

User Details:

Assessor Name:James McglashanStroma Number:STRO000976Software Name:Stroma FSAP 2009Software Version:Version: 1.5.0.95

| Software Name:  | Stroma FSAP 2009   | Software \                  | Version:  | Versio                                       | n: 1.5.0.95  |          |
|---|--|-----------------------------|---|--|--------------|----------|
|   |  | roperty Address: 22 A       |   |  |              |          |
| Address :   | Flat 22, Anello Building, 116                                    | Bayham Street, LON          | IDON, NW1 0B                                      | 4  |              |          |
| 1. Overall dwelling dime                              | nsions:  | A ( 2)                      | According to the                                  | (m)  | Malassa (sa) | o)       |
| Ground floor  |  | Area(m²)                    | Ave Height  | <u>`                                    </u> | Volume(m     | <u>-</u> |
|   |  | 191.89 (1a)                 | x 2.476   | (2a) =                                       | 475.12       | (3a)     |
| Total floor area TFA = (1a                            | a)+(1b)+(1c)+(1d)+(1e)+(1n                                       | ) 191.89 (4)                |   |  |              |          |
| Dwelling volume                                       |  | (3a)+                       | +(3b)+(3c)+(3d)+(3e                               | )+(3n) =                                     | 475.12       | (5)      |
| 2. Ventilation rate:                                  |  |                             |   |  |              |          |
|   | main Secondar<br>heating heating                                 | y other                     | total   |  | m³ per hou   | ır       |
| Number of chimneys                                    | 0 + 0  | + 0 =                       | 0   | x 40 =                                       | 0            | (6a)     |
| Number of open flues                                  | 0 + 0  | + 0 =                       | 0   | x 20 =                                       | 0            | (6b)     |
| Number of intermittent far                            | ns   |                             | 0   | x 10 =                                       | 0            | (7a)     |
| Number of passive vents                               |  |                             | 0   | x 10 =                                       | 0            | (7b)     |
| Number of flueless gas fir                            | es   |                             | 0   | x 40 =                                       | 0            | (7c)     |
|   |  |                             |   |  |              |          |
|   |  |                             |   | Air ch                                       | anges per h  | our      |
| Infiltration due to chimney                           | vs, flues and fans = $(6a)+(6b)+(7a)$                            | a)+(7b)+(7c) =              | 0   | ÷ (5) =                                      | 0            | (8)      |
|   | een carried out or is intended, proceed                          | to (17), otherwise continu  | ue from (9) to (16)                               |  |              | _        |
| Number of storeys in th                               | e dwelling (ns)  |                             |   |  | 0            | (9)      |
| Additional infiltration                               |  |                             |   | [(9)-1]x0.1 =                                | 0            | (10)     |
|   | 25 for steel or timber frame or                                  | •                           |   |  | 0            | (11)     |
| if both types of wall are producting areas of opening | esent, use the value corresponding to<br>as): if equal user 0.35 | the greater wall area (afte | er  |  |              |          |
| =   | oor, enter 0.2 (unsealed) or 0.                                  | 1 (sealed), else enter      | r 0   |  | 0            | (12)     |
| If no draught lobby, ent                              | er 0.05, else enter 0  |                             |   |  | 0            | (13)     |
| Percentage of windows                                 | and doors draught stripped                                       |                             |   |  | 0            | (14)     |
| Window infiltration                                   |  | 0.25 - [0.2 x (14)          | ) ÷ 100] =  |  | 0            | (15)     |
| Infiltration rate                                     |  | (8) + (10) + (11)           | + (12) + (13) + (15)                              | =  | 0            | (16)     |
| Air permeability value,                               | q50, expressed in cubic metre                                    | s per hour per square       | e metre of envel                                  | ope area                                     | 9.83         | (17)     |
| If based on air permeabili                            | ty value, then $(18) = [(17) \div 20] + (8)$                     | s), otherwise (18) = (16)   |   |  | 0.49         | (18)     |
| Air permeability value applies                        | s if a pressurisation test has been don                          | e or a degree air permeab   | ility is being used                               | '  |              |          |
| Number of sides on which                              | n sheltered  |                             |   |  | 2            | (19)     |
| Shelter factor  |  | (20) = 1 - [0.075           | x (19)] =   |  | 0.85         | (20)     |
| Infiltration rate incorporati                         | ng shelter factor  | $(21) = (18) \times (20)$   | )) =  |  | 0.42         | (21)     |
| Infiltration rate modified for                        | or monthly wind speed  |                             | <del>, , , , , , , , , , , , , , , , , , , </del> |  |              |          |

|   | Jan  | Feb  | Mar  | Apr  | May  | Jun  | Jul  | Aug  | Sep  | Oct  | Nov | Dec  |
|---|------|------|------|------|------|------|------|------|------|------|-----|------|
| Monthly average wind speed from Table 7 |      |      |      |      |      |      |      |      |      |      |     |      |
| (22)m=                                  | 5.4  | 5.1  | 5.1  | 4.5  | 4.1  | 3.9  | 3.7  | 3.7  | 4.2  | 4.5  | 4.8 | 5.1  |
| Wind Factor (22a)m = (22)m ÷ 4          |      |      |      |      |      |      |      |      |      |      |     |      |
| (22a)m=                                 | 1.35 | 1.27 | 1.27 | 1.12 | 1.02 | 0.98 | 0.92 | 0.92 | 1.05 | 1.12 | 1.2 | 1.27 |



