		User Details:				
Assessor Name: Software Name:	George Farr Stroma FSAP 2012	Stroma Nui Software V	ersion:		028460 n: 1.0.4.6	
Address :	Pro	pperty Address: Hous	e 1			
1. Overall dwelling dimer	nsions:					
7. Overall aweiling airrier	iolorio.	Area(m²)	Av. Height(m)	Volume(m³))
Ground floor		650.34 (1a) x	2.97	(2a) =	1931.51	(3a)
First floor		290.69 (1b) x	3.5	(2b) =	1017.42	(3b)
Second floor		175.1 (1c) x	3.27	(2c) =	572.58	(3c)
Third floor		169.13 (1d) x	3.27	(2d) =	553.06	(3d)
Total floor area TFA = (1a	n)+(1b)+(1c)+(1d)+(1e)+(1n)	1285.26 (4)				
Dwelling volume		(3a)+(3	3b)+(3c)+(3d)+(3e)+	(3n) =	4074.56	(5)
2. Ventilation rate:	main secondary heating heating	other	total		m³ per hou	r
Number of chimneys		+ 0 =	0	40 =	0	(6a)
Number of open flues	0 + 0	+ 0 =	0)	(20 =	0	(6b)
Number of intermittent far	ns		0 ,	(10 =	0	(7a)
Number of passive vents			0 ,	(10 =	0	(7b)
Number of flueless gas fir	es		0)	40 =	0	(7c)
				Air ch	anges per ho	ur
Infiltration due to chimney	s, flues and fans = $(6a)+(6b)+(7a)$)+(7b)+(7c) =	0	÷ (5) =	0	(8)
•	en carried out or is intended, proceed			+ (0) =	U	
Number of storeys in th	e dwelling (ns)			[0	(9)
Additional infiltration			[(9	9)-1]x0.1 =	0	(10)
Structural infiltration: 0.2	25 for steel or timber frame or 0	0.35 for masonry cons	struction		0	(11)
if both types of wall are pre deducting areas of opening	esent, use the value corresponding to to	he greater wall area (after				
•	oor, enter 0.2 (unsealed) or 0.1	(sealed), else enter ()	ſ	0	(12)
If no draught lobby, ento	,	(,,,		ļ	0	(13)
Percentage of windows	and doors draught stripped				0	(14)
Window infiltration		0.25 - [0.2 x (14) -	- 100] =	Ī	0	(15)
Infiltration rate		(8) + (10) + (11) +	(12) + (13) + (15) =	Ī	0	(16)
Air permeability value, o	q50, expressed in cubic metres	per hour per square	metre of envelop	e area	3	(17)
If based on air permeabilit	ty value, then $(18) = [(17) \div 20] + (8)$, otherwise (18) = (16)			0.15	(18)
	if a pressurisation test has been done	or a degree air permeabili	ty is being used	_		_
Number of sides sheltered	d	(00) 4 50 075	(40)1	[3	(19)
Shelter factor		(20) = 1 - [0.075 x]		ļ	0.78	(20)
Infiltration rate incorporati		$(21) = (18) \times (20) =$	=	Į	0.12	(21)
Infiltration rate modified for	or monthly wind speed	1 . 1		 		

