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REPORT AS8573.151112.NIA

HEATH PARK, NORTH END WAY, LONDON







NOISE IMPACT ASSESSMENT

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1.0 INTRODUCTION

Planning approval is being sought for the installation of new plant within the grounds of Heath Park, North End Way, London.

Clarke Saunders Associates has been commissioned by Adair Associates to undertake an environmental noise survey in order to measure the prevailing background noise climate at the site. The background noise levels measured will be used to determine daytime and night-time noise emission limits and subsequently, top assess the noise impact of proposed building services plant in accordance with the planning requirements of Camden Council.

2.0 SURVEY PROCEDURE & EQUIPMENT

A survey of the existing background noise levels was undertaken at the north western site boundary at the location shown in site plan AS8573/SP1. Measurements of consecutive 5-minute L_{Aeq} , L_{Amax} , L_{A10} and L_{A90} sound pressure levels were taken between 11:30 hours on Friday 30th October and 11:50 hours on Wednesday 2nd November 2015.

These measurements will allow suitable noise criteria to be set for the new building services plant, dependent on hours of operation.

The following equipment was used during the course of the survey:

- Rion data logging sound level meter type NA28;
- Rion sound level calibrator type NC-74.

The calibration of the sound level meter was verified before and after use. No significant calibration drift was detected.

The weather during the survey was dry with light winds, which made the conditions suitable for the measurement of environmental noise.

Measurements were made generally in accordance with ISO 1996-2:2007 Acoustics - Description, measurement and assessment of environmental noise – Part 2: Determination of environmental noise levels.

Please refer to Appendix A for details of the acoustic terminology used throughout this report.

3.0 RESULTS

Figures AS8573/TH1-TH3 show the L_{Aeq}, L_{Amax}, L_{A10} and L_{A90} sound pressure levels as time histories at the measurement position.

4.0 DISCUSSION

The background noise climate at the measurement location is determined by nearby water pump equipment and road traffic noise in the surrounding streets.

On review of the survey data, it was noted that water pump equipment was operational 24 hours per day, regularly switching off for short periods.

Following liaison with Paul Newman, EHO at Camden Council, it has been agreed that the minimum night time L_{A90} measured during one of the off periods would be representative of the minimum night time background level at the receptor.

Measured minimum background noise levels are shown in Table 4.1 below.

Monitoring period	Minimum L _{A90,10mins}
07:00 - 23:00 hours	42 dB 22:30-22:35, 01/11/15
23:00 - 07:00 hours	36 dB 02:40-02:45, 02/11/15
24 hours	36 dB

Table 4.1 - Minimum measured background noise levels

[dB ref. 20µPa]

5.0 **DESIGN CRITERIA**

5.1 **Local Authority Requirements**

Camden Council currently requires new plant to be 5dB below the background level. In addition, the background level must not be exceeded by more than 1dB in any octave band between 63Hz and 8kHz.

Noise levels at a point 1 metre external to sensitive facades shall be at least 5dB(A) less than the existing background measurement (L_{A90}), expressed in dB(A) when all plant/equipment (or any part of it) is in operation unless the plant/equipment hereby permitted will have a noise that has a distinguishable, discrete continuous note (whine, hiss, screech, hum) and/or if there are distinct impulses (bangs, clicks, clatters, thumps), then the noise levels from that piece of plant/equipment at any sensitive façade shall be at least 10dB(A) below the L_{A90} , expressed in dB(A).

It is not expected that noise character of the proposed plant units will be sufficiently distinctive to attract attention and so the plant noise emissions criteria that should not be exceeded at the nearest noise sensitive receiver should be set to the proposed levels detailed in Table 5.1.

Daytime (07:00 – 23:00 hours)	,	
L _{Aeq} 37 dB	L _{Aeq} 31 dB	L _{Aeq} 31 dB

Table 5.1 - Proposed design noise criteria

[dB ref. 20µPa]

Table 5.2 provides the spectral noise criterion at the nearest receiver.

