

# Fabric Efficiency WorkSheet: New dwelling as built

## User Details:

**Assessor Name:** James Mcglashan **Stroma Number:** STRO000976  
**Software Name:** Stroma FSAP 2009 **Software Version:** Version: 1.5.0.95

## Property Address: 22 ASHP

**Address :** Flat 22, Anello Building, 116 Bayham Street, LONDON, NW1 0BA

### 1. Overall dwelling dimensions:

	Area(m <sup>2</sup> )	Ave Height(m)	Volume(m <sup>3</sup> )
Ground floor	191.89 (1a)	2.476 (2a)	475.12 (3a)
Total floor area TFA = (1a)+(1b)+(1c)+(1d)+(1e)+.....(1n)	191.89 (4)		
Dwelling volume		(3a)+(3b)+(3c)+(3d)+(3e)+.....(3n)	475.12 (5)

### 2. Ventilation rate:

	main heating	Secondary heating	other	total	m <sup>3</sup> per hour
Number of chimneys	0	0	0	0	0 (6a)
Number of open flues	0	0	0	0	0 (6b)
Number of intermittent fans				4	40 (7a)
Number of passive vents				0	0 (7b)
Number of flueless gas fires				0	0 (7c)

### Air changes per hour

Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7b)+(7c) =	40	÷ (5) =	0.08 (8)
<i>If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)</i>			
Number of storeys in the dwelling (ns)			0 (9)
Additional infiltration		[(9)-1]x0.1 =	0 (10)
Structural infiltration: 0.25 for steel or timber frame or 0.35 for masonry construction <i>if both types of wall are present, use the value corresponding to the greater wall area (after deducting areas of openings); if equal user 0.35</i>			0 (11)
If suspended wooden floor, enter 0.2 (unsealed) or 0.1 (sealed), else enter 0			0 (12)
If no draught lobby, enter 0.05, else enter 0			0 (13)
Percentage of windows and doors draught stripped			0 (14)
Window infiltration	0.25 - [0.2 x (14) ÷ 100] =		0 (15)
Infiltration rate	(8) + (10) + (11) + (12) + (13) + (15) =		0 (16)
Air permeability value, q50, expressed in cubic metres per hour per square metre of envelope area			9.83 (17)
If based on air permeability value, then (18) = [(17) ÷ 20] + (8), otherwise (18) = (16)			0.58 (18)
<i>Air permeability value applies if a pressurisation test has been done or a degree air permeability is being used</i>			
Number of sides on which sheltered			2 (19)
Shelter factor	(20) = 1 - [0.075 x (19)] =		0.85 (20)
Infiltration rate incorporating shelter factor	(21) = (18) x (20) =		0.49 (21)

Infiltration rate modified for monthly wind speed

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Monthly average wind speed from Table 7

(22)m=	5.4	5.1	5.1	4.5	4.1	3.9	3.7	3.7	4.2	4.5	4.8	5.1
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Wind Factor (22a)m = (22)m ÷ 4

(22a)m=	1.35	1.27	1.27	1.12	1.02	0.98	0.92	0.92	1.05	1.12	1.2	1.27
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Adjusted infiltration rate (allowing for shelter and wind speed) = (21a) x (22a)m

0.66	0.62	0.62	0.55	0.5	0.48	0.45	0.45	0.51	0.55	0.59	0.62
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Calculate effective air change rate for the applicable case

If mechanical ventilation:

0 (23a)

If exhaust air heat pump using Appendix N, (23b) = (23a) x Fmv (equation (N5)) , otherwise (23b) = (23a)

0 (23b)

If balanced with heat recovery: efficiency in % allowing for in-use factor (from Table 4h) =

0 (23c)

a) If balanced mechanical ventilation with heat recovery (MVHR) (24a)m = (22b)m + (23b) x [1 - (23c) ÷ 100]

(24a)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24a)

b) If balanced mechanical ventilation without heat recovery (MV) (24b)m = (22b)m + (23b)