| Adjusted infilt                        | ration rate                | e (allowi    | ng for sh   | nelter an   | d wind s     | speed) =         | (21a) x      | (22a)m      |                      |             |           |          |          |
|--|----------------------------|--------------|-------------|-------------|--------------|------------------|--------------|-------------|----------------------|-------------|-----------|----------|----------|
| 0.56                                   | 0.53                       | 0.53         | 0.47        | 0.43        | 0.41         | 0.39             | 0.39         | 0.44        | 0.47                 | 0.5         | 0.53      |          |          |
| Calculate effe                         |                            | _            | rate for t  | he appli    | cable ca     | se               | !            | !           | !                    | !           |           |          |          |
| If mechanic                            |                            |              | l' N. (0    | al.) (aa    | <b>.</b> - ( | /                |              | . (00)      | \ (00 \              |             |           | 0.5      | (238     |
| If exhaust air                         |                            |              |             |             |              |                  |              |             | ) = (23a)            |             |           | 0.5      | (23h     |
| If balanced wi                         |                            | •            | •           | J           |              | •                |              | ,           |                      |             |           | 73.1     | (230     |
| a) If balanc                           | 1 -                        | 1            |             |             | 1            | <del> </del>     |              | <u> </u>    |                      | <del></del> | · ·       | ÷ 100]   | ,        |
| (24a)m= 0.7                            | 0.67                       | 0.67         | 0.6         | 0.56        | 0.54         | 0.52             | 0.52         | 0.57        | 0.6                  | 0.64        | 0.67      |          | (24a     |
| b) If balanc                           | ed mecha                   | anical ve    | entilation  | without     | heat red     | overy (N         | ЛV) (24b     | m = (22)    | 2b)m + (2            | 23b)        |           | İ        |          |
| (24b)m= 0                              | 0                          | 0            | 0           | 0           | 0            | 0                | 0            | 0           | 0                    | 0           | 0         |          | (24)     |
| c) If whole if (22b)                   | house ext $m < 0.5 \times$ |              |             | •           | •            |                  |              |             | 5 × (23h             | ))          |           |          |          |
| (24c)m= 0                              | 0                          | 0            | 0           | 0           | 0            | 0                | 0            | 0           | 0                    | 0           | 0         |          | (240     |
| d) If natura                           | l ventilatio               | on or wh     | ole hous    | e nositiv   | /e innut     | L<br>ventilatio  | n from l     | oft.        |                      |             |           |          |          |
| ,                                      | m = 1, the                 |              |             |             | •            |                  |              |             | 0.5]                 |             |           |          |          |
| (24d)m= 0                              | 0                          | 0            | 0           | 0           | 0            | 0                | 0            | 0           | 0                    | 0           | 0         |          | (240     |
| Effective ai                           | r change                   | rate - er    | ter (24a    | or (24b     | o) or (24    | c) or (24        | d) in box    | x (25)      |                      |             |           | •        |          |
| (25)m= 0.7                             | 0.67                       | 0.67         | 0.6         | 0.56        | 0.54         | 0.52             | 0.52         | 0.57        | 0.6                  | 0.64        | 0.67      |          | (25)     |
| 2 Hoot local                           | oc and he                  | ot loce r    | oromote     | or:         |              |                  |              |             |                      |             |           |          |          |
| 3. Heat loss                           | es and ne<br>Gros          | •            |             |             | Net Ar       | 00               | U-valı       |             | AXU                  |             | k-value   |          | A X k    |
| ELEMENT                                | area                       | -            | Openin<br>m |             | A,r          |                  | W/m2         |             | (W/I                 | K)          | kJ/m²·l   |          | kJ/K     |
| Windows Typ                            | e 1                        |              |             |             | 30.97        | x1.              | /[1/( 1.6 )+ | 0.04] =     | 46.57                |             |           |          | (27)     |
| Windows Typ                            | e 2                        |              |             |             | 18.5         | x1.              | /[1/( 1.6 )+ | 0.04] =     | 27.82                | =           |           |          | (27)     |
| Windows Typ                            | e 3                        |              |             |             | 2.23         | x <sub>1</sub> , | /[1/( 1.6 )+ | 0.04] =     | 3.35                 |             |           |          | (27)     |
| Windows Typ                            | e 4                        |              |             |             | 63.46        |                  | /[1/( 1.6 )+ | 0.04] =     | 95.43                | =           |           |          | (27)     |
| Vindows Typ                            | e 5                        |              |             |             | 2.23         | = ,              | /[1/( 1.6 )+ | l.          | 3.35                 | =           |           |          | (27)     |
| Rooflights                             |                            |              |             |             | 1.44         | _                | /[1/(1.6) +  | l.          | 2.304                | ╡           |           |          | (27)     |
| Walls                                  | 454                        | 40           | 447.0       |             |              | =                | /            |             |                      | ╡ ,         |           | <b>–</b> |          |
|  | 151.                       |              | 117.3       |             | 33.77        | _                | 0.29         | =           | 9.79                 | 믁 ¦         |           |          | (29)     |
| Roof                                   | 191.8                      |              | 4.32        |             | 187.5        | =                | 0.14         | = [         | 26.26                |             |           |          | (30)     |
| Total area of                          | elements                   | , <b>m</b> ² |             |             | 343.0        | 5                |              |             |                      |             |           |          | (31)     |
| Party wall                             |                            |              |             |             | 27.51        |                  | 0.2          | = [         | 5.5                  |             |           |          | (32)     |
| * for windows an<br>** include the are |                            |              |             |             |              | ated using       | formula 1    | /[(1/U-valu | ıe)+0.04] a          | as given in | paragraph | 3.2      |          |
| abric heat lo                          |                            |              |             | s and pan   | uuons        |                  | (26)(30)     | ) + (32) =  |                      |             |           | 224.58   | (33      |
| Heat capacity                          | •                          | `            | 0)          |             |              |                  | , , , ,      |             | (30) + (32           | 2) + (32a)  | (32e) =   | 2711.110 | <b>=</b> |
| Thermal mas                            | ,                          | ,            | P = Cm =    | - TFΔ) ir   | n k.l/m²K    |                  |              | ., ,        | tive Value:          | , , ,       | (020)     |          | =        |
| For design asses                       | •                          | `            |             | ,           |              |                  | ecisely the  |             |                      |             | able 1f   | 100      | (35      |
| can be used inst                       |                            |              |             |             |              | ,                |              |             |                      |             |           |          |          |
| Thermal bridg                          | ,                          | •            |             |             | •            | <b>\</b>         |              |             |                      |             |           | 51.46    | (36      |
| if details of thern                    | nal bridging               | are not kn   | own (36) -  | = 0 15 x (3 | 11)          |                  |              |             |                      |             |           |          |          |
| Total fabric h                         |                            |              | own (00) -  | - 0.70 % (0 | ,            |                  |              | (33) +      | (36) =               |             |           | 276.04   | (37)     |
|  | eat loss                   |              |             |             | ,            |                  |              |             | (36) =<br>= 0.33 × ( | 25)m x (5)  |           | 276.04   | (37)     |



