

# **BEDFORD HOUSE, 21A JOHN STREET, LONDON**

## **NOISE IMPACT ASSESSMENT**

Report 15392.NIA.01 Rev.B

Prepared on 26 January 2017

**For:**

**Benesco Charity Ltd**

**8/10 Hallam Street**

**London**

**W1W 6NS**

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## 1.0 INTRODUCTION

KP Acoustics has been commissioned by Benesco Charity Ltd, 8/10 Hallam Street, London, W1W 6NS, to assess the suitability of Bedford House, 21A John Street, London, for office development in accordance with the provisions of the National Planning Policy Framework and the Noise Policy Statement for England (NPSE).

This report presents the results of the environmental survey undertaken in order to measure prevailing background noise levels and outlines any necessary mitigation measures.

## 2.0 ENVIRONMENTAL NOISE SURVEY

### 2.1 Procedure

A noise survey was undertaken at the positions as shown in Figure 15392.SP1. These locations were chosen in order to collect data representative of the worst-case levels expected on the site due to all nearby sources.

Continuous automated monitoring was undertaken for the duration of the survey between 05/01/17 and 06/01/17.

Weather conditions were generally dry with light winds and therefore suitable for the measurement of environmental noise.

The measurement procedure complied with ISO 1996-2:2007 Acoustics "Description, measurement and assessment of environmental noise - Part 2: Determination of environmental noise levels".

### 2.2 Equipment

The equipment calibration was verified before and after use and no abnormalities were observed.

The equipment used was as follows.

- 2 No. Svantek Type 958 Class 1 Sound Level Meter
- 1 No. Svantek Type 948 Class 1 Sound Level Meter
- B&K Type 4231 Class 1 Calibrator

## 3.0 RESULTS

### 3.1 Noise Survey

$L_{Aeq}$ : 5min,  $L_{Amax}$ : 5min,  $L_{A10}$ : 5min and  $L_{A90}$ : 5min acoustic parameters were measured throughout the duration of the survey. Measured levels are shown time histories in Figures 15392.TH1-3.

Average daytime and night time noise levels are shown in Table 4.1.

#### 4.0 DISCUSSION

The site is bounded by John Street to the East, John's Mews and a school to the West, and existing office and residential properties to all other façades. At the time of the survey, the background noise climate was dominated by road traffic noise from surrounding roads, in addition to existing plant units towards the centre of the site.

Measured noise levels are representative of noise exposure levels expected to be experienced by all façades of the proposed development.

	Level dB(A)
Position 1 (John Street)	
Daytime $L_{Aeq,16hour}$	63
Night-time $L_{Aeq,8hour}$	54
Position 2 (Central Facades)	
Daytime $L_{Aeq,16hour}$	57
Night-time $L_{Aeq,8hour}$	49
Position 3 (John's Mews)	
Daytime $L_{Aeq,16hour}$	56
Night-time $L_{Aeq,8hour}$	46

Table 4.1 Site average noise levels for daytime and night time

#### 5.0 NOISE IMPACT ASSESSMENT

##### 5.1 Noise Assessment

BS8233:2014 "*Sound insulation and noise reduction for buildings*" describes recommended internal noise levels for office spaces. These levels are shown in Table 5.1.

Criterion	Typical Situations	Design range $L_{Aeq,T}$ dB
Study and Work Requiring Concentration	Open Plan Offices Private Offices	35 – 45 35 – 40

Table 5.1 BS8233 recommended internal background noise levels

The external building fabric would need to be carefully designed to achieve these recommended internal levels. It is understood that the non-glazed external building fabric elements of the proposed development would be comprised of blockwork. This would

contribute towards a significant reduction of ambient noise levels in combination with a good quality double-glazed window configuration, as shown in Section 6.

## 6.0 EXTERNAL BUILDING FABRIC SPECIFICATION

Sound reduction performance calculations have been undertaken in order to specify the minimum performance required from glazed and non-glazed elements in order to achieve recommended internal noise levels shown in Table 5.1, taking into account average and maximum noise levels monitored during the environmental noise survey.

Office dimensions from available plans have been used for all glazing calculations for all elevations.

### 6.1 Non-Glazed Elements

All non-glazed elements of the building façade have been assumed to provide a sound reduction performance of at least the figures shown in Table 6.1 when tested in accordance with BS EN ISO, 140-3:1995.