(24b)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24b)

c) If whole house extract ventilation or positive input ventilation from outside

if (22b)m < 0.5 x (23b), then (24c) = (23b); otherwise (24c) = (22b) m + 0.5 x (23b)

(24c)m= 0 0 0 0 0 0 0 0 0 0 0 0 (24c)

d) If natural ventilation or whole house positive input ventilation from loft

if (22b)m = 1, then (24d)m = (22b)m otherwise (24d)m = 0.5 + [(22b)m² x 0.5]

(24d)m= 0.72 0.69 0.69 0.65 0.63 0.61 0.6 0.6 0.63 0.65 0.67 0.69 (24d)

Effective air change rate - enter (24a) or (24b) or (24c) or (24d) in box (25)

(25)m= 0.72 0.69 0.69 0.65 0.63 0.61 0.6 0.6 0.63 0.65 0.67 0.69 (25)

### 3. Heat losses and heat loss parameter:

ELEMENT	Gross area (m²)	Openings m²	Net Area A ,m²	U-value W/m²K	A X U (W/K)	k-value kJ/m²·K	A X k kJ/K
Windows Type 1			30.97	$x1/[1/(1.6) + 0.04] =$	46.57		(27)
Windows Type 2			18.5	$x1/[1/(1.6) + 0.04] =$	27.82		(27)
Windows Type 3			2.23	$x1/[1/(1.6) + 0.04] =$	3.35		(27)
Windows Type 4			63.46	$x1/[1/(1.6) + 0.04] =$	95.43		(27)
Windows Type 5			2.23	$x1/[1/(1.6) + 0.04] =$	3.35		(27)
Rooflights			1.44	$x1/[1/(1.6) + 0.04] =$	2.304		(27b)
Walls	151.16	117.39	33.77	x 0.29 =	9.79		(29)
Roof	191.89	4.32	187.57	x 0.14 =	26.26		(30)
Total area of elements, m²			343.05				(31)
Party wall			27.51	x 0.2 =	5.5		(32)

\* for windows and roof windows, use effective window U-value calculated using formula  $1/[(1/U\text{-value})+0.04]$  as given in paragraph 3.2

\*\* include the areas on both sides of internal walls and partitions

Fabric heat loss, W/K = S (A x U) (26)...(30) + (32) = 224.58 (33)

Heat capacity Cm = S(A x k ) ((28)...(30) + (32) + (32a)...(32e) = 2711.1101 (34)

Thermal mass parameter (TMP = Cm ÷ TFA) in kJ/m²K Indicative Value: Low 100 (35)

For design assessments where the details of the construction are not known precisely the indicative values of TMP in Table 1f can be used instead of a detailed calculation.

Thermal bridges : S (L x Y) calculated using Appendix K 51.46 (36)

if details of thermal bridging are not known (36) = 0.15 x (31)

Total fabric heat loss (33) + (36) = 276.04 (37)

Ventilation heat loss calculated monthly (38)m = 0.33 x (25)m x (5)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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(38)m= 

112.61	108.91	108.91	102.15	98.12	96.24	94.46	94.46	99.09	102.15	105.43	108.91
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 (38)

Heat transfer coefficient, W/K

(39)m = (37) + (38)m

(39)m= 

388.64	384.95	384.95	378.19	374.15	372.27	370.49	370.49	375.13	378.19	381.46	384.95
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Average = Sum(39)<sub>1...12</sub> / 12 = 

378.65
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 (39)

Heat loss parameter (HLP), W/m²K

(40)m = (39)m ÷ (4)

(40)m= 

2.03	2.01	2.01	1.97	1.95	1.94	1.93	1.93	1.95	1.97	1.99	2.01
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Average = Sum(40)<sub>1...12</sub> / 12 = 

1.97
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 (40)

Number of days in month (Table 1a)

(41)m= 

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
31	28	31	30	31	30	31	31	30	31	30	31

 (41)

### 4. Water heating energy requirement:

kWh/year:

Assumed occupancy, N

if TFA > 13.9, N = 1 + 1.76 x [1 - exp(-0.000349 x (TFA - 13.9)²)] + 0.0013 x (TFA - 13.9)

if TFA ≤ 13.9, N = 1

2.99

(42)

Annual average hot water usage in litres per day Vd,average = (25 x N) + 36

105.24

(43)

Reduce the annual average hot water usage by 5% if the dwelling is designed to achieve a water use target of not more than 125 litres per person per day (all water use, hot and cold)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Hot water usage in litres per day for each month Vd,m = factor from Table 1c x (43)

(44)m= 

115.77	111.56	107.35	103.14	98.93	94.72	94.72	98.93	103.14	107.35	111.56	115.77
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Total = Sum(44)<sub>1...12</sub> = 

1262.94
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 (44)

Energy content of hot water used - calculated monthly = 4.190 x Vd,m x nm x DTm / 3600 kWh/month (see Tables 1b, 1c, 1d)

(45)m= 

172.09	150.51	155.32	135.41	129.93	112.12	103.89	119.22	120.64	140.6	153.47	166.66
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Total = Sum(45)<sub>1...12</sub> = 

1659.87
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 (45)

If instantaneous water heating at point of use (no hot water storage), enter 0 in boxes (46) to (61)

(46)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (46)

Water storage loss:

a) If manufacturer's declared loss factor is known (kWh/day):

0

(47)

Temperature factor from Table 2b

0

(48)

Energy lost from water storage, kWh/year

((47) x (48)) =

0

(49)

If manufacturer's declared cylinder loss factor is not known:

Cylinder volume (litres) including any solar storage within same

0

(50)

If community heating and no tank in dwelling, enter 110 litres in box (50)

Otherwise if no stored hot water (this includes instantaneous combi boilers) enter '0' in box (50)

Hot water storage loss factor from Table 2 (kWh/litre/day)

0

(51)

Volume factor from Table 2a

0

(52)

Temperature factor from Table 2b

0

(53)

Energy lost from water storage, kWh/year

((50) x (51) x (52) x (53)) =

0

(54)

Enter (49) or (54) in (55)

0

(55)

Water storage loss calculated for each month

((56)m = (55) x (41)m

(56)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (56)

If cylinder contains dedicated solar storage, (57)m = (56)m x [(50) - (H11)] ÷ (50), else (57)m = (56)m where (H11) is from Appendix H

(57)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (57)

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Primary circuit loss (annual) from Table 3 0 (58)

Primary circuit loss calculated for each month (59)m = (58) ÷ 365 × (41)m

(modified by factor from Table H5 if there is solar water heating and a cylinder thermostat)

(59)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (59)

Combi loss calculated for each month (61)m = (60) ÷ 365 × (41)m

(61)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (61)

Total heat required for water heating calculated for each month (62)m = 0.85 × (45)m + (46)m + (57)m + (59)m + (61)m

(62)m= 

146.28	127.94	132.02	115.1	110.44	95.3	88.31	101.34	102.55	119.51	130.45	141.66
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 (62)

Solar DHW input calculated using Appendix G or Appendix H (negative quantity) (enter '0' if no solar contribution to water heating)

(add additional lines if FGHRs and/or WWHRs applies, see Appendix G)

(63)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (63)

Output from water heater

(64)m= 

146.28	127.94	132.02	115.1	110.44	95.3	88.31	101.34	102.55	119.51	130.45	141.66
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Output from water heater (annual)<sub>1...12</sub> 1410.89 (64)

Heat gains from water heating, kWh/month 0.25 × [0.85 × (45)m + (61)m] + 0.8 × [(46)m + (57)m + (59)m]

(65)m= 

36.57	31.98	33	28.77	27.61	23.83	22.08	25.33	25.64	29.88	32.61	35.42
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 (65)

include (57)m in calculation of (65)m only if cylinder is in the dwelling or hot water is from community heating

### 5. Internal gains (see Table 5 and 5a):

Metabolic gains (Table 5), Watts

(66)m= 

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
149.57	149.57	149.57	149.57	149.57	149.57	149.57	149.57	149.57	149.57	149.57	149.57