| (38)m= 109.52                              | 104.6                  | 104.6                 | 94.78        | 88.23             | 84.95       | 81.68             | 81.68               | 89.87       | 94.78                  | 99.69                  | 104.6   |         | (38)         |
|--|------------------------|-----------------------|--------------|-------------------|-------------|-------------------|---------------------|-------------|------------------------|------------------------|---------|---------|--------------|
| Heat transfer                              | coefficie              | nt, W/K               |              |                   |             |                   |                     | (39)m       | = (37) + (3            | 38)m                   |         |         |              |
| (39)m= 385.55                              | 380.64                 | 380.64                | 370.81       | 364.26            | 360.99      | 357.71            | 357.71              | 365.9       | 370.81                 | 375.73                 | 380.64  |         | _            |
| Heat loss para                             | ameter (I              | HLP), W               | /m²K         |                   |             |                   |                     |             | Average =<br>= (39)m ÷ |                        | 12 /12= | 370.95  | (39)         |
| (40)m= 2.01                                | 1.98                   | 1.98                  | 1.93         | 1.9               | 1.88        | 1.86              | 1.86                | 1.91        | 1.93                   | 1.96                   | 1.98    |         |              |
| Number of da                               | vs in mo               | nth (Tab              | le 1a)       |                   |             |                   | •                   | ,           | Average =              | Sum(40) <sub>1</sub>   | 12 /12= | 1.93    | (40)         |
| Jan  | Feb                    | Mar                   | Apr          | May               | Jun         | Jul               | Aug                 | Sep         | Oct                    | Nov                    | Dec     |         |              |
| (41)m= 31                                  | 28                     | 31                    | 30           | 31                | 30          | 31                | 31                  | 30          | 31                     | 30                     | 31      |         | (41)         |
| · · · <u>L</u>                             | ı                      |                       |              | I.                |             | I.                |                     | I.          |                        | I.                     |         |         |              |
| 4. Water hea                               | ting ene               | rgy requ              | irement:     |                   |             |                   |                     |             |                        |                        | kWh/ye  | ar:     |              |
| Assumed occ                                |                        |                       |              |                   |             |                   |                     |             |                        |                        | .99     |         | (42)         |
| if TFA > 13.<br>if TFA £ 13.               |                        | + 1.76 x              | [1 - exp     | (-0.0003          | 849 x (TF   | FA -13.9          | )2)] + 0.0          | 0013 x (    | TFA -13.               | .9)                    |         |         |              |
| Annual average                             | •                      | ater usad             | ge in litre  | es per da         | ay Vd,av    | erage =           | (25 x N)            | + 36        |                        | 10:                    | 5.24    |         | (43)         |
| Reduce the annu                            | al average             | hot water             | usage by     | 5% if the $c$     | lwelling is | designed          |                     |             | se target o            |                        | 0.2.    |         | ` '          |
| not more that 125                          | · ·                    | person pei<br>T       |              | rater use, i<br>T | not and co  | <u> </u>          | ·                   | 1           | ·                      | 1                      |         |         |              |
| Jan Hot water usage                        | Feb                    | Mar<br>Mar day for ea | Apr          | May               | Jun         | Jul<br>Table 1c v | Aug                 | Sep         | Oct                    | Nov                    | Dec     |         |              |
|  | <del></del>            |                       | 103.14       | · ·               | 94.72       | 94.72             | · <i>'</i>          | 102.14      | 107.35                 | 111 56                 | 115.77  |         |              |
| (44)m= 115.77                              | 111.56                 | 107.35                | 103.14       | 98.93             | 94.72       | 94.72             | 98.93               | 103.14      | Total = Su             | 111.56<br>m(44)        | L       | 1262.94 | (44)         |
| Energy content of                          | f hot water            | used - cal            | culated me   | onthly $= 4$ .    | 190 x Vd,r  | n x nm x E        | OTm / 3600          |             |                        | . ,                    |         | 1202.54 | (\.,         |
| (45)m= 172.09                              | 150.51                 | 155.32                | 135.41       | 129.93            | 112.12      | 103.89            | 119.22              | 120.64      | 140.6                  | 153.47                 | 166.66  |         |              |
|  |                        |                       |              |                   |             |                   |                     |             | Total = Su             | m(45) <sub>112</sub> = | =       | 1659.87 | (45)         |
| If instantaneous v                         | vater heati            | ng at point           | t of use (no | hot water         | storage),   | enter 0 in        | boxes (46           | ) to (61)   | 1                      |                        |         |         |              |
| (46)m= 25.81<br>Water storage              | 22.58                  | 23.3                  | 20.31        | 19.49             | 16.82       | 15.58             | 17.88               | 18.1        | 21.09                  | 23.02                  | 25      |         | (46)         |
| a) If manufact                             |                        | clared lo             | oss facto    | r is knov         | vn (kWh     | /day):            |                     |             |                        | 1.                     | .67     |         | (47)         |
| Temperature f                              |                        |                       |              |                   | `           | • •               |                     |             |                        |                        | .54     |         | (48)         |
| Energy lost from                           | om water               | storage               | , kWh/ye     | ear               |             |                   | (47) x (48)         | ) =         |                        |                        | 9018    |         | (49)         |
| If manufacture                             |                        | •                     |              |                   |             |                   |                     |             |                        |                        |         |         |              |
| Cylinder volun                             | •                      | •                     | •            |                   | •           |                   | •                   |             |                        |                        | 0       |         | (50)         |
| If community h<br>Otherwise if no          | _                      |                       | _            |                   |             |                   | enter 'O' in        | hov (50)    |                        |                        |         |         |              |
|  |                        |                       |              |                   |             |                   | enter o m           | DOX (30)    |                        |                        |         |         | (=4)         |
| Hot water stor                             | J                      |                       | om rabi      | ie z (KVV         | n/iitre/ua  | iy)               |                     |             |                        |                        | 0       |         | (51)         |
| Volume factor<br>Temperature f             |                        |                       | 2b           |                   |             |                   |                     |             |                        |                        | 0       |         | (52)<br>(53) |
| . omporataro                               | actor no               |                       |              | -ar               |             |                   | ((50) x (51         | I) x (52) x | (53) =                 |                        |         |         | . ,          |
| Energy lost fro                            | m watei                | · storage             | KWWW         |                   |             |                   | ((00) / (01)        | , , , (02)  | (30) –                 |                        | 0       |         | (54)         |
| Energy lost fro<br>Enter (49) or (         |                        | _                     | e, Kvvii/ye  |                   |             |                   |                     |             |                        | 0                      | .9 l    |         | (55)         |
| ••   | (54) in (5             | 5)                    | ·            |                   |             |                   | ((56)m = (          | (55) × (41) | m                      | 0                      | 0.9     |         | (55)         |
| Enter (49) or (                            | (54) in (5             | 5)                    | ·            |                   | 27.05       | 27.96             | ((56)m = (<br>27.96 | 55) × (41)  | m<br>27.96             | 27.05                  | 27.96   |         | (55)<br>(56) |
| Enter (49) or (                            | (54) in (5<br>loss cal | 5)<br>culated t       | for each     | month 27.96       | <u> </u>    | 27.96             | 27.96               | 27.05       | 27.96                  | 27.05                  | 27.96   | x H     |              |
| Enter (49) or ( Water storage (56)m= 27.96 | (54) in (5<br>loss cal | 5)<br>culated t       | for each     | month 27.96       | <u> </u>    | 27.96             | 27.96               | 27.05       | 27.96                  | 27.05                  | 27.96   | хН      |              |



