

## GROUND MOVEMENT ASSESSMENT REPORT

The Great Hall  
Lincoln's Inn  
Newman's Row  
London  
WC2A 3TL

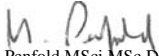
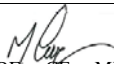
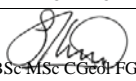

Client: The Honourable Society of  
Lincoln's Inn

Engineer: Eckersley O'Callaghan

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## 1.0 INTRODUCTION

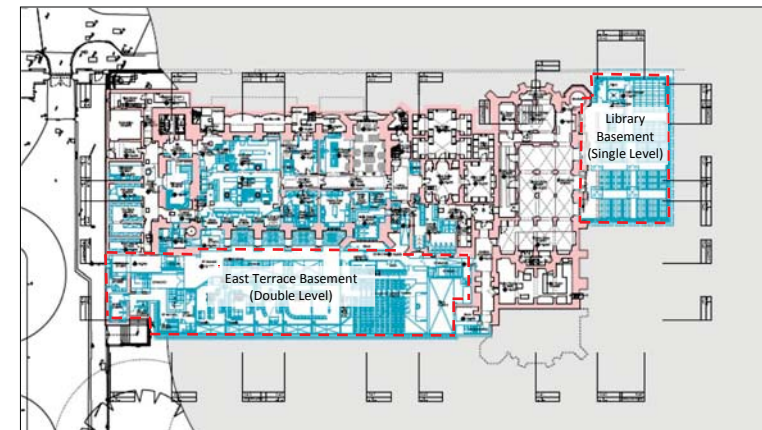
Geotechnical and Environmental Associates (GEA) has been commissioned by Eckersley O'Callaghan (EO'C), on behalf of The Honourable Society of Lincoln's Inn, to complete a ground movement assessment for the proposed redevelopment of The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL, which is to include the construction of new single and double level basements adjacent to the existing structures.

A Site Investigation and Basement Impact Assessment Report has previously been carried out by GEA (report ref J15050, dated June 2015), the findings of which have been used in the derivation of parameters for use in this assessment. An initial ground movement assessment was previously carried out by GEA and this report enhances the analysis following design development.

The purpose of this assessment has been to determine the effects of the proposed basement construction upon the neighbouring structures.

### 1.1 Proposed Development

It is understood that it is proposed to extend the existing basement space beneath The Great Hall and adjoining Library through the construction of two new basement structures, as shown on the drawing below.



The main area will comprise a double level basement that will extend to a depth of approximately 6.5 m below the current East Terrace, to a formation level of 13.45 m OD, whilst the second smaller area will comprise a single level basement extending to depths of between 3.5 m (approx. 17.8 m OD) and 4.8 m (approx. 16.3 m OD) in the area of the existing Treasures House adjacent to the north-western corner of the Library, which will be demolished and replaced with a new two-storey structure. It is also understood that the development works will include refurbishment of the existing basement beneath the great hall, which is presently occupied by the kitchens. For both of the proposed structures a combination of underpinning and new retaining walls is to be used. For the deeper basement in the East Terrace a secant wall is proposed whilst for the library extension a contiguous

bored pile wall is deemed suitable since the maximum excavation does not extend below the measured groundwater table.

This report is specific to the proposed development and the advice herein should be reviewed if the proposals are amended.

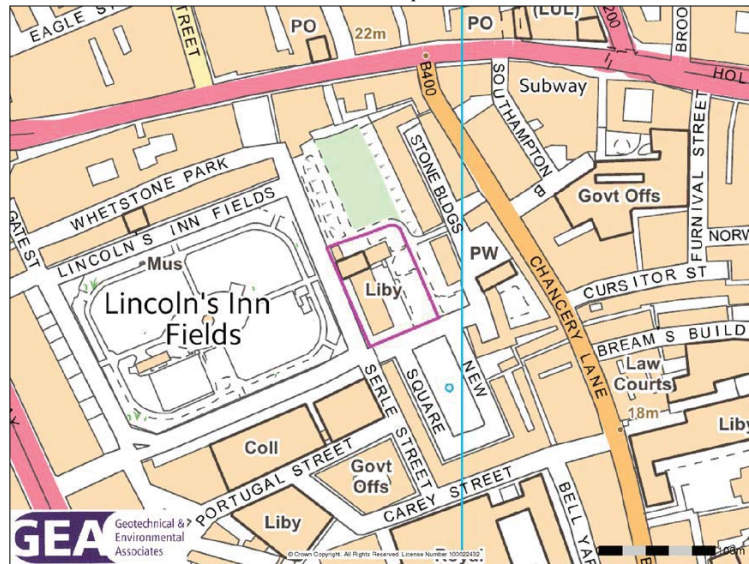
## 1.2 Limitations

The conclusions and recommendations made in this report are limited to those that can be made on the basis of the investigation. The results of the work should be viewed in the context of the range of data sources consulted, the number of locations where the ground was sampled and the number of soil, gas or groundwater samples tested; no liability can be accepted for information in other data sources or conditions not revealed by the sampling or testing. Any comments made on the basis of information obtained from the client or other third parties are given in good faith on the assumption that the information is accurate; no independent validation of such information has been made by GEA.

## 2.0 THE SITE

### 2.1 Site Description

The site is located in the London Borough of Camden, at the eastern end of Lincoln's Inn Fields, approximately 225 m to the southwest of Chancery Lane London Underground station. It fronts onto Newman's Row to the west and is bounded by New Square to the south, Old Buildings to the east, Stone Buildings to the northeast, and an area of open space to the north, all of which form part of Lincoln's Inn. The site may be additionally located by National Grid Reference 530930, 181420 and is shown on the map extract below.



The site is essentially rectangular in shape, measuring approximately 100 m by 60 m and slopes down at a very gentle angle towards the south, with a reduction in elevation of approximately 1.5 m.

The site is located on the central western part of Lincoln's Inn and is principally occupied by the Great (or New) Hall and adjoining Library building, located at the northern end of the Great Hall, both of which were constructed in the mid-1800s, although the Library was extended eastwards to give the building its present L-Shaped form in the early 1870s. An additional building, comprising the two-storey Treasurer's House, is situated adjacent to the north-western corner of the Library Building.

A single level of basement accommodation extends beneath both the Great Hall and the adjoining Library, although there is no linked access at this level between the two buildings. The basement beneath the Library is principally used as archive and storage space, whilst the basement beneath the Great Hall is occupied by the existing kitchens, wine cellar and laundry rooms. The basement beneath the Great Hall also includes a number of vaults that extend beneath the southern part of the East Terrace, which comprises an elevated platform that runs along the eastern side of the Great Hall.

Whilst the existing buildings, East Terrace and service area along the western side of the Great Hall occupy the majority of the site, the eastern part comprises an area of landscaping known as Benchers Lawn, the eastern boundary of which is lined with a number of mature deciduous trees.

## 3.0 SUMMARY OF GROUND CONDITIONS

The investigation has confirmed the expected ground conditions in that, below a moderate to significant thickness of made ground, Hackney Gravel was encountered overlying the London Clay, which was proved to the full depth investigated.

The made ground extended to depths of between 2.9 m (18.3 m OD) and 5.4 m (15.9 m OD). The Hackney Gravel typically comprised dense to dense becoming medium dense brown sand and gravel and extended to depths of between 6.2 m (13.8 m OD) and 8.3 m (13.0 m OD), although in a number of locations an initial layer of firm to stiff brown sandy clay with occasional gravel was present to depths of between 4.6 m (16.6 m OD) and 5.7 m (15.6 m OD).

The London Clay comprises an upper weathered horizon of generally firm to stiff brown clay, which extended to depths of between 6.8 m (13.2 m OD) and 8.7 m (12.6 m OD) and was underlain by stiff high strength becoming very stiff very high strength brownish grey fissured clay with occasional partings of silt to the maximum depth investigated of 29.0 m (-8.9 m OD).

Groundwater inflows were encountered within the Hackney Gravel at depths of between 5.0 m (15.0 m OD) and 7.0 m (14.3 m OD) and within the London Clay in Borehole No 2 at a depth of 13.2 m (6.9 m OD). All of the inflows comprised either slow seepages or inflows, with no observable rise.

Standpipes were installed to the base of the Hackney Gravel in each of the boreholes and the results of the monitoring visits conducted so far are shown in the table below.

Borehole No	Standpipe depth (m) (Level m OD)	Depth to groundwater (m) (Level m OD)			
		28/03/2015	14/04/2014	27/04/2015	13/05/2015
1	6.50 (13.50)	5.76 (14.24)	5.82 (14.18)	5.83 (14.17)	5.82 (14.18)
2	8.00 (12.10)	5.80 (14.30)	5.86 (14.24)	5.87 (14.23)	5.85 (14.25)
3	8.00 (13.20)	6.87 (14.33)	6.93 (14.27)	6.93 (14.27)	6.93 (14.27)
4	8.00 (13.30)	6.83 (14.47)	6.90 (14.40)	6.90 (14.40)	6.92 (14.38)

A review of borehole records held on the British Geological Society (BGS) database, has yielded records of a number of boreholes, drilled to depths of between 140 m and 180 m in the early part of the 20<sup>th</sup> Century, approximately 150 m to the southwest of the site. These boreholes show the London Clay extending to depths of between 40.0 m and 41.0 m, whereupon the Lambeth Group was encountered to depths of between 58.0 m and 59.0 m. The Thanet Sands were then proved to depths of between 66.5 m and 67.0 m, below which the Upper Chalk was proved to the maximum depth investigated.

#### 4.0 CONSTRUCTION SEQUENCE

The following sequence of operations has been provided by EO'C to enable analysis of the ground movements around the basement both during and after construction.

Essentially the sequence may be considered as three groups of activities, the first two comprising the short and medium term temporary works whilst the third represents the construction of the permanent works.

##### 4.1 Temporary Support to Underpinned Sections

The current proposals include limited sections of underpinning, including part of the existing boundary wall with Newman's Row to form part of the single level basement beneath the existing Treasurers House. Underpinning will also be carried out within the south-western parts of the proposed double level basement, where it abuts existing structures including the vaults that extend beneath these parts of the East Terrace.

Underpinning of the existing foundations will be undertaken on a 'hit and miss' basis as set out by EO'C. with short sections not exceeding 1.0 m in length, with no adjacent pin to be excavated until a minimum of 48 hours after the adjacent pin has been cast and dry-packed placed, with the sides of the excavation adequately shored and propped.

##### 4.2 Temporary Support to Piled Walls

Following installation of the bored pile wall and the lowering of the site by roughly 1.0 m, capping beams will be cast to tie the piles together and to provide load spread from vertical loads that will be supported by the piled walls. Temporary steel props will be installed and bear against steel 'king-post' upstands roughly 0.3 m above the top of the capping beam and basement excavation will proceed. The detail of section sizes and spacings will be finalised by the contractor but the general philosophy adopted will be for diagonal braces to be used across the corners or returns of the basement walls whilst props will be positioned between the two

wall at 5.0 m intervals along the long walls of the basement.

Steel temporary props will be used with strut forces spread along the 5.0 m sections of wall by a stiff reinforced concrete capping beam. Given that the buildings of Lincoln's Inn are listed, hydraulic or mechanical 'active' props will be used so that the design propping force can be applied prior to excavation in order to minimise movement at critical locations.

#### 4.3 Permanent Works

When the final excavation depths have been reached the permanent works will be formed, which will comprise a 0.3 m thick basement slab cast upon a 0.20 m thick layer of heave protection and 50 mm of blinding concrete. The basement walls are to be cast from the 'bottom-up' and will be formed of reinforced concrete walls with a drained cavity lining that is cast against the inside of the bored pile wall. A series of 'fin' walls are to cast at 5 m centres along the east wall of the East Terrace basement and will provide full height support through diaphragm action. Reinforced concrete will be used for floor slabs which will be cast on top of sections of lining wall. Following the curing of the ground floor slab, the temporary steel prop bearing against the upstands will be released and removed.

#### 5.0 PRELIMINARY RETAINING WALL DESIGN

It is recognised that the final retaining wall design will be undertaken by the successful piling contractor and that it will be tied into elements of both temporary and permanent works undertaken by the principal contractor appointed for the construction. A contractor has not yet been appointed so a preliminary geotechnical design of the piled retaining walls has been undertaken by GEA. The design has been carried out to establish the most likely pile diameter and depths required for the basement and to estimate the movement of the retaining walls both in the short term during construction and also in the long term when different soil properties will govern wall behaviour. The design outputs have also been used by EO'C to develop a preliminary propping arrangement.

##### 5.1 Basis of Design

The design has been undertaken using the Wallap software (Version 6.05 Revision A42.B57.R48) produced and licensed by Geosolve and commonly used for the design of multi-propped pile retaining walls. This analysis has adopted the BS EN 1997 Eurocode 7 method of analysis although it is understood that some piling contractors may prefer to use the approach set out in CIRIA Report C580<sup>1</sup>.

Observation of groundwater during the drilling of the boreholes and the subsequent monitoring has indicated that the groundwater level is expected to be at around 14.2 m OD in the East Terrace and 14.4 m OD in the library area. This is above the proposed formation level for the East Terrace basement of 13.45 m OD. It is therefore expected that the basement will need to be sealed against groundwater ingress from within the Hackney Gravel. In order to prevent the possible ingress of groundwater it is proposed that the piled retaining walls will be of secant construction and at this stage it is thought likely that a hard / soft wall will be suitable to restrict groundwater ingress. In such a wall the 'female' piles are constructed from a weak grout made from cement, sand and bentonite.

1 Gaba, A, Simpson, B, Powrie, W and Beadman, D (2003) *Embedded retaining walls – guidance for economic design* CIRIA Report C580.



The female piles have been assumed to provide no contribution to the structural strength of the wall and are present only to limit ingress of groundwater and to prevent the ingress of fine materials. These piles do not therefore need to extend to the full depth of the male piles and may be terminated within non-productive strata below the basement formation level. At this site the London Clay, assumed to be a non-productive stratum is present at around 13.2 m OD. Good practice would suggest that female piles should extend to a level no shallower than 12.2 m OD. At such a toe level, all piles will be formed with a roughly 1.0 m penetration into the London Clay which is considered sufficient to provide a 'seal' against significant groundwater ingress.

The soil parameters adopted are those set out in the GEA Site Investigation Report reference J15050 dated June 2015.

Details of the foundations and loadings of the surrounding buildings have been provided by EO'C in their Structural Report and Basement Impact Assessment. Existing walls have been modelled as buried surcharges and the proposed ramped ground level outside the basement of the East Terrace has been modelled as a sloping surcharge that is in continuity with the strata beneath. Two sections have been analysed for the eastern and western walls of the East Terrace along with two sections of the library extension structure. These are considered to provide a sufficiently broad view of the proposed basement as to satisfy this assessment whilst acknowledging that a number of further piled wall cases will need to be considered by the piling contractor in due course.

Props have been adopted at levels equivalent to the mid-points of the slabs noted on the EO'C drawings. The ground floor and basement floor concrete slabs have been taken as 250 mm and 300 mm thick in accordance with EO'C drawings.

At this stage in the process, the retaining walls have only been designed for the Serviceability Limit State (SLS) and the maximum bending moments shown to confirm the suitability of the proposed pile diameter. The various load factors, soil parameter factors and output factors are indicated within the results of each of the four design cases.

The detailed design within each case has been based on undrained soil parameters during temporary works and construction with long term drained soil parameters adopted for the long term permanent case with a reversion to at-rest earth pressures. At this stage drained cohesion  $c'$  has been ignored and an at-rest earth pressure  $K_0$  of 1.0 has been adopted. The results of these runs are appended and confirm that 450 mm diameter piles at 600 mm centre to centre spacing are acceptable. It is assumed that the outline pile wall design will be developed by the piling contractor at a later stage.

## 5.2 Summary Results and Bored Pile Wall Proposals

The proposed secant piled wall for the East Terrace comprises 450 mm diameter piles installed at 600 mm male to male and female to female centre to centre spacings; the contiguous wall piles will be of a similar diameter and spacing. These spacings would allow each male pile to cut roughly 150 mm into the adjacent female piles and would allow for the piles to still intersect at excavation formation level if they were installed at the limits of 1 in 100 verticality tolerance and the potential depth to the impermeable barrier of 6 m. The toe level of the female piles is proposed as 12.2 m OD (5.9 m long piles) and the male piles would extend to 7.0 m OD in the eastern wall (11.1 m long piles) and 8.5 m OD in the western wall of the East Terrace basement.

A summary of the retaining wall designs and predicted movements is shown below.

Wall Section	Pile Toe Level (m OD)	Pile Length (m)	Maximum Unfactored Bending Moment (kNm/pile)	Maximum Predicted Wall Deflection (mm)	Maximum Predicted U/F Load per Strut (kN)
East Terrace East Wall	7.0	11.0	34	11	120
East Terrace West Wall	8.5	9.5	30	6	116
Library East Wall	12.0	9.2	21	5	103
Library North Wall	12.0	9.2	38	8	137

The maximum unfactored bending moment is given as 38 kNm per pile; detailed reinforcement design will be undertaken by the piling contractor but at this stage these values are deemed sufficient to confirm that the 450 mm diameter scheme is appropriate.

## 6.0 GROUND MOVEMENTS

An assessment of ground movements within and surrounding the excavation has been undertaken using the X-Disp and P-Disp computer programs licensed from the OASYS suite of geotechnical modelling software from Arup. These programs are commonly used within the ground engineering industry and are considered to be appropriate tools for this analysis.

The X-Disp program has been used to predict ground movements likely to arise from the construction of the proposed basement. This includes the settlement of the ground (vertical movement) and the lateral movement of soil behind the proposed retaining walls (horizontal movement).

The analysis of potential ground movements within the excavation, as a result of unloading of the underlying soils, has been carried out using the Oasys P-Disp (Version 19.2 – Build 12) software package and is based on the assumption that the soils behave elastically, which provides a reasonable approximation to soil behaviour at small strains.

For the purpose of these analyses, the corners have been defined by x and y coordinates, with the x-direction parallel with the orientation north-south, whilst the y-direction is parallel with the orientation of east-west. Vertical movement is in the z-direction. The full outputs of all the analyses can be provided on request but samples of the output movement contour plots are included within the appendix.

### 6.1 Ground Movements – Surrounding the Basement

#### 6.1.1 Model Used

For the X-Disp analysis, the soil movement relationships used for the embedded retaining walls are based on the default values within CIRIA report C580<sup>2</sup> but have been adjusted in the light of the movement predictions from the Wallap analysis summarised above. The C580 movements were derived from a number of historic case studies of the short term movements that result from wall installation and basement excavation. The ground movement curves for 'installation of contiguous bored pile wall in stiff clay' has been adopted as appropriate for

<sup>2</sup> Gaba, A, Simpson, B, Powrie, W and Beadman, D (2003) *Embedded retaining walls – guidance for economic design*. CIRIA Report C580.

both the contiguous wall at the library as well as the secant wall at the East Terrace. This is because the movement predictions for the secant wall are based on a very limited dataset and provided careful sequencing of the pile installation takes place then the contiguous curve is more realistic.

