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# **Technical Note**

# **Surface Water Drainage Summary**

The following document has been produced to summarise the Flood Risk Assessment (FRA), and the subsequent design works, in order to demonstrate the compliance of the proposed surface water drainage strategy for the Greenwood Community Resource Centre with Condition 19 of the London Borough of Camden Planning Consent (2013/5947/P). This document should be read in conjunction with the FRA prepared for the site (BSF11167-100315-Level 2 FRA F2).

Condition 19: The development hereby approved shall not be commenced, other than for site clearance & preparation, relocation of services, utilities and public infrastructure and demolition, until details of a surface water drainage scheme for the site, aiming by reasonable endeavours towards at least a 50% reduction from the current brownfield discharge rate, shall be submitted to and approved by the local planning authority in consultation with Thames Water. The development shall not be implemented other than in complete accordance with the surface water drainage scheme that has been approved.

## **Flood Risk Assessment**

In August 2013, the London Borough of Camden (LBC) commissioned Campbell Reith Hill LLP (CampbellReith), as part of the Tibbalds Multi-Disciplinary team, to prepare a FRA in support of the Planning Application for the proposed redevelopment of Greenwood Place, London. The latest revision of the FRA, F2, was issued in March 2015 (BSF11167-100315-Level 2 FRA F2).

As part of the FRA process, a proposed surface water management strategy for the development was proposed. This strategy was designed to prevent flooding of buildings up to the 1 in 100 year storm event including an allowance of +20% for future climate change.

# Surface Water Runoff Betterment

As the development is on a brownfield site, in accordance with the Mayor's London Plan and the North London SFRA, the proposed peak surface water discharges are to be limited to 50% of the peak surface runoff from the existing site, for the 1 in 1 year event.

The current peak discharge from the existing buildings and surrounding hard landscaping were calculated in Windes and were included in Appendix C of the FRA. These are summarised, along with the proposed peak surface water flow to be discharged from the proposed building and hardstanding area in the table below:

Return Period	Existing Peak Discharge (l/s)	Proposed Peak Flow (50% of Existing) (l/s)
1 in 1 year	26.6	13.3
1 in 2 year	30.1	15.1
1 in 30 year	37.7	18.9
1 in 100 year	37.8	18.9
1 in 100 year +20%		18.9

In order to limit the sites surface water discharge to the peak flows listed in the above table, attenuation storage was deemed to be required.

## Surface Water Drainage Strategy and Calculations

A preliminary surface water drainage strategy for the proposed development, including a proposed layout and calculations, was developed for the site as part of the FRA. This strategy proposes to limit the peak surface water discharge of the proposed development to the 1 in 1 year flow (13.3 l/s) for all events up to the 1 in 100 year storm event, including an allowance of +20% for climate change. Subsequently the proposed storm water layout and calculations for the development have been updated and refined at later design stages, in accordance with the above surface water drainage strategy.

The surface water drainage strategy consists of runoff generated from roof and external hardstanding areas, being collected via rain water pipes and linear channels respectively, before discharging into storm water sewer, where it is conveyed via gravity to a flow control manhole (hydrobrake). The restricted outfall from the hydrobrake (13.3 l/s) causes runoff to back up into the system during high flows and discharge into the offline 32m<sup>3</sup> cellular attenuation tank. Downstream of the hydrobrake, the storm water discharges into a combined water manhole and sewer before outfalling to the existing combined manhole located within Highgate Road carriageway. The latest issue of the Proposed Storm Water Drainage Layout (12291-CRH-GC-XX-DR-C-5055 P3) drawing is appended to this Technical Note.

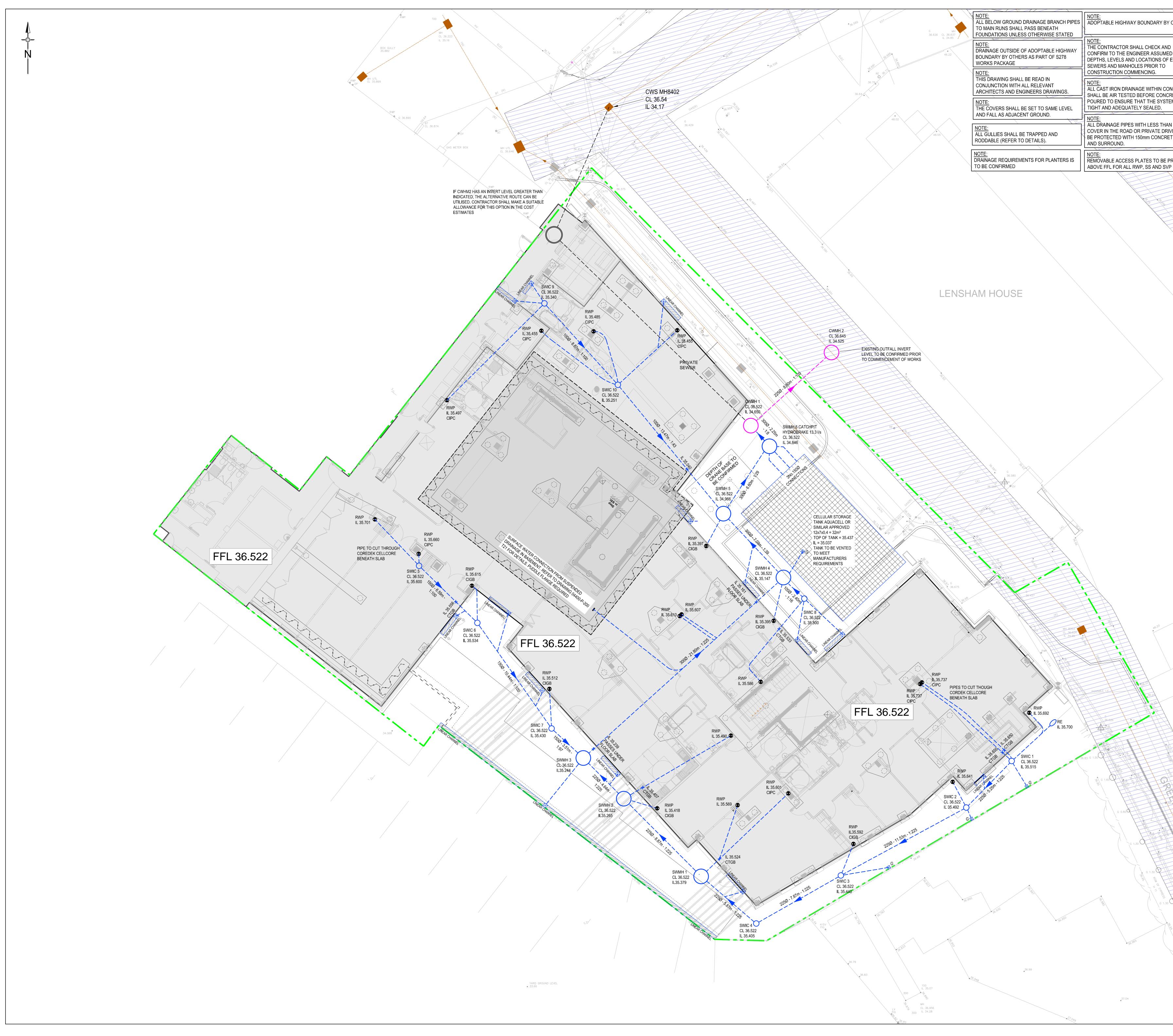
The accompanying calculations for the developed scenario have been updated since the FRA, and are also appended to this Technical Note.



