Regards

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100 Avenue Road Swiss Cottage - Infrastructure Protection Works B112 Jubilee Line

Document reference: 1813694-RPT-TRK-B112-001-01

100 Avenue Road Project Infrastructure Protection Works Swiss Cottage to St. John's Wood Northbound and Southbound Jubilee Lines

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	Engineering Design Manager	H.J.Din	

Document History

Revision	Date	Summary of changes
01	10/06/2016	First draft issue



1. Executive Summary

An assessment of the existing track geometry condition has been undertaken to assess the impact of any ground movements arising as a result of demolition for the proposed redevelopment at 100 Avenue Road, London, NW3.

100 Avenue Road is located in the vicinity of Swiss Cottage London Underground Train Station above the Northbound and Southbound Jubilee Line tunnels.

The track geometry condition on both the Northbound and Southbound roads has been found to be out of tolerance with a number of safety standard exceedances and maintenance limit exceedances when compared to a theoretical design alignment. There is little concern with regard to wheel unloading characteristic, with exception in the area of point numbers 105 & 106 on the Northbound, as shown by the twist assessment in the appendix. These areas marginally exceed the Maintenance Target (MT).

This assessment covers the effect of track movements and existing tunnel clearance only.

The trigger values are set conservatively. Some of the trigger values are not the absolute values specified in standards S1156 and S1159.

Track trigger values are detailed in Section 6 of this document.

Where possible, trigger values are aligned to actions prescribed in the Standard.

Where applicable, a "Change of" value relative to the survey baseline readings have been used.

Issues that require further action are highlighted in red



Contents

5		
1.	Executive Summary	2
2.	Introduction	4
3.	Track Geometry Condition Assessment	5
4.	Infringements to Structure Profile Assessment – S1156	7
5.	Discussion / Summary	7
6.	Survey Trigger Values	8
7.	General Recommendations / Actions	10
8.	Appendices	11



2. Introduction

This report has been prepared by London Underground Track Engineering (LUTE) based upon survey information supplied by the London Underground Survey Team (LUST). The report relates to the existing track geometry and clearances for the Jubilee Line tracks between Swiss Cottage and St. John's Wood adjacent to the development at 100 Avenue Road.

This report gives an overview of existing track conditions showing track dimensions and tolerances relative to track standard:

Track - Dimensions and tolerances No S1159

Track - Gauging and Clearances No S1156



3. Track Geometry Condition Assessment

Compliance to LUL category 1 standard S1159 is described in the following sections.

Notes

- Data is based upon the static track position
- As design data is unavailable, the existing alignment has been 'design smoothed' to enable
 an allowance for levels, transitions, vertical curves and gradients. This information is not
 exact but it does give a good indication of the track geometry.
- Survey data at 2m and 5m intervals has been provided by LU Survey Team dated 2nd October 2014.

3.1 Northbound

An assessment of the track geometry against the following clauses (where available) within S1159 has been undertaken. The table summarises areas where the standards have been exceeded and describes the worst case.

NB Jubilee	Maintenance Target	Maintenance Limit	Safety Standard
Deviation between consecutive levels	5	7	10
(clause 2.1.1):	5	7	15
Deviation between vertical position of	-14 / +5	-16 / +5	-18 / +5
running surfaces (2.1.6):	-14 & 5	-16 & 5	10
Deviation between lateral alignments	8	10	15
(2.2.1):	8	10	16
Deviation from lateral alignment (2.2.4):	-8 / +8	-10 / +10	-13 / +13
, (2.2.1).	-8 & 8	-10 & 10	16
Deviation from marked cant (2.3):	-10 / +8	-12 / +10	-15 / +10
outit (2.0).	-6 & 4		
Deviation in gauge (3.1):	-5 / +11	-7 / +22	-10 / +27
(0.1).	-5	-7	-8

Table 1 - Summary assessment of track geometry NB

Based upon static survey data for **10m twist (2.5.2)** it is noted that the results are within limiting values.



3.2 Southbound

An assessment of the track geometry against the following clauses (where available) within S1159 has been undertaken. The table summarises areas where the standards have been exceeded and describes the worst case.