Temporary works drawings provided by EO'C indicate that the mass concrete underpinning to form the new basement structure will be supported or propped in the temporary condition to maintain its stability during the excavation and that reinforced concrete retaining walls will be cast at a later stage in the appropriate areas. It would seem reasonable to adopt the ground movement curves for 'no horizontal and vertical movement' for this analysis but in practice there will always be a potential for a small degree of movement to take place, typically 2 mm to 5 mm and a more conservative approach using the same ground movement curves as the bored pile wall has been adopted.

### 6.1.2 Results

The X-Disp analysis has been used to estimate the movements behind the walls resulting from pile installation and basement excavation. This includes the settlement of the ground (vertical movement) and the lateral movement of soil behind the wall (horizontal movement). The contour graphs of these movement predictions are appended for the piling phase together with the total movement prediction which combined the effects.

In each of the four design cases, the ground movement predictions using the C580 relationships have been compared with the predictions from the Wallap designs; the latter having been based on the greatest movements which in all cases relate to the long term drained conditions. The C580 correlations have been amended as set out below.

Table 2.4 of C580 indicates that horizontal movement should be around 0.15 % of the maximum excavation depth (Column 2 in the table below) for a stiff wall embedded in stiff clay and no horizontal movement for a wall wholly embedded in sand. With the benefit of the Wallap runs a revised wall deflection has been derived (Column 3) since at this site a combination of sand and gravel over clay is present. This has been used with the excavation depth to derive a new horizontal movement factor (Column 4). This value has been used in the X-Disp program to produce wall movement contours that correlate with the Wallap data. The proportionate decrease in horizontal movement has then been applied to the vertical movement profile to produce a new movement curve for vertical movements (Column 5).

The predicted movements are summarised in the table below; the results are presented to the degree of accuracy required to allow predicted variations in ground movements around the structure to be illustrated, but may not reflect the anticipated accuracy of the predictions.

Design Case	Stiff Wall Horizontal Movement Factor d/h (%)	Average Wall Deflection Wallap (mm)	Adopted Stiff Wall Horizontal Movement Factor d/h (%)	Vertical Movement Reduction Factor (%)
East Terrace East Wall	0.15	5	0.12	80
East Terrace West Wall	0.15	4	0.12	80
Library East Wall	0.15	4	0.12	80
Library North Wall	0.15	7	0.14	93

The above data has been used in an X-Disp analysis and the contours and results are appended. These are based on the full Wallap movements which may be considered highly conservative since the added stiffness of the lining wall and the entire basement box have not been taken into account.

Phase of Works	Maximum Movement at 17.0 m OD – sensibly average foundation level	
	Vertical Settlement (mm)	Horizontal Movement (mm)
Piling	Up to 5	Up to 5
Combined Piling and Basement Excavation	5 to 10	10 to 15

The movements set out in the table above are the maximum movements and generally occur immediately or just outside the line of the piled walls; the effects of the excavation reduce with distance away from the piled wall.

### 6.2 Movements within the Excavation (Heave)

#### 6.2.1 Model Used

Unloading of the London Clay and underlying Lambeth Group will take place as a result of the basement excavation and the reduction in vertical stress will cause heave to take place. Undrained soil parameters have been used to estimate the potential short term movements, which include the "immediate" or elastic movements as a result of the basement excavation. Drained parameters have been used to provide an estimate of the total long-term movement.

The elastic analysis requires values of soil stiffness at various levels to calculate displacements. Values of stiffness for the soils at this site are readily available from published data and we have used a well-established method to provide our estimates. This relates values of  $E_u$  and  $E'$ , the drained and undrained stiffness respectively, to values of undrained cohesion, as described by Padfield and Sharrock<sup>3</sup> and Butler<sup>4</sup> and more recently by O'Brien and Sharp<sup>5</sup>. Relationships of  $E_u = 500 C_u$  and  $E' = 300 C_u$  for the cohesive soils and 2000 x SPT 'N' for granular soils have been used to obtain values of Young's modulus. More recent published data<sup>6</sup> indicates stiffness values of 750 x  $C_u$  for the London Clay and a ratio of  $E'$  to  $C_u$  of 0.75, but it is considered that the use of the more conservative values provides a sensible approach for this stage in the design.

The proposed construction of the 4.00 m to 5.0 m deep basement on the north-western part of the site will result in an approximate unloading of about 70 kN/m<sup>2</sup> to 90 kN/m<sup>2</sup>, whilst the deeper excavations beneath the East Terrace are likely to result in an approximate unloading of about 125 kN/m<sup>2</sup>.

A rigid boundary for the analysis has been set at a depth of about 60 m below existing ground level, where nearby BGS records indicate that the base of the Lambeth Group is likely to be present. Below this depth the essentially incompressible soils of the Thanet Sand should be present.

<sup>3</sup> Padfield CJ and Sharrock MJ (1983) *Settlement of structures on clay soils*. CIRIA Special Publication 27

<sup>4</sup> Butler FG (1974) *Heavily overconsolidated clays: a state of the art review*. Proc Conf Settlement of Structures, Cambridge, 531-578, Pentech Press, Lond

<sup>5</sup> O'Brien AS and Sharp P (2001) *Settlement and heave of overconsolidated clays - a simplified non-linear method*. Part Two, Ground Engineering, Nov 2001, 48-53

<sup>6</sup> Burland JB, Standing, JR, and Jardine, FM (2001) *Building response to tunnelling, case studies from construction of the Jubilee Line Extension..* CIRIA Special Publication 200

## 6.2.2 Results

The P-Disp analysis indicates that, by the time the basement construction is complete, up to 22 mm of heave is likely to have taken place at the centre of the proposed double level, reducing to less than 14 mm at the edges, whilst for the proposed single level basement the movements range from 14 mm at the centre of the excavations to less than 10 mm at the edges.

In the long term, following completion of each of the proposed double level basement, a further 18 mm of heave is estimated as a result of long term swelling of the underlying London Clay, whilst a further 10 mm is estimate at the centre of the single level basement on the north-western part of the site.

The results of the P-Disp analysis also indicate the likely impact of the proposed basement constructions beyond the extent of the excavations. On the basis of the analysis, total vertical heave movements outside the proposed basement are unlikely to exceed 12 mm for the proposed double level basement and less than 6 mm for the proposed single level basement, at a distance of approximately 5 m.

The potential movements are summarised in the tables below.

### 6.2.2.1 East Terrace – Double Level Basement

Location	Movement (mm)		
	Short-term Heave (Excavation Phase)	Long-term Heave (post construction)	Total Heave
Centre of excavations	22	18	40
Edge of excavations	12 to 14	8 to 12	20 to 26
At 5 m from edge of excavations	4 to 6	2 to 6	6 to 12

### 6.2.2.2 Library & Treasurer's House – Single Level Basement

Location	Movement (mm)		
	Short-term Heave (Excavation Phase)	Long-term Heave (post construction)	Total Heave
Centre of excavations	14	10	24
Edge of excavations	4 to 8	6 to 8	10 to 16
At 5 m from edge of excavations	<4	<2	4 to 6

In order to mitigate the effects of heave on the new building, a layer of compressible material has been incorporated into the design to accommodate these potential long term movements. This material will need to be designed to be able to resist the potential uplift forces generated by the ground movements. In this respect potential heave pressures are typically taken to equate to around 50 % to 60 % of the total unloading pressure.

## 6.3 Differential Movements

The piled walls will in places be adjacent to underpins and different mechanisms of load

transmittal to the underlying soils could be a cause of differential settlement. Both are understood to be subject to vertical load with the wall piles being more slender will be more likely to move under lateral earth pressure. However the construction sequence will allow for some form of waterproof movement joint to be cast between the two. Both piles and pins will be also be subject to propping by the basement and floor slabs and with movement restricted the effect of differential lateral movement is considered to be limited.

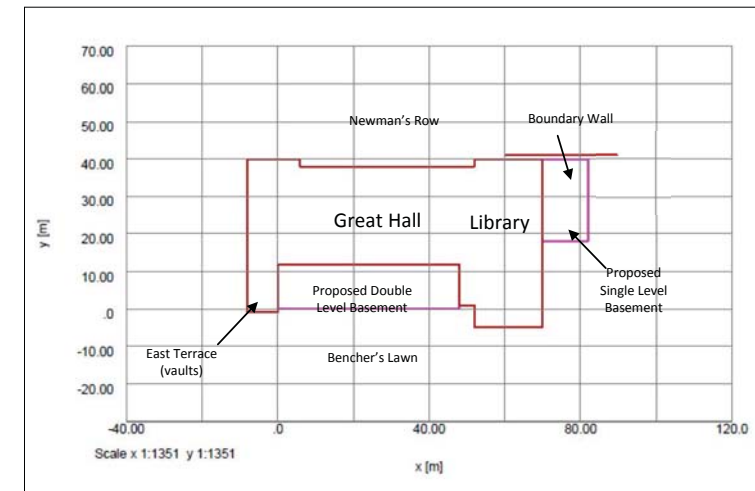
Both underpins and wall piles will also be subject to vertical loading. The underpins will bear within the Hackney Gravel which will support the load as a spread foundation and settlement of typically 2 mm to 5 mm could be anticipated. The piles will transfer the vertical loading into the underlying clay through the shaft friction of the front and rear faces of the embedded portion of the wall. Assuming that a factor of safety of 3.0 will be applied to such loading then settlement under working load is likely to be less than 5 mm; that is in the same order as may be expected for the underpins.

## 7.0 DAMAGE ASSESSMENT

In addition to the above assessment of the likely movements that will result from the proposed development, some of the neighbouring structures have been considered as sensitive structures, requiring Building Damage Assessments, on the basis of the classification given in Table 2.5 of C580<sup>1</sup>. These include:

- The existing structures of the Great Hall (incl East Terrace) and adjoining Library Building;
- The boundary wall with Newman's Row.

The sensitive structures outlined above have been modelled as lines in the analysis and are those along which the damage assessment has been undertaken, as shown on the plan below.



For the analyses it has been assumed that the average foundation depths of the adjoining buildings, which include existing basement structures, can be taken to be around 18 m OD to 17 m OD. Trial Pit excavations have also shown that the foundations of the boundary wall with Newman's Row also extend to a similar depth of approximately 18 m OD.

## 7.1 Damage to Neighbouring Structures

The combined movements resulting from both pile installation and basement excavation calculated using the X-Disp modelling software have been used to carry out an assessment of the likely damage to adjacent properties and the results are summarised in the table below.

The potential heave movements predicted by P-Disp have not been included in this assessment, which can therefore be considered as conservative, as these movements are likely to have a mitigating effect on the downward settlement predicted by X-Disp.

Building Damage Assessment		
Sensitive Structure	Elevation	Category of Damage*
The Great Hall	East Terrace – Existing Vaults	Category 0 (Negligible) to Category 1 (Very Slight)
	Eastern - East Terrace Frontage	Category 0 (Negligible) to Category 1 (Very Slight)
	Western	Less than the limit of detection
	Southern	Category 0 (Negligible)
Library Building	Southern – East Terrace Frontage	Category 0 (Negligible) to Category 1 (Very Slight)
	Eastern	Category 0 (Negligible)
	Northern	Category 1 (Very Slight)
	Western	Less than the limit of detection
Boundary Wall with Newman's Row (Section close to proposed single level basement on north-western part of the site)	Western	Category 0 (Negligible)

\*From Table 2.5 of C580<sup>1</sup>: Classification of visible damage to walls.

The building damage reports for sensitive structures highlighted in the above table and shown graphically on the appended plan predict that the damage to the adjoining and nearby structures would generally be Category 0 (negligible), with a limited areas of Category 1 (Very Slight), along the elevations of the Great Hall closest to the proposed double level basement.

On this basis, the damage that would inevitably occur as a result of such an excavation would fall within acceptable limits.

## 7.2 Monitoring of Ground Movements

The predictions of ground movement based on the ground movement analysis should be checked by monitoring of adjacent properties and structures. The structures to be monitored during the construction stages include:

- The elevations of the Great Hall (incl East Terrace) and adjoining Library Building that bound the East Terrace;
- The boundary wall with Newman's Row adjacent to the proposed single level basement on the north-western part of the site.

Condition surveys of the above existing structures will be carried out before and after the proposed works.

The precise monitoring strategy will be developed at a later stage but EO'C have indicated the potential target locations on their drawings whilst remaining subject to discussions and agreements with the owners of the adjacent properties and structures before construction takes place. It is, however, expected that monthly monitoring would take place throughout the construction and that the frequency would increase to at least weekly during the groundworks elements and daily where excavation against critical areas is underway.

## 7.3 Mitigation

Reference to the detailed results indicates that the predicted damage to the existing structures is within Categories 0 and 1.

The sections of wall that are identified as being susceptible to 'very slight' damage will be identified and subject to close scrutiny during the monitoring process. Each of the piled walls that relate to these locations will be designed in detail in due course and will be subject to a specific propping arrangement which will be adjustable to that greater or lesser load can be applied depending on the performance of the piles at each location.

## 8.0 CONCLUSIONS

The analysis has concluded that the predicted damage to the neighbouring properties would generally be 'Negligible', with some limited areas of 'Very Slight' along sections of the existing structures that adjoin the East Terrace. On this basis, the damage that would inevitably occur as a result of such an excavation would fall within the acceptable limits.

The separate phases of work, including piling / underpinning and subsequent excavation of the proposed basement structures, will in practice be separated by a number of weeks during which time construction of capping beams and pile curing will take place. This will provide an opportunity for the ground movements during and immediately after piling to be measured and the data acquired can be fed back into the design and compared with the predicted values. Such a comparison will allow the ground model to be reviewed and the predicted wall movements to be reassessed prior to the main excavation taking place so that propping arrangements can be adjusted if required.



**APPENDICES**

**WALLAP RETAINING WALL DESIGN RUNS**

**SOIL DISPLACEMENT MODEL RESULTS**

**X-DISP ANALYSIS**

**Pile Installation**

Contour Plots of Vertical Movements and Horizontal Movements

**Pile Installation and Basement Excavation**

Contour Plots of Combined Vertical Movements and Horizontal Movements

**P-DISP ANALYSIS**

Short Term Movement

Total Movement

**BUILDING DAMAGE ASSESSMENT (X-DISP)**

Tabular Output of Results

Damage Category Plan

GEOTECHNICAL & ENVIRONMENTAL ASSOCIATES | Sheet No.  
Program: WALLAP Version 6.05 Revision A45.B58.R48 | Job No. J15050  
Licensed from GEOSOLVE | Made by : MC  
Data filename/Run ID: East Terrace S2.1 S2 East SLS1\_SLS | Date: 4-02-2016  
Lincoln's Inn Fields, London WC2A 3TL | Checked :  
East Terrace S2.1 Section 2 East

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Active side	Soil types	Passive side
1	18.02	1 Made Ground		1 Made Ground
2	16.50	2 Hackney Gravel		2 Hackney Gravel
3	13.20	3 London Clay		3 London Clay
4	3.50	4 London Clay		4 London Clay

**SOIL PROPERTIES**

No.	Description (Datum elev.)	Bulk density (kN/m3)	Young's Modulus (Eh, kN/m2)	At rest coeff. (dKo/dy)	Consol. state. (Nu)	Active limit (Kac)	Passive limit (Kpc)	Cohesion (dc/dy)
1	Made Ground	17.00	15000	0.500	NC	1.000	1.000	30.00u
2	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
3	London Clay (13.20)	19.50	35000	1.000	OC	1.000	1.000	70.00u
4	London Clay	19.50	87500	1.000	OC	1.000	1.000	175.0u
5	Made Ground Drained	17.00	9000	0.500	NC	0.490	2.040	0.0d
6	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
7	London Cl.. (13.20)	19.50	21000	1.000	OC	0.585	1.247	5.000d
8	London Clay Drained	19.50	52500	1.000	OC	0.585	1.247	5.000d

**Additional soil parameters associated with Ka and Kp**

No.	Description	parameters for Ka			parameters for Kp		
		Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1	Made Ground	0.00	0.000	0.00	0.00	0.000	0.00
2	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
3	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
5	Made Ground Drained	20.00	0.000	0.00	20.00	0.000	0.00
6	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
7	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00
8	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3  
Initial water table elevation Active side 14.20 Passive side 14.20  
Automatic water pressure balancing at toe of wall : No

profile no.	Point no.	Active side			Passive side			
		Elev. (m)	Piezo elev. (m)	Water press. (kN/m2)	Point no.	Elev. (m)	Piezo elev. (m)	Water press. (kN/m2)
1	1	14.20	14.20	0.0	1	14.20	14.20	0.0 MC
2	1	14.20	14.20	0.0	1	13.45	13.45	0.0 MC

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 7.00  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.0000E+07 kN/m2  
 Moment of inertia of wall I = 3.2000E-03 m4/m run  
 E.I = 64000 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	18.32	5.00	0.100000	2.000E+08	5.00	0.00	50.00	Yes
2	13.85	1.00	0.300000	2.000E+07	5.00	0.00	0	No
3	17.98	1.00	0.250000	2.000E+07	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev. m	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge Near edge	Surcharge Far edge	Equiv. type	Partial soil factor/ Category
1	18.02	1.00(A)	20.00	1.99	0.00	33.70	1	N/A
2	18.02	2.99(A)	20.00	20.00	33.70	=	1	N/A
3	13.45	-0.00(P)	20.00	20.00	7.50	=	0	1.00 -
4	18.02	2.99(A)	20.00	20.00	5.00	=	0	1.00 Var

Note: A = Active side, P = Passive side  
 A trapezoidal surcharge is defined by two values:  
 N = at edge near to wall, F = at edge far from wall  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.1 at elevation 18.02 No analysis at this stage
2	Apply surcharge no.2 at elevation 18.02 No analysis at this stage
3	Apply surcharge no.4 at elevation 18.02
4	Excavate to elevation 17.11 on PASSIVE side
5	Install strut or anchor no.1 at elevation 18.32
6	Apply surcharge no.3 at elevation 13.45 No analysis at this stage
7	Apply water pressure profile no.2 ( Mod. Conserv. ) No analysis at this stage
8	Excavate to elevation 13.45 on PASSIVE side
9	Install strut or anchor no.2 at elevation 13.85
10	Install strut or anchor no.3 at elevation 17.98
11	Remove strut or anchor no.1 at elevation 18.32
12	Change properties of soil type 1 to soil type 5 No analysis at this stage Ko pressures will not be reset
13	Change properties of soil type 2 to soil type 6 No analysis at this stage Ko pressures will not be reset
14	Change properties of soil type 3 to soil type 7 No analysis at this stage Ko pressures will not be reset
15	Change properties of soil type 4 to soil type 8 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: Serviceability Limit State  
 All loads and soil strengths are unfactored