## **Planning Condition 19 Compliance**

The proposed storm water drainage strategy has achieved a 50% reduction from the current brownfield discharge rate through SuDs recognised attenuation devices, flow control and cellular storage, therefore is considered to have complied with the requirement to be '*aiming by reasonable endeavours towards at least a 50% reduction from the current brownfield discharge rate*'.

Please consider this Technical Note, and the appended Storm Water Drainage Layout and calculations, as evidence of compliance for the approval of the local planning authority in consultation with Thames Water, in regards to the requirements of Condition 19 of the London Borough of Camden Planning Consent (2013/5947/P).



NOTE:	2499\12291 - THE GREENWOOD CENTRE\2-CIVILS\1-AUTOCAD\1-WORKING DRAWINGS\12291-CRH-GC-XX-DR-C-5055
OTHERS SETTING OUT OF ALL RWP, STUB-STACK AND SVP POSITIONS BY ARCHITECT/M&E.	<ol> <li>DO NOT SCALE THIS DRAWING ON PRINT OR ELECTRONICALLY. WORK FROM FIGURED DIMENSIONS ONLY.</li> <li>No deviation from the details shown on this drawing is allowed without CampbellReith's prior permission in writing.</li> </ol>
D D SIZES, EXISTING NOTE: DRAWING IS SUBJECT TO ALTERATION PENDING RECEIPT OF REVISED ARCHITECTURAL GA / SECTIONS, FOUNDATION SOLUTION, FOUL WATER POP-UPS / RWP	<ol> <li>Read this drawing with all Architects, Service Engineers and CampbellReith's relevant details and drawings. NB. Setting-out dimensions as per the Architect's drawings take precedence.</li> <li>All work is to be in accordance with the relevant specifications issued by CampbellReith, British Standard Codes of Practice, Statutory requirements and the Contract Documents.</li> <li>DRAWING STATUS         <ul> <li>P : PRELIMINARY - Evolving drawings for approvals, Tenders, Billings, etc.</li> <li>C : CONSTRUCTION - Fully developed drawings issued under instruction for construction.</li> </ul> </li> </ol>
LOCATIONS, POOL BACKWASH DISCHARGE, CCTV SURVEY AND STATUTORY CONSULTANTS.	ONLY STATUS C DRAWINGS TO BE USED FOR CONSTRUCTION.         6. SUITABILITY CODE         WORK IN PROGRESS:
RETE IS EM IS AIR WWA/1611/LL/105.	S0 - Work in progress         SHARED (NON-CONTRACTUAL):         S1 - For coordination, S2 - For information, S3 - For internal review and comment, S4 - For construction approval.         DOCUMENTATION (FOR CONTRACTOR PURPOSES):
N 600mm VE SHALL THIS DRAWING HAS BEEN BASED ON TOPOGRAPHICAL SURVEY PREPARED BY ENGINEERING LAND & BUILDING SURVEYS REF:B7542_TOPO_rev3 DATED MAY 2010 WHICH	<ul> <li>D1 - For costing, D2 - For Tender, D3 - For contractor design, D4 - For manufacture / procurement.</li> <li><u>CONSTRUCTION:</u></li> <li>A - For construction, B - For construction but with comments (i.e. areas in abeyance), C - Comprehensive revisions required.</li> </ul>
PROVIDED SHOULD BE REFERRED TO FOR KEY	<ul> <li>6 Existing details shown on this drawing including kerblines, sewerage pipework, stub connections, levels &amp; inverts etc. Must be confirmed on site by the contractor for their accuracy. If any discrepancies occur the engineer must be informed.</li> <li>7 The proposed building outlines shown on this drawing are indicative only. Refer to architects</li> </ul>
NOTE: ALL PIPEWORK NOT CAST WITHIN CONCRETE AND GREATER THAN 600mm BELOW SLABS SHALL BE uPVC IN ACCORDANCE WITH ALL RELEVANT MANUFACTURING STANDARDS, WITH A 150mm SHINGLE SURROUND, EXCEPT SEWER CONNECTIONS THAT SHALL BE VITRIFIED CLAY PIPES IN ACCORDANCE WITH BS EN 295.	<ul> <li>layouts for exact external outline of proposed blds.</li> <li>External rain water pipes, &amp; internal svp's, ss's, dp's &amp; floor gully locations/connections etc. Shown on this drawing are approximate/ indicative only. Refer to archs drgs for their exact locations &amp; types.</li> <li>All external adoptable storm pipework &amp; lateral connections shown falls of 1:120 unless stated otherwise.</li> <li>All external private storm pipework &amp; lateral connections shown on this drawing are to be 1000 &amp; are to have minimum falls of 1:100 unless stated otherwise. All external private foul pipework &amp; lateral connections shown on this drawing are to be 1000 &amp; are to have minimum falls of 1:100 unless stated otherwise. All external private foul pipework &amp; lateral connections shown on this dra are to have minimum falls of 1:100 unless stated otherwise.</li> <li>Existing adopted/non-adopted storm &amp; foul water mh's &amp; sewers which have been made redundant by new storm/foul systems, shall be abandoned/removed. Existing sewer &amp; manholes are to be abandoned / removed in compliance with L.A. specifications.</li> <li>Cover levels shown on this drawing are approximate &amp; are to be adjusted to suit finished pavement levels on site by contractor. Covers shall be orientated to suit pavement finishes.</li> <li>UNDERSLAB DRAINAGE CONNECTIONS:</li> </ul>
