



Project	Designed	JO	Date	Dec 2014	Project No:	GA19787
69 REDINGTON ROAD, LONDON, NW3 7RP	Checked	MJ	Date	Dec 2014	Sheet No.	APP/E - 01

APPENDIX E – Permanent Stage FE Model results and Calculations

General View	APP/E - 03
Bedding Stress	APP/E - 04
Nodal displacement (minimum values) - Basement	APP/E - 05
Nodal displacement (maximum values) - Basement	APP/E - 06
Nodal displacement – Lower Ground Floor	APP/E - 07
Loads in contiguous pile wall (SWL)	APP/E - 08
Loads in columns (unfactored)	APP/E - 09
Lower Ground Floor Transfer Slab - Contours of bending reinforcement	
T1 (mm ² /m over the base mat of H12@200mm)	APP/E - 10
T2	APP/E - 11
B1	APP/E - 12
B2	APP/E - 13
Upper Basement Slab - Contours of bending reinforcement	
T1 (mm ² /m over the base mat of H16@200mm)	APP/E - 14
T2	APP/E - 15
B1 (mm ² /m over the base mat of H12@200m)	APP/E - 16
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Lower Basement Slab - Contours of bending reinforcement	
T1 (mm ² /m over the base mat of H16@200mm)	APP/E - 18
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B2	APP/E - 21
Step between Basements - Contours of bending reinforcement	
Air side horizontal (mm ² /m over the base mat of H12@200mm)	APP/E - 22
Air side vertical	APP/E - 23
Soil side horizontal	APP/E - 24
Soil side vertical	APP/E - 25
Lining Walls - Contours of bending reinforcement	
Air side horizontal (mm ² /m over the base mat of H12@200mm)	APP/E - 26
Air side vertical	APP/E - 27
Soil side horizontal	APP/E - 28
Soil side vertical	APP/E - 29



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Loading

LC1 Self Weight of structural elements (not shown)	
LC2 Weight of water (pool)	APP/E - 30
LC3 DL self-weight of brickwork wall	APP/E - 31
LC4 DL upper floors	APP/E - 32
LC5 LL upper floors	APP/E - 33
LC6 LL LGF level inside	APP/E - 34
LC7 LL LGF level outside	APP/E - 35
LC8 DL finishes	APP/E - 36
LC9 LL basement	APP/E - 37
LC10 LL Plant room	APP/E - 38
LC11-LC12 Uplift force / water pressure	APP/E - 39

Note: The structure as the permanent model analysis has been also assessed with the loading with the original brickwork walls. So the loading shown in appendix D.

Shear Punching Checks

400x400 mm column (worst case central column)	APP/E - 40-42
400x400 mm edge column, 30% of the column's load is inside the shear perimeter	APP/E - 43-45
350x350 mm column (worst case) 30% of the column's load is inside the shear perimeter	APP/E - 46-48

Column reinforcement calculation

400x400 mm column (worst case)	APP/E - 49-50
350x350 mm column (worst case)	APP/E - 51-52



DESIGN CALCULATION SHEET

Project
69 REDINGTON ROAD, LONDON, NW3 7RP

Designed **JO**

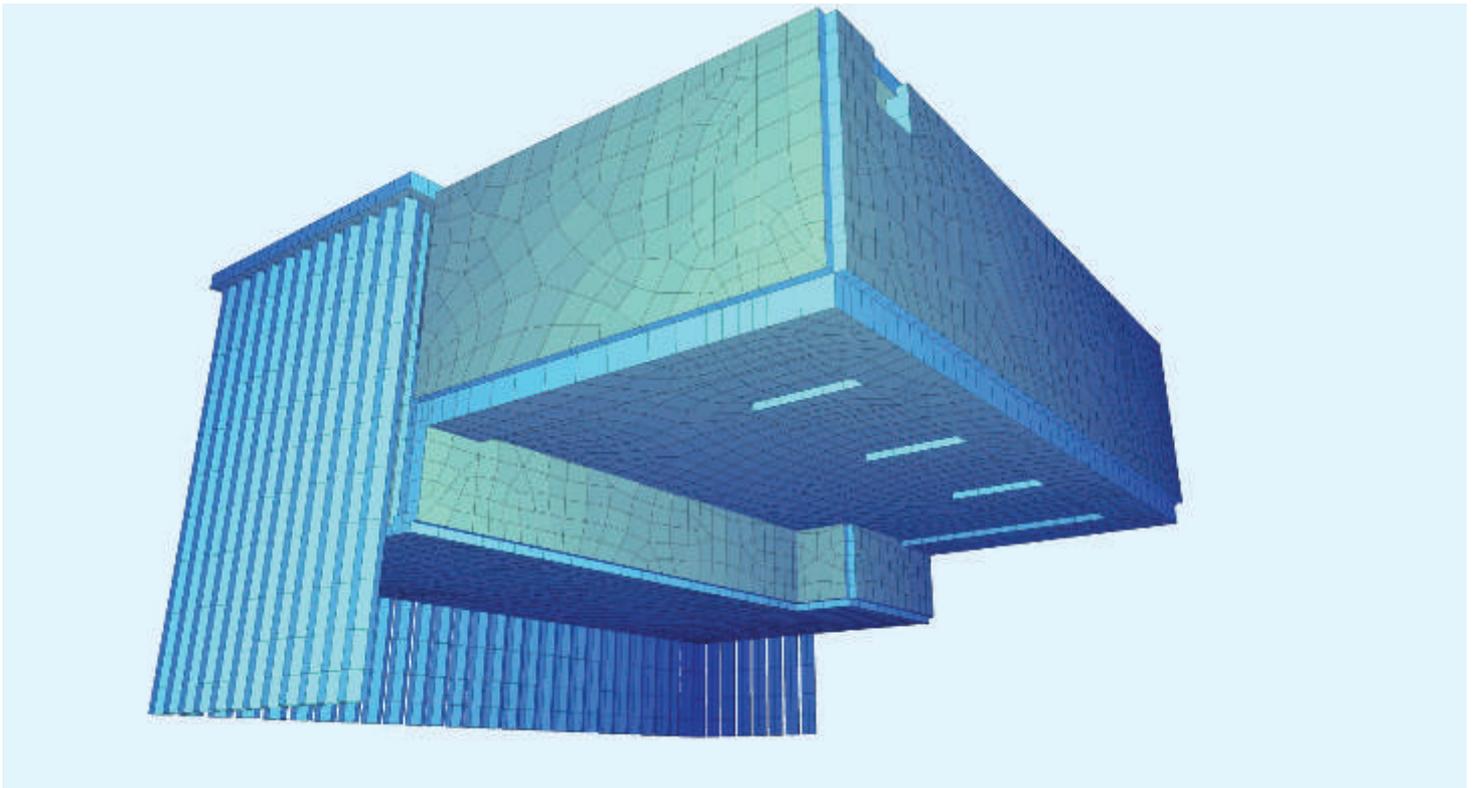
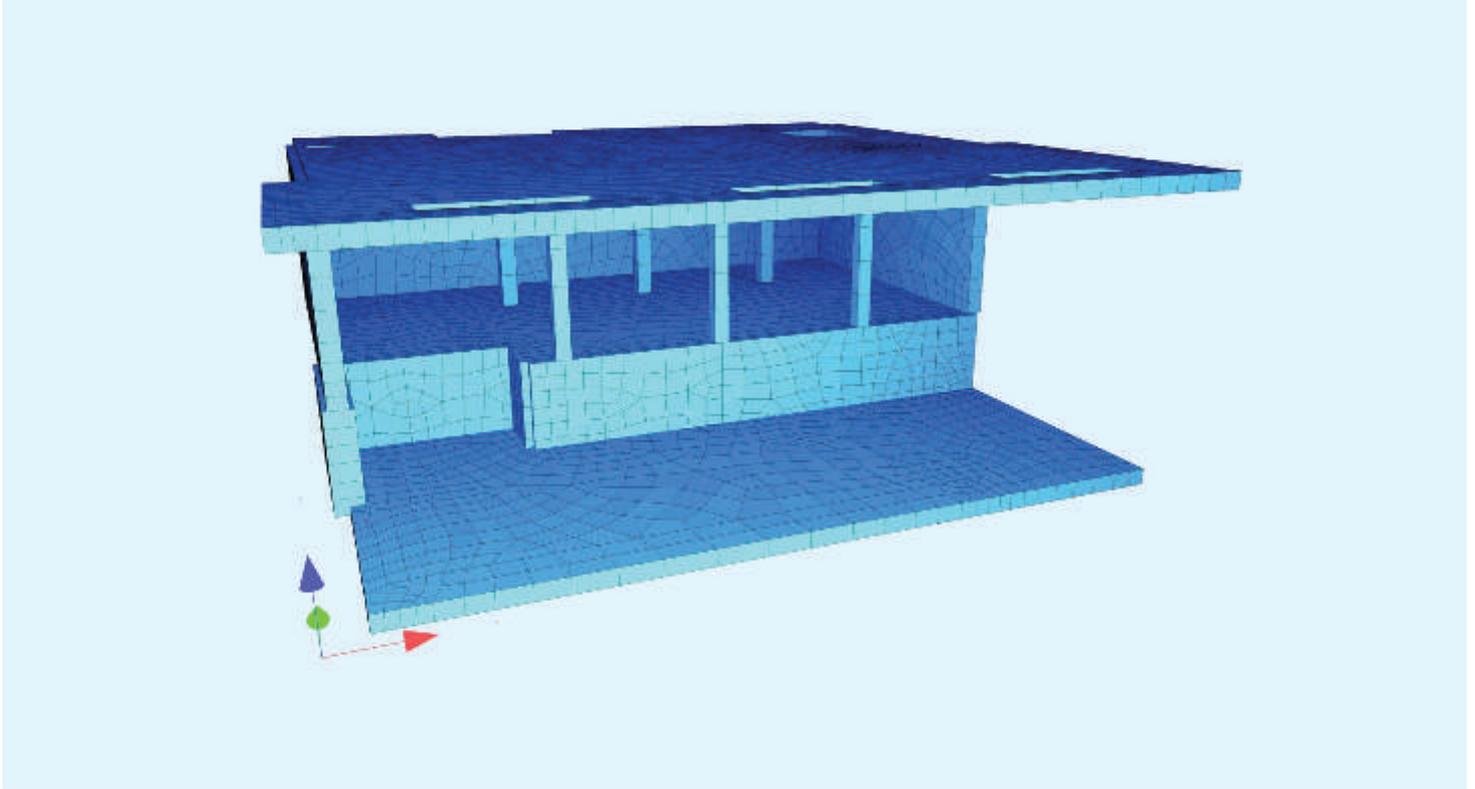
Date **Dec 2014**

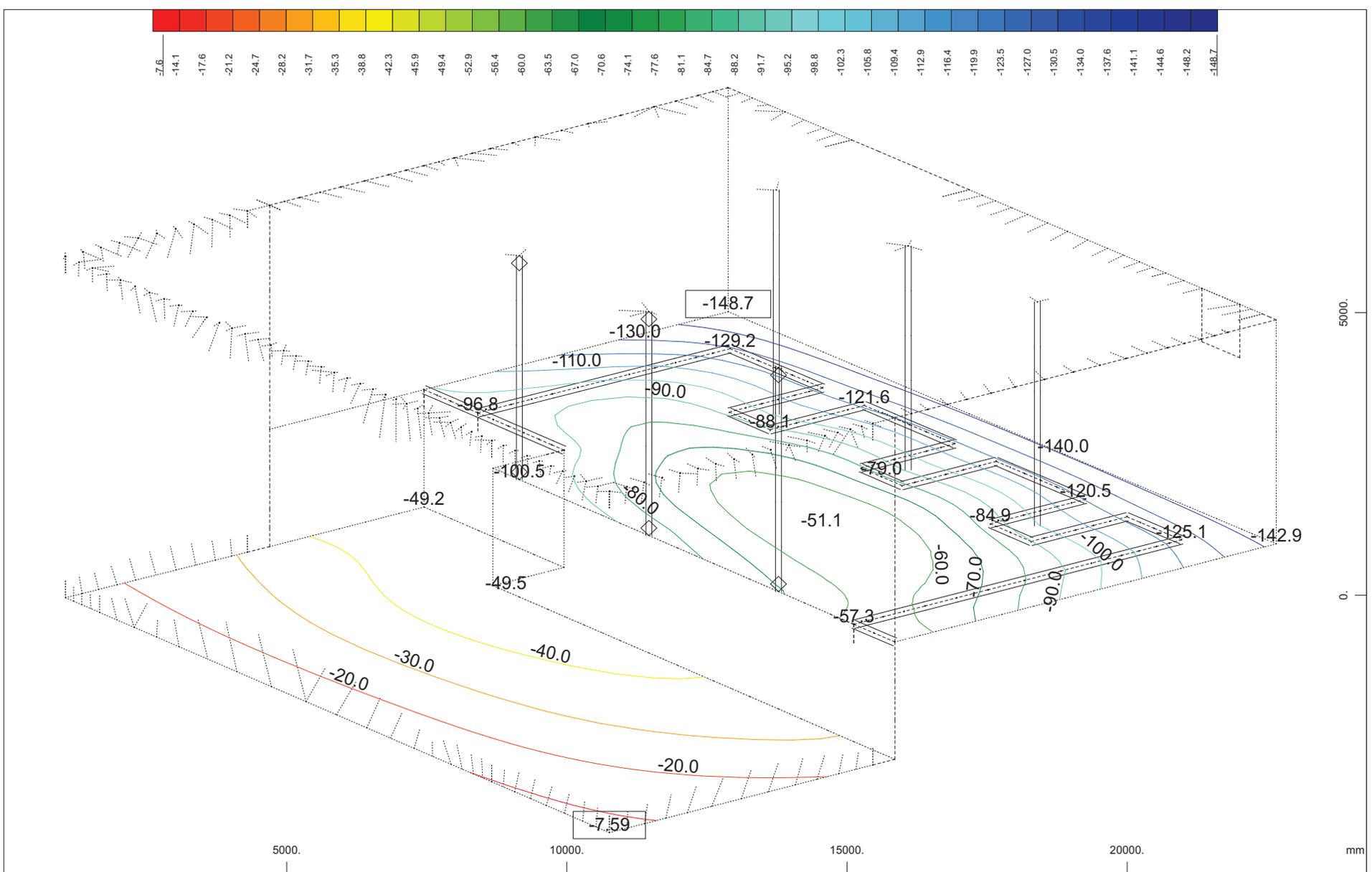
Project No: **GA19787**

Checked **MJ**

Date **Dec 2014**

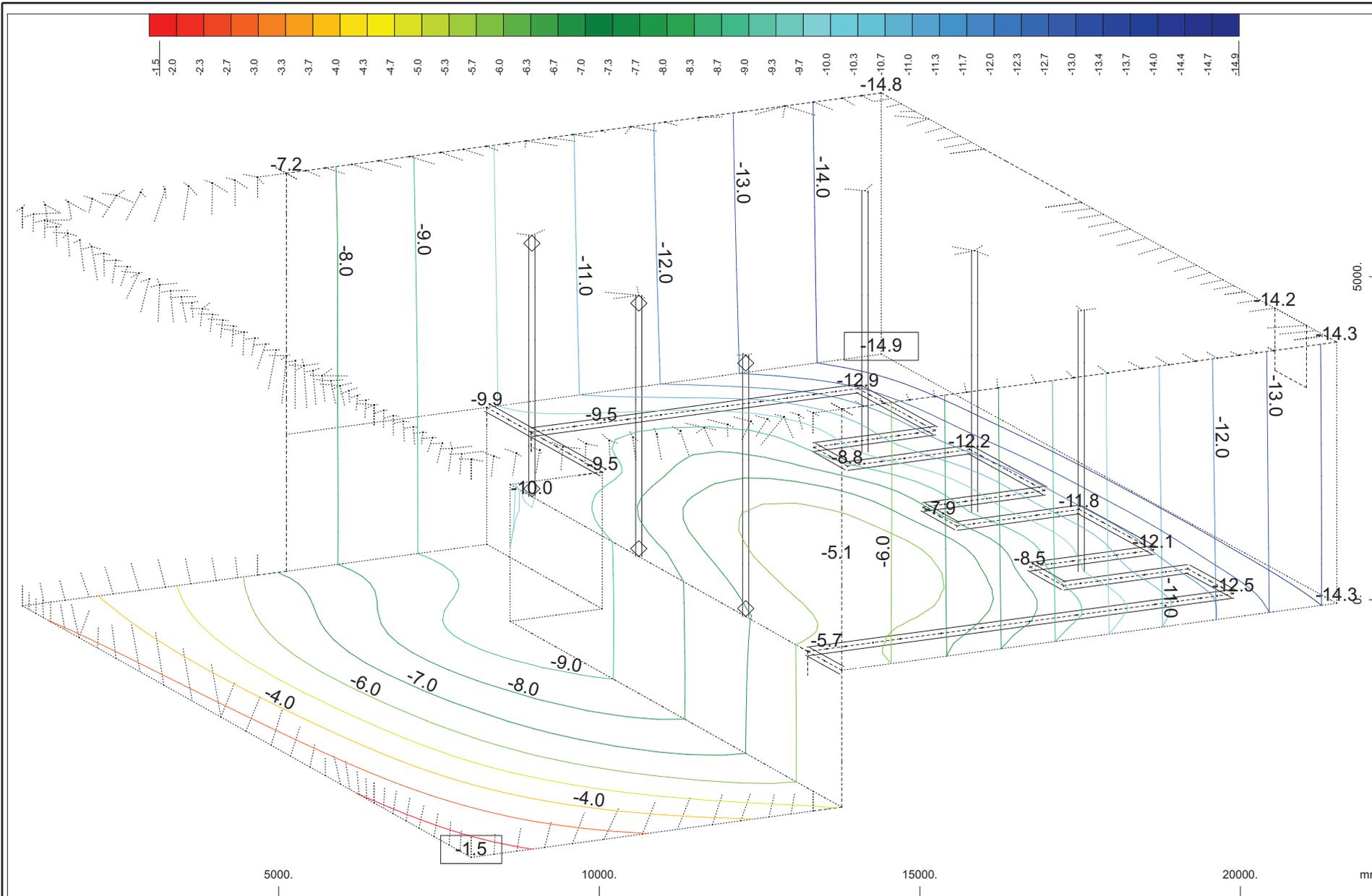
Sheet No. **APP/E - 03**





Z Sector of system Group 110 120 125 130 135
 Bedding stress in Node \diamond , Loadcase 1118 MINR-P QUAD Bedding Stresses , from -148.7 to -7.59 step 10.0 kN/m²

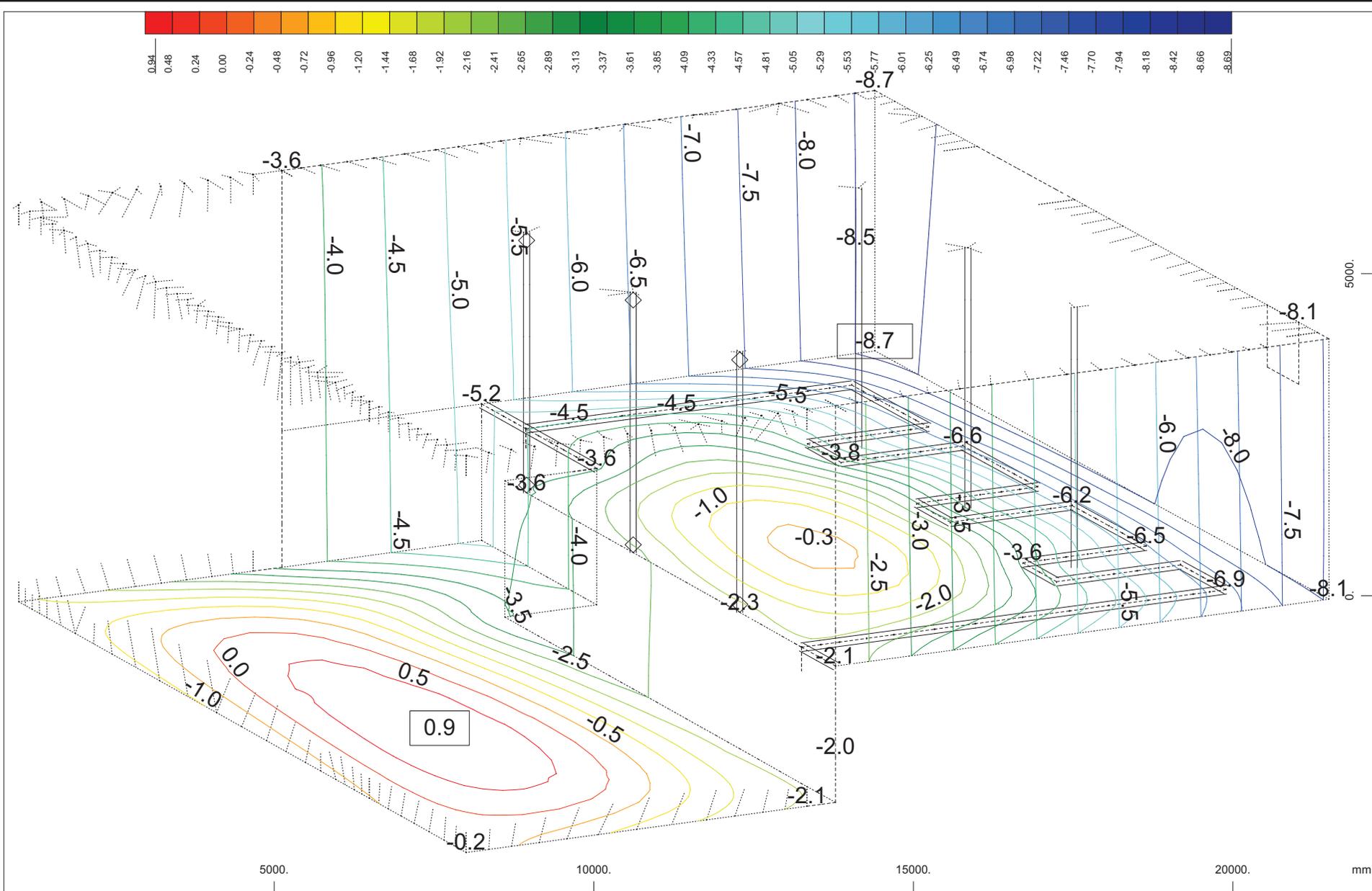
M 1 : 95
 X * 0.662
 Y * 0.818
 Z * 0.944



Z Sector of system Group 110 120 125 130 135
 X Y Nodal displacement in global Z in Node

↕, Loadcase 1176 MINR-UZ NODE Nodal Displacements, from -14.9 to -1.52 step 1.00 mm

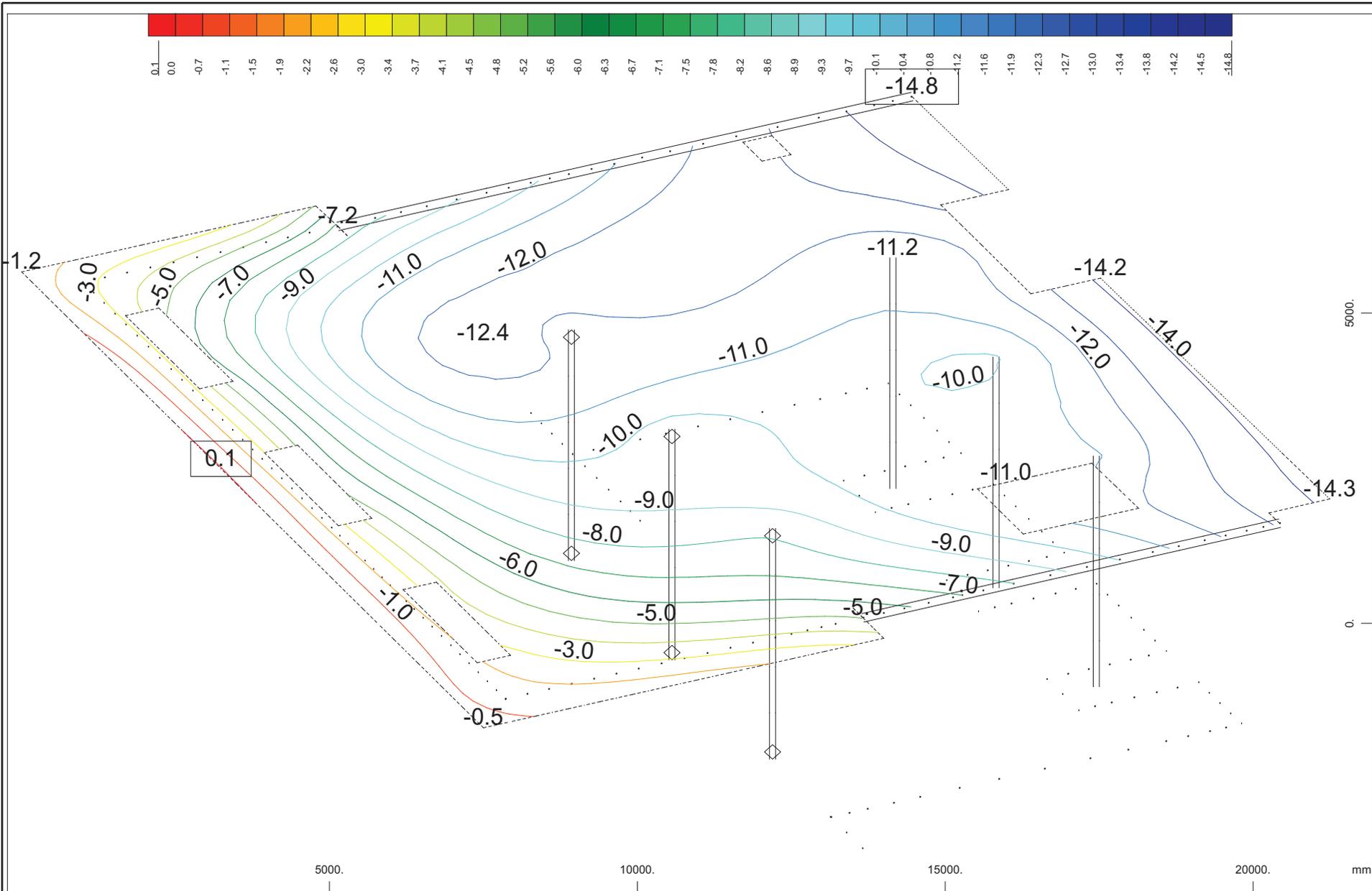
M 1 : 85
 X* 0.502
 Y* 0.906
 Z* 0.962



Z Sector of system Group 110 120 125 130 135
 X Y Nodal displacement in global Z in Node