Mar

Apr

May

Jun

Jul

Sep

Aug

Oct

Nov

Dec

Jan

Feb

22)m=	5.1	5	4.9	4.4	4.3	3.8	3.8	3.7	4	4.3	4.5	4.7		
Wind Fac	ctor (2	2a\m -	(22)m ÷	4										
_	1.27	1.25	1.23	1.1	1.08	0.95	0.95	0.92	1	1.08	1.12	1.18]	
								(5.1.)	(5.5.)		ļ		ı	
· —	0.15	ation rat 0.15	e (allowi	ng for sh 0.13	elter an 0.12	d wind s	peed) 0.11	= (21a) x	(22a)m 0.12	0.12	0.12	0.14	1	
			change i	••••	-	l -		0.11	0.12	0.12	0.13	0.14		
If mecl	hanica	ıl ventila	ition:										0.5	(23a
If exhau	ıst air he	eat pump i	using Appe	endix N, (2	3b) = (23a	a) × Fmv (e	equation	(N5)) , othe	erwise (23b	o) = (23a)			0.5	(23b
If balance	ced with	heat reco	overy: effic	iency in %	allowing f	or in-use f	actor (fr	om Table 4h	n) =				72.25	(23c
				entilation		at recov	- `	VHR) (24	í `	- 	(23b) × [- ` 	÷ 100]	
` ′ ∟	0.29	0.28	0.28	0.27	0.26	0.25	0.25	0.25	0.26	0.26	0.27	0.28		(24a
´ —								(MV) (24I	í `	, 	` 		1	(- 1)
(24b)m=	0	0	0	0	0	0	0	0	0	0	0	0		(24b
,					•	•		tion from (4c) = (22		E v (22)	h)			
(24c)m=	0	0.5 ×	0	0	0 = (23L	0	0	$\frac{(40)}{100} = \frac{(22)}{100}$	T 0	0	0	0	1	(240
					_	l		tion from					J	(= .0
,					•			= 0.5 + [(2		0.5]				
(24d)m=	0	0	0	0	0	0	0	0	0	0	0	0		(24d
Effecti	ve air	change	rate - er	nter (24a	or (24b	o) or (24	c) or (2	24d) in bo	x (25)					
(25)m=	0.29	0.28	0.28	0.27	0.26	0.25	0.25	0.25	0.26	0.26	0.27	0.28		(25)
3. Heat	losses	s and he	eat loss p	oaramete	er:									
ELEME		Gros		Openin		Net Ar	ea	U-val		ΑXU		k-value		Χk
		area	(m²)	m	2	A ,r	n²	W/m2	2K	(W/	′K)	kJ/m²-l	K kJ	
Doors	_					7.58		1.4	=	10.612	2			(26)
Windows						42.16	_	(1/[1/(2.4)+		92.32				(27)
Windows	• •					13.01	<u> </u>	(1/[1/(2.4)	+ 0.04] =	28.49				(27)
Windows	• •					4.35		<1/[1/(1.2)+	+ 0.04] =	4.98				(27)
Windows	s Type	4				51.85	<u> </u>	<1/[1/(1.2)+	+ 0.04] =	59.37				(27)
Floor						650.3	4	0.14	=	91.0476	61			(28)
Walls Ty	pe1	393.	37	0		393.3	7	0.18	=	70.81				(29)
Walls Ty	pe2	491.	94	69.2	1	422.7	3	0.18	=	76.09				(29)
vvalio i y	ma2	142.	97	49.74	1	93.23	3 ;	0.3	=	27.97				(29)
Walls Ty	pes						<i>γ</i> ,	0.12	_	78.04			\neg	(30)
	pes	650.	34	0		650.3	4	0.12	_					
Walls Ty		L		0		650.3 2328.9	=	0.12		7 0.0 .				
Walls Ty Roof Total are	ea of e	lements	s, m² lows, use e	effective wi		2328.9 alue calcul	96	ng formula				n paragraph	1 3.2	
Walls Ty Roof Total are * for windo ** include t	ea of e	lements roof winde	s, m² lows, use e sides of in	effective winternal wall		2328.9 alue calcul	96	ng formula	1/[(1/U-valu			n paragraph		(31)
Walls Ty Roof Total are * for windo ** include t	ea of ellows and the area	lements roof winders on both s, W/K:	s, m² lows, use e sides of in = S (A x	effective winternal wall		2328.9 alue calcul	96	ng formula	1/[(1/U-valu)) + (32) =	ue)+0.04] i	as given in		539.73	(31)
Walls Ty Roof Total are * for windo *** include t Fabric he Heat cap	ea of element and the area eat los pacity (lements roof winders on both s, W/K =	s, m² lows, use e sides of in = S (A x	effective winternal wall	ls and part	2328.9 alue calcul titions	96 ated usi	ng formula	1/[(1/U-valu)) + (32) = ((28).	ue)+0.04] i	as given in 2) + (32a)			(31)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f

can be ເ	ısed instea	ad of a de	tailed calci	ulation.										
Therm	al bridge	es : S (L	x Y) cal	culated	using Ap	pendix l	K						0.08	(36)
	_	,	are not kn		• .	-								` ′
Total fa	abric hea	at loss							(33) +	(36) =			539.81	(37)
Ventila	tion hea	it loss ca	alculated	monthl	y				(38)m	= 0.33 × ((25)m x (5)		_	
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(38)m=	385.86	381.95	378.04	358.5	354.6	335.06	335.06	331.15	342.87	354.6	362.41	370.23		(38)
Heat tr	ansfer c	oefficier	nt, W/K						(39)m	= (37) + (38)m		_	
(39)m=	925.67	921.76	917.85	898.31	894.41	874.87	874.87	870.96	882.68	894.41	902.22	910.04		
Heat Id	oss para	meter (H	HLP), W/	/m²K						Average = = (39)m ÷	Sum(39) ₁ .	12 /12=	897.34	(39)
(40)m=	0.72	0.72	0.71	0.7	0.7	0.68	0.68	0.68	0.69	0.7	0.7	0.71		
Numbe	er of day	s in mor	nth (Tab	le 1a)					,	Average =	Sum(40) ₁	12 /12=	0.7	(40)
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec]	
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31		(41)
						•	•	•			•		-	
4. Wa	iter heat	ing ener	rgy requi	irement:								kWh/y	ear:	
A			\ 1										1	
if TF	ed occu A > 13.9 A £ 13.9	0, N = 1	N + 1.76 x	[1 - exp	(-0.0003	349 x (TF	FA -13.9)2)] + 0.0	0013 x (ΓFA -13.		41	l	(42)
Annua	l averag	e hot wa	ater usaç									39	1	(43)
		_	hot water person per			_	_	to achieve	a water us	se target o	f		•	
notmore	. 1				<u> </u>		•	T .	0				1	
Hot wate	Jan er usage ir	Feb	Mar day for ea	Apr ach month	May <i>Vd.m</i> = fa	Jun ctor from	Jul Table 1c x	Aug (43)	Sep	Oct	Nov	Dec		
(44)m=	152.9	147.34	141.78	136.22	130.66	125.1	125.1	130.66	136.22	141.78	147.34	152.9	1	
(44)111=	102.0	147.04	141.70	100.22	130.00	120.1	120.1	130.00			m(44) ₁₁₂ =		1668.04	(44)
Energy o	content of	hot water	used - cal	culated m	onthly $= 4$.	190 x Vd,ı	m x nm x E	OTm / 3600					1000.04	(\.,
(45)m=	226.75	198.32	204.65	178.42	171.19	147.73	136.89	157.09	158.96	185.25	202.22	219.6]	
					!					Total = Su	m(45) ₁₁₂ =	=	2187.06	(45)
If instant	taneous w	ater heatii	ng at point	of use (no	hot water	r storage),	enter 0 in	boxes (46) to (61)				•	
(46)m=	34.01	29.75	30.7	26.76	25.68	22.16	20.53	23.56	23.84	27.79	30.33	32.94		(46)
	storage e volum		includin	na anv sa	olar or M	MHRS	storana	within s	ame ves	امء		00	1	(47)
•		,	ind no ta	•			_		arric voo	001		00		(47)
	-	_	hot wate		_			. ,	ers) ente	er '0' in (47)			
Water	storage	loss:		`					,	·	,			
a) If m	anufact	urer's de	eclared l	oss facto	or is kno	wn (kWl	n/day):				0.	54]	(48)
Tempe	erature fa	actor fro	m Table	2b							0.	54]	(49)
• • • • • • • • • • • • • • • • • • • •			storage	-				(48) x (49)) =		2.	04]	(50)
•			eclared of factor fr	-								0	1	(E4)
		_	ee secti		EZ (KVV	11/11111 C /Uc	ay <i>)</i>					0	J	(51)
	e factor	-		-								0]	(52)
Tempe	erature fa	actor fro	m Table	2b								0]	(53)
													-	