Contraction of the second seco	<ul> <li>a) All underslab foul connections upto first external inspection chamber/ manhole are to be 100Ø &amp; are to have a minimum fall of 1:40 unless stated otherwise. After first external inspection chamber/manhole connections are to be 100Ø &amp; have a minimum fall of 1:80 unless stated otherwise.</li> <li>b) All underslab storm connections upto first external inspection chamber/ manhole are to be</li> </ul>
	<ol> <li>All understab storm connections upto first external inspection chamber/maininger first external inspection chamber/manhole connections are to be 100Ø &amp; have a minimum fall of 1:100 unless stated otherwise.</li> <li>Final orientation &amp; position of first external chambers receiving underslab connections are to be determined on site by contractor.</li> <li>Bends along underslab connections are to be long radius 5-45°. Bends at bottom of stacks/soil vent pipes are to be long radius 90°.</li> <li>All under slab drainage connections are to be clear of unit foundations unless unavoidable. Refer to CRH structural drawings for exact location of unit foundations.</li> <li>Finished underslab drainage route connections ie. Bend &amp; straight combinations are to be determined on site to suit the number of bends in each connection is to be kept to a minimum.</li> <li>All adoptable storm sewerage runs to be laid soffit to soffit unless stated otherwise. All Adoptable foul sewerage runs to be laid soffit to soffit unless stated otherwise. All non-adoptable storm/foul sewerage to be laid soffit to soffit unless stated otherwise.</li> <li>Adoptable pipe work to be concrete or unified clay.</li> <li>Class Z concrete encasement required where vertical clearance between two pipes is less than 300mm.</li> <li>For the provision of land drainage if required refer to landscape architect for details/specification.</li> <li>At ladoptable drainage shown on this drawing shall be constructed in accordance with water authorities association sewers for adoption 7th edition.</li> </ol>
	LEGEND PROPOSED STORM WATER SEWER
	PROPOSED STORM WATER MANHOLE AND SEWER.
	RWP       PROPOSED RAIN WATER PIPE         OIC       PROPOSED STORM WATER         INSPECTION CHAMBER.
	G PROPOSED STORM WATER GULLY. ■ 35.650 PROPOSED STORM WATER PIPE
	+ INVERT LEVEL MARKER
	LINEAR CHANNEL AND SUMP PROPOSED COMBINED WATER
	MANHOLE AND SEWER
	STORAGE TANK
	<u>150Ø</u> PIPE INFO:
	_ · _ · _ · _ · _ · _ · _ DIRECTION OF FLOR DE FALL OF PIPE-LENGTH.     FALL OF PIPE-LENGTH.     FALL OF PIPE-LENGTH.     FALL OF PIPE-LENGTH.
*38.2 <sup>5</sup>	EXTENT OF BUILDING BASEMENT
38.291 38.210 38.210	PROPOSED SITE BOUNDARY
38.35 38.22	*CIPC - DENOTES CAST IN PILE CAP
50 50 78 78 78	*CIGB - DENOTES CAST IN GROUND BEAM *CTGB - DENOTES CUT THROUGH GROUND BEAM AND CELLCORE LOCALLY REMOVED
	NOTE: ALL PIPES TO PASS BENEATH GROUND BEAMS AND PILECAPS UNLESS NOTED OTHERWISE
37.00 31.1 37.00	
57.859 404 57.859 407 407 407 407 407 407 407 407	
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	P3ISSUED FOR TENDER01.12.16STP2ISSUED FOR TENDER28.06.16MGP1ISSUED FOR INFORMATION24.03.16MG
	Status/Rev Description Date By
	CampbellReith consulting engineers
	LONDON       020 7340 1700 □       □       MANCHESTER       0161 819 3060         SURREY       01737 784 500 ■       □       BIRMINGHAM       01675 467 484         BRISTOL       0117 916 1066 □       □       DUBAI       00 971 4345 7088         www.campbellreith.com       0       0       0
	Job Title GREENWOOD CENTRE Client KIER
G 1.50	PROPOSED STORM WATER DRAINAGE LAYOUT
	drawn     date     scale @ A0     C1 checked     CR Project No.       MG     JUN'16     1:100     RAI     12291
MH 8301 J CL \$7.013	Drg No. 12291-CRH-GC-XX-DR-C-5055 © Campbell Reith Hill LLP 2010

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XP Solutions	Network 2016.1.1	

#### STORM SEWER DESIGN by the Modified Rational Method

#### Design Criteria for Storm

Pipe Sizes STANDARD Manhole Sizes STANDARD

FSR Rainfall	Model	- England and Wales	
Return Period (years)	100	PIMP (%) 100	)
M5-60 (mm)	20.800	Add Flow / Climate Change (%) 0	)
Ratio R	0.441	Minimum Backdrop Height (m) 0.200	)
Maximum Rainfall (mm/hr)	50	Maximum Backdrop Height (m) 1.500	)
Maximum Time of Concentration (mins)	30	Min Design Depth for Optimisation (m) 1.200	)
Foul Sewage (l/s/ha)	0.000	Min Vel for Auto Design only (m/s) 1.00	)
Volumetric Runoff Coeff.	0.750	Min Slope for Optimisation (1:X) 500	)