Element	Octave band centre frequency SRI, dB					
	125	250	500	1k	2k	4k
Non glazed element SRI	41	43	48	50	55	55

**Table 6.1 Non-glazed elements assumed sound reduction performance**

### 6.2 Glazed Elements

Minimum octave band sound reduction index (SRI) values required for all glazed elements to be installed are shown in Table 6.2. The performance is specified for the whole window unit, including the frame and other design features such as the inclusion of trickle vents. Sole glass performance data would not demonstrate compliance with this specification.

Glazing performance calculations have been based on average measured daytime noise levels as recommended by BS8233. The most robust results of these calculations are shown in Table 6.2.

Glazing Type	Octave band centre frequency SRI, dB					
	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz
John Street Elevation	15	18	20	25	28	23
Central Elevations	11	13	14	18	18	12
John's Mews Elevations	11	12	15	20	20	15

**Table 6.2 Required glazing performance**

All major building elements should be tested in accordance with BS EN ISO 140-3:1995.

Independent testing at a UKAS accredited laboratory will be required in order to confirm the performance of the chosen system for an “actual” configuration.

No further mitigation measures would be required to achieve recommended internal noise levels.

## **7.0 CONCLUSION**

An environmental noise survey has been undertaken at Bedford House, 21A John Street, London in order to assess noise levels in the area. Measured noise levels have allowed the proposal of a robust glazing specification which would provide internal noise levels for all office environments of the development commensurate to the recommendations of BS8233:2014.

No further mitigation measures should be required in order to protect the proposed offices from external noise intrusion.

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Bedford House, 21A John Street, London  
Environmental Noise Time History  
5th January to 6th January 2017