Maintenance Target	Maintenance Limit	Safety Standard
5	7	10
5	7	14
-14 / +5	-16 / +5	-18 / +5
-14 & 5	9	9
8	10	15
8	12	
-8 / +8	-10 / +10	-13 / +13
-9 & 8	10	14
-10 / +8	-12 / +10	-15 / +10
-5 / +11	-7 / +22	-10 / +27
	5 5 -14/+5 -14 & 5 8 8 -8/+8 -9 & 8 -10/+8	5 7 5 7 -14/+5 -16/+5 -14 & 5 9 8 10 8 12 -8/+8 -10/+10 -9 & 8 10 -10/+8 -12/+10

Table 2 - Summary assessment of track geometry SB

Based upon static survey data for **10m twist (2.5.2)** it is noted that the results are within limiting values.



4. Infringements to Structure Profile Assessment - S1156

A clearance assessment by LUTE has been included in this report based upon survey data from September 2014.

4.1 Northbound Infringements

The worst case infringement is stated as -108mm using the "C4 Structure Profile Tunnel and Platform Offside". We believe this to be the correct profile as the infringement is under the platform nosing.

An inspection is recommended at this location to verify structure clearances.

4.2 Southbound Infringements

The worst case infringement is stated as -126mm using the "C4 Structure Profile Tunnel and Platform Offside". We believe this to be the correct profile as the infringement is under the platform nosing.

An inspection is recommended at this location to verify structure clearances.

5. Discussion / Summary

Based upon the TRV track survey for static 2m/10m/wheel unload, the track cant appears to be acceptable.

Other areas of the track geometry appear to be in a less favorable condition as noted in the tables above.

The report produced by URS Geotechnical Engineers on 100 Avenue Road, Swiss Cottage (Document No.47066169 Rev 2, dated July 2015) shows the following as expected ground movements:

- <u>During the Un-load Stage (i.e. demolition and excavation)</u>. Maximum heave of 10mm in the zones with the largest load removal.
- <u>During the Re-Load Stage (i.e. construction phase).</u> Maximum net settlement on the southbound track is 5mm.

The structural integrity of the tunnel will be beyond the scope of this report; advice should be sought from the relevant LU Civil Engineer.

Based on these findings, advice must be sought from the LU Asset Performance Track Infrastructure Manager, Kyle Newman, to establish if there is a history of geometry non-compliance in this area. In addition, the clearance non-compliance needs to be checked to establish any risk.



6. Survey Trigger Values

If Civils values are triggered, it is presumed this will initiate a further survey, to which the Track trigger values can be applied to for further assessment. It is requested that the Civils trigger values are supplied to LUTE so that the process and actions can be understood.

Based upon URS Geotechnical Engineer Calculations & Report, survey trigger values are detailed below. Any breach of the trigger values will necessitate the implementation of the specified actions. They are not all the absolute values in standards S1156/S1159, some are based upon any detected **change** from the OPs surveyed baseline set before works commence.

Table 3 - Summary of trigger values based on track assessment

Trigger	Clearance	2m Twist	10m Twist	Cant	Lateral Alignment	Vertical Profile
	S1156 (5.2.9)	S1159 (2.4)	S1159 (2.5.1)	S1159 (2.3)	S1159 (2.2.1)	S1159 (2.1.1)
GREEN	Change of clearance ≤ 3mm	Absolute Value(s)* < 20mm	Absolute Value(s)* < 37mm	Change of cant ≤ 3mm	Change of overlapping versines ≤ 3mm	Change from baseline ≤ 3mm
AMBER	Change of clearance > 3mm ≤ 6mm	Absolute Value(s)* ≥ 20mm < 25mm	Absolute Value(s)* ≥ 37mm < 40mm	Change of cant > 3mm ≤ 6mm	Change of overlapping versines > 3mm ≤ 6mm	Change from baseline > 3mm ≤ 6mm
RED	Change of clearance > 6mm ≤ 12mm	Absolute Value(s)* ≥ 25mm < 30mm	Absolute Value(s)* ≥ 40mm < 50mm	Change of cant > 6mm ≤ 12mm	Change of overlapping versines > 6mm ≤ 12mm	Change from baseline > 6mm ≤ 12mm
BLACK	Change of clearance > 12mm	Absolute Value(s)* ≥ 30mm	Absolute Value(s)* ≥ 50mm	Change of cant > 12mm	Change of overlapping versines > 12mm	Change from baseline > 12mm

^{*} Absolute values are taken directly from Standard S1159.