**Stability analysis:**

Method of analysis - Burland-Potts  
 Factor on passive for calculating wall depth = 1.00  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

**Parameters for undrained strata:**

Minimum equivalent fluid density = 5.00 kN/m3  
 Maximum depth of water filled tension crack = 0.00 m

**Bending moment and displacement calculation:**

Method - Subgrade reaction model using Influence Coefficients  
 Open Tension Crack analysis? - No  
 Non-linear Modulus Parameter (L) = 0 m

**Boundary conditions:**

Length of wall (normal to plane of analysis) = 1000.00 m  
 Width of excavation on active side of wall = 20.00 m  
 Width of excavation on passive side of wall = 20.00 m  
 Distance to rigid boundary on active side = 20.00 m  
 Distance to rigid boundary on passive side = 20.00 m

**OUTPUT OPTIONS**

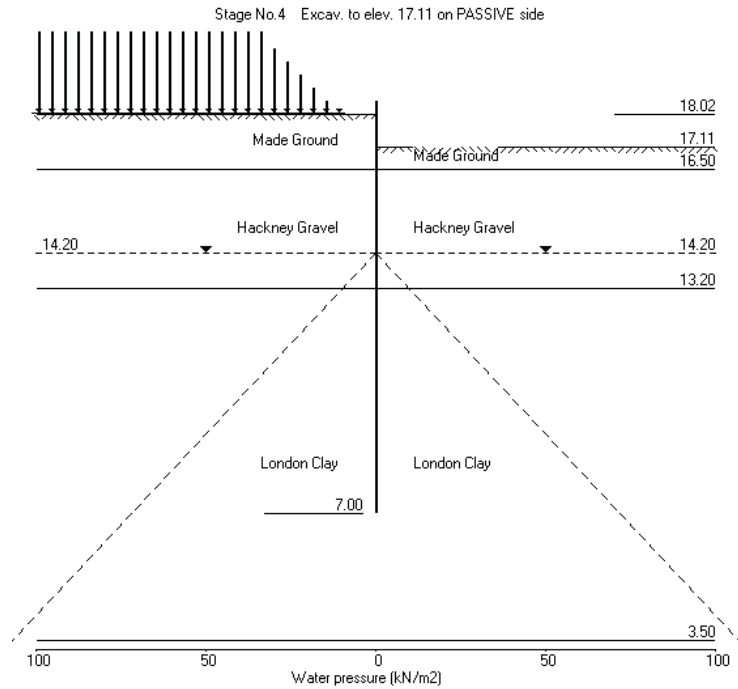
Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.1 at elev. 18.02	No	No	No
2	Apply surcharge no.2 at elev. 18.02	No	No	No
3	Apply surcharge no.4 at elev. 18.02	No	No	No
4	Excav. to elev. 17.11 on PASSIVE side	Yes	Yes	Yes
5	Install strut no.1 at elev. 18.32	No	No	No
6	Apply surcharge no.3 at elev. 13.45	No	No	No
7	Apply water pressure profile no.2	No	No	No
8	Excav. to elev. 13.45 on PASSIVE side	No	No	No
9	Install strut no.2 at elev. 13.85	No	No	No
10	Install strut no.3 at elev. 17.98	No	No	No
11	Remove strut no.1 at elev. 18.32	No	No	No
12	Change soil type 1 to soil type 5	No	No	No
13	Change soil type 2 to soil type 6	No	No	No
14	Change soil type 3 to soil type 7	No	No	No
15	Change soil type 4 to soil type 8	No	No	No
*	Summary output	Yes	-	Yes

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 Data filename/Run ID: East Terrace S2.1 S2 East SLS1\_SLS  
 Lincoln's Inn Fields, London WC2A 3TL  
 East Terrace S2.1 Section 2 East

Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 4-02-2016  
 Checked :

Units: kN,m



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 Lincoln's Inn Fields, London WC2A 3TL  
 East Terrace S2.1 Section 2 East

Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 4-02-2016  
 Checked :

Units: kN,m

Stage No. 4 Excavate to elevation 17.11 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**  
 Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	Act. Elev.	Pass. Elev.	Strut Elev.	Factor of Safety at elev.	Moment of equilib. at elev.	Toe elev.	Wall Penetration
4	18.02	17.11	Cant.	16.885	7.35	***	***

Legend: \*\*\* Result not found

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**  
 Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	18.32	0.00	0.001	1.17E-05	0.0	-0.0	
2	18.02	0.00	0.001	1.17E-05	0.0	-0.0	
3	17.98	0.18	0.001	1.17E-05	0.0	-0.0	
4	17.55	2.77	0.001	1.11E-05	0.6	0.2	
5	17.11	7.19	0.001	7.65E-06	2.8	0.9	
		5.31	0.001	7.65E-06	2.8	0.9	
6	16.81	9.37	0.001	6.23E-07	5.1	2.1	
7	16.50	12.33	0.001	-1.40E-05	8.4	4.1	
		-5.91	0.001	-1.40E-05	8.4	4.1	
8	16.05	-5.58	0.001	-5.39E-05	5.8	7.3	
9	15.60	-5.54	0.001	-1.12E-04	3.3	9.3	
10	15.00	-6.09	0.001	-2.04E-04	-0.2	10.4	
11	14.60	-6.89	0.001	-2.67E-04	-2.8	9.8	
12	14.20	-8.02	0.001	-3.23E-04	-5.8	8.2	
13	13.85	-9.24	0.001	-3.61E-04	-8.8	5.7	
14	13.45	-10.82	0.002	-3.83E-04	-12.8	1.4	
15	13.20	-11.86	0.002	-3.82E-04	-15.6	-2.1	
		14.15	0.002	-3.82E-04	-15.6	-2.1	
16	12.60	10.98	0.002	-3.30E-04	-8.1	-8.9	
17	12.00	7.69	0.002	-2.33E-04	-2.5	-11.7	
18	11.40	4.68	0.002	-1.23E-04	1.2	-11.8	
19	10.80	2.21	0.002	-2.04E-05	3.3	-10.2	
20	10.20	0.38	0.002	6.40E-05	4.1	-7.8	
21	9.60	-0.83	0.002	1.25E-04	3.9	-5.3	

Run ID. East Terrace S2.1 S2 East SLS1\_SLS | Sheet No.  
 Lincoln's Inn Fields, London WC2A 3TL | Date: 4-02-2016  
 East Terrace S2.1 Section 2 East | Checked :

Run ID. East Terrace S2.1 S2 East SLS1\_SLS | Sheet No.  
 Lincoln's Inn Fields, London WC2A 3TL | Date: 4-02-2016  
 East Terrace S2.1 Section 2 East | Checked :

(continued)

(continued)

Stage No.4 Excavate to elevation 17.11 on PASSIVE side

Stage No.4 Excavate to elevation 17.11 on PASSIVE side

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
22	9.00	-1.50	0.002	1.65E-04	3.2	-3.1	
23	8.40	-1.75	0.002	1.86E-04	2.2	-1.5	
24	7.80	-1.70	0.002	1.95E-04	1.2	-0.4	
25	7.40	-1.54	0.002	1.97E-04	0.6	-0.1	
26	7.00	-1.29	0.002	1.97E-04	-0.0	0.0	

Node no.	Y coord	Effective stresses					Total earth pressure	Soil stiffness coeff. kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
9	15.60	0.00	26.66	6.56	102.01	44.09	5473	
10	15.00	0.00	37.46	9.16	146.72	55.53	5473	
11	14.60	0.00	44.67	10.30	172.55	63.34	5473	
12	14.20	0.00	51.87	13.06	197.38	71.29	5473	
13	13.85	3.50	54.68	15.12	212.08	74.84	5473	
14	13.45	7.50	57.89	15.01	225.28	78.98	5473	
15	13.20	10.00	59.90	14.24	232.53	81.58	5473	
		Total>	69.90	19.57m	224.05	79.71	5018	
16	12.60	Total>	81.63	22.57m	251.16	93.60	5483	
17	12.00	Total>	93.36	25.57m	277.97	107.41	5949	
18	11.40	Total>	105.09	28.57m	303.17	120.97	6414	
19	10.80	Total>	116.84	31.57m	324.38	134.16	6880	
20	10.20	Total>	128.59	34.57m	346.45	146.94	7346	
21	9.60	Total>	140.35	37.57m	368.07	159.35	7811	
22	9.00	Total>	152.12	40.57m	391.05	171.44	8277	
23	8.40	Total>	163.89	43.57m	415.19	183.27	8742	
24	7.80	Total>	175.67	46.57m	438.42	194.92	9208	
25	7.40	Total>	183.53	48.58m	451.71	202.60	9518	
26	7.00	Total>	191.39	50.57m	466.61	210.24	9828	

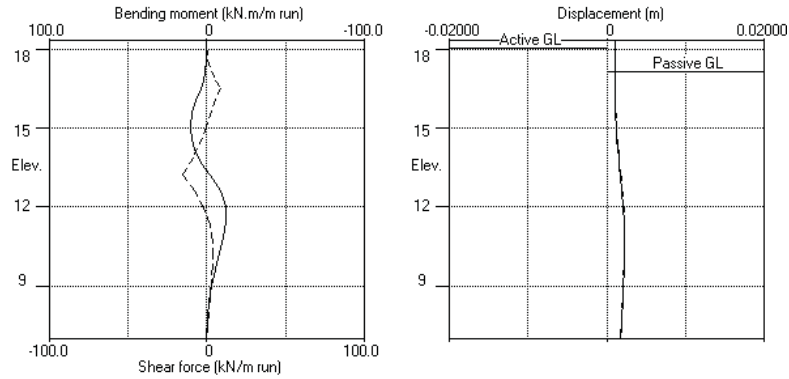
Note: 3.07a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Node no.	Y coord	Effective stresses					Total earth pressure	Soil stiffness coeff. kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	18.32	0.00	0.00	0.00	0.00	0.00	0.0	
2	18.02	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	0.00	0.00	2092	
3	17.98	Total>	0.60	0.18m	60.10	0.18a	2092	
4	17.55	Total>	8.24	2.34m	70.22	2.77	2092	
5	17.11	Total>	16.87	4.50m	77.04	7.19	2092	
6	16.81	Total>	23.52	6.04m	93.67	11.15	2092	
7	16.50	Total>	30.40	7.58m	110.10	15.41	2092	
		Total>	30.40	2.57	234.49	21.55	5267	
8	16.05	0.00	41.03	3.66	348.21	30.13	5267	
9	15.60	0.00	51.58	6.06	348.39	38.55	5267	
10	15.00	0.00	65.29	11.61	325.51	49.44	5267	
11	14.60	0.00	74.17	16.93	368.58	56.45	5267	
12	14.20	0.00	82.84	15.92	396.86	63.27	5267	
13	13.85	3.50	86.76	18.29	417.85	65.60	5267	
14	13.45	7.50	91.07	23.97	440.60	68.16	5267	
15	13.20	10.00	93.68	26.65	453.27	69.72	5267	
		Total>	103.68	24.08m	368.48	93.86	4881	
16	12.60	Total>	116.59	27.08m	369.03	104.58	5334	
17	12.00	Total>	129.22	30.08m	381.87	115.10	5787	
18	11.40	Total>	141.59	33.08m	378.26	125.64	6239	
19	10.80	Total>	153.76	36.08m	352.91	136.36	6692	
20	10.20	Total>	165.75	39.08m	399.86	147.32	7145	
21	9.60	Total>	177.61	42.08m	425.66	158.52	7598	
22	9.00	Total>	189.35	45.08m	419.14	169.94	8051	
23	8.40	Total>	200.99	48.08m	426.36	181.52	8504	
24	7.80	Total>	212.55	51.08m	464.48	193.22	8956	
25	7.40	Total>	220.22	53.08m	495.75	201.07	9258	
26	7.00	Total>	227.87	55.08m	510.41	208.95	9560	

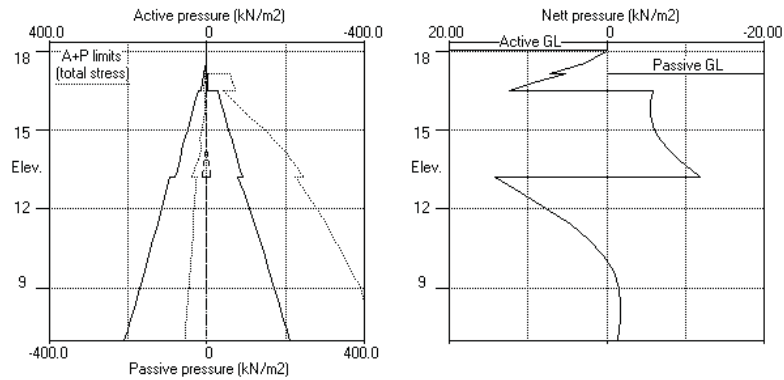
Node no.	Y coord	Effective stresses					Total earth pressure	Soil stiffness coeff. kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	18.32	0.00	0.00	0.00	0.00	0.00	0.0	
2	18.02	0.00	0.00	0.00	0.00	0.00	0.0	
3	17.98	0.00	0.00	0.00	0.00	0.00	0.0	
4	17.55	0.00	0.00	0.00	0.00	0.00	0.0	
5	17.11	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	59.92	1.88	2151	
6	16.81	Total>	5.23	1.54m	65.14	1.79	2151	
7	16.50	Total>	10.46	3.07m	70.36	3.07a	2151	
		Total>	0.00	10.46	1.92	41.16	27.46	5473
8	16.05	0.00	18.56	3.93	71.33	35.71	5473	

Units: kN,m

Stage No.4 Excav. to elev. 17.11 on PASSIVE side



Stage No.4 Excav. to elev. 17.11 on PASSIVE side



Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: Serviceability Limit State  
 All loads and soil strengths are unfactored

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**

Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	G.L.		Strut Elev.	Factor of Safety	Moment of equil.	Toe	
	Act.	Pass.				elev. =	Penetr
1	18.02	18.02	---	---	---	7.00	1.000
2	18.02	18.02	---	---	---	---	---
3	18.02	18.02	---	---	---	---	---
4	18.02	17.11	Cant.	16.885	7.35	---	---
5	18.02	17.11	18.32	20.668	n/a	---	---
6	18.02	17.11	---	---	---	---	---
7	18.02	17.11	---	---	---	---	---
8	18.02	13.45	18.32	3.606	n/a	---	---
9	18.02	13.45	---	---	---	---	---

All remaining stages have more than one strut - FoS calculation n/a

Legend: \*\*\* Result not found

Note: To obtain a Factor of Safety for the case of wall failing from right to left you should reverse the data (Ctrl+K) and re-analyse.



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 East Terrace S2.1 Section 2 East  
 Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 4-02-2016  
 Checked :

Run ID: East Terrace S2.1 S2 East SLS1\_SLS  
 Lincoln's Inn Fields, London WC2A 3TL  
 East Terrace S2.1 Section 2 East  
 Sheet No.  
 Date: 4-02-2016  
 Checked :

**Summary of results**

Units: kN,m

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement	Bending moment				Shear force				
			Calculated		Factored		Calculated		Factored		
		max. min.	max. min.	max. min.	max. min.	max. min.	max. min.	max. min.	max. min.		
		m	kN.m/m	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m	
1	18.32	0.001	-0.000	0	-0	0	-0	0	-24	0	-32
2	18.02	0.001	-0.000	0	-7	0	-10	0	-24	0	-32
3	17.98	0.001	0.000	0	-8	0	-11	0	-26	0	-36
4	17.55	0.002	0.000	0	-17	0	-24	1	-24	1	-33
5	17.11	0.003	0.000	1	-26	1	-35	3	-22	4	-30
6	16.81	0.004	0.000	2	-32	3	-43	5	-21	7	-28
7	16.50	0.004	0.000	4	-37	5	-50	8	-18	11	-25
8	16.05	0.005	0.000	7	-44	10	-59	8	-17	11	-22
9	15.60	0.006	0.000	9	-49	13	-67	7	-14	10	-19
10	15.00	0.007	0.000	10	-55	14	-74	18	-8	25	-11
11	14.60	0.007	0.000	10	-56	13	-76	28	-3	37	-4
12	14.20	0.007	0.000	12	-54	16	-73	38	-6	51	-8
13	13.85	0.007	0.000	27	-51	37	-69	48	-65	65	-87
14	13.45	0.008	0.000	4	-42	5	-57	29	-51	39	-68
15	13.20	0.008	0.000	0	-35	0	-47	31	-49	42	-66
16	12.60	0.009	0.000	0	-31	0	-42	24	-29	32	-40
17	12.00	0.010	0.000	0	-44	0	-59	17	-15	23	-20
18	11.40	0.010	0.000	3	-50	3	-68	10	-4	14	-5
19	10.80	0.011	0.000	7	-50	9	-67	5	0	7	0
20	10.20	0.011	0.000	8	-45	11	-61	11	0	15	0
21	9.60	0.010	0.000	7	-36	10	-49	14	-2	19	-3
22	9.00	0.010	0.000	6	-27	8	-37	15	-3	21	-4
23	8.40	0.009	0.000	3	-18	5	-24	16	-4	22	-5
24	7.80	0.008	0.000	1	-9	2	-12	16	-3	22	-4
25	7.40	0.008	0.000	0	-3	1	-4	11	-2	15	-2
26	7.00	0.007	0.000	0	0	0	0	0	-0	0	-0

**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force							
	Calculated		Factored		Calculated		Factored					
	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.				
	kN.m/m	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m				
1	1	15.00	-2	12.00	1	-3	1	16.50	-2	13.20	1	-3
2	No calculation at this stage											
3	4	15.00	-7	12.00	5	-10	3	16.50	-8	13.20	3	-11
4	10	15.00	-12	11.40	14	-16	8	16.50	-16	13.20	11	-21
5	5	14.60	-11	12.00	6	-15	8	16.05	-14	13.20	11	-19
6	No calculation at this stage											
7	No calculation at this stage											
8	8	10.20	-56	14.60	11	-76	31	13.20	-24	18.32	42	-32
9	No calculation at this stage											
10	No calculation at this stage											
11	8	10.20	-56	14.60	11	-76	31	13.20	-26	17.98	41	-36
12	No calculation at this stage											
13	No calculation at this stage											
14	No calculation at this stage											
15	27	13.85	-50	11.40	37	-68	48	13.85	-65	13.85	65	-87

**Maximum and minimum displacement at each stage**

Stage no.	Displacement				Stage description
	maximum	elev.	minimum	elev.	
	m				
1	0.000	11.40	0.000	18.32	Apply surcharge no.1 at elev. 18.02
2	No calculation at this stage				
3	0.001	10.80	-0.000	18.32	Apply surcharge no.4 at elev. 18.02
4	0.002	10.80	0.000	18.32	Excav. to elev. 17.11 on PASSIVE side
5	0.002	10.80	-0.000	18.32	Install strut no.1 at elev. 18.32
6	No calculation at this stage				
7	No calculation at this stage				
8	0.007	13.85	-0.000	18.32	Excav. to elev. 13.45 on PASSIVE side
9	No calculation at this stage				
10	No calculation at this stage				
11	0.007	13.85	0.000	18.32	Install strut no.2 at elev. 13.85
12	No calculation at this stage				
13	No calculation at this stage				
14	No calculation at this stage				
15	0.011	10.80	0.000	18.32	Install strut no.3 at elev. 17.98
					Remove strut no.1 at elev. 18.32
					Change soil type 1 to soil type 5
					Change soil type 2 to soil type 6
					Change soil type 3 to soil type 7
					Change soil type 4 to soil type 8

Run ID: East Terrace S2.1 S2 East SLS1\_SLS | Sheet No.  
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**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

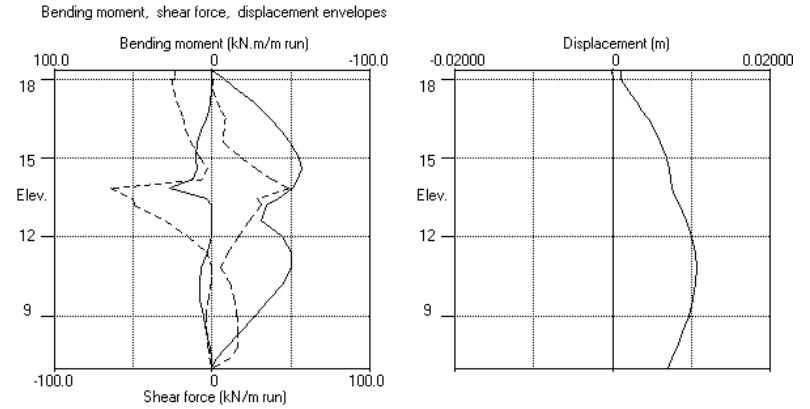
**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 at elev. 18.32			Strut no. 2 at elev. 13.85			Strut no. 3 at elev. 17.98		
	Calculated	Factored		Calculated	Factored		Calculated	Factored	
	kN per m run	kN per strut	kN per strut	kN per m run	kN per strut	kN per strut	kN per m run	kN per strut	kN per strut
5	10	50	68	---	---	---	---	---	---
8	24	119	160	---	---	---	---	---	---
11	---	---	---	slack	slack	slack	26	26	36
15	---	---	---	113	113	152	17	17	23

\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load. Force components are listed in the detailed results for individual stages.