↕ , Loadcase 1175 MAXR-UZ NODE Nodal Displacements , from -8.69 to 0.935 step 0.500 mm

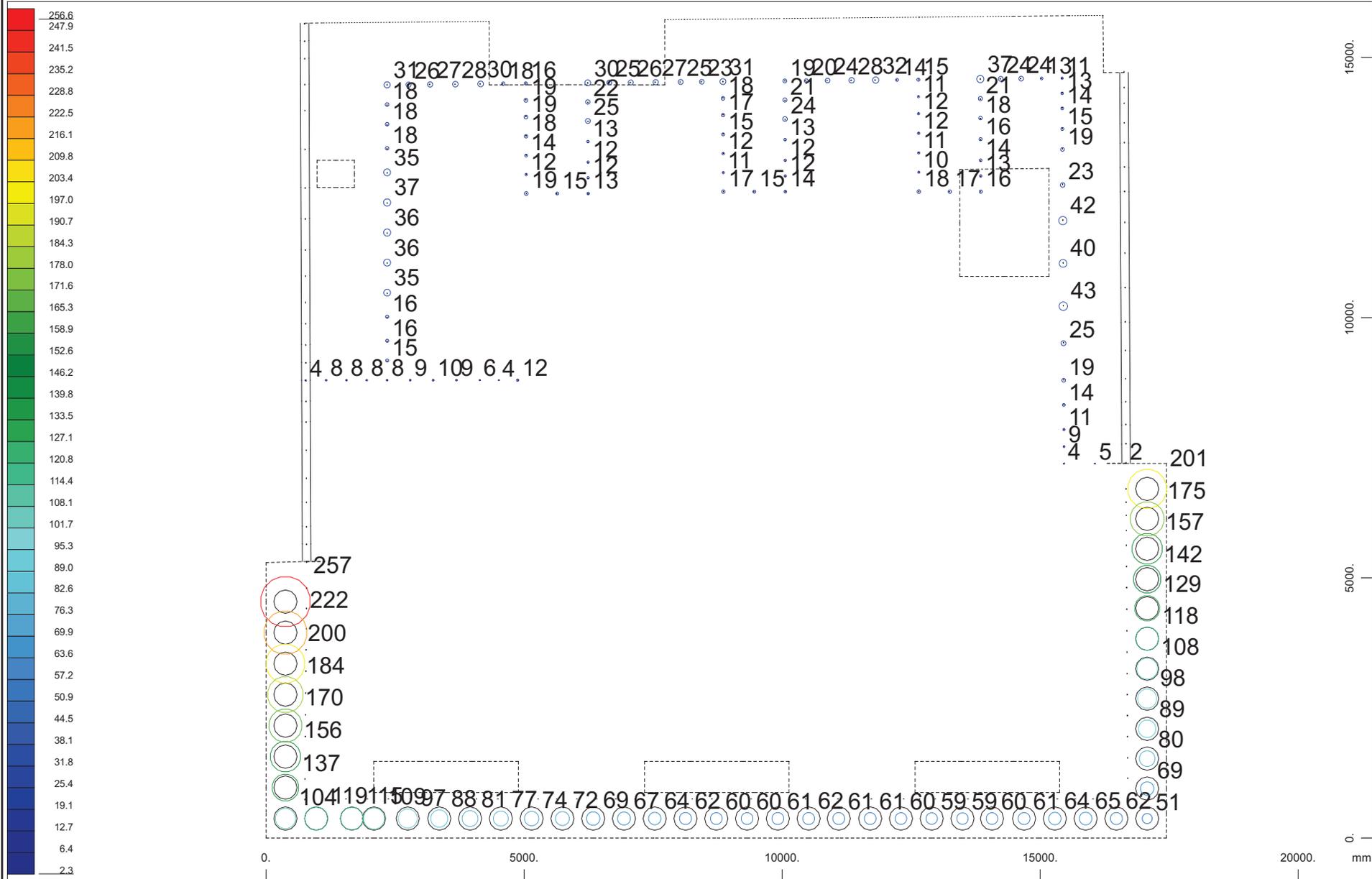
M 1 : 85
 X* 0.502
 Y* 0.906
 Z* 0.962



Sector of system Group 100 130
Nodal displacement in global Z in Node

↕, Loadcase 1176 MINR-UZ NODE Nodal Displacements, from -14.8 to 0.0632 step 1.00 mm

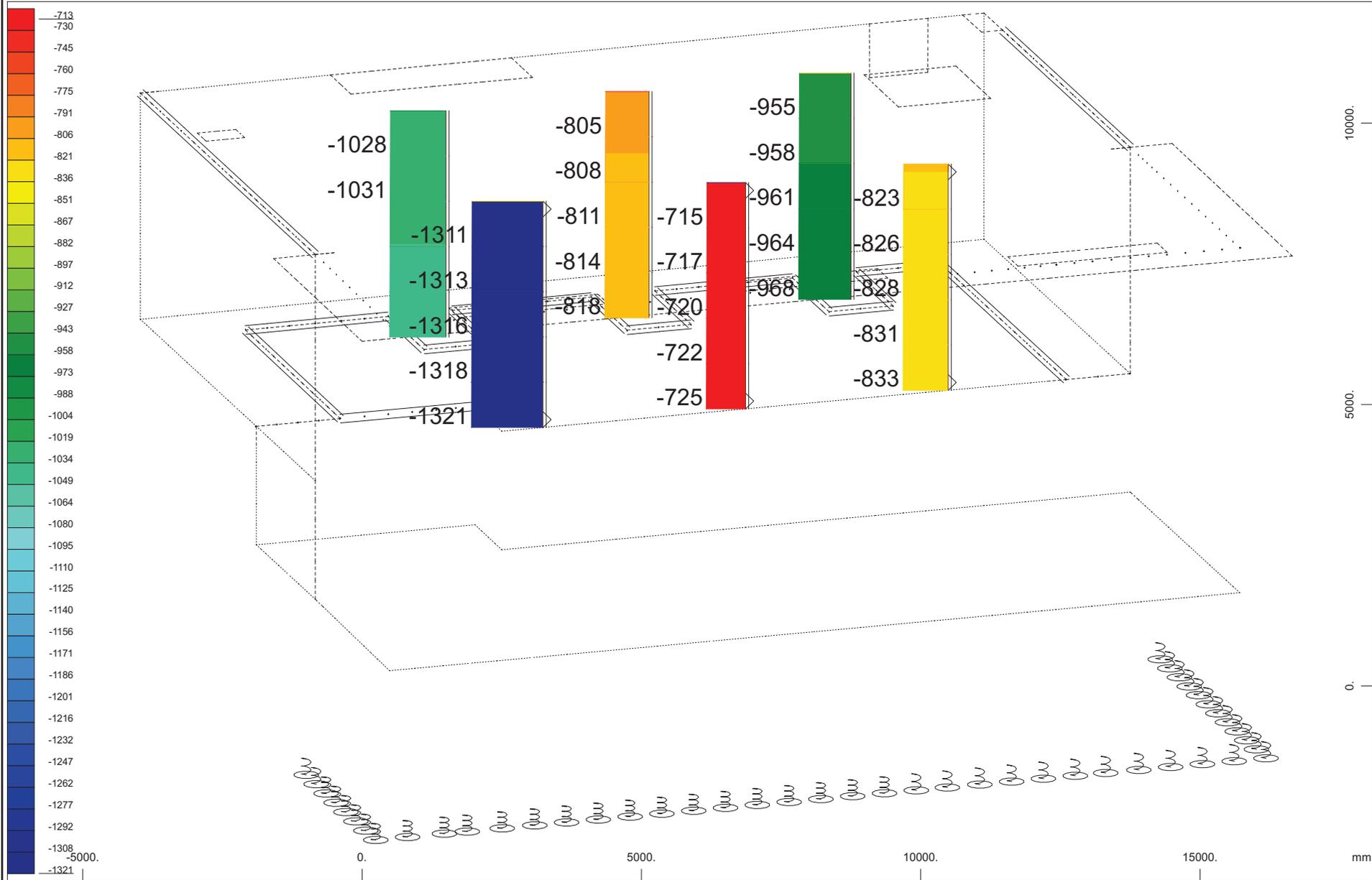
M 1 : 88
X* 0.602
Y* 0.925
Z* 0.885



Y Sector of system Group 100 140
 Z-X Nodes , Support force in global Z, Loadcase 1155 MAXR-PZ NODE Supporting Forces i , 1 cm 3D = 200.0 kN
 6687.)

△ (Max=256.6) (total:

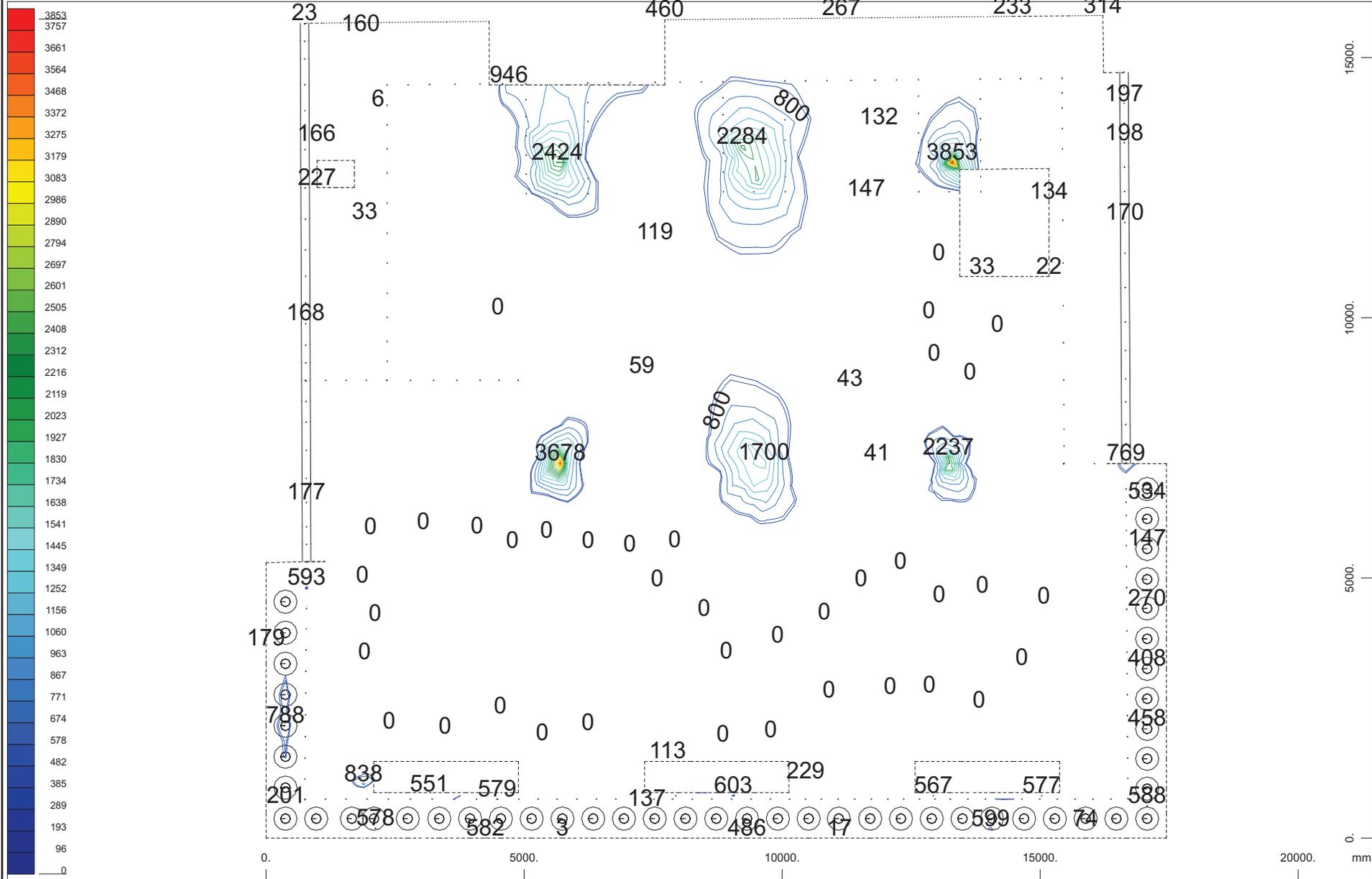
M 1 : 105



10000.
5000.
0.
mm

Sector of system Group 0 100 110 120 130 135
 Beam Elements , Normal force Nx, Loadcase 1122 MINR-N BEAM Forces in Beam-Element , 1 cm 3D = 1000. kN (Min=-1321.) (Max=-712.5)

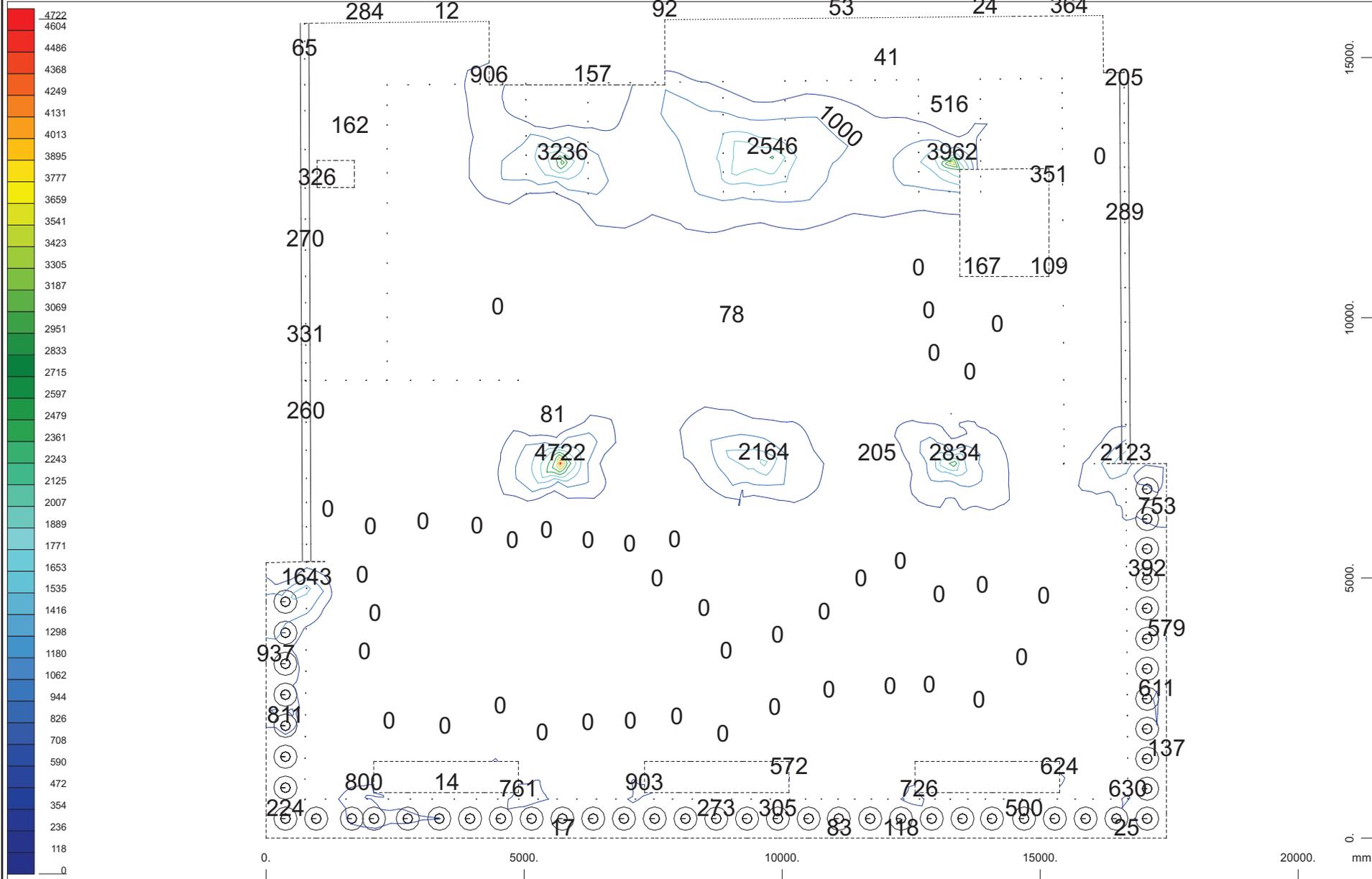
M 1 : 97
 X* 0.958
 Y* 0.408
 Z* 0.957



Y Sector of system Group 0 100
 Z-X Quadrilateral Elements , upper Principal reinforcements (1st layer) in Node

→ , Design Case 1 , from 565.0 to 3853. step 200.0 mm²/m

M 1 : 105

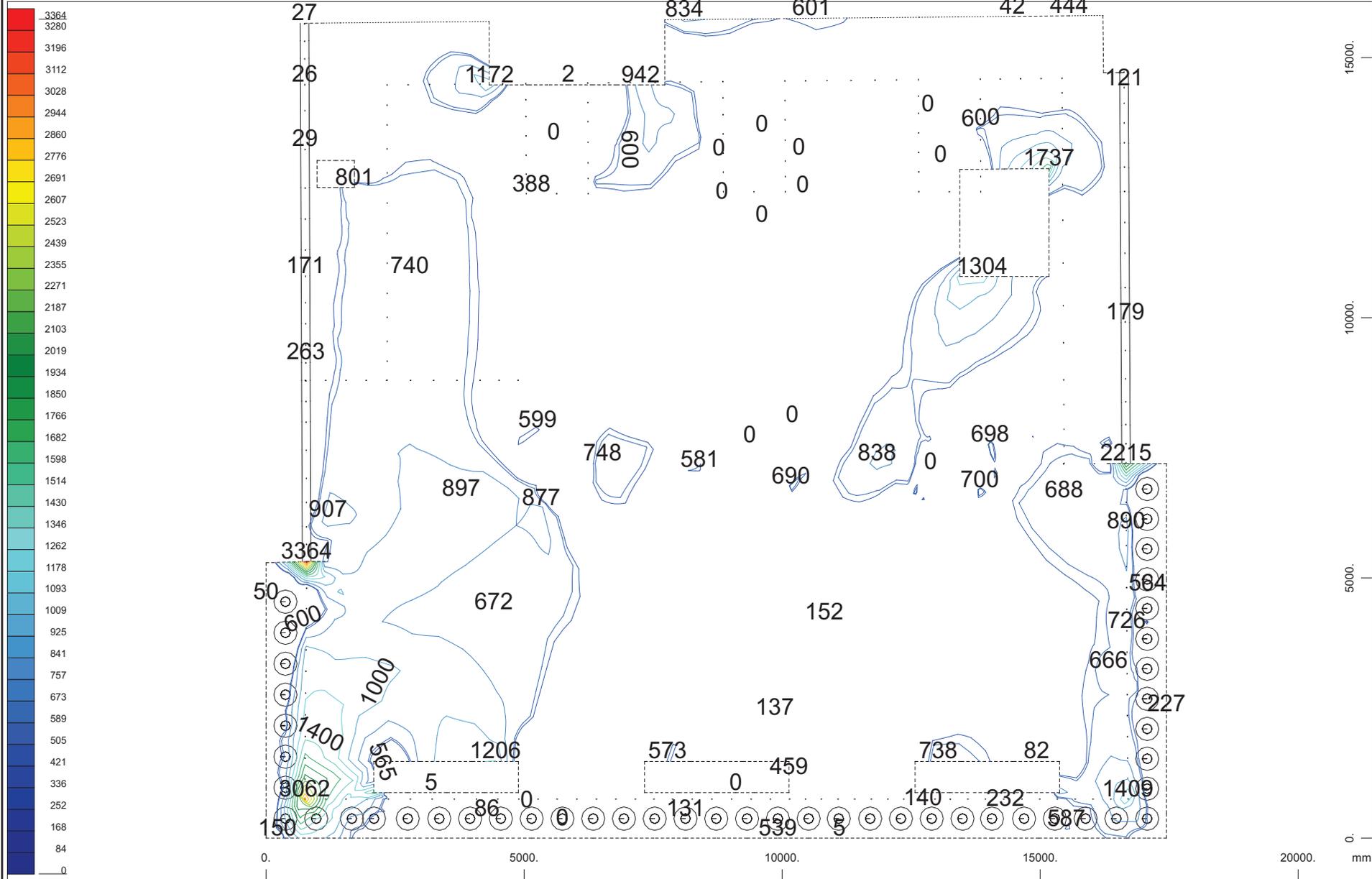


Abbej Pynford PLC Hemel Hempstead, HP2 7DX
 WINGRAF - GRAPHICS FOR FINITE ELEMENTS (V 16.17-27)
 FE GA19787 TEMP
 Interactive Graphic

Y Sector of system Group 0 100
 Z-X Quadrilateral Elements , upper Cross reinforcements (2nd layer) in Node

¼ Design Case 1 , from 565.0 to 4722. step 500.0 mm2/m

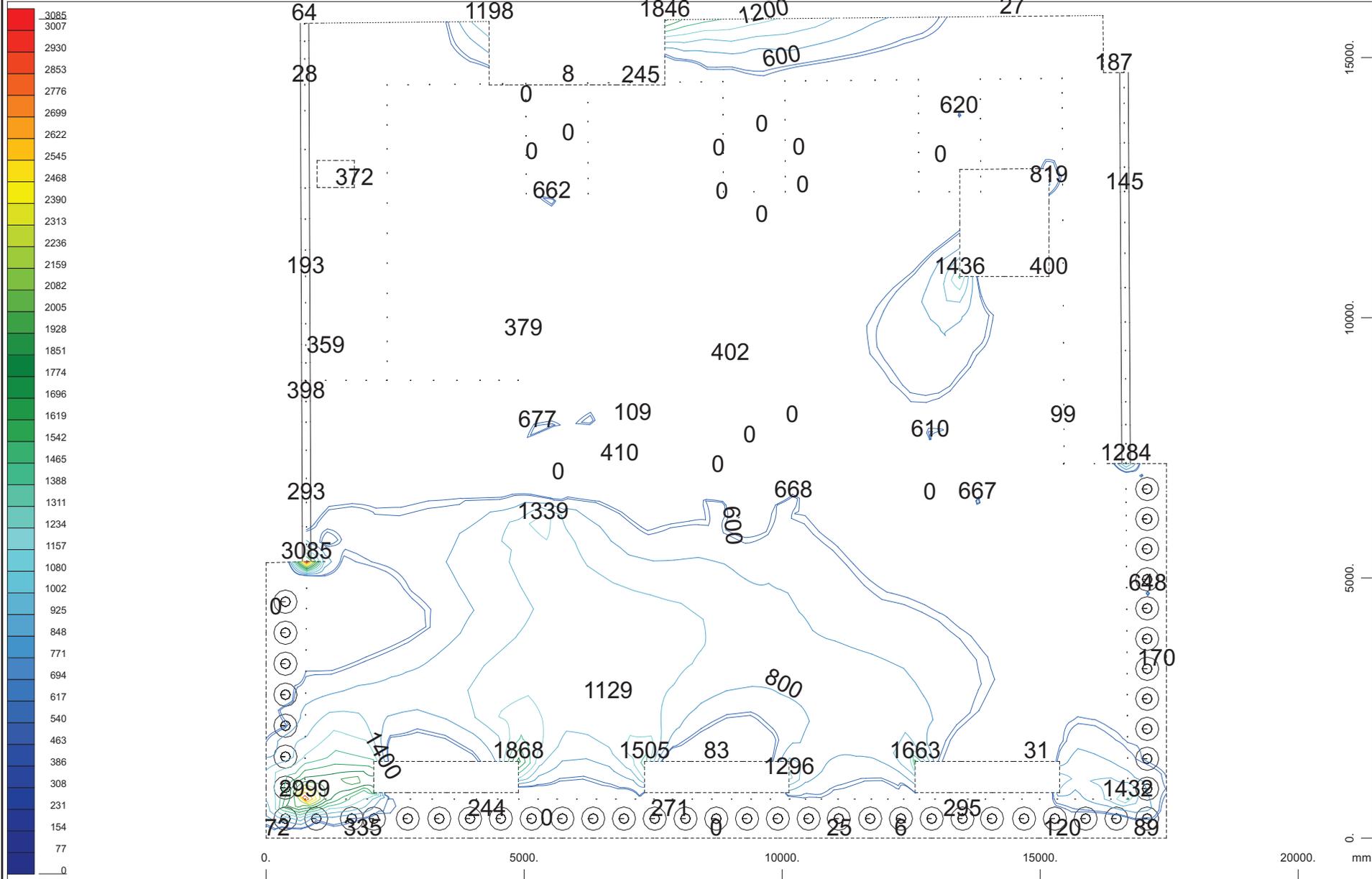
M 1 : 105



Y Sector of system Group 0 100
Z-X Quadrilateral Elements , lower Principal reinforcements (1st layer) in Node

