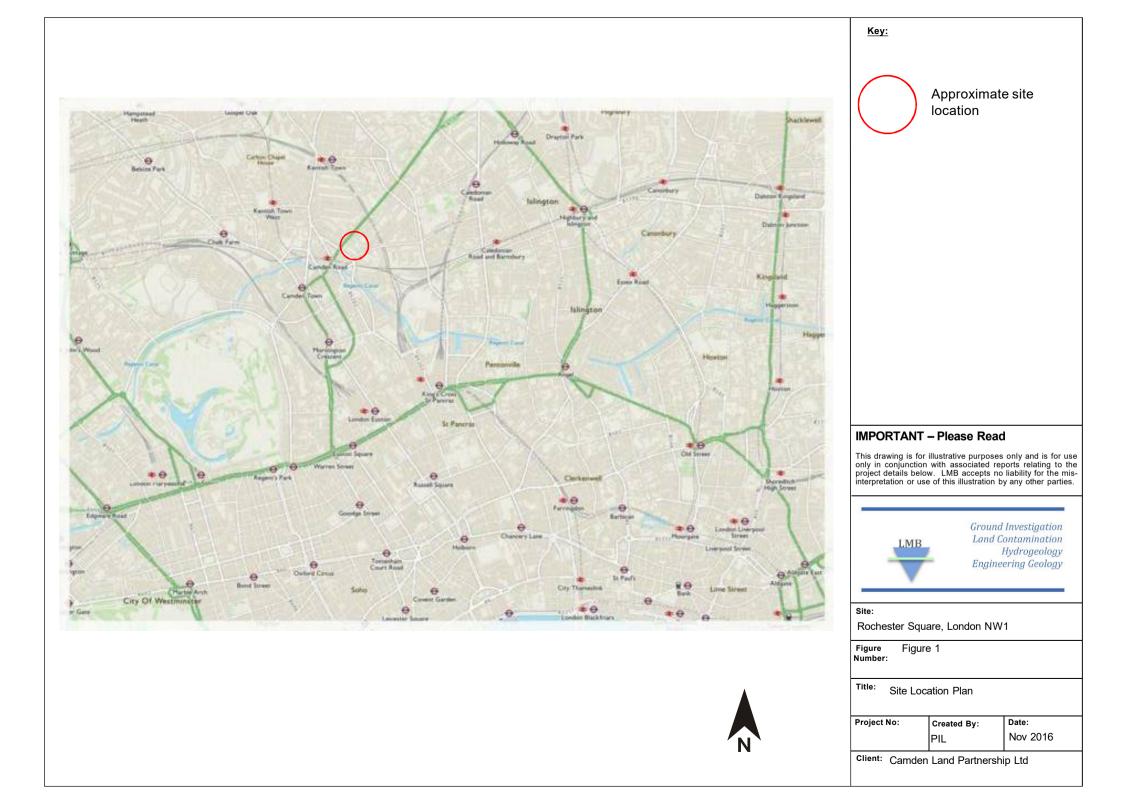
<sup>&</sup>lt;sup>2</sup> This document has been withdrawn but is considered to remain useful in proving technical background for designing ground investigation works.

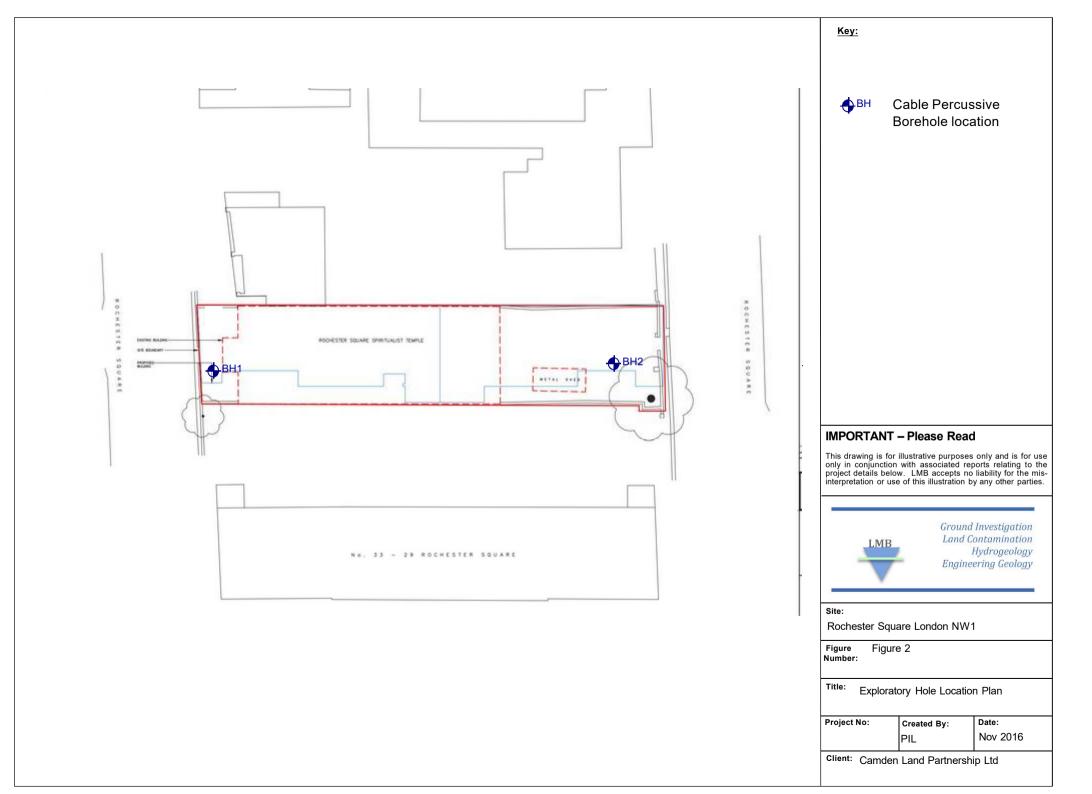
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# FIGURES