Designed with Level Soffits

Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	ase (l/s)	k (mm)	HYD SECT	DIA (mm)	Section Type	Auto Design
1.000		0.023		0.014	5.00		0.600	0		Pipe/Conduit	ê
1.001	11.533	0.051	225.0	0.014	0.00	0.0		0		Pipe/Conduit	đ
1.002	7.870	0.035	225.0	0.010	0.00	0.0	0.600	0	225	Pipe/Conduit	æ
1.003	5.866	0.026	225.0	0.001	0.00	0.0	0.600	0	225	Pipe/Conduit	æ
1.004	8.868	0.039	225.0	0.017	0.00	0.0	0.600	0	225	Pipe/Conduit	æ
1.005	4.637	0.021	225.0	0.012	0.00	0.0	0.600	0	300	Pipe/Conduit	æ
2.000	6.592	0.066	100.0	0.029	5.00	0.0	0.600	0	150	Pipe/Conduit	8
2.001	10.437	0.104	100.0	0.000	0.00	0.0	0.600	0	150	Pipe/Conduit	ē
2.002	3.508	0.036	97.4	0.000	0.00	0.0	0.600	0	150	Pipe/Conduit	Ð
1.006	21.796	0.097	225.0	0.025	0.00	0.0	0.600	0	300	Pipe/Conduit	æ
3.000	2.401	0.153	15.7	0.000	5.00	0.0	0.600	0	100	Pipe/Conduit	Ů
1.007	7.089	0.181	39.2	0.017	0.00	0.0	0.600	0	300	Pipe/Conduit	ð
4.000	8.867	0.089	99.6	0.029	5.00	0.0	0.600	0	150	Pipe/Conduit	0

Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (1/s)	Foul (1/s)	Add Flow (1/s)	Vel (m/s)	Cap (1/s)	Flow (l/s)
1.000	50.00	5.10	35.515	0.014	0.0	0.0	0.0	0.87	34.5	1.9
1.001	50.00	5.32	35.492	0.028	0.0	0.0	0.0	0.87	34.5	3.8
1.002	50.00	5.47	35.440	0.038	0.0	0.0	0.0	0.87	34.5	5.2
1.003	50.00	5.59	35.405	0.039	0.0	0.0	0.0	0.87	34.5	5.3
1.004	50.00	5.76	35.379	0.056	0.0	0.0	0.0	0.87	34.5	7.6
1.005	50.00	5.83	35.265	0.068	0.0	0.0	0.0	1.04	73.8	9.2
2.000	50.00	5.11	35.600	0.029	0.0	0.0	0.0	1.00	17.8	3.9
2.001	50.00	5.28	35.534	0.029	0.0	0.0	0.0	1.00	17.8	3.9
2.002	50.00	5.34	35.430	0.029	0.0	0.0	0.0	1.02	18.0	3.9
1.006	50.00	6.18	35.244	0.123	0.0	0.0	0.0	1.04	73.8	16.6
3.000	50.00	5.02	35.500	0.000	0.0	0.0	0.0	1.96	15.4	0.0
1.007	50.00	6.23	35.147	0.140	0.0	0.0	0.0	2.52	178.1	18.9
4.000	50.00	5.15	35.340	0.029	0.0	0.0	0.0	1.01	17.8	3.9

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#### Network Design Table for Storm

PN	Length (m)	Fall (m)	Slope (1:X)	I.Area (ha)	T.E. (mins)	ase (l/s)	k (mm)	HYD SECT	DIA (mm)	Section Type	Auto Design
4.001	13.469	0.135	99.4	0.000	0.00	0.0	0.600	0	150	Pipe/Conduit	ď
5.000	3.035	0.379	8.0	0.000	5.00	0.0	0.600	0	100	Pipe/Conduit	æ
1.008	6.599	0.120	55.0	0.041	0.00	0.0	0.600	0	300	Pipe/Conduit	ď
6.000	6.187	0.041	150.9	0.000	5.00	0.0	0.600	0	150	Pipe/Conduit	ð
1.009 1.010	2.253 8.803		8.3 27.1	0.000	0.00		0.600 0.600	0		Pipe/Conduit Pipe/Conduit	⊕ ≜

## Network Results Table

PN	Rain (mm/hr)	T.C. (mins)	US/IL (m)	Σ I.Area (ha)	Σ Base Flow (l/s)		Add Flow (1/s)	Vel (m/s)	Cap (1/s)	Flow (l/s)
4.001	50.00	5.37	35.251	0.029	0.0	0.0	0.0	1.01	17.8	3.9
5.000	50.00	5.02	35.545	0.000	0.0	0.0	0.0	2.75	21.6	0.0
1.008	50.00	6.28	34.966	0.210	0.0	0.0	0.0	2.12	150.2	28.4
6.000	50.00	5.13	35.037	0.000	0.0	0.0	0.0	0.82	14.4	0.0
1.009 1.010	50.00 50.00		34.846 34.650	0.210 0.210	0.0	0.0	0.0		387.7 100.4	28.4 28.4

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# Manhole Schedules for Storm

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam.,L*W (mm)	PN	Pipe Out Invert Level (m)	Diameter (mm)	PN	Pipes In Invert Level (m)	Diameter (mm)	Backdrop (mm)
1	36.522	1.007	Open Manhole	450	1.000	35.515	225				
2	36.522	1.030	Open Manhole	450	1.001	35.492	225	1.000	35.492	225	
3	36.522	1.082	Open Manhole	450	1.002	35.440	225	1.001	35.440	225	
4	36.522	1.117	Open Manhole	450	1.003	35.405	225	1.002	35.405	225	
5	36.522	1.143	Open Manhole	1200	1.004	35.379	225	1.003	35.379	225	
6	36.522	1.257	Open Manhole	1200	1.005	35.265	300	1.004	35.340	225	
7	36.522	0.922	Open Manhole	450	2.000	35.600	150				
8	36.522	0.988	Open Manhole	450	2.001	35.534	150	2.000	35.534	150	
9	36.522	1.092	Open Manhole	450	2.002	35.430	150	2.001	35.430	150	
10	36.522	1.278	Open Manhole	1200	1.006	35.244	300	1.005	35.244	300	1
								2.002	35.394	150	
11	36.522	1.022	Open Manhole	450	3.000	35.500	100				
12	36.522	1.375	Open Manhole	1200	1.007	35.147	300	1.006	35.147	300	
								3.000	35.347	100	
13	36.522	1.182	Open Manhole	450	4.000	35.340	150				
14	36.522	1.271	Open Manhole	450	4.001	35.251	150	4.000	35.251	150	
15	36.522	0.977	Open Manhole	450	5.000	35.545	100				
16	36.522	1.556	Open Manhole	1200	1.008	34.966	300	1.007	34.966	300	
								4.001	35.116	150	
								5.000	35.166	100	
17	36.522	1.485	Junction	0	6.000	35.037	150				
18	36.522	1.676	Open Manhole	1200	1.009	34.846	300	1.008	34.846	300	
								6.000	34.996	150	
CWMH	36.522	1.947	Open Manhole	1200	1.010	34.650	225	1.009	34.575	300	
	36.575	2.250	Open Manhole	0		OUTFALL		1.010	34.325	225	

