

LAND TO THE REAR OF 159-163 KINGS CROSS ROAD, LONDON

PLANNING COMPLIANCE REVIEW

Report 14682.PCR.Rev.A

For:

Mr Clemente Cappello

BALCAP RE LTD

4 Bourlet Close

London

W1W 7BJ

Site Address	Report Date	Revision History
Land to the rear of 159-163 Kings Cross Road, London	12/09/2016	1/10/2016

CONTENTS

1.0	INTRODUCTION	3
2.0	ENVIRONMENTAL NOISE SURVEY AND EQUIPMENT	3
2.1	Procedure	3
2.2	Equipment	3
3.0	RESULTS	4
4.0	NOISE CRITERIA	4
5.0	DISCUSSION	5
5.1	Objective overview	5
5.2	Proposed Mitigation Measures for Plant Units Installations	5
5.3	BS8233 Assessment	6
6.0	CONCLUSION	7

List of Attachments

14682.SP1.Rev.A	Site Location Plan
14682.TH1	Environmental Noise Time History
Appendix A	Glossary of Acoustic Terminology
Appendix B	Acoustic Calculations
Appendix C	Anti-Vibration Mounting Specification Reference Document

1.0 INTRODUCTION

KP Acoustics Ltd, Britannia House, 11 Glenthorne Road, London, W6 0LH, has been commissioned by Balcap Re Ltd, 4 Bourlet Close, London, W1W 7BJ, to undertake an environmental noise survey at Land to the rear of 159-163 Kings Cross Road, London.

The background noise levels measured will be used to determine daytime and night-time noise emission criteria for a proposed installation of plant units, in agreement with the planning requirements of The London Borough of Camden.

This report presents the overall methodology and results from the environmental survey followed by calculations to demonstrate the feasibility of the plant installation to satisfy the emissions criterion at the closest noise-sensitive receivers and outline mitigation measures as appropriate.

2.0 ENVIRONMENTAL NOISE SURVEY AND EQUIPMENT

2.1 Procedure

Automated noise monitoring was undertaken at the position shown in Site Plan 14682.SP1.Rev.A. The choice of this position was based both on accessibility and on collecting representative noise data in relation to the nearest noise sensitive receiver relative to the proposed plant installation. Continuous automated monitoring was undertaken for the duration of the survey between 17th of August and 18th of August 2016.

Initial inspection of the site revealed that the background noise profile at the monitoring location was wholly dominated by road traffic noise from the surrounding roads.

The weather during the course of the survey was generally dry with wind speeds within acceptable tolerances and therefore suitable for the measurement of environmental noise. The measurement procedure complied with ISO 1996-2:2007 Acoustics *"Description, measurement and assessment of environmental noise - Part 2: Determination of environmental noise levels"*.

2.2 Equipment

The equipment calibration was verified before and after use and no abnormalities were observed.

The equipment used was as follows.

- 1 No. Svantek Type 958 Class 1 Sound Level Meter
- B&K Type 4231 Class 1 Calibrator

3.0 RESULTS

The results from the continuous noise monitoring are shown as a time history of L_{Aeq} , L_{Amax} , L_{A10} and L_{A90} averaged over 5 minute sample periods in Figures 14682.TH1.

Minimum background noise levels are shown in Table 3.1.

	Minimum background noise level $L_{A90: 5min}$ dB(A)
Daytime (07:00-23:00)	48
Night-time (23:00-07:00)	46

Table 3.1: Minimum measured background noise levels

4.0 NOISE CRITERIA

In order to ensure that the amenity of the nearest noise sensitive receiver is preserved, this report will aim to demonstrate inaudibility at the nearest noise sensitive receiver. In order to achieve inaudibility, noise received as a result of the newly installed plant unit should not exceed a level 10dB below the measured minimum background L_{A90} .

We therefore propose to set the noise criterion as shown in Table 4.1 in order to comply with the above requirement.

	Daytime (07:00 to 23:00)	Night-time (23:00 to 07:00)
Noise criterion at nearest residential receiver (10dB below minimum L_{A90})	38dB(A)	36dB(A)

Table 4.1: Proposed Noise Emissions Criterion

As the proposed air conditioning units will only be used during office hours, we would recommend the adoption of the day-time criterion in order to ensure that the amenity of the closest receivers will be protected.