### FIGURES





# APPENDICES

# Appendices

APPENDIX A EXPLORATORY HOLE LOGS

LMB	ound Investigation nd Contamination Hydrogeology gineering Geology				Bo	reho	ole Log	Borehole N BH1 Sheet 1 of	
oject Nan	ne: Rocheste	r Squai	<b>Δ</b>	Project No. ₋MB_Roche	ster	Co-ords:	-	Hole Typ CP	е
ocation:	Rocheste	r Squai	re, London NW1			Level:		Scale 1:50	
ient:	Camden I	and P	artnerships Ltd			Dates:	22/11/2016 - 22/11/2016	Logged B	Зy
Wate	er Sample	s and	In Situ Testing	Depth	Level			PIL	Т
ell Strike	es Depth (m)	Туре	Results	(m)	(m)	Legend	Stratum Description	1	
	0.50	ES		0.05			Concrete. MADE GROUND: dark brown slight slightly gravelly clay. Gravel sub-an medium brick and occasional grave broken tile and brick. Soft becoming firm brown to light br (HEAD DEPOSITS).	gular fine to I.	
	1.20 1.20	В	N=10 (1,1/2,2,3,3)						
	2.00 2.00	D	N=25 (4,5/5,6,7,7)	1.75			Firm brown to light brown gravelly ( sub-angular to rounded fine to coar (HEAD DEPOSITS).		
	3.00 3.00	В	N=21 (6,5/6,6,4,5)	3.65					
	4.00	U					Firm becoming stiff brown with occa grey veining CLAY. Closely fissured CLAY FORMATION). becomes stiff.		
	5.00 5.00	D	N=18 (2,2/3,4,5,6)						
	6.50	U					occasional rare orange/brown silty partings		
	8.00 8.00	D	N=18 (3,4/4,4,5,5)						
	9.50	U		8.75			Stiff becoming very stiff dark grey/b with rare fine white shell gravel. Ver fissured. (LONDON CLAY FORMAT	y closely	_

LMB	Borehole Log						Borehole No. BH1 Sheet 2 of 2		
ojec	t Name:	Rochester	Squar		Project No. .MB_Roche	stor	Co-ords:	-	Hole Type CP
catio	on:	Rochester	Squar	e, London NW1		3101	Level:		Scale 1:50
ent:		Camden L	and Pa	artnerships Ltd			Dates:	22/11/2016 - 22/11/2016	Logged By
ell	Water	Samples	s and I	n Situ Testing	Depth	Level	Logond		PIL
	Strikes	Depth (m)	Туре	Results	(m)	(m)	Legend	Stratum Description	1
		11.00 11.00	D	N=21 (3,4/5,5,5,6)					1
		12.50	U						1
		14.55 14.55	D	N=26 (3,4/5,6,7,8)					1
~ ~ ~ ~					15.00			End of borehole at 15.00 n	1
									1
									1
									1
mar	ks								2

LMB Land C	Investigation ontamination lydrogeology rring Geology				ole Log	Borehole No. BH2 Sheet 1 of 2			
roject Name	: Rochester	Squar		Project No. .MB_Roche	ster	Co-ords:	-	Hole Type CP	e
ocation:	Rochester	Squar	e, London NW1			Level:		Scale 1:50	
lient:	Camden L	and Pa	artnerships Ltd			Dates:	21/11/2016 - 21/11/2016	Logged B	y
, "Water	Samples	s and I	n Situ Testing	Depth	Level	<u> </u>			Γ
Vell Strikes	Depth (m)	Туре	Results	(m)	(m)	Legend	Stratum Description		
	0.30 0.50 1.20 1.20	ES B D	N=14 (1,2/2,3,3,6)	0.15 0.50 1.50			MADE GROUND: dark brown slight with numerous rootlets and occasion gravel. MADE GROUND: brown to light brov rare angular fine to medium brick gr Soft becoming firm light brown to br (HEAD DEPOSITS).	wn clay with avel. own CLAY.	-
	2.00 2.00	В	N=18 (3,5/3,5,4,6)				grey mottling very gravelly CLAY. Gr angular to rounded fine to coarse fli DEPOSITS).	ravel sub-	
	3.00 3.00	D	N=19 (7,5/5,4,4,6)						
	4.00	U		3.75			Firm becoming stiff brown with occa orange/brown sandy partings CLAY fissuring visible. (LONDON CLAY Fo	Some close	-
	5.00 5.00	D	N=17 (2,3/3,4,4,6)				becomes very closely fissured and stiff.		
	6.50	U							
	8.00 8.00	D	N=18 (2,3/4,4,5,5)						
	9.50	U		9.50			Stiff becoming very stiff dark grey C closely fissured. (LONDON CLAY F		-

AGS

LMB Land Co	Investigation ntamination lydrageology ring Geology				Bo	reho	ole Log	Borehole No. BH2 Sheet 2 of 2
oject Name:	Rochester	Squar		roject No. MB_Roche	ster	Co-ords:	-	Hole Type CP
ation:	Rochester	Squar	e, London NW1	—		Level:		Scale 1:50
nt:	Camden L	and Pa	artnerships Ltd			Dates:	21/11/2016 - 21/11/2016	Logged By
Water	Sample	s and	n Situ Testing	Depth	Level	Legend	Stratum Descriptior	
"Strikes	Depth (m)	Туре	Results	(m)	(m)			1
	11.00 11.00	D	N=22 (3,4/4,5,6,7) N=28 (3,4/6,6,7,9)	15.00			End of borehole at 15.00 m	11 12 13 14 14 14 14 14 14 14 15 14 15 15 15 15 15 15 15 15 15 15
marks er level at	1.40m in ope	n hole	overnight.					AGS