 (66)

Lighting gains (calculated in Appendix L, equation L9 or L9a), also see Table 5

(67)m= 

32.39	28.76	23.39	17.71	13.24	11.18	12.08	15.7	21.07	26.75	31.22	33.29
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 (67)

Appliances gains (calculated in Appendix L, equation L13 or L13a), also see Table 5

(68)m= 

363.27	367.04	357.54	337.32	311.79	287.8	271.77	268	277.5	297.72	323.25	347.24
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 (68)

Cooking gains (calculated in Appendix L, equation L15 or L15a), also see Table 5

(69)m= 

37.96	37.96	37.96	37.96	37.96	37.96	37.96	37.96	37.96	37.96	37.96	37.96
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 (69)

Pumps and fans gains (Table 5a)

(70)m= 

0	0	0	0	0	0	0	0	0	0	0	0
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 (70)

Losses e.g. evaporation (negative values) (Table 5)

(71)m= 

-119.65	-119.65	-119.65	-119.65	-119.65	-119.65	-119.65	-119.65	-119.65	-119.65	-119.65	-119.65
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 (71)

Water heating gains (Table 5)

(72)m= 

49.15	47.6	44.36	39.96	37.11	33.09	29.67	34.05	35.61	40.16	45.3	47.6
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 (72)

**Total internal gains =** (66)m + (67)m + (68)m + (69)m + (70)m + (71)m + (72)m

(73)m= 

512.68	511.27	493.17	462.86	430.01	399.94	381.39	385.62	402.05	432.5	467.64	496
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 (73)

### 6. Solar gains:

Solar gains are calculated using solar flux from Table 6a and associated equations to convert to the applicable orientation.

Orientation:	Access Factor Table 6d	Area m <sup>2</sup>	Flux Table 6a	g_ Table 6b	FF Table 6c	Gains (W)
Northeast 0.9x	0.77	30.97	11.51	0.63	0.8	124.5
Northeast 0.9x	0.77	18.5	11.51	0.63	0.8	74.37