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 Units: kN,m



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 East Terrace S2.1 Section 2 West | Checked :

Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Soil types	
		Active side	Passive side
1	18.02	1 Made Ground	1 Made Ground
2	16.50	2 Hackney Gravel	2 Hackney Gravel
3	13.20	3 London Clay	3 London Clay
4	3.50	4 London Clay	4 London Clay

**SOIL PROPERTIES**

No.	Description (Datum elev.)	Bulk density kN/m3	Young's Modulus Eh, kN/m2 (dEh/dy)	At rest coeff. Ko (dKo/dy)	Consol. state. NC/OC	Active limit Ka (Kac)	Passive limit Kp (Kpc)	Cohesion kN/m2 (dc/dy)
1	Made Ground	17.00	15000	0.500	NC	1.000	1.000	30.00u
2	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
3	London Clay (13.20)	19.50	35000	1.000	OC	1.000	1.000	70.00u
4	London Clay	19.50	87500	1.000	OC	1.000	1.000	175.0u
5	Made Ground Drained	17.00	9000	0.500	NC	0.490	2.040	0.0d
6	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
7	London Cl.. (13.20)	19.50	21000	1.000	OC	0.585	1.247	5.000d
8	London Clay Drained	19.50	52500	1.000	OC	0.585	1.247	5.000d

**Additional soil parameters associated with Ka and Kp**

No.	Description	parameters for Ka			parameters for Kp		
		Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1	Made Ground	0.00	0.000	0.00	0.00	0.000	0.00
2	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
3	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
5	Made Ground Drained	20.00	0.000	0.00	20.00	0.000	0.00
6	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
7	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00
8	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3  
 Initial water table elevation Active side 14.20 Passive side 14.20  
 Automatic water pressure balancing at toe of wall : No

Water profile no.	Active side				Passive side			
	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2	Point no.	Elev. m	Piezo elev. m	Water press. kN/m2
1	1	14.20	14.20	0.0	1	14.20	14.20	0.0
2	1	14.20	14.20	0.0	1	14.20	14.20	0.0

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 8.50  
 Maximum finite element length = 0.60 m  
 Youngs modulus of wall E = 2.0000E+07 kN/m2  
 Moment of inertia of wall I = 3.2000E-03 m4/m run  
 E.I = 64000 kN.m2/m run  
 Yield Moment of wall = Not defined

**STRUTS and ANCHORS**

Strut/anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre-stress /strut kN	Tension allowed
1	18.32	5.00	0.100000	2.000E+08	5.00	0.00	50.00	Yes
2	14.69	1.00	0.300000	2.000E+07	5.00	0.00	0	No
3	17.98	1.00	0.250000	2.000E+07	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length parallel to wall	Width perpendicular to wall	Surcharge Near edge kN/m2	Surcharge Far edge kN/m2	Equiv. soil type	Partial factor/Category
1	Not defined							
2	Not defined							
3	13.45	-0.00(P)	20.00	20.00	7.50	=	0	1.00 -
4	14.00	4.00(A)	20.00	2.00	100.00	=	0	1.00 P/U

Note: A = Active side, P = Passive side  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.4 at elevation 14.00
2	Excavate to elevation 17.11 on PASSIVE side
3	Install strut or anchor no.1 at elevation 18.32
4	Excavate to elevation 14.29 on PASSIVE side
5	Install strut or anchor no.2 at elevation 14.69
6	Install strut or anchor no.3 at elevation 17.98
7	Remove strut or anchor no.1 at elevation 18.32
8	Change properties of soil type 1 to soil type 5 No analysis at this stage Ko pressures will not be reset
9	Change properties of soil type 2 to soil type 6 No analysis at this stage Ko pressures will not be reset
10	Change properties of soil type 3 to soil type 7 No analysis at this stage Ko pressures will not be reset
11	Change properties of soil type 4 to soil type 8 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: Serviceability Limit State  
 All loads and soil strengths are unfactored

Stability analysis:  
 Method of analysis - Burland-Potts  
 Factor on passive for calculating wall depth = 1.00  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Parameters for undrained strata:  
 Minimum equivalent fluid density = 5.00 kN/m3  
 Maximum depth of water filled tension crack = 0.00 m

Bending moment and displacement calculation:  
 Method - Subgrade reaction model using Influence Coefficients  
 Open Tension Crack analysis? - No  
 Non-linear Modulus Parameter (L) = 0 m

Boundary conditions:

Length of wall (normal to plane of analysis) = 1000.00 m

Width of excavation on active side of wall = 20.00 m

Width of excavation on passive side of wall = 12.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

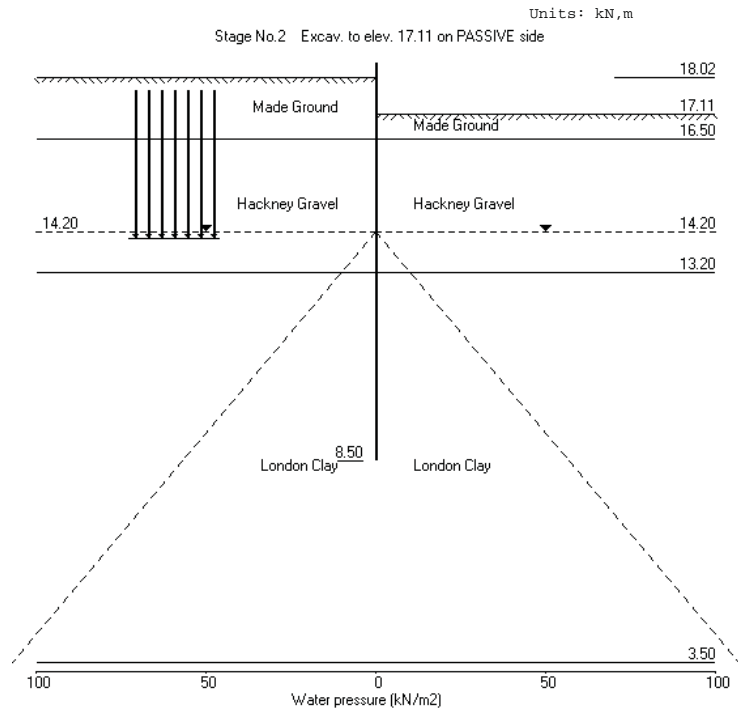
OUTPUT OPTIONS

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.4 at elev. 14.00	No	No	No
2	Excav. to elev. 17.11 on PASSIVE side	Yes	Yes	Yes
3	Install strut no.1 at elev. 18.32	No	No	No
4	Excav. to elev. 14.29 on PASSIVE side	No	No	No
5	Install strut no.2 at elev. 14.69	No	No	No
6	Install strut no.3 at elev. 17.98	No	No	No
7	Remove strut no.1 at elev. 18.32	No	No	No
8	Change soil type 1 to soil type 5	No	No	No
9	Change soil type 2 to soil type 6	No	No	No
10	Change soil type 3 to soil type 7	No	No	No
11	Change soil type 4 to soil type 8	No	No	No
*	Summary output	Yes	-	Yes

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 Data filename/Run ID: East Terrace S2.1 S2 West SLS1\_SLS Amended 080216  
 Lincoln's Inn Fields, London WC2A 3TL | Date: 9-02-2016  
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Units: kN,m

Stage No. 2 Excavate to elevation 17.11 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**  
 Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	G.L. Act.	G.L. Pass.	Strut Elev.	Factor of Safety	Moment of equilib. at elev.	Toe elev. for FoS = 1.000	
						Toe elev.	Wall Penetration
2	18.02	17.11	Cant.	17.805	8.81	***	***

Legend: \*\*\* Result not found

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**  
**Analysis options**

Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	18.32	0.00	0.001	1.70E-04	0.0	-0.0	
2	18.02	0.00	0.001	1.70E-04	0.0	0.0	
3	17.98	0.18	0.001	1.70E-04	0.0	0.0	
4	17.55	2.34	0.001	1.69E-04	0.5	0.1	
5	17.11	5.79	0.001	1.67E-04	2.3	0.7	
		3.80	0.001	1.67E-04	2.3	0.7	
6	16.81	6.64	0.001	1.61E-04	3.9	1.6	
7	16.50	8.16	0.001	1.49E-04	6.2	3.1	
		-4.78	0.001	1.49E-04	6.2	3.1	
8	16.05	-4.09	0.001	1.19E-04	4.2	5.4	
9	15.60	-3.61	0.001	7.62E-05	2.5	6.9	
10	15.15	-3.40	0.001	2.44E-05	0.9	7.7	
11	14.69	-3.51	0.001	-3.01E-05	-0.7	7.7	
12	14.29	-3.87	0.001	-7.65E-05	-2.2	7.1	
13	14.20	-3.98	0.001	-8.63E-05	-2.5	6.9	
14	14.00	-4.28	0.001	-1.07E-04	-3.4	6.3	
15	13.60	-5.04	0.001	-1.41E-04	-5.2	4.6	
16	13.20	-5.95	0.001	-1.62E-04	-7.4	2.2	
		5.96	0.001	-1.62E-04	-7.4	2.2	
17	12.60	4.35	0.001	-1.67E-04	-4.3	-1.2	
18	12.00	3.13	0.001	-1.47E-04	-2.1	-2.9	
19	11.40	2.26	0.001	-1.17E-04	-0.5	-3.5	
20	10.80	1.56	0.001	-8.59E-05	0.7	-3.3	
21	10.20	0.81	0.001	-5.90E-05	1.4	-2.5	



Run ID. East Terrace S2.1 S2 West SLS1\_SLS Amended 080216 | Sheet No.  
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Run ID. East Terrace S2.1 S2 West SLS1\_SLS Amended 080216 | Sheet No.  
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 East Terrace S2.1 Section 2 West | Checked :

(continued)

Stage No.2 Excavate to elevation 17.11 on PASSIVE side

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
22	9.60	-0.15	0.001	-4.10E-05	1.6	-1.4	
23	9.05	-1.35	0.001	-3.29E-05	1.2	-0.5	
24	8.50	-2.91	0.001	-3.09E-05	-0.0	0.0	

Node no.	Y coord	Effective stresses					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	18.32	0.00	0.00	0.00	0.00	0.00	0.0	
2	18.02	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	0.00	0.00	2197	
3	17.98	Total>	0.60	0.18m	60.23	0.18	0.18a	
4	17.55	Total>	7.95	2.34m	70.44	2.34	2.34a	
5	17.11	Total>	15.30	4.50m	75.21	5.79	5.79	
6	16.81	Total>	20.53	6.04m	80.44	8.52	8.52	
7	16.50	Total>	25.76	7.58m	85.66	11.24	11.24	
			0.00	25.76	3.52	99.41	21.56	
8	16.05	0.00	33.85	6.17	130.71	30.00	5633	
9	15.60	0.00	41.96	8.41	161.31	38.33	5633	
10	15.15	0.00	50.15	11.98	193.00	46.62	5633	
11	14.69	0.00	58.34	15.65	224.77	54.76	5633	
12	14.29	0.00	65.54	15.66	251.06	61.79	5633	
13	14.20	0.00	67.16	13.13	256.49	63.35	5633	
14	14.00	2.00	68.76	0.89	232.18	64.81	5633	
15	13.60	6.00	71.98	0.00	234.67	67.64	5633	
16	13.20	10.00	75.38	0.00	253.67	70.43	5633	
		Total>	85.38	24.08m	234.31	81.06	5127	
17	12.60	Total>	97.91	27.08m	258.04	92.42	5602	
18	12.00	Total>	111.17	30.08m	284.71	104.33	6078	
19	11.40	Total>	124.95	33.08m	328.04	116.67	6554	
20	10.80	Total>	138.91	36.08m	380.51	129.19	7029	
21	10.20	Total>	152.77	39.08m	395.14	141.64	7505	
22	9.60	Total>	166.34	42.08m	445.00	153.85	7980	
23	9.05	Total>	178.44	44.83m	462.46	164.74	8416	
24	8.50	Total>	190.21	47.58m	416.14	175.28	8852	

Node no.	Y coord	Effective stresses					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	18.32	0.00	0.00	0.00	0.00	0.00	0.0	
2	18.02	0.00	0.00	0.00	0.00	0.00	0.0	
3	17.98	0.00	0.00	0.00	0.00	0.00	0.0	
4	17.55	0.00	0.00	0.00	0.00	0.00	0.0	
5	17.11	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	59.92	2.00	2281	
6	16.81	Total>	5.23	1.54m	65.14	1.88	2281	
7	16.50	Total>	10.46	3.07m	70.36	3.07	2281	
			0.00	10.46	1.92	41.15	26.34	
8	16.05	0.00	18.56	3.93	71.33	34.09	5912	
9	15.60	0.00	26.67	6.34	102.18	41.94	5912	
10	15.15	0.00	34.87	8.56	136.80	50.03	5912	
11	14.69	0.00	43.09	10.24	166.42	58.27	5912	
12	14.29	0.00	50.31	11.27	189.99	65.66	5912	

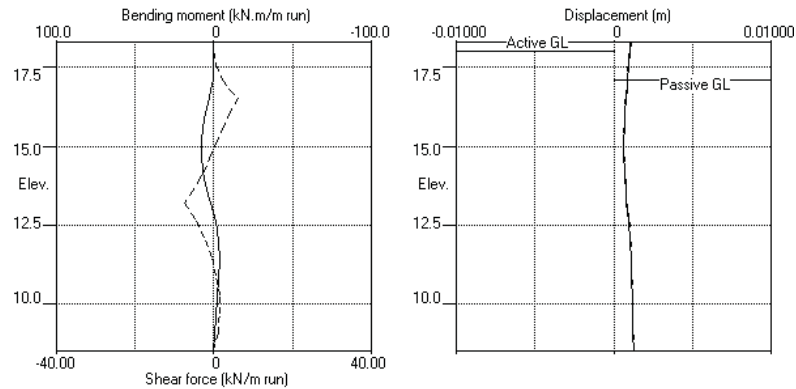
Stage No.2 Excavate to elevation 17.11 on PASSIVE side

Node no.	Y coord	Effective stresses					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
13	14.20	0.00	51.94	15.25	196.59	67.34	5912	
14	14.00	2.00	53.56	14.54	207.21	69.09	5912	
15	13.60	6.00	56.80	14.47	220.94	72.68	5912	
16	13.20	10.00	60.05	15.52	232.74	76.37	5912	
		Total>	70.05	19.57m	224.01	75.10	5323	
17	12.60	Total>	81.85	22.57m	251.16	88.07	5817	
18	12.00	Total>	93.67	25.57m	277.97	101.20	6310	
19	11.40	Total>	105.50	28.57m	303.16	114.40	6804	
20	10.80	Total>	117.36	31.57m	324.38	127.63	7298	
21	10.20	Total>	129.23	34.57m	346.45	140.83	7792	
22	9.60	Total>	141.12	37.57m	368.23	154.01	8286	
23	9.05	Total>	152.03	40.32m	388.94	166.08	8738	
24	8.50	Total>	162.96	43.07m	412.98	178.19	9191	

Note: 3.07a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.2 Excav. to elev. 17.11 on PASSIVE side



Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: Serviceability Limit State  
 All loads and soil strengths are unfactored

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**

Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

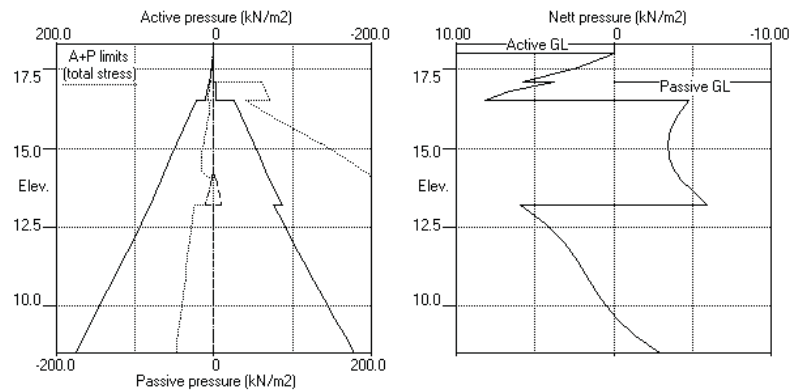
Stage No.	G.L. Act.	G.L. Pass.	Strut Elev.	Factor of Safety	Moment of equilib. at elev.	FoS	
						Toe elev.	Wall Penetr. -ation
1	18.02	18.02				8.50	1.000
2	18.02	17.11	Cant.	17.805	8.81	***	***
3	18.02	17.11	18.32	21.323	n/a	***	***
4	18.02	14.29	18.32	4.061	n/a	13.27	1.02
5	18.02	14.29				No analysis at this stage	

All remaining stages have more than one strut - FoS calculation n/a

Legend: \*\*\* Result not found

Note: To obtain a Factor of Safety for the case of wall failing from right to left you should reverse the data (Ctrl+K) and re-analyse.