Energy lost from water storage, kWh/year Enter (50) or (54) in (55)		(47) x (51) x (52) x (53) =		0	(54) (55)
Water storage loss calculated for each month		((56)m =	(55) × (41)ı	m	0.	.59	(55)
(56)m= 18.41 16.63 18.41 17.82 18.41	17.82 18.41	<u> </u>	17.82	18.41	17.82	18.41	(56)
If cylinder contains dedicated solar storage, (57)m = (56)							` '
(57)m= 18.41 16.63 18.41 17.82 18.41	17.82 18.41	18.41	17.82	18.41	17.82	18.41	(57)
Primary circuit loss (annual) from Table 3						0	(58)
Primary circuit loss calculated for each month	. , , , ,	•		_			
(modified by factor from Table H5 if there is			· ·	—	- 		(50)
(59)m= 23.26 21.01 23.26 22.51 23.26	22.51 23.26	23.26	22.51	23.26	22.51	23.26	(59)
Combi loss calculated for each month (61)m =	- 	-i					
(61)m= -44.59 -40.27 -44.59 -43.15 -44.59	<u> </u>	<u> </u>	-43.15	-44.59	-43.15	-44.59	(61)
Total heat required for water heating calculate		``	0.85 × (` 	(46)m +	<u> </u>	ı` <i>′</i> , ` <i>′</i>
(62)m= 223.84 195.69 201.73 175.6 168.28			156.14	182.34	199.4	216.68	(62)
Solar DHW input calculated using Appendix G or Append				r contribut	ion to wate	er heating)	
(add additional lines if FGHRS and/or WWHR	- 	``	·				(63)
(63)m= 0 0 0 0 0 0	0 0	0	0	0	76.24	81.71	(63) (G2)
FHRS 83.03 76.08 76.59 63.98 49.92	10.64 9.86	11.31	11.45	65.21	76.34	01./1	(03) (02)
Output from water heater (64)m= 142.96 121.45 126.95 113.04 119.62	2 135.2 124.8	3 143.89	145.81	118.61	124.87	137.01	
(64)m= 142.96 121.45 126.95 113.04 119.62	135.2 124.6		out from wa	<u> </u>	<u> </u>		1554.25 (64)
Heat going from water heating kW/h/month 0	25 ′ [0 95 ·· /45]					!	· · ·
Heat gains from water heating, kWh/month 0. (65)m= 97.59 85.99 90.24 80.8 79.12	 		74.33	83.79	88.72	95.21] (65)
include (57)m in calculation of (65)m only if	<u> </u>	_!		<u> </u>		<u> </u>	·
5. Internal gains (see Table 5 and 5a):	Cylinder is in the	e aweiling	OI HOLW	ater is ii	OIII COIII	munity n	eaung
Metabolic gains (Table 5), Watts							
Jan Feb Mar Apr May	/ Jun Jul	Aug	Sep	Oct	Nov	Dec	
(66)m= 220.64 220.64 220.64 220.64 220.64	220.64 220.6	4 220.64	220.64	220.64	220.64	220.64	(66)
Lighting gains (calculated in Appendix L, equa	ation L9 or L9a),	also see	Table 5				
(67)m= 112.32 99.76 81.13 61.42 45.91	38.76 41.88	54.44	73.07	92.78	108.29	115.44	(67)
Appliances gains (calculated in Appendix L, e	quation L13 or I	_13a), also	see Tal	ble 5			
(68)m= 1069.48 1080.57 1052.61 993.07 917.92	847.28 800.0	9 789	816.96	876.5	951.65	1022.29	(68)
Cooking gains (calculated in Appendix L, equ	ation L15 or L15	ia), also s	ee Table	5			
(69)m= 45.06 45.06 45.06 45.06 45.06	45.06 45.06	45.06	45.06	45.06	45.06	45.06	(69)
Pumps and fans gains (Table 5a)							
(70)m= 3 3 3 3 3	3 3	3	3	3	3	3	(70)
Losses e.g. evaporation (negative values) (Ta	able 5)						
(71)m= -176.51 -176.51 -176.51 -176.51 -176.51	l -176.51 -176.5	1 -176.51	-176.51	-176.51	-176.51	-176.51	(71)
Water heating gains (Table 5)							
(72)m= 131.17 127.96 121.29 112.22 106.34	98.05 91.01	100.03	103.24	112.62	123.22	127.97	(72)
Total internal gains =	(66)m + (67	r)m + (68)m	+ (69)m + ((70)m + (7	1)m + (72))m	
(73)m= 1405.15 1400.48 1347.22 1258.9 1162.3	6 1076.29 1025.	8 1035.66	1085.46	1174.09	1275.35	1357.89	(73)