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#### PIPELINE SCHEDULES for Storm

# Upstream Manhole

PN	-	Diam (mm)		C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.000	0	225	1	36.522			Open Manhole	450
1.001	0	225	2	36.522			Open Manhole	450
1.002	0	225	3				Open Manhole	450
1.003	0	225	4				Open Manhole	450
1.004	0	225	5				Open Manhole	1200
1.005	0	300	6	36.522	35.265	0.957	Open Manhole	1200
2.000	0	150	7	36.522	35.600	0.772	Open Manhole	450
2.001	0	150	8	36.522	35.534	0.838	Open Manhole	450
2.002	0	150	9	36.522	35.430	0.942	Open Manhole	450
1.006	0	300	10	36.522	35.244	0.978	Open Manhole	1200
3.000	0	100	11	36.522	35.500	0.922	Open Manhole	450
1.007	0	300	12	36.522	35.147	1.075	Open Manhole	1200
4.000	0	150	13	36.522	35.340	1.032	Open Manhole	450
4.001	0	150	14	36.522	35.251	1.121	Open Manhole	450
5.000	0	100	15	36.522	35.545	0.877	Open Manhole	450
1.008	0	300	16	36.522	34.966	1.256	Open Manhole	1200
6.000	0	150	17	36.522	35.037	1.335	Junction	

#### Downstream Manhole

PN	Length	Slope	MH	C.Level	I.Level	D.Depth	MH	MH DIAM., L*W	
	(m)	(1:X)	Name	(m)	(m)	(m)	Connection	(mm)	
1.000	5.253	225.0	2	36.522	35.492	0.805	Open Manhole	450	
1.001	11.533	225.0	3	36.522	35.440	0.857	Open Manhole	450	
1.002	7.870	225.0	4	36.522	35.405	0.892	Open Manhole	450	
1.003	5.866	225.0	5	36.522	35.379	0.918	Open Manhole	1200	
1.004	8.868	225.0	6	36.522	35.340	0.957	Open Manhole	1200	
1.005	4.637	225.0	10	36.522	35.244	0.978	Open Manhole	1200	
	6.592		8				Open Manhole		
	10.437		9				Open Manhole		
2.002	3.508	97.4	10	36.522	35.394	0.978	Open Manhole	1200	
1.006	21.796	225.0	12	36.522	35.147	1.075	Open Manhole	1200	
3.000	2.401	1 5 7	12	36.522	35.347	1 075	Onen Manhala	1200	
3.000	2.401	13./	12	30.322	33.347	1.075	Open Manhole	1200	
1.007	7.089	39.2	16	36.522	34.966	1.256	Open Manhole	1200	
1.000		0012	10	00.022	01.900	1.200	opon namoro	1200	
4.000	8.867	99.6	14	36.522	35.251	1.121	Open Manhole	450	
4.001	13.469	99.4	16	36.522	35.116		Open Manhole		
5.000	3.035	8.0	16	36.522	35.166	1.256	Open Manhole	1200	
1.008	6.599	55.0	18	36.522	34.846	1.376	Open Manhole	1200	
6.000	6.187	150.9	18	36.522	34.996	1.376	Open Manhole	1200	

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#### PIPELINE SCHEDULES for Storm

#### Upstream Manhole

PN	-	Diam (mm)	C.Level (m)	I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.009 1.010						Open Manhole Open Manhole	1200 1200

#### Downstream Manhole

PN	Length (m)	Slope (1:X)			I.Level (m)	D.Depth (m)	MH Connection	MH DIAM., L*W (mm)
1.009	2.253	8.3	CWMH	36.522	34.575	1.647	Open Manhole	1200
1.010	8.803	27.1		36.575	34.325	2.025	Open Manhole	0

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#### Area Summary for Storm

Pipe	PIMP	PIMP	PIMP	Gross	Imp.	Pipe Total
Number	Туре	Name	(%)	Area (ha)	Area (ha)	(ha)
1.000	User	_	100	0.014	0.014	0.014
1.001	User	-	100	0.014	0.014	0.014
1.002	User	-	100	0.010	0.010	0.010
1.003	User	-	100	0.001	0.001	0.001
1.004	User	-	100	0.017	0.017	0.017
1.005	User	-	100	0.012	0.012	0.012
2.000	User	-	100	0.029	0.029	0.029
2.001	-	-	100	0.000	0.000	0.000
2.002	-	-	100	0.000	0.000	0.000
1.006	User	-	100	0.025	0.025	0.025
3.000	-	-	100	0.000	0.000	0.000
1.007	User	-	100	0.007	0.007	0.007
	User	-	100	0.011	0.011	0.017
4.000	User	-	100	0.029	0.029	0.029
4.001	-	-	100	0.000	0.000	0.000
5.000	-	-	100	0.000	0.000	0.000
1.008	User	-	100	0.010	0.010	0.010
	User	-	100	0.032	0.032	0.041
6.000	-	-	100	0.000	0.000	0.000
1.009	-	-	100	0.000	0.000	0.000
1.010	-	-	100	0.000	0.000	0.000
				Total	Total	Total
				0.210	0.210	0.210

Free Flowing Outfall Details for Storm

Outfall	Outfall	c.	Level	I.	Level		Min	D,L	W
Pipe Number	Name		(m)		(m)	I.	Level	(mm)	(mm)
							(m)		

1.010 36.575 34.325 34.525 0 0

#### Simulation Criteria for Storm

Volumetric Runoff Coeff	0.750	Additional Flow - % of Total Flow O	.000
Areal Reduction Factor	1.000	MADD Factor * 10m³/ha Storage 2	2.000
Hot Start (mins)	0	Inlet Coeffiecient 0	.800
Hot Start Level (mm)	0	Flow per Person per Day (1/per/day) 0	.000
Manhole Headloss Coeff (Global)	0.500	Run Time (mins)	60
Foul Sewage per hectare (l/s)	0.000	Output Interval (mins)	1