→, Design Case 1 , from 565.0 to 3364. step 200.0 mm²/m

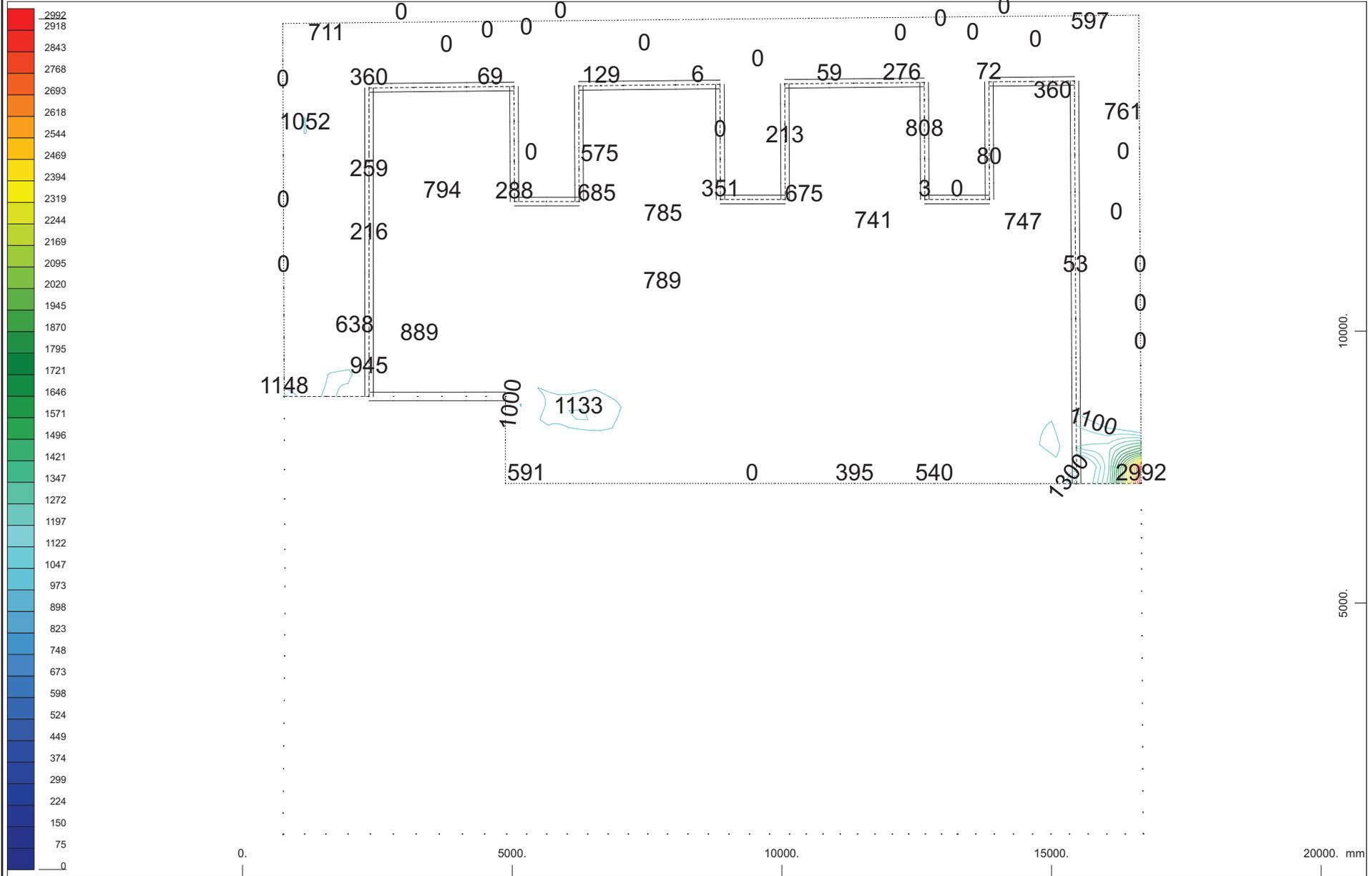
M 1 : 105



Y Sector of system Group 0 100
 Z-X Quadrilateral Elements, lower Cross reinforcements (2nd layer) in Node

1/4 Design Case 1, from 565.0 to 3085. step 200.0 mm2/m

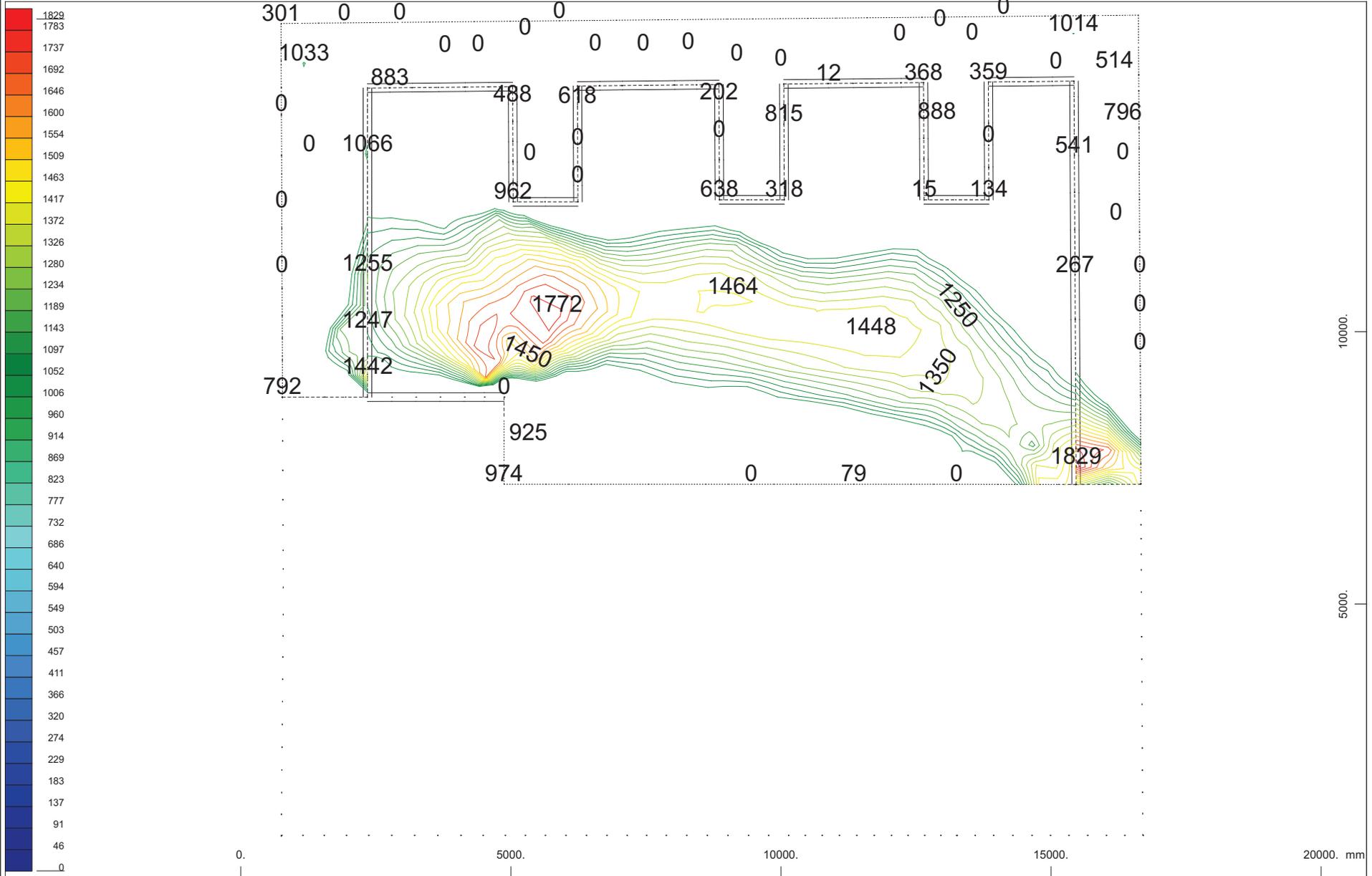
M 1 : 105



Y Sector of system Quadrilateral Elements Group 120
 Z-X Quadrilateral Elements , upper Principal reinforcements (1st layer) in Node

→ , Design Case 1 , from 1000. to 2992. step 100.0 mm²/m

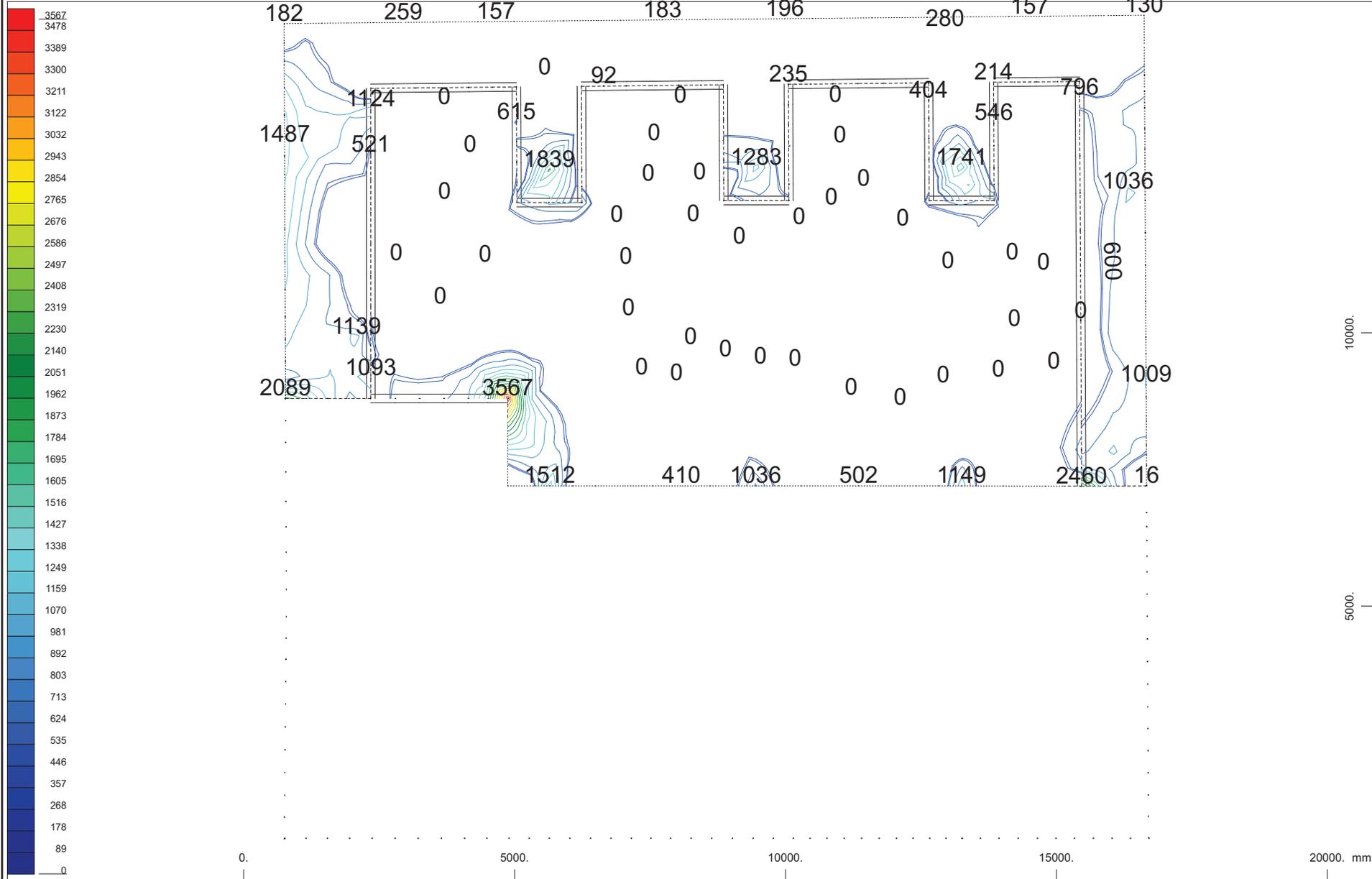
M 1 : 100



Y Sector of system Quadrilateral Elements Group 120
 X Quadrilateral Elements , upper Cross reinforcements (2nd layer) in Node

1/4 Design Case 1 , from 1000. to 1829. step 50.0 mm2/m

M 1 : 100

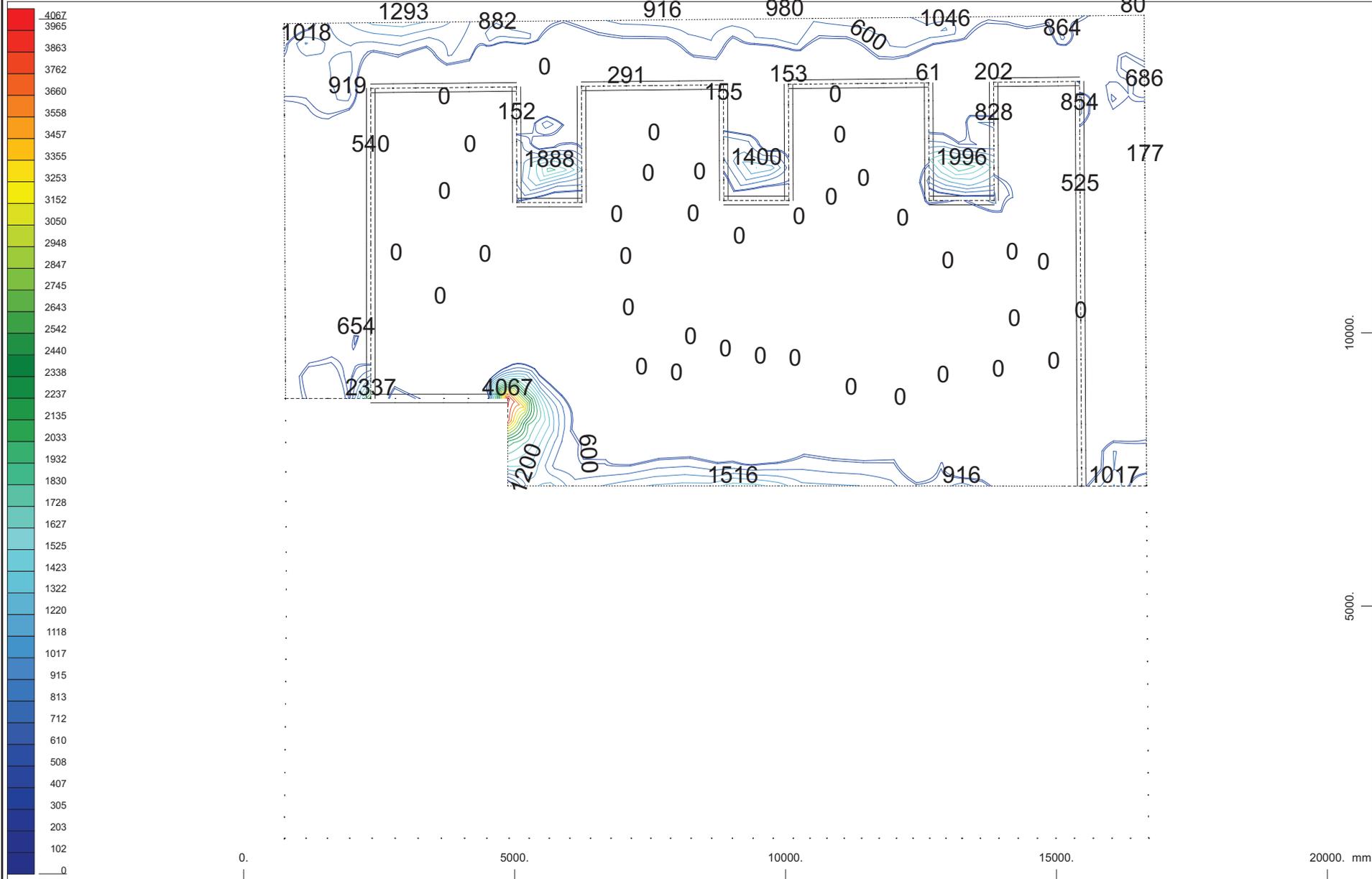


Abbej Pynford PLC Hemel Hempstead, HP2 7DX
 WINGRAF - GRAPHICS FOR FINITE ELEMENTS (V16.17-27)
 FE GA19787 TEMP
 Interactive Graphic

Y Sector of system Quadrilateral Elements Group 120
 Z-X Quadrilateral Elements , lower Principal reinforcements (1st layer) in Node

→ , Design Case 1 , from 565.0 to 3567. step 200.0 mm2/m

M 1 : 100

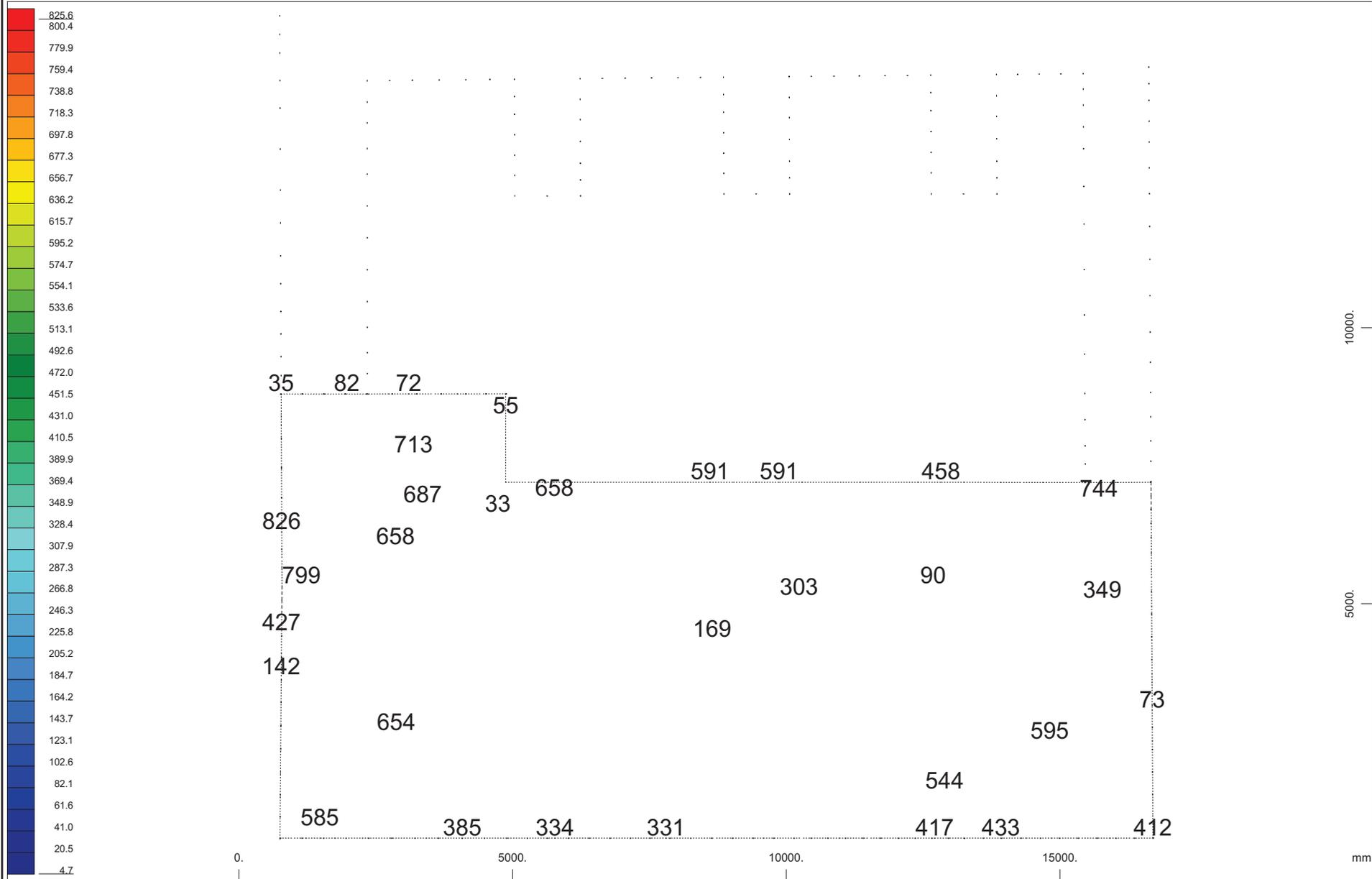


Abbeey Pynford PLC Hemel Hempstead, HP2 7DX
 WINGRAF - GRAPHICS FOR FINITE ELEMENTS (V 16.17-27)
 FE GA19787 TEMP
 Interactive Graphic

Y Sector of system Quadrilateral Elements Group 120
 Z-X Quadrilateral Elements , lower Cross reinforcements (2nd layer) in Node

1/4 Design Case 1 , from 565.0 to 4067. step 200.0 mm2/m

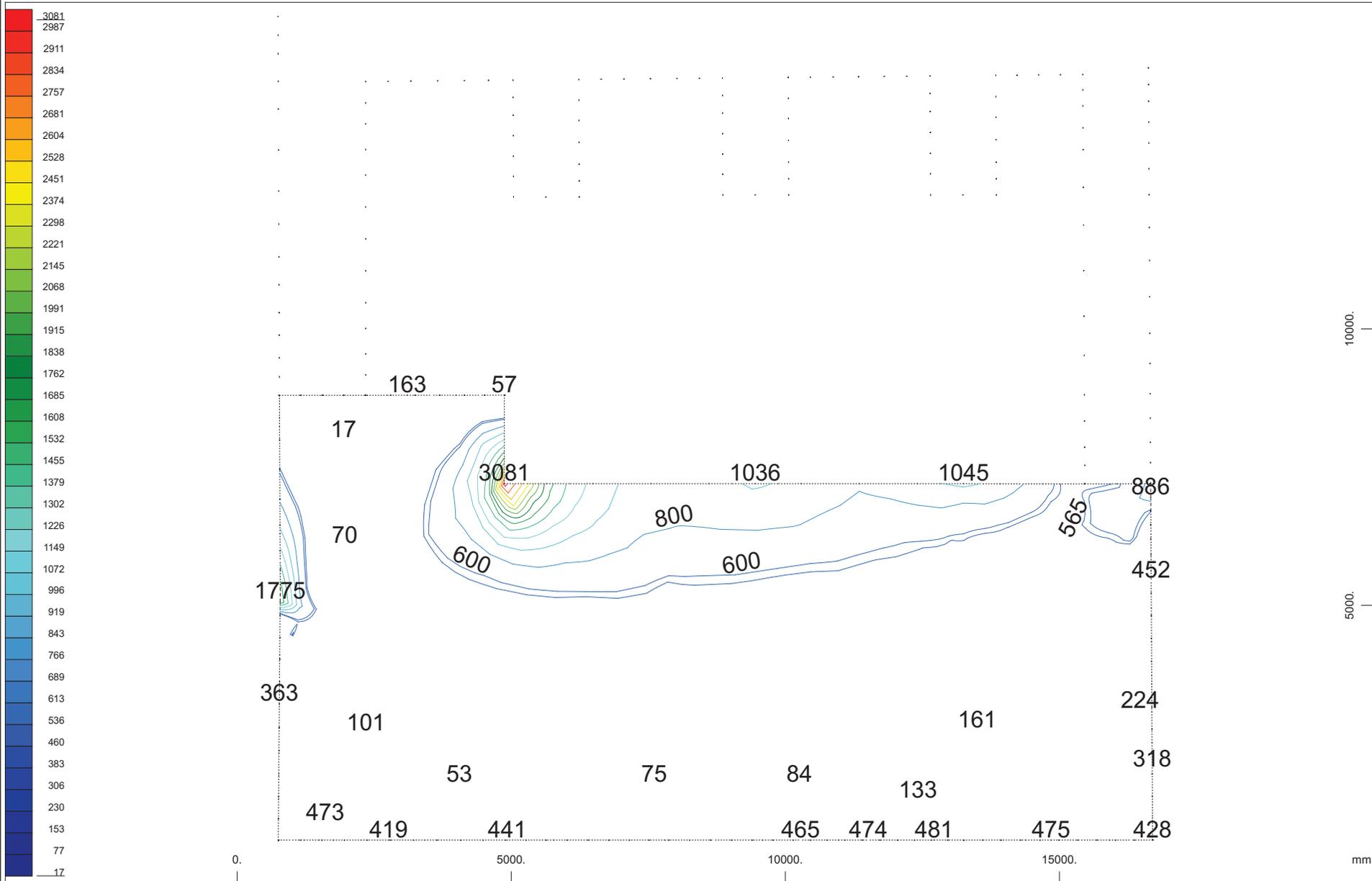
M 1 : 100



Y Sector of system Quadrilateral Elements Group 135
 Z-X Quadrilateral Elements , upper Principal reinforcements (1st layer) in Node