6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation: Access Fact Table 6d		Area m²		Flux Table 6a		g_ Table 6b		FF Table 6c		Gains (W)	
North 0.9x 0.77	x	4.35	X	10.63	x	0.63	x	0.7] = [14.14	(74)
North 0.9x 0.77	X	4.35	X	20.32	X	0.63	х	0.7] = [27.02	(74)
North 0.9x 0.77	x	4.35	X	34.53	X	0.63	х	0.7	= [45.91	(74)
North 0.9x 0.77	x	4.35	X	55.46	x	0.63	х	0.7	= [73.74	(74)
North 0.9x 0.77	x	4.35	X	74.72	X	0.63	х	0.7] = [99.33	(74)
North 0.9x 0.77	x	4.35	X	79.99	x	0.63	x	0.7	= [106.33	(74)
North 0.9x 0.77	x	4.35	x	74.68	x	0.63	x	0.7] = [99.28	(74)
North 0.9x 0.77	x	4.35	X	59.25	x	0.63	x	0.7] = [78.76	(74)
North 0.9x 0.77	X	4.35	X	41.52	x	0.63	x	0.7] = [55.19	(74)
North 0.9x 0.77	x	4.35	X	24.19	x	0.63	x	0.7] = [32.16	(74)
North 0.9x 0.77	X	4.35	X	13.12	x	0.63	x	0.7] = [17.44	(74)
North 0.9x 0.77	X	4.35	X	8.86	X	0.63	X	0.7] = [11.78	(74)
Northeast 0.9x 0.77	x	51.85	X	11.28	x	0.63	x	0.7] = [178.79	(75)
Northeast 0.9x 0.77	X	51.85	X	22.97	x	0.63	x	0.7] = [363.93	(75)
Northeast 0.9x 0.77	X	51.85	X	41.38	x	0.63	x	0.7	= [655.69	(75)
Northeast 0.9x 0.77	X	51.85	X	67.96	x	0.63	x	0.7] = [1076.83	(75)
Northeast 0.9x 0.77	X	51.85	X	91.35	x	0.63	x	0.7] = [1447.47	(75)
Northeast 0.9x 0.77	x	51.85	X	97.38	x	0.63	x	0.7	= [1543.16	(75)
Northeast 0.9x 0.77	x	51.85	X	91.1	x	0.63	x	0.7] = [1443.59	(75)
Northeast 0.9x 0.77	X	51.85	X	72.63	x	0.63	x	0.7] = [1150.85	(75)
Northeast 0.9x 0.77	x	51.85	X	50.42	x	0.63	x	0.7] = [798.97	(75)
Northeast 0.9x 0.77	X	51.85	X	28.07	x	0.63	x	0.7] = [444.75	(75)
Northeast 0.9x 0.77	X	51.85	X	14.2	X	0.63	x	0.7] = [224.96	(75)
Northeast 0.9x 0.77	X	51.85	X	9.21	X	0.63	X	0.7] = [146.01	(75)
Southwest _{0.9x} 0.77	X	42.16	X	36.79]	0.85	x	0.7] = [639.63	(79)
Southwest _{0.9x} 0.77	X	13.01	X	36.79		0.63	X	0.7] = [146.29	(79)
Southwest _{0.9x} 0.77	X	42.16	X	62.67]	0.85	X	0.7] = [1089.52	(79)
Southwest _{0.9x} 0.77	X	13.01	X	62.67]	0.63	x	0.7] = [249.19	(79)
Southwest _{0.9x} 0.77	X	42.16	X	85.75		0.85	X	0.7] = [1490.73	(79)
Southwest _{0.9x} 0.77	X	13.01	X	85.75]	0.63	X	0.7] = [340.95	(79)
Southwest _{0.9x} 0.77	X	42.16	X	106.25		0.85	x	0.7] = [1847.08	(79)
Southwest _{0.9x} 0.77	X	13.01	X	106.25		0.63	x	0.7] = [422.46	(79)
Southwest _{0.9x} 0.77	x	42.16	X	119.01]	0.85	x	0.7] = [2068.89	(79)
Southwest _{0.9x} 0.77	X	13.01	x	119.01]	0.63	x	0.7] = [473.19	(79)
Southwest _{0.9x} 0.77	X	42.16	x	118.15]	0.85	x	0.7] = [2053.93	(79)
Southwest _{0.9x} 0.77	X	13.01	x	118.15]	0.63	x	0.7] = [469.77	(79)