Freq (Hz)	63	125	250	500	1k	2k	4k	8k
Criterion	63	44	33	28	29	29	29	30

Table 5.2 - Spectral design criterion

5.2 BS8233:2014 Guidance on sound insulation and noise reduction for buildings

The guidance in this document indicates suitable noise levels for various activities within residential and commercial buildings.

The relevant sections of this standard are shown in the following table:

Activity	Location	07:00 to 23:00	23:00 to 07:00
Resting	Living Room	35 dB L _{Aeq, 16 hour}	-
Dining	Dining Room	40 dB L _{Aeq, 16 hour}	-
Sleeping (daytime resting)	Bedroom	35 dB L _{Aeq, 16 hour}	30 dB L _{Aeq, 8 hour}

Table 5.3 - Excerpt from BS8233: 2014

[dB ref. 20µPa]

6.0 PREDICTED NOISE IMPACT

6.1 Proposed plant

The selected plant has been confirmed as:

- 2 no. Daikin Condensing Units Type REYQ16P8
- 2 no. Daikin Condensing Units Type REYQ20P9 (comprising 1×REMQ8P9Y1B + 1×REMQ12P8Y1B)

The approximate location of the plant to be installed is shown in site plan AS8573/SP1.

Noise levels generated by the plant items to be installed have been confirmed by the manufacturer as follows:

Freq (Hz)	63	125	250	500	1000	2000	4000	8000	dB(A)
REYQ16P8 L _p @ 1m (dB)	67	63	63	60	59	54	46	43	63
REYQ20P9 L _p @ 1m (dB)	65	65	63	59	57	52	47	45	62

Table 6.1 - Source noise data for the proposed condensing units

[dB ref. 20µPa]

6.2 Predicted Noise Levels

Following an inspection of the site, the most affected noise sensitive receptor is a 2nd floor, south-eastern aspect window of Inverforth House, as shown on the indicative site plan AS8573/SP1. This window is at least 75 metres away from the proposed plant location.

The cumulative noise level at these receptors has been calculated and is shown in the following Table 6.2.

Freq (Hz)	63	125	250	500	1k	2k	4k	8k	dB(A)
Criterion	63	44	33	28	29	29	29	30	31
Predicted level at 1m from receiver	35	33	32	28	27	22	15	13	31

Table 6.2 - Predicted noise level and criteria at receptor location

[dB ref. 20 µPa]

The predicted overall level complies with the single figure criterion. No predicted single octave band level exceeds the spectral criteria by more than 1dB.

A summary of the calculations are shown in Appendix B.

It should be noted that although the design criteria at the nearest residential window are achieved by a narrow margin, the criteria are derived from the minimum background level during the whole operational period.

It is unlikely that all condensing units would be operating at full duty at the time when the minimum background noise level occurred and thus, the noise level at these locations would most likely be lower than that indicated above in the calculations.

6.3 Comparison to BS8233:2014 Criteria

BS8233:2014 recommends that a loss of 15dB is appropriate for external noise ingress via a partially open window. The external noise level shown in 0 would result in an internal noise level that would comfortably meet the level required for sleeping in bedrooms at night, as shown in Table 5.3.

7.0 CONCLUSION

An environmental noise survey has been undertaken at Heath Park, North End Way, London by Clarke Saunders Associates between Friday 30th October and 11:50 hours on Wednesday 2nd November 2015.

Measurements have been made to establish the current background noise climate. This has enabled a 24-hour design criterion to be set for the control of plant noise emissions to noise sensitive properties, in accordance with the requirements of Camden Council.