Stage No.2 Excav. to elev. 17.11 on PASSIVE side



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 East Terrace S2.1 Section 2 West | Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**

Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement	Bending moment				Shear force				
			Calculated		Factored		Calculated		Factored		
			max.	min.	max.	min.	max.	min.	max.	min.	
		m	m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m		
1	18.32	0.001	-0.000	0	-0	0	-0	0	-23	0	-31
2	18.02	0.001	-0.000	0	-7	0	-9	0	-23	0	-31
3	17.98	0.001	-0.000	0	-8	0	-11	0	-26	0	-35
4	17.55	0.002	-0.000	0	-17	0	-23	1	-24	1	-32
5	17.11	0.003	-0.000	1	-26	1	-35	2	-22	3	-30
6	16.81	0.003	-0.000	2	-31	2	-42	4	-20	5	-27
7	16.50	0.004	-0.000	3	-36	4	-49	6	-18	8	-24
8	16.05	0.005	-0.000	5	-42	7	-57	6	-15	9	-20
9	15.60	0.005	-0.000	7	-47	9	-63	7	-11	9	-15
10	15.15	0.006	-0.000	8	-50	10	-67	7	-5	10	-7
11	14.69	0.006	0.000	8	-50	10	-67	16	-14	21	-19
12	14.29	0.006	0.000	7	-47	10	-63	13	-6	18	-8
13	14.20	0.006	0.000	7	-46	9	-62	15	-4	21	-5
14	14.00	0.006	0.000	6	-42	9	-57	19	-3	26	-5
15	13.60	0.007	0.000	5	-34	6	-45	24	-5	33	-7
16	13.20	0.007	0.000	2	-24	3	-32	26	-7	35	-10
17	12.60	0.007	0.000	1	-20	2	-27	19	-4	25	-6
18	12.00	0.007	0.000	1	-15	1	-21	11	-2	15	-3
19	11.40	0.007	0.000	4	-11	6	-15	7	-1	10	-1
20	10.80	0.007	0.000	6	-7	8	-9	6	-1	8	-1
21	10.20	0.007	0.000	5	-5	6	-7	3	-3	4	-3
22	9.60	0.007	0.000	3	-4	4	-5	2	-3	3	-5
23	9.05	0.007	0.000	1	-2	1	-3	3	-3	5	-3
24	8.50	0.007	0.000	0	-0	0	-0	0	-0	0	-0

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**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force							
	Calculated		Factored		Calculated		Factored					
	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.				
	kN.m/m	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m				
1	2	13.20	-0	10.20	2	-1	1	14.69	-1	11.40	1	-1
2	8	14.69	-4	11.40	10	-5	6	16.50	-7	13.20	8	-10
3	3	14.00	-9	16.81	4	-12	7	15.60	-10	18.32	9	-14
4	6	10.80	-50	15.15	8	-67	26	13.20	-23	18.32	35	-31
5	No calculation at this stage											
6	No calculation at this stage											
7	5	10.80	-50	14.69	7	-67	26	13.20	-26	17.98	35	-35
8	No calculation at this stage											
9	No calculation at this stage											
10	No calculation at this stage											
11	0	18.02	-26	15.60	0	-35	16	14.69	-19	17.98	21	-26

**Maximum and minimum displacement at each stage**

Stage no.	Displacement			Stage description	
	maximum	elev.	minimum		
	m	m	m		
1	0.000	8.50	-0.000	18.32	Apply surcharge no.4 at elev. 14.00
2	0.001	8.50	0.000	18.32	Excav. to elev. 17.11 on PASSIVE side
3	0.001	8.50	0.000	18.32	Install strut no.1 at elev. 18.32
4	0.006	14.20	0.000	18.32	Excav. to elev. 14.29 on PASSIVE side
5	No calculation at this stage				Install strut no.2 at elev. 14.69
6	No calculation at this stage				Install strut no.3 at elev. 17.98
7	0.006	14.00	0.000	18.32	Remove strut no.1 at elev. 18.32
8	No calculation at this stage				Change soil type 1 to soil type 5
9	No calculation at this stage				Change soil type 2 to soil type 6
10	No calculation at this stage				Change soil type 3 to soil type 7
11	0.007	11.40	0.000	18.32	Change soil type 4 to soil type 8

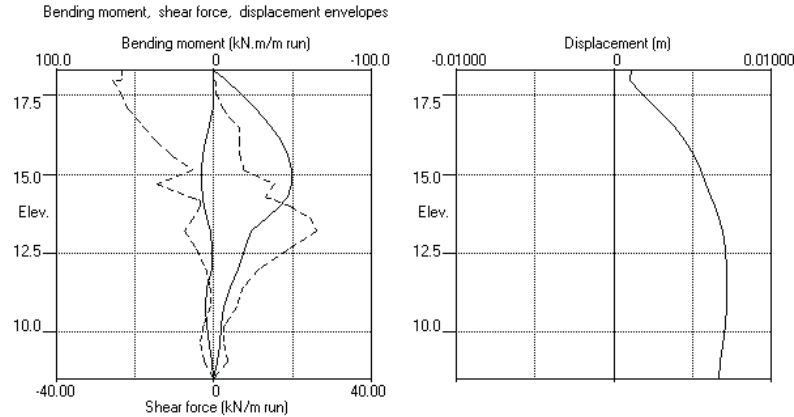
**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1		Strut no. 2		Strut no. 3	
	at elev. 18.32		at elev. 14.69		at elev. 17.98	
	--Calculated--	Factored	--Calculated--	Factored	--Calculated--	Factored
	kN per m run	kN per strut	kN per m run	kN per strut	kN per m run	kN per strut
3	10	50	68	---	---	---
4	23	116	157	---	---	---
7	---	---	---	slack	slack	slack
11	---	---	---	30	30	41
				26	26	35
				19	19	26

\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load. Force components are listed in the detailed results for individual stages.

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 Library S12.1 Section 1 East | Checked :

Units: kN,m

INPUT DATA

SOIL PROFILE

Stratum no.	Elevation of top of stratum	Soil types
1	21.18	Made Ground
2	16.50	Hackney Gravel
3	13.20	London Clay
4	3.50	London Clay

SOIL PROPERTIES

No.	Description (Datum elev.)	Bulk density (kN/m3)	Young's Modulus (Eh, kN/m2)	At rest coeff. (dKo/dy)	Consol. state. (Nu)	Active limit (Ka)	Passive limit (Kpc)	Cohesion (dc/dy)
1	Made Ground	17.00	15000	0.500	NC	1.000	1.000	30.00u
2	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
3	London Clay (13.20)	19.50	35000	1.000	OC	1.000	1.000	70.00u
4	London Clay	19.50	87500	1.000	OC	1.000	1.000	175.0u
5	Made Ground Drained	17.00	9000	0.500	NC	0.490	2.040	0.0d
6	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
7	London Cl.. (13.20)	19.50	21000	1.000	OC	0.585	1.247	5.000d
8	London Clay Drained	19.50	52500	1.000	OC	0.585	1.247	5.000d

Additional soil parameters associated with Ka and Kp

No.	Description	parameters for Ka			parameters for Kp		
		Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1	Made Ground	0.00	0.000	0.00	0.00	0.000	0.00
2	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
3	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
5	Made Ground Drained	20.00	0.000	0.00	20.00	0.000	0.00
6	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
7	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00
8	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00

GROUND WATER CONDITIONS

Density of water = 10.00 kN/m3  
 Initial water table elevation: Active side 14.40, Passive side 14.40  
 Automatic water pressure balancing at toe of wall : No

Water press. profile no.	Point no.	Active side			Passive side			
		Elev. (m)	Piezo elev. (m)	Water press. (kN/m2)	Point no.	Elev. (m)	Piezo elev. (m)	Water press. (kN/m2)
1	1	14.40	14.40	0.0	1	14.40	14.40	0.0
2	1	14.20	14.20	0.0	1	13.45	13.45	0.0

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 12.00  
 Maximum finite element length = 0.50 m  
 Youngs modulus of wall E = 2.0000E+07 kN/m2  
 Moment of inertia of wall I = 3.2000E-03 m4/m run  
 E.I = 64000 kN.m2/m run  
 Yield Moment of wall = Not defined

**Boundary conditions:**

Length of wall (normal to plane of analysis) = 1000.00 m  
 Width of excavation on active side of wall = 20.00 m  
 Width of excavation on passive side of wall = 20.00 m  
 Distance to rigid boundary on active side = 20.00 m  
 Distance to rigid boundary on passive side = 20.00 m

**STRUTS and ANCHORS**

Strut/ anchor no.	Elev. m	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre- stress /strut kN	Tension allowed
1	21.48	5.00	0.100000	2.000E+08	5.00	0.00	50.00	Yes
2	18.16	1.00	0.300000	2.000E+07	5.00	0.00	0	No
3	21.05	1.00	0.250000	2.000E+07	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev. m	Distance from wall	Length parallel to wall	Width perpend. to wall	Surcharge Near edge kN/m2	Surcharge Far edge kN/m2	Equiv. soil type	Partial factor/ Category
1	Not defined							
2	Not defined							
3	Not defined							
4	21.18	0.50(A)	20.00	20.00	5.00	=	0	1.00 Var

Note: A = Active side, P = Passive side

Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.4 at elevation 21.18
2	Excavate to elevation 20.10 on PASSIVE side
3	Install strut or anchor no.1 at elevation 21.48
4	Excavate to elevation 17.76 on PASSIVE side
5	Install strut or anchor no.2 at elevation 18.16
6	Install strut or anchor no.3 at elevation 21.05
7	Remove strut or anchor no.1 at elevation 21.48
8	Change properties of soil type 1 to soil type 5 No analysis at this stage Ko pressures will not be reset
9	Change properties of soil type 2 to soil type 6 No analysis at this stage Ko pressures will not be reset
10	Change properties of soil type 3 to soil type 7 No analysis at this stage Ko pressures will not be reset
11	Change properties of soil type 4 to soil type 8 Ko pressures will be reset

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: Serviceability Limit State  
 All loads and soil strengths are unfactored

**Stability analysis:**

Method of analysis - Burland-Potts  
 Factor on passive for calculating wall depth = 1.00  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

**Parameters for undrained strata:**

Minimum equivalent fluid density = 5.00 kN/m3  
 Maximum depth of water filled tension crack = 0.00 m

**Bending moment and displacement calculation:**

Method - Subgrade reaction model using Influence Coefficients  
 Open Tension Crack analysis? - No  
 Non-linear Modulus Parameter (L) = 0 m



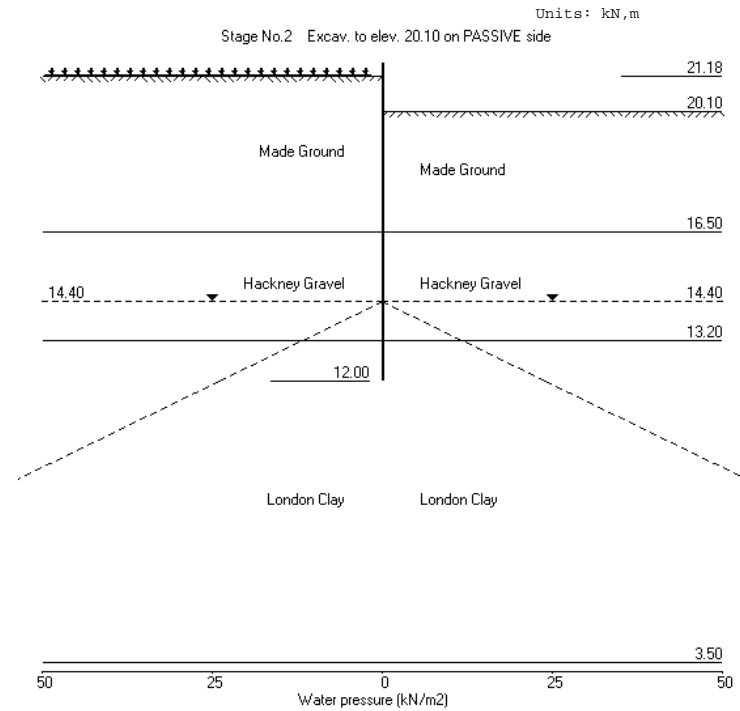
**OUTPUT OPTIONS**

Stage no.	Stage description	Displacement	Active, Bending mom.	Graph. Passive output
		Shear force	pressures	
1	Apply surcharge no.4 at elev. 21.18	No	No	No
2	Excav. to elev. 20.10 on PASSIVE side	Yes	Yes	Yes
3	Install strut no.1 at elev. 21.48	No	No	No
4	Excav. to elev. 17.76 on PASSIVE side	No	No	No
5	Install strut no.2 at elev. 18.16	No	No	No
6	Install strut no.3 at elev. 21.05	No	No	No
7	Remove strut no.1 at elev. 21.48	No	No	No
8	Change soil type 1 to soil type 5	No	No	No
9	Change soil type 2 to soil type 6	No	No	No
10	Change soil type 3 to soil type 7	No	No	No
11	Change soil type 4 to soil type 8	No	No	No
*	Summary output	Yes	-	Yes

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 Checked :

Units: kN,m  
 Stage No. 2 Excavate to elevation 20.10 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**  
 Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	G.L. Act.	G.L. Pass.	Strut Elev.	Factor of Safety	Moment at elev.	Toe elev.	Wall Penetration
2	21.18	20.10	Cant.	6.288	14.09	***	***

Legend: \*\*\* Result not found

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**  
 Analysis options

Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	21.48	0.00	0.004	6.94E-04	0.0	0.0	
2	21.18	0.00	0.004	6.94E-04	0.0	-0.0	
3	21.05	0.63	0.004	6.94E-04	0.0	0.0	
4	20.58	3.01	0.004	6.94E-04	0.9	0.2	
5	20.10	5.40	0.003	6.89E-04	2.9	1.1	
		-8.43	0.003	6.89E-04	2.9	1.1	
6	19.80	-5.99	0.003	6.82E-04	0.8	1.6	
7	19.50	-3.57	0.003	6.75E-04	-0.7	1.6	
8	19.00	-0.52	0.003	6.63E-04	-1.7	1.3	
9	18.58	2.05	0.002	6.58E-04	-1.4	0.5	
10	18.16	4.52	0.002	6.56E-04	-0.0	0.1	
11	17.76	6.81	0.002	6.54E-04	2.3	0.5	
12	17.38	8.93	0.002	6.47E-04	5.3	1.8	
13	17.00	10.98	0.001	6.28E-04	9.0	4.5	
14	16.50	13.48	0.001	5.70E-04	15.2	10.4	
		-19.43	0.001	5.70E-04	15.2	10.4	
15	16.00	-13.46	0.001	4.69E-04	6.9	15.5	
16	15.50	-8.85	0.001	3.41E-04	1.4	17.3	
17	15.00	-5.78	0.001	2.08E-04	-2.3	16.9	
18	14.70	-4.66	0.000	1.31E-04	-3.9	15.9	
19	14.40	-4.06	0.000	6.00E-05	-5.2	14.5	
20	14.10	-3.92	0.000	-4.03E-06	-6.4	12.8	
21	13.80	-4.19	0.000	-5.91E-05	-7.6	10.7	
22	13.50	-4.80	0.000	-1.03E-04	-8.9	8.2	

Stage No.2 Excavate to elevation 20.10 on PASSIVE side (continued)

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
23	13.20	-5.67	0.001	-1.35E-04	-10.5	5.3	
		11.83	0.001	-1.35E-04	-10.5	5.3	
24	12.85	10.18	0.001	-1.56E-04	-6.7	2.4	
25	12.50	8.32	0.001	-1.64E-04	-3.4	0.7	
26	12.00	5.37	0.001	-1.67E-04	0.0	-0.0	

Node no.	Y coord	Effective stresses				Earth pressure kN/m2	Total earth pressure kN/m2	Soil stiffness coeff. kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2			
1	21.48	0.00	0.00	0.00	0.00	0.00	0.0	
2	21.18	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	59.97	0.00	4104	
3	21.05	Total>	2.16	0.63m	62.39	0.63	4104	
4	20.58	Total>	11.47	3.01m	72.84	3.01	4104	
5	20.10	Total>	20.76	5.40m	83.09	5.40	4104	
6	19.80	Total>	26.33	6.90m	87.85	6.90	4104	
7	19.50	Total>	31.76	8.40m	92.87	8.40	4104	
8	19.00	Total>	40.63	10.90m	101.54	11.42	4104	
9	18.58	Total>	47.97	13.00m	108.60	16.31	4104	
10	18.16	Total>	55.25	15.10m	115.73	21.13	4104	
11	17.76	Total>	62.15	17.10m	122.53	25.67	4104	
12	17.38	Total>	68.67	19.00m	128.98	29.95	4104	
13	17.00	Total>	75.18	20.90m	135.44	34.18	4104	
14	16.50	Total>	83.71	23.95	143.96	39.64	4104	
			0.00	83.71	17.31	310.86	68.68	11473
15	16.00	0.00	92.72	19.13	330.72	80.52	11473	
16	15.50	0.00	101.72	21.00	376.07	91.70	11473	
17	15.00	0.00	110.70	22.57	420.68	102.17	11473	
18	14.70	0.00	116.08	25.14	423.69	108.10	11473	
19	14.40	0.00	121.46	29.62	490.13	113.79	11473	
20	14.10	3.00	123.84	28.68	481.29	116.25	11473	
21	13.80	6.00	126.21	25.87	449.09	118.53	11473	
22	13.50	9.00	128.58	27.47	476.49	120.64	11473	
23	13.20	12.00	130.95	29.78	495.97	122.63	11473	
		Total>	142.95	39.90m	316.49	138.31	9577	
24	12.85	Total>	149.73	41.65m	311.97	144.35	10095	
25	12.50	Total>	156.51	43.40m	314.66	150.29	10613	
26	12.00	Total>	166.20	45.90m	341.74	158.64	11354	

Node no.	Y coord	Effective stresses				Earth pressure kN/m2	Total earth pressure kN/m2	Soil stiffness coeff. kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2			
1	21.48	0.00	0.00	0.00	0.00	0.00	0.0	
2	21.18	0.00	0.00	0.00	0.00	0.00	0.0	
3	21.05	0.00	0.00	0.00	0.00	0.00	0.0	
4	20.58	0.00	0.00	0.00	0.00	0.00	0.0	
5	20.10	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	59.92	13.83	4581	
6	19.80	Total>	5.10	1.50m	65.01	12.89	4581	
7	19.50	Total>	10.20	3.00m	70.11	11.97	4581	
8	19.00	Total>	18.70	5.50m	78.61	11.94	4581	
9	18.58	Total>	25.84	7.60m	85.75	14.27	4581	

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Stage No.2 Excavate to elevation 20.10 on PASSIVE side