Southw															
	est _{0.9x}	0.77	X	42.	16	X	11:	3.91		0.85	X	0.7	=	1980.2	(79)
Southw	est _{0.9x}	0.77	X	13.	01	x	11:	3.91		0.63	x	0.7	=	452.91	(79)
Southw	est _{0.9x}	0.77	X	42.	16	X	10-	4.39		0.85	x	0.7	=	1814.73	(79)
Southw	est _{0.9x}	0.77	X	13.	01	X	10-	4.39		0.63	x	0.7	=	415.06	(79)
Southw	est _{0.9x}	0.77	X	42.	16	X	92	2.85		0.85	x	0.7	=	1614.14	(79)
Southw	est _{0.9x}	0.77	X	13.	01	X	92	2.85		0.63	x	0.7	=	369.18	(79)
Southw	est _{0.9x}	0.77	X	42.	16	x	69).27		0.85	x	0.7	=	1204.15	(79)
Southw	est _{0.9x}	0.77	X	13.	01	x	69).27		0.63	x	0.7	=	275.41	(79)
Southw	est _{0.9x}	0.77	X	42.	16	x	44	1.07		0.85	x	0.7	=	766.12	(79)
Southw	est _{0.9x}	0.77	X	13.	01	X	44	1.07		0.63	x	0.7	=	175.23	(79)
Southw	est _{0.9x}	0.77	X	42.	16	x	31	.49		0.85	x	0.7	=	547.39	(79)
Southw	est _{0.9x}	0.77	X	13.	01	X	31	.49		0.63	x	0.7	=	125.2	(79)
															_
_		watts, ca				_	70.40			Sum(74)m		7 4400 75		1	(02)
(83)m=			2533.28		4088.88			3975.98	3459	4 2837.48	1956.4	7 1183.75	830.38		(83)
_	2383.99	nternal a	3880.49	4679.01	5251.23	·		5001.15	4495.	06 3922.95	3130.5	6 2459.1	2188.26]	(84)
						_	49.47	3001.13	4495.	3922.93	3130.0	2459.1	2100.20		(04)
		nal temp		`		<i>'</i>									_
-		during h							ole 9,	Th1 (°C)				21	(85)
Utilisa	ation fac	tor for ga	ains for I	iving are	ea, h1,m) (Se	ee Tab	ole 9a)			ı			1	
	Jan	Feb	Mar	Apr	May	<u> </u>	Jun	Jul	Au	g Sep	Oct	Nov	Dec		
(86)m=	1	1	0.99	0.97	0.92	(0.81	0.68	0.74	0.92	0.99	1	1		(86)
Mean	interna	temper	ature in	living are	ea T1 (fo	ollo	w step	s 3 to 7	in Ta	ble 9c)				_	
(87)m=	19.32	19.49	19.76	20.15	20.5	I -									
Temn				20.15	20.5	2	0.76	20.87	20.8	20.62	20.16	19.68	19.31		(87)
i Gilib	erature	during h				<u> </u>					20.16	19.68	19.31		(87)
(88)m=	erature 20.32	during h				dw				Th2 (°C)	20.16	-	19.31		(87)
(88)m=	20.32	20.33	eating p	eriods ir 20.34	rest of 20.34	dw 2	elling 1	from Ta 20.36	ble 9, 20.3	Th2 (°C)	I	-			, ,
(88)m=	20.32		eating p	eriods ir 20.34	rest of 20.34	dw 2 h2,	elling 1	from Ta 20.36	ble 9, 20.3	Th2 (°C)	I	-			, ,
(88)m= Utilisa (89)m=	20.32 ation fac	20.33 tor for ga	eating p 20.33 ains for r 0.99	eriods ir 20.34 rest of d	n rest of 20.34 welling, 0.91	dw 2 h2,	relling 1	from Ta 20.36 e Table 0.6	ble 9, 20.3 9a) 0.67	Th2 (°C) 5 20.35	20.34	20.34	20.33		(88)
(88)m= Utilisa (89)m= Mean	20.32 ation fac 1 interna	20.33 tor for ga	eating p 20.33 ains for 1 0.99 ature in	eriods in 20.34 rest of d 0.97 the rest	rest of 20.34 welling, 0.91 of dwell	dw 2 h2, ing	m (see	from Ta 20.36 Table 0.6	9a) 0.67	Th2 (°C) 5 20.35 0.9 7 in Tab	20.34 0.98 le 9c)	20.34	20.33		(88)
(88)m= Utilisa (89)m=	20.32 ation fac	20.33 tor for ga	eating p 20.33 ains for r 0.99	eriods ir 20.34 rest of d	n rest of 20.34 welling, 0.91	dw 2 h2, ing	relling 1	from Ta 20.36 e Table 0.6	ble 9, 20.3 9a) 0.67	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88	20.34 0.98 e 9c)	20.34	20.33	0.06	(88)
(88)m= Utilisa (89)m= Mean (90)m=	20.32 ation fac 1 interna 17.98	20.33 tor for ga 1 tempera 18.22	eating p 20.33 ains for r 0.99 ature in 1 18.63	eriods ir 20.34 rest of d 0.97 the rest 19.19	velling, 0.91 of dwell	dw 2 h2, c	relling to 0.36 m (see 0.77 T2 (fo 0.07	from Ta 20.36 e Table 0.6 llow ste	9a) 0.67 ps 3 t	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88	20.34 0.98 e 9c)	20.34	20.33	0.06	(88)
Utilisa (89)m= Mean (90)m=	20.32 ation fac 1 interna 17.98	20.33 tor for ga 1 tempera 18.22	eating p 20.33 ains for r 0.99 ature in 1 18.63	eriods ir 20.34 rest of d 0.97 the rest 19.19	velling, 0.91 of dwell 19.7	dw 2 h2, ing 2	relling to 0.36 m (see 0.77 T2 (fo 0.07 g) = fL	from Ta 20.36 e Table 0.6 llow ste 20.2	9a) 0.67 ps 3 t 20.16	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2	20.34 0.98 le 9c) 19.22 fLA = Liv	20.34 1 18.51 ving area ÷ (-	20.33 1 17.97 4) =	0.06	(88) (89) (90) (91)
(88)m= Utilisa (89)m= Mean (90)m= Mean (92)m=	20.32 ation fac 1 interna 17.98 interna 18.06	20.33 tor for ga 1 tempera 18.22 tempera 18.3	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (fo	eriods ir 20.34 rest of d 0.97 the rest 19.19 r the wh	velling, 0.91 of dwell 19.7 ole dwe	dw 2 h2, c ing 2	relling to 0.36 m (see 0.77 T2 (fo 0.07 g) = fL 0.11	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1	9a) 0.67 ps 3 1 20.16	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93	20.34 0.98 le 9c) 19.22 fLA = Liv	20.34 1 18.51 ving area ÷ (-	20.33	0.06	(88)
(88)m= Utilisa (89)m= Mean (90)m= Mean (92)m= Apply	20.32 ation fac 1 interna 17.98 interna 18.06 adjustn	20.33 tor for ga 1 tempera 18.22 tempera 18.3 nent to the	eating p 20.33 ains for r 0.99 ature in 1 18.63 ature (fo 18.69 ne mean	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper	dw 2 h2, ing 2 elling 2 atu	m (see 0.77 T2 (fo 0.07 g) = fL 0.11 ure from	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 there appre	20.34 0.98 le 9c) 19.22 fLA = Liv 19.27 opriate	1 18.51 ring area ÷ (-	20.33 1 17.97 4) =	0.06	(88) (89) (90) (91) (92)
(88)m= Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m=	20.32 ation fac 1 interna 17.98 interna 18.06 adjustn 17.91	20.33 tor for ga 1 tempera 18.22 I tempera 18.3 nent to th	eating p 20.33 ains for r 0.99 ature in 1 18.63 ature (fo 18.69 ne mean 18.54	eriods ir 20.34 rest of d 0.97 the rest 19.19 r the wh	velling, 0.91 of dwell 19.7 ole dwe	dw 2 h2, ing 2 elling 2 atu	relling to 0.36 m (see 0.77 T2 (fo 0.07 g) = fL 0.11	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1	9a) 0.67 ps 3 1 20.16	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 there appre	20.34 0.98 le 9c) 19.22 fLA = Liv	1 18.51 ring area ÷ (-	20.33 1 17.97 4) =	0.06	(88) (89) (90) (91)