5.0 DISCUSSION

It is understood that the plant installation is comprised of the following units:

- 3 No. PURY-P350 YLM-A1 Air Conditioning Units

2 No. plant units are proposed to be installed on the 2nd level of the property (Location 1 as shown in 14682.SP1.Rev A). 1 No. plant unit is proposed to be installed on the 2nd level of the property (Location 2 as shown in 14682.SP1.Rev.A).

The closest noise sensitive receiver to this location will be a window located approximately 9 metres from the proposed installation Location 1, and 7 metres from proposed installation Location 2.

The sound pressure levels at 1m as provided by the manufacturer for the unit is shown in Table 5.1.

Unit	Sound Power Level (dB) in each Frequency Band							
	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz
PURY-P350 YLM-A1	74	69	65	62	56	48	43	38

Table 5.1 Manufacturer's Sound Pressure Levels at 1m

5.1 Objective overview

Taking all acoustic corrections into consideration, including distance corrections, the noise level expected at the closest residential window would be as shown in Table 5.2. Detailed calculations are shown in Appendix B.

Receiver - Nearest Noise Sensitive Window	Criterion	Noise Level at closest Receiver
Receiver 1 As shown in 14682.SP1.Rev.A	38dB(A)	36 dB(A)

Table 5.2 Predicted noise level and criterion at nearest noise sensitive receivers

As shown in Appendix B and Table 5.2, transmission of noise to the nearest sensitive windows due to the effects of the plant unit installations fully satisfies the emissions criteria set based on the requirements of The London Borough of Camden, providing that the mitigation measure as outlined in Section 5.2 are implemented.

5.2 Proposed Mitigation Measures for Plant Units Installations

In order to reduce noise emissions from the proposed plant units to within the criteria specified in Section 4.0, we would recommend the installation of acoustic enclosures, which should provide the minimum attenuation characteristics as shown in Table 5.3.

Unit	Attenuation Levels (dB) in each Frequency Band (at 1m)							
	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz
Location 1 Acoustic enclosure	-9	-10	-14	-18	-23	-26	-25	-24
Location 2 Acoustic enclosure	-5	-7	-10	-12	-14	-16	-13	-12

Table 5.3 Required attenuation levels of the acoustic enclosure to be installed on location 1

The aforementioned acoustic enclosures can be provided by companies such as EEC, Noico or any similar acoustic solutions supplier.

5.3 BS8233 Assessment

Furthermore, the predicted noise level of 36 dB(A) at the nearest noise sensitive receiver is to be considered outside of the window. The windows may be closed or partially closed leading to further attenuation, as follows. Further calculations have been undertaken to assess whether the noise emissions from the plant units installation would be expected to meet the recognised British Standard recommendations, in order to further ensure the amenity of nearby noise sensitive receivers.

British Standard 8233:2014 '*Sound insulation and noise reduction for buildings – Code of Practice*' gives recommendations for acceptable internal noise levels in residential properties. Assuming worst case conditions, of the closest window being for a bedroom, BS8233:2014 recommends 30dB(A) as being the value for internal resting/sleeping conditions in night-time.

With a calculated external levels at nearest noise sensitive receiver of 36dB(A), the residential windows itself would need to provide minimal attenuation in order for the conditions to be achieved. According to BS8233:2014, even a partially open window offers 10-15dB attenuation, thus leading to a further reduced interior noise level.

Receiver	Design Range – For resting/sleeping conditions in a bedroom, in BS8233:2014	Noise Level within Nearest Residential Space
Closest to proposed plant unit installations	30 dB(A)	26 dB(A)

Table 5.4 Noise levels and criteria inside nearest residential spaces.

Predicted levels are shown in Table 5.4, with detailed calculations shown in Appendix B. It can therefore be stated that, as well as complying with the requirements of The London Borough of Camden, the noise emissions from the plant unit installations would be expected to comfortably meet the most stringent recommendations of the relevant British Standard.