APPENDIX B GEOTECHNICAL LABORATORY RESULTS



### TEST CERTIFICATE

#### **Determination of Moisture Content**

Tested in Accordance with BS 1377-2:1990: Clause 3.2

Client:LMB Geosolutions LtdClient Address:28 Dresden Road<br/>London<br/>N19 3BDContact:Philip LewisSite Name:Rochester SquareSite Address:Not Given

#### **Test results**

i2 Analytical Ltd 7 Woodshots Meadow Croxley Green Business Park Watford Herts WD18 8YS



Client Reference:	16-33913
Job Number:	16-33913
Date Sampled:	Not Given
Date Received:	22/11/2016
Date Tested:	01/12/2016
Sampled By:	PIL

Laboratory Reference	Sample Reference	Location	Depth Top [m]	Depth Base [m]	Sample Type	Description	Moisture Content [%]
664320	Not Given	BH1	2	Not Given	D	Yellowish brown gravelly clayey SAND	12
664322	Not Given	BH1	5	Not Given	D	Brown CLAY	29

Remarks

Approved:

Mirosława Pytlik PL Head of Geotechnical Section

Date Reported: 05/12/2016

Signed:

Sushil Sharda Technical Manager (Geotechnical Division)

Schorta

for and on behalf of i2 Analytical Ltd

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The results included within the report are representative of the samples submitted for analysis.

The analysis was carried out at i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland."

	Detern	ninatio	n of L	<u>iquid</u>		Plastic			7 W Crox Wat	dey Gr	al Ltd ots Mea een Bu erts WI	sines	ss Pa	rk Env	ironmental Scien
4041 Client: Client Address: Contact: Site Name: Site Address:	28 Dres Londor N19 3B Philip L	eosolution sden Road BD .ewis ster Squar	s Ltd I	377-2: 19	90: Claus	e 4.4 & 5:		nt Metr	Clie	Job N Date Sa ate Re Date	erence: lumber: ampled: eceived: Tested: bled By:	: 16 : N : 22 : 0 <sup>7</sup>	1/12/2	013 ven 2016	
TEST RESUL Description: Location: Sample Prepara	Yellowi BH1 ation:	sh brown y N/A	Samp gravelly		ence: AND	664320 Not Gir	/en				Dep Depth	th To n Bas		]: ]: Not	D 2 Given
As Received Content		Liq	uid Lin [%]	nit	PI	astic Lir [%]	nit	F	lastic I	ity In [%]	dex	%		-	l 425µm Sieve
12	. [ /0]		N/A		NP					N/A			00	N/A	
- 000 - 00 - 00 - 00 - 00 - 00 - 00 - 0	•-664320 0 10	CL 20 3			Сн МН 60	,			<b>CE</b> <b>ME</b> 100	110	120	130		ine	150
		Legend, base C Cla M Silt	y	930:2015 (	Code of pra Plasticity L Lov I Me H Hig	ctice for site v dium		tions	Liquid L below 3 35 to 50 50 to 70 70 to 90	5					

Remarks Sample unsuitable for the Atterberg test

Approved:

Mirosława Pytlik PL Head of Geotechnical Section

Minomawa Bythis

Organic

Signed:

append to classification for organic material ( eg CHO )

Sushil Sharda Technical Manager (Geotechnical Division)

exceeding 90

Schorta

Date Reported:

05/12/2016

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Е

0

Extremely high

Page 1 of 1

#### for and on behalf of i2 Analytical Ltd

	Detern		ST CER <sup>-</sup> n of Liqui		<u>E</u> astic Limit	i2 Analytical Ltd 7 Woodshots Me Croxley Green Bu Watford Herts W	usiness Park
U K A S TESTING	Tested in A	ccordance w	vith BS1377-2:	1990: Clause 4	4.4 & 5: One Point	Method	
4041 Client: Client Address:	28 Dres Londor N19 3E	BD	Ltd				r: 16-33913 I: Not Given I: 22/11/2016
Contact: Site Name: Site Address:	Philip L Roches Not Giv	ster Square				Date Testec Sampled By	
TEST RESUL Description: Location: Sample Prepara	Brown BH1	CLAY	aboratory Ref Sample Ref natural condit	erence:	664322 Not Given	Dep	mple Type: D oth Top [m]: 5 h Base [m]: Not Given
As Received Content		-	iid Limit [%]	Plas	stic Limit [%]	Plasticity Index [%]	% Passing 425µm BS Test Sieve
29					33	44	100
100 -							
90 -		_	_				A line
80 -							
70 - 60 -						CE	
<b>X INDE</b> 50 - 40 -					CV	ME	
40 -				CH	• 664322 MV		
- 30 - 20 -			CI	мн			
10 -		CL	MI				
0 -	) 10	20 30		0 60	70 80 90	) 100 110 120	130 140 150
				LIC	QUID LIMIT		
		Logona, babba	01120 0000.201	Plasticity L Low	-	Liquid Limit below 35 35 to 50	
		C Clay M Silt		I Mediu H High V Very h E Extren		50 to 70 70 to 90 exceeding 90	

Approved:

Mirosława Pytlik PL Head of Geotechnical Section

Minemawa Mythis

Signed:

Sushil Sharda Technical Manager (Geotechnical Division)

Schorta

Date Reported:

05/12/2016

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#### for and on behalf of i2 Analytical Ltd

#### TEST CERTIFICATE

#### Summary of Classification Test Results

i2 Analytical Ltd 7 Woodshots Meadow Croxley Green Business Park Watford Herts WD18 8YS



Client Reference: 16-33913 Job Number: 16-33913 Date Sampled: Not Given Date Received: 22/11/2016 Date Tested: 01/12/2016 Sampled By: PIL

#### Test results

Site Address:

Client:

Contact: Site Name:

Client Address:

			Sa	mple	-		Der	nsity	M/C		Atte	nberg	-	PD
Laboratory Reference	Hole No.	Reference	Top depth [m]	Base depth [m]	Туре	Soil Description	bulk	dry	101/0	% Passing 425um	LL	PL	PI	
							Mg/m3	Mg/m3	%	%	%	%	%	Mg/m3
664320	BH1	Not Given	2.00	Not Given	D	Yellowish brown gravelly clayey SAND	-	-	12	N/A	NP	N/A	N/A*	-
664322	BH1	Not Given	5.00	Not Given	D	Brown CLAY	-	-	29	100	77	33	44	-

Comments: \* Sample unsuitable for the Atterberg test

LMB Geosolutions Ltd

28 Dresden Road

Rochester Square

London

N19 3BD

Philip Lewis

Not Given

Minomawa Bythis

Mirosława Pytlik PL Head of Geotechnical Section

Approved:

05/12/2016 Date Reported:

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Signed:

Division)

Schorta

Sushil Sharda Technical Manager (Geotechnical

for and on behalf of i2 Analytical Ltd

		Det		T CERTIFIC	<u>CATE</u> Size Distributio	i2 Analytical Ltd 7 Woodshots Meado Croxley Green Busin Watford Herts WD18	ess Park	
Clie		ddress:	ested in Accordanc LMB Geosoluti 28 Dresden Ro London N19 3BD	ons Ltd	art 2:1990, clause 9.2	Job Number:	Environmental Scient 16-33913 16-33913 Not Given	ce
Site	ntact: e Nan e Add		Philip Lewis Rochester Squ Not Given	are		Date Tested:	22/11/2016 07/11/3718 PIL	
Sai Loc			n: Yellowish	y Reference: brown slightly	664323 sandy gravelly CLAY	Sample Reference: Sample Type: Depth Top [m]: Depth Base [m]:	Not Given B 2 Not Given	
	-	CLAY	SILT ine Medium	Coarse Fine	SAND Medium Coarse	GRAVEL Fine Medium Coarse	COBBLES BOULDERS	-
Percentage Passing %		D01	0.01	0.1	I Particle Size	10 mm Dry Mass of sample [g]:		000
		125 90	100 100			Sample Proportions Very coarse	% dry mass 0.00	$\neg$
		75 63	100 100			Gravel Sand	53.40 20.50	
		50	100					
		37.5 28	100 97			Fines <0.063mm	26.10	
		20	90			Grading Analysis	n 37.5	
		14 10	79 71			D100 mr D60 mr	F 75	
		6.3	62			D30 mr	0.000	_
	—	5 3.35	57 52		+	D10 mr Uniformity Coefficient	n	_
		2	47			Curvature Coefficient		
		1.18 0.6 0.425 0.3 0.212	41 35 32 30 29			Remarks Preparation and testing in accordance	e with BS1377 unless noted belo	w
		0.15	28					
		0.063	26					

Approved:

Minonawa Bythis

Mirosława Pytlik PL Head of Geotechnical Section

Date Reported: 05/12/2016

Signed:

Sushil Sharda Technical Manager (Geotechnical Division)

S. Growth

for and on behalf of i2 Analytical Ltd

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### **Total Stress Triaxial Compression**

### Unconsolidated Undrained (Single Stage)

#### Summary Report

Sample Details	Depth Description Type	4.00 Yellowish b U	rown CLAY w	vith thin laminae of grey clay
	Initial Sample Length Initial Sample Diameter	Lo Do	(mm) (mm)	199.0 98.2
sketch showing specimen location in original sample	Initial Sample Weight Bulk Density Particle Density	VVο ρο ρs	(gr) (Mg/m3) (Mg/m3)	2994.1 1.99 2.65
Initial Conditions				
Initial Cell Pressure		σз	(kPa)	80
Strain Rate		ms	(mm/min)	3.98020
MembraneThickness		mь	(mm)	0.27
Displacement Input		LIP	(mm)	CH 2
Load Input		N IP	(N)	CH 1
Initial Moisture		ω;%	(%)	31
Initial Dry Density		Obβ	(Mg/m3)	1.51
Initial Voids Ratio		eo		0.75
Initial Degree of Saturation		So	(%)	100
Final Conditions				
Max Deviator Stress		(σ1-σ3)f	(kPa)	102
MembraneCorrection		m c	(kPa)	0.337
Strain At Max Stress		ε <sub>f</sub> %	(%)	3.28
Shear Strength		CU	(kPa)	51
Final Moisture		ω <b>ŕ</b> %	(%)	31
Final Dry Density		ρdf	(Mg/m3)	1.51
Final Voids Ratio		ef		0.75
Final Degree of Saturation		Sf	(%)	100.0
Notes				
Triaxial at over burden				
				Failura Skatah

Failure Sketch

(surface inclination)

	Test Method	BS1377-7 : 1990 C PRESS \ 6171-I2 A		Test Name Test Date	664321 01/12/2016	
lytical	Site Reference	Rochester Square	•	Borehole	BH1	
	Jobfile	16-33913		Sample	664321	
Environmental Science	Client Operator pa	LMB Geosolutions		Depth	4.00 Approved	pytlikm

i2 Analytical Limited, 7 Woodshots Meadow, Croxley Green Business Park, Herts WD18 8YS i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### **Total Stress Triaxial Compression**

### Unconsolidated Undrained (Single Stage)

#### **Summary Report**

Sample Details	Depth	4.00			
	Description		rown CLAY w	ith thin laminae o	f grey clay
	Туре	U			
	Initial Sample Length	Lo	(mm)	198.6	
	Initial Sample Diameter	Do	(mm)	98.8	
sketch showing specimen	Initial Sample Weight	Wo	(gr)	2979.4	
location in original sample	Bulk Density Particle Density	ρο ρs	(Mg/m3) (Mg/m3)	1.96	
		P>	(109/113)	2.65	
Initial Conditions					
Initial Cell Pressure		σ3	(kPa)	80	
Strain Rate		ms	(mm/min)	3.97220	
MembraneThickness		mь	(mm)	0.28	
Displacement Input		LIP	(mm)	CH 2	
Load Input		N IP	(N)	CH 1	
Initial Moisture		ω;%	(%)	32	
Initial Dry Density		ΟbΟ	(Mg/m3)	1.48	
Initial Voids Ratio		eo		0.79	
Initial Degree of Saturation		So	(%)	100	
Final Conditions					
Max Deviator Stress		(σ1-σ3)f	(kPa)	161	
MembraneCorrection		тc	(kPa)	0.893	
Strain At Max Stress		۶f%	(%)	11.36	
Shear Strength		сU	(kPa)	81	1 Andrews
Final Moisture		ωf%	(%)	32	Rest I
Final Dry Density		ρdf	(Mg/m3)	1.48	
Final Voids Ratio		ef		0.79	
Final Degree of Saturation		Sf	(%)	100.0	Martin Martin

