

User Details

Assessor Name:James McglashanStroma Number:STRO000976Software Name:Stroma FSAP 2009Software Version:Version: 1.5.0.95

Software Name:	Stroma FSAP 2009	Software \	Version:	Versio	n: 1.5.0.95	
		roperty Address: 22 A				
Address :	Flat 22, Anello Building, 116	Bayham Street, LON	IDON, NW1 0BA	4		
1. Overall dwelling dime	ensions:			, ,		-
Cround floor		Area(m²)	Ave Height	<u>`                                    </u>	Volume(m	<u> </u>
Ground floor		191.89 (1a)	x 2.476	(2a) =	475.12	(3a)
Total floor area TFA = (1	a)+(1b)+(1c)+(1d)+(1e)+(1r	191.89 (4)				
Dwelling volume		(3a)+	+(3b)+(3c)+(3d)+(3e)	)+(3n) =	475.12	(5)
2. Ventilation rate:						
	main Secondar heating heating	y other	total		m³ per hou	ır
Number of chimneys		+ 0 =	0	x 40 =	0	(6a)
Number of open flues	0 + 0	+ 0 =	0	x 20 =	0	(6b)
Number of intermittent fa	ins		3	x 10 =	30	(7a)
Number of passive vents	3		0	x 10 =	0	(7b)
Number of flueless gas f	ires		0	x 40 =	0	(7c)
· ·					-	<b></b> ` ′
				Air ch	anges per h	our
Infiltration due to chimne	ys, flues and fans = $(6a)+(6b)+(7a)$	(a)+(7b)+(7c) =	30	÷ (5) =	0.06	(8)
If a pressurisation test has I	peen carried out or is intended, proceed	d to (17), otherwise continu	ue from (9) to (16)			_
Number of storeys in t	he dwelling (ns)				0	(9)
Additional infiltration				[(9)-1]x0.1 =	0	(10)
	.25 for steel or timber frame or	•			0	(11)
• • • • • • • • • • • • • • • • • • • •	resent, use the value corresponding to	the greater wall area (afte	er			
deducting areas of openi	floor, enter 0.2 (unsealed) or 0.	1 (sealed) else enter	r ()		0	(12)
If no draught lobby, er	,	. (554.54), 5.55 5.115			0	(12)
	s and doors draught stripped				0	(14)
Window infiltration	0 11	0.25 - [0.2 x (14)	) ÷ 100] =		0	(15)
Infiltration rate		(8) + (10) + (11)	+ (12) + (13) + (15)	=	0	(16)
Air permeability value,	q50, expressed in cubic metre	s per hour per square	e metre of envel	ope area	10	(17)
If based on air permeabi	lity value, then $(18) = [(17) \div 20] + (8)$	3), otherwise (18) = (16)			0.56	(18)
Air permeability value applie	es if a pressurisation test has been don	e or a degree air permeab	ility is being used			
Number of sides on which	h sheltered				2	(19)
Shelter factor		(20) = 1 - [0.075]	x (19)] =		0.85	(20)
Infiltration rate incorpora	ting shelter factor	$(21) = (18) \times (20)$	)) =		0.48	(21)
Infiltration rate modified	for monthly wind speed					
lon Fob	Mor Apr Moy lup	Jul Aug Sc	on Oot N	ov Doo		

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Monthly average wind speed from Table 7												
(22)m=	5.4	5.1	5.1	4.5	4.1	3.9	3.7	3.7	4.2	4.5	4.8	5.1
Wind F	actor (2	2a)m =	(22)m ÷	4								
(22a)m=	1.35	1.27	1.27	1.12	1.02	0.98	0.92	0.92	1.05	1.12	1.2	1.27