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Northeast 0.9x	0.77	x	30.97	x	23.55	x	0.63	x	0.8	=	254.79	(75)
Northeast 0.9x	0.77	x	18.5	x	23.55	x	0.63	x	0.8	=	152.2	(75)
Northeast 0.9x	0.77	x	30.97	x	41.13	x	0.63	x	0.8	=	444.87	(75)
Northeast 0.9x	0.77	x	18.5	x	41.13	x	0.63	x	0.8	=	265.74	(75)
Northeast 0.9x	0.77	x	30.97	x	67.8	x	0.63	x	0.8	=	733.37	(75)
Northeast 0.9x	0.77	x	18.5	x	67.8	x	0.63	x	0.8	=	438.08	(75)
Northeast 0.9x	0.77	x	30.97	x	89.77	x	0.63	x	0.8	=	970.99	(75)
Northeast 0.9x	0.77	x	18.5	x	89.77	x	0.63	x	0.8	=	580.03	(75)
Northeast 0.9x	0.77	x	30.97	x	97.5	x	0.63	x	0.8	=	1054.67	(75)
Northeast 0.9x	0.77	x	18.5	x	97.5	x	0.63	x	0.8	=	630.01	(75)
Northeast 0.9x	0.77	x	30.97	x	92.98	x	0.63	x	0.8	=	1005.75	(75)
Northeast 0.9x	0.77	x	18.5	x	92.98	x	0.63	x	0.8	=	600.79	(75)
Northeast 0.9x	0.77	x	30.97	x	75.42	x	0.63	x	0.8	=	815.79	(75)
Northeast 0.9x	0.77	x	18.5	x	75.42	x	0.63	x	0.8	=	487.31	(75)
Northeast 0.9x	0.77	x	30.97	x	51.24	x	0.63	x	0.8	=	554.31	(75)
Northeast 0.9x	0.77	x	18.5	x	51.24	x	0.63	x	0.8	=	331.12	(75)
Northeast 0.9x	0.77	x	30.97	x	29.6	x	0.63	x	0.8	=	320.17	(75)
Northeast 0.9x	0.77	x	18.5	x	29.6	x	0.63	x	0.8	=	191.25	(75)
Northeast 0.9x	0.77	x	30.97	x	14.52	x	0.63	x	0.8	=	157.12	(75)
Northeast 0.9x	0.77	x	18.5	x	14.52	x	0.63	x	0.8	=	93.85	(75)
Northeast 0.9x	0.77	x	30.97	x	9.36	x	0.63	x	0.8	=	101.25	(75)
Northeast 0.9x	0.77	x	18.5	x	9.36	x	0.63	x	0.8	=	60.48	(75)
Southeast 0.9x	0.77	x	2.23	x	37.39	x	0.63	x	0.8	=	29.12	(77)
Southeast 0.9x	0.77	x	2.23	x	63.74	x	0.63	x	0.8	=	49.64	(77)
Southeast 0.9x	0.77	x	2.23	x	84.22	x	0.63	x	0.8	=	65.59	(77)
Southeast 0.9x	0.77	x	2.23	x	103.49	x	0.63	x	0.8	=	80.61	(77)
Southeast 0.9x	0.77	x	2.23	x	113.34	x	0.63	x	0.8	=	88.28	(77)
Southeast 0.9x	0.77	x	2.23	x	115.04	x	0.63	x	0.8	=	89.61	(77)
Southeast 0.9x	0.77	x	2.23	x	112.79	x	0.63	x	0.8	=	87.85	(77)
Southeast 0.9x	0.77	x	2.23	x	105.34	x	0.63	x	0.8	=	82.05	(77)
Southeast 0.9x	0.77	x	2.23	x	92.9	x	0.63	x	0.8	=	72.36	(77)
Southeast 0.9x	0.77	x	2.23	x	72.36	x	0.63	x	0.8	=	56.36	(77)
Southeast 0.9x	0.77	x	2.23	x	44.83	x	0.63	x	0.8	=	34.91	(77)
Southeast 0.9x	0.77	x	2.23	x	31.95	x	0.63	x	0.8	=	24.88	(77)
Southwest 0.9x	0.77	x	63.46	x	37.39		0.63	x	0.8	=	828.69	(79)
Southwest 0.9x	0.77	x	63.46	x	63.74		0.63	x	0.8	=	1412.68	(79)
Southwest 0.9x	0.77	x	63.46	x	84.22		0.63	x	0.8	=	1866.63	(79)
Southwest 0.9x	0.77	x	63.46	x	103.49		0.63	x	0.8	=	2293.81	(79)
Southwest 0.9x	0.77	x	63.46	x	113.34		0.63	x	0.8	=	2512.08	(79)
Southwest 0.9x	0.77	x	63.46	x	115.04		0.63	x	0.8	=	2549.93	(79)
Southwest 0.9x	0.77	x	63.46	x	112.79		0.63	x	0.8	=	2499.99	(79)