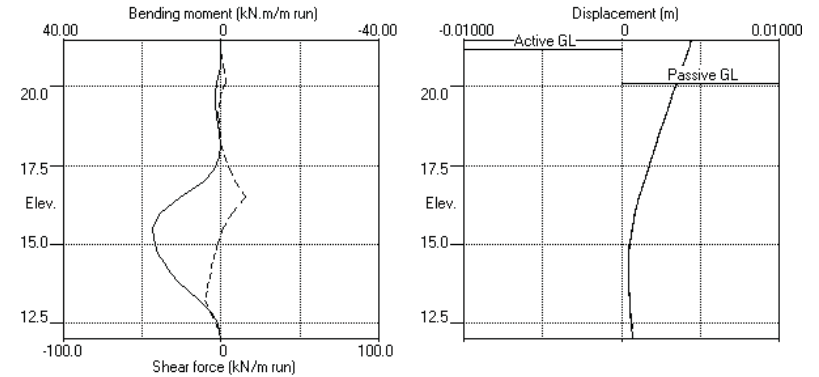
(continued)

Node no.	Y coord	Effective stresses					Total earth pressure	Soil stiffness
		Water press.	Vertic -al	Active limit	Passive limit	Earth pressure		
10	18.16	Total>	32.99	9.70m	92.89	16.61	16.61	4581
11	17.76	Total>	39.79	11.70m	99.69	18.86	18.86	4581
12	17.38	Total>	46.26	13.60m	106.15	21.01	21.01	4581
13	17.00	Total>	52.73	15.50m	112.61	23.20	23.20	4581
14	16.50	Total>	61.24	18.00m	121.12	26.16	26.16	4581
			0.00	61.24	13.31	216.68	88.11	12897
15	16.00		0.00	70.26	13.27	257.71	93.97	12897
16	15.50		0.00	79.29	16.49	299.73	100.56	12897
17	15.00		0.00	88.32	21.61	343.10	107.95	12897
18	14.70		0.00	93.74	19.85	358.15	112.76	12897
19	14.40		0.00	99.16	18.20	359.37	117.85	12897
20	14.10		3.00	101.59	24.09	385.48	120.17	12897
21	13.80		6.00	104.02	29.25	409.08	122.72	12897
22	13.50		9.00	106.45	27.08	407.87	125.44	12897
23	13.20		12.00	108.88	27.27	402.05	128.30	12897
		Total>	120.88	34.50m	256.74	126.48	126.48	10690
24	12.85	Total>	127.74	36.25m	281.65	134.17	134.17	11268
25	12.50	Total>	134.61	38.00m	308.39	141.97	141.97	11847
26	12.00	Total>	144.43	40.50m	331.04	153.26	153.26	12673

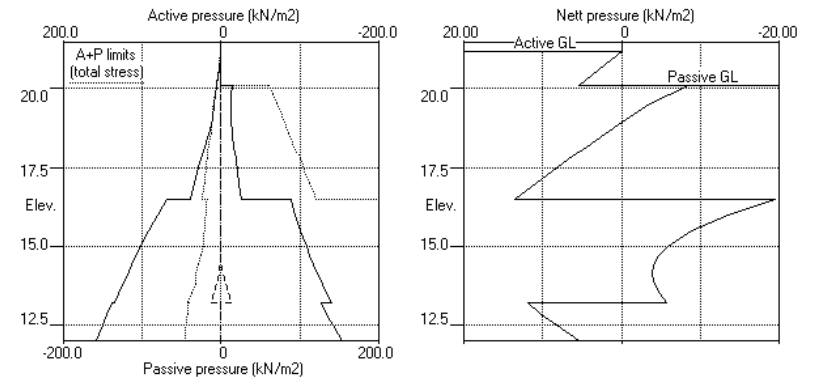
Note: 8.40a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Units: kN,m

Stage No.2 Excav. to elev. 20.10 on PASSIVE side



Stage No.2 Excav. to elev. 20.10 on PASSIVE side



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Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: Serviceability Limit State  
 All loads and soil strengths are unfactored

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**

Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	--- G.L. Act.	--- G.L. Pass.	Strut Elev.	Factor of Safety	Moment of equil.	Toe elev.	Wall Penetr
				FoS for toe elev. = 12.00		Toe elev. for FoS = 1.000	
1	21.18	21.18	---	---	---	---	---
2	21.18	20.10	Cant.	6.288	14.09	***	***
3	21.18	20.10	21.48	19.319	n/a	***	***
4	21.18	17.76	21.48	5.408	n/a	***	***
5	21.18	17.76		No analysis at this stage			
All remaining stages have more than one strut - FoS calculation n/a							

Legend: \*\*\* Result not found

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Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 5-02-2016  
 Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**  
 Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement				Bending moment				Shear force			
		Calculated		Factored		Calculated		Factored		Calculated		Factored	
		max.	min.	max.	min.	max.	min.	max.	min.	max.	min.	max.	min.
		m	m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m
1	21.48	0.004	0.000	0	-0	0	-0	0	-21	0	-28	0	-28
2	21.18	0.004	0.000	0	-6	0	-8	0	-21	0	-28	0	-28
3	21.05	0.004	0.000	0	-9	0	-12	1	-26	1	-36	1	-36
4	20.58	0.004	0.000	0	-17	0	-23	1	-24	1	-32	1	-32
5	20.10	0.004	0.000	1	-24	1	-33	3	-19	4	-26	4	-26
6	19.80	0.004	0.000	2	-28	2	-38	1	-16	1	-21	1	-21
7	19.50	0.005	0.000	2	-32	2	-43	0	-12	0	-16	0	-16
8	19.00	0.005	0.000	1	-35	2	-47	1	-7	1	-9	1	-9
9	18.58	0.005	0.000	1	-35	1	-47	7	-1	10	-2	10	-2
10	18.16	0.004	0.000	0	-33	0	-45	18	-7	24	-9	24	-9
11	17.76	0.004	0.000	0	-29	1	-39	14	0	19	0	19	0
12	17.38	0.004	0.000	2	-25	2	-34	20	0	27	0	27	0
13	17.00	0.004	0.000	4	-17	6	-23	28	0	38	0	38	0
14	16.50	0.003	0.000	10	0	14	0	42	0	57	0	57	0
15	16.00	0.003	0.000	20	0	27	0	29	0	39	0	39	0
16	15.50	0.002	0.000	30	0	40	0	15	0	21	0	21	0
17	15.00	0.002	0.000	34	0	46	0	5	-2	6	-3	6	-3
18	14.70	0.002	0.000	34	0	46	0	0	-4	0	-5	0	-5
19	14.40	0.002	0.000	33	0	45	0	0	-7	0	-9	0	-9
20	14.10	0.002	0.000	31	0	42	0	0	-11	0	-15	0	-15
21	13.80	0.002	0.000	27	0	37	0	0	-16	0	-21	0	-21
22	13.50	0.002	0.000	22	0	30	0	0	-21	0	-28	0	-28
23	13.20	0.002	0.000	15	0	21	0	0	-26	0	-36	0	-36
24	12.85	0.002	0.000	7	0	10	0	0	-19	0	-25	0	-25
25	12.50	0.003	0.000	2	0	3	0	0	-11	0	-14	0	-14
26	12.00	0.003	0.000	0	-0	0	-0	0	-0	0	-0	0	-0

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 Job No. J15050  
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 Date: 5-02-2016  
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**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	Calculated		Factored		Calculated		Factored	
	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.
	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m	kN/m
1	3 15.00	-2 18.16	4 -3	4 16.50	-2 13.20	5 -3		
2	17 15.50	-0 21.18	23 -0	15 16.50	-11 13.20	20 -14		
3	17 15.00	-9 19.50	23 -12	18 16.50	-11 13.20	24 -15		
4	34 14.70	-35 18.58	46 -47	41 16.50	-26 13.20	55 -36		
5	No calculation at this stage							
6	No calculation at this stage							
7	33 14.70	-33 18.58	45 -44	40 16.50	-26 13.20	54 -35		
8	No calculation at this stage							
9	No calculation at this stage							
10	No calculation at this stage							
11	34 14.70	-35 19.00	46 -47	42 16.50	-26 21.05	57 -36		

**Maximum and minimum displacement at each stage**

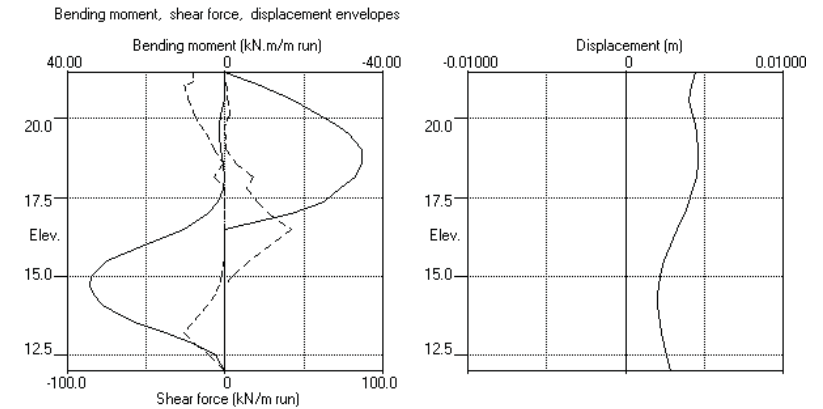
Stage no.	Displacement				Stage description
	maximum elev.	minimum elev.	maximum elev.	minimum elev.	
	m	m	m	m	
1	0.000 20.10	0.000 21.48	Apply surcharge no.4 at elev. 21.18		
2	0.004 21.48	0.000 21.48	Excav. to elev. 20.10 on PASSIVE side		
3	0.003 21.48	0.000 21.48	Install strut no.1 at elev. 21.48		
4	0.005 19.00	0.000 21.48	Excav. to elev. 17.76 on PASSIVE side		
5	No calculation at this stage				Install strut no.2 at elev. 18.16
6	No calculation at this stage				Install strut no.3 at elev. 21.05
7	0.004 19.00	0.000 21.48	Remove strut no.1 at elev. 21.48		
8	No calculation at this stage				Change soil type 1 to soil type 5
9	No calculation at this stage				Change soil type 2 to soil type 6
10	No calculation at this stage				Change soil type 3 to soil type 7
11	0.005 19.00	0.000 21.48	Change soil type 4 to soil type 8		

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1 at elev. 21.48		Strut no. 2 at elev. 18.16		Strut no. 3 at elev. 21.05	
	Calculated	Factored	Calculated	Factored	Calculated	Factored
	kN per m run	kN per strut	kN per m run	kN per strut	kN per m run	kN per strut
3	10	50	68			
4	21	103	139			
7			slack	slack	slack	slack
11			25	25	34	34

\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load. Force components are listed in the detailed results for individual stages.

Units: kN,m



Units: kN,m

**INPUT DATA**

**SOIL PROFILE**

Stratum no.	Elevation of top of stratum	Active side	Soil types	Passive side
1	21.18	1	Made Ground	1 Made Ground
2	16.50	2	Hackney Gravel	2 Hackney Gravel
3	13.20	3	London Clay	3 London Clay
4	3.50	4	London Clay	4 London Clay

**SOIL PROPERTIES**

No.	Description	Bulk density kN/m3	Young's Modulus Eh, kN/m2	At rest coeff. Ko	Consol. state NC/OC	Active limit Ka	Passive limit Kp	Cohesion kN/m2
1	Made Ground	17.00	15000	0.500	NC	1.000	1.000	30.00u
2	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
3	London Clay ( 13.20 )	19.50	35000	1.000	OC	1.000	1.000	70.00u
4	London Clay	19.50	87500	1.000	OC	1.000	1.000	175.0u
5	Made Ground Drained	17.00	9000	0.500	NC	0.490	2.040	0.0d
6	Hackney Gravel	18.00	60000	1.000	OC	0.260	3.852	
7	London Cl.. ( 13.20 )	19.50	21000	1.000	OC	0.585	1.247	5.000d
8	London Clay Drained	19.50	52500	1.000	OC	0.585	1.247	5.000d

**Additional soil parameters associated with Ka and Kp**

No.	Description	parameters for Ka			parameters for Kp		
		Soil friction angle	Wall adhesion coeff.	Back-fill angle	Soil friction angle	Wall adhesion coeff.	Back-fill angle
1	Made Ground	0.00	0.000	0.00	0.00	0.000	0.00
2	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
3	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
4	London Clay	0.00	-0.674	0.00	0.00	-0.674	0.00
5	Made Ground Drained	20.00	0.000	0.00	20.00	0.000	0.00
6	Hackney Gravel	36.00	0.000	0.00	36.00	0.000	0.00
7	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00
8	London Clay Drained	23.00	-0.674	0.00	23.00	-0.674	0.00

**GROUND WATER CONDITIONS**

Density of water = 10.00 kN/m3  
 Initial water table elevation Active side 14.40 Passive side 14.40

Automatic water pressure balancing at toe of wall : No

Water profile no.	Active side			Passive side		
	Point no.	Elev. m	Piezo elev. kN/m2	Point no.	Elev. m	Piezo elev. kN/m2
1	1	14.40	14.40	1	14.40	14.40
2	1	14.20	14.20	1	13.45	13.45

**WALL PROPERTIES**

Type of structure = Fully Embedded Wall  
 Elevation of toe of wall = 12.00  
 Maximum finite element length = 0.50 m  
 Youngs modulus of wall E = 2.0000E+07 kN/m2  
 Moment of inertia of wall I = 3.2000E-03 m4/m run  
 Yield Moment of wall = Not defined  
 E.I = 64000 kN.m2/m run

**STRUTS and ANCHORS**

Strut/anchor no.	Elev.	Strut spacing m	X-section area of strut sq.m	Youngs modulus kN/m2	Free length m	Inclin -ation (degs)	Pre-stress /strut kN	Tension allowed
1	21.48	5.00	0.100000	2.000E+08	5.00	0.00	50.00	Yes
2	16.74	1.00	0.300000	2.000E+07	5.00	0.00	0	No
3	19.58	1.00	0.250000	2.000E+07	5.00	0.00	0	No

**SURCHARGE LOADS**

Surch -arge no.	Elev.	Distance from wall	Length to wall	Width parallel to wall	Surcharge Near edge	Surcharge Far edge	Equiv. soil type	Partial factor/Category
1	Not defined							
2	Not defined							
3	Not defined							
4	21.18	0.50(A)	20.00	20.00	5.00	=	0	1.00 Var

Note: A = Active side, P = Passive side  
 Limit State Categories P/U = Permanent Unfavourable  
 P/F = Permanent Favourable  
 Var = Variable (unfavourable)

**CONSTRUCTION STAGES**

Construction stage no.	Stage description
1	Apply surcharge no.4 at elevation 21.18
2	Excavate to elevation 20.10 on PASSIVE side
3	Install strut or anchor no.1 at elevation 21.48
4	Excavate to elevation 16.34 on PASSIVE side
5	Install strut or anchor no.2 at elevation 16.74
6	Install strut or anchor no.3 at elevation 19.58
7	Remove strut or anchor no.1 at elevation 21.48
8	Change properties of soil type 1 to soil type 5 No analysis at this stage Ko pressures will not be reset
9	Change properties of soil type 2 to soil type 6 No analysis at this stage Ko pressures will not be reset
10	Change properties of soil type 3 to soil type 7 No analysis at this stage Ko pressures will not be reset
11	Change properties of soil type 4 to soil type 8 Ko pressures will be reset
12	Remove surcharge no.4 at elevation 21.18

**FACTORS OF SAFETY and ANALYSIS OPTIONS**

Limit State options: Serviceability Limit State  
 All loads and soil strengths are unfactored

**Stability analysis:**

Method of analysis - Burland-Potts  
 Factor on passive for calculating wall depth = 1.00  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Parameters for undrained strata:  
 Minimum equivalent fluid density = 5.00 kN/m3  
 Maximum depth of water filled tension crack = 0.00 m

**Bending moment and displacement calculation:**

Method - Subgrade reaction model using Influence Coefficients  
 Open Tension Crack analysis? - No  
 Non-linear Modulus Parameter (L) = 0 m

Boundary conditions:

Length of wall (normal to plane of analysis) = 1000.00 m

Width of excavation on active side of wall = 20.00 m

Width of excavation on passive side of wall = 20.00 m

Distance to rigid boundary on active side = 20.00 m

Distance to rigid boundary on passive side = 20.00 m

OUTPUT OPTIONS

Stage no.	Stage description	Displacement Bending mom. Shear force	Active, Passive pressures	Graph. output
1	Apply surcharge no.4 at elev. 21.18	No	No	No
2	Excav. to elev. 20.10 on PASSIVE side	Yes	Yes	Yes
3	Install strut no.1 at elev. 21.48	No	No	No
4	Excav. to elev. 16.34 on PASSIVE side	No	No	No
5	Install strut no.2 at elev. 16.74	No	No	No
6	Install strut no.3 at elev. 19.58	No	No	No
7	Remove strut no.1 at elev. 21.48	No	No	No
8	Change soil type 1 to soil type 5	No	No	No
9	Change soil type 2 to soil type 6	No	No	No
10	Change soil type 3 to soil type 7	No	No	No
11	Change soil type 4 to soil type 8	No	No	No
12	Remove surcharge no.4 at elev. 21.18	Yes	Yes	Yes
*	Summary output	Yes	-	Yes

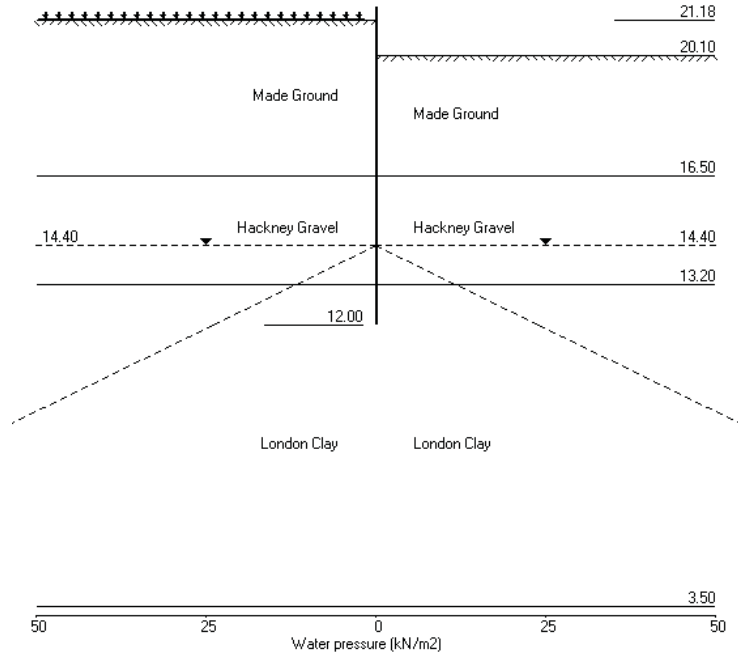
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 Library S12.1 Section 2 North

Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 5-02-2016  
 Checked :