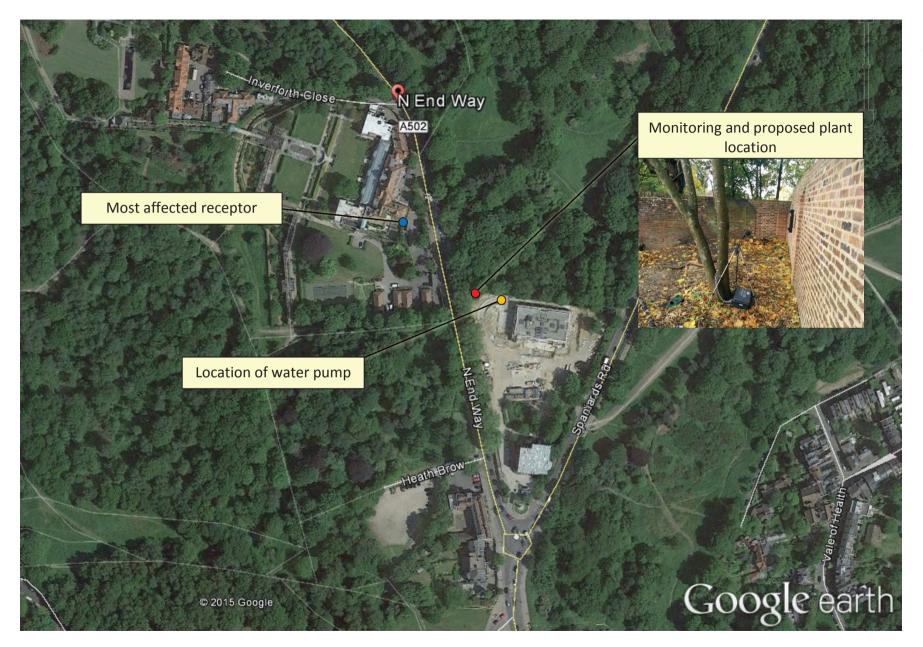
Data for the new condensing plant items has been used to predict the noise impact of the new plant on neighbouring residential properties.

Compliance with the noise emission design criterion has been demonstrated. No further mitigation measures are required for external noise emissions.

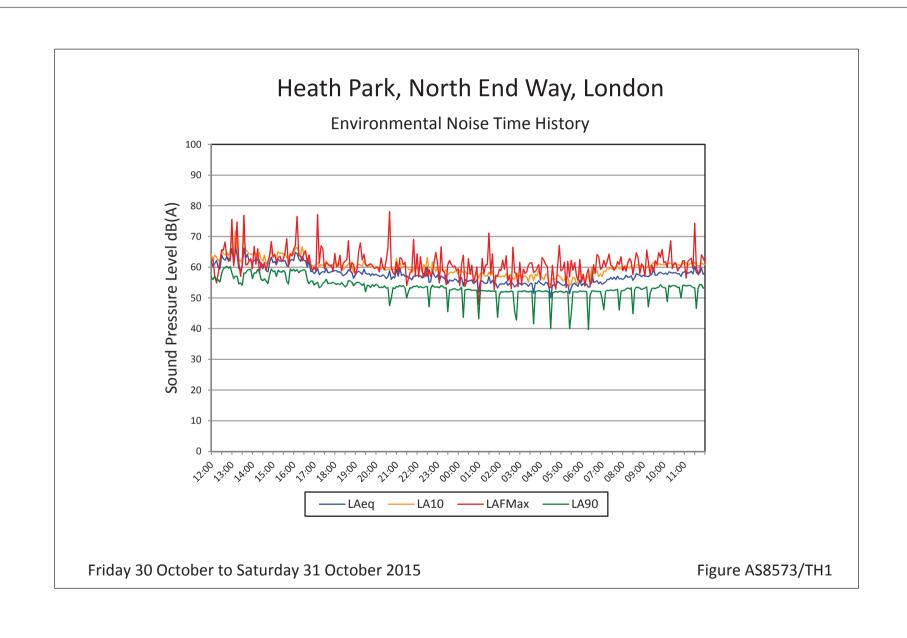
Jamie Duncan
Jamie Duncan (Nov 12, 2015)