| Primary circuit loss (annual) from Table 3   | 360                       | (58)          |
|--|---------------------------|---------------|
| Primary circuit loss calculated for each month (59)m = $(58) \div 365 \times (41)$ m   |                           | -             |
| (modified by factor from Table H5 if there is solar water heating and a cylinder thermo  | <del></del>               | 1             |
| (59)m= 30.58 27.62 30.58 29.59 30.58 29.59 30.58 29.59 30.58   | 29.59 30.58               | (59)          |
| Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m  |                           | _             |
| (61)m= 0 0 0 0 0 0 0 0 0 0   | 0 0                       | (61)          |
| Total heat required for water heating calculated for each month (62)m = $0.85 \times (45)$ m +   | (46)m + (57)m +           | (59)m + (61)m |
| (62)m= 230.62 203.38 213.85 192.05 188.46 168.76 162.43 177.75 177.29 199.13   | 210.12 225.19             | (62)          |
| Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution  | ion to water heating)     | 1             |
| (add additional lines if FGHRS and/or WWHRS applies, see Appendix G)   |                           | _             |
| (63)m= 0 0 0 0 0 0 0 0 0   | 0 0                       | (63)          |
| Output from water heater   | _                         | _             |
| (64)m= 230.62 203.38 213.85 192.05 188.46 168.76 162.43 177.75 177.29 199.13   | 210.12 225.19             |               |
| Output from water heater   | r (annual) <sub>112</sub> | 2349.03 (64)  |
| Heat gains from water heating, kWh/month 0.25 x $[0.85 \times (45)\text{m} + (61)\text{m}] + 0.8 \times [(46)\text{m}]$  | + (57)m + (59)n           | <u>n</u> ]    |
| (65)m= 104.05 92.34 98.47 90.34 90.03 82.59 81.37 86.47 85.43 93.57  | 96.34 102.24              | (65)          |
| include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is fr   | om community I            | neating       |
| 5. Internal gains (see Table 5 and 5a):  |                           |               |
| Metabolic gains (Table 5), Watts   |                           |               |
| Jan Feb Mar Apr May Jun Jul Aug Sep Oct  | Nov Dec                   | ]             |
| (66)m= 149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57   | 149.57 149.57             | (66)          |
| Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5  |                           | •             |
| (67)m= 32.39 28.76 23.39 17.71 13.24 11.18 12.08 15.7 21.07 26.75  | 31.22 33.29               | (67)          |
| Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5  | •                         | 1             |
| (68)m= 363.27 367.04 357.54 337.32 311.79 287.8 271.77 268 277.5 297.72  | 323.25 347.24             | (68)          |
| Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5   |                           | •             |
| (69)m= 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96   | 37.96 37.96               | (69)          |
| Pumps and fans gains (Table 5a)  | !                         | ,             |
| (70)m= 10 10 10 10 10 10 10 10 10 10   | 10 10                     | (70)          |
| Losses e.g. evaporation (negative values) (Table 5)  | l l                       | 1             |
| (71)m= -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65   | -119.65 -119.65           | (71)          |
| Water heating gains (Table 5)  |                           | 1             |
| (72)m= 139.85 137.41 132.35 125.47 121 114.71 109.37 116.22 118.65 125.77  | 133.81 137.42             | (72)          |
| Total internal gains = $(66)m + (67)m + (68)m + (69)m + (70)m  | <u> </u>                  | ]             |
| (73)m= 613.37 611.09 591.15 558.37 523.9 491.56 471.08 477.79 495.09 528.12  | 566.16 595.82             | (73)          |
| 6. Solar gains:  | 000.10                    | ( )           |
| Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicab  | le orientation.           |               |
| Orientation: Access Factor Area Flux g_  | FF                        | Gains         |
| <b>∪</b>   | able 6c                   | (W)           |
| Northeast 0.9x 0.77 x 30.97 x 11.51 x 0.63 x   | 0.8                       | 124.5 (75)    |
| Northeast 0.9x   | 0.8 =                     | 74.37 (75)    |
|  |                           |               |



| N. a                      |      | ,          |       | 1 |        | 1 1 |      | 1 |     | 1        |         | _    |
|---------------------------|------|------------|-------|---|--------|-----|------|---|-----|----------|---------|------|
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | X | 23.55  | X   | 0.63 | X | 0.8 | =        | 254.79  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | X | 23.55  | X   | 0.63 | X | 0.8 | =        | 152.2   | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | X | 41.13  | X   | 0.63 | X | 0.8 | =        | 444.87  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | X | 41.13  | X   | 0.63 | X | 0.8 | =        | 265.74  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | X | 67.8   | X   | 0.63 | X | 0.8 | =        | 733.37  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | X | 67.8   | X   | 0.63 | X | 0.8 | =        | 438.08  | (75) |
| Northeast 0.9x            | 0.77 | X          | 30.97 | X | 89.77  | X   | 0.63 | X | 0.8 | =        | 970.99  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | X | 89.77  | X   | 0.63 | X | 0.8 | =        | 580.03  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | X | 97.5   | X   | 0.63 | X | 0.8 | =        | 1054.67 | (75) |
| Northeast 0.9x            | 0.77 | X          | 18.5  | x | 97.5   | X   | 0.63 | X | 0.8 | =        | 630.01  | (75) |
| Northeast 0.9x            | 0.77 | X          | 30.97 | x | 92.98  | x   | 0.63 | x | 0.8 | =        | 1005.75 | (75) |
| Northeast 0.9x            | 0.77 | X          | 18.5  | x | 92.98  | X   | 0.63 | x | 0.8 | =        | 600.79  | (75) |
| Northeast 0.9x            | 0.77 | X          | 30.97 | x | 75.42  | x   | 0.63 | x | 0.8 | =        | 815.79  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | x | 75.42  | X   | 0.63 | x | 0.8 | =        | 487.31  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | x | 51.24  | X   | 0.63 | x | 0.8 | =        | 554.31  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | x | 51.24  | x   | 0.63 | x | 0.8 | ] =      | 331.12  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | x | 29.6   | x   | 0.63 | x | 0.8 | ] =      | 320.17  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | x | 29.6   | x   | 0.63 | x | 0.8 | ] =      | 191.25  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | x          | 30.97 | x | 14.52  | x   | 0.63 | x | 0.8 | =        | 157.12  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | × | 14.52  | x   | 0.63 | x | 0.8 | ] =      | 93.85   | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 30.97 | x | 9.36   | x   | 0.63 | x | 0.8 | j =      | 101.25  | (75) |
| Northeast <sub>0.9x</sub> | 0.77 | X          | 18.5  | x | 9.36   | x   | 0.63 | x | 0.8 | j =      | 60.48   | (75) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 37.39  | X   | 0.63 | x | 0.8 | =        | 29.12   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 63.74  | x   | 0.63 | x | 0.8 | j =      | 49.64   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 84.22  | x   | 0.63 | x | 0.8 | j =      | 65.59   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 103.49 | X   | 0.63 | x | 0.8 | =        | 80.61   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 113.34 | x   | 0.63 | x | 0.8 | j =      | 88.28   | (77) |
| Southeast 0.9x            | 0.77 | x          | 2.23  | x | 115.04 | x   | 0.63 | x | 0.8 | j =      | 89.61   | (77) |
| Southeast 0.9x            | 0.77 | x          | 2.23  | x | 112.79 | x   | 0.63 | x | 0.8 | j =      | 87.85   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 105.34 | x   | 0.63 | x | 0.8 | j =      | 82.05   | (77) |
| Southeast 0.9x            | 0.77 | j×         | 2.23  | x | 92.9   | x   | 0.63 | x | 0.8 | j =      | 72.36   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 72.36  | x   | 0.63 | x | 0.8 | j =      | 56.36   | (77) |
| Southeast 0.9x            | 0.77 | X          | 2.23  | x | 44.83  | x   | 0.63 | x | 0.8 | j =      | 34.91   | (77) |
| Southeast 0.9x            | 0.77 | j×         | 2.23  | x | 31.95  | x   | 0.63 | x | 0.8 | j =      | 24.88   | (77) |
| Southwest <sub>0.9x</sub> | 0.77 | X          | 63.46 | x | 37.39  |     | 0.63 | x | 0.8 | j =      | 828.69  | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | X          | 63.46 | x | 63.74  | j   | 0.63 | x | 0.8 | =        | 1412.68 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | X          | 63.46 | x | 84.22  | j   | 0.63 | x | 0.8 | =        | 1866.63 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | X          | 63.46 | x | 103.49 | j   | 0.63 | X | 0.8 | =        | 2293.81 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | )<br> <br> | 63.46 | X | 113.34 | i   | 0.63 | x | 0.8 | ,<br>  = | 2512.08 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | X          | 63.46 | X | 115.04 | i   | 0.63 | x | 0.8 | ,<br>  = | 2549.93 | (79) |
| Southwest <sub>0.9x</sub> | 0.77 | X          | 63.46 | X | 112.79 |     | 0.63 | x | 0.8 | ,<br>] = | 2499.99 | (79) |
| L                         | ·    | 1          |       | 1 |        |     |      | ı |     | ,        |         | _ ′  |