(88)m= Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa	20.32 ation fac 1 interna 17.98 interna 18.06 adjustn 17.91 ace hea	20.33 tor for gate of the period of the per	eating p 20.33 ains for r 0.99 ature in 1 18.63 ature (fo 18.69 ne mean 18.54	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper	dw 2 h2, conting 2 elling 2 ratu 1	m (see 0.77 T2 (fo 0.07 g) = fL 0.11 ure from 9.96	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 here appre	20.34 0.98 e 9c) 19.22 fLA = Liv 19.27 opriate 19.12	1 18.51 ving area ÷ (20.33 1 17.97 4) = 18.05		(88) (89) (90) (91) (92)
Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa	20.32 ation fac 1 interna 17.98 interna 18.06 adjustn 17.91 ace hea	20.33 tor for gate of the period of the per	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (for r 18.69 ne mean 18.54 direment ernal ter	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper 19.59	dw 2 h2, conting 2 elling 2 ratu 1	m (see 0.77 T2 (fo 0.07 g) = fL 0.11 ure from 9.96	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 there appre	20.34 0.98 e 9c) 19.22 fLA = Liv 19.27 opriate 19.12	1 18.51 ving area ÷ (20.33 1 17.97 4) = 18.05		(88) (89) (90) (91) (92)
Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa	20.32 ation fac 1 interna 17.98 interna 18.06 adjustn 17.91 ace hea	20.33 tor for ga 1 I tempera 18.22 I tempera 18.3 hent to the 18.15 ting requesting requestions.	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (for r 18.69 ne mean 18.54 direment ernal ter	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper 19.59	dw 2 h2, c ing 2 atu 1	m (see 0.77 T2 (fo 0.07 g) = fL 0.11 ure from 9.96	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 here approx 19.78 9b, so that	20.34 0.98 e 9c) 19.22 fLA = Liv 19.27 opriate 19.12	1 18.51 ving area ÷ (-1 18.58 18.43 =(76)m an	20.33 1 17.97 4) = 18.05		(88) (89) (90) (91) (92)
Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa Set Ti the ut	interna 18.06 adjustn 17.91 ace head to the rillisation Jan	20.33 tor for ga 1 I tempera 18.22 I tempera 18.3 nent to th 18.15 ting requesting req	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (for r 18.69 ne mean 18.54 direment ernal ternal	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1 mperaturusing Ta	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper 19.59	dw 2 h2, c ing 2 atu 1	relling to 0.36 m (see 0.77 T2 (fo 0.07 m) m (see 0.77 m) m (see 0	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09 p 11 of	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0	Th2 (°C) 5 20.35 0.9 0 7 in Tab 3 19.88 fLA) × T2 2 19.93 here apprendiction of the properties of	20.34 0.98 le 9c) 19.22 19.27 opriate 19.12 t Ti,m:	1 18.51 ving area ÷ (-1 18.58 18.43 =(76)m an	20.33 1 17.97 4) = 18.05 17.9 d re-calc		(88) (89) (90) (91) (92)
Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa Set Ti the ut	interna 18.06 adjustn 17.91 ace head to the rillisation Jan	20.33 tor for ga 1 I tempera 18.22 I tempera 18.3 hent to the string requesting request	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (for r 18.69 ne mean 18.54 direment ernal ternal	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1 mperaturusing Ta	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper 19.59	dw 2 h2, cing 2 illing 2 atu 1	relling to 0.36 m (see 0.77 T2 (fo 0.07 m) m (see 0.77 m) m (see 0	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09 p 11 of	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 here approx 19.78 9b, so that	20.34 0.98 le 9c) 19.22 19.27 opriate 19.12 t Ti,m:	1 18.51 ving area ÷ (-1 18.58 18.43 =(76)m an	20.33 1 17.97 4) = 18.05 17.9 d re-calc		(88) (89) (90) (91) (92)
Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa Set Ti the ut Utilisa (94)m= Usefu	20.32 ation factor of the result of the resu	20.33 tor for ga 1 I tempera 18.22 I tempera 18.3 nent to th 18.15 ting requ mean interfactor for ga 0.99 hmGm ,	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (for r 18.69 ne mean 18.54 direment ernal ternor gains of mar ains, hm 0.98	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1 mperaturusing Ta Apr : 0.96	n rest of 20.34 welling, 0.91 of dwell 19.7 ole dwe 19.74 temper 19.59 re obtainable 9a May 0.88	dw 2 h2, cing 2 illing 2 atu 1	relling to 0.36	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09 p 11 of Jul	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0 Table	Th2 (°C) 5 20.35 0.9 7 in Tab 19.88 fLA) × T2 19.93 here approx 19.78 9b, so that	20.34 0.98 le 9c) 19.22 fLA = Liv 19.27 opriate 19.12 tt Ti,m=	20.34 1 18.51 ring area ÷ (20.33 1 17.97 4) = 18.05 17.9 d re-cald		(88) (89) (90) (91) (92) (93)
Utilisa (89)m= Mean (90)m= Mean (92)m= Apply (93)m= 8. Spa Set Ti the ut Utilisa (94)m= Usefu	20.32 ation factor of the result of the resu	20.33 tor for ga 1 I tempera 18.22 I tempera 18.3 nent to th 18.15 ting requirement interpretation for ga 0.99 hmGm ,	eating p 20.33 ains for r 0.99 ature in r 18.63 ature (for r 18.69 ne mean 18.54 direment ernal ternor gains of mar ains, hm 0.98	eriods ir 20.34 rest of dr 0.97 the rest 19.19 r the wh 19.25 interna 19.1 mperatur using Ta Apr : 0.96 4)m x (84	velling, 0.91 of dwell 19.7 ole dwe 19.74 temper 19.59 re obtain ble 9a May 0.88 4)m	dw 2 h2, c ing 2 illing 2 atu 1	relling to 0.36 m (see 0.77 T2 (fo 0.07 T2	from Ta 20.36 e Table 0.6 llow ste 20.2 A × T1 20.24 n Table 20.09 p 11 of Jul	ble 9, 20.3 9a) 0.67 ps 3 1 20.1 + (1 - 20.2 4e, w 20.0 Table	Th2 (°C) 5 20.35 0.9 0.7 in Tab 3 19.88 fLA) × T2 2 19.93 there approx 19.78 9b, so that g Sep 0.87	20.34 0.98 le 9c) 19.22 fLA = Liv 19.27 opriate 19.12 t Ti,m: Oct 0.98	20.34 1 18.51 ring area ÷ (20.33 1 17.97 4) = 18.05 17.9 d re-calc		(88) (89) (90) (91) (92) (93)