Notes Triaxial at over burden Failure Sketch (surface inclination)

	Test Method	BS1377-7 : 1990 (	Clause 8		Test Name	664324	
8	Database: .\SQLE	XPRESS \ 6171-I2 A	nalytical		Test Date	01/12/2016	
	Site Reference	Rochester Square	9		Borehole	BH2	
	Jobfile	16-33913			Sample	664324	
	Client	LMB Geosolutions	s Ltd		Depth	4.00	
Environmental Science	Operator p	almowskia	Checked	pytli	km	Approved	pytlikm

palmowski CII eckeu i2 Analytical Limited, 7 Woodshots Meadow, Croxley Green Business Park, Herts WD18 8YS i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland

### **Total Stress Triaxial Compression**

### Unconsolidated Undrained (Single Stage)

#### Summary Report

Sample Details	Depth	9.50			
	Description	Brown CLA	Y		
	Туре	U			
	Initial Sample Length	Lo	(mm)	196.6	
	Initial Sample Diameter	Do	(mm)	97.9	
	Initial Sample Weight	Wo	(gr)	3010.2	
sketch showing specimen	Bulk Density	ρο	(Mg/m3)	2.03	
location in original sample	Particle Density	ρs	(Mg/m3)	2.65	
Initial Conditions					
Initial Cell Pressure		σ3	(kPa)	190	
Strain Rate		ms	(mm/min)	3.93260	
MembraneThickness		mь	(mm)	0.29	
Displacement Input		LIP	(mm)	CH 2	
Load Input		N IP	(N)	CH 1	
Initial Moisture		ω i%	(%)	29	
Initial Dry Density		ρdΟ	(Mg/m3)	1.58	
Initial Voids Ratio		eo		0.68	
Initial Degree of Saturation		So	(%)	100	
Final Conditions					
Max Deviator Stress		(σ1-σ3)f	(kPa)	164	
MembraneCorrection		тc	(kPa)	0.500	Comments and and and
Strain At Max Stress		ε <sub>f</sub> %	(%)	5.28	
Shear Strength		сU	(kPa)	82	1 C

Strain At Max Stress	6 f 70	(%)	5.28	
Shear Strength	сU	(kPa)	82	A
Final Moisture	ω <del>1</del> %	(%)	29	
Final Dry Density	ρdf	(Mg/m3)	1.58	
Final Voids Ratio	ef		0.68	
Final Degree of Saturation	Sf	(%)	100.0	
Notes				
Triaxial at over burden				
			Failure Sketc	h
			(surface inclin	ation)

		Test Method	BS1377-7 : 1	990 Clause 8		Test Name	664325		
	7	Database: .\SQ	LEXPRESS \ 617	I-I2 Analytical		Test Date	01/12/2016		
	jä ja	Site Reference	Rochester S	quare		Borehole	BH2		
	₩ <sup>2</sup>	Jobfile	16-33913			Sample	664325		
		Client	LMB Geosol	utions Ltd		Depth	9.50		
	Environmental Science	Operator	palmowskia	Checked	pvtli	km	Approved	pytlikm	

i2 Analytical Limited, 7 Woodshots Meadow, Croxley Green Business Park, Herts WD18 8YS i2 Analytical Limited, ul. Pionierow 39, 41-711 Ruda Slaska, Poland APPENDIX C CHEMICAL LABORATORY TESTING RESULTS



Philip Lewis LMB Geosolutions Ltd 28 Dresden Road London N19 3BD



i2 Analytical Ltd. 7 Woodshots Meadow, Croxley Green Business Park, Watford, Herts, WD18 8YS

t: 01923 225404 f: 01923 237404 e: reception@i2analytical.com

e: philip@lmbgeosolutions.com

# Analytical Report Number : 16-33916

Project / Site name:	Rochester Square	Samples received on:	22/11/2016
Your job number:		Samples instructed on:	23/11/2016
Your order number:		Analysis completed by:	02/12/2016
Report Issue Number:	1	Report issued on:	02/12/2016

Samples Analysed:

4 soil samples

Signed:

Rexona Rahman Reporting Manager For & on behalf of i2 Analytical Ltd.

Signed:

Emma Winter Assistant Reporting Manager For & on behalf of i2 Analytical Ltd.

Standard Geotechnical, Asbestos and Chemical Testing Laboratory located at: ul. Pionierów 39, 41 -711 Ruda Śląska, Poland.

Accredited tests are defined within the report, opinions and interpretations expressed herein are outside the scope of accreditation.