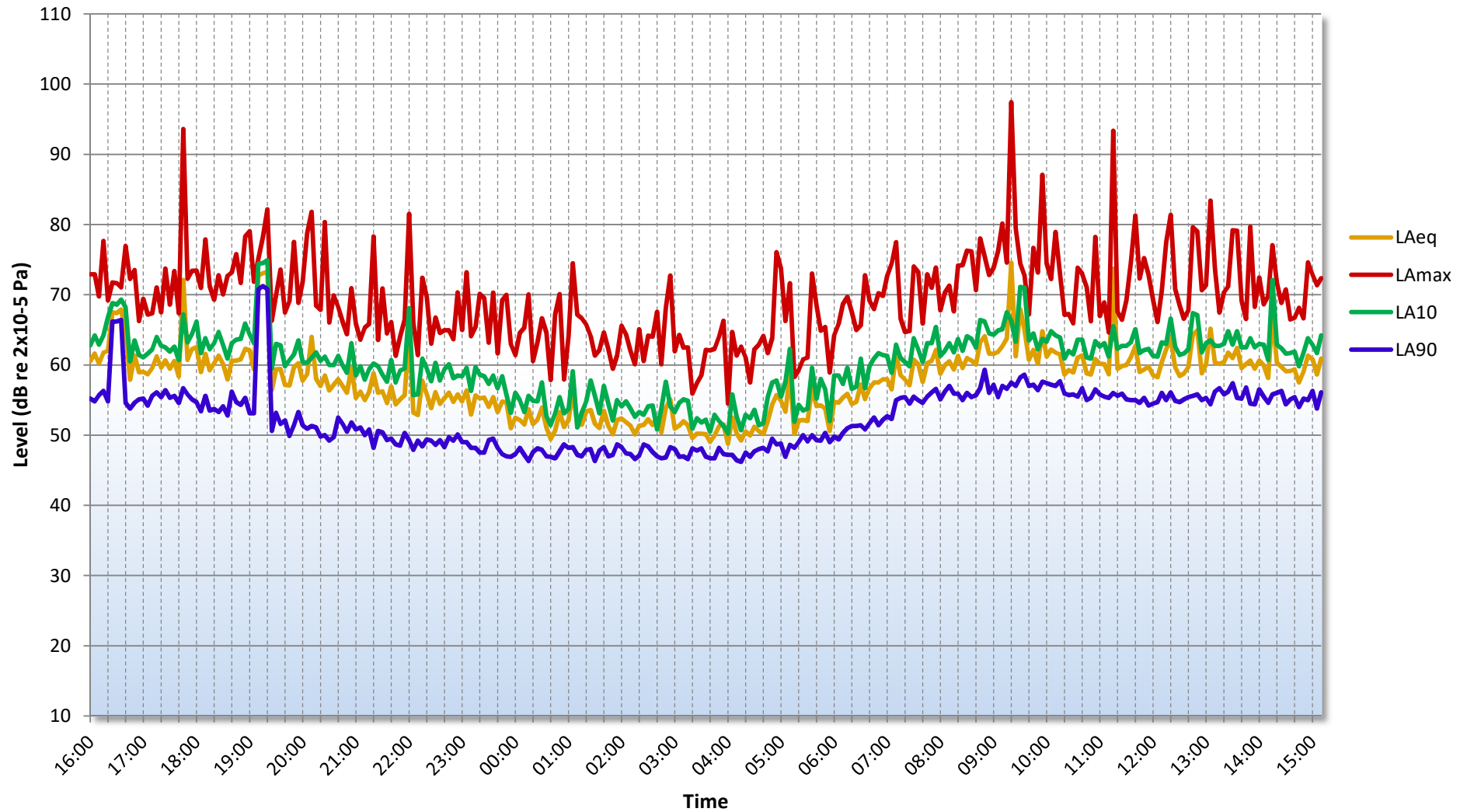


Figure 15392.TH1.Front

Bedford House, 21A John Street, London  
Environmental Noise Time History  
5th January to 6th January 2017