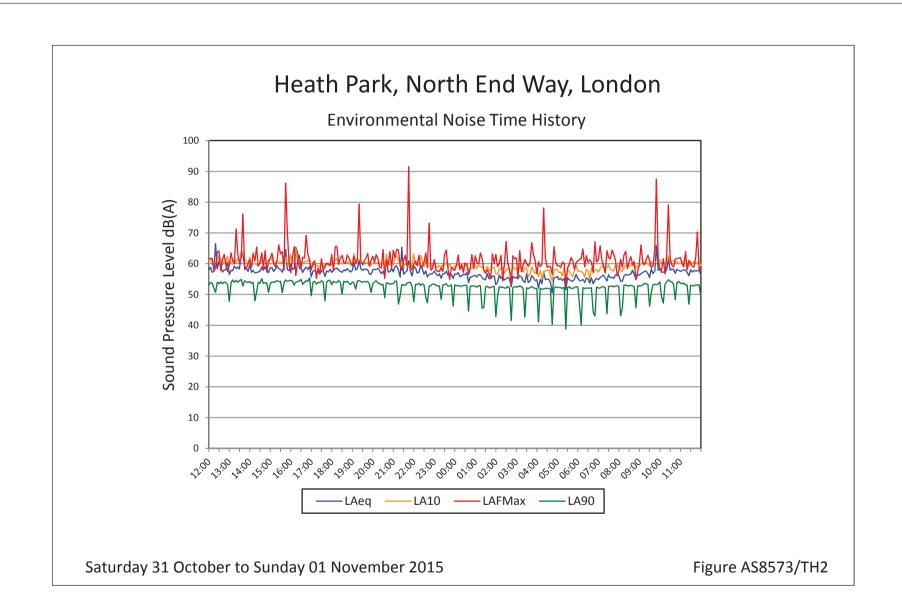
Jamie Duncan MIOA
CLARKE SAUNDERS ASSOCIATES

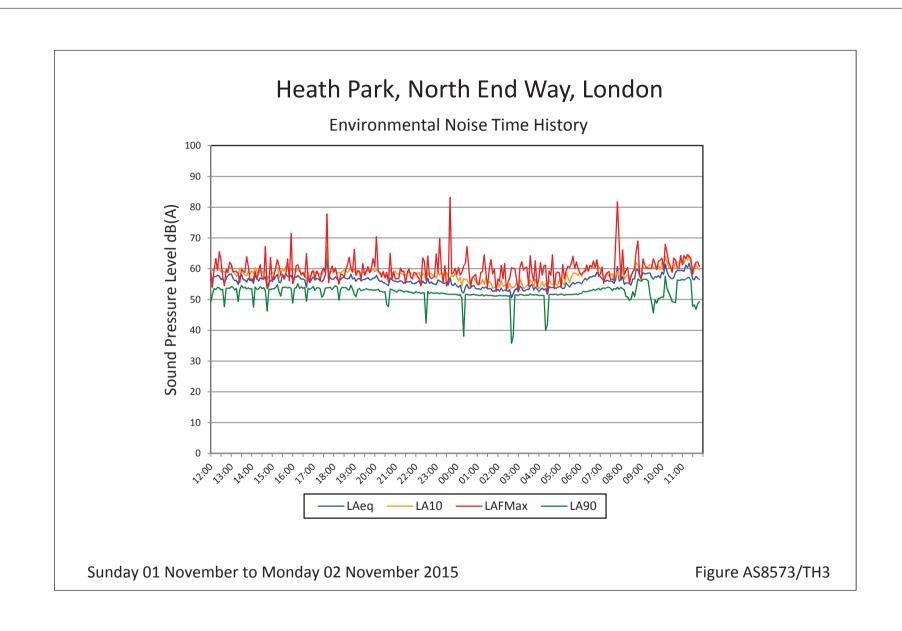
Indicative Site Plan 12 November 2015











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APPENDIX A

ACOUSTIC TERMINOLOGY & HUMAN RESPONSE TO BROADBAND NOISE

1.0 ACOUSTIC TERMINOLOGY

The annoyance produced by noise is dependent upon many complex interrelated factors such as 'loudness', its frequency (or pitch) and any variations in its level. In order to have some objective measure of the annoyance, scales have been derived to allow for these subjective factors.

dB (A):

The human ear is more susceptible to mid-frequency noise than the high and low frequencies. To take account of this when measuring noise, the 'A' weighting scale is used so that the measured noise corresponds roughly to the overall level of noise that is discerned by the average human. It is also possible to calculate the 'A' weighted noise level by applying certain corrections to an un-weighted spectrum. The measured or calculated 'A' weighted noise level is known as the dB(A) level.