Calculate effe	0.61	0.61	0.54	0.49	0.47	0.44	0.44	0.5	0.54	0.57	0.61		
		•	rate for t	he appli	cable ca	se	ļ		ļ		!	<u> </u>	
If mechanica												0	(2
If exhaust air h		0 11		, ,	, ,	. `	,, .	`	) = (23a)			0	(2:
If balanced with	n heat reco	very: effic	iency in %	allowing f	or in-use f	actor (fron	n Table 4h	) =				0	(2:
a) If balance	1					<u> </u>	HR) (24a	m = (22)	2b)m + (	23b) × [	1 – (23c)	÷ 100]	
24a)m= 0	0	0	0	0	0	0	0	0	0	0	0		(2
b) If balance						_ ``	<del>É</del> È	<del>``</del>	2b)m + (2		1	1	
24b)m= 0	0	0	0	0	0	0	0	0	0	0	0		(2
c) If whole h				•					F (00)	,			
	n < 0.5 ×	(23b), t	nen (240 0	$\frac{(230)}{0}$	o); otner\	vise (24	C) = (220)	ŕ	$\frac{15 \times (230)}{0}$	<u> </u>		1	(2
								0	0	0	0		(2
d) If natural if (22b)n	ventilation			•	•				0.51				
24d)m= 0.71	0.69	0.69	0.64	0.62	0.61	0.6	0.6	0.63	0.64	0.66	0.69	]	(2
Effective air	change	rate - er	ıter (24a	or (24b	o) or (24	c) or (24	d) in box	(25)	!			ı	
25)m= 0.71	0.69	0.69	0.64	0.62	0.61	0.6	0.6	0.63	0.64	0.66	0.69	]	(2
3. Heat losse		•			NI a t A a		11 -1	_	A 3/11		1 -1	- ^	V I
LEMENT	Gros area		Openin m		Net Ar A ,r		U-valı W/m2		A X U (W/I	<b>〈</b> )	k-value kJ/m²-l		X k J/K
Doors		,			1.85	х	2	=	3.7	,			(2
Vindows					46.122	25 x	1/[1/( 2 )+	0.04] =	85.41	一			(2
Valls	151.	16	47.97	7	103.1	9 x	0.35	— լi	36.12	<b>=</b>			(2
Roof	191.8	89	0	=	191.8	9 x	0.16	<b>=</b>	30.7	Ħ i		7	(3
otal area of e					343.0	_							` (3
for windows and			ffective wi	ndow U-va		<del>_</del>	formula 1	/[(1/U-valu	ıe)+0.04] a	s given ir	n paragraph	n 3.2	(-
* include the area	as on both	sides of in	ternal wall	s and part	titions								
abric heat los	3s, W/K =	= S (A x	U)				(26)(30)	+ (32) =				155.93	(3
	Cm = S(	Axk)						((28).	(30) + (32	2) + (32a)	(32e) =	1727.01	(3
Heat capacity		ter /TN/F	$P = Cm \div$	TFA) ir	k I/m2K				tive Value	Medium		250	(3
, ,	parame	tor ( i ivir	• • • • • • • • • • • • • • • • • • • •	,	1 10/111 10			Indica	ilivo valuo		abla 1f		
Heat capacity Thermal mass For design assess	sments wh	ere the de	tails of the	,			ecisely the			TMP in T	able II		
Thermal mass For design assess an be used inste	sments whe	ere the de tailed calcu	tails of the ulation.	constructi	ion are no	known pr	ecisely the			TMP in T	able II	27.74	
Thermal mass For design assess an be used inste Thermal bridge	sments whead of a det es:S(L	ere the de tailed calcu x Y) calc	tails of the ulation. culated u	constructi	ion are not pendix l	known pr	recisely the			TMP in T	able II	37.74	(3
Thermal mass For design assess an be used inste	· sments who ead of a det es:S(L al bridging	ere the de tailed calcu x Y) calc	tails of the ulation. culated u	constructi	ion are not pendix l	known pr	recisely the	e indicative		TMP in T	аые п	37.74	(3
Thermal mass for design assess an be used inste Thermal bridge details of thermal	sments whe ead of a det es:S(L al bridging eat loss	ere the de tailed calcu x Y) calcu are not kn	tails of the ulation. culated u	constructiusing Ap	ion are not pendix l	known pr	recisely the	e indicative	e values of				