- Where existing results are compliant, "Absolute" values are taken directly from the standard.
- Where existing values are non-compliant "Change of " values have been supplied.
- Where ± values exist in the Standard, to avoid unnecessary complexity the trigger values have been supplied as "Change of......" Values due to the relatively small predicted movements.



- The LU Standard minimum actions (detailed in S1156 & S1159) have been adjusted to 'trigger values' and relate to the worst case site situation, i.e. allowing for irregularities or non-compliance already within the track. A summary of the worst case situation is detailed within this document.
- Should a red or black trigger value be breached and actioned, i.e. a speed restriction imposed or trains stopped based upon the trigger values, then LU Engineering Standards (S1159 & S1156) minimum actions must be referenced by the on-site T002/3 to avoid unnecessary disruption of the passenger service as the movement causing the trigger to be breached may not have occurred at the worst case location.

Trigger	Actions
GREEN	No action required.
AMBER	Inform LUTE and Jubilee Line Track Manager ASAP with details of the recorded Track movement.
RED	 a. Contact the Duty Operations Manager Engineering (DOME)/Duty Engineer/ Signals Operations Manager to alert them of movement and arrange for a 20mph speed restriction; b. Inform LUTE, Jubilee Line Track Manager and Infrastructure Protection ASAP with details of the recorded tunnel movement; c. Inform the Jubilee Line Track Manager and Duty Engineer to arrange for rectification works as necessary and to undertake an assessment (by a THP T002/3) on whether it is safe to continue to run trains at normal speed. d. The Site Contractor via LU Infrastructure Protection is to arrange and undertake a track survey to check the recorded movements against the baseline track survey data. New track survey is to be issued to LUTE within 48 hours of the survey having taken place.
BLACK	 a. Contact the DOME/Duty Engineer and/or the Signals System Manager to arrange for the suspension of trains immediately; b. Inform LUTE, Jubilee Line Track Manager and Infrastructure Protection ASAP with details of the recorded tunnel movement; c. Inform the Jubilee Line Track Manager and Duty Engineer to arrange for rectification works as necessary and to undertake an assessment (by a THP T002/3) on whether it is safe to continue to run trains.



7. General Recommendations / Actions

- To avoid the possibility of track maintenance work causing a breach of trigger values, close contact with the local track manager via the Outside Parties Engineer is recommended.
 LU Asset Performance –Jubilee Line Kyle Newman
 LU Capital Programmes Infrastructure Protection Engineer Peter Brierley
- > LUTE must be informed of any breach in the trigger values ASAP so that track assessments can take place to help alleviate the impact of that breach.
- The Emergency Preparedness Plan must include details on how a nominated Track Hand-Back Person (THP) T002/3 will be contacted should the relevant trigger value be breached.
 - The THP T002/3 must have the availability of a tunnel gauge, be competent with its use, and will need adequate help with its transportation to site.
 Note: This is a 3 person operation.
 - The THP T002/3 must also be competent to check:-
 - 10m Twist as described in LU Engineering Standards S1159, Clause 2.5.1.
 - 2m Twist as described in LU Engineering Standards S1159, Clause 2.4.
 - Change in Cross Level over 5 sleepers as described in LU Engineering Standards S1159, Clause 2.3.
 - Lateral Alignment deviation as described in LU Engineering Standards S1159, Clause 2.2.4.
 - Versine variation as described in LU Engineering Standards S1159, Clause
 2.2.1. Note: This is a 3 person operation.
 - Vertical Profile as described in LU Engineering Standards S1159, Clause 2.1.1.
 - Note: This is a 3 person operation.
 - A general inspection of track condition.
- ➤ Liaison to enable the THP T002/3 attendance can be made as follows:
- ➤ LU Asset Performance –Jubilee Line Kyle Newman

8. Appendices

- i. Northbound 5m Station Track Geometry Assessment
- ii. Southbound 5m Station Track Geometry Assessment
- iii. Northbound Clearance Assessment
- iv. Southbound Clearance Assessment
- v. Northbound Twist & Wheel Unload
- vi. Southbound Twist & Wheel Unload



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Southbound 5m Station Track Geometry Assessment

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iii. Northbound Clearance Assessment

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Track Engineering

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Clearance Log Track 1	Local Database	Local Database														
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v. Northbound Twist & Wheel Unload Wheel Unload Monitoring - Track Stations @ 2M Intervals