Number of Input Hydrographs 0 Number of Offline Controls 0 Number of Time/Area Diagrams 0 Number of Online Controls 1 Number of Storage Structures 1 Number of Real Time Controls 0

#### Synthetic Rainfall Details

Rainfall Model	FSR	Profile Type Summer
Return Period (years)	100	Cv (Summer) 0.750
Region Enc	gland and Wales	Cv (Winter) 0.840
M5-60 (mm)	20.800 Storm	Duration (mins) 30
Ratio R	0.441	

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XP Solutions	Network 2016.1.1	
<u>O1</u>	line Controls for Storm	
Hydro-Brake® Optimum	Manhole: 18, DS/PN: 1.009, Vol	ume (m <sup>3</sup> ): 2.4
	Unit Reference MD-SHE-0163-1330-12	
	Design Head (m)	1.200
I	esign Flow (l/s)	13.3
		culated
	Objective Minimise upstream Application	Surface
	Sump Available	Yes
	Diameter (mm)	163
	Invert Level (m)	34.846
Minimum Outlet Pi		225
Suggested Manho	le Diameter (mm)	1500
Control Points Head (r	a) Flow (1/s) Control Points	Head (m) Flow (l/s)
Design Point (Calculated) 1.20	0 13.3 Kick-F	lo® 0.801 11.0
Flush-Flo™ 0.36	4 13.3 Mean Flow over Head Ram	nge - 11.5
The hydrological calculations have been be specified. Should another type of contro- storage routing calculations will be inva-	device other than a Hydro-Brake Opt	

Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow (l/s)	Depth (m)	Flow $(1/s)$	Depth (m)	Flow (l/s)
0.100	5.8	0.800	11.0	2.000	16.9	4.000	23.6	7.000	30.9
0.200	12.5	1.000	12.2	2.200	17.7	4.500	25.0	7.500	31.9
0.300	13.2	1.200	13.3	2.400	18.5	5.000	26.3	8.000	32.9
0.400	13.3	1.400	14.3	2.600	19.2	5.500	27.5	8.500	33.9
0.500	13.1	1.600	15.2	3.000	20.6	6.000	28.7	9.000	34.9
0.600	12.8	1.800	16.1	3.500	22.1	6.500	29.8	9.500	35.8

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## Storage Structures for Storm

Tank or Pond Manhole: 17, DS/PN: 6.000

Invert Level (m) 35.037

Depth (m) Area (m<sup>2</sup>) Depth (m) Area (m<sup>2</sup>) Depth (m) Area (m<sup>2</sup>)

0.000 8	30.0	0.400	80.0	0.401	0.0
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XP Solutions	Network 2016.1.1		
<u>1 year Return Period Summa</u>	ary of Critical Results by Ma	aximum Level (Rank 1)	for Storm
	Simulation Criteria		
	ction Factor 1.000 Additional Fl		
	Start (mins) 0 MADD Fact		
	Level (mm) 0	Inlet Coefficcient 0.80	
Manhole Headloss Coe Foul Sewage per he	eff (Global) 0.500 Flow per Person	per Day (1/per/day) 0.00	00
Number of Input Hydrograph	as 0 Number of Offline Controls	0 Number of Time/Area Dia	igrams 0
1 1 9 1	s 1 Number of Storage Structures		2
	Synthetic Rainfall Details		
Rainfall Model		300 Cv (Summer) 0.750	
Region	England and Wales Ratio R 0.4	141 Cv (Winter) 0.840	
Margin for Flo	ood Risk Warning (mm)	300.0	
Margin for Flo	ood Risk Warning (mm) Analysis Timestep 2.5 Second I		
Margin for Fl	-		
Margin for Fl	Analysis Timestep 2.5 Second 3	Increment (Extended)	
Margin for Fl	Analysis Timestep 2.5 Second : DTS Status	Increment (Extended) ON	
Margin for Fl	Analysis Timestep 2.5 Second : DTS Status DVD Status Inertia Status	Increment (Extended) ON OFF OFF	
	Analysis Timestep 2.5 Second : DTS Status DVD Status Inertia Status Profile(s)	Encrement (Extended) ON OFF OFF Summer and Winter	
	Analysis Timestep 2.5 Second : DTS Status DVD Status Inertia Status Profile(s) n(s) (mins) 15, 30, 60, 120, 240,	Encrement (Extended) ON OFF OFF Summer and Winter	

												5 a = 0.1.a = 9 0 a			
	US/MH			Return	Climate	First	t (X)	First (Y)	First (Z)	Overflow	Level	Depth	Volume	Flow /	
PN	Name	S	torm	Period	Change	Surcl	harge	Flood	Overflow	Act.	(m)	(m)	(m³)	Cap.	
1.000	1	15 T	Winter	1	+0%	30/15	Winter				35.561	-0.179	0.000	0.08	
1.001	2	15 T	Winter	1	+0%	30/15	Summer				35.546	-0.171	0.000	0.13	
1.002	3	15 T	Winter	1	+0%	30/15	Summer				35.507	-0.159	0.000	0.19	
1.003	4	15 1	Winter	1	+0읭	30/15	Summer				35.476	-0.155	0.000	0.20	
1.004	5	15 1	Winter	1	+0%	30/15	Summer				35.458	-0.147	0.000	0.26	
1.005	6	15 1	Winter	1	+0%	30/15	Summer				35.358	-0.207	0.000	0.18	
2.000	7	15 1	Winter	1	+0%	30/15	Winter				35.655	-0.095	0.000	0.29	
2.001	8	15 1	Winter	1	+0%	30/15	Summer				35.588	-0.096	0.000	0.27	
2.002	9	15 1	Winter	1	+0%	30/15	Summer				35.493	-0.086	0.000	0.37	
1.006	10	15 1	Winter	1	+0%	30/15	Summer				35.345	-0.199	0.000	0.25	
3.000	11	60 T	Winter	1	+0%	30/15	Summer				35.500	-0.100	0.000	0.00	
1.007	12	15 1	Winter	1	+0%	30/15	Summer				35.261	-0.186	0.000	0.17	
4.000	13	15 1	Winter	1	+0%	30/15	Summer				35.394	-0.096	0.000	0.28	
4.001	14	15 T	Winter	1	+0%	30/15	Summer				35.304	-0.097	0.000	0.26	
5.000	15	60 T	Winter	1	+0%	30/15	Winter				35.545	-0.100	0.000	0.00	
1.008	16	15 T	Winter	1	+0%	30/15	Summer				35.252	-0.013	0.000	0.30	
6.000	17	15 T	Winter	1	+0%	30/15	Summer				35.081	-0.106	0.000	0.18	
1.009	18	15 T	Winter	1	+0%	1/15	Summer				35.240	0.094	0.000	0.10	
1.010	CWMH	60 3	Summer	1	+0읭						34.711	-0.164	0.000	0.16	