Thermal mass for design assess an be used inste Thermal bridge details of therma Total fabric he	sments whe ead of a det es:S(L al bridging eat loss	ere the de tailed calcu x Y) calcu are not kn	tails of the ulation. culated u	constructiusing Ap	ion are not pendix l	known pr	ecisely the	e indicative	e values of				
Thermal mass for design assess an be used inste Thermal bridge details of thermal fotal fabric he Ventilation hea	sments whead of a detection and	ere the de tailed calcu x Y) calcu are not kn	tails of the ulation. culated u own (36) =	constructions constructions constructions constructions constructed constructed constructions constructed	pendix I	t known pr		(33) + (38)m	(36) = = 0.33 × (	25)m x (5	)		
Thermal mass for design assess an be used inste Thermal bridge details of thermal fotal fabric here a details of thermal fotal fabric here a details of the details of the design and the design and the design and the design as	esments who add of a detection and of a detection a	ere the de tailed calculated are not kn alculated Mar	tails of the ulation. culated to own (36) = I monthly	constructions and constructions are constructed using Ap = 0.15 x (3)	pendix I  Jun	known pr	Aug	(33) + (38)m Sep 98.2	(36) = = 0.33 × (	25)m x (5 Nov 104.26	) Dec		(3
Thermal mass for design assess an be used inste Thermal bridge details of thermal fotal fabric he Ventilation hea	esments who add of a detection and of a detection a	ere the de tailed calculated are not kn alculated Mar	tails of the ulation. culated to own (36) = I monthly	constructions and constructions are constructed using Ap = 0.15 x (3)	pendix I  Jun	known pr	Aug	(33) + (38)m Sep 98.2	(36) = = 0.33 × ( Oct 101.13	25)m x (5 Nov 104.26	) Dec		(3
Thermal mass for design assess an be used insternal bridge details of thermal fotal fabric hermal dentilation head as many series of the details of the deta	sments whead of a detection and	ere the de tailed calculated Mar 107.59	tails of the ulation. culated to own (36) = I monthly Apr 101.13	constructions constructions constructions constructions constructed constructed constructions constructed constructions constructed constructions constructed constructed constructions constructed constructions constructed constructions constructed constructed constructions constructed co	pendix I  Jun  95.47	Jul 93.76	Aug 93.76	(33) + (38)m Sep 98.2 (39)m 291.86	e values of (36) = = 0.33 × ( Oct 101.13 = (37) + (3	25)m x (5 Nov 104.26 38)m 297.93	Dec 107.59		(3
Thermal mass for design assess an be used insternal bridge details of thermal fotal fabric hermal dentilation head as many series of the details of the deta	sments who ad of a detection and of a detection and bridging eat loss cat l	ere the de tailed calculated Mar 107.59 ant, W/K 301.26	tails of the ulation. culated to own (36) = monthly Apr 101.13	constructions constructions constructions constructions constructed constructed constructions constructed constructions constructed constructions constructed constructed constructions constructed constructions constructed constructions constructed constructed constructions constructed co	pendix I  Jun  95.47	Jul 93.76	Aug 93.76	(33) + (38)m Sep 98.2 (39)m 291.86	(36) = = 0.33 × ( Oct 101.13 = (37) + (32)	25)m x (5 Nov 104.26 38)m 297.93 Sum(39)	Dec 107.59	193.67	(3