Units: kN,m

Stage No.2 Excav. to elev. 20.10 on PASSIVE side



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 Library S12.1 Section 2 North

Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 5-02-2016  
 Checked :

Units: kN,m

Stage No. 2 Excavate to elevation 20.10 on PASSIVE side

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**

Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	G.L. Act.	G.L. Pass.	Strut Elev.	Factor of Safety	Moment of equil. at elev.	Toe elev.	Wall Penetration
2	21.18	20.10	Cant.	6.284	14.09	***	***

Legend: \*\*\* Result not found

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**  
 Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m <sup>2</sup>	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	21.48	0.00	0.004	6.87E-04	0.0	-0.0	
2	21.18	0.00	0.004	6.87E-04	0.0	0.0	
3	20.91	1.35	0.004	6.87E-04	0.2	0.0	
4	20.64	2.70	0.004	6.87E-04	0.7	0.1	
5	20.37	4.05	0.004	6.86E-04	1.6	0.5	
6	20.10	5.40	0.003	6.83E-04	2.9	1.1	
7	19.84	-8.44	0.003	6.83E-04	2.9	1.1	
8	19.58	-6.32	0.003	6.77E-04	1.0	1.6	
9	19.58	-4.22	0.003	6.71E-04	-0.4	1.6	
10	19.29	-1.90	0.003	6.64E-04	-1.3	1.3	
11	19.00	-0.53	0.003	6.59E-04	-1.6	1.0	
12	18.50	2.50	0.002	6.54E-04	-1.1	0.2	
13	18.00	5.41	0.002	6.53E-04	0.9	-0.1	
14	17.50	8.23	0.002	6.50E-04	4.3	1.0	
15	17.12	10.31	0.002	6.37E-04	7.8	3.3	
16	16.74	12.28	0.001	6.06E-04	12.1	7.0	
17	16.50	13.45	0.001	5.74E-04	15.2	10.2	
18	16.34	-19.52	0.001	5.74E-04	15.2	10.2	
19	15.92	-17.47	0.001	5.46E-04	12.2	12.4	
20	15.92	-12.67	0.001	4.53E-04	5.9	16.0	
21	15.50	-8.89	0.001	3.43E-04	1.4	17.4	
22	15.00	-5.81	0.001	2.09E-04	-2.3	16.9	
23	14.70	-4.68	0.000	1.32E-04	-3.9	16.0	
24	14.40	-4.07	0.000	6.12E-05	-5.2	14.6	



(continued)

(continued)

Stage No.2 Excavate to elevation 20.10 on PASSIVE side

Stage No.2 Excavate to elevation 20.10 on PASSIVE side

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
23	14.10	-3.92	0.000	-3.00E-06	-6.4	12.8	
24	13.80	-4.19	0.000	-5.82E-05	-7.6	10.7	
25	13.50	-4.79	0.000	-1.02E-04	-9.0	8.3	
26	13.20	-5.66	0.001	-1.34E-04	-10.5	5.4	
		11.84	0.001	-1.34E-04	-10.5	5.4	
27	12.85	10.20	0.001	-1.55E-04	-6.7	2.4	
28	12.50	8.34	0.001	-1.64E-04	-3.4	0.7	
29	12.00	5.40	0.001	-1.67E-04	0.0	-0.0	

Node no.	Y coord	Effective stresses					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
5	20.37	0.00	0.00	0.00	0.00	0.00	0.0	
6	20.10	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	59.92	13.84	4573	
7	19.84	Total>	4.42	1.30m	64.34	13.02	4573	
8	19.58	Total>	8.84	2.60m	68.75	12.22	4573	
9	19.29	Total>	13.77	4.05m	73.68	11.35	4573	
10	19.00	Total>	18.70	5.50m	78.61	11.94	4573	
11	18.50	Total>	27.20	8.00m	87.11	14.72	4573	
12	18.00	Total>	35.71	10.50m	95.61	17.52	4573	
13	17.50	Total>	44.22	13.00m	104.11	20.35	4573	
14	17.12	Total>	50.69	14.90m	110.57	22.52	4573	
15	16.74	Total>	57.16	16.80m	117.03	24.74	4573	
16	16.50	Total>	61.24	18.00m	121.11	26.17	4573	
			0.00	61.24	0.00	195.50	88.15	
17	16.34	0.00	64.13	13.37	232.82	89.96	12872	
18	15.92	0.00	71.71	15.90	269.52	95.00	12872	
19	15.50	0.00	79.29	16.64	296.81	100.58	12872	
20	15.00	0.00	88.32	21.61	343.10	107.96	12872	
21	14.70	0.00	93.74	19.85	358.15	112.77	12872	
22	14.40	0.00	99.16	18.20	359.37	117.85	12872	
23	14.10	3.00	101.59	24.09	385.48	120.17	12872	
24	13.80	6.00	104.02	29.25	409.08	122.71	12872	
25	13.50	9.00	106.45	27.08	407.87	125.43	12872	
26	13.20	12.00	108.88	27.27	402.05	128.29	12872	
		Total>	120.88	34.50m	256.74	126.48	10670	
27	12.85	Total>	127.74	36.25m	281.65	134.16	11247	
28	12.50	Total>	134.61	38.00m	308.39	141.96	11825	
29	12.00	Total>	144.43	40.50m	331.04	153.24	12650	

Note: 9.45a Soil pressure at active limit  
 123.45p Soil pressure at passive limit

Node no.	Y coord	ACTIVE side					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	21.48	0.00	0.00	0.00	0.00	0.00	0.0	
2	21.18	0.00	0.00	0.00	0.00	0.00	0.0	
		Total>	0.00	0.00	59.88	0.00a	4099	
3	20.91	Total>	4.84	1.35m	64.16	1.35a	4099	
4	20.64	Total>	10.22	2.70m	71.64	2.70a	4099	
5	20.37	Total>	15.59	4.05m	78.87	4.05a	4099	
6	20.10	Total>	20.76	5.40m	82.76	5.40a	4099	
7	19.84	Total>	25.60	6.70m	87.19	6.70a	4099	
8	19.58	Total>	30.32	8.00m	91.46	8.00a	4099	
9	19.29	Total>	35.51	9.45m	96.55	9.45a	4099	
10	19.00	Total>	40.63	10.90m	101.48	11.41a	4099	
11	18.50	Total>	49.36	13.40m	109.96	17.22a	4099	
12	18.00	Total>	58.01	15.90m	118.45	22.94a	4099	
13	17.50	Total>	66.61	18.40m	126.96	28.58a	4099	
14	17.12	Total>	73.12	20.30m	133.40	32.83a	4099	
15	16.74	Total>	79.62	24.27	139.87	37.02a	4099	
16	16.50	Total>	83.71	24.16	143.95	39.63a	4099	
			0.00	83.71	18.88	270.49	68.64	
17	16.34	0.00	86.60	17.76	315.59	72.49	11458	
18	15.92	0.00	94.16	19.09	341.19	82.33	11458	
19	15.50	0.00	101.72	21.11	379.68	91.68	11458	
20	15.00	0.00	110.70	22.57	420.68	102.15	11458	
21	14.70	0.00	116.08	25.14	423.69	108.09	11458	
22	14.40	0.00	121.46	29.62	490.13	113.78	11458	
23	14.10	3.00	123.84	28.68	481.29	116.25	11458	
24	13.80	6.00	126.21	25.87	449.09	118.53	11458	
25	13.50	9.00	128.58	27.47	476.49	120.64	11458	
26	13.20	12.00	130.95	29.78	495.97	122.63	11458	
		Total>	142.95	39.90m	316.49	138.32	9565	
27	12.85	Total>	149.73	41.65m	311.97	144.36	10083	
28	12.50	Total>	156.51	43.40m	314.66	150.29	10601	
29	12.00	Total>	166.20	45.90m	341.74	158.65	11340	

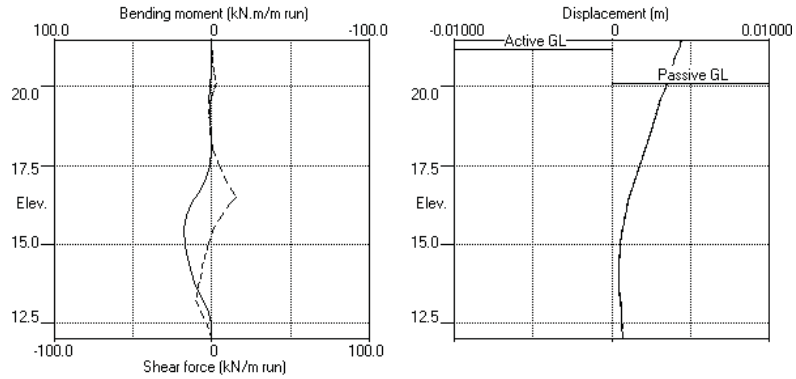
Node no.	Y coord	PASSIVE side					Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al kN/m2	Active limit kN/m2	Passive limit kN/m2	Earth pressure kN/m2		
1	21.48	0.00	0.00	0.00	0.00	0.00	0.0	
2	21.18	0.00	0.00	0.00	0.00	0.00	0.0	
3	20.91	0.00	0.00	0.00	0.00	0.00	0.0	
4	20.64	0.00	0.00	0.00	0.00	0.00	0.0	

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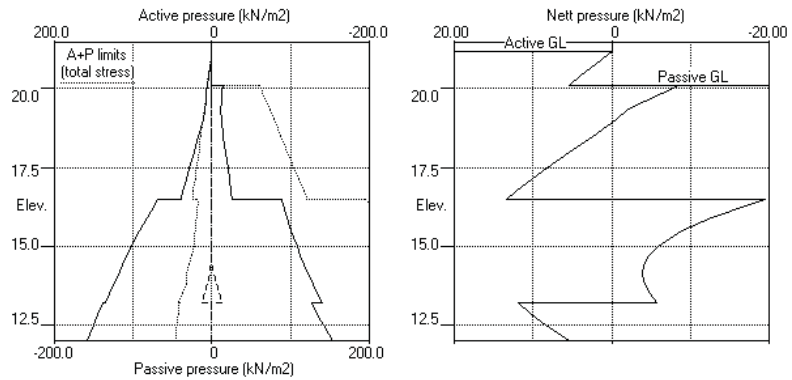
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Stage No.2 Excav. to elev. 20.10 on PASSIVE side



Stage No.2 Excav. to elev. 20.10 on PASSIVE side

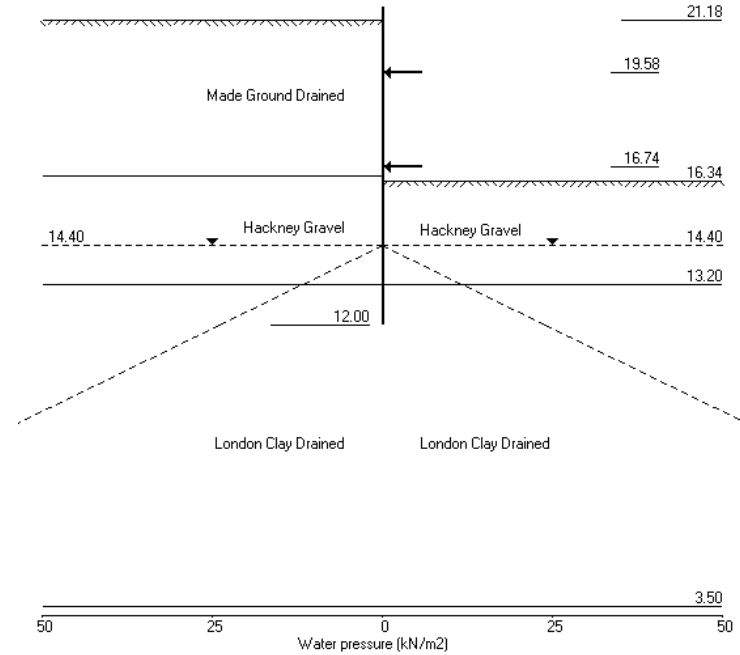


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Stage No.12 Remove surcharge no.4 at elev. 21.18



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 Library S12.1 Section 2 North | Checked :

Units: kN,m  
 Stage No. 12 Remove surcharge no.4 at elevation 21.18

Stage No.12 Remove surcharge no.4 at elevation 21.18

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**  
 Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
25	13.50	-44.06	0.003	7.80E-04	-25.0	31.9	
26	13.20	-40.36	0.003	6.53E-04	-37.7	22.5	
		31.25	0.003	6.53E-04	-37.7	22.5	
27	12.85	32.75	0.003	5.61E-04	-26.5	11.2	
28	12.50	30.39	0.003	5.19E-04	-15.4	3.9	
29	12.00	31.23	0.002	5.04E-04	0.0	0.0	
At elev. 19.58 Strut force =					65.3 kN/strut =	65.3 kN/m run	
At elev. 16.74 The strut is slack							

FoS for toe | Toe elev. for  
 elev. = 12.00 | FoS = 1.000

Stage No.	G.L. Act.	G.L. Pass.	Strut Elev.	Factor of Safety	Moment at elev.	Toe elev. Penetration	Wall Penetration
12	21.18	16.34		More than one strut			

Node Y ----- ACTIVE side -----

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**  
**Analysis options**

Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Node no.	Y coord	Effective stresses				Earth pressure kN/m2	Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al limit kN/m2	Active limit kN/m2	Passive limit kN/m2			
1	21.48	0.00	0.00	0.00	0.00	0.00	0.00	
2	21.18	0.00	0.00	0.00	0.00	0.00	0.00	
3	20.91	0.00	4.59	2.16	9.20	2.86	4369	
4	20.64	0.00	9.18	4.44	18.58	5.28	4369	
5	20.37	0.00	13.77	6.69	27.93	8.07	4369	
6	20.10	0.00	18.36	8.94	37.31	10.15	4369	
7	19.84	0.00	22.78	11.10	46.33	12.48	4369	
8	19.58	0.00	27.20	13.27	55.35	14.68	1039	
9	19.29	0.00	32.13	15.69	65.40	17.05	1039	
10	19.00	0.00	37.06	18.11	75.46	19.47	1039	
11	18.50	0.00	45.56	22.27	92.79	23.62	1039	
12	18.00	0.00	54.06	26.44	110.13	27.76	1039	
13	17.50	0.00	62.56	30.60	127.47	31.90	1039	
14	17.12	0.00	69.02	33.77	140.64	35.05	1039	
15	16.74	0.00	75.48	36.94	153.82	38.25	1039	
16	16.50	0.00	79.56	38.94	162.14	40.29	1039	
		0.00	79.56	16.92	268.46	24.39	6927	
17	16.34	0.00	82.44	19.00	298.37	28.91	6927	
18	15.92	0.00	90.00	22.56	330.56	41.20	6927	
19	15.50	0.00	97.56	24.71	356.13	53.84	6927	
20	15.00	0.00	106.56	26.02	395.73	68.83	6927	
21	14.70	0.00	111.96	28.45	433.94	77.55	6927	
22	14.40	0.00	117.36	31.24	467.02	85.93	6927	
23	14.10	3.00	119.76	31.63	456.49	90.91	6927	
24	13.80	6.00	122.16	30.83	479.75	95.47	6927	
25	13.50	9.00	124.56	30.83	440.76	99.45	6927	
26	13.20	12.00	126.96	31.76	361.05	103.04	6927	
		12.00	126.96	51.57	181.95	98.38	2424	
27	12.85	15.50	130.28	51.84	202.53	112.07	2556	
28	12.50	19.00	133.61	53.87	245.52	115.43	2687	
29	12.00	24.00	138.36	57.25	269.76	120.32	2874	

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**  
 Calculated Bending Moments and Strut Forces are to be multiplied by a factor of 1.35 to obtain values for structural design. See summary for factored values.

Node no.	Y coord	Nett pressure kN/m2	Wall disp. m	Wall rotation rad.	Shear force kN/m	Bending moment kN.m/m	Strut forces kN/m
1	21.48	0.00	0.006	-7.98E-04	0.0	-0.0	
2	21.18	0.00	0.006	-7.98E-04	0.0	0.0	
3	20.91	2.86	0.006	-7.98E-04	0.4	0.0	
4	20.64	5.28	0.006	-7.99E-04	1.5	0.4	
5	20.37	8.07	0.006	-8.01E-04	3.3	0.9	
6	20.10	10.15	0.007	-8.08E-04	5.7	2.1	
7	19.84	12.48	0.007	-8.20E-04	8.7	4.0	
8	19.58	14.68	0.007	-8.42E-04	12.2	6.7	65.3
		14.68	0.007	-8.42E-04	-53.1	6.7	
9	19.29	17.05	0.007	-8.39E-04	-48.5	-8.0	
10	19.00	19.47	0.008	-7.73E-04	-43.2	-21.2	
11	18.50	23.62	0.008	-5.33E-04	-32.4	-40.2	
12	18.00	27.76	0.008	-1.68E-04	-19.5	-53.4	
13	17.50	31.90	0.008	2.73E-04	-4.6	-59.6	
14	17.12	35.05	0.008	6.25E-04	8.1	-59.0	
15	16.74	38.25	0.008	9.59E-04	22.0	-53.4	-0.0
16	16.50	40.29	0.007	1.14E-03	31.4	-47.0	
		24.39	0.007	1.14E-03	31.4	-47.0	
17	16.34	28.91	0.007	1.25E-03	35.7	-41.6	
18	15.92	13.49	0.007	1.47E-03	44.6	-24.8	
19	15.50	-3.37	0.006	1.57E-03	46.7	-5.7	
20	15.00	-23.07	0.005	1.53E-03	40.1	16.2	
21	14.70	-35.18	0.005	1.43E-03	31.4	26.9	
22	14.40	-47.66	0.004	1.29E-03	19.0	34.5	
23	14.10	-51.99	0.004	1.12E-03	4.0	38.0	
24	13.80	-48.66	0.004	9.43E-04	-11.1	37.5	

Node Y ----- PASSIVE side -----

Node no.	Y coord	Effective stresses				Earth pressure kN/m2	Total earth pressure kN/m2	Soil stiffness kN/m3
		Water press. kN/m2	Vertic -al limit kN/m2	Active limit kN/m2	Passive limit kN/m2			
1	21.48	0.00	0.00	0.00	0.00	0.00	0.00	
2	21.18	0.00	0.00	0.00	0.00	0.00	0.00	
3	20.91	0.00	0.00	0.00	0.00	0.00	0.00	
4	20.64	0.00	0.00	0.00	0.00	0.00	0.00	

Run ID: Library S13.1 S1 North SLS1\_SLS  
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 Library S12.1 Section 2 North