→ , Design Case 1 , from 825.6 to 835.6 step 0.500 mm²/m

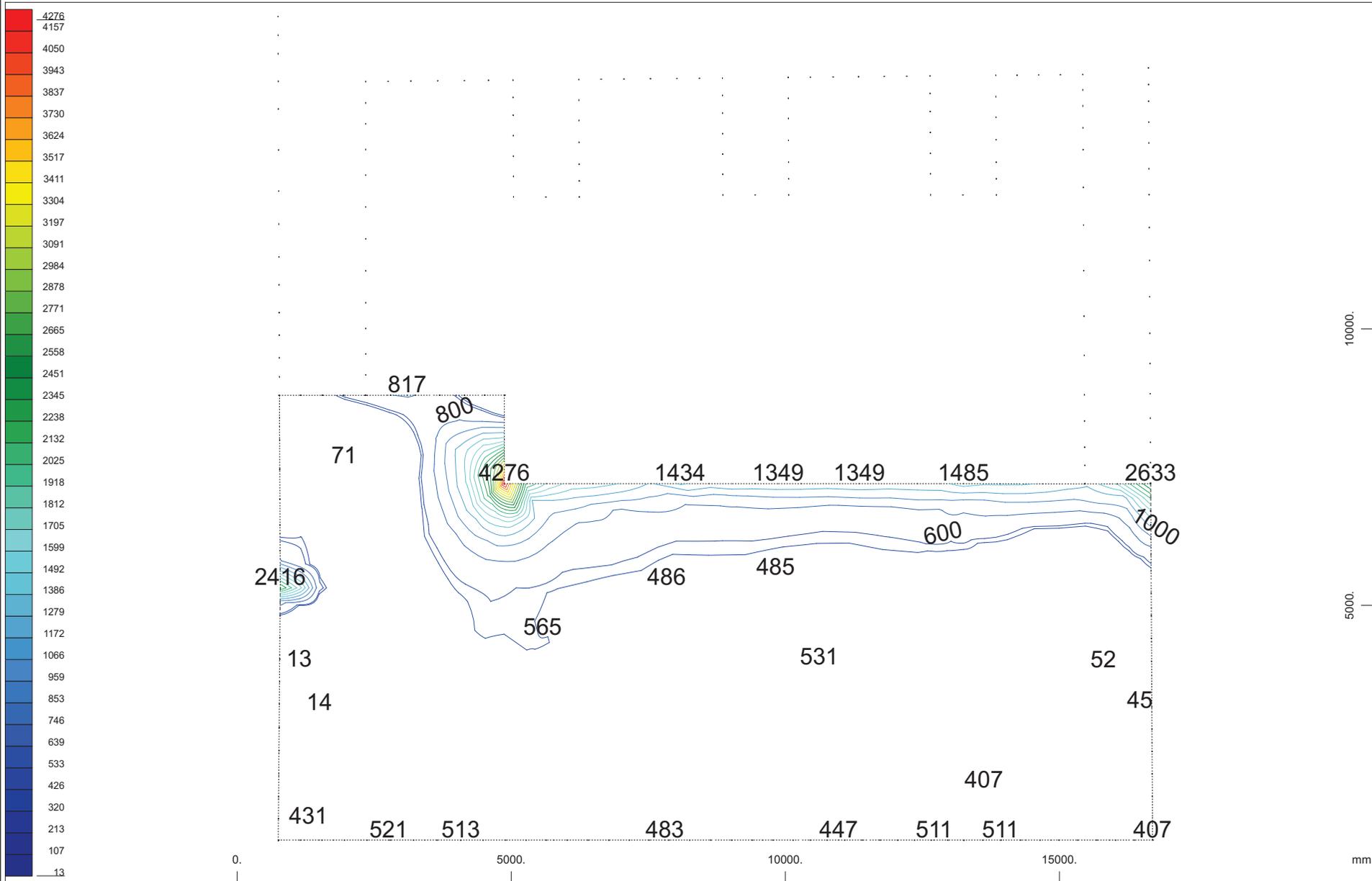
M 1 : 99



Y Sector of system Quadrilateral Elements Group 135
Z-X Quadrilateral Elements , lower Principal reinforcements (1st layer) in Node

→ , Design Case 1 , from 565.0 to 3081. step 200.0 mm2/m

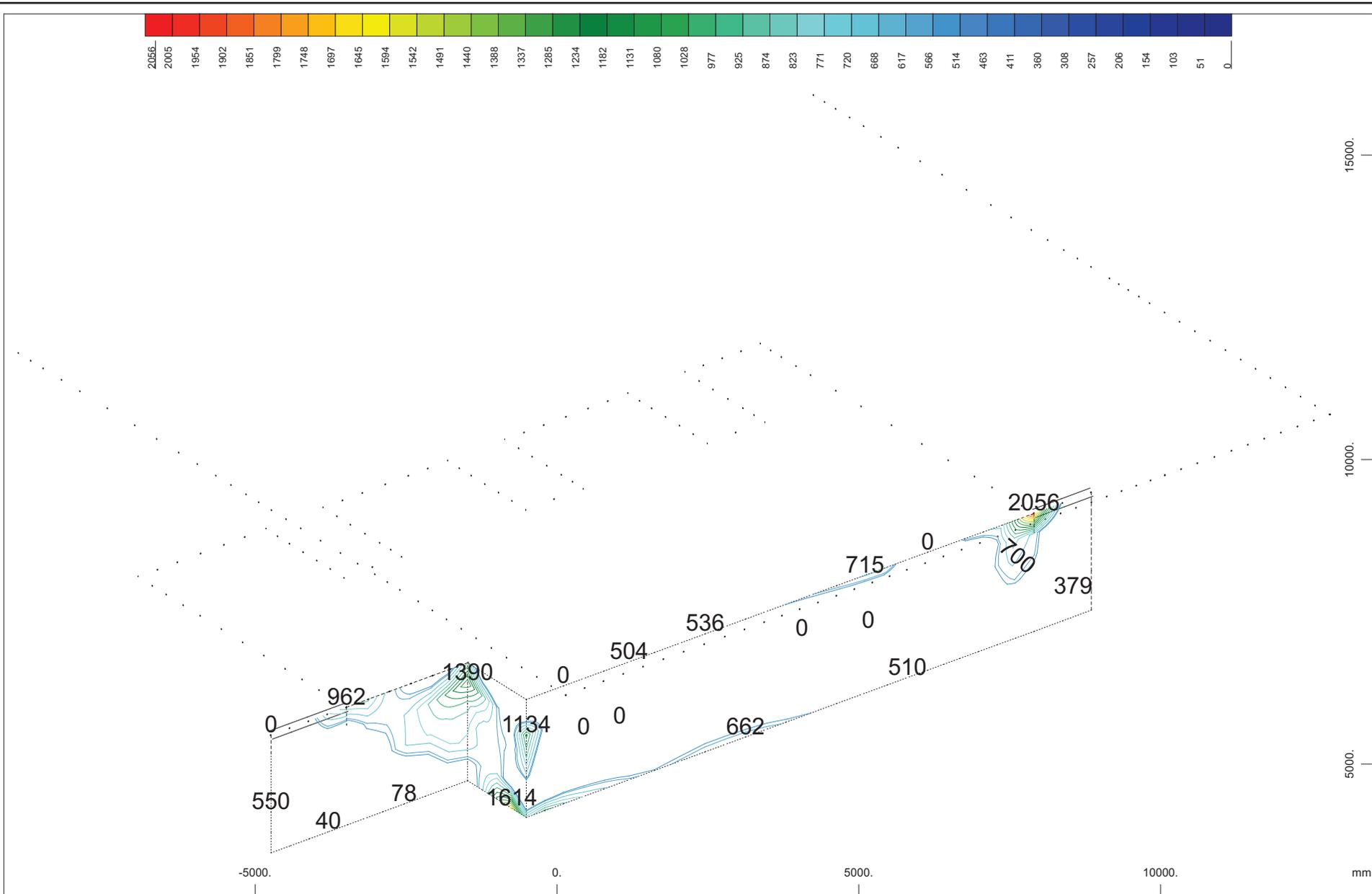
M 1 : 99



Y Sector of system Quadrilateral Elements Group 135
Z-X Quadrilateral Elements , lower Cross reinforcements (2nd layer) in Node

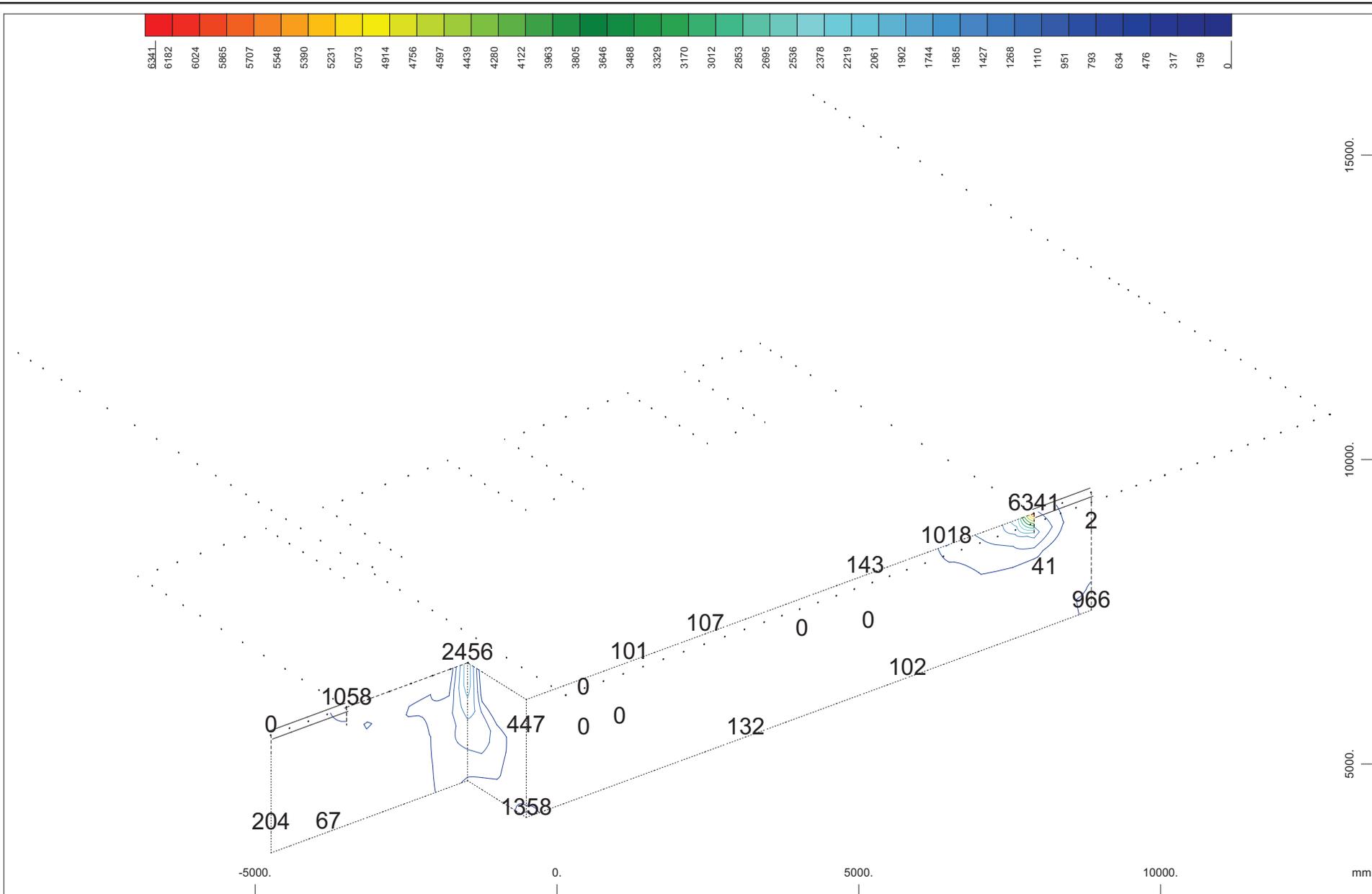
1/4 Design Case 1 , from 565.0 to 4276. step 200.0 mm2/m

M 1 : 99



Sector of system Quadrilateral Elements Group 125
 Quadrilateral Elements , upper Principal reinforcements (1st layer) in Node, Design Case 1 , from 565.0 to 2056. step 100.0 mm2/m

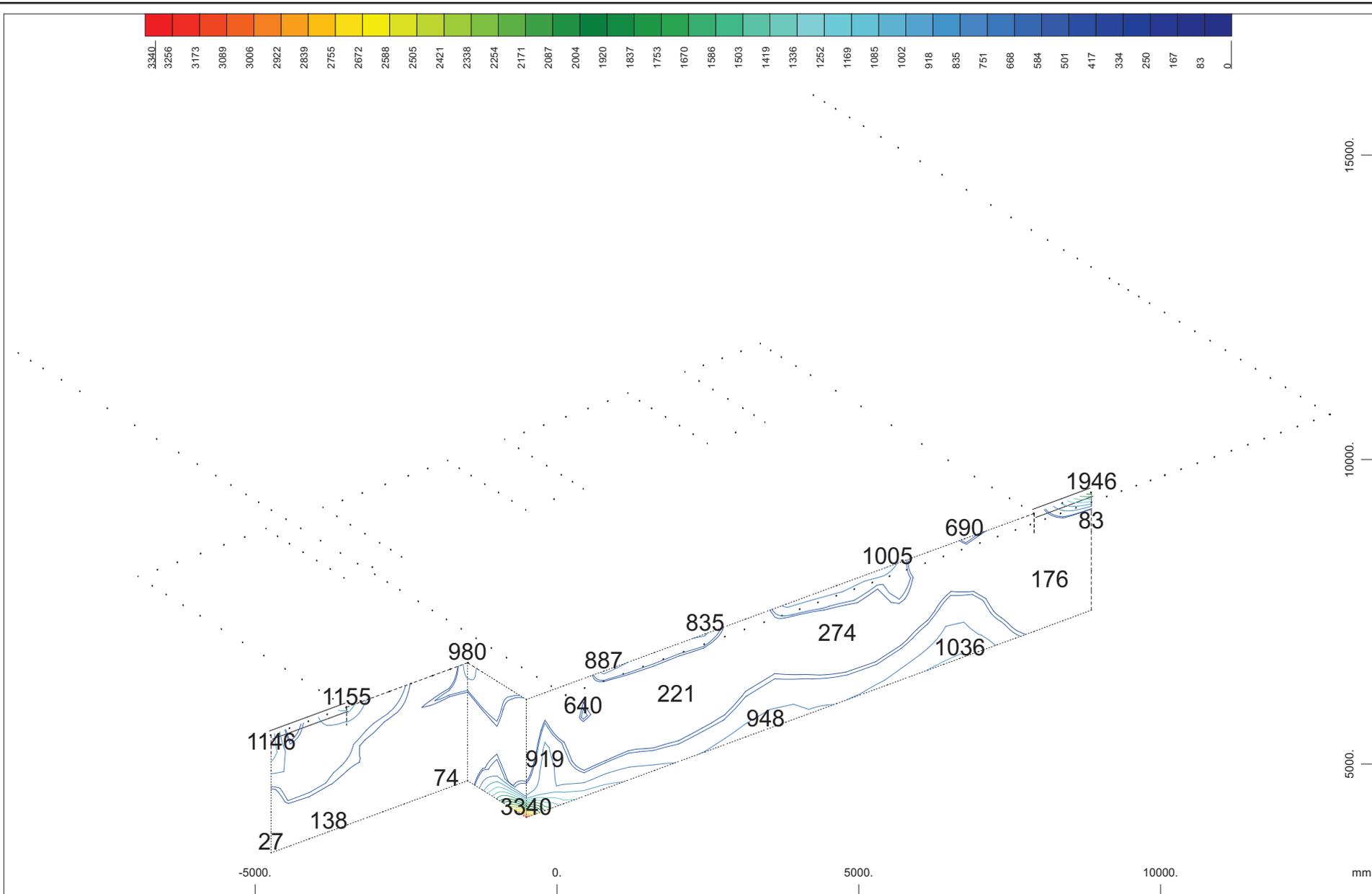
M 1 : 90
 X* 0.845
 Y* 0.715
 Z* 0.880



Sector of system Quadrilateral Elements Group 125
 Quadrilateral Elements , upper Cross reinforcements (2nd layer) in Node

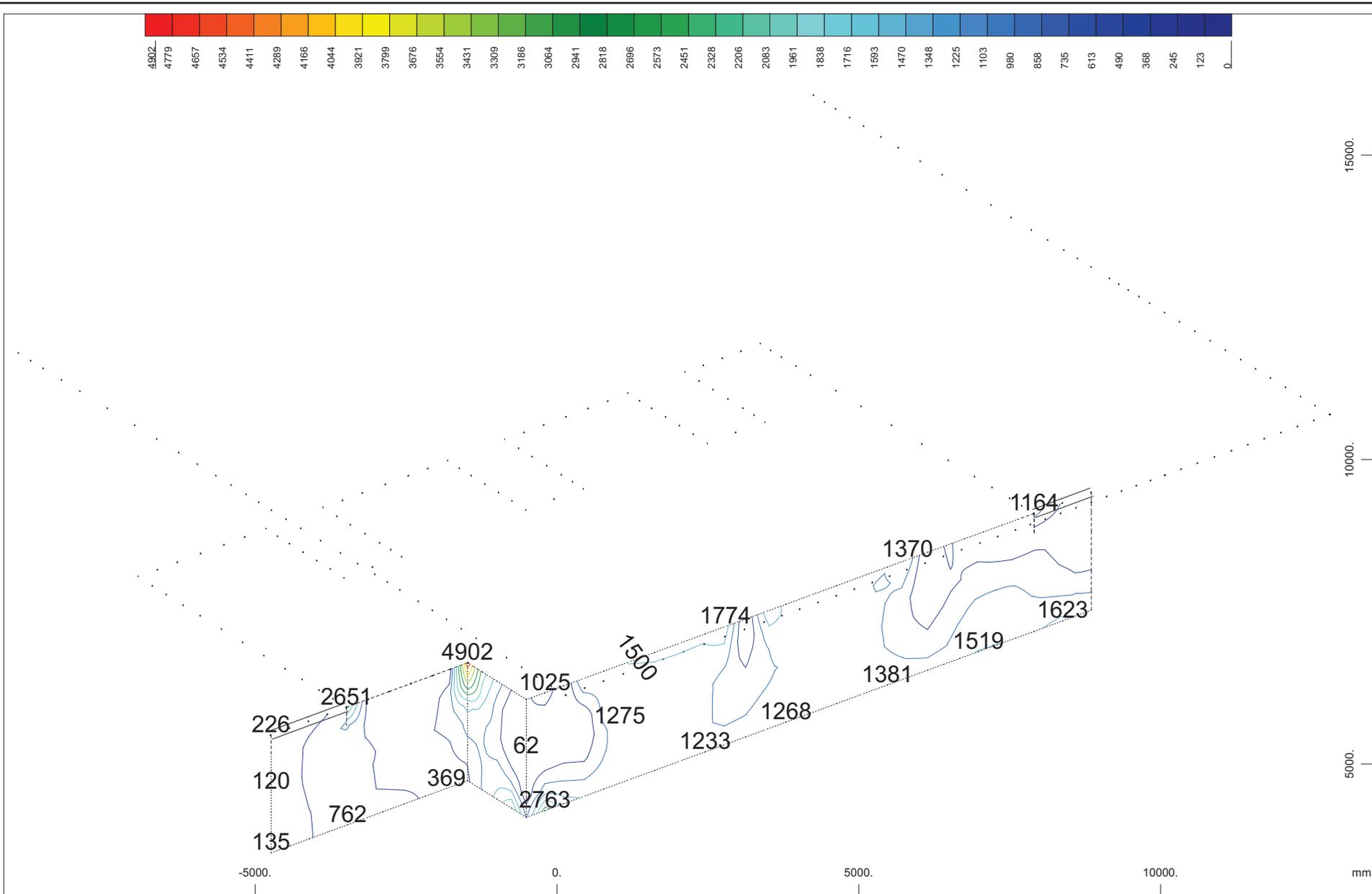
1/4 Design Case 1 , from 565.0 to 6341. step 500.0 mm2/m

M 1 : 90
 X* 0.845
 Y* 0.715
 Z* 0.880



Sector of system Quadrilateral Elements Group 125
 Quadrilateral Elements , lower Principal reinforcements (1st layer) in Node, Design Case 1 , from 565.0 to 3340. step 200.0 mm2/m

M 1 : 90
 X* 0.845
 Y* 0.715
 Z* 0.880

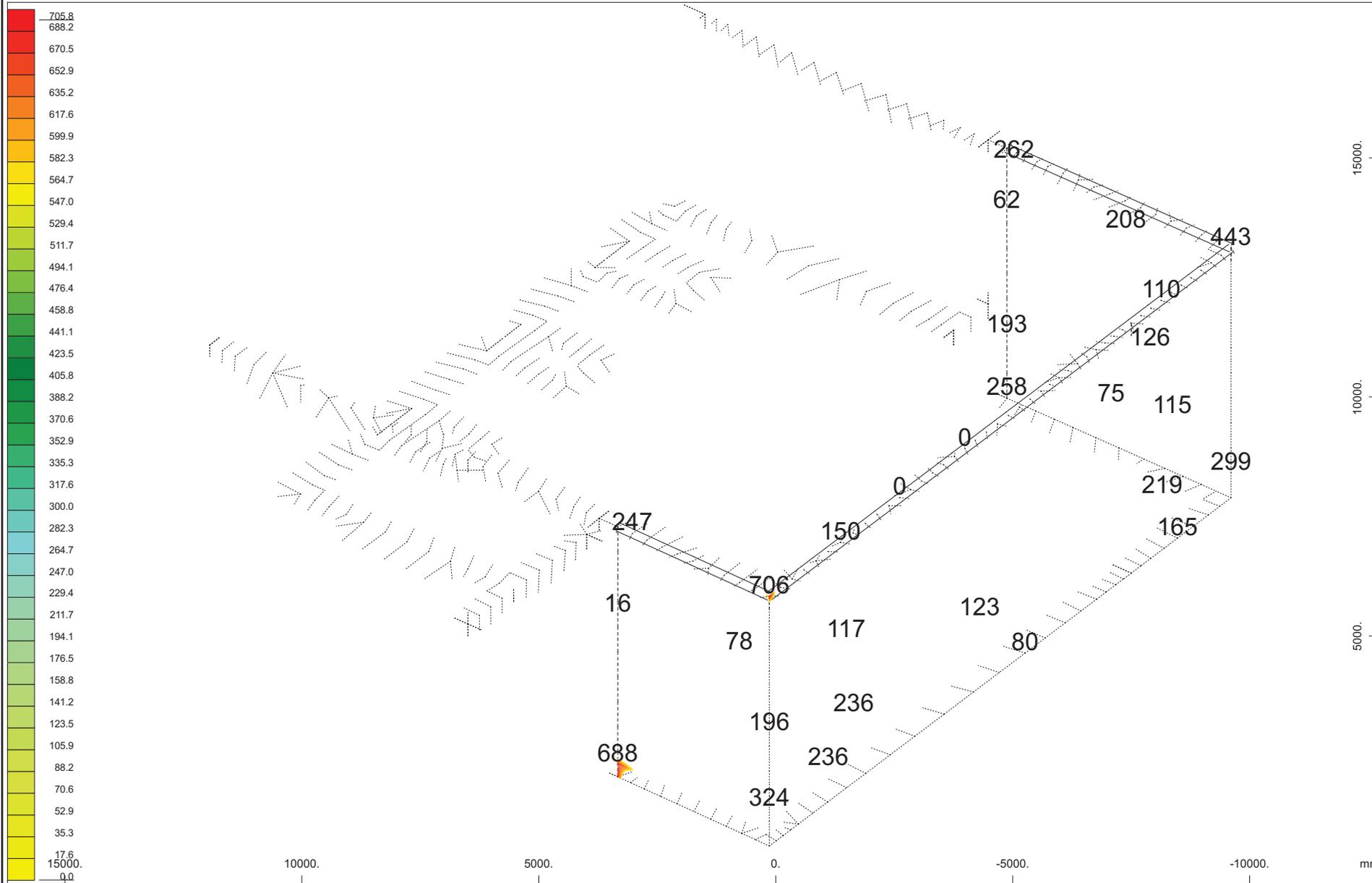


Y Z X

Sector of system Quadrilateral Elements Group 125
 Quadrilateral Elements , lower Cross reinforcements (2nd layer) in Node