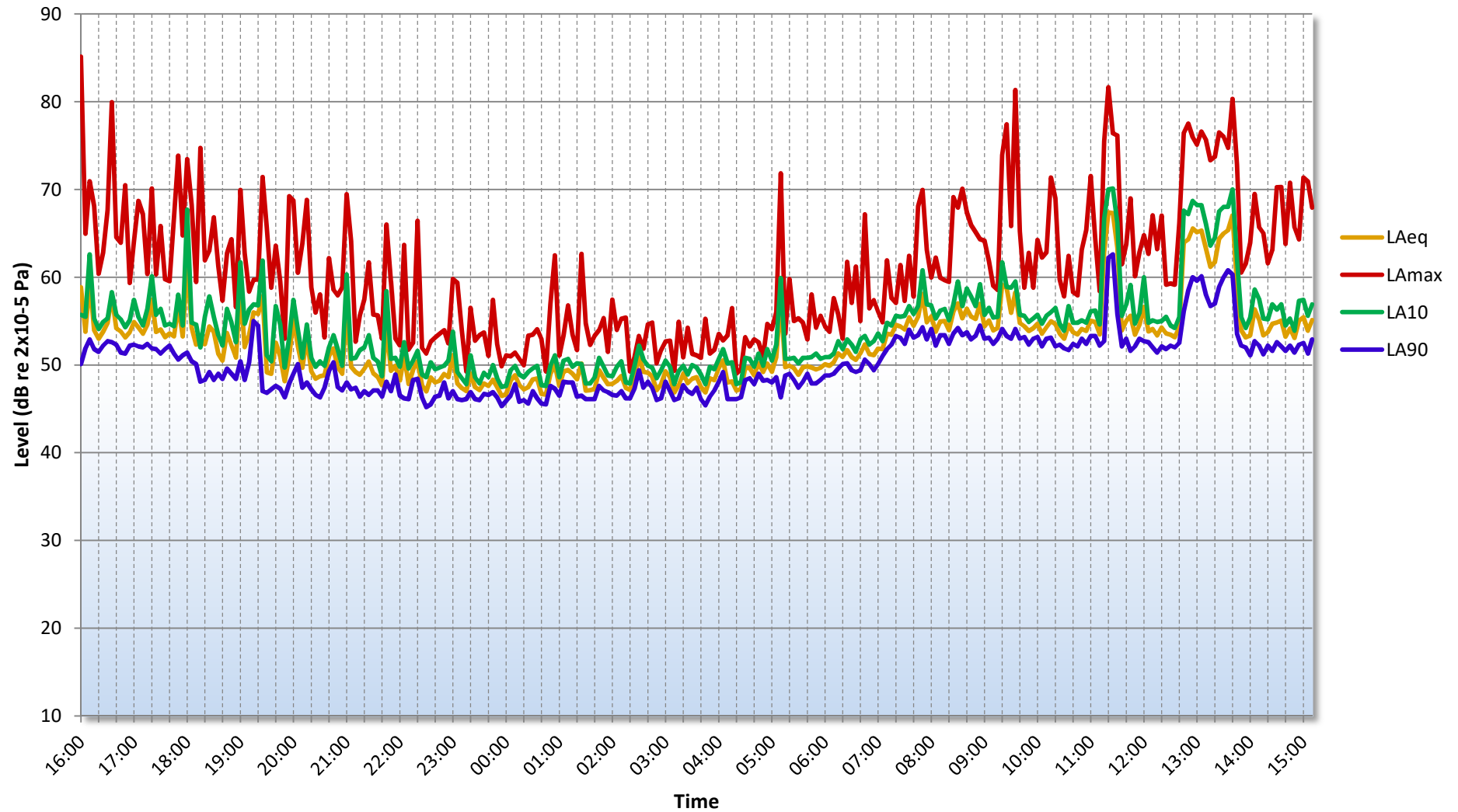


Figure 15392.TH2.Central Facades



Bedford House, 21A John Street, London  
Environmental Noise Time History  
5th January to 6th January 2017