| Southwesto 92  |
|--|
| Southwesto, 9x   |
| Southwesto, 9x   |
| Southwesto, 9s, 0.77 x 0.63.46 x 31.95 y 0.63 x 0.8 = 709.16 (79) Northwesto, 9s, 0.77 x 2.23 x 11.51 x 0.63 x 0.8 = 8.96 (81) Northwesto, 9s, 0.77 x 2.23 x 23.65 x 0.63 x 0.8 = 18.35 (81) Northwesto, 9s, 0.77 x 2.23 x 41.13 x 0.63 x 0.8 = 18.35 (81) Northwesto, 9s, 0.77 x 2.23 x 867.8 x 0.63 x 0.8 = 20.03 (81) Northwesto, 9s, 0.77 x 2.23 x 89.77 x 0.63 x 0.8 = 50.20 (81) Northwesto, 9s, 0.77 x 2.23 x 89.77 x 0.63 x 0.8 = 50.20 (81) Northwesto, 9s, 0.77 x 2.23 x 97.5 x 0.63 x 0.8 = 75.94 (81) Northwesto, 9s, 0.77 x 2.23 x 97.5 x 0.63 x 0.8 = 75.94 (81) Northwesto, 9s, 0.77 x 2.23 x 97.5 x 0.63 x 0.8 = 75.94 (81) Northwesto, 9s, 0.77 x 2.23 x 97.5 x 0.63 x 0.8 = 70.85 (81) Northwesto, 9s, 0.77 x 2.23 x 1.85 (91) Northwesto, 9s, 0.77 x 2.23 x 1.85 (91) Northwesto, 9s, 0.77 x 2.23 x 2.85 (91) North |
| Northwest 0.9x   |
| Northwest 0,9x   |
| Northwest 0.9x   |
| Northwest 0,9x   |
| Northwest 0.9x   |
| Northwest 0.9x   |
| Northwest 0.9x   |
| Northwest 0.9x   |
| Rooflights 0.9x  |
| Rooflights 0.9x  |
| Rooflights 0.9x  |
| Rooflights 0.9x  |
| Rooflights 0.9x  |
| Rooflights 0.9x  |
| Rooflights 0.9x  |
| Rooflights 0.9x 1  |
| Rooflights 0.9x 1  |
| Rooflights $0.9x$ 1  |
| Rooflights 0.9x 1  |
| Rooflights 0.9x 1  |
| Solar gains in watts, calculated for each month (83)m = Sum(74)m(82)m  (83)m= 1116.6 1993.47 2859.06 3892.6 4593.61 4794.02 4646.95 4100.11 3284.05 2327.99 1355.41 943.22 (83)  Total gains – internal and solar (84)m = (73)m + (83)m , watts  (84)m= 1729.97 2604.55 3450.21 4450.97 5117.51 5285.58 5118.03 4577.9 3779.14 2856.11 1921.57 1539.04 (84)  |
| (83)m= 1116.6 1993.47 2859.06 3892.6 4593.61 4794.02 4646.95 4100.11 3284.05 2327.99 1355.41 943.22 Total gains – internal and solar (84)m = (73)m + (83)m , watts  (84)m= 1729.97 2604.55 3450.21 4450.97 5117.51 5285.58 5118.03 4577.9 3779.14 2856.11 1921.57 1539.04 (84)   |
| (83)m= 1116.6 1993.47 2859.06 3892.6 4593.61 4794.02 4646.95 4100.11 3284.05 2327.99 1355.41 943.22 Total gains – internal and solar (84)m = (73)m + (83)m , watts  (84)m= 1729.97 2604.55 3450.21 4450.97 5117.51 5285.58 5118.03 4577.9 3779.14 2856.11 1921.57 1539.04 (84)   |
| Total gains – internal and solar (84)m = (73)m + (83)m , watts  (84)m= 1729.97 2604.55 3450.21 4450.97 5117.51 5285.58 5118.03 4577.9 3779.14 2856.11 1921.57 1539.04 (84)   |
| (84)m= 1729.97 2604.55 3450.21 4450.97 5117.51 5285.58 5118.03 4577.9 3779.14 2856.11 1921.57 1539.04 (84)   |
|  |
| 7. Mean internal temperature (heating season)  |
|  |
| Temperature during heating periods in the living area from Table 9, Th1 (°C)   |
| Utilisation factor for gains for living area, h1,m (see Table 9a)  |
| Jan Feb Mar Apr May Jun Jul Aug Sep Oct Nov Dec  |
| (86)m= 0.94 0.88 0.79 0.67 0.52 0.39 0.27 0.3 0.51 0.75 0.91 0.95 (86)   |
| Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)  |
|  |
| (87)m= 18.32 18.81 19.42 20 20.47 20.71 20.82 20.81 20.58 19.96 18.95 18.34 (87)   |
| (87)m= 18.32 18.81 19.42 20 20.47 20.71 20.82 20.81 20.58 19.96 18.95 18.34 (87)  Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)  (88)m= 19.33 19.35 19.35 19.39 19.41 19.42 19.43 19.43 19.4 19.39 19.37 19.35 (88)  |