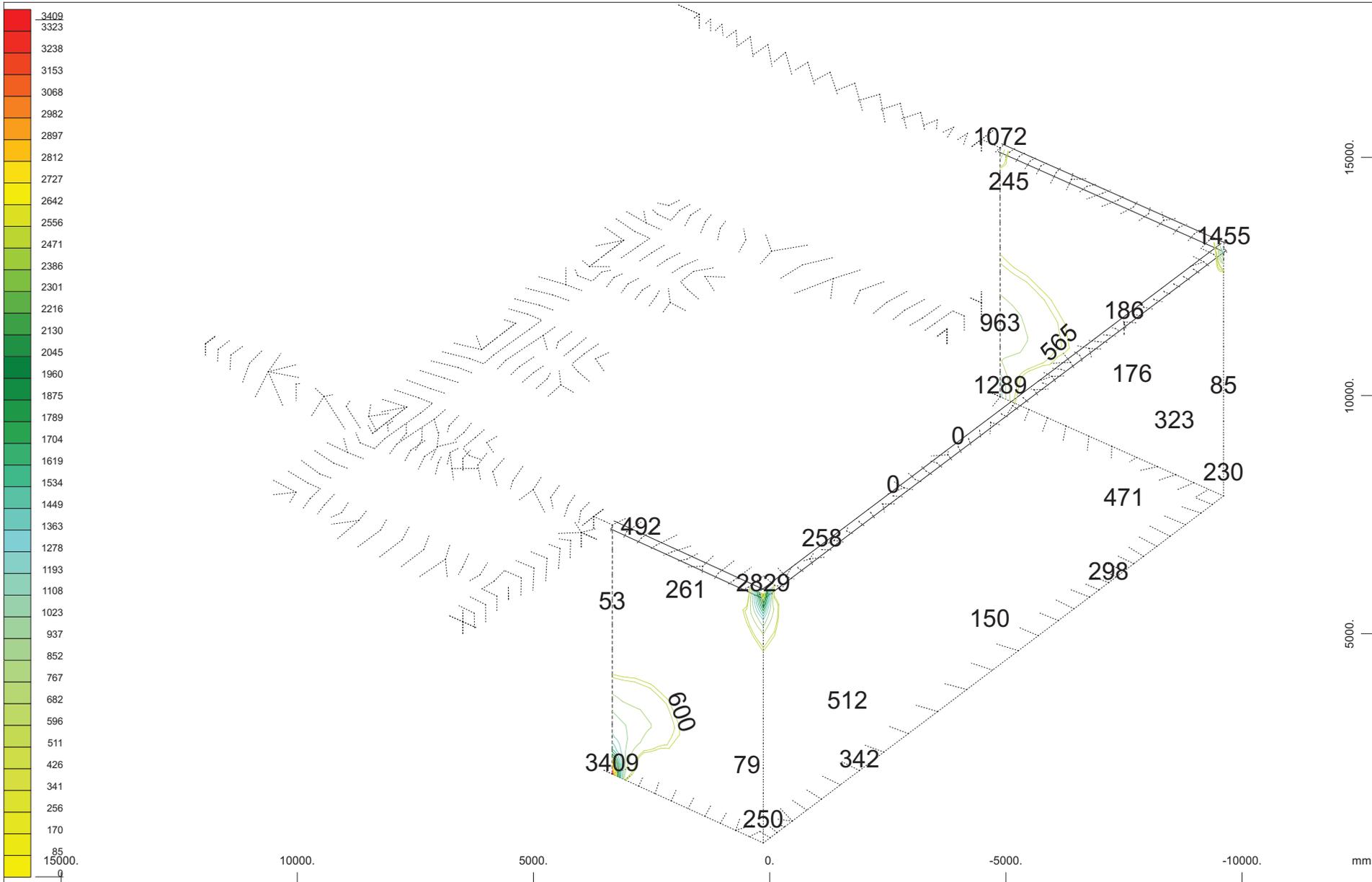
1/4 Design Case 1 , from 565.0 to 4902. step 500.0 mm2/m

M 1 : 90
 X* 0.845
 Y* 0.715
 Z* 0.880



Sector of system Quadrilateral Elements Group 150
 Quadrilateral Elements , upper Principal reinforcements (1st layer) in Node, Design Case 1 , from 565.0 to 705.8 step 10.0 mm2/m

M 1 : 115
 X * 0.763
 Y * 0.867
 Z * 0.817

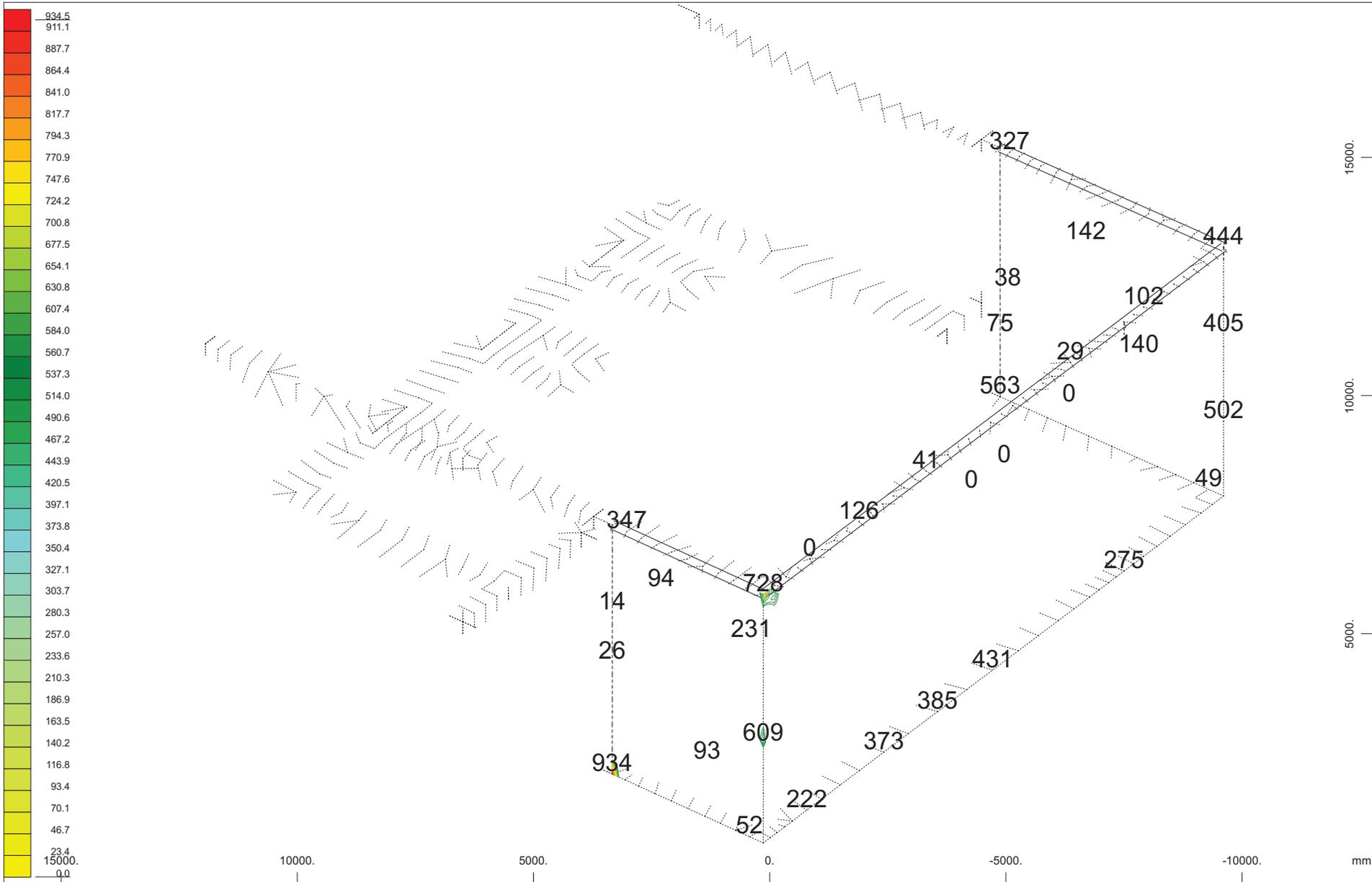


Y Z X

Sector of system Quadrilateral Elements Group 150
Quadrilateral Elements , upper Cross reinforcements (2nd layer) in Node

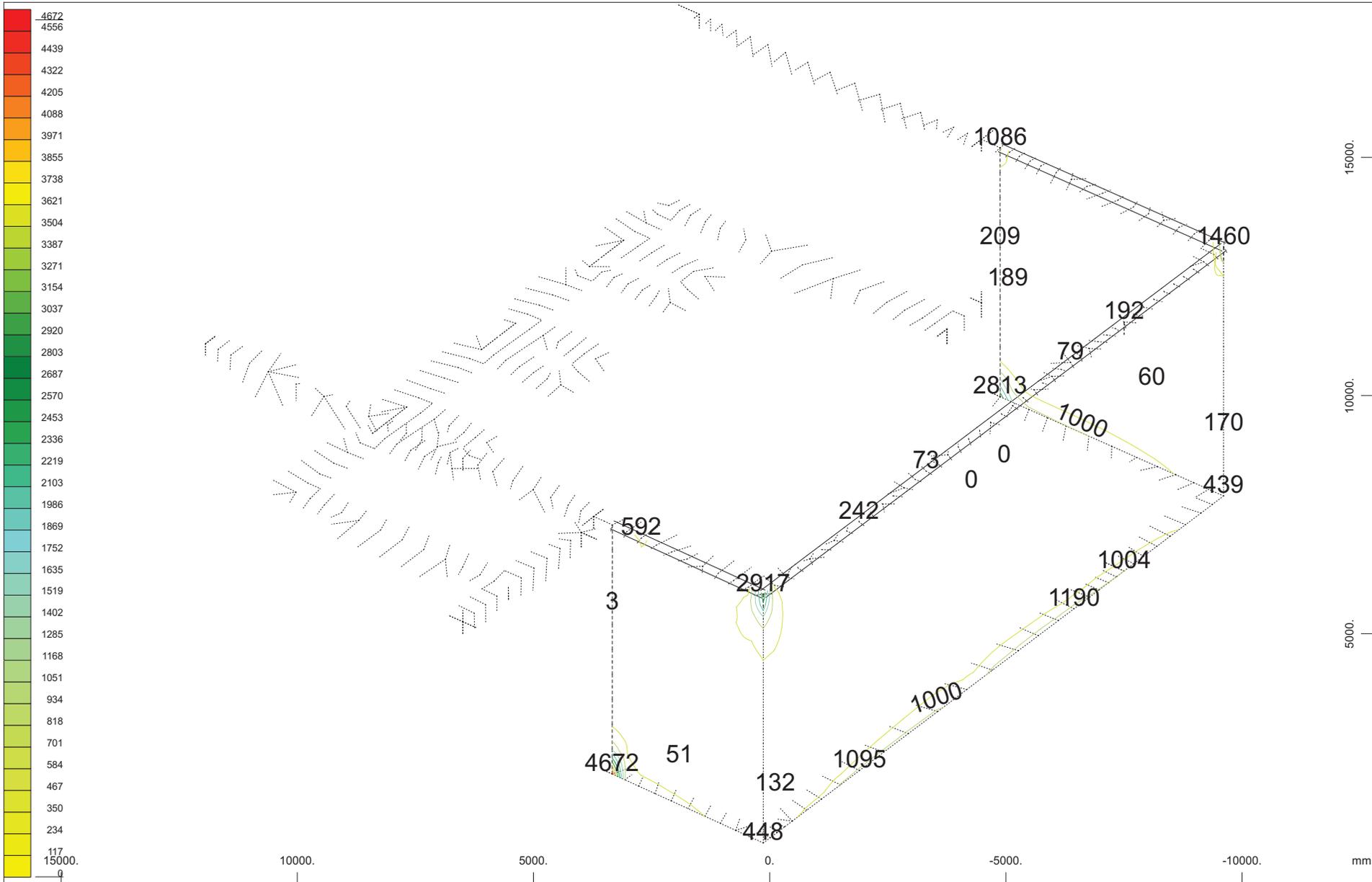
↓ , Design Case 1 , from 565.0 to 3409. step 200.0 mm2/m

M 1 : 115
X* 0.763
Y* 0.867
Z* 0.817



Sector of system Quadrilateral Elements Group 150
 Quadrilateral Elements , lower Principal reinforcements (1st layer) in Node, Design Case 1 , from 565.0 to 934.5 step 20.0 mm2/m

M 1 : 115
 X * 0.763
 Y * 0.867
 Z * 0.817

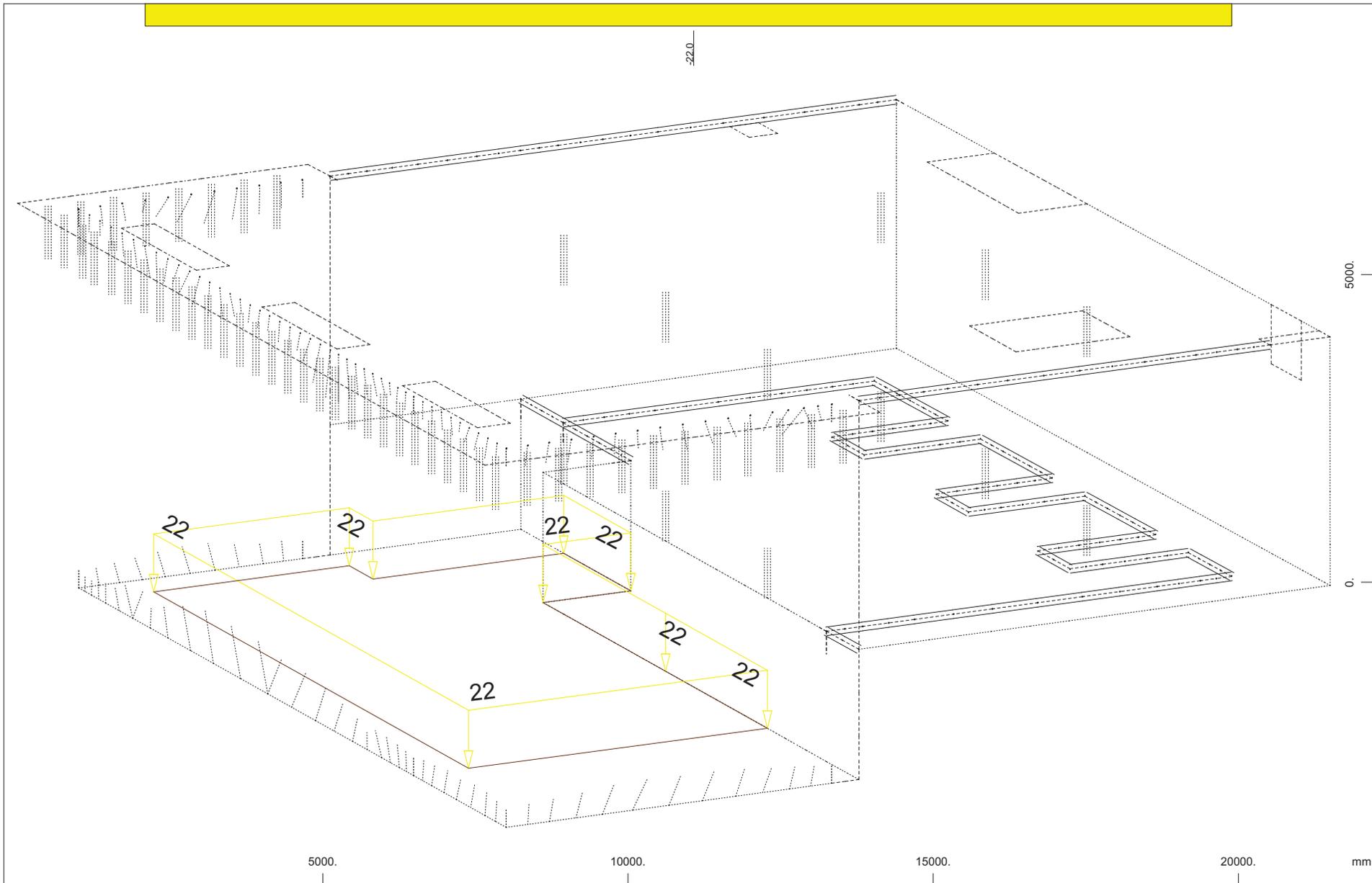


Y Z X

Sector of system Quadrilateral Elements Group 150
Quadrilateral Elements , lower Cross reinforcements (2nd layer) in Node

↓ , Design Case 1 , from 565.0 to 4672. step 500.0 mm2/m

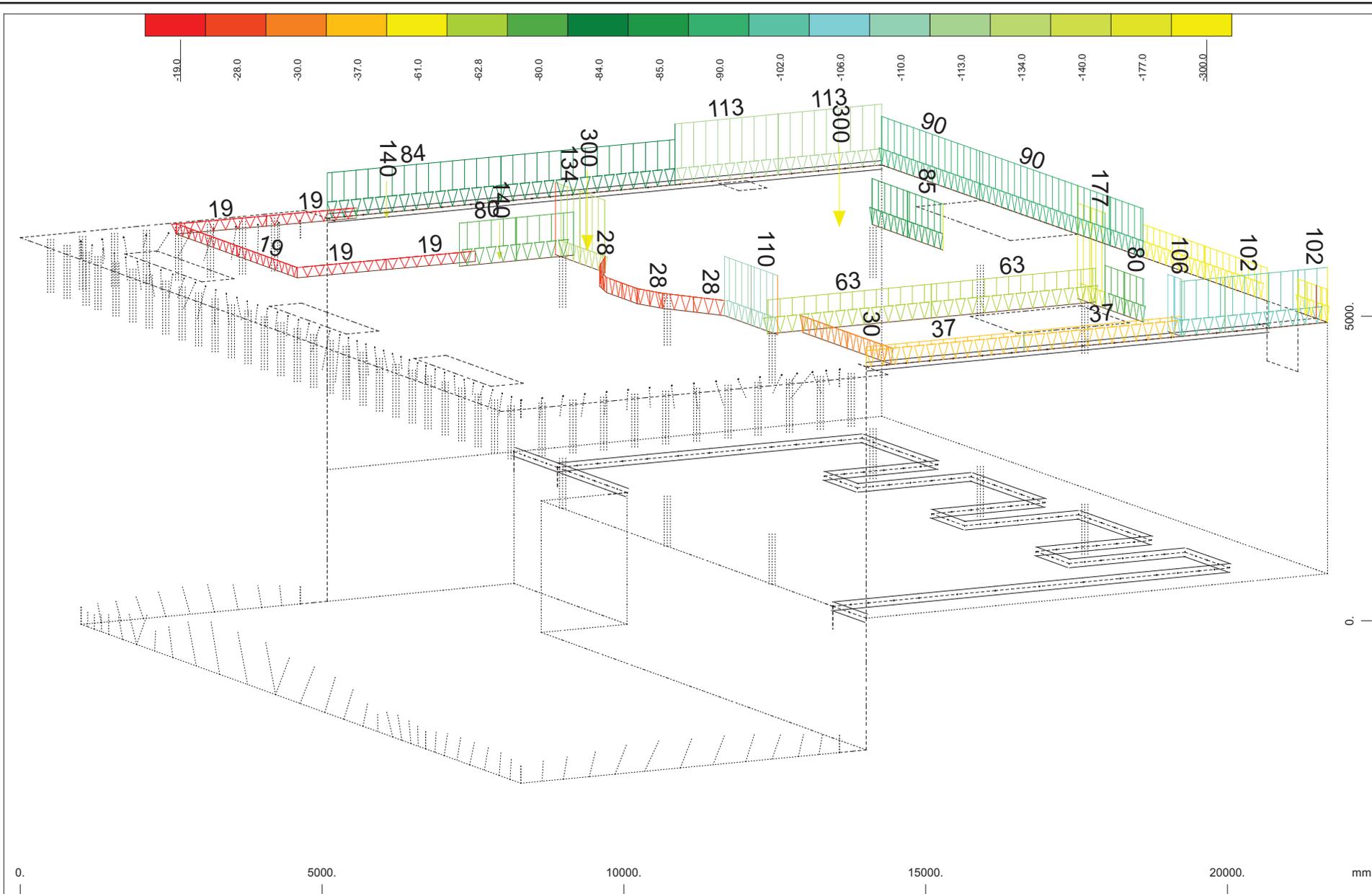
M 1 : 115
X * 0.763
Y * 0.867
Z * 0.817



Z Sector of system Quadrilateral Elements Group 100 110 120 125 135
 X Y All loads, Loadcase 2 POOL WATER , (1 cm 3D = unit) Free area load (force) in global Z (Unit=20.0 kN/m2)

(Min=-22.0) (Max=-22.0)

M 1 : 89
 X* 0.502
 Y* 0.906
 Z* 0.962

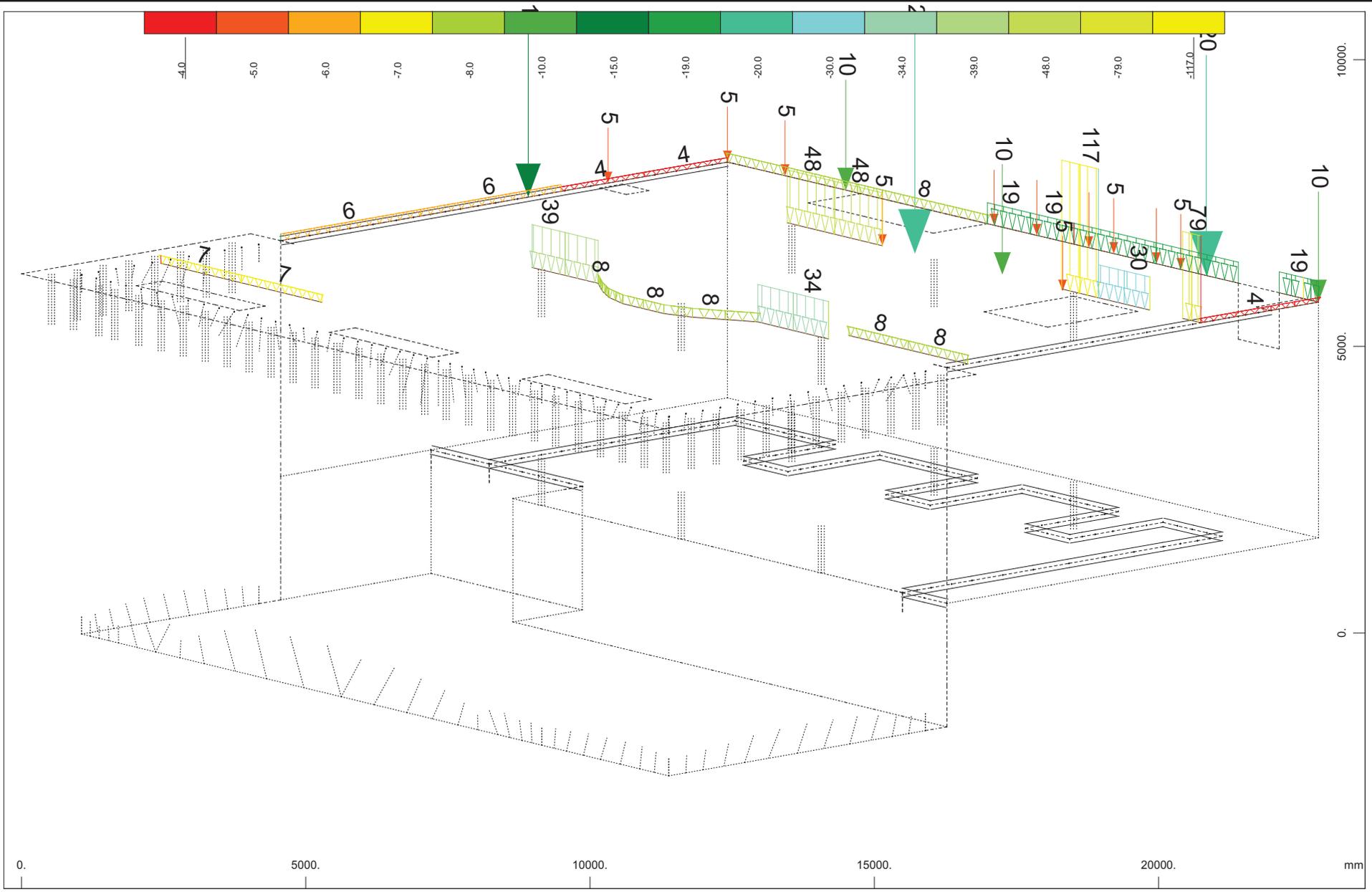


FE GA19787 TEMP
Interactive Graphic

Abbeey Pynford PLC Hemel Hempstead, HP2 7DX
WINGRAF - GRAPHICS FOR FINITE ELEMENTS (V 16.17-27)