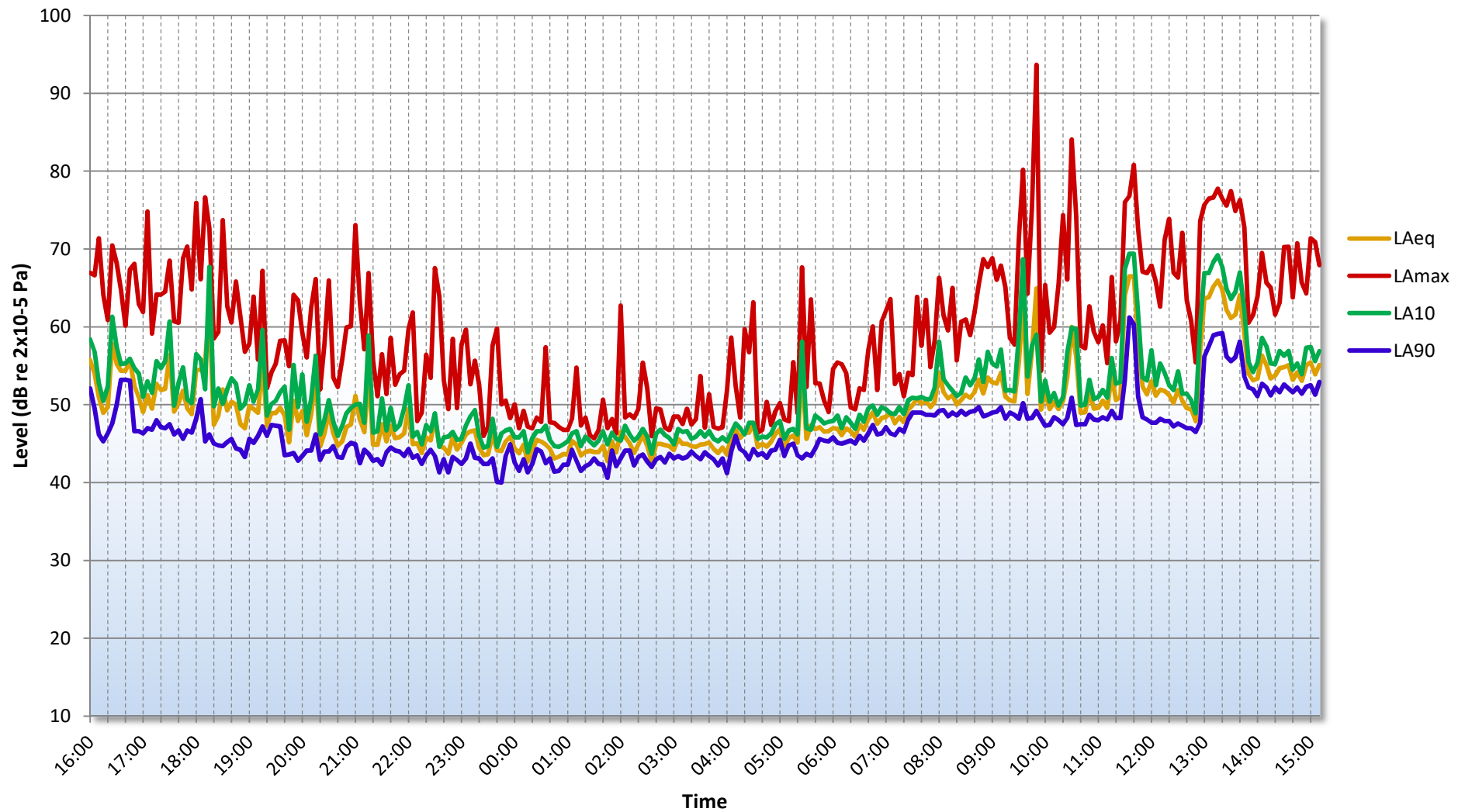
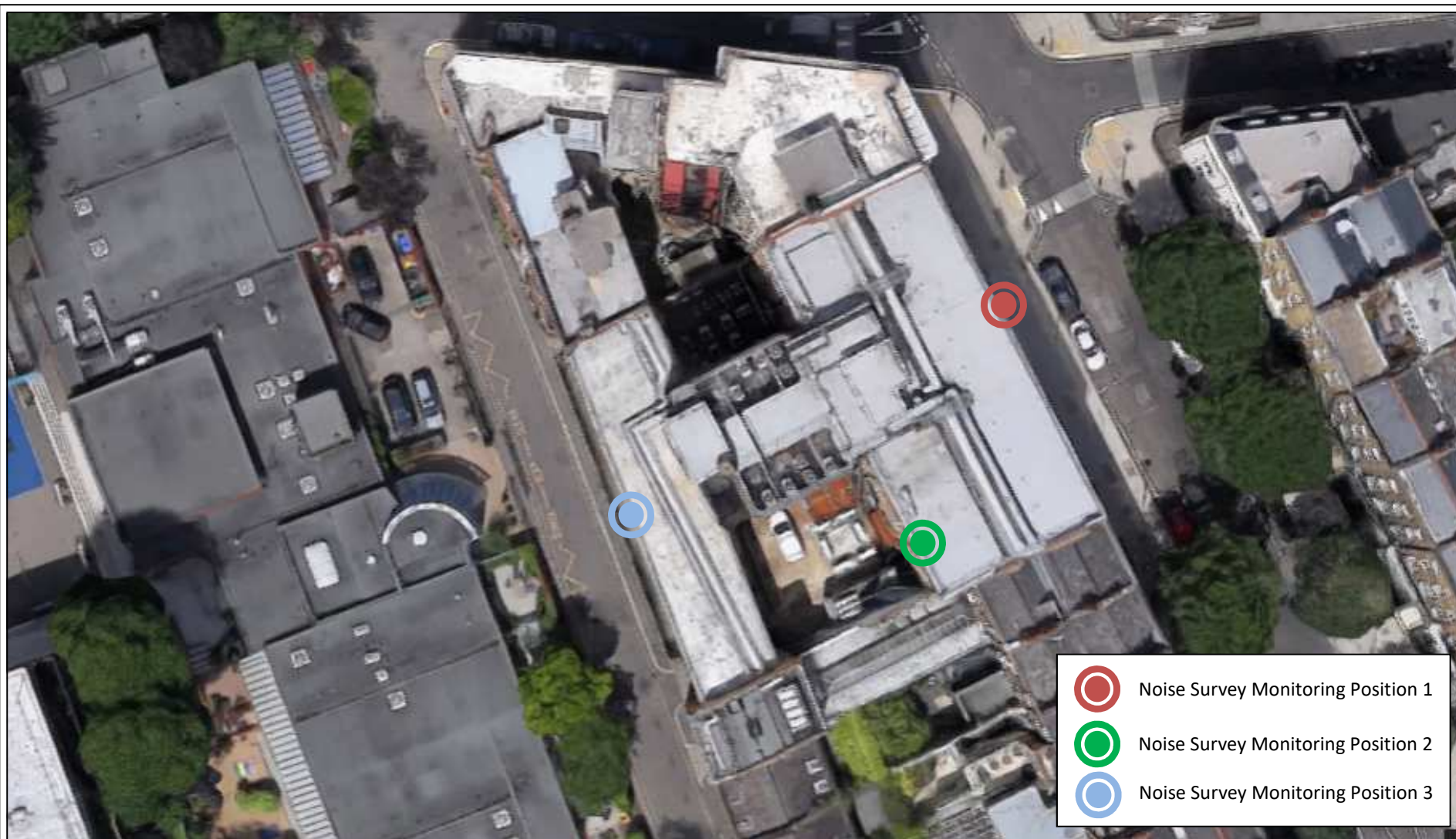