| I Itilic  | ation fac   | tor for a  | aine for i  | rest of d   | walling   | h2 m (co  | o Tablo  | 02)  |  |                               |                                       |                              |          |                         |
|---|---|--|---|---|---|---|--|--|--|-------------------------------|---------------------------------------|------------------------------|----------|-------------------------|
| (89)m=  | 0.93  | 0.86   | 0.76  | 0.62  | 0.46  | 0.3   | 0.17   | 0.19   | 0.42                                   | 0.7                           | 0.89                                  | 0.94                         |          | (89)                    |
|   | internal  | temper   | ature in <sup>.</sup>   | the rest  | of dwelli   | na T2 (fa   | ollow ste  | ens 3 to 7   | in Tabl                                | e 9c)                         |                                       |                              |          |                         |
| (90)m=  | 15.95   | 16.64  | 17.47   | 18.25   | 18.84   | 19.12   | 19.22  | 19.21  | 18.99                                  | 18.24                         | 16.86                                 | 15.99                        |          | (90)                    |
|   |   |  |   |   |   |   |  |  | f                                      | LA = Livin                    | g area ÷ (4                           | l) =                         | 0.57     | (91)                    |
| Mean  | internal  | temner   | atura (fo   | or the wh   | ole dwel  | lling) – fl   | Δ <b>~</b> T1  | ⊥ (1 _ fl  | Δ) <b>~</b> T2                         |                               |                                       | l                            |          |                         |
| (92)m=  | 17.3  | 17.88  | 18.58   | 19.25   | 19.77   | 20.03   | 20.13  | 20.12  | 19.9                                   | 19.23                         | 18.05                                 | 17.33                        |          | (92)                    |
| Apply   | ســــــــــــــــــــــــــــــــــــ   | nent to th   | ne mean   | internal  | temper  | ature fro   | m Table  | 4e, whe  | re appro                               | priate                        |                                       |                              |          |                         |
| (93)m=  | 17.3  | 17.88  | 18.58   | 19.25   | 19.77   | 20.03   | 20.13  | 20.12  | 19.9                                   | 19.23                         | 18.05                                 | 17.33                        |          | (93)                    |
| 8. Sp   | ace hea   | ting requ  | uirement  |   |   |   |  |  |  |                               |                                       |                              |          |                         |
| Set T   | i to the r  | nean int   | ernal ter   | mperatur  | e obtain  | ed at ste   | ep 11 of   | Table 9b   | o, so tha                              | t Ti,m=(7                     | 76)m and                              | d re-calc                    | ulate    |                         |
| the u   | tilisation  | factor fo  | r gains i   | using Ta  | ble 9a  |   |  |  |  |                               |                                       |                              |          |                         |
|   | Jan   | Feb  | Mar   | Apr   | May   | Jun   | Jul  | Aug  | Sep                                    | Oct                           | Nov                                   | Dec                          |          |                         |
|   |   |  | ains, hm  | 1   |   | · ·   |  |  |  |                               |                                       |                              |          | ( <b>5</b> .1)          |
| (94)m=  | 0.91  | 0.84   | 0.74  | 0.62  | 0.47  | 0.34  | 0.22   | 0.24   | 0.45                                   | 0.69                          | 0.87                                  | 0.92                         |          | (94)                    |
|   | <u> </u>  |  |   | 4)m x (84   | _   | 4770.00   | 1100.10  | 4000.05  | 474400                                 | 407400                        | 4004.44                               | 4440.00                      |          | (OE)                    |
|   |   |  |   | 2752.35   |   |   | 1109.16  | 1096.95  | 1714.39                                | 1974.22                       | 1664.44                               | 1416.09                      |          | (95)                    |
|   | niy avera   | age exte   | rnai tem<br>6.8   | perature<br>8.7   | 11.7  |   | 16.0   | 16.9   | 112                                    | 10.8                          | 7                                     | 4.0                          |          | (96)                    |
| (96)m=  |   |  |   |   |   | 14.6  | 16.9   |  | 14.3                                   |                               | 1                                     | 4.9                          |          | (90)                    |
|   | 1   |  | 1   | al tempe<br>3910.7  |   | 1959.61   |  | 1153.09  |  |                               | <i>4</i> 151 75                       | <i>∆</i> 731 31              |          | (97)                    |
|   |   |  |   | r each m  |   |   |  |  |  |                               |                                       | 4701.01                      |          | (01)                    |
| -   | 2502.74   |  |   |   | 385.32  | 0   | 0.02   | 0  | 0                                      | 855.78                        | 1790.87                               | 2466.52                      |          |                         |
| ()  |   |  |   |   |   |   |  |  |  | (kWh/year                     |                                       |                              | 12099.53 | (98)                    |
| Snac  | o hoatin  | a roquire  | amont in  | kWh/m²  | lvoar   |   |  |  | 7 - 7                                  | <b>(</b>                      | , (-                                  | - /·····-,-····- [           |          | ╡                       |
|   |   | •  |   |   | уваг  |   |  |  |  |                               |                                       | L                            | 63.05    | (99)                    |
|   |   |  | uiremen   | it  |   |   |  |  |  |                               |                                       |                              |          |                         |
| Calcu   |   | <u>r June, J</u>   |   |   |   |   |  |  |  |                               |                                       |                              |          |                         |
| Haat  | Jan   | rah l  |   | August.   |   |   | led  | ۸۰۰۰   | Con                                    | Oct                           | Nov                                   | Doo                          |          |                         |
| Heat  | lace rate   | Feb  | Mar   | Apr   | May   | Jun   | Jul  | Aug  | Sep                                    | Oct                           | Nov                                   | Dec                          |          |                         |
| (100)m=   |   | Lm (ca   | Mar   |   | May<br>5°C inter                                    | Jun<br>nal temp                                       | erature  | and exte   | ernal ten                              | nperatur                      | e from T                              | able 10)                     |          | (100)                   |
| (100)m=   | 0   | Lm (ca   | Mar<br>Iculated   | Apr<br>using 25   | May   | Jun   | erature  |  |  |                               |                                       |                              |          | (100)                   |
|   | 0<br>ation fac  | Lm (ca   | Mar<br>Iculated   | Apr<br>using 25   | May<br>5°C inter                                    | Jun<br>nal temp                                       | erature  | and exte   | ernal ten                              | nperatur                      | e from T                              | able 10)                     |          | (100)                   |
| Utilisa<br>(101)m=  | etion fac   | e Lm (ca<br>0<br>tor for lo  | Mar<br>lculated<br>0<br>ess hm                                    | Apr<br>using 25<br>0  | May<br>5°C inter<br>0                               | Jun<br>nal temp<br>3104.5                             | perature<br>2217.82  | and exte   | ernal ten                              | nperatur<br>0                 | e from T                              | able 10)<br>0                |          |                         |
| Utilisa<br>(101)m=  | ation fac   | e Lm (ca<br>0<br>tor for lo  | Mar<br>lculated<br>0<br>ess hm                                    | Apr<br>using 25   | May<br>5°C inter<br>0                               | Jun<br>nal temp<br>3104.5                             | perature<br>2217.82  | 2217.82<br>0.9   | ernal ten                              | nperatur<br>0                 | e from T                              | able 10)<br>0                |          |                         |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=  | ation fac 0 al loss, h  | e Lm (ca<br>0<br>tor for lo<br>0<br>mLm (W   | Mar lculated 0 ss hm 0 /atts) = ( 0                               | Apr using 25 0  0 (100)m x  | May 5°C inter 0  0  (101)m 0                        | Jun nal temp 3104.5  0.87                             | 0.92<br>2029.33  | and exter<br>2217.82<br>0.9  | o<br>0<br>0                            | o<br>0                        | e from T<br>0                         | able 10)<br>0                |          | (101)                   |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=  | ation fac  o  l loss, h  o  s (solar c  | e Lm (ca<br>0<br>tor for lo<br>0<br>mLm (W   | Mar lculated 0 ss hm 0 /atts) = ( 0                               | Apr using 25 0  0 (100)m x  | May 5°C inter 0  0  (101)m 0                        | Jun nal temp 3104.5  0.87                             | 0.92<br>2029.33  | and exter<br>2217.82<br>0.9  | o<br>0<br>0                            | o<br>0                        | e from T<br>0                         | able 10)<br>0                |          | (101)                   |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Space   | ation fac   | e Lm (ca  0  tor for lo  0  mLm (W  0  gains cal  0  grequire                                | Mar lculated 0 ss hm 0 /atts) = ( 0 lculated 0 ement for          | Apr using 25 0  (100)m x 0 for appli 0 r month,   | May 5°C inter 0  0  (101)m 0  cable we 0  whole c   | Jun nal temp 3104.5  0.87  2690.7 eather re 6573.82   | 0.92<br>2029.33<br>egion, se                               | and extermination and extermin | 0<br>0<br>0<br>0<br>10)                | o<br>0<br>0                   | 0 0 0                                 | able 10) 0 0 0               | ς (41)m  | (101)                   |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Space<br>set (1                               | ation fac  ation fac  oul loss, h  os (solar g  cooling 04)m to   | e Lm (ca  0  tor for lo  0  mLm (W  0  gains cal  0  grequire                                | Mar lculated 0 ss hm 0 /atts) = ( 0 lculated 0 ement for          | Apr using 25 0  (100)m x 0 for appli  | May 5°C inter 0  0  (101)m 0  cable we 0  whole c   | Jun 3104.5  0.87  2690.7 eather re 6573.82            | 0.92<br>0.92<br>2029.33<br>egion, se<br>6280.5<br>continuo | and extermination and extermin | 0<br>0<br>0<br>10)<br>0<br>(h) = 0.0   | o<br>0<br>0                   | 0 0 0                                 | able 10) 0 0 0               | c (41)m  | (101)                   |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Space   | ation fac  ation fac  oul loss, h  os (solar g  cooling 04)m to   | e Lm (ca  0  tor for lo  0  mLm (W  0  gains cal  0  grequire                                | Mar lculated 0 ss hm 0 /atts) = ( 0 lculated 0 ement for          | Apr using 25 0  (100)m x 0 for appli 0 r month,   | May 5°C inter 0  0  (101)m 0  cable we 0  whole c   | Jun 3104.5  0.87  2690.7 eather re 6573.82            | 0.92<br>0.92<br>2029.33<br>egion, se<br>6280.5<br>continuo | and extermination and extermin | 0<br>0<br>0<br>10)<br>0<br>0/h) = 0.00 | 0<br>0<br>0<br>0<br>24 x [(10 | 0<br>0<br>0<br>0<br>03)m - (*         | able 10) 0 0 0               | c (41)m  | (101)<br>(102)<br>(103) |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Space<br>set (1<br>(104)m=                    | 0 ation fac ation fac 0 ul loss, h 0 s (solar g 0 e cooling 04)m to   | e Lm (ca<br>0<br>tor for lo<br>0<br>mLm (W<br>0<br>gains cal<br>0<br>g required<br>zero if ( | Mar lculated 0 ss hm 0 /atts) = ( culated 0 ement for 104)m <     | 0 (100)m x 0 for application of the contraction of | May 5°C inter 0  (101)m 0 cable we 0 whole come     | Jun 3104.5  0.87  2690.7 eather re 6573.82            | 0.92<br>0.92<br>2029.33<br>egion, se<br>6280.5<br>continuo | and extermination and extermin | 0 0 10) 0 7h) = 0.00                   | 0 0 0 24 x [(10 0 = Sum(      | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | able 10)  0  0  0  102)m ] > | 8719.64  | (101)<br>(102)<br>(103) |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Spac<br>set (1<br>(104)m=                     | ation faction | e Lm (ca  0  tor for lo  0  mLm (W  0  gains cal  0  g require zero if (                     | Mar lculated 0 ss hm 0 /atts) = ( 0 culated 0 ement for 104)m <   | Apr using 25 0  (100)m x 0 for appli 0 r month, 3 x (98)  | May 5°C inter 0  (101)m 0 cable we 0 whole come     | Jun 3104.5  0.87  2690.7 eather re 6573.82            | 0.92<br>0.92<br>2029.33<br>egion, se<br>6280.5<br>continuo | and extermination and extermin | 0 0 10) 0 7h) = 0.00                   | 0<br>0<br>0<br>0<br>24 x [(10 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | able 10)  0  0  0  102)m ] > |          | (101)<br>(102)<br>(103) |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Spac<br>set (1<br>(104)m=<br>Cooled<br>Interm | ation fac  ation fac  out loss, h  s (solar c  out  | e Lm (ca  0 tor for lo  0 mLm (W  0 gains cal  0 g require zero if (  0                      | Mar lculated 0 ss hm 0 /atts) = ( 0 culated 0 ement for 104)m < 0 | Apr using 25 0 (100)m x 0 for appli 0 r month, 3 x (98) 0   | May  5°C inter  0  (101)m  0  cable we  whole comes | Jun 2690.7 2690.7 eather re 6573.82 dwelling, 2795.84 | 0.92<br>0.92<br>2029.33<br>egion, se<br>6280.5<br>continuo | and exte<br>2217.82<br>0.9<br>1999.01<br>e Table<br>5709.93<br>ous ( kW<br>2760.93   | 0 0 10) 0 Total f C =                  | 0 0 0 24 x [(10 0 = Sum(      | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | able 10)  0  0  0  102)m ] > | 8719.64  | (101)<br>(102)<br>(103) |
| Utilisa<br>(101)m=<br>Usefu<br>(102)m=<br>Gains<br>(103)m=<br>Spac<br>set (1<br>(104)m=                     | ation fac  ation fac  out loss, h  s (solar c  out  | e Lm (ca  0  tor for lo  0  mLm (W  0  gains cal  0  g require zero if (                     | Mar lculated 0 ss hm 0 /atts) = ( 0 culated 0 ement for 104)m <   | Apr using 25 0  (100)m x 0 for appli 0 r month, 3 x (98)  | May 5°C inter 0  (101)m 0 cable we 0 whole come     | Jun 3104.5  0.87  2690.7 eather re 6573.82            | 0.92<br>0.92<br>2029.33<br>egion, se<br>6280.5<br>continuo | and extermination and extermin | 0 0 10) 0 Total f C =                  | 0 0 0 24 x [(10 0 = Sum(      | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | able 10)  0  0  0  102)m ] > | 8719.64  | (101)<br>(102)<br>(103) |