				Pipe		
		US/MH	Overflow	Flow		Level
	PN	Name	(1/s)	(l/s)	Status	Exceeded
:	1.000	1		2.1	OK	
	1.001	2		3.8	OK	
	1.002	3		5.2	OK	
	1.003	4		5.3	OK	
-	1.004	5		7.4	OK	
-	1.005	6		8.8	OK	
, ,	2.000	7		4.4	OK	
2	2.001	8		4.3	OK	
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1 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

			Pipe		
	US/MH	Overflow	Flow		Level
PN	Name	(1/s)	(l/s)	Status	Exceeded
2.002	9		4.4	OK	
1.006	10		16.1	OK	
3.000	11		0.0	OK	
1.007	12		17.7	OK	
4.000	13		4.3	OK	
4.001	14		4.3	OK	
5.000	15		0.0	OK	
1.008	16		26.0	OK	
6.000	17		2.2	OK*	
1.009	18		13.3	SURCHARGED	
1.010	CWMH		13.3	OK	

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Raven House	Greenwood Centre	
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XP Solutions	Network 2016.1.1	1
30 year Return Period Summary of Cr	ritical Results by Maximum Level (Rank 1)	for Storm
30 year Return Period Summary of Cr	ritical Results by Maximum Level (Rank 1)	for Storm
<b>_</b>	citical Results by Maximum Level (Rank 1) Simulation Criteria	for Storm
<b>4</b>	<u> </u>	for Storm
Areal Reduction Factor Hot Start (mins)	Simulation Criteria r 1.000 Additional Flow - % of Total Flow 0.000 ) 0 MADD Factor * 10m³/ha Storage 2.000	for Storm
Areal Reduction Factor	Simulation Criteria r 1.000 Additional Flow - % of Total Flow 0.000 ) 0 MADD Factor * 10m³/ha Storage 2.000	for Storm
Areal Reduction Factor Hot Start (mins) Hot Start Level (mm)	Simulation Criteria r 1.000 Additional Flow - % of Total Flow 0.000 ) 0 MADD Factor * 10m³/ha Storage 2.000	for Storm
Areal Reduction Factor Hot Start (mins) Hot Start Level (mm)	Simulation Criteria r 1.000 Additional Flow - % of Total Flow 0.000 ) 0 MADD Factor * 10m³/ha Storage 2.000 ) 0 Inlet Coeffiecient 0.800 ) 0.500 Flow per Person per Day (1/per/day) 0.000	for Storm

	S	ynth	etic R	ainfall	L Deta	ails			
Rainfall Model			FSR	M5-60	(mm)	20.800	Cv	(Summer)	0.750
Region	England	and	Wales	Rat	io R	0.441	Cv	(Winter)	0.840

Margin f	for	Flood	Risk Warn	ing	g (mm)				300.0
			Analysis	Tir	nestep	2.5	Second	Increment	(Extended)
			DI	'S S	Status				ON
			DV	D S	Status				OFF
			Inerti	a S	Status				OFF

 Profile(s)
 Summer and Winter

 Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440

 Return Period(s) (years)
 1, 30, 100

 Climate Change (%)
 0, 0, 20

	US/MH			Return	Climate	First (X)	First (Y)	First (Z)	Overflow	Water Level	Surcharged Depth	Flooded Volume	Flow /
PN	Name	S	Storm		Change	Surcharge	Flood	Overflow	Act.	(m)	(m)	(m <sup>3</sup> )	Cap.
1.000	1	15	Winter	30	+0%	30/15 Winte	r			35.774	0.034	0.000	0.19
1.001	2	15	Winter	30	+0%	30/15 Summe	r			35.770	0.054	0.000	0.33
1.002	3	15	Winter	30	+0%	30/15 Summe	r			35.759	0.094	0.000	0.47
1.003	4	15	Winter	30	+0%	30/15 Summe	r			35.749	0.118	0.000	0.47
1.004	5	15	Winter	30	+0%	30/15 Summe	r			35.740	0.136	0.000	0.62
1.005	6	15	Winter	30	+0%	30/15 Summe	r			35.723	0.158	0.000	0.36
2.000	7	15	Winter	30	+0%	30/15 Winte	r			35.781	0.031	0.000	0.70
2.001	8	15	Winter	30	+0%	30/15 Summe	r			35.760	0.076	0.000	0.62
2.002	9	15	Winter	30	+0%	30/15 Summe	r			35.730	0.150	0.000	0.76
1.006	10	15	Winter	30	+0%	30/15 Summe	r			35.716	0.173	0.000	0.48
3.000	11	15	Winter	30	+0%	30/15 Summe	r			35.683	0.083	0.000	0.02
1.007	12	15	Winter	30	+0%	30/15 Summe	r			35.683	0.236	0.000	0.33
4.000	13	15	Winter	30	+0%	30/15 Summe	r			35.731	0.241	0.000	0.61
4.001	14	15	Winter	30	+0%	30/15 Summe	r			35.700	0.299	0.000	0.57
5.000	15	15	Winter	30	+0%	30/15 Winte	r			35.665	0.020	0.000	0.01
1.008	16	15	Winter	30	+0%	30/15 Summe	r			35.665	0.399	0.000	0.62
6.000	17	30	Winter	30	+0%	30/15 Summe	r			35.319	0.132	0.000	0.96
1.009	18	15	Winter	30	+0%	1/15 Summe	r			35.634	0.489	0.000	0.10
1.010	CWMH	60	Summer	30	+0%					34.711	-0.164	0.000	0.16