Standard sample disposal times, unless otherwise agreed with the laboratory, are :

soils	<ul> <li>4 weeks from reporting</li> </ul>
leachates	- 2 weeks from reporting
waters	- 2 weeks from reporting
asbestos	- 6 months from reporting

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Project / Site name: Rochester Square

Lab Sample Number				664337	664338	664339	664340	
Sample Reference			BH1	BH1	BH2	BH2		
Sample Number				None Supplied	None Supplied	None Supplied	None Supplied	
Depth (m)				5.00	0.50	0.30	2.00	
Date Sampled				Deviating	Deviating	Deviating	Deviating	
Time Taken	-			None Supplied	None Supplied	None Supplied	None Supplied	
Analytical Parameter (Soil Analysis)	Units	Limit of detection	Accreditation Status					
Stone Content	%	0.1	NONE	< 0.1	< 0.1	< 0.1	< 0.1	
Moisture Content	%	N/A	NONE	19	15	20	12	
Total mass of sample received	kg	0.001	NONE	0.25	0.86	1.1	0.49	
Asbestos in Soil	Туре	N/A	ISO 17025	-	Not-detected	Not-detected		
Asbestos III Soli	туре	IN/A	150 17025	-	Not-delected	NUI-UELELLEU	<u> </u>	
General Inorganics								
pH - Automated	pH Units	N/A	MCERTS	8.3	-	7.2	8.4	
Water Soluble SO4 16hr extraction (2:1 Leachate	prionits	19/5	PICENTS	0.5		1.2	0.1	
Equivalent)	g/l	0.00125	MCERTS	0.55	-	0.018	0.065	
	v.	-	-	-	-	-		
Speciated PAHs								
Naphthalene	mg/kg	0.05	MCERTS	-	-	< 0.05	-	
Acenaphthylene	mg/kg	0.1	MCERTS	-	-	< 0.10	-	
Acenaphthene	mg/kg	0.1	MCERTS	-	-	< 0.10	-	
Fluorene	mg/kg	0.1	MCERTS	-	-	< 0.10	-	
Phenanthrene	mg/kg	0.1	MCERTS	-	-	0.42	-	
Anthracene	mg/kg	0.1	MCERTS	-	-	< 0.10	-	
Fluoranthene	mg/kg	0.1	MCERTS	-	-	0.97	-	
Pyrene	mg/kg	0.1	MCERTS	-	-	0.86	-	
Benzo(a)anthracene	mg/kg	0.1	MCERTS	-	-	0.51	-	
Chrysene	mg/kg	0.05	MCERTS	-	-	0.53	-	
Benzo(b)fluoranthene	mg/kg	0.1	MCERTS	-	-	0.46	-	
Benzo(k)fluoranthene	mg/kg	0.1	MCERTS	-	-	0.25	-	
Benzo(a)pyrene	mg/kg	0.1	MCERTS	-	-	0.34	-	
Indeno(1,2,3-cd)pyrene	mg/kg	0.1	MCERTS	-	-	< 0.10	-	
Dibenz(a,h)anthracene	mg/kg	0.1	MCERTS	-	-	< 0.10	-	
Benzo(ghi)perylene	mg/kg	0.05	MCERTS	-	-	< 0.05	-	
Total PAH								
Speciated Total EPA-16 PAHs	mg/kg	1.6	MCERTS	-	-	4.34	-	
Herer Metels / Metellaide								
Heavy Metals / Metalloids	ma = //	1	MCEDIC	-	20	13		
Arsenic (aqua regia extractable)	mg/kg	_	MCERTS	-	28		-	
Boron (water soluble)	mg/kg	0.2	MCERTS	-	1.0	2.0	-	
Cadmium (aqua regia extractable)	mg/kg	0.2	MCERTS		< 0.2 27	< 0.2 38	-	
Chromium (aqua regia extractable)	mg/kg	1	MCERTS	-	27 97	<u>38</u> 65	-	
Copper (aqua regia extractable)	mg/kg		MCERTS	-	-		-	
Lead (aqua regia extractable)	mg/kg	1	MCERTS		610	360		
Mercury (aqua regia extractable)	mg/kg	0.3	MCERTS	-	1.8	1.2	-	
Nickel (aqua regia extractable)	mg/kg	1	MCERTS	-	25	24		
Selenium (aqua regia extractable)	mg/kg	1	MCERTS	-	< 1.0	< 1.0	-	
Zinc (aqua regia extractable)	mg/kg	1	MCERTS	-	150	140	-	
Petroleum Hydrocarbons	iiig/kg	1	MCERTS		150	140		

Petroleum Hydrocarbons								
TPH C10 - C40	mg/kg	10	MCERTS	-	-	< 10	-	





#### Project / Site name: Rochester Square

\* These descriptions are only intended to act as a cross check if sample identities are questioned. The major constituent of the sample is intended to act with respect to MCERTS validation. The laboratory is accredited for sand, clay and loam (MCERTS) soil types. Data for unaccredited types of solid should be interpreted with care.

Stone content of a sample is calculated as the % weight of the stones not passing a 10 mm sieve. Results are not corrected for stone content.

Lab Sample Number	Sample Reference	Sample Number	Depth (m)	Sample Description *
664337	BH1	None Supplied	5.00	Brown clay.
664338	BH1	None Supplied	0.50	Brown loam and clay with gravel and vegetation.
664339	BH2	None Supplied	0.30	Brown loam and clay with gravel and vegetation.
664340	BH2	None Supplied	2.00	Light brown sandy clay.





Project / Site name: Rochester Square

Water matrix abbreviations: Surface Water (SW) Potable Water (PW) Ground Water (GW)

Analytical Test Name	Analytical Method Description	Analytical Method Reference	Method number	Wet / Dry Analysis	Accreditation Status
Asbestos identification in soil	Asbestos Identification with the use of polarised light microscopy in conjunction with disperion staining techniques.	In house method based on HSG 248	A001-PL	D	ISO 17025
Boron, water soluble, in soil	Determination of water soluble boron in soil by hot water extract followed by ICP-OES.	In-house method based on Second Site Properties version 3	L038-PL	D	MCERTS
Metals in soil by ICP-OES	Determination of metals in soil by aqua-regia digestion followed by ICP-OES.	In-house method based on MEWAM 2006 Methods for the Determination of Metals in Soil.	L038-PL	D	MCERTS
Moisture Content	Moisture content, determined gravimetrically.	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests	L019-UK/PL	W	NONE
pH in soil (automated)	Determination of pH in soil by addition of water followed by automated electrometric measurement.	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests	L099-PL	D	MCERTS
Speciated EPA-16 PAHs in soil	Determination of PAH compounds in soil by extraction in dichloromethane and hexane followed by GC-MS with the use of surrogate and internal standards.	In-house method based on USEPA 8270	L064-PL	D	MCERTS
Stones content of soil     Standard preparation for all samples unless otherwise detailed. Gravimetric determination of stone > 10 mm as % dry weight.		In-house method based on British Standard Methods and MCERTS requirements.	L019-UK/PL	D	NONE
Sulphate, water soluble, in soil (16hr extraction)	Determination of water soluble sulphate by ICP- OES. Results reported directly (leachate equivalent) and corrected for extraction ratio (soil equivalent).	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests, 2:1 water:soil extraction, analysis by ICP- OES.	L038-PL	D	MCERTS
TPH Banding in Soil by FID	Determination of hexane extractable hydrocarbons in soil by GC-FID.	In-house method, TPH with carbon banding.	L076-PL	W	MCERTS