| Space cooling r                  | 0                 | 0          | 0         | 0        | 602.94   | 682.1     | 595.41      | 0                | 0                     | 0                       | 0       |                           |          |
|----------------------------------|-------------------|------------|-----------|----------|----------|-----------|-------------|------------------|-----------------------|-------------------------|---------|---------------------------|----------|
| , <u> </u>                       |                   |            |           |          | <u> </u> | <u> </u>  |             | Total            | l = Sum(              | 1 <u>0</u> 7)           | =       | 1880.45                   | (10      |
| Space cooling r                  | equirer           | nent in k  | :Wh/m²/y  | ear/     |          |           |             | (107)            | ) ÷ (4) =             |                         | F       | 9.8                       | (10      |
| a. Energy requ                   | uiremer           | nts – Indi | vidual h  | eating s | ystems i | ncluding  | micro-C     | HP)              |                       |                         |         |                           |          |
| Space heating                    | g:                |            |           |          | -        |           |             |                  |                       |                         | _       |                           |          |
| Fraction of spa                  | ace hea           | it from se | econdar   | //supple | mentary  | system    |             |                  |                       |                         |         | 0                         | (20      |
| Fraction of spa                  | ace hea           | it from m  | ain syst  | em(s)    |          |           | (202) = 1 - | - (201) <b>=</b> |                       |                         |         | 1                         | (20      |
| Fraction of total                | al heatii         | ng from i  | main sys  | stem 1   |          |           | (204) = (20 | 02) × [1 –       | (203)] =              |                         |         | 1                         | (20      |
| Efficiency of m                  | ain spa           | ace heati  | ing syste | em 1     |          |           |             |                  |                       |                         |         | 250                       | (20      |
| Efficiency of se                 | econda            | ry/supple  | ementar   | y heatin | g systen | າ, %      |             |                  |                       |                         |         | 0                         | (20      |
| Cooling Syster                   | m Ener            | gy Efficie | ency Rat  | io       |          |           |             |                  |                       |                         |         | 4.63                      | (20      |
| Jan                              | Feb               | Mar        | Apr       | May      | Jun      | Jul       | Aug         | Sep              | Oct                   | Nov                     | Dec     | kWh/ye                    | ear      |
| Space heating                    | require           | ement (c   | alculate  | d above  | )        |           |             |                  |                       |                         |         |                           |          |
| 2502.74                          | 1829.92           | 1434.38    | 834.01    | 385.32   | 0        | 0         | 0           | 0                | 855.78                | 1790.87                 | 2466.52 |                           |          |
| 211)m = {[(98)                   | m x (20           | 4)]} x 10  | 0 ÷ (206  | 5)       |          |           |             |                  |                       |                         |         |                           | (21      |
| 1001.09                          | 731.97            | 573.75     | 333.6     | 154.13   | 0        | 0         | 0           | 0                | 342.31                | 716.35                  | 986.61  |                           |          |
|                                  |                   |            |           |          |          |           | Tota        | I (kWh/yea       | ar) =Sum(2            | 211) <sub>15,1012</sub> | <u></u> | 4839.81                   | (21      |
| Space heating                    | fuel (se          | econdar    | y), kWh/  | month    |          |           |             |                  |                       |                         |         |                           |          |
| = {[(98)m x (201                 | l)] } x 1         | 100 ÷ (20  | 08)       |          |          | г         |             |                  | <b>I</b>              | <b>I</b>                | т 1     |                           |          |
| 215)m= 0                         | 0                 | 0          | 0         | 0        | 0        | 0         | 0           | 0                | 0                     | 0                       | 0       |                           | _        |
|                                  |                   |            |           |          |          |           | Tota        | I (kWh/yea       | ar) =Sum(2            | 215) <sub>15,1012</sub> | =       | 0                         | (21      |
| Water heating                    |                   | . , ,      |           | ,        |          |           |             |                  |                       |                         |         |                           |          |
| Output from wa                   | ter hea<br>203.38 | ter (calc  | ulated al | 188.46   | 168.76   | 162.43    | 177.75      | 177.29           | 199.13                | 210.12                  | 225.19  |                           |          |
| [230:02]<br>Efficiency of wa     |                   |            | 192.00    | 100.40   | 100.70   | 102.43    | 177.73      | 177.23           | 199.15                | 210.12                  | 223.19  | 175                       | (21      |
| 217)m= 175                       | 175               | 175        | 175       | 175      | 175      | 175       | 175         | 175              | 175                   | 175                     | 175     | 175                       | (21      |
| uel for water h                  |                   |            |           |          |          |           |             |                  |                       |                         |         |                           | `        |
| 219)m = (64)n                    |                   |            |           |          |          |           |             |                  |                       |                         |         |                           |          |
| 219)m= 131.79                    | 116.22            | 122.2      | 109.74    | 107.69   | 96.43    | 92.81     | 101.57      | 101.31           | 113.79                | 120.07                  | 128.68  |                           |          |
|                                  |                   |            |           |          |          |           | Tota        | I = Sum(2        | 19a) <sub>112</sub> = |                         |         | 1342.3                    | (21      |
| Space cooling                    |                   |            | nth.      |          |          |           |             |                  |                       |                         |         |                           |          |
| (221)m = (107)m = 0              | n÷ (∠US           | 0          | 0         | 0        | 130.21   | 147.31    | 128.59      | 0                | 0                     | 0                       | 0       |                           |          |
| 221/111-                         | 0                 | Ů          | U         | 0        | 100.21   | 147.51    |             | I = Sum(2:       |                       |                         |         | 406.1                     | (22      |
| Annual tatala                    |                   |            |           |          |          |           |             |                  | 00                    | Mbbaar                  |         |                           |          |
| Annual totals<br>Space heating t | uel use           | ed, main   | system    | 1        |          |           |             |                  | K                     | Wh/year                 | Г       | <b>kWh/yea</b><br>4839.81 | <u>r</u> |
| Vater heating f                  |                   |            | ,         |          |          |           |             |                  |                       |                         | L       | 1342.3                    | ╡        |
| _                                |                   |            |           |          |          |           |             |                  |                       |                         | L       |                           | $\dashv$ |
| Space cooling f                  |                   |            | _         |          |          |           |             |                  |                       |                         | L       | 406.1                     |          |
| Electricity for pu               | ımps, fa          | ans and    | electric  | keep-ho  | t        |           |             |                  |                       |                         |         |                           |          |
|                                  |                   |            |           | •        |          |           |             |                  |                       |                         |         |                           |          |
| mechanical ve                    | ntilatior         | n - balan  |           | ·        |          | nput fron | n outside   | e                |                       |                         | 739.05  |                           | (23      |