Mont	hlv aver	age exte	rnal tem	perature	e from Ta	able 8								
(96)m=	<u> </u>	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2		(96)
Heat	loss rate	e for mea	an intern	al tempe	erature,	Lm , W =	=[(39)m :	x [(93)m	– (96)m	1	l	<u> </u>		
		12209.02						3193.88			10224.66	12467.07		(97)
Spac	e heatin	g require	ement fo	r each n	nonth, k\	Wh/mont	h = 0.02	24 x [(97)	m – (95)m] x (4	1)m			
(98)m=	7601.1	6112.97	5380.7	3376	1799.04	0	0	0	0	3394.56	5598.75	7649.92		
		-						Tota	l per year	(kWh/yeaı	r) = Sum(9	8) _{15,912} =	40913.03	(98)
Spac	e heatin	g require	ement in	kWh/m²	² /year								31.83	(99)
8c. S	pace co	oling rec	luiremen	t										
Calcı	ulated fo	r June, J	luly and	August.	See Tal	ole 10b				ī	ī		ı	
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
		e Lm (ca	lculated	using 2	5°C inter				ernal ten	nperatur	e from T	able 10)	ı	
(100)m=		0	0	0	0	8223.75	6474.02	6619.29	0	0	0	0		(100)
		tor for lo						ı					l	
(101)m=		0	0	0	0	0.69	0.77	0.72	0	0	0	0	I	(101)
		mLm (V	i		<u> </u>			.=			Ι.			(400)
(102)m=		. 0	0	0	0	5648.25	4986.4	4761.1	0	0	0	0	I	(102)
		gains ca						r						(402)
(103)m=		0	0	0	0	6491.45			0	0	0	0	(44)	(103)
		g require zero if (iweiiing,	continuo	ous (KVV	(n) = 0.0	24 X [(10)3)m – (102)m] ɔ	₹ (41)m	
(104)m=		0	0	0	0	0	896.43	632.57	0	0	0	0		
, ,		l							L Total	l = Sum(104)	=	1529	(104)
Coole	d fractio	n								`	area ÷ (4	1) =	0.07	(105)
Interm	ittency f	actor (Ta	able 10b)							•	· I		
(106)m=	0	0	0	0	0	0.25	0.25	0.25	0	0	0	0		
		-	-					-	Tota	l = Sum((104)	=	0	(106)
		requirer								1	1			_
(107)m=	0	0	0	0	0	0	16.56	11.69	0	0	0	0		_
									Total	l = Sum(107)	=	28.25	(107)
Space	cooling	requirer	nent in k	Wh/m²/y	/ear				(107)	$) \div (4) =$			0.02	(108)
9a. En	nergy rec	quiremer	nts – Indi	vidual h	eating sy	ystems i	ncluding	micro-C	HP)					
Spac	e heatir	ng:												_
Fract	ion of sp	ace hea	it from se	econdar	y/supple	mentary	system						0.1	(201)
Fract	ion of sp	ace hea	it from m	ain syst	em(s)			(202) = 1 -	- (201) =			Ī	0.9	(202)
Fract	ion of to	tal heatii	ng from i	main sys	stem 1			(204) = (20	02) x [1 –	(203)] =		İ	0.9	(204)
Effici	ency of ı	main spa	ace heati	ng syste	em 1								90.3	(206)
Effici	ency of	seconda	ry/supple	ementar	y heating	g system	ո, %						75	(208)
Cooli	ng Syste	em Ener	gy Efficie	ency Ra	tio								4.45	(209)
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/ye	- ear
Spac	e heatin	g require	ement (c	alculate	d above)								1	
	7601.1	6112.97	5380.7	3376	1799.04	0	0	0	0	3394.56	5598.75	7649.92	I	