			Pipe		
	US/MH	Overflow	Flow		Level
PN	Name	(1/s)	(1/s)	Status	Exceeded
1.000	1		4.7	SURCHARGED	
1.001	2		9.8	SURCHARGED	
1.002	3		12.9	SURCHARGED	
1.003	4		12.3	SURCHARGED	
1.004	5		17.5	SURCHARGED	
1.005	6		17.4	SURCHARGED	
2.000	7		10.5	SURCHARGED	
2.001	8		9.8	SURCHARGED	

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30 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

			Pipe		
	US/MH	Overflow	Flow		Level
PN	Name	(1/s)	(l/s)	Status	Exceeded
2.002	9		0 0	GUDGUADCED	
	-		9.0	SURCHARGED	
1.006	10		31.3	SURCHARGED	
3.000	11		0.2	SURCHARGED	
1.007	12		35.6	SURCHARGED	
4.000	13		9.5	SURCHARGED	
4.001	14		9.3	SURCHARGED	
5.000	15		0.2	SURCHARGED	
1.008	16		53.6	SURCHARGED	
6.000	17		12.2	SURCHARGED*	
1.009	18		13.3	SURCHARGED	
1.010	CWMH		13.3	OK	

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Date 01/02/2017	Designed by MJB		
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XP Solutions	Network 2016.1.1		
Hot St Hot Start Manhole Headloss Coef Foul Sewage per hec Number of Input Hydrographs Number of Online Controls Rainfall Model	s 0 Number of Offline Controls s 1 Number of Storage Structures <u>Synthetic Rainfall Details</u> FSR M5-60 (mm) 20. England and Wales Ratio R 0.	tor * 10m³/ha Storage 2.000 Inlet Coeffiecient 0.800 n per Day (1/per/day) 0.000 0 Number of Time/Area Diag 1 Number of Real Time Cont 800 Cv (Summer) 0.750 441 Cv (Winter) 0.840	) ) grams O
	ood Risk Warning (mm) Analysis Timestep 2.5 Second DTS Status DVD Status Inertia Status Profile(s)	300.0 Increment (Extended) ON OFF OFF Summer and Winter	
	Analysis Timestep 2.5 Second DTS Status DVD Status Inertia Status Profile(s) h(s) (mins) 15, 30, 60, 120, 240,	Increment (Extended) ON OFF OFF Summer and Winter	

	US/MH		Return	Climate	Firs	t (X)	First (Y)	First (Z)	Overflow	Water Level	Surcharged Depth	Flooded Volume	Flow /
PN	Name	Storm		Change		harge	Flood	Overflow	Act.	(m)	(m)	(m <sup>3</sup> )	Cap.
1.000	1	15 Wint	er 100	+20%	30/15	Winter				36.475	0.735	0.000	0.24
1.001	2	15 Wint	er 100	+20%	30/15	Summer				36.470	0.753	0.000	0.41
1.002	3	15 Wint	er 100	+20%	30/15	Summer				36.453	0.788	0.000	0.60
1.003	4	15 Wint	er 100	+20%	30/15	Summer				36.437	0.807	0.000	0.63
1.004	5	15 Wint	er 100	+20%	30/15	Summer				36.425	0.820	0.000	0.75
1.005	6	15 Wint	er 100	+20%	30/15	Summer				36.400	0.835	0.000	0.51
2.000	7	15 Wint	er 100	+20%	30/15	Winter				36.520	0.770	0.000	0.86
2.001	8	15 Wint	er 100	+20%	30/15	Summer				36.483	0.799	0.000	0.79
2.002	9	15 Wint	er 100	+20%	30/15	Summer				36.427	0.848	0.000	1.05
1.006	10	15 Wint	er 100	+20%	30/15	Summer				36.392	0.848	0.000	0.69
3.000	11	15 Wint	er 100	+20%	30/15	Summer				36.343	0.743	0.000	0.04
1.007	12	15 Wint	er 100	+20%	30/15	Summer				36.344	0.897	0.000	0.47
4.000	13	15 Wint	er 100	+20%	30/15	Summer				36.452	0.962	0.000	0.87
4.001	14	15 Wint	er 100	+20%	30/15	Summer				36.395	0.994	0.000	0.80
5.000	15	15 Wint	er 100	+20%	30/15	Winter				36.315	0.670	0.000	0.02
1.008	16	15 Wint	er 100	+20%	30/15	Summer				36.317	1.051	0.000	0.88
6.000	17	30 Wint	er 100	+20%	30/15	Summer				35.438	0.251	0.000	0.84
1.009	18	15 Wint	er 100	+20%		Summer				36.222	1.077	0.000	0.11
1.010	CWMH	15 Wint	er 100	+20%						34.713	-0.162	0.000	0.18

		0	Pipe		• 1
PN	Name	Overflow (1/s)	flow (1/s)	Status	Level Exceeded
	manie	(1)0)	(1)0)	blacab	Intecueu
1.000	1		6.2	FLOOD RISK	
1.001	2		12.1	FLOOD RISK	
1.002	3		16.7	FLOOD RISK	
1.003	4		16.5	FLOOD RISK	
1.004	5		21.1	FLOOD RISK	
1.005	6		24.2	FLOOD RISK	
2.000	7		12.9	FLOOD RISK	
2.001	8		12.5	FLOOD RISK	
		1000 001	<u> </u>		
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Surrey RH1 1SS		Micro
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100 year Return Period Summary of Critical Results by Maximum Level (Rank 1) for Storm

			Pipe		
	US/MH	Overflow	Flow		Level
PN	Name	(1/s)	(l/s)	Status	Exceeded
2,002	9		12.4	FLOOD RISK	
1.006	10		44.6		
3.000	11		0.4	FLOOD RISK	
1.007	12		50.1	FLOOD RISK	t.
4.000	13		13.6	FLOOD RISK	
4.001	14		13.1	FLOOD RISK	t.
5.000	15		0.4	FLOOD RISK	t.
1.008	16		76.6	FLOOD RISK	
6.000	17		10.7	SURCHARGED*	
1.009	18		14.1	FLOOD RISK	t.
1.010	CWMH		14.1	OF	Ξ.