6.0 CONCLUSION

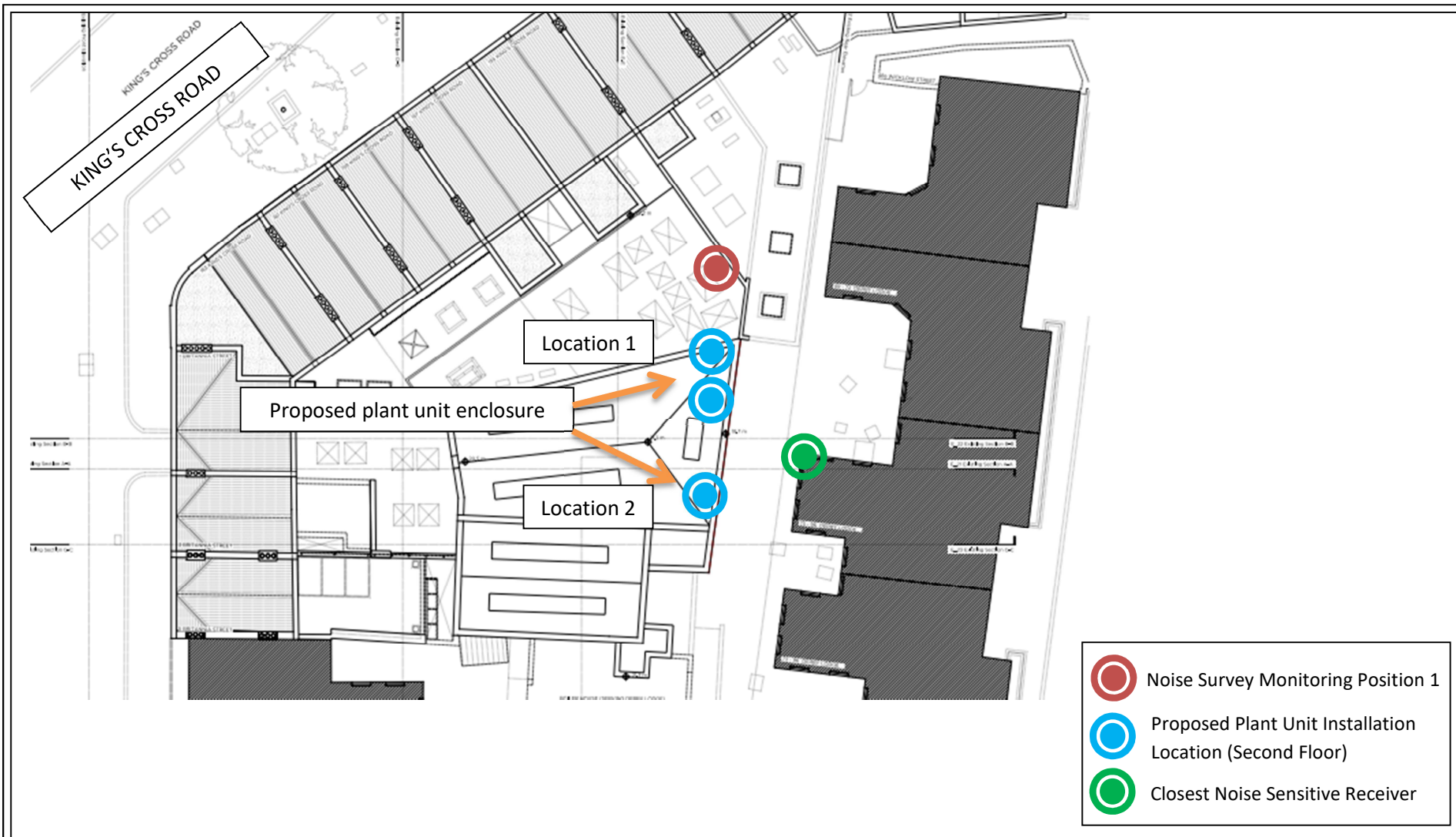
An environmental noise survey has been undertaken at Land to the rear of 159-163 Kings Cross Road, London, by KP Acoustics Ltd between 17th August and 18th August 2016. The results of the survey have enabled criteria to be set for noise emissions from proposed plant units.

Using manufacturer noise data, noise levels are predicted at the nearby noise sensitive receivers for compliance with current requirements.

Calculations show that noise emissions from the proposed air conditioning unit installations would meet the requirements of The London Borough of Camden, providing that the mitigation measures outlined in Section 5.2 are implemented.

Report by:
George Hadjilambri BSc (Hons)
KP Acoustics Ltd.

Checked by:
Kyriakos Papanagiotou MIOA
KP Acoustics Ltd.