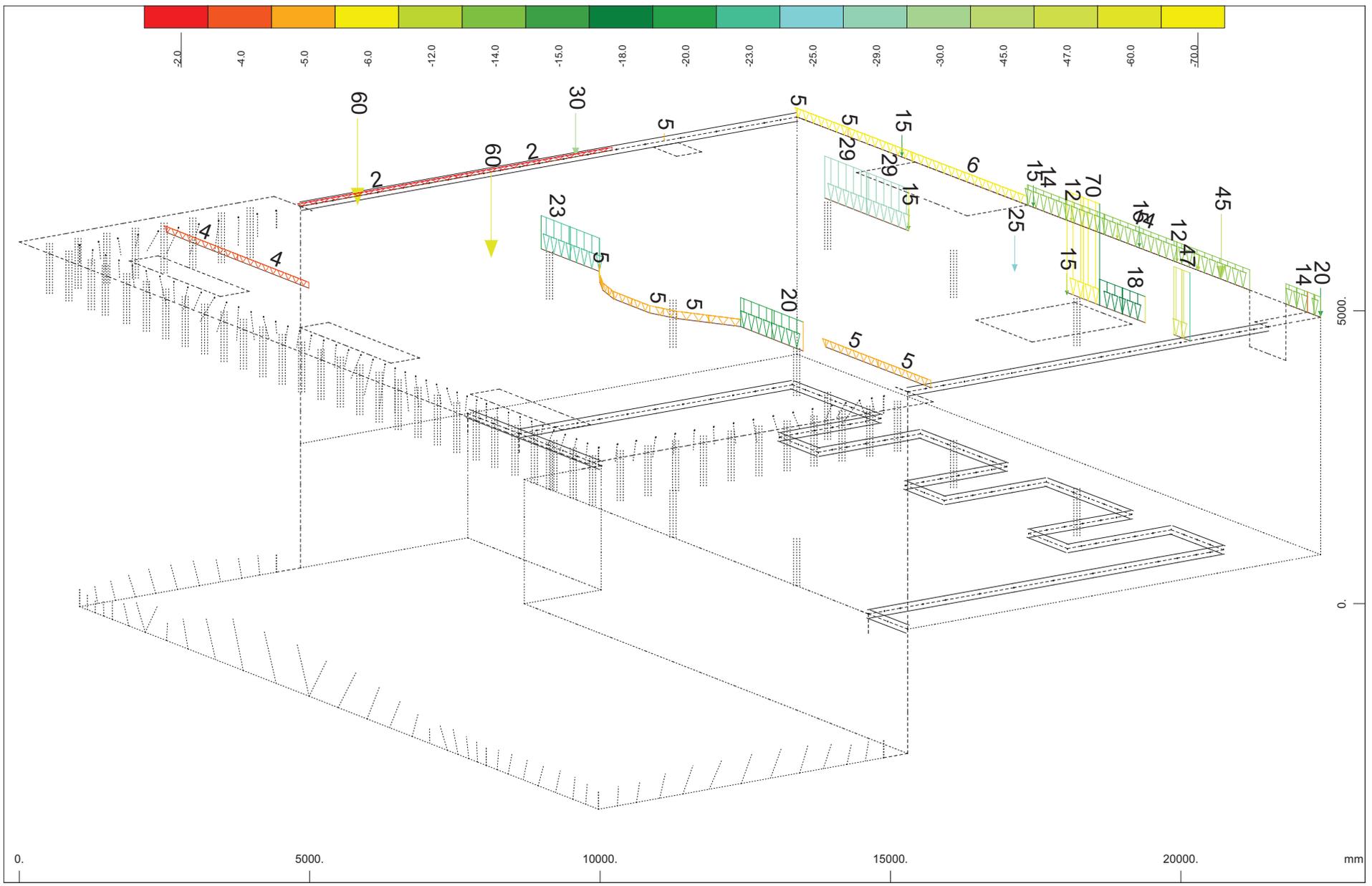
Sector of system Quadrilateral Elements Group 100 110 120 125 135
All loads, Loadcase 3 DL WALLS , (1 cm 3D = unit) Free single load (force) in global Z (Unit=200.0 kN,Min=-300.0 Max=-140.0)
Free line load (force) in global Z (Unit=100.0 kN/m,Min=-177.0 Max=-19.0)

M 1 : 90
X * 0.485
Y * 0.894
Z * 0.983



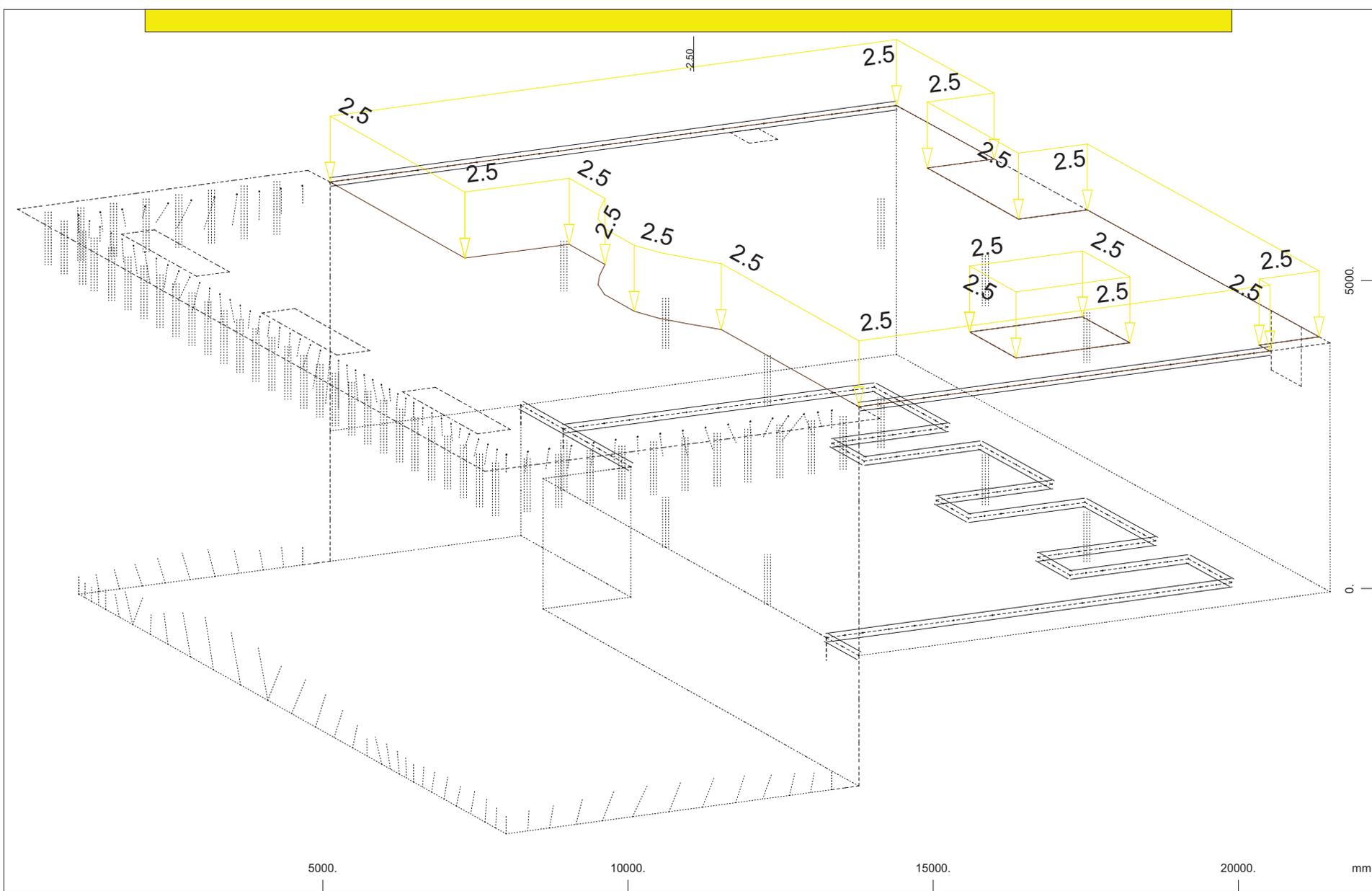
Sector of system Quadrilateral Elements Group 100 110 120 125 135
 All loads, Loadcase 4 DL UPPER FLOORS , (1 cm 3D = unit) Free single load (force) in global Z (Unit=4.84 kN, Min=-20.0 Max=-5.00
), Free line load (force) in global Z (Unit=48.4 kN/m, Min=-117.0 Max=-4.00

M 1 : 95
 X* 0.666
 Y* 0.773
 Z* 0.979



Sector of system Quadrilateral Elements Group 100 110 120 125 135
 All loads, Loadcase 5 LL UPPER FLOORS , (1 cm 3D = unit) Free single load (force) in global Z (Unit=36.3 kN,Min=-60.0 Max=-5.00), Free line load (force) in global Z (Unit=36.3 kN/m,Min=-70.0 Max=-2.00)

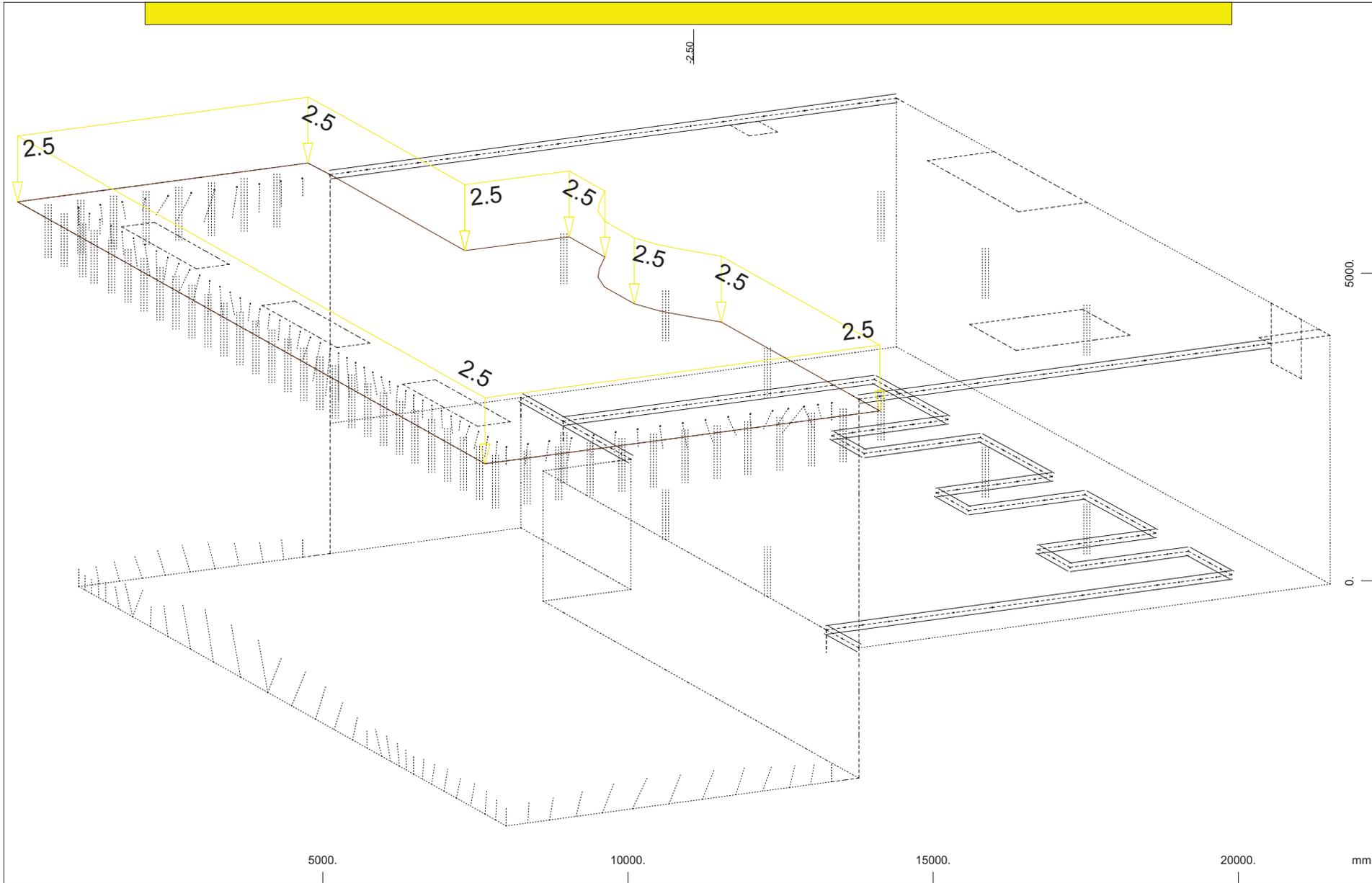
M 1 : 93
 X * 0.600
 Y * 0.841
 Z * 0.965



Z
 X Y
 Sector of system Quadrilateral Elements Group 100 110 120 125 135
 All loads, Loadcase 6 IMPOSED LGF INSIDE , (1 cm 3D = unit) Free area load (force) in global Z (Unit=2.00 kN/m2)
 (Max=-2.50)

(Min=-2.50)

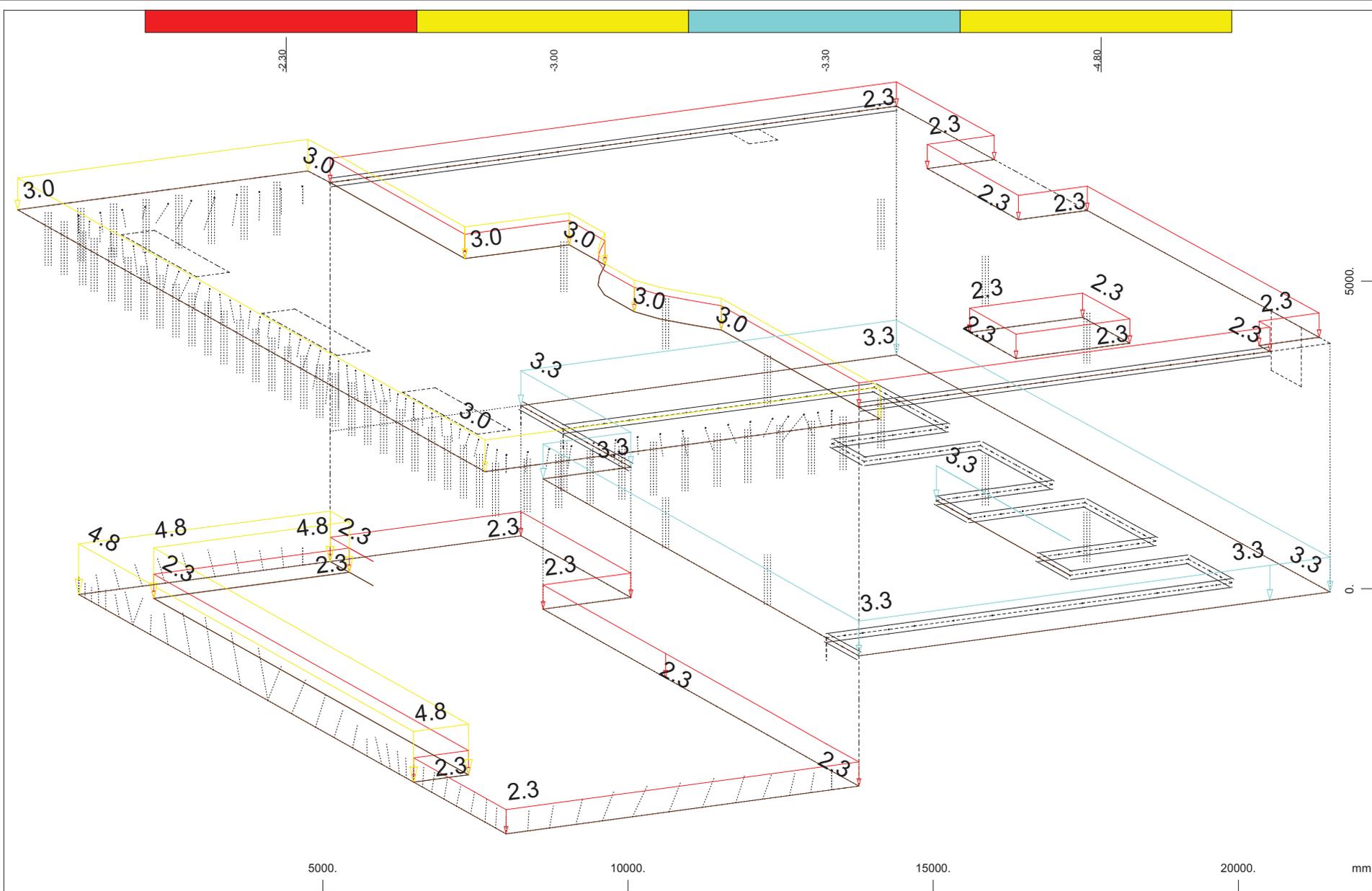
M 1 : 89
 X* 0.502
 Y* 0.906
 Z* 0.962



$\begin{matrix} Z \\ | \\ X \end{matrix} \begin{matrix} Y \\ | \\ X \end{matrix}$ Sector of system Quadrilateral Elements Group 100 110 120 125 135
 All loads, Loadcase 7 IMPOSED LGF OUTSIDE , (1 cm 3D = unit) Free area load (force) in global Z (Unit=2.00 kN/m2)
 (Max=-2.50)

∇ (Min=-2.50)

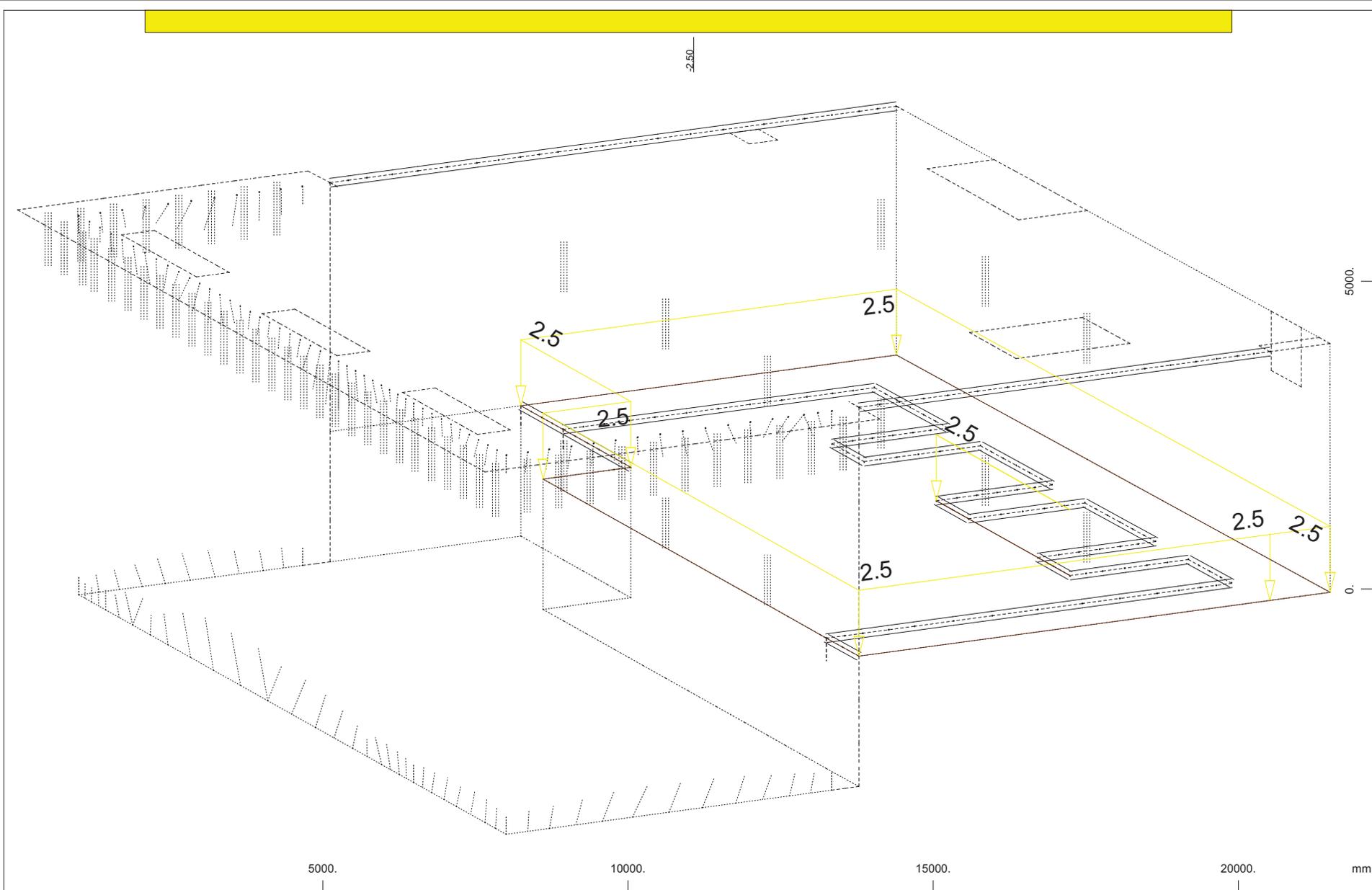
M 1 : 89
 X* 0.502
 Y* 0.906
 Z* 0.962



Z Sector of system Quadrilateral Elements Group 100 110 120 125 135
 X Y All loads, Loadcase 8 FINISHES , (1 cm 3D = unit) Free area load (force) in global Z (Unit=5.00 kN/m2)

△ (Min=-4.80) (Max=-2.30)

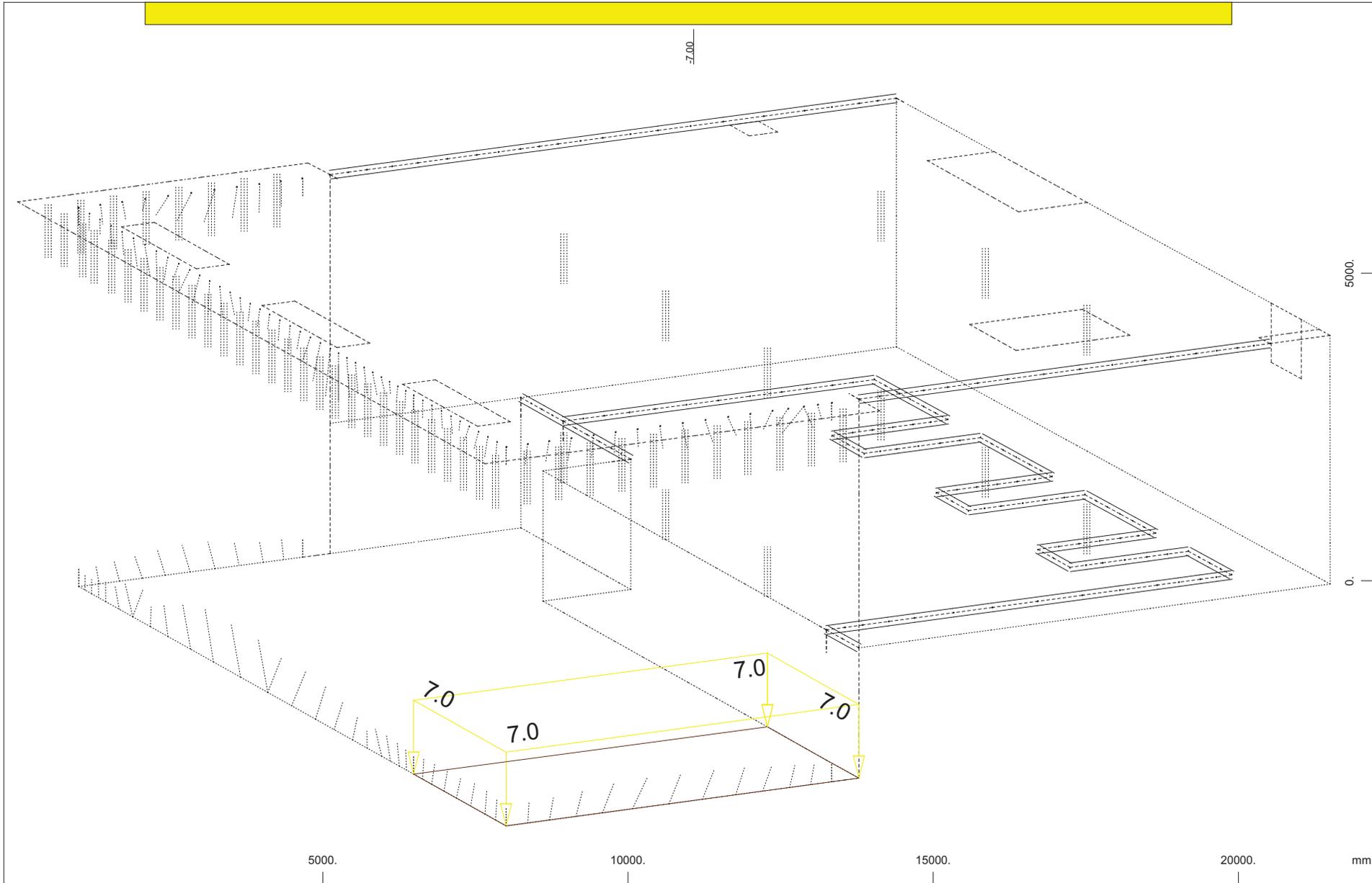
M 1 : 89
 X* 0.502
 Y* 0.906
 Z* 0.962



Z
 X Y
 Sector of system Quadrilateral Elements Group 100 110 120 125 135
 All loads, Loadcase 9 IMPOSED UPPER BASEMENT , (1 cm 3D = unit) Free area load (force) in global Z (Unit=2.00 kN/m2)
 (Max=-2.50)