Figure 15392.TH3.Rear Facade



**Title:**

Indicative site plan showing noise monitoring positions  
Ref: Google Maps

**Date:** 18 January 2017

**FIGURE 15392.SP1**



## GENERAL ACOUSTIC TERMINOLOGY

### Decibel scale - dB

In practice, when sound intensity or sound pressure is measured, a logarithmic scale is used in which the unit is the 'decibel', dB. This is derived from the human auditory system, where the dynamic range of human hearing is so large, in the order of  $10^{13}$  units, that only a logarithmic scale is the sensible solution for displaying such a range.

### Decibel scale, 'A' weighted - dB(A)

The human ear is less sensitive at frequency extremes, below 125Hz and above 16Khz. A sound level meter models the ears variable sensitivity to sound at different frequencies. This is achieved by building a filter into the Sound Level Meter with a similar frequency response to that of the ear, an A-weighted filter where the unit is dB(A).

### $L_{eq}$

The sound from noise sources often fluctuates widely during a given period of time. An average value can be measured, the equivalent sound pressure level  $L_{eq}$ . The  $L_{eq}$  is the equivalent sound level which would deliver the same sound energy as the actual fluctuating sound measured in the same time period.

### $L_{10}$

This is the level exceeded for no more than 10% of the time. This parameter is often used as a "not to exceed" criterion for noise.

### $L_{90}$

This is the level exceeded for no more than 90% of the time. This parameter is often used as a descriptor of "background noise" for environmental impact studies.

### $L_{max}$

This is the maximum sound pressure level that has been measured over a period.

### Octave Bands

In order to completely determine the composition of a sound it is necessary to determine the sound level at each frequency individually. Usually, values are stated in octave bands. The audible frequency region is divided into 11 such octave bands whose centre frequencies are defined in accordance with international standards. These centre frequencies are: 16, 31.5, 63, 125, 250, 500, 1000, 2000, 4000, 8000 and 16000 Hertz.

Environmental noise terms are defined in BS7445, *Description and Measurement of Environmental Noise*.

## APPLIED ACOUSTIC TERMINOLOGY

### Addition of noise from several sources

Noise from different sound sources combines to produce a sound level higher than that from any individual source. Two equally intense sound sources operating together produce a sound level which is 3dB higher than a single source and 4 sources produce a 6dB higher sound level.

### Attenuation by distance

Sound which propagates from a point source in free air attenuates by 6dB for each doubling of distance from the noise source. Sound energy from line sources (e.g. stream of cars) drops off by 3dB for each doubling of distance.

### Subjective impression of noise

Hearing perception is highly individualised. Sensitivity to noise also depends on frequency content, time of occurrence, duration of sound and psychological factors such as emotion and expectations. The following table is a guide to explain increases or decreases in sound levels for many scenarios.

Change in sound level (dB)	Change in perceived loudness
1	Imperceptible
3	Just barely perceptible
6	Clearly noticeable
10	About twice as loud

### Transmission path(s)

The transmission path is the path the sound takes from the source to the receiver. Where multiple paths exist in parallel, the reduction in each path should be calculated and summed at the receiving point. Outdoor barriers can block transmission paths, for example traffic noise. The effectiveness of barriers is dependent on factors such as its distance from the noise source and the receiver, its height and construction.

### Ground-borne vibration

In addition to airborne noise levels caused by transportation, construction, and industrial sources there is also the generation of ground-borne vibration to consider. This can lead to structure-borne noise, perceptible vibration, or in rare cases, building damage.

### Sound insulation - Absorption within porous materials

Upon encountering a porous material, sound energy is absorbed. Porous materials which are intended to absorb sound are known as absorbents, and usually absorb 50 to 90% of the energy and are frequency dependent. Some are designed to absorb low frequencies, some for high frequencies and more exotic designs being able to absorb very wide ranges of frequencies. The energy is converted into both mechanical movement and heat within the material; both the stiffness and mass of panels affect the sound insulation performance.