Title: Indicative site plan showing noise monitoring position,
proposed plant unit location and closest noise sensitive receiver
Ref: google.earth

Date: 1 November 2016

FIGURE 14682.SP1.Rev.A



Land to the rear of 159-163 Kings Cross Road, London
Environmental Noise Time History
17th of August to 18th of August 2016

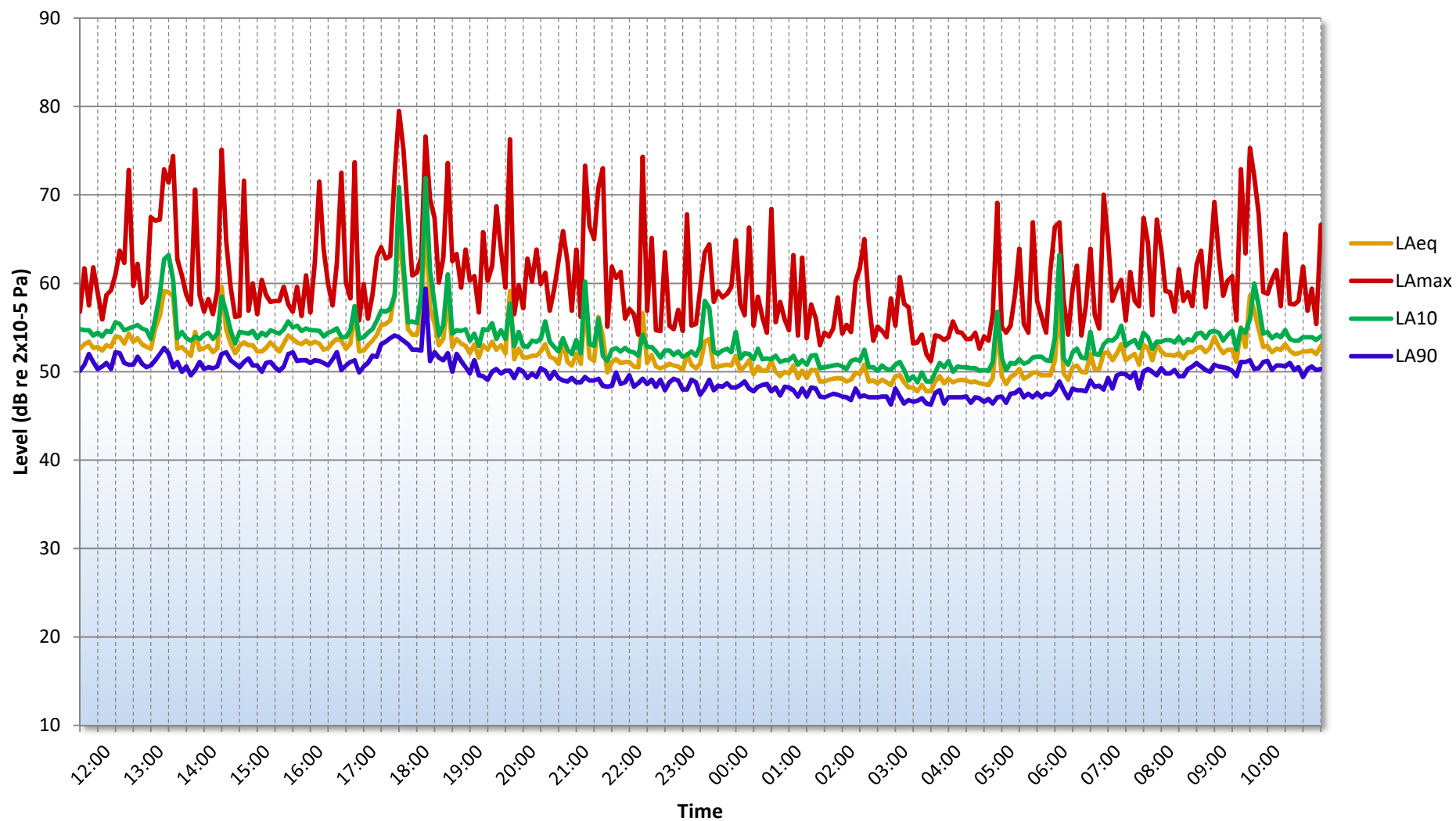


Figure 14682.TH1

GENERAL ACOUSTIC TERMINOLOGY

Decibel scale - dB

In practice, when sound intensity or sound pressure is measured, a logarithmic scale is used in which the unit is the 'decibel', dB. This is derived from the human auditory system, where the dynamic range of human hearing is so large, in the order of 10^{13} units, that only a logarithmic scale is the sensible solution for displaying such a range.

Decibel scale, 'A' weighted - dB(A)

The human ear is less sensitive at frequency extremes, below 125Hz and above 16Khz. A sound level meter models the ears variable sensitivity to sound at different frequencies. This is achieved by building a filter into the Sound Level Meter with a similar frequency response to that of the ear, an A-weighted filter where the unit is dB(A).

