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Date

Eng. PS

Job No. 16440

Sheet No.

PC-14

28 CANFIELD GARDENS
NW6.

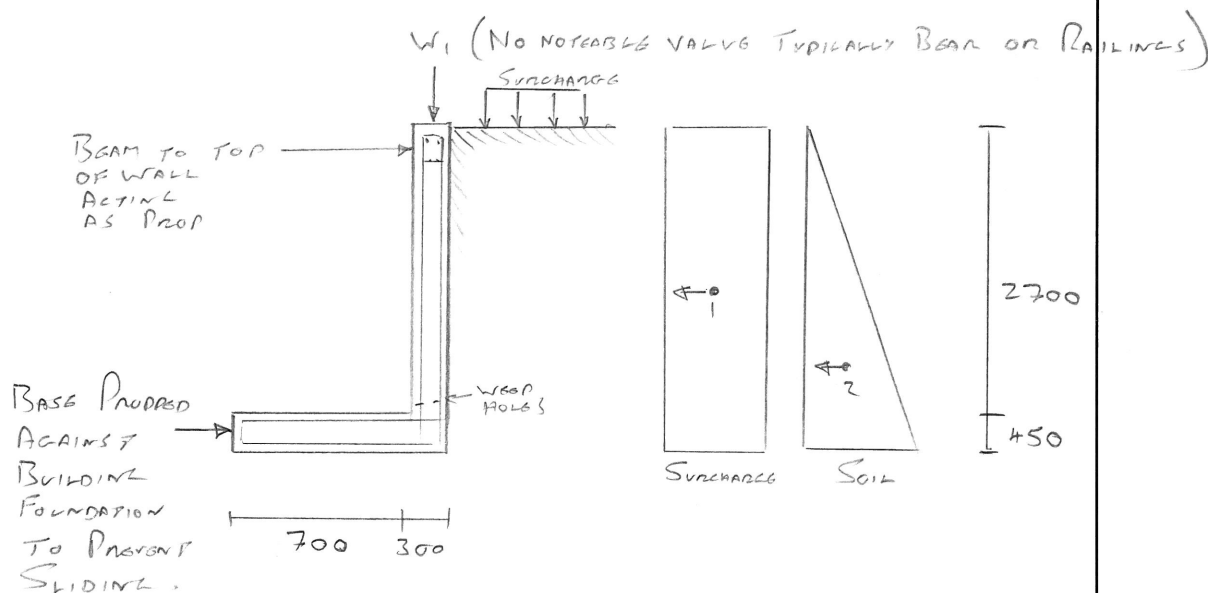
EXTERNAL LIGHTWELL RETAINING WALL DESIGN.

SURCHARGE : SIMILAR TO OTHER EXTERNAL WALLS.
LOAD
CASES

FRONT (VEHICLE AXLES) = 10.0 kN/m^2


REAR (GARDEN) = 5.0 kN/m^2

WATER : LINED WEEP HOLES ARE TO BE FORMED
PRESSURE NEAR THE BASE OF THE WALL. WATER
TO RUN INTO DRAINAGE (BY OTHERS) IN THE
BASE OF THE LIGHTWELLS.



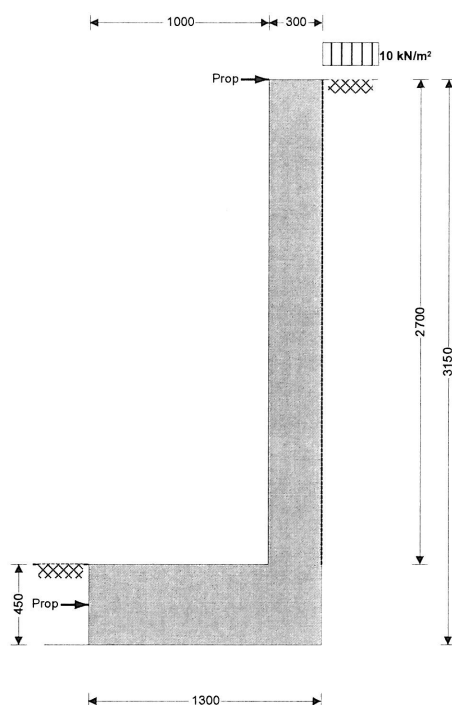
GENERAL WALL DESIGN CARRIED OUT USING TEDDS PROGRAM & ASSUMING:

- C-35(SR) GRADE CONCRETE
- H-16 BARS @ 200mm c/c TOP & BOTTOM TO BASE.
- H16 BARS @ 200mm c/c TO BOTH FACES IN WALL VERTICALLY.
- H12 BARS @ 250mm c/c TO BOTH FACES IN WALL HORIZONTALLY.