Input by		AV		Input Da	nte	25/1	11/2015		
				Checked					
Trigger	values		- Constitution of the Cons			-	-		
		load constants		12	166.7	35	286	40	5
	2 metre	2.611		20	100	37	270.27	85	7
	10 metre	0.650		25	80	40	250	100	10
		Cant		Т		Twis	st		Vertica
Point No.		Cant (mm)		2m Track		10m Track		Vheel	Difference in level from
		Guille (IIIII)	LiR	Twist (mm)	Gradient 1 in	Twist (mm)	Gradient 1 in	Unload (%)	baseline. Deviations over 5m (absolute) (mm)
1		59	R	*		*			
2		55	R.	-4.0	*	*			
3		56	R	1.0	*	*			
4		54	R	-2.0	*	*			0.0
5		52	R	-2.0	*	*			0.0
6		56	R	4.0	500.0	-3.0	*	9.8	0.0
7		57	R	1.0	*	2.0	*	3.9	0.0
8		56	R	-1.0	*	0.0	2	-5.9	0.0
9		55	R	-1.0	*	1.0	*	-6.5	0.0
10		56	R	1.0	*	4.0	*	5.2	0.0
11		55	R	-1.0	2	-1.0	*	-7.8	0.0
12		52	R	-3.0	*	-5.0	2	-12.4	0.0
13		51	R	-1.0	*	-5.0	2	-7.8	0.0
14		49	R	-2.0	*	-6.0	*	-10.4	0.0
15		48	R	-1.0	2	-8.0	2	-10.4	0.0
16		47	R	-1.0	*	-8.0	2	-12.4	0.0
17		45	R	-2.0	*	-7.0	*	-15.6	0.0
18		43	R	-2.0	*	-8.0	*	-15.6	0.0
19		41	R	-2.0	*	-8.0	*	-16.3	0.0
20		36	R	-5.0	400.0	-12.0	*	-22.8	0.0
21		32	R	-4.0	*	-15.0	*	-22.1	0.0
22		29	R	-3.0	x	-16.0	*	-18.9	0.0
23		27	R	-2.0		-16.0		-17.6	0.0
24		24	R	-3.0		-17.0	***************************************	-19.5	0.0
25		21	R	-3.0	*	-15.0	***************************************	-19.5	0.0
26		14	R	-7.0	285.7	-18.0	*	-30.0	0.0
27		12	R	-2.0		-17.0	*	-16.3	0.0
28		8	R	-4.0		-19.0	***************************************	-22.8	0.0
29		6	R	-2.0	***************************************	-18.0		-16.9	0.0
30		3	R	-3.0	***************************************	-18.0	*	-19.5	0.0
31		0		3.0	*	14.0	*	16.9	0.0
32		1	R	1.0	*	-11.0	*	5.2	0.0
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34	6	<u>-</u>		333.3	12.0	***************************************	15.6	0.0
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36	0	<u>L</u>	-1.0 -5.0	400.0	4.0	*	-15.7	0.0 0.0
37	3	<u>_</u>		400.0 400.0	2.0	*	-15.7 -13.7	0.0
38	2	R R	-5.0	400.0		*	-5.2	0.0
39	2	R	0.0		-8.0 9.0	***************************************	11.1	0.0
40	0		2.0		-9.0	2	3.3	0.0
41		R R R	1.0		-9.0	*	-2.6	0.0
42		<u> </u>	0.0	***************************************	-4.0	*	13	0.0
43	1	K	0.0		-1.0	*	3.0	0.0
44	0		1.0		2.0	***************************************	1.3 3.9 0.7	0.0 0.0 0.0
45	0		0.0		0.0 1.0	2	0.7	0.0
46	0		0.0	***************************************	1.0	***************************************	1.3	0.0
47 48	0		0.0		1.0	***************************************	3.0	0.0
48	1		1.0		2.0	***************************************	3.9 -1.3	0.0 0.0
49	11		0.0		1.0 1.0	*	-2.6	0.0
50	1	<u>-</u>	0.0		1.0	***************************************	-3.2	0.0
51	1	LL	0.0		1.0	***************************************	3.0	0.0
52	2	<u>L</u>	1.0		2.0		3.9 0.7	0.0 0.0
53	2	<u>L</u>	0.0		1.0 -2.0		0.7	0.0
54		R	-3.0		-2.0		-9.1	0.0
55	3	R R R	2.0		-4.0		7.8	0.0
56	4	R	1.0		-5.0		0.7 -9.8	0.0
57	1		-3.0		-3.0		-9.6 7.8	0.0
58	2	L	3.0		0.0			0.0
59	3	L	1.0		4.0		5.2	0.0 0.0 0.0
60	1	L	-2.0		4.0 -3.0		-4.6	0.0
61	1	R	-2.0		-3.0		-7.2	0.0
62	2	R	1.0	***************************************	1.0		3.9	0.0
63	1	R	-1.0		-3.0		-4.6	0.0
64	0		1.0	***************************************	3.0		4.6	0.0 0.0
65	0		0.0		1.0		1.9 0.7	
66	0		0.0		1.0			0.0
67	0		0.0		2.0		1.3	0.0
68	1	R	1.0		0.0		3.9	0.0 0.0
69	2	R R	1.0	*	2.0		5.2	0.0
70	3	R	1.0 -2.0		3.0		6.5	0.0
71	1	R	-2.0		1.0		-4.6	0.0
72	0		1.0		0.0		3.9	0.0
73	1	L	1.0	*	2.0		3.9	0.0
74	2	L	1.0	*	4.0		5.2	0.0
75	3	L	1.0	*	6.0		6.5	0.0
76	1	L	-2.0		2.0		-7.8	0.0
77	2	R	-3.0	*	2.0		-8.5	Betretterterterterterterterterter
78	3	R	1.0	*	-4.0		1.3	0.0
79	3	R	0.0	2	-5.0		-3.2	0.0
80	3	R	0.0	*	-6.0		-3.9	0.0
81	3	R	0.0	*	-4.0		-2.6	0.0
82	1	R	-2.0	*	-1.0		-5.9	0.0
83	1	R	0.0	*	-2.0		3.2	0.0
84	0		1.0	2	3.0		4.6	0.0
85	2	R	2.0	*	-1.0		6.5	0.0
86	0		2.0	*	3.0		7.2	0.0
87	3	L L	3.0		4.0		10.4	0.0
88	4	L	1.0	*	5.0	×	5.9	0.0