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Southwest 0.9x	0.77	x	63.46	x	105.34	0.63	x	0.8	=	2334.86	(79)
Southwest 0.9x	0.77	x	63.46	x	92.9	0.63	x	0.8	=	2059.05	(79)
Southwest 0.9x	0.77	x	63.46	x	72.36	0.63	x	0.8	=	1603.91	(79)
Southwest 0.9x	0.77	x	63.46	x	44.83	0.63	x	0.8	=	993.55	(79)
Southwest 0.9x	0.77	x	63.46	x	31.95	0.63	x	0.8	=	708.16	(79)
Northwest 0.9x	0.77	x	2.23	x	11.51	0.63	x	0.8	=	8.96	(81)
Northwest 0.9x	0.77	x	2.23	x	23.55	0.63	x	0.8	=	18.35	(81)
Northwest 0.9x	0.77	x	2.23	x	41.13	0.63	x	0.8	=	32.03	(81)
Northwest 0.9x	0.77	x	2.23	x	67.8	0.63	x	0.8	=	52.81	(81)
Northwest 0.9x	0.77	x	2.23	x	89.77	0.63	x	0.8	=	69.92	(81)
Northwest 0.9x	0.77	x	2.23	x	97.5	0.63	x	0.8	=	75.94	(81)
Northwest 0.9x	0.77	x	2.23	x	92.98	0.63	x	0.8	=	72.42	(81)
Northwest 0.9x	0.77	x	2.23	x	75.42	0.63	x	0.8	=	58.74	(81)
Northwest 0.9x	0.77	x	2.23	x	51.24	0.63	x	0.8	=	39.91	(81)
Northwest 0.9x	0.77	x	2.23	x	29.6	0.63	x	0.8	=	23.05	(81)
Northwest 0.9x	0.77	x	2.23	x	14.52	0.63	x	0.8	=	11.31	(81)
Northwest 0.9x	0.77	x	2.23	x	9.36	0.63	x	0.8	=	7.29	(81)
Rooflights 0.9x	1	x	1.44	x	26	0.63	x	0.8	=	50.95	(82)
Rooflights 0.9x	1	x	1.44	x	54	0.63	x	0.8	=	105.82	(82)
Rooflights 0.9x	1	x	1.44	x	94	0.63	x	0.8	=	184.2	(82)
Rooflights 0.9x	1	x	1.44	x	150	0.63	x	0.8	=	293.93	(82)
Rooflights 0.9x	1	x	1.44	x	190	0.63	x	0.8	=	372.31	(82)
Rooflights 0.9x	1	x	1.44	x	201	0.63	x	0.8	=	393.87	(82)
Rooflights 0.9x	1	x	1.44	x	194	0.63	x	0.8	=	380.15	(82)
Rooflights 0.9x	1	x	1.44	x	164	0.63	x	0.8	=	321.37	(82)
Rooflights 0.9x	1	x	1.44	x	116	0.63	x	0.8	=	227.31	(82)
Rooflights 0.9x	1	x	1.44	x	68	0.63	x	0.8	=	133.25	(82)
Rooflights 0.9x	1	x	1.44	x	33	0.63	x	0.8	=	64.67	(82)
Rooflights 0.9x	1	x	1.44	x	21	0.63	x	0.8	=	41.15	(82)

Solar gains in watts, calculated for each month

(83)m = Sum(74)m ... (82)m

(83)m=	1116.6	1993.47	2859.06	3892.6	4593.61	4794.02	4646.95	4100.11	3284.05	2327.99	1355.41	943.22	(83)
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Total gains – internal and solar (84)m = (73)m + (83)m , watts

(84)m=	1629.28	2504.74	3352.23	4355.46	5023.62	5193.96	5028.34	4485.73	3686.1	2760.5	1823.05	1439.22	(84)
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### 7. Mean internal temperature (heating season)

Temperature during heating periods in the living area from Table 9, Th1 (°C)

21 (85)

Utilisation factor for gains for living area, h1,m (see Table 9a)

(86)m=	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	(86)
	0.94	0.89	0.8	0.68	0.54	0.4	0.28	0.31	0.53	0.76	0.91	0.95	

Mean internal temperature in living area T1 (follow steps 3 to 7 in Table 9c)

(87)m=	17.53	18.18	19.01	19.78	20.43	20.77	20.92	20.91	20.59	19.73	18.36	17.54	(87)
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Temperature during heating periods in rest of dwelling from Table 9, Th2 (°C)

(88)m=	19.32	19.34	19.34	19.36	19.37	19.38	19.39	19.39	19.37	19.36	19.35	19.34	(88)
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Utilisation factor for gains for rest of dwelling, h2,m (see Table 9a)

(89)m=	0.93	0.87	0.77	0.63	0.47	0.31	0.18	0.2	0.44	0.71	0.9	0.94	(89)
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Mean internal temperature in the rest of dwelling T2 (follow steps 3 to 7 in Table 9c)