▾ (Min=-2.50)

M 1 : 89
 X* 0.502
 Y* 0.906
 Z* 0.962

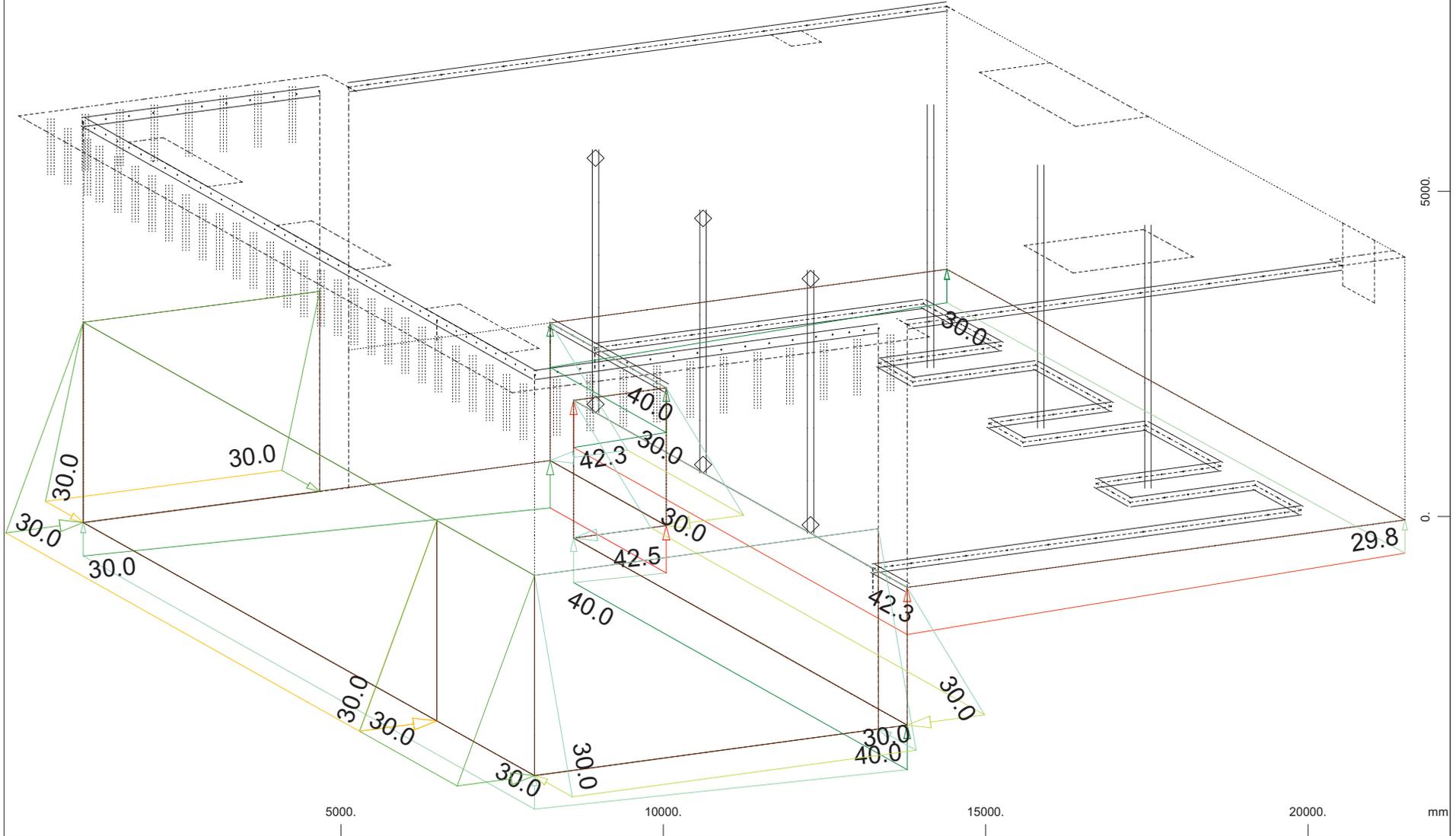
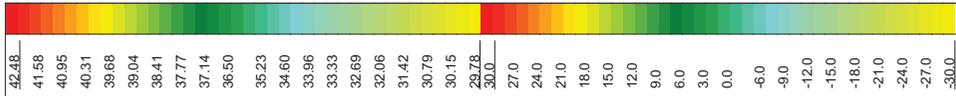


Z
Y
X

Sector of system Quadrilateral Elements Group 100 110 120 125 135
All loads, Loadcase 10 IMPOSED LOWER BASEMENT , (1 cm 3D = unit) Free area load (force) in global Z (Unit=5.00 kN/m2)
(Max=-7.00)

(Min=-7.00)

M 1 : 89
X* 0.502
Y* 0.906
Z* 0.962



Z
Y
X

Sector of system Group 100 110 120 125 130 135 150
 All loads, Loadcase 11 UPLIFT FORCE , (1 cm 3D = unit) Free area load (force) in global Z (Unit=50.0 kN/m2)
 All loads, Loadcase 12 WATER PRESSURE , (1 cm 3D = unit) Free area load (force) in global X (Unit=20.0 kN/m2,Min=-30.0 Max=30.0)

(Max=42.5)

,

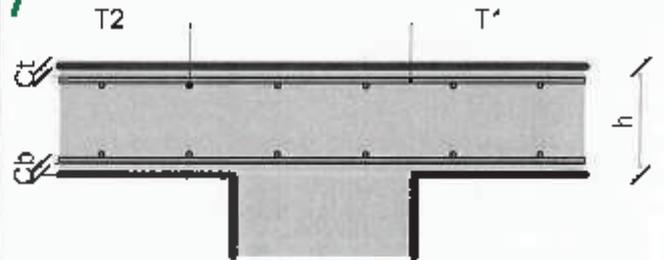
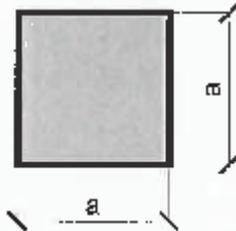
M 1 : 89
 X* 0.502
 Y* 0.906
 Z* 0.962

Project Ref:	400mm Column		 APP/E-40 Telephone
Project Title:	69 Redington Rd	REV	
		-	
Block/Building:		Floor:	
Column Ref:		Sheet:	1 of 3

Design Input

Column type: Square internal
 Column size (a): 400 mm
 Slab depth (h): 350 mm
 Top cover (Ct): 35 mm
 Bottom cover (Cb): 35 mm
 T1 reinforcement: $\varnothing 20 = 2136.29 \text{ mm}^2$
 T2 reinforcement: $\varnothing 20 = 2136.29 \text{ mm}^2$

Shear load (Vt): 1397 kN : Max. Load
 fcu: 35 N/mm²
 fyv: 500 N/mm²
 Load factor: 1.15
 (Factors)



Area table

Perimeter	Shearlink® $\varnothing 10 \text{ mm}$	Steel area provided [mm ²]	Steel area required [mm ²]
0.5d	8	628.32	557.72
U1	8 + 16 = 24	1884.96	1394.30
U2	16 + 24 = 40	3141.59	1874.44

Stud length: 280 mm
 Effective depth: 295.0 mm

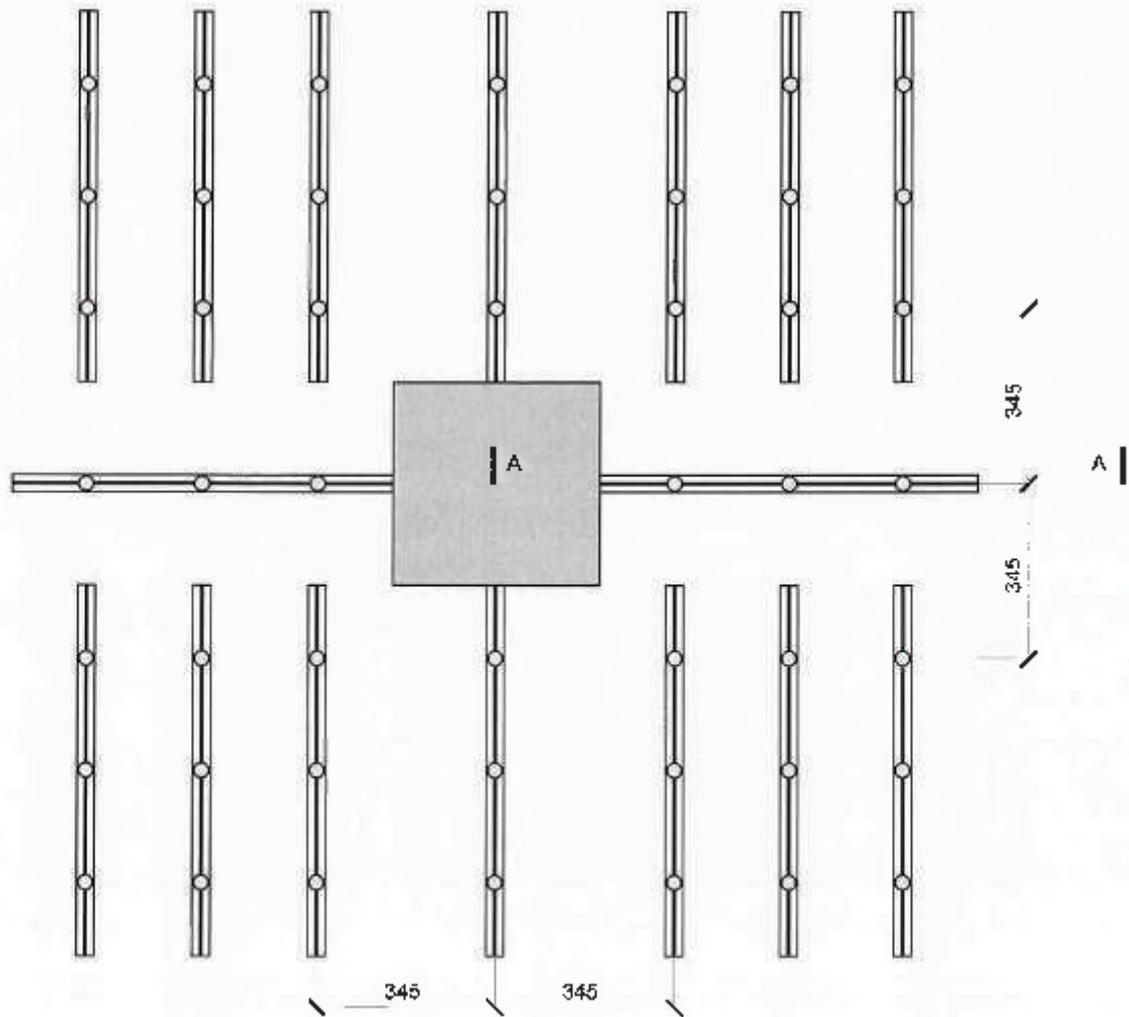
Project Ref:				 APP/E-41
Project Title:			REV	
			-	
Block/Building:		Floor:		
Column Ref:		Sheet:	2 of 3	Telephone:

Results

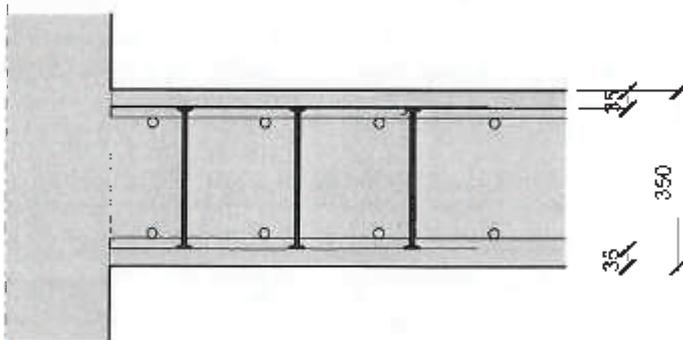
$d = 350 - 35 - 20/2 - 20/2$	=	295.0 mm
$V_{eff} = 1.15 \times 1397$	=	1606.55 kN
$u_0 = 4 \times 400$	=	1600.0 mm
$v = 1606.55 \times 10^3 / (1600.0 \times 295.0)$	=	3.404 N/mm ²
$0.8 \times 35^{1/2}$	=	4.73 N/mm ²
3.40 < 4.73 PASS		
$100 \times A_s / (b \times d) = (100 \times 2136.29 / (1000 \times 305.0) + 100 \times 2136.29 / (1000 \times 285.0)) / 2$	=	0.725 (Average)
$(400 / d)^{1/4} = (400 / 295.0)^{1/4}$	=	1.08
$vc = [0.79 \times (0.725^{1/3} \times 1.08) / 1.25] \times (35/25)^{1/3}$	=	0.685 N/mm ²
Perimeter U1		
$u_1 = 4 \times 400 + 12.0 \times 295.0$	=	5140.0 mm
$v = (1606.55 \times 10^3) / (5140.0 \times 295.0)$	=	1.060 N/mm ²
$A_{sv(min)} > A_{sv}$ therefore minimum required steel area used		
$A_{sv(min)} = (0.4 \times 5140.0 \times 295.0) / (0.87 \times 500)$	=	1394.30 mm ²
Perimeter U2		
$u_2 = 4 \times 400 + 18.0 \times 295.0$	=	6910.0 mm
$v = (1606.55 \times 10^3) / (6910.0 \times 295.0)$	=	0.788 N/mm ²
$A_{sv(min)} > A_{sv}$ therefore minimum required steel area used		
$A_{sv(min)} = (0.4 \times 6910.0 \times 295.0) / (0.87 \times 500)$	=	1874.44 mm ²
Perimeter U3		
$u_3 = 4 \times 400 + 24.0 \times 295.0$	=	8680.0 mm
$v = (1606.55 \times 10^3) / (8680.0 \times 295.0)$	=	0.627 N/mm ²
$v < vc$ therefore no more punching shear reinforcement is required		

Project Ref:				 <i>AR/E-42</i>
Project Title:			REV	
			-	
Block/Building:		Floor:		Telephone:
Column Ref:		Sheet:	3 of 3	

Layout Plan



Section A-A



Shearail® requirement

16 rails per location
 Number of locations: 1
 Total number of rails: 16

Rail code: ES1DE917D3CR

Project Ref:	400mm Column on EDGE			 APP/E - 43 Telephone:
Project Title:	69 Redington Rd		REV	
			-	
Block/Building:		Floor:		
Column Ref:		Sheet:	1 of 3	

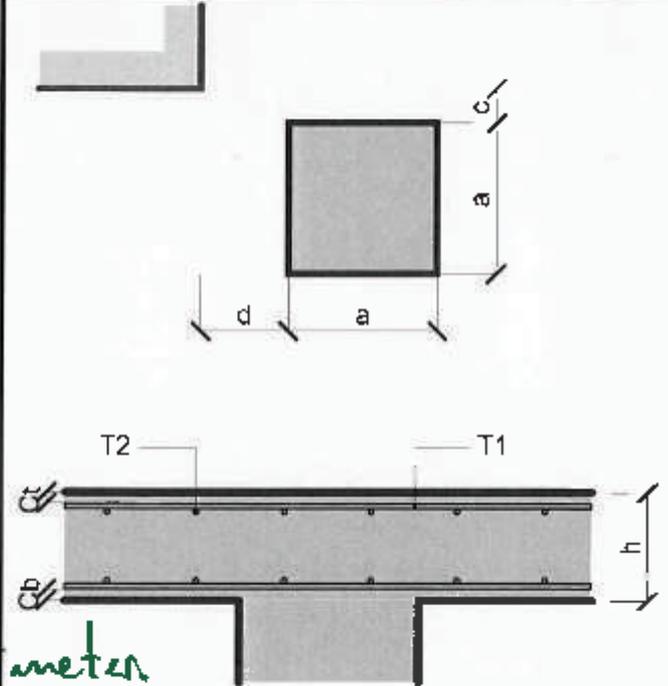
Design Input

Column type: Square external corner
 Column size (a): 400 mm
 Offset (c): 0 mm
 Offset (d): 0 mm
 Slab depth (h): 350 mm
 Top cover (Ct): 35 mm
 Bottom cover (Cb): 35 mm
 T1 reinforcement: $\varnothing 20 = 2136.29 \text{ mm}^2$
 T2 reinforcement: $\varnothing 20 = 2136.29 \text{ mm}^2$

Shear load (Vt): 938 kN
 fcu: 35 N/mm²
 fyv: 500 N/mm²
 Load factor: 1.25

$$938 = 70\% \text{ of } 1340 \text{ kN}$$

min 30% of the load is inside the shear perimeter



Area table

Perimeter	Shearail@ $\varnothing 10 \text{ mm}$	Steel area provided [mm ²]	Steel area required [mm ²]
0.5d	7	549.78	461.69
U1	7 + 13 = 20	1570.80	1154.23
U2	13 + 19 = 32	2513.27	1514.33

Stud length: 280 mm
 Effective depth: 295.0 mm



Project Ref:			
Project Title:			REV
			-
Block/Building:		Floor:	
Column Ref:		Sheet:	2 of 3

Telephone:

Results

$d = 350 - 35 - 20/2 - 20/2$	=	295.0 mm
$V_{eff} = 1.25 \times 938$	=	1172.50 kN
$u_0 = (4 \times 400)$	=	1600.0 mm
$v = 1172.50 \times 10^3 / (1600.0 \times 295.0)$	=	2.484 N/mm ²
$0.8 \times 35^{1/3}$	=	4.73 N/mm ²
2.48 < 4.73 PASS		
$100 \times A_s / (b \times d) = (100 \times 2136.29 / (1000 \times 305.0) + 100 \times 2136.29 / (1000 \times 285.0)) / 2$	=	0.725 (Average)
$(400 / c)^{1/4} = (400 / 295.0)^{1/4}$	=	1.08
$v_c = [0.79 \times (0.725^{1/3} \times 1.08) / 1.25] \times (35/25)^{1/3}$	=	0.685 N/mm ²

Perimeter U1

$u_1 = 4 \times 400 + 0 + 0 + 9.0 \times 295.0$	=	4255.0 mm
$v = (1172.50 \times 10^3) / (4255.0 \times 295.0)$	=	0.934 N/mm ²
$A_{sv(min)} > A_{sv}$ therefore minimum required steel area used		
$A_{sv(min)} = (0.4 \times 4255.0 \times 295.0) / (0.87 \times 500)$	=	1154.23 mm ²

Perimeter U2

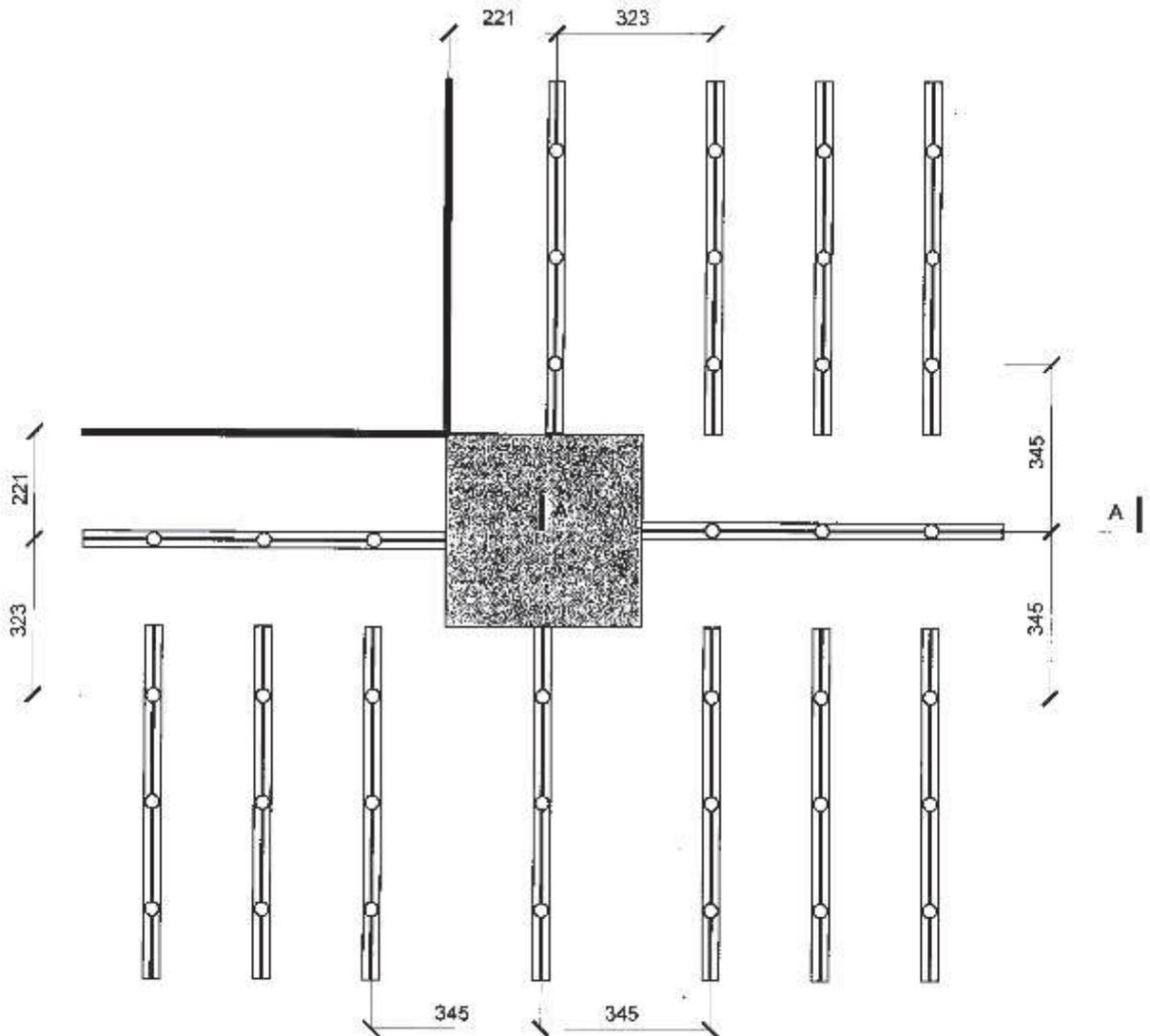
$u_2 = 4 \times 400 + 0 + 0 + 13.5 \times 295.0$	=	5582.5 mm
$v = (1172.50 \times 10^3) / (5582.5 \times 295.0)$	=	0.712 N/mm ²
$A_{sv(min)} > A_{sv}$ therefore minimum required steel area used		
$A_{sv(min)} = (0.4 \times 5582.5 \times 295.0) / (0.87 \times 500)$	=	1514.33 mm ²

Perimeter U3

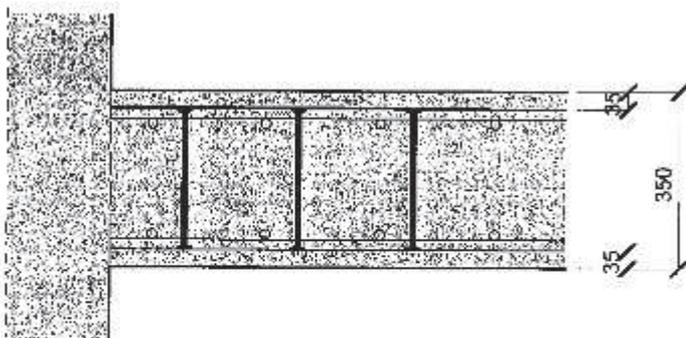
$u_3 = 4 \times 400 + 0 + 0 + 18.0 \times 295.0$	=	6910.0 mm
$v = (1172.50 \times 10^3) / (6910.0 \times 295.0)$	=	0.575 N/mm ²
$v < v_c$ therefore no more punching shear reinforcement is required		

Project Ref:				 APP/E-45
Project Title:			REV	
			-	
Block/Building:		Floor:		
Column Ref:		Sheet:	3 of 3	
				Telephone:

Layout Plan



Section A-A



Shearail® requirement

13 rails per location
 Number of locations: 1
 Total number of rails: 13

Rail code: ES1DE917D3CR

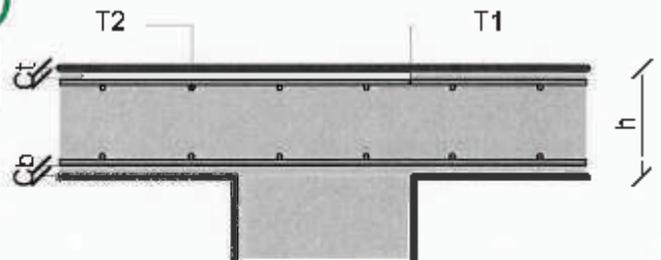
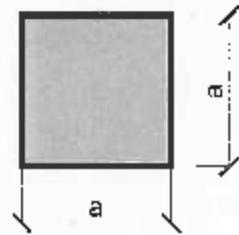
Project Ref:	350 mm Column			 APP/E-46 Telephone
Project Title:	69 Redington Rd		REV	
Block/Building:		Floor:	-	
Column Ref:		Sheet:	1 of 3	

Design Input

Column type: Square internal
 Column size (a): 350 mm
 Slab depth (h): 350 mm
 Top cover (Ct): 35 mm
 Bottom cover (Cb): 35 mm
 T1 reinforcement: $\varnothing 20 = 2136.29 \text{ mm}^2$
 T2 reinforcement: $\varnothing 20 = 2136.29 \text{ mm}^2$

Shear load (Vt): 1277 kN : Max load (factored)
 fcu: 35 N/mm²
 fyv: 500 N/mm²
 Load factor: 1.15

Max. factored load is 1277 kN; but min. 30% of this load is inside the shear perimeter.