 Tedds Martin Redston Associates 4 Edward Square London N1 0SP	Project		28 CANFIELD GARDENS, LONDON		Job no.		16.440
	Calcs for		LIGHTWELL RETAINING WALL SECTION (front)		Start page no./Revision		06-15
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RETAINING WALL ANALYSIS (BS 8002:1994)

TEDDS calculation version 1.2.01.06



Wall details

Retaining wall type

Height of wall stem

Length of toe

Overall length of base

Height of retaining wall

Depth of downstand

Position of downstand

Depth of cover in front of wall

Height of ground water

Density of wall construction

Angle of soil surface

Mobilisation factor

Moist density

Design shear strength

Design shear strength

Moist density

Using Coulomb theory

Active pressure

At-rest pressure

Loading details

Surcharge load

Vertical dead load

Cantilever

$h_{\text{stem}} = 2700 \text{ mm}$

$l_{\text{toe}} = 1000 \text{ mm}$

$l_{\text{base}} = 1300 \text{ mm}$

$h_{\text{wall}} = 3150 \text{ mm}$

$d_{\text{ds}} = 0 \text{ mm}$

$l_{\text{ds}} = -250 \text{ mm}$

$d_{\text{cover}} = 0 \text{ mm}$

$h_{\text{water}} = 0 \text{ mm}$

$\gamma_{\text{wall}} = 23.6 \text{ kN/m}^3$

$\beta = 0.0 \text{ deg}$

$M = 1.5$

$\gamma_m = 18.0 \text{ kN/m}^3$

$\phi' = 24.2 \text{ deg}$

$\phi'_b = 24.2 \text{ deg}$

$\gamma_{\text{mb}} = 18.0 \text{ kN/m}^3$

$K_a = 0.419$

$K_0 = 0.590$

Surcharge = 10.0 kN/m²

$W_{\text{dead}} = 0.0 \text{ kN/m}$

Wall stem thickness

Length of heel

Base thickness

Thickness of downstand

Unplanned excavation depth

Density of water

Density of base construction

Effective height at back of wall

Saturated density

Angle of wall friction

Design base friction

Allowable bearing

Passive pressure

Vertical live load

$t_{\text{wall}} = 300 \text{ mm}$

$l_{\text{heel}} = 0 \text{ mm}$

$t_{\text{base}} = 450 \text{ mm}$

$t_{\text{ds}} = 450 \text{ mm}$

$d_{\text{exc}} = 0 \text{ mm}$

$\gamma_{\text{water}} = 9.81 \text{ kN/m}^3$

$\gamma_{\text{base}} = 23.6 \text{ kN/m}^3$

$h_{\text{eff}} = 3150 \text{ mm}$

$\gamma_s = 21.0 \text{ kN/m}^3$


$\delta = 0.0 \text{ deg}$

$\delta_b = 18.6 \text{ deg}$

$P_{\text{bearing}} = 100 \text{ kN/m}^2$

$K_p = 4.187$

$W_{\text{live}} = 0.0 \text{ kN/m}$

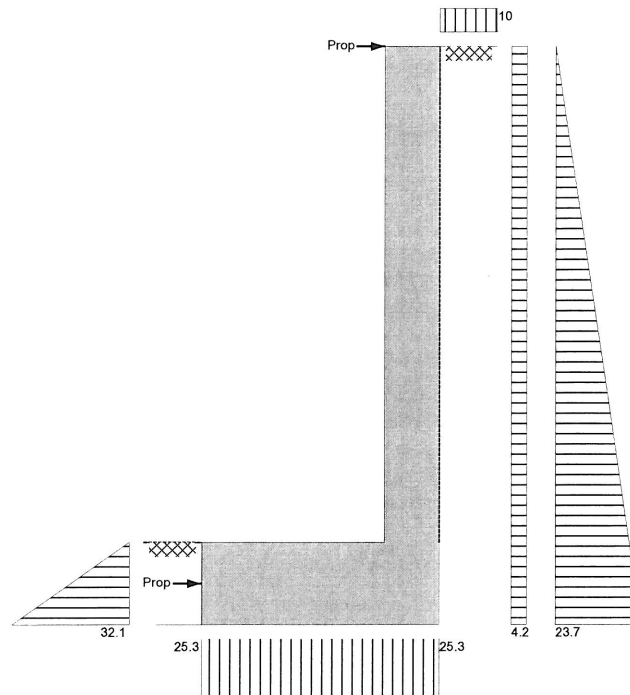
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Horizontal dead load
Position of vertical load

$F_{\text{dead}} = 0.0 \text{ kN/m}$
 $l_{\text{load}} = 0 \text{ mm}$

Horizontal live load
Height of horizontal load

$F_{\text{live}} = 0.0 \text{ kN/m}$
 $h_{\text{load}} = 0 \text{ mm}$



Loads shown in kN/m, pressures shown in kN/m²

Calculate propping force

Propping force $F_{\text{prop}} = 32.2 \text{ kN/m}$

Check bearing pressure

Total vertical reaction $R = 32.9 \text{ kN/m}$
Eccentricity of reaction $e = 0 \text{ mm}$

