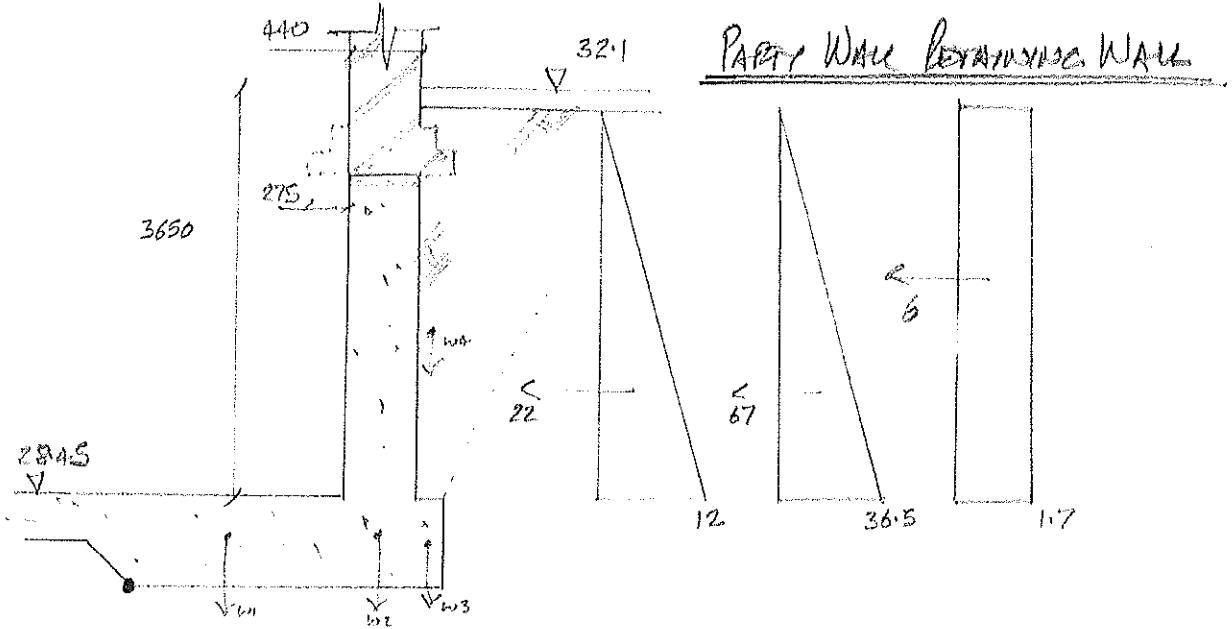




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Job Title
 13 PRINCE ALBERT ROAD



VERTICAL LOAD DOWN PARTY WALL : DL = 157 kN/m
 LL = 20 kN/m

R.C. WALL PL. : $0.44 \times 24.5 \times 3.5 = 38 \text{ kN/m}$

$K_A = 0.33$

SATURATED SOIL : $(3.65 \times 10) \times 0.33 = 12 \text{ kN/m}^2$

WATER : $3.65 \times 10 = 36.5 \text{ kN/m}^2$

SURCHARGE : $5 \times 0.33 = 1.7 \text{ kN/m}^2$

$$\therefore \text{BM} = (22 \times 1.2) + (67 \times 1.2) + (6 \times 1.8)$$

$$= 118 \text{ kNm/m}$$

$$d = 440 - 50 = 390$$

$$K = 118 \times 10^6 / (10500 \times 390^3) = 0.35$$

$$A_s = 118 \times 10^6 / (0.95 \times 460 \times 0.94 \times 390) = 737 \text{ mm}^2/\text{m}$$

PROVIDE : 116 - 150 VERTICAL BARS $1340 \text{ mm}^2/\text{m}$ ✓



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 13 PRINCE ALBERT ROAD

BEARING PRESSURES

NOTE IN THE PERMANENT STATE THE BASEMENT R.C. SLAB WILL RESIST ROTATION AND PROVIDE HORIZONTAL SUPPORT. HOWEVER CIRC BEARING PRESSURES IN BANK CONDITIONS. PROPPING WILL BE PROVIDED FOR SLIDING.

$$\hat{v}_M = 118 \text{ kNm/m}$$

$$\hat{M}_1 = w_1 = (24 \times 0.75 \times 1.965) \times 0.98 = 35$$

$$w_2 = (157.38) \times 1.47 = 228$$

$$w_3 = (0.275 \times 0.75 \times 24) \times 1.83 = 9$$

$$\Sigma \underline{331 \text{ kNm/m}}$$

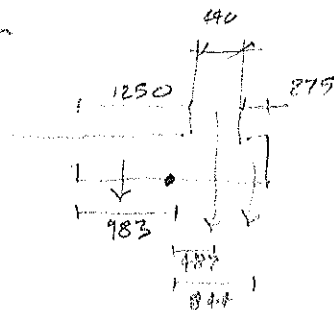
$$\therefore \text{F.O.S} = 2.8 \therefore \text{O.K.} \checkmark$$

MOMENTS ABOUT CENTRE OF BASE:

$$\hat{M} = (157.38) \times 0.49 + (0.275 \times 0.75 \times 24) \times 0.94 = 99.7 \text{ kNm}$$

$$\hat{v}_M = 118 \text{ kNm/m} + (0.98 \times 0.75 \times 24) \times 0.49 = 127 \text{ kNm}$$

$$\therefore \text{NET } \hat{v}_M = 27 \text{ kNm/m}$$





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Job Title
13 PRINCE ALBERT ROAD

$$\begin{aligned} \text{TOTAL VERTICAL LOAD DOWN STBM} &= 157 + 20 + 38 \\ &= 215 \text{ kN (CHAR)} \end{aligned}$$

$$D = 1.97 \text{ m}$$

$$p_{\text{toe}} = \frac{N}{D} + \frac{6M}{D^2} = \frac{215}{1.97} + \frac{6 \cdot 27}{1.97^2} = 151 \text{ kN/m}^2$$

$$p_{\text{heel}} = \frac{N}{D} - \frac{6M}{D^2} = 67 \text{ kN/m}^2$$

FROM SOILS REPORT SAFE BEARING CAPACITY = 160 kN/m²

∴ O.K. IN TEMP CASE AND PERMANENT.