(90)m=	16.31	16.94	17.73	18.44	19	19.27	19.37	19.36	19.16	18.44	17.13	16.33	(90)
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fLA = Living area ÷ (4) =

0.57 (91)

Mean internal temperature (for the whole dwelling) = fLA × T1 + (1 – fLA) × T2

(92)m=	17	17.65	18.46	19.21	19.81	20.13	20.26	20.24	19.98	19.18	17.83	17.02	(92)
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Apply adjustment to the mean internal temperature from Table 4e, where appropriate

(93)m=	17	17.65	18.46	19.21	19.81	20.13	20.26	20.24	19.98	19.18	17.83	17.02	(93)
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### 8. Space heating requirement

Set Ti to the mean internal temperature obtained at step 11 of Table 9b, so that Ti,m=(76)m and re-calculate the utilisation factor for gains using Table 9a

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Utilisation factor for gains, hm:

(94)m=	0.91	0.84	0.75	0.63	0.49	0.35	0.24	0.26	0.47	0.7	0.87	0.93	(94)
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Useful gains, hmGm, W = (94)m x (84)m

(95)m=	1489.83	2109.34	2508.72	2740.17	2454.28	1840.21	1181.5	1165.33	1743.81	1943.75	1592.33	1332.16	(95)
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Monthly average external temperature from Table 8

(96)m=	4.5	5	6.8	8.7	11.7	14.6	16.9	16.9	14.3	10.8	7	4.9	(96)
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Heat loss rate for mean internal temperature, Lm, W = [(39)m x [(93)m – (96)m]

(97)m=	4859.77	4868.84	4488.03	3973.37	3035.86	2057.71	1243.02	1239.1	2129.06	3167.99	4131.5	4666.83	(97)
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Space heating requirement for each month, kWh/month = 0.024 x [(97)m – (95)m] x (41)m

(98)m=	2507.24	1854.38	1472.61	887.9	432.69	0	0	0	0	910.83	1828.21	2481	(98)
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Total per year (kWh/year) = Sum(98)<sub>1...5,9...12</sub> = 12374.85 (98)

Space heating requirement in kWh/m<sup>2</sup>/year

64.49 (99)

### 8c. Space cooling requirement

Calculated for June, July and August. See Table 10b

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
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Heat loss rate Lm (calculated using 25°C internal temperature and external temperature from Table 10)

(100)m=	0	0	0	0	0	3201.56	2297.05	2297.05	0	0	0	0	(100)
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Utilisation factor for loss hm

(101)m=	0	0	0	0	0	0.85	0.9	0.89	0	0	0	0	(101)
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Useful loss, hmLm (Watts) = (100)m x (101)m

(102)m=	0	0	0	0	0	2736.44	2078.83	2044.29	0	0	0	0	(102)
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Gains (solar gains calculated for applicable weather region, see Table 10)

(103)m=	0	0	0	0	0	6492.19	6200.81	5627.76	0	0	0	0	(103)
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Space cooling requirement for month, whole dwelling, continuous (kWh) = 0.024 x [(103)m – (102)m] x (41)m

set (104)m to zero if (104)m < 3 x (98)m

(104)m=	0	0	0	0	0	2704.14	3066.75	2666.11	0	0	0	0	(104)
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Total = Sum(104) = 8437 (104)

Cooled fraction

f C = cooled area ÷ (4) = 1 (105)

Intermittency factor (Table 10b)

(106)m=	0	0	0	0	0	0.25	0.25	0.25	0	0	0	0	(106)
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Total = Sum(104) = 0 (106)

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Space cooling requirement for month = (104)m × (105) × (106)m

(107)m=	0	0	0	0	0	675.79	766.41	666.29	0	0	0	0	
Total = Sum(107) =													2108.5 (107)

Space cooling requirement in kWh/m²/year (107) ÷ (4) = 10.99 (108)

8f. Fabric Energy Efficiency (calculated only under special conditions, see section 11)

Fabric Energy Efficiency (99) + (108) = 75.48 (109)