L₁₀ & L₉₀:

If a non-steady noise is to be described it is necessary to know both its level and the degree of fluctuation. The L_n indices are used for this purpose, and the term refers to the level exceeded for n% of the time, hence L_{10} is the level exceeded for 10% of the time and as such can be regarded as the 'average maximum level'. Similarly, L_{90} is the average minimum level and is often used to describe the background noise.

It is common practice to use the L_{10} index to describe traffic noise, as being a high average, it takes into account the increased annoyance that results from the non-steady nature of traffic noise.

L_{eq}:

The concept of L_{eq} (equivalent continuous sound level) has up to recently been primarily used in assessing noise in industry but seems now to be finding use in defining many other types of noise, such as aircraft noise, environmental noise and construction noise.

 L_{eq} is defined as a notional steady sound level which, over a stated period of time, would contain the same amount of acoustical energy as the actual, fluctuating sound measured over that period (e.g. 8 hour, 1 hour, etc).

The use of digital technology in sound level meters now makes the measurement of L_{eq} very straightforward.

Because L_{eq} is effectively a summation of a number of noise events, it does not in itself limit the magnitude of any individual event, and this is frequently used in conjunction with an absolute noise limit.

L_{max}:

 L_{max} is the maximum sound pressure level recorded over the period stated. L_{max} is sometimes used in assessing environmental noise where occasional loud noises occur, which may have little effect on the L_{eq} noise level.

D

The sound insulation performance of a construction is a function of the difference in noise level either side of the construction in the presence of a loud noise source in one of the pair of rooms under test. *D*, is therefore simply the *level difference* in decibels between the two rooms in different frequency bands.

 D_{w}

 D_w is the Weighted Level Difference The level difference is determined as above, but weighted in accordance with the procedures laid down in BS EN ISO 717-1.

 $D_{nT,w}$

 $D_{nT,w}$ is the Weighted Standardised Level Difference as defined in BS EN ISO 717-1 and represents the weighted level difference, as described above, corrected for room reverberant characteristics.

 C_{tr}

 C_{tr} is a spectrum adaptation term to be added to a single number quantity such as $D_{nT,w}$, to take account of characteristics of a particular sound.

L'nT.w

 $L'_{nT,w}$ is the Weighted Standardised Impact Sound Pressure Level as defined in BS EN ISO 717-2 and represents the level of sound pressure when measured within room where the floor above is under excitation from a calibrated tapping machine, corrected for the receive room reverberant characteristics.

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APPENDIX A

ACOUSTIC TERMINOLOGY & HUMAN RESPONSE TO BROADBAND NOISE

2.0 OCTAVE BAND FREQUENCIES

In order to determine the way in which the energy of sound is distributed across the frequency range, the International Standards Organisation have agreed on "preferred" bands of frequency for sound measurement and analysis. The widest and most commonly used band for frequency measurement and analysis is the Octave Band. In these bands, the upper frequency limit is twice the lower frequency limit, with the band being described by its "centre frequency" which is the average (geometric mean) of the upper and lower limits, eg. 250 Hz octave band runs from 176 Hz to 353 Hz. The most commonly used bands are:

Octave Band Centre Frequency Hz 63 125 250 500 1000 2000 4000 8000

3.0 HUMAN PERCEPTION OF BROADBAND NOISE

Because of the logarithmic nature of the decibel scale, it should be borne in mind that noise levels in dB(A) do not have a simple linear relationship. For example, 100dB(A) is not twice as loud as 50dB(A) sound level. It has been found experimentally that changes in the average level of fluctuating sound, such as traffic noise, need to be of the order of 3dB(A) before becoming definitely perceptible to the human ear. Data from other experiments have indicated that a change in sound level of 10dB(A) is perceived by the average listener as a doubling or halving of loudness. Using this information, a guide to the subjective interpretation of changes in traffic noise level can be given.