$(211)m = \{[(98)m \times (204)] \} \times 100 \div (206)$	3)									(211)
7575.85 6092.66 5362.82 3364.78		0	0	0	0	3383.28	5580.15	7624.51		, ,
	•			Tota	l (kWh/yea	ar) =Sum(2	211),15,1012	=	40777.1	(211)
Space heating fuel (secondary), kWh/n	nonth							·		_
$= \{[(98) \text{m x } (201)]\} \times 100 \div (208)$	239.87	0	0			452.61	746.5	1019.99		
(215)m= 1013.48 815.06 717.43 450.13	239.67	0	0	0 Tota	0 I (kWh/yea	ar) =Sum(2			5455.07	(215)
Water heating						,	715,1012		0400.07	
Output from water heater (calculated ab	ove)									
142.96 121.45 126.95 113.04	119.62	135.2	124.83	143.89	145.81	118.61	124.87	137.01		7
Efficiency of water heater	00.47	70.0	70.0	70.0	70.0	00.05	00.04	00.00	79.6	(216)
(217)m= 90.05 90.04 89.99 89.87 Fuel for water heating, kWh/month	89.47	79.6	79.6	79.6	79.6	89.85	90.01	90.06		(217)
(219) $m = (64)m \times 100 \div (217)m$						-				
(219)m= 158.76 134.89 141.07 125.79	133.7	169.85	156.82	180.77	183.17	132.01	138.73	152.13		,
On the second second second				Tota	I = Sum(2	19a) ₁₁₂ =			1807.68	(219)
Space cooling fuel, kWh/month. $(221)m = (107)m \div (209)$										
(221)m= 0 0 0 0	0	0	3.72	2.62	0	0	0	0		
				Tota	I = Sum(2	21) ₆₈ =			6.34	(221)
Annual totals						k'	Wh/year	•	kWh/year	_
Space heating fuel used, main system 1									40777.1	╛
Space heating fuel used, secondary									5455.07	╛
Water heating fuel used									1807.68	
Space cooling fuel used									6.34	
Electricity for pumps, fans and electric k	eep-hot	:								
mechanical ventilation - balanced, extra	act or p	ositive ir	nput fron	n outside	€			8574.91		(230a)
central heating pump:								30		(230c)
boiler with a fan-assisted flue								45		(230e)
Total electricity for the above, kWh/year				sum	of (230a).	(230g) =			8649.91	(231)
Electricity for lighting									1983.52	(232)
12a. CO2 emissions – Individual heatir	ng syste	ms inclu	uding mi	cro-CHP)					
		En	ergy			Emice	ion fac	tor	Emissions	
			/h/year			kg CO		loi	kg CO2/yea	
Space heating (main system 1)		(211	I) x			0.2	16	=	8807.85	(261)
Space heating (secondary)		(215	5) x			0.0	19	=	103.65] (263)
Water heating		(219	9) x			0.2	16	=	390.46] (264)
Space and water heating		(261	1) + (262) -	+ (263) + (264) =				9301.96	(265)
Space cooling		(221	I) x			0.5	10	=	3.29] (266)
							ו פו			
Electricity for pumps, fans and electric k	een-hot	· (231	l) x			0.5		=	4489.3	(267)

(232) x Electricity for lighting (268) 1029.45 0.519 sum of (265)...(271) = Total CO2, kg/year (272) 14824 **Dwelling CO2 Emission Rate** $(272) \div (4) =$ (273) 11.53 El rating (section 14) 85 (274)