L_{eq}

The sound from noise sources often fluctuates widely during a given period of time. An average value can be measured, the equivalent sound pressure level L_{eq} . The L_{eq} is the equivalent sound level which would deliver the same sound energy as the actual fluctuating sound measured in the same time period.

L_{10}

This is the level exceeded for no more than 10% of the time. This parameter is often used as a "not to exceed" criterion for noise.

L_{90}

This is the level exceeded for no more than 90% of the time. This parameter is often used as a descriptor of "background noise" for environmental impact studies.

L_{max}

This is the maximum sound pressure level that has been measured over a period.

Octave Bands

In order to completely determine the composition of a sound it is necessary to determine the sound level at each frequency individually. Usually, values are stated in octave bands. The audible frequency region is divided into 11 such octave bands whose centre frequencies are defined in accordance with international standards. These centre frequencies are: 16, 31.5, 63, 125, 250, 500, 1000, 2000, 4000, 8000 and 16000 Hertz.

Environmental noise terms are defined in BS7445, *Description and Measurement of Environmental Noise*.

APPLIED ACOUSTIC TERMINOLOGY

Addition of noise from several sources

Noise from different sound sources combines to produce a sound level higher than that from any individual source. Two equally intense sound sources operating together produce a sound level which is 3dB higher than a single source and 4 sources produce a 6dB higher sound level.

Attenuation by distance

Sound which propagates from a point source in free air attenuates by 6dB for each doubling of distance from the noise source. Sound energy from line sources (e.g. stream of cars) drops off by 3dB for each doubling of distance.

Subjective impression of noise

Hearing perception is highly individualised. Sensitivity to noise also depends on frequency content, time of occurrence, duration of sound and psychological factors such as emotion and expectations. The following table is a guide to explain increases or decreases in sound levels for many scenarios.

Change in sound level (dB)	Change in perceived loudness
1	Imperceptible
3	Just barely perceptible
6	Clearly noticeable
10	About twice as loud

Transmission path(s)

The transmission path is the path the sound takes from the source to the receiver. Where multiple paths exist in parallel, the reduction in each path should be calculated and summed at the receiving point. Outdoor barriers can block transmission paths, for example traffic noise. The effectiveness of barriers is dependent on factors such as its distance from the noise source and the receiver, its height and construction.

Ground-borne vibration

In addition to airborne noise levels caused by transportation, construction, and industrial sources there is also the generation of ground-borne vibration to consider. This can lead to structure-borne noise, perceptible vibration, or in rare cases, building damage.

Sound insulation - Absorption within porous materials

Upon encountering a porous material, sound energy is absorbed. Porous materials which are intended to absorb sound are known as absorbents, and usually absorb 50 to 90% of the energy and are frequency dependent. Some are designed to absorb low frequencies, some for high frequencies and more exotic designs being able to absorb very wide ranges of frequencies. The energy is converted into both mechanical movement and heat within the material; both the stiffness and mass of panels affect the sound insulation performance.

APPENDIX B

Land to the rear of 159-163 Kings Cross Road, London

PLANT UNIT EMISSIONS CALCULATIONS - SECOND FLOOR

Source: Plant Unit Installation at Second Floor Level Receiver 1: Nearest Residential Window opposite the plant installation	Frequency, Hz								dB(A)
	63	125	250	500	1k	2k	4k	8k	
Manufacturer's sound pressure level at 1m									
Mitsubishi PURY-P350 YLM-A1 Unit	74	69	65	62	56	48	43	38	
Correction for number of units (2)	3	3	3	3	3	3	3	3	
Attenuation provided by distance, dB (9m)	-19	-19	-19	-19	-19	-19	-19	-19	
Minimum attenuation provided by acoustic enclosure with acoustic louvres (600mm), dB	-9	-10	-14	-18	-23	-26	-25	-24	
Sound Pressure Level 1m from receiver	49	43	35	28	17	6	2	0	
Mitsubishi PURY-P350 YLM-A1 Unit	74	69	65	62	56	48	43	38	
Attenuation provided by distance, dB (7m)	-17	-17	-17	-17	-17	-17	-17	-17	
Minimum attenuation provided by acoustic enclosure with acoustic louvres (300mm), dB	-5	-7	-10	-12	-14	-16	-13	-12	
Sound Pressure Level 1m from receiver	52	45	38	33	25	15	13	9	
Sound pressure level 1m from nearest receiver	53	47	39	34	25	16	13	9	36
Design Criterion									38