For method numbers ending in 'UK' analysis have been carried out in our laboratory in the United Kingdom. For method numbers ending in 'PL' analysis have been carried out in our laboratory in Poland. Soil analytical results are expressed on a dry weight basis. Where analysis is carried out on as-received the results obtained are multiplied by a moisture correction factor that is determined gravimetrically using the moisture content which is carried out at a maximum of 30oC.



Sample ID	Other_ID	Sample Type	Job	Sample Number	Sample Deviation Code	test_name	test_ref	Test Deviation code
BH1		S	16-33916	664337	а			
BH1		S	16-33916	664338	а			
BH2		S	16-33916	664339	а			
BH2		S	16-33916	664340	а			



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e: philip@Imbgeosolutions.com

## Analytical Report Number : 16-33918

Project / Site name:	Rochester Square	Samples received on:	22/11/2016
Your job number:		Samples instructed on:	23/11/2016
Your order number:		Analysis completed by:	05/12/2016
Report Issue Number:	1	Report issued on:	05/12/2016

Signed:

Samples Analysed:

Rexona Rahman Reporting Manager For & on behalf of i2 Analytical Ltd.

M Signed:

Emma Winter Assistant Reporting Manager For & on behalf of i2 Analytical Ltd.

Standard Geotechnical, Asbestos and Chemical Testing Laboratory located at: ul. Pionierów 39, 41 -711 Ruda Śląska, Poland.

Accredited tests are defined within the report, opinions and interpretations expressed herein are outside the scope of accreditation.

Standard sample disposal times, unless otherwise agreed with the laboratory, are :

1 10:1 WAC sample

soils	- 4 weeks from reporting
leachates	- 2 weeks from reporting
waters	- 2 weeks from reporting
asbestos	- 6 months from reporting

Excel copies of reports are only valid when accompanied by this PDF certificate.

12	Analytical

7 Woodshots Meadow Croxley Green Business Park Watford, WD18 8YS

Report No:		16-3	3918				
					Client:	LMBGEOSOL	
Location		Rocheste	er Square				
Lab Reference (Sample Number)		664345	/ 664346		Landfill	Waste Acceptanc	e Criteria
Sampling Date		Devia				Limits Stable Non-	
Sample ID		BH				reactive	
Depth (m)		0.!			Inert Waste Landfill	HAZARDOUS waste in non- hazardous Landfill	Hazardous Waste Landfi
Solid Waste Analysis							
FOC (%)**	1.3				3%	5%	6%
loss on Ignition (%) **	-						10%
3TEX (μg/kg) **	-				6000		
Sum of PCBs (mg/kg) **	-				1		
Mineral Oil (mg/kg)	-				500		
Fotal PAH (WAC-17) (mg/kg)	-				100		
oH (units)**	8.4					>6	
Acid Neutralisation Capacity (mol / kg)	6.1					To be evaluated	To be evaluat
iluate Analysis	10:1			10:01	Limit valu	es for compliance le	eaching test
PC EN 12457 2 proparation utilising and over and leaching					using BS EN	12457-2 at L/S 10	) l/kg (mg/kg)
(BS EN 12457 - 2 preparation utilising end over end leaching procedure)	mg/l			mg/kg	-		
	0.0202			0.446	0.5		25
Arsenic *	0.0203			0.146	0.5	2	25
Barium *	0.0321			0.230	20	100	300
Cadmium * Chromium *	< 0.0001 0.0054			< 0.0008	0.04	1 10	5
Copper *	0.0054			0.039	2	50	100
Mercury *	< 0.0005			< 0.0050	0.01	0.2	2
Molybdenum *	0.0030			0.0218	0.5	10	30
Vickel *	0.0027			0.019	0.4	10	40
_ead *	0.036			0.26	0.5	10	50
Antimony *	0.0027			0.019	0.06	0.7	5
Selenium *	< 0.0040			< 0.040	0.1	0.5	7
Zinc *	0.019			0.14	4	50	200
Chloride *	0.84			6.0	800	4000	25000
Fluoride	0.51			3.7	10	150	500
Sulphate *	3.2			23	1000	20000	50000
TDS	33			240	4000	60000	100000
Phenol Index (Monhydric Phenols) *	< 0.010			< 0.10	1	-	-
200	3.75			26.9	500	800	1000
Leach Test Information							
Stone Content (%)	< 0.1						
Sample Mass (kg)	0.86						
Dry Matter (%)	85						
Aoisture (%)	15						
tesults are expressed on a dry weight basis, after correction for moisture content v							



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#### Project / Site name: Rochester Square

\* These descriptions are only intended to act as a cross check if sample identities are questioned. The major constituent of the sample is intended to act with respect to MCERTS validation. The laboratory is accredited for sand, clay and loam (MCERTS) soil types. Data for unaccredited types of solid should be interpreted with care.

Stone content of a sample is calculated as the % weight of the stones not passing a 10 mm sieve. Results are not corrected for stone content.