Total electricity for the above, kWh/year sum of (230a)...(230g) = 869.05 (231)

Electricity for lighting 571.94 (232)

Electricity generated by PVs -686.72 (233)

| 120  | CO2 omissions   | Individual heating systems | including miora CHD |
|------|-----------------|----------------------------|---------------------|
| ⊥∠a. | COZ emissions – | maividuai nealing systems  | including micro-ChP |

|   | <b>Energy</b><br>kWh/year       | Emission factor<br>kg CO2/kWh | <b>Emissions</b><br>kg CO2/year |
|---|---------------------------------|-------------------------------|---------------------------------|
| Space heating (main system 1)                     | (211) x                         | 0.517 =                       | 2502.18 (261)                   |
| Space heating (secondary)                         | (215) x                         | 0 =                           | 0 (263)                         |
| Water heating                                     | (219) x                         | 0.517                         | 693.97 (264)                    |
| Space and water heating                           | (261) + (262) + (263) + (264) = |                               | 3196.15 (265)                   |
| Space cooling                                     | (221) x                         | 0.517 =                       | 209.95 (266)                    |
| Electricity for pumps, fans and electric keep-hot | (231) x                         | 0.517                         | 449.3 (267)                     |
| Electricity for lighting                          | (232) x                         | 0.517 =                       | 295.7 (268)                     |
| Energy saving/generation technologies             |                                 |                               |                                 |
| Item 1  |                                 | 0.529                         | -363.27 (269)                   |
| Total CO2, kg/year                                | sum                             | of (265)(271) =               | 3787.83 (272)                   |
| Dwelling CO2 Emission Rate                        | (272                            | ?) ÷ (4) =                    | 19.74 (273)                     |
| El rating (section 14)                            |                                 |                               | 79 (274)                        |