Distance to reaction $x_{\text{bar}} = 650 \text{ mm}$

Reaction acts within middle third of base

Bearing pressure at toe $p_{\text{toe}} = 25.3 \text{ kN/m}^2$


Bearing pressure at heel $p_{\text{heel}} = 25.3 \text{ kN/m}^2$

PASS - Maximum bearing pressure is less than allowable bearing pressure

Calculate propping forces to top and base of wall

Propping force to top of wall $F_{\text{prop_top}} = 14.767 \text{ kN/m}$

Propping force to base of wall $F_{\text{prop_base}} = 17.480 \text{ kN/m}$

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RETAINING WALL DESIGN (BS 8002:1994)

TEDDS calculation version 1.2.01.06

Ultimate limit state load factors

Dead load factor $\gamma_{f_d} = 1.4$ Live load factor $\gamma_{f_l} = 1.6$
Earth pressure factor $\gamma_{f_e} = 1.4$

Calculate propping force

Propping force $F_{prop} = 32.2 \text{ kN/m}$

Calculate propping forces to top and base of wall

Propping force to top of wall $F_{prop_top_f} = 31.931 \text{ kN/m}$ Propping force to base of wall $F_{prop_base_f} = 45.947 \text{ kN/m}$

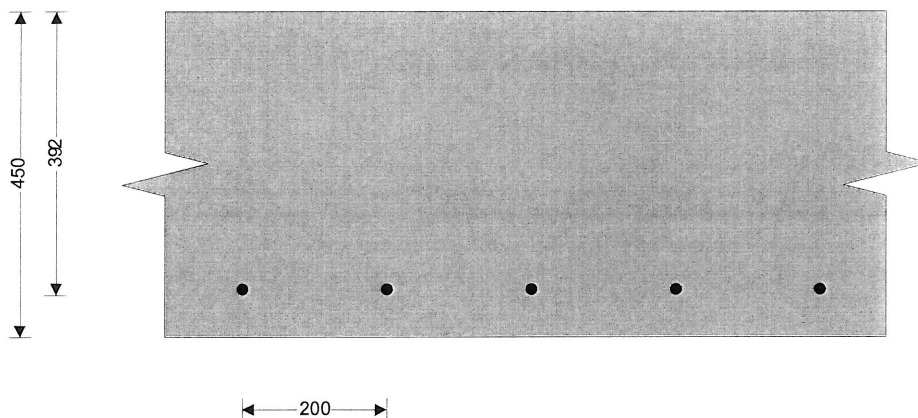
Design of reinforced concrete retaining wall toe (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 35 \text{ N/mm}^2$ Strength of reinforcement $f_y = 500 \text{ N/mm}^2$

Base details

Minimum reinforcement $k = 0.13 \%$ Cover in toe $C_{toe} = 50 \text{ mm}$



Design of retaining wall toe

Shear at heel $V_{toe} = 20.6 \text{ kN/m}$ Moment at heel $M_{toe} = 13.6 \text{ kNm/m}$
Compression reinforcement is not required

Check toe in bending

Reinforcement provided **16 mm dia.bars @ 200 mm centres**
Area required $A_{s_toe_req} = 585.0 \text{ mm}^2/\text{m}$ Area provided $A_{s_toe_prov} = 1005 \text{ mm}^2/\text{m}$
PASS - Reinforcement provided at the retaining wall toe is adequate

Check shear resistance at toe

Design shear stress $V_{toe} = 0.053 \text{ N/mm}^2$ Allowable shear stress $V_{adm} = 4.733 \text{ N/mm}^2$
PASS - Design shear stress is less than maximum shear stress
Concrete shear stress $V_{c_toe} = 0.451 \text{ N/mm}^2$
 $V_{toe} < V_{c_toe}$ - No shear reinforcement required


Design of reinforced concrete retaining wall stem (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 35 \text{ N/mm}^2$ Strength of reinforcement $f_y = 500 \text{ N/mm}^2$