INTERPRETATION

Change in Sound Level dB(A)	Subjective Impression	Human Response
0 to 2	Imperceptible change in loudness	Marginal
3 to 5	Perceptible change in loudness	Noticeable
6 to 10	Up to a doubling or halving of loudness	Significant
11 to 15	More than a doubling or halving of loudness	Substantial
16 to 20	Up to a quadrupling or quartering of loudness	Substantial
21 or more	More than a quadrupling or quartering of loudness	Very Substantial

4.0 EARTH BUNDS AND BARRIERS - EFFECTIVE SCREEN HEIGHT

When considering the reduction in noise level of a source provided by a barrier, it is necessary to establish the "effective screen height". For example if a 3 metre high barrier exists between a noise source and a listener, with the barrier close to the listener, the listener will perceive the noise source is louder, if he climbs up a ladder (and is closer to the top of the barrier) than if he were standing at ground level. Equally if he sat on the ground the noise source would seem quieter than it was if he were standing. This may be explained by the fact that the "effective screen height" is changing with the three cases above, the greater the effective screen height, in general, the greater the reduction in noise level.

Where the noise sources are various roads, the attenuation provided by a fixed barrier at a specific property will be greater for roads close to the barrier than for roads further away.

CLARKE SAUNDERS ASSOCIATES

November 2015

APPENDIX B

EXTERNAL PLANT NOISE EMISSIONS CALCULATIONS

Calculation: Plant noise emissions to nearest 2nd floor window of Inverforth House

	63	125	250	500	1000	2000	4000	8000	dB(A)
<u>Lp @ 1 m</u>	67	63	63	60	59	54	46	43	63
75 m	-38	-38	-38	-38	-38	-38	-38	-38	
	29	25	25	22	21	16	8	5	26
	63	125	250	500	1000	2000	4000	8000	dB(A)
<u>Lp @ 1 m</u>	67	63	63	60	59	54	46	43	63
75 m	-38	-38	-38	-38	-38	-38	-38	-38	
	29	25	25	22	21	16	8	5	26
	63	125	250	500	1000	2000	4000	8000	dB(A)
Lp @ 1 m	65	65	63	59	57	52	47	45	62
75 m	-38	-38	-38	-38	-38	-38	-38	-38	
	27	27	25	21	19	14	9	7	24
	63	125	250	500	1000	2000	4000	8000	dB(A)
<u>Lp @ 1 m</u>	65	65	63	59	57	52	47	45	62
75 m	-38	-38	-38	-38	-38	-38	-38	-38	
	27	27	25	21	19	14	9	7	24
Cumulative Plant Noise Level at Receptor	35	33	32	28	27	22	15	13	31
	T5 m Lp@ 1 m 75 m Lp@ 1 m 75 m	75 m -38 29 63 Lp @ 1 m 67 75 m -38 29 63 Lp @ 1 m 65 75 m -38 27 63 Lp @ 1 m 65 75 m -38 27	75 m -38 -38 29 25 63 125 Lp@ 1 m 67 63 75 m -38 -38 29 25 63 125 Lp@ 1 m 65 65 75 m -38 -38 27 27 Lp@ 1 m 65 65 75 m -38 -38 27 27	75 m -38 -38 -38 29 25 25 63 125 250 Lp @ 1 m 67 63 63 75 m -38 -38 -38 29 25 25 29 25 25 29 25 25 29 25 25 29 27 27 25 Lp @ 1 m 65 65 63 75 m -38 -38 -38 27 27 27 25 Lp @ 1 m 65 65 63 75 m -38 -38 -38 27 27 27 25	75 m -38 -38 -38 -38 -38 29 25 25 22 63 125 250 500 Lp @ 1 m 67 63 63 63 60 75 m -38 -38 -38 -38 -38 -38 29 25 25 22 63 125 250 500 Lp @ 1 m 65 65 65 63 59 75 m -38 -38 -38 -38 -38 -38 27 27 27 25 21 Lp @ 1 m 65 65 63 59 75 m -38 -38 -38 -38 -38 -38 27 27 27 25 21	75 m -38 -38 -38 -38 -38 -38 29 25 25 22 21	75 m -38 -38 -38 -38 -38 -38 -38 -38 -38 -38	75 m -38 -38 -38 -38 -38 -38 -38 -38 -38 -38	75 m -38

Camden Council Criterion for Night Time Operation 31

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