89	1	L	-3.0	*	1.0	*	-7.8	0.0
90	0		1.0	*	2.0	2	4.6	0.0
91	0		0.0	*	0.0	*	2.6	0.0
92	2	R	2.0	*	-5.0	*	7.2	0.0
93	2	R	0.0	*	-6.0	*	-3.9	0.0
94	1	L	3.0	*	0.0	*	7.8	0.0
95	3	L	2.0	*	3.0	2	7.2	0.0
96	4	L	1.0	*	4.0	*	5.2	0.0
97	1	L	-3.0	*	3.0	*	-15.6	0.0
98	1	L	0.0	*	3.0	*	-10.4	0.0
99	2	R	-3.0	*	-3.0	*	-9.8	0.0
100	4	R	2.0	*	-7.0	*	22.8	0.0
101	7	R	3.0	*	-11.0	. *	29.3	0.0
102	11	R	4.0	*	-12.0	*	30.6	0.0
103	15	R	4.0	*	-16.0	2	29.9	0.0
104	22	R	7.0	285.7	20.0	*	37.1	0.0
105	31	R	9.0	222.2	27.0	370.4	41.0	0.0
106	40	R	9.0	222.2	33.0	303.0	44.9	0.0
107	42	R	2.0	*	31.0	322.6	25.4	0.0
108	45	R	3.0	*	30.0	333.3	27.3	0.0
109	51	R	6.0	333.3	29.0	344.8	34.5	0.0
110	54	R	3.0	. 2	23.0	434.8	22.8	0.0
111	60	R	6.0	333.3	20.0	500.0	28.7	0,0
112	59	R	-1.0	*	17.0	2	8.4	0.0
113	61	R	2.0	*	16.0	*	15.6	0.0
114	63	R	2.0	*	12.0	*	13.0	0.0

vi. Southbound Twist & Wheel Unload Wheel Unload Monitoring - Track Stations @ 2M Intervals