Jan

### TER WorkSheet: New dwelling as built

Aug

Sep

Oct

Nov

Dec

Jul

May

Jun



Number of days in month (Table 1a) Feb

Mar

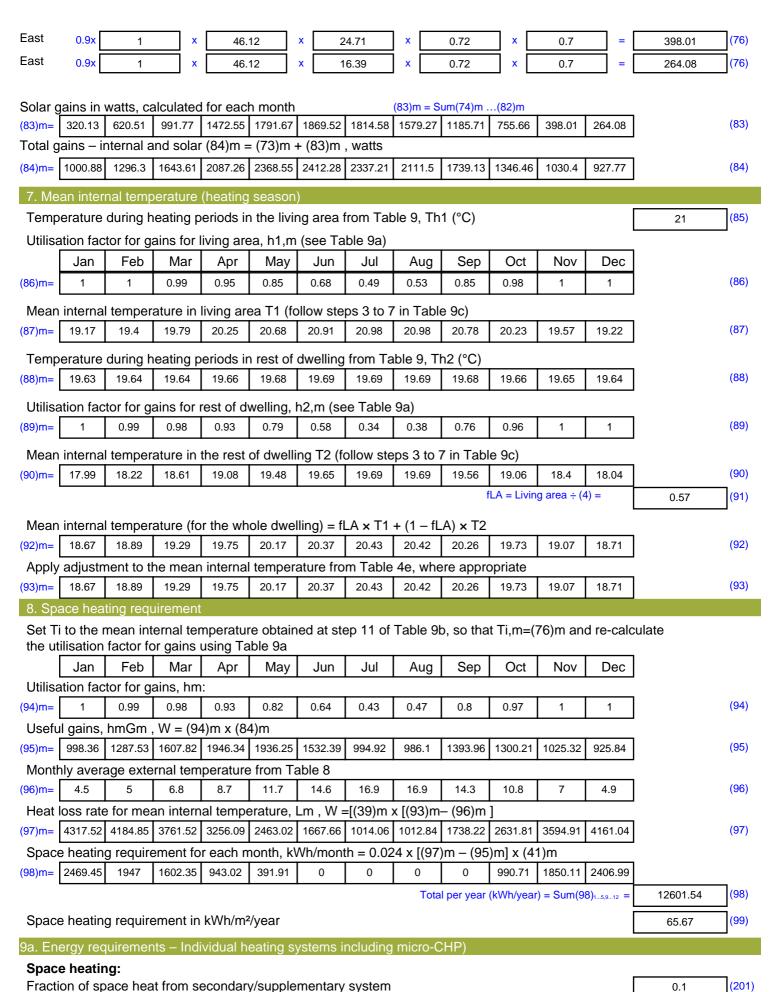
Apr

┕				17.	,			14.9					4	
1)m=	31	28	31	30	31	30	31	31	30	31	30	31	j	(41)
Wat	er heat	ing enei	rgy requi	irement:								kWh/ye	ear:	
oumo	ad again	nonov l	NI.										1	(40)
		pancy, l		:[1 - exp	(-0.0003	349 x (TF	-A -13.9	)2)] + 0.0	0013 x (	ΓFA -13.		99	İ	(42)
	£ 13.9			ι ολρ	( 0.0000	710 X (11	71 10.0	<i>)</i> _/] . o	3010 X (		.0)			
								(25 x N)				0.78		(43
		_				lwelling is hot and co	-	to achieve	a water us	se target o	f			
<i>о.</i> г			· ·					Ι	0	0.1	NI.	D	1	
water	Jan rusage ir	Feb	Mar day for ea	Apr	May	Jun ctor from 7	Jul Table 1c x	Aug	Sep	Oct	Nov	Dec	İ	
_									100.57		1 4 7 40	101.00	1	
m=	121.86	117.43	113	108.57	104.14	99.71	99.71	104.14	108.57	113	117.43	121.86	1000 11	٦٫٫٫
ergy co	ontent of	hot water	used - cal	culated mo	onthly = $4$ .	190 x Vd,r	n x nm x E	OTm / 3600			m(44) <sub>112</sub> = ables 1b, 1		1329.41	(44)
m= [	181.15	158.44	163.49	142.54	136.77	118.02	109.36	125.49	126.99	148	161.55	175.43	1	
)'''- L	101.10	100.44	100.40	142.04	100.77	110.02	100.00	123.43	<u> </u>	<u> </u>	m(45) <sub>112</sub> =	l	1747.23	(45
stanta	aneous w	ater heatii	ng at point	of use (no	hot water	r storage),	enter 0 in	boxes (46		rotar – ou	111(40)112 -		1747.20	٦,٠٠,
m=	27.17	23.77	24.52	21.38	20.52	17.7	16.4	18.82	19.05	22.2	24.23	26.32		(46
ter s	torage	loss:		l .		l			l		l	ļ	ı	