'	Lab Sample Number	Sample Reference	Sample Number	Depth (m)	Sample Description *
	664345	BH1	None Supplied	0.50	Brown loam and clay with gravel and vegetation.





Project / Site name: Rochester Square

#### Water matrix abbreviations: Surface Water (SW) Potable Water (PW) Ground Water (GW)

Analytical Test Name	Analytical Method Description	Analytical Method Reference	Method number	Wet / Dry Analysis	Accreditation Status
Acid neutralisation capacity of soil	Determination of acid neutralisation capacity by addition of acid or alkali followed by electronic probe.	In-house method based on Guidance an Sampling and Testing of Wastes to Meet Landfill Waste Acceptance""	L046-UK	W	NONE
BS EN 12457-2 (10:1) Leachate Prep	Prep 10:1 (as recieved, moisture adjusted) end over end In-house method based on BSEN12457-2. extraction with water for 24 hours. Eluate filtered prior to analysis.		L043-PL	W	NONE
Chloride 10:1 WAC	Determination of Chloride colorimetrically by In house based on MEWAM Method ISBN discrete analyser. 0117516260.		L082-PL	W	ISO 17025
Dissolved organic carbon 10:1 WAC	Determination of dissolved inorganic carbon in leachate by TOC/DOC NDIR Analyser. In-house method based on Examination of Water and Wastewater 20th Edition: Clesceri, Greenberg & Eaton		L037-PL	W	NONE
Fluoride 10:1 WAC	Determination of fluoride in leachate by 1:1ratio       In-house method based on Use of Total         with a buffer solution followed by Ion Selective       Ionic Strength Adjustment Buffer for         Electrode.       Electrode Determination"		L033-PL	w	NONE
Metals in leachate by ICP-OES	Determination of metals in leachate by acidification followed by ICP-OES.	In-house method based on MEWAM 2006 Methods for the Determination of Metals in Soil""	L039-PL	w	ISO 17025
Moisture Content	Moisture content, determined gravimetrically.	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests	L019-UK/PL	W	NONE
Monohydric phenols 10:1 WAC	Determination of phenols in leachate by distillation followed by colorimetry.	In-house method based on Examination of Water and Wastewater 20th Edition: Clesceri, Greenberg & Eaton	L080-PL	W	ISO 17025
pH in soil	Determination of pH in soil by addition of water followed by electrometric measurement.	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests	L005-PL	W	MCERTS
Stones content of soil	Standard preparation for all samples unless otherwise detailed. Gravimetric determination of stone > 10 mm as % dry weight.	In-house method based on British Standard Methods and MCERTS requirements.	L019-UK/PL	D	NONE
Sulphate 10:1 WAC	Determination of sulphate in leachate by ICP-OES	In-house method based on MEWAM 1986 Methods for the Determination of Metals in Soil""	L039-PL	w	ISO 17025
Total dissolved solids 10:1 WAC	Determination of total dissolved solids in water by electrometric measurement.	In-house method based on Examination of Water and Wastewater 20th Edition: Clesceri, Greenberg & Eaton	L004-PL	W	NONE
Total organic carbon in soil	Determination of organic matter in soil by oxidising with potassium dichromate followed by titration with iron (II) sulphate.	In-house method based on BS1377 Part 3, 1990, Chemical and Electrochemical Tests	L023-PL	D	MCERTS

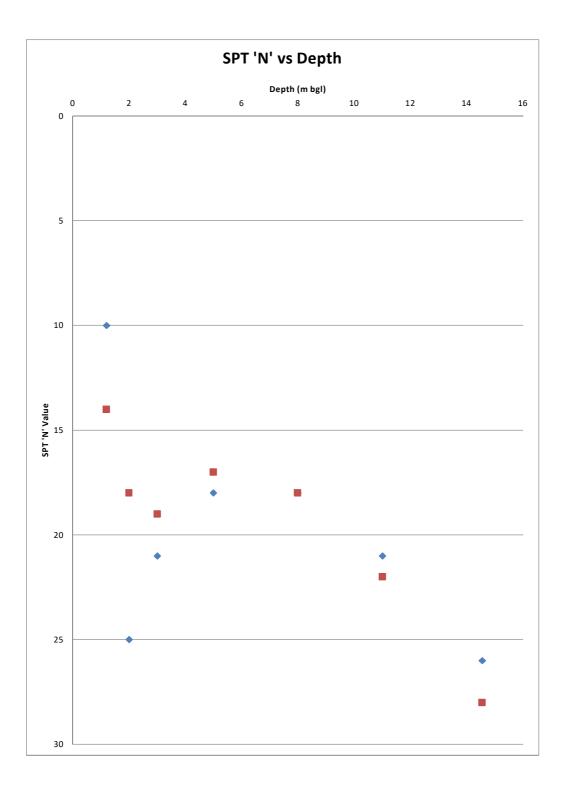
For method numbers ending in 'UK' analysis have been carried out in our laboratory in the United Kingdom. For method numbers ending in 'PL' analysis have been carried out in our laboratory in Poland. Soil analytical results are expressed on a dry weight basis. Where analysis is carried out on as-received the results obtained are multiplied by a moisture correction factor that is determined gravimetrically using the moisture content which is carried out at a maximum of 30oC.



Sample ID	Other_ID	Sample Type	Job	Sample Number	Sample Deviation Code	test_name	test_ref	Test Deviation code
BH1		L	16-33918	664346	а			
BH1		S	16-33918	664345	а			

# APPENDICES

APPENDIX D PLOT OF SPT 'N' VLAUE VS DEPTH



# LMB GEOSOLUTIONS LTD

#### SPT N DEPTH PLOT

Project:Rochester Square Spiritualist TempleClient:Camden Land Partnership LtdLogged By:PIL

	SPT N			
Depth	BH1	BH2		Geol
	1.2	10	14	HD
	2	25	18	HD
	3	21	19	HD
	5	18	17	LC
	8	18	18	LC
	11	21	22	LC
14	4.55	26	28	LC