Input by		AV		Input Date Checked			25/11/2015				
Trigger value								+			
		load constants		12	166.7	35	286	40	5		
2 m		2.611		20	100	37	270.27	85	7		
10 m	netre	0.650		25	80	40	250	100	10		
	T	Cant			1	Twis	t	,	Vertical		
Point					L/B		2m rack	1	l0m rack	Wheel	Difference in level from
No.		July (IIIII)		Twist (mm)	Gradient 1 in	Twist (mm)	Gradient 1 in	Unload (%)	baseline. Deviations over 5m (absolute) (mm)		
1		41	L	*		Ŕ					
2		42	L	1.0	*	*					
3		43	L	1.0	2	*			ļ		
4		40	L	-3.0	*	±			0.0		
5		46	Ļ	6.0	333.3	*			0.0		
6		41	<u> </u>	-5.0	400.0	0.0	*	-13.1	0.0		
		41	Ļ	0.0	**************************************	-1.0	***************************************	-0.7	0.0		
8		43	ļ	2.0		0.0		5.2	0.0		
9		45	<u> </u>	2.0		5.0	*	8.5	0.0		
10		43	ļ <u>Ļ</u>	-2.0		-3.0	*	-7.2	0.0		
11		42	L	-1.0		1.0		-2.0	0.0		
12		41	<u>-</u>	-1.0		0.0		-2.6	0.0		
13		41		0.0		-2.0	*	1.3	0.0		
14		41	ļĻ	0.0		-4.0		3.2	0.0		
15		43	L L	2.0		0.0		6.5	0.0		
16		44	<u>_</u>	1.0		2.0		3.9	0.0		
17		41	ļ	-3.0		0.0		-7.8	0.0		
18 19		43	<u>-</u>	2.0		2.0		6.5	0.0		
20		46 45	<u>L</u>	3.0		5.0		11.1	0.0		
21		42	L	-1.0	***************************************	2.0 -2.0		-2.6	0.0		
22		41	<u>-</u>	-3.0 -1.0	*	0.0	***************************************	-9.1 -2.6	0.0 0.0		
23			<u>-</u>	2.0	*		***************************************				
24		43 44	<u>-</u>	1.0	*	0.0 -2.0	*	7.8	0.0		
25		45 45	7	1.0	*	0.0	*	4.6 3.3	0.0		
26		44	L	-1.0	***************************************	2.0	*	-3.3	0.0 0.0		
27		45	Ĺ	1.0	*	4.0	*	5.2	0.0		
28		47	Ĺ	2.0	*	4.0	*	7.8	0.0		
29		47	Ĺ	0.0	*	3.0	2	7.8 -3.9 -8.5 -14.3	0.0		
30		46	L	0.0 -1.0	*	1.0	2	-8.5	0.0		
31		43	L	-3.0	2	-1.0	*	-14.3	0.0		
32		42	L	-1.0	*	-3.0	2	-6.5	0.0		
33		41	Ī	-1.0	2	-6.0	2	-6.5	0.0		