lf ma	nufactu	ırer's de	clared lo	oss facto	r is knov	vn (kWh	/day):					0		(47
mper	ature fa	actor fro	m Table	2b								0		(48
ergy	lost fro	m water	storage	, kWh/ye	ear			(47) x (48)	) =			0		(49
			•			s not kno							' 1	
		•	•	•		age with		!			1:	50	j	(50
	-	_		_		litres in bo		enter '0' in	hov (50)					
								cinci o in	DOX (00)				1	(5.4
		Ū		om rabi	e z (kvv	h/litre/da	ıy)					02	j 1	(51
		from Ta	bie 2a m Table	2h							-	93		(52
'								((50) (54	I) ( <b>50</b> )	(EO)		54	j 1	(53
•		m water 54) in (5	-	, kWh/ye	ear			((50) x (51	I) X (52) X	(53) =	-	44		(54
`	, ,	, ,	,	for each	month			((56)m = (	55) × (41)	m	1.	44	İ	(55
_								· · · · · ·			1	1	1	(50
m= L	44.53	40.22	44.53	43.09	44.53	43.09	44.53	44.53 0), else (5	43.09	44.53	43.09	44.53	liv L	(56
ıınder								· · ·			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	п Аррепа	1.X F1	
m=	44.53	40.22	44.53	43.09	44.53	43.09	44.53	44.53	43.09	44.53	43.09	44.53		(57
mary	circuit	loss (ar	nual) fro	om Table	3						6	10		(58
					,	•	. ,	65 × (41)						
	ified by	factor f	rom Tab	le H5 if t	here is s	solar wat	er heati	ng and a	cylinde	r thermo	stat)	1	1	
m=	51.81	46.79	51.81	50.14	51.81	50.14	51.81	51.81	50.14	51.81	50.14	51.81		(59
mbi l	oss cal	culated	for each	month (	(61)m =	(60) ÷ 36	65 × (41)	)m						
m=	0	0	0	0	0	0	0	0	0	0	0	0		(61
al he	eat requ	ired for	water h	eating ca	alculated	for eacl	h month	(62)m =	· 0.85 × (	(45)m +	(46)m +	(57)m +	(59)m + (61)m	
	277.49	245.45	259.83	235.76	233.1	211.25	205.7	221.83	220.22	244.33	254.78	271.77	[	(62
L	-		L				l		L	L		l	i	•



Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating) (add additional lines if FGHRS and/or WWHRS applies, see Appendix G) (63)(63)m =0 0 0 0 Output from water heater (64)m =277.49 245.45 259.83 235.76 233.1 211.25 205.7 221.83 220.22 244.33 254.78 271.77 (64)Output from water heater (annual) 1...12 2881.52 Heat gains from water heating, kWh/month  $0.25 \times [0.85 \times (45) \text{m} + (61) \text{m}] + 0.8 \times [(46) \text{m} + (57) \text{m} + (59) \text{m}]$ (65)(65)m =137.3 122.29 131.43 121.98 122.54 113.82 113.43 118.8 116.81 126.28 128.3 135.4 include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating 5. Internal gains (see Table 5 and 5a): Metabolic gains (Table 5), Watts May Jul Sep Oct Jan Feb Mar Apr Jun Aug Nov Dec (66)149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57 149.57 (66)m =149.57 equation L9 or L9a), also see Table 5 Lighting gains (calculated in Appendix L, 55.06 39.77 45.48 (67)(67)m =30.11 19 20.53 35.82 53.08 56.59 Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5 337.32 (68)(68)m =363.27 367.04 357.54 311.79 287.8 271.77 268 277.5 297.72 323.25 347.24 also see Table 5 Cooking gains (calculated in Appendix L, equation L15 or L15a), (69)(69)m =37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 37.96 Pumps and fans gains (Table 5a) (70)m =10 10 10 10 10 10 10 10 10 10 10 10 (70)Losses e.g. evaporation (negative values) (Table 5) -119.65 (71)(71)m =-119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 -119.65 Water heating gains (Table 5) (72)184.55 181.98 176.65 169.41 164.71 158.09 152.46 159.67 162.23 169.73 178.19 181.99 (72)m =(66)m + (67)m + (68)m +(69)m + (70)m + (71)m + (72)mTotal internal gains = 680.74 675.79 651.83 614.71 576.88 542.76 522.63 532.23 (73)(73)m =553.42 590.8 632.39 663.69 6. Solar gains Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation. FF Gains Orientation: Access Factor Area Flux Table 6d m<sup>2</sup> Table 6a Table 6b Table 6c (W) East 0.9x(76)1 46.12 19.87 0.72 x 0.7 320.13 East 0.9x (76)х x 1 46.12 38.52 0.72 0.7 620.51 East 0.9x1 Х 46.12 Х 61.57 Х 0.72 х 0.7 991.77 (76)East 0.9x46.12 91.41 х 0.72 0.7 1472.55 (76)East 0.9x1 46.12 111.22 0.72 0.7 1791.67 (76)East 0.9x(76)46.12 116.05 0.72 0.7 1869.52 East 0.9x46.12 112.64 0.72 0.7 1814.58 (76)East 0.9x(76)1 46.12 98.03 0.72 0.7 1579.27 East 0.9x1 46.12 73.6 0.72 0.7 1185.71 (76)East 0.9x(76)46.12 46.91 0.72 0.7 755.66