Source: Plant Unit Installation at Second Floor Level Receiver: Inside Nearest Residential Space	Frequency, Hz								dB(A)
	63	125	250	500	1k	2k	4k	8k	
Sound pressure level outside window	52	44	37	29	18	8	2	0	36
Minimum attenuation from partially open window, dB	-10	-10	-10	-10	-10	-10	-10	-10	-10
Sound pressure level inside nearest residential window	42	34	27	19	8	0	0	0	26

ANTI-VIBRATION MOUNTING SPECIFICATION REFERENCE DOCUMENT

1.0 General

- 1.1 All mountings shall provide the static deflection, under the equipment weight, shown in the schedules. Mounting selection should allow for any eccentric load distribution or torque reaction, so that the design deflection is achieved on all mountings under the equipment, under operating conditions.
- 1.2 It is the supplier's responsibility to ensure that all mountings offered are suitable for the loads, operating and environmental conditions which will prevail. Particular attention should be paid to mountings which will be exposed to atmospheric conditions to prevent corrosion.
- 1.3 All mountings shall be colour coded, or otherwise marked, to indicate their load capacity, to facilitate identification during installation.

Where use of resilient supports allows omission of pipe flexible connections for vibration/noise isolation, it shall be the Mechanical Service Consultant's or Contractor's responsibility to decide whether such devices are required to compensate for misalignment or thermal strain.

2.1 Type A Mounting (Caged Spring Type)

- 2.1.1 Each mounting shall consist of cast or fabricated telescopic top and bottom housings enclosing one or more helical steel springs as the principle isolation elements, and shall incorporate a built-in levelling device. The housing should be designed to permit visual inspection of the springs after installation, i.e. the spring must not be totally enclosed.
- 2.1.2 The springs shall have an outside diameter of not less than 75% of the operating height, and be selected to have at least 50% overload capacity before becoming coil-bound.
- 2.1.3 The bottom plate of each mounting shall have bonded to it a rubber/neoprene pad designed to attenuate any high frequency energy transmitted by the springs.
- 2.1.4 Mountings incorporating snubbers or restraining devices shall be designed so that the snubbing, damping or restraining mechanism is capable of being adjusted to have no significant effect during the normal running of the isolated machine.
- 2.1.5 All nuts, bolts or other elements used for adjustment of a mounting shall incorporate locking mechanisms to prevent the isolator going out of adjustment as a result of vibration or accidental or unauthorised tampering.

2.2 Type B Mounting (Open Spring Type)

- 2.2.1 Each mounting shall consist of one or more helical steel springs as the principal isolation elements, and shall incorporate a built-in levelling device.
- 2.2.2 The springs shall be fixed or otherwise securely located to cast or fabricated top and bottom plates, shall have an outside diameter of not less than 75% of the operating height, and shall be selected to have at least 50% overload capacity before becoming coil-bound.
- 2.2.3 The bottom plate shall have bonded to it a rubber/ neoprene pad designed to attenuate any high frequency energy transmitted by the springs.

2.3 Type C Mounting (Rubber/Neoprene Type)

Each mounting shall consist of a steel top plate and base plate completely embedded in oil resistant rubber/neoprene. Each mounting shall be capable of being fitted with a levelling device, and should have bolt holes in the base plate and a threaded metal insert in the top plate so that they can be bolted to the floor and equipment where required.

3.0 Plant Bases

3.1 Type A Bases (A.V. Rails)

An A.V. Rail shall comprise a steel beam with two or more height-saving brackets. The steel sections must be sufficiently rigid to prevent undue strain in the equipment and if necessary should be checked by the Structural Engineer.

3.2 Type B Bases (Steel Plant Bases)

Steel plant bases shall comprise an all-welded steel framework of sufficient rigidity to provide adequate support for the equipment, and fitted with isolator height saving brackets. The frame depth shall be approximately 1/10 of the longest dimension of the equipment with a minimum of 150 mm. This form of base may be used as a composite A.V. rail system.

3.3 Type C Bases (Concrete Inertia Base: for use with steel springs)

These shall consist of an all-welded steel pouring frame-work with height saving brackets, and a frame depth of approximately 1/12 of the longest dimension of the equipment, with a minimum of 100 mm. The bottom of the pouring frame should be blanked off, and concrete (2300 kg/m³) poured in over steel reinforcing rods positioned 35 mm above the bottom. The inertia base should be sufficiently large to provide support for all parts of the equipment, including any components which over-hang the equipment base, such as suction and discharge elbows on centrifugal pumps.