34	41	L	0.0	*	-6.0	*	-3.9	0.0
35	37	L	-4.0		-9.0		-16.3	0.0
36	33	L	-4.0	500.0	-10.0	*	-16.9	0.0
37	33 36	- L	-4.0 3.0	*	-6.0	*	3.9	0.0
38	39	L	3.0	2	-2.0	*	6.5	0.0
39	39 37	L	-2.0	2	-4.0	***************************************	-7.8	0.0
40	29	L	-80	250.0	-8.0	*	-26.1	0.0
41	27	······································	-8.0 -2.0	*	-6.0	*	-9.1	0.0
42	20		2.0	2	-7.0	*	6.5	0.0
43	29 30		10	2	-9.0	***************************************	3.3	0.0
44	30		1.0 3.0	*	-4.0	***************************************	6.5	0.0
	33		0.0	*	10	***************************************	2.6	0.0
45	33		0.0		4.0		2.6	0.0
46	33	<u>-</u>	0.0		6.0		3.9	0.0
47	31	<u>_</u>	-2.0		2.0		-5.2	0.0
48	- 31		0.0		1.0		2.6	0.0
49	31	L	0.0	*	-2.0		1.9	0.0
50	30 30	L	-1.0		-3.0	***************************************	-4.6	0.0
51	30	L	0.0	2	-3.0	***************************************	-1.9	0.0
52	31	L	1.0	*	0.0	2	2.6	0.0
53	35	L	4.0	*	4.0	*	13.0	0.0
54	34	L	-1.0	*	3.0	*	-2.6	0.0
55	34 33	L	-1.0	*	3.0	*	-2.6	0.0
56	30	L	-3.0	*	0.0	*	-7.8	0.0
57	29	L	-1.0	*	-2.0	*	-3.9	0.0
58	31	L	2.0	*	-4.0	***************************************	7.2	0.0
59	34	- T	2.0 3.0	2	0.0	*	7.8	0.0
60	34 33	1	-1.0	***************************************	0.0	***************************************	-3.9	0.0
61	30	1	-3.0	. *	0.0	***************************************	-7.8	0.0
62	3/		4.0	*	5.0	***************************************	13.7	0.0
63	34	<u>-</u>	0.0	•	3.0	***************************************	-2.6	0.0
64	34 31		0.0	*	3.0	2	-10.4	0.0
		<u>-</u>	-3.0		-3.0		2.6	0.0
65	31	<u>-</u>	0.0		-2.0		-2.6	0.0
66	35		4.0		5.0		13.7	0.0
67	36	Ļ	1.0		2.0		-5.8	0.0
68	30		-6.0	333.3	-4.0		-18.9	0.0
69	27	L L	-3.0	*	-4.0 -4.0	***************************************	-10.4	0.0
70	27	L	0.0	*	-4.0	*	-2.6	0.0
71	24	L	-3.0	*	-11.0	*	-15.0	0.0
72	23	L	-1.0	*	-13.0	2	-11.1	0.0
73	25	L	2.0	*	-5.0	*	7.2	0.0
74	27	L	2.0	2	0.0	2	7.2	0.0
75	28	L	1.0	*	1.0	*	3.9	0.0
76	29	L	1.0	*	5.0	2	5.9	0.0
77	29	L	0.0	*	6.0	*	3.9	0.0
78	28	L	-1.0	*	3.0	*	-3.9	0.0
79	30	Ī	2.0	***************************************	3.0	2	7.2	0.0
80	30	1	0.0	***************************************	2.0	*	-3.9	0.0
81	29	1	-1.0	2	0.0	*	-5.9	0.0
	28		-1.0	***************************************	-10	*		0.0
82	28 26			***************************************	-1.0	2	-3.3 -6.5	
83	26	<u>-</u>	-2.0	***************************************	-2.0		-6.5	0.0
84	24	<u>-</u>	-2.0		-6.0		-9.1	0.0
85	24	<u>L</u>	0.0		-6.0		-3.9	0.0
86	24	L L	0.0		-5.0		3.9	0.0
87	27	L	3.0	***************************************	-1.0		10.4	0.0
88	28	L	1.0	*	2.0	*	5.9	0.0
89	28	L	0.0	*	4.0	*	2.6	0.0

90	28	L	0.0	*	4.0	*	2.6	0.0
91	30	L	2.0	*	6.0	2	9.1	0.0
92	31	L	1.0	2	4.0	*	5.2	0.0
93	33	L	2.0	*	5.0	*	8.5	0.0
94	31	L	-2.0	*	3.0	*	-5.9	0.0
95	28	L	-3.0	*	0.0	*	-7.8	0.0
96	28	L	0.0	*	-2.0	*	3.2	0.0
97	29	L	1.0	*	-2.0	*	2.6	0.0
98	27	L	-2.0	2	-6.0	*	-9.1	0.0
99	30	L	3.0	*	-1.0	2	7.2	0.0
100	33	L	3.0	*	5.0	*	11.1	0.0
101	33	L	0.0	***************************************	5.0	*	3.2	0.0
102	29	L	-4.0	*	0.0	2	-11.1	0.0
103	28	L	-1.0	*	1.0	*	-2.6	0.0
104	29	L	1.0	2	-1.0	*	2.6	0.0
105	30	L	1.0	*	-3.0	*	2.6	0.0
106	30	L	0.0	*	-3.0	2	-1.9	0.0
107	28	L	-2.0	*	-1.0	*	-5.9	0.0
108	28	L	0.0	*	0.0	*	0.7	0.0
109	29	L	1.0	*	0.0	*	2.6	0.0
110	30	L	1.0	*	0.0	*	2.6	0.0
111	29	L	-1.0	*	-1.0	*	-3.3	0.0
112	31	L	2.0	2	3.0	*	7.2	0.0
113	29	L	-2.0	*	1.0	*	-5.2	0.0
114	29	L	0.0	*	0.0	*	0.0	0.0