Fraction of space heat from main system(s)			(202) = 1 -	- (201) =				0.9	(202)
Fraction of total heating from main system 1			(204) = (20	02) × [1 –	(203)] =			0.9	(204)
Efficiency of main space heating system 1								78.9	(206)
Efficiency of secondary/supplementary heating s	system,	%						100	(208)
Jan Feb Mar Apr May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	kWh/ye	<del>-</del> ar
Space heating requirement (calculated above)									
2469.45 1947 1602.35 943.02 391.91	0	0	0	0	990.71	1850.11	2406.99		
(211)m = {[(98)m x (204)]} x 100 ÷ (206)									(211)
2816.87 2220.91 1827.78 1075.69 447.05	0	0	0	0		2110.39			_
			Total	l (kWh/yea	ar) =Sum(2	211) <sub>15,1012</sub>	Ē	14374.38	(211)
Space heating fuel (secondary), kWh/month									
$= \{ [(98)m \times (201)] \} \times 100 \div (208)$ $(215)m = 246.95  194.7  160.24  94.3  39.19$	0	0	0	0	99.07	185.01	240.7		
(213)111= 240.93 194.7 100.24 94.3 39.19	<u> </u>	U		-		215) <sub>15.1012</sub>		1260.15	(215)
Water heating			. • • • • • • • • • • • • • • • • • • •	. ()	)	- 1 15,1012		1200.13	
Output from water heater (calculated above)									
·	211.25	205.7	221.83	220.22	244.33	254.78	271.77		
Efficiency of water heater								68.8	(216)
(217)m= 77.64 77.5 77.17 76.46 74.55	68.8	68.8	68.8	68.8	76.48	77.39	77.63		(217)
Fuel for water heating, kWh/month									
$(219)$ m = $(64)$ m x $100 \div (217)$ m (219)m= $357.43$ $316.7$ $336.69$ $308.35$ $312.7$ $3$	307.05	298.98	322.43	320.09	319.45	329.21	350.09		
(=/			0						_
			Total	I = Sum(2)	19a), <sub>12</sub> =			3879.16	(219)
Annual totals			Total	I = Sum(2 <sup>-</sup>		Wh/year		3879.16 <b>kWh/year</b>	(219)
Annual totals Space heating fuel used, main system 1			Total	I = Sum(2 <sup>-</sup>		Wh/year	•	3879.16 <b>kWh/year</b> 14374.38	
			Total	I = Sum(2 <sup>-</sup>		Wh/year		kWh/year	
Space heating fuel used, main system 1			Total	I = Sum(2 <sup>-</sup>		Wh/year		kWh/year 14374.38	
Space heating fuel used, main system 1 Space heating fuel used, secondary			Total	l = Sum(2 <sup>-</sup>		Wh/year		kWh/year 14374.38 1260.15	
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used			Total	I = Sum(2 <sup>-</sup>		Wh/year	130	kWh/year 14374.38 1260.15	
Space heating fuel used, main system 1  Space heating fuel used, secondary  Water heating fuel used  Electricity for pumps, fans and electric keep-hot			Total	I = Sum(2 <sup>-</sup>		Wh/year		kWh/year 14374.38 1260.15	
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump:							130	kWh/year 14374.38 1260.15	(230c)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue					k¹		130	kWh/year 14374.38 1260.15 3879.16	(230c) (230e)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year	ns includ	ding mi	sum	of (230a).	k¹		130	kWh/year 14374.38 1260.15 3879.16	(230c) (230e) (231)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year Electricity for lighting	Ene		sum	of (230a).	(230g) =	ion fac	130	kWh/year 14374.38 1260.15 3879.16	(230c) (230e) (231) (232)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year Electricity for lighting	Ene	e <b>rgy</b> n/year	sum	of (230a).	(230g) =	ion fac 2/kWh	130	kWh/year 14374.38 1260.15 3879.16 175 972.31	(230c) (230e) (231) (232)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year Electricity for lighting 12a. CO2 emissions – Individual heating system	<b>Ene</b> kWł	e <b>rgy</b> n/year ×	sum	of (230a).	(230g) =  Emiss kg CO	ion fac 2/kWh	130 45 <b>tor</b>	14374.38 1260.15 3879.16  175 972.31  Emissions kg CO2/yea	(230c) (230e) (231) (232)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year Electricity for lighting 12a. CO2 emissions – Individual heating system Space heating (main system 1)	<b>Ene</b> kWh	ergy n/year x	sum	of (230a).	(230g) =  Emiss kg CO:	ion fac 2/kWh	130 45 tor	kWh/year 14374.38 1260.15 3879.16 175 972.31 Emissions kg CO2/year 2788.63	(230c) (230e) (231) (232)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year Electricity for lighting 12a. CO2 emissions – Individual heating system Space heating (main system 1) Space heating (secondary)	Ene kWh (211) (215) (219)	ergy n/year x x	sum	of (230a).	(230g) =  Emiss kg CO:  0.4:	ion fac 2/kWh	130 45 <b>tor</b> =	14374.38 1260.15 3879.16  175 972.31  Emissions kg CO2/yea 2788.63 531.79	(230c) (230e) (231) (232) (261) (263)
Space heating fuel used, main system 1 Space heating fuel used, secondary Water heating fuel used Electricity for pumps, fans and electric keep-hot central heating pump: boiler with a fan-assisted flue Total electricity for the above, kWh/year Electricity for lighting 12a. CO2 emissions – Individual heating system Space heating (main system 1) Space heating (secondary) Water heating	Ene kWh (211) (215) (219)	ergy n/year x x x	sum	of (230a).	(230g) =  Emiss kg CO:  0.4:	ion fac 2/kWh 94 22	130 45 <b>tor</b> =	kWh/year 14374.38 1260.15 3879.16  175 972.31  Emissions kg CO2/yea 2788.63 531.79 752.56	(230c) (230e) (231) (232) (261) (263) (264)

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### TER WorkSheet: New dwelling as built



Electricity for lighting Total CO2, kg/year (232) x

0.422

410.31

sum of (265)...(271) =

4557.14 (272)

(268)

TER =

24.92 (273)