Wall details

Minimum reinforcement $k = 0.13 \%$

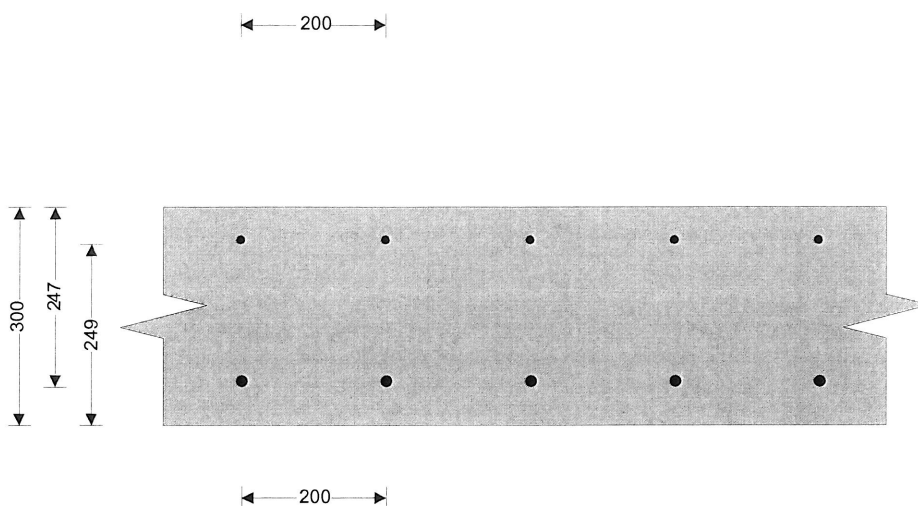
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Cover in stem

$C_{stem} = 45 \text{ mm}$

Cover in wall

$C_{wall} = 45 \text{ mm}$



Design of retaining wall stem

Shear at base of stem

$V_{stem} = 57.4 \text{ kN/m}$

Moment at base of stem

$M_{stem} = 33.2 \text{ kNm/m}$

Compression reinforcement is not required

Check wall stem in bending

Reinforcement provided

16 mm dia.bars @ 200 mm centres

Area required

$A_{s_stem_req} = 390.0 \text{ mm}^2/\text{m}$

Area provided

$A_{s_stem_prov} = 1005 \text{ mm}^2/\text{m}$

PASS - Reinforcement provided at the retaining wall stem is adequate

Check shear resistance at wall stem

Design shear stress

$V_{stem} = 0.233 \text{ N/mm}^2$

Allowable shear stress

$V_{adm} = 4.733 \text{ N/mm}^2$

PASS - Design shear stress is less than maximum shear stress

Concrete shear stress

$V_{c_stem} = 0.591 \text{ N/mm}^2$

$V_{stem} < V_{c_stem}$ - No shear reinforcement required

Design of retaining wall at mid height

Moment at mid height

$M_{wall} = 15.7 \text{ kNm/m}$

Compression reinforcement is not required

Reinforcement provided

12 mm dia.bars @ 200 mm centres

Area required

$A_{s_wall_req} = 390.0 \text{ mm}^2/\text{m}$

Area provided

$A_{s_wall_prov} = 565 \text{ mm}^2/\text{m}$

PASS - Reinforcement provided to the retaining wall at mid height is adequate

Check retaining wall deflection


Max span/depth ratio

$ratio_{max} = 40.00$

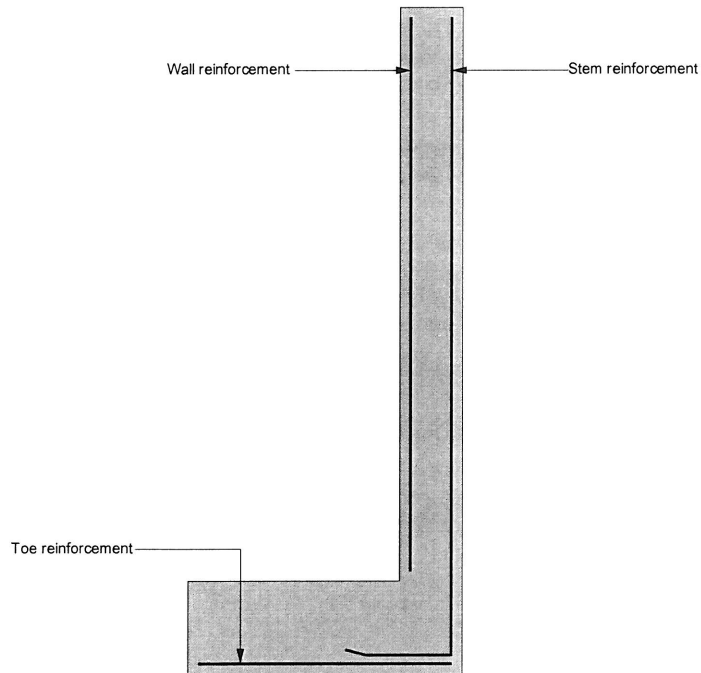
Actual span/depth ratio

$ratio_{act} = 10.93$

PASS - Span to depth ratio is acceptable

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Indicative retaining wall reinforcement diagram



Toe bars - 16 mm dia.@ 200 mm centres - (1005 mm²/m)
Wall bars - 12 mm dia.@ 200 mm centres - (565 mm²/m)
Stem bars - 16 mm dia.@ 200 mm centres - (1005 mm²/m)