Area table

Perimeter	Shearail® Ø 10 mm	Steel area provided [mm ²]	Steel area required [mm ²]
0.5d	8	628.32	536.02
U1	8 + 16 = 24	1884.96	1340.05
U2	16 + 24 = 40	3141.59	1820.18

Stud length: 280 mm
 Effective depth: 295.0 mm



Project Ref:			
Project Title:			REV
			-
Block/Building:		Floor:	
Column Ref:		Sheet:	2 of 3

Telephone:

Results

$d = 350 - 35 - 20/2 - 20/2$	=	295.0 mm
$V_{eff} = 1.15 \times 1277$	=	1468.55 kN
$u_0 = 4 \times 350$	=	1400.0 mm
$v = 1468.55 \times 10^{-3} / (1400.0 \times 295.0)$	=	3.556 N/mm ²
$0.8 \times 35^{1/3}$	=	4.73 N/mm ²
3.56 < 4.73 PASS		
$100 \times A_s / (b \times d) = (100 \times 2'36.29 / (1000 \times 305.0) + 100 \times 2'36.29 / (1000 \times 285.0)) / 2$	=	0.725 (Average)
$(400 / d)^{1/4} = (400 / 295.0)^{1/4}$	=	1.08
$vc = [0.79 \times (0.725^{1/3} \times 1.08) / 1.25] \times (35/25)^{1/3}$	=	0.685 N/mm ²

Perimeter U1

$u_1 = 4 \times 350 + 12.0 \times 295.0$	=	4940.0 mm
$v = (1468.55 \times 10^{-3}) / (4940.0 \times 295.0)$	=	1.008 N/mm ²
$A_{sv(min)} > A_{sv}$ therefore minimum required steel area used		
$A_{sv(min)} = (0.4 \times 4940.0 \times 295.0) / (0.87 \times 500)$	=	1340.05 mm ²

Perimeter U2

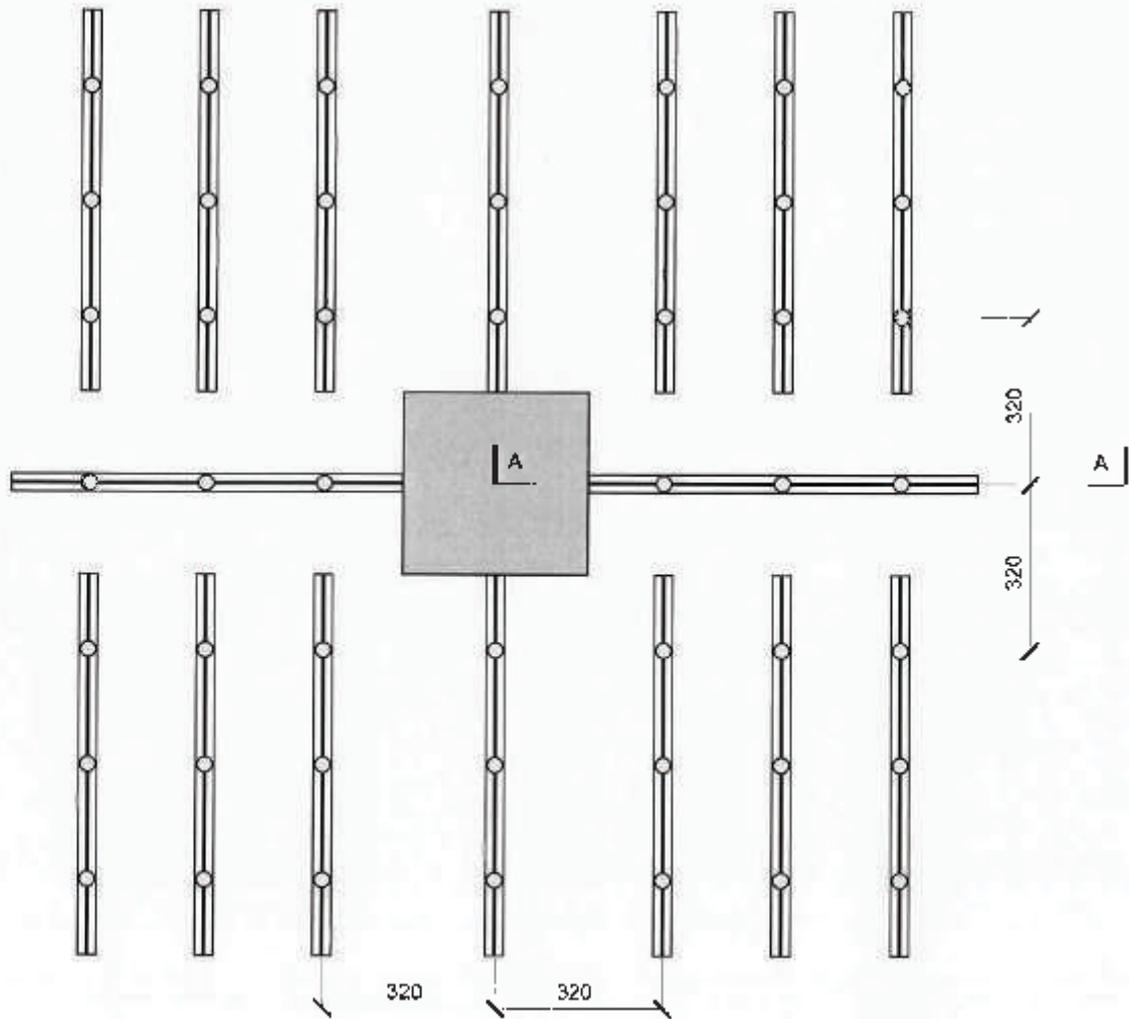
$u_2 = 4 \times 350 + 18.0 \times 295.0$	=	6710.0 mm
$v = (1468.55 \times 10^{-3}) / (6710.0 \times 295.0)$	=	0.742 N/mm ²
$A_{sv(min)} > A_{sv}$ therefore minimum required steel area used		
$A_{sv(min)} = (0.4 \times 6710.0 \times 295.0) / (0.87 \times 500)$	=	1820.18 mm ²

Perimeter U3

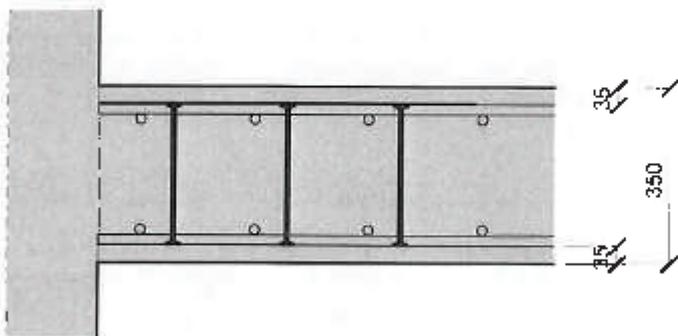
$u_3 = 4 \times 350 + 24.0 \times 295.0$	=	8480.0 mm
$v = (1468.55 \times 10^{-3}) / (8480.0 \times 295.0)$	=	0.587 N/mm ²
$v < vc$ therefore no more punching shear reinforcement is required		

Project Ref:				 APP/E-4B Telephone:
Project Title:			REV	
			-	
Block/Building:		Floor:		
Column Ref:		Sheet:	3 of 3	

Layout Plan



Section A-A



Shearail® requirement

16 rails per location
 Number of locations: 1
 Total number of rails: 16

Rail code: ES1DE917D3CR

Project 69 Redington Rd
 Client SHAKIB
 Location LONDON
 SYMMETRICALLY REINFORCED RECTANGULAR COLUMN DESIGN, BENT ABOUT TWO AXES TO BS 8110:2005
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The Concrete Centre

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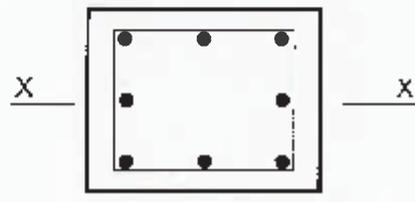
Made by JO	Date 09-Dec-14	Page APP/E-49
Checked MJ	Revision -	Job No GA19787

MATERIALS

fcu	35	N/mm ²	ym. steel	1.15	Cover to link	35	mm
fy	500	N/mm ²	ym. conc	1.5	h agg	20	mm
steel class	A						

SECTION

h	400	mm
b	400	mm
with	3	#N/A
and	3	#N/A



RESTRAINTS

	Lo (mm)	Top Condition	Btm Condition	Braced ?	β	Le (mm)	Slenderness	Status
X-AXIS	3000	2	3	Y	0.95	2850	Lex/h = 7.13	Column is SHORT
Y-AXIS	3000	2	3	Y	0.95	2850	Ley/b = 7.13	

LOADCASES

	AXIAL N (kN)	TOP MOMENTS (kNm)		BTM MOMENTS (kNm)	
		M _{ix}	M _{iy}	M _{ix}	M _{iy}
B1	1472	110.0	110.0	0.0	0.0
B2	1472		110.0	0.0	0.0
Loadcase 3				0.0	0.0
Loadcase 4				0.0	0.0
Loadcase 5				0.0	0.0
Loadcase 6				0.0	0.0

BAR ARRANGEMENTS

Bar \emptyset	Asc %	Link \emptyset	BAR CENTRES (mm)		Nuz (kN)	Checks
			400 Face	400 Face		
H 40	6.28	10	135	135	0	Asc > 6% (3.12.6.2)
H 32	4.02	8	141	141	5198	ok
H 25	2.45	8	145	145	4147	ok
H 20	1.57	6	149	149	3555	ok
H 16	1.01	6	151	151	3176	ok
H 12	0.57	6	153	153	2881	ok

DESIGN MOMENTS (kNm)

	X AXIS			Y AXIS		COMBINED		REBAR	max V [*]
	K	M add	M _x	M add	M _y	Axis	M'		
B1	0.000	0.0	110.0	0.0	110.0	X	186.3	8 H [*] 6	75.2
B2	0.000	0.0	0.0	0.0	110.0	Y	110.0	8 H [*] 2	62.5
Loadcase 3									#DIV/0!
Loadcase 4									#DIV/0!
Loadcase 5									#DIV/0!
Loadcase 6									#DIV/0!

SEE CHARTS ON NEXT SHEET

eccentricity = 75mm applied to both axis

Project 69 Redington Rd

Client SHAKIB

Location LONDON

SYMMETRICALLY REINFORCED RECTANGULAR COLUMN DESIGN,
BENT ABOUT TWO AXES TO BS 8110:2005

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Date
09-Dec-14

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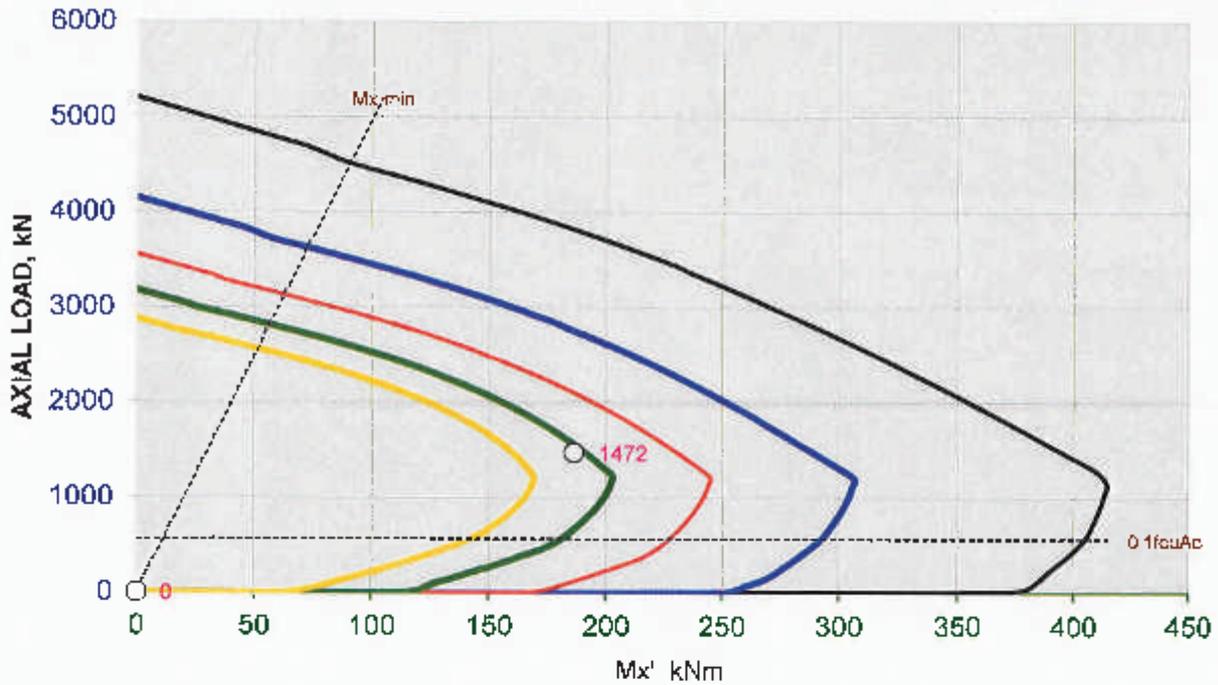
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Revision
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Job No
GA19787

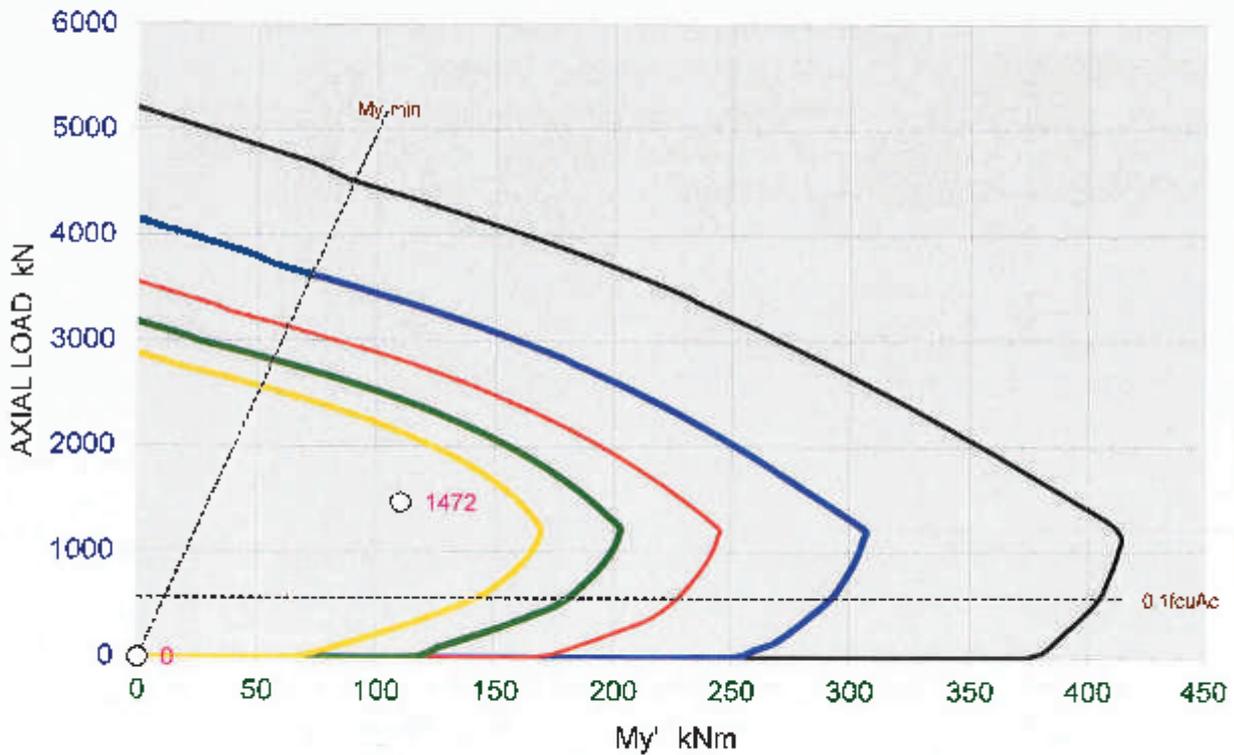
N:M interaction chart: M_x' critical

400 x 400 column (h x b), grade C35, 35 mm cover



N:M interaction chart: M_y' critical

400 x 400 column (h x b), moment about yy axis), Grade C35, 35 Cover



Project 69 Redington Rd
 Client SHAKIB
 Location LONDON
 SYMMETRICALLY REINFORCED RECTANGULAR COLUMN DESIGN, BENT ABOUT TWO AXES TO BS 8110:2005
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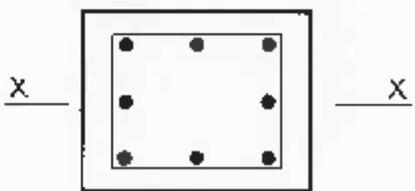
Made by JO	Date 09-Dec-14	Page APP/E-51
Checked MJ	Revision -	Job No GA19787

MATERIALS

fcu	35	N/mm ²	ym. steel	1.15	Cover to link	35	mm
fy	500	N/mm ²	ym. conc	1.5	h agg	20	mm
steel class	A						

SECTION

h	350	mm
b	350	mm
with	3	#N/A
and	3	#N/A



RESTRAINTS

	Lo (mm)	Top Condition	Btm Condition	Braced ?	β	Le (mm)	Slenderness	Status
X-AXIS	3000	2	3	Y	0.95	2850	Lex/h = 8.14	Column is SHORT
Y-AXIS	3000	2	3	Y	0.95	2850	Ley/b = 8.14	

LOADCASES

	AXIAL N (kN)	TOP MOMENTS (kNm)		BTM MOMENTS (kNm)	
		M ix	M iy	M ix	M iy
B1	1890	95.0	95.0	0.0	0.0
B2	1188	60.0	60.0	0.0	0.0
Loadcase 3	1188		60.0	0.0	0.0
Loadcase 4	1890		95.0	0.0	0.0
Loadcase 5				0.0	0.0
Loadcase 6				0.0	0.0

BAR ARRANGEMENTS

Bar Ø	Asc %	Link Ø	BAR CENTRES (mm)		Nuz (kN)	Checks
			350 Face	350 Face		
H 40	8.21	10	110	110	0	Asc > 6 % (3.12.6.2)
H 32	5.25	8	116	116	4612	ok
H 25	3.21	8	120	120	3561	ok
H 20	2.05	6	124	124	2969	ok
H 16	1.31	6	126	126	2589	ok
H 12	0.74	6	128	128	2294	ok

DESIGN MOMENTS (kN)

	X AXIS			Y AXIS		COMBINED		REBAR	max V ⁺
	K	M add	Mx	M add	My	Axis	M'		
B1	0.000	0.0	95.0	0.0	95.0	X	141.1	8 H25	86.4
B2	0.000	0.0	60.0	0.0	60.0	X	100.6	8 H12	53.3
Loadcase 3	0.000	0.0	0.0	0.0	60.0	Y	60.0	8 H12	53.6
Loadcase 4	0.000	0.0	0.0	0.0	95.0	Y	95.0	8 H20	74.6
Loadcase 5									#DIV/0!
Loadcase 6									#DIV/0!

SEE CHARTS ON NEXT SHEET

eccentricity = 50mm applied to both axis

Project 69 Redington Rd

Client SHAKIB

Location LONDON

SYMMETRICALLY REINFORCED RECTANGULAR COLUMN DESIGN,
BENT ABOUT TWO AXES TO BS 8110:2005

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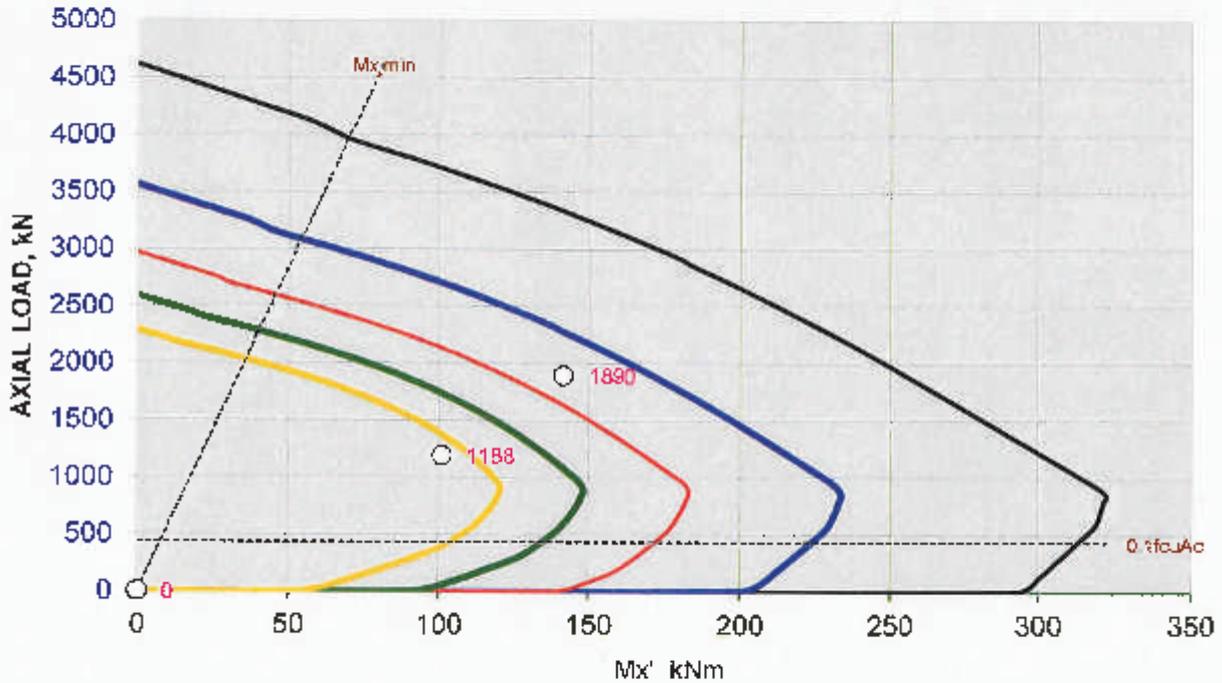
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MJ

Revision
-

Job No
GA19787

N:M interaction chart: M_x' critical

350 x 350 column (h x b), grade C35, 35 mm cover



N:M interaction chart: M_y' critical

350 x 350 column (h x b), moment about yy axis), Grade C35, 35 Cover