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Sheet No.  
 Job No. J15050  
 Made by : MC  
 Date: 5-02-2016  
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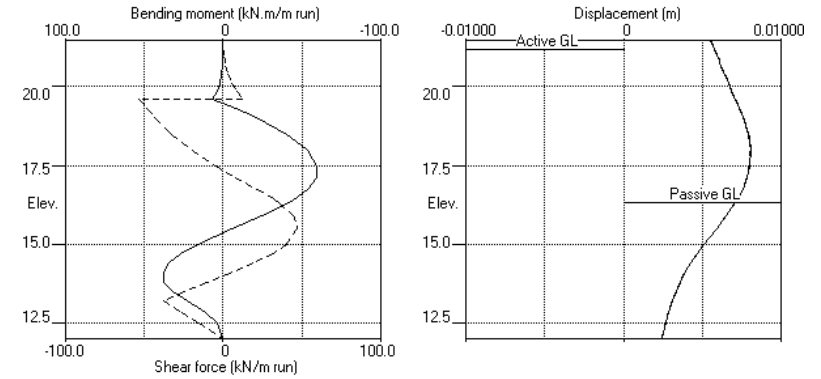
Stage No.12 Remove surcharge no.4 at elevation 21.18

(continued)

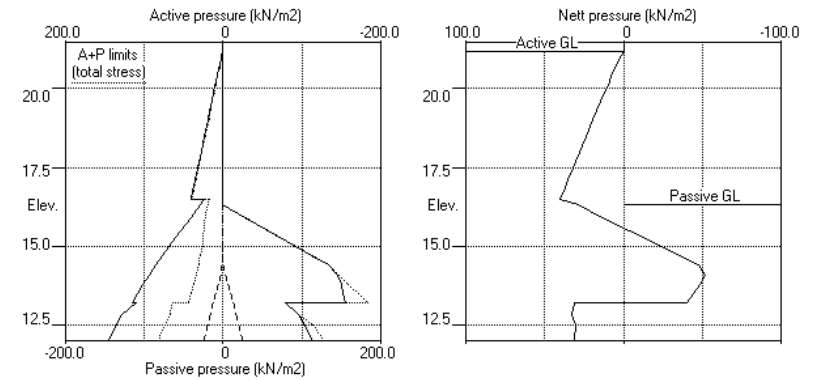
Node no.	Y coord	PASSIVE side					Total earth pressure kN/m <sup>2</sup>	Soil stiffness kN/m <sup>3</sup>
		Water press. kN/m <sup>2</sup>	Vertic -al kN/m <sup>2</sup>	Effective Active limit kN/m <sup>2</sup>	Effective Passive limit kN/m <sup>2</sup>	Earth pressure kN/m <sup>2</sup>		
5	20.37	0.00	0.00	0.00	0.00	0.00	0.0	
6	20.10	0.00	0.00	0.00	0.00	0.00	0.0	
7	19.84	0.00	0.00	0.00	0.00	0.00	0.0	
8	19.58	0.00	0.00	0.00	0.00	0.00	0.0	
9	19.29	0.00	0.00	0.00	0.00	0.00	0.0	
10	19.00	0.00	0.00	0.00	0.00	0.00	0.0	
11	18.50	0.00	0.00	0.00	0.00	0.00	0.0	
12	18.00	0.00	0.00	0.00	0.00	0.00	0.0	
13	17.50	0.00	0.00	0.00	0.00	0.00	0.0	
14	17.12	0.00	0.00	0.00	0.00	0.00	0.0	
15	16.74	0.00	0.00	0.00	0.00	0.00	0.0	
16	16.50	0.00	0.00	0.00	0.00	0.00	0.0	
17	16.34	0.00	0.00	0.00	0.00	0.00	0.0	
18	15.92	0.00	7.56	1.89	28.87	27.71	8699	
19	15.50	0.00	15.12	3.87	58.04	57.22	8699	
20	15.00	0.00	24.13	6.20	92.71	91.90	8699	
21	14.70	0.00	29.54	7.61	113.54	112.73	8699	
22	14.40	0.00	34.95	8.94	134.41	133.59	8699	
23	14.10	3.00	37.37	9.51	143.72	142.91	8699	
24	13.80	6.00	39.79	10.14	152.95	144.12	8699	
25	13.50	9.00	42.22	10.78	162.19	143.51	8699	
26	13.20	12.00	44.65	11.42	171.48	143.40	8699	
		12.00	44.65	13.73	67.43	67.13	3045	
27	12.85	15.50	48.02	15.46	79.91	79.32	3209	
28	12.50	19.00	51.41	18.06	94.18	85.04	3374	
29	12.00	24.00	56.26	20.70	103.26	89.09	3609	

Units: kN,m

Stage No.12 Remove surcharge no.4 at elev. 21.18



Stage No.12 Remove surcharge no.4 at elev. 21.18



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Sheet No.  
 Job No. J15050  
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 Date: 5-02-2016  
 Checked :

Units: kN,m

**Summary of results**

**LIMIT STATE PARAMETERS**

Limit State: Serviceability Limit State  
 All loads and soil strengths are unfactored

**STABILITY ANALYSIS of Fully Embedded Wall according to Burland-Potts method**

Factor of safety on nett available passive  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability

Stage No.	--- G.L. Act.	--- G.L. Pass.	Strut Elev.	Factor of Safety	Moment of equil.	Toe elev.	Wall Penetr
						12.00	1.000
1	21.18	21.18	---	---	---	---	---
2	21.18	20.10	Cant.	6.284	14.09	---	---
3	21.18	20.10	21.48	19.314	n/a	---	---
4	21.18	16.34	21.48	3.267	n/a	15.03	1.31
5	21.18	16.34		No analysis at this stage			

Conditions not suitable for FoS calc.  
 All remaining stages have more than one strut - FoS calculation n/a

Legend: \*\*\* Result not found

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 Checked :

Units: kN,m

**Summary of results**

**BENDING MOMENT and DISPLACEMENT ANALYSIS of Fully Embedded Wall**

**Analysis options**  
 Length of wall perpendicular to section = 1000.00m  
 Subgrade reaction model - Boussinesq Influence coefficients  
 Soil deformations are elastic until the active or passive limit is reached  
 Active limit pressures calculated by Wedge Stability  
 Passive limit pressures calculated by Wedge Stability  
 Open Tension Crack analysis - No

Rigid boundaries: Active side 20.00 from wall  
 Passive side 20.00 from wall

**Limit State: Serviceability Limit State**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Bending moment, shear force and displacement envelopes**

Node no.	Y coord	Displacement				Bending moment				Shear force			
		Calculated		Factored		Calculated		Factored		Calculated		Factored	
		max.	min.	max.	min.	max.	min.	max.	min.	max.	min.	max.	min.
		m	m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m	kN/m
1	21.48	0.006	0.000	0	-0	0	-0	0	-27	0	-37	0	-37
2	21.18	0.006	0.000	0	-8	0	-11	0	-27	0	-37	0	-37
3	20.91	0.006	0.000	0	-15	0	-21	0	-26	1	-35	0	-35
4	20.64	0.006	0.000	0	-22	1	-30	2	-25	2	-34	0	-34
5	20.37	0.007	0.000	1	-29	1	-39	4	-24	5	-32	0	-32
6	20.10	0.007	0.000	2	-35	3	-47	6	-23	8	-30	0	-30
7	19.84	0.007	0.000	4	-41	6	-55	9	-21	13	-28	0	-28
8	19.58	0.007	0.000	7	-46	10	-62	13	-55	18	-24	0	-24
9	19.29	0.007	0.000	1	-51	2	-69	0	-50	0	-67	0	-67
10	19.00	0.008	0.000	1	-55	1	-75	1	-44	1	-60	0	-60
11	18.50	0.008	0.000	0	-61	0	-82	2	-33	3	-45	0	-45
12	18.00	0.008	0.000	0	-63	0	-85	4	-20	6	-27	0	-27
13	17.50	0.008	0.000	1	-61	1	-82	8	-6	11	-7	0	-7
14	17.12	0.008	0.000	3	-60	4	-81	16	0	21	0	0	0
15	16.74	0.008	0.000	7	-54	9	-73	24	0	33	0	0	0
16	16.50	0.007	0.000	10	-48	14	-65	32	0	43	0	0	0
17	16.34	0.007	0.000	12	-42	17	-57	37	0	49	0	0	0
18	15.92	0.007	0.000	16	-25	22	-34	45	0	61	0	0	0
19	15.50	0.006	0.000	17	-8	23	-10	47	0	64	0	0	0
20	15.00	0.005	0.000	19	0	25	0	41	-2	55	-3	0	-3
21	14.70	0.005	0.000	29	0	39	0	32	-4	43	-5	0	-5
22	14.40	0.004	0.000	36	0	49	0	20	-5	27	-7	0	-7
23	14.10	0.004	0.000	39	0	53	0	5	-6	7	-9	0	-9
24	13.80	0.004	0.000	38	0	52	0	0	-12	0	-16	0	-16
25	13.50	0.003	0.000	33	0	44	0	0	-26	0	-35	0	-35
26	13.20	0.003	0.000	23	0	31	0	0	-38	0	-51	0	-51
27	12.85	0.003	0.000	12	0	16	0	0	-27	0	-37	0	-37
28	12.50	0.003	0.000	4	0	5	0	0	-16	0	-22	0	-22
29	12.00	0.003	0.000	0	-0	0	-0	0	0	0	0	0	0

Run ID: Library S13.1 S1 North SLS1\_SLS  
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 Date: 5-02-2016  
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**Summary of results (continued)**

Calculated Bending Moments and Strut Forces have been multiplied by a factor of 1.35 to obtain values for structural design.

**Maximum and minimum bending moment and shear force at each stage**

Stage no.	Bending moment				Shear force			
	Calculated		Factored		Calculated		Factored	
	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.	max. elev.	min. elev.
	kN.m/m	kN.m/m	kN.m/m	kN/m	kN/m	kN/m	kN/m	kN/m
1	3 15.00	-3 18.50	4 -3	4 16.50	-2 13.20	5 -3		
2	17 15.50	-0 18.00	23 -0	15 16.50	-11 13.20	20 -14		
3	17 15.00	-9 19.29	23 -13	18 16.50	-11 13.20	24 -15		
4	39 14.10	-63 18.00	53 -85	45 15.50	-38 13.20	61 -51		
5	No calculation at this stage							
6	No calculation at this stage							
7	35 14.10	-46 17.12	47 -62	42 15.50	-37 19.58	57 -50		
8	No calculation at this stage							
9	No calculation at this stage							
10	No calculation at this stage							
11	38 14.10	-61 17.50	52 -82	47 15.50	-55 19.58	64 -74		
12	38 14.10	-60 17.50	51 -80	47 15.50	-53 19.58	63 -72		

**Maximum and minimum displacement at each stage**

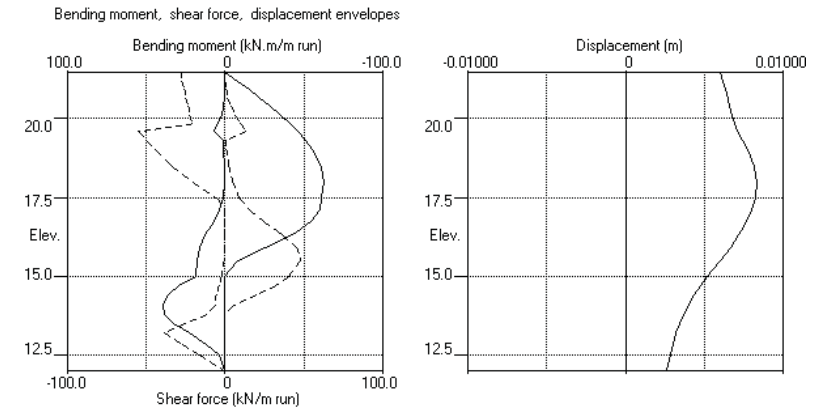
Stage no.	Displacement				Stage description
	maximum elev.	minimum elev.	maximum elev.	minimum elev.	
	m	m	m	m	
1	0.000 19.84	0.000 21.48	Apply surcharge no.4 at elev. 21.18		
2	0.004 21.48	0.000 21.48	Excav. to elev. 20.10 on PASSIVE side		
3	0.003 21.48	0.000 21.48	Install strut no.1 at elev. 21.48		
4	0.008 18.00	0.000 21.48	Excav. to elev. 16.34 on PASSIVE side		
5	No calculation at this stage				Install strut no.2 at elev. 16.74
6	No calculation at this stage				Install strut no.3 at elev. 19.58
7	0.008 18.00	0.000 21.48	Remove strut no.1 at elev. 21.48		
8	No calculation at this stage				Change soil type 1 to soil type 5
9	No calculation at this stage				Change soil type 2 to soil type 6
10	No calculation at this stage				Change soil type 3 to soil type 7
11	0.008 18.00	0.000 21.48	Change soil type 4 to soil type 8		
12	0.008 18.00	0.000 21.48	Remove surcharge no.4 at elev. 21.18		

**Strut forces at each stage (horizontal components)**

Stage no.	Strut no. 1			Strut no. 2			Strut no. 3		
	at elev. 21.48			at elev. 16.74			at elev. 19.58		
	Calculated	Factored		Calculated	Factored		Calculated	Factored	
	kN per m run	kN per strut	kN per strut	kN per m run	kN per strut	kN per strut	kN per m run	kN per strut	
3	10	50	68	---	---	---	---	---	
4	27	137	184	---	---	---	---	---	
7	---	---	---	slack	slack	slack	43	43	
11	---	---	---	0	0	0	68	68	
12	---	---	---	slack	slack	slack	65	65	

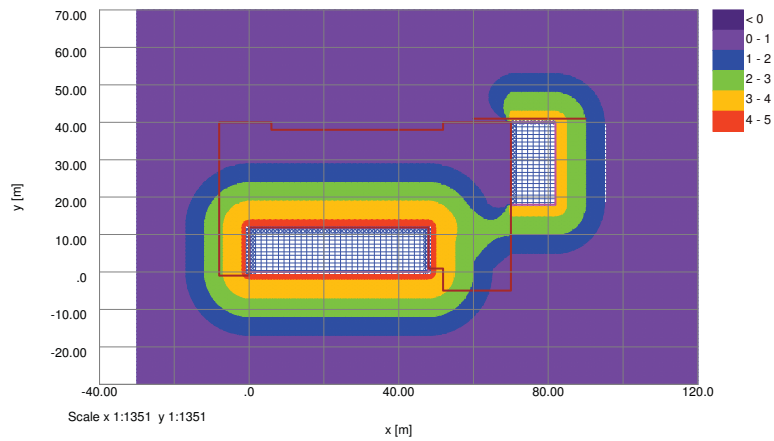
\* Indicates that the total force shown is the sum of the force in the strut plus a force applied at the same elevation which may represent temperature load or other forces which are part of the strut load. Force components are listed in the detailed results for individual stages.

Units: kN,m



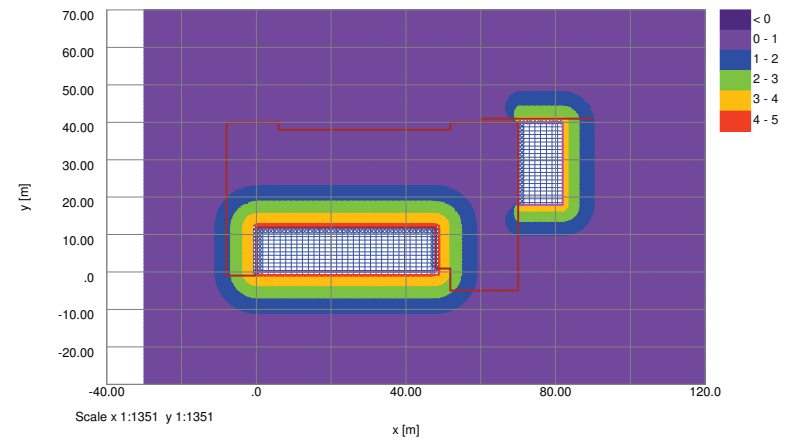
Job No.	Sheet No.	Rev.
J15050A		
<i>Drq. Ref.</i>		
<i>Made by</i> MP	<i>Date</i> 09-Feb-2016	<i>Checked</i>

Vertical Settlement Contours: Grid 1 (level 17.000m) (Interval 1mm)



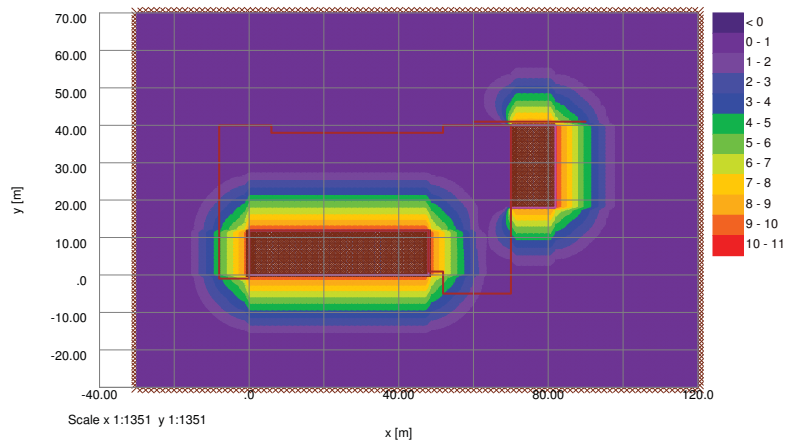
Job No.	Sheet No.	Rev.
J15050A		
<i>Drq. Ref.</i>		
<i>Made by</i> MP	<i>Date</i> 09-Feb-2016	<i>Checked</i>

Horizontal Displacement Contours: Grid 1 (level 17.000m) Interval 1mm



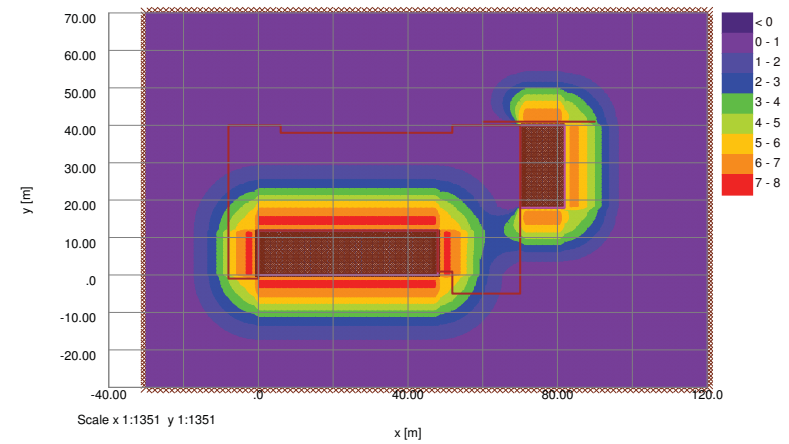
Job No.	Sheet No.	Rev.
J15050A		
Drg. Ref.		
Made by	Date	Checked
MP	08-Feb-2016	

Horizontal Displacement Contours: Grid 1 (level 17.000m) Interval 1mm



Job No.	Sheet No.	Rev.
J15050A		
Drg. Ref.		
Made by	Date	Checked
MP	08-Feb-2016	

Vertical Settlement Contours: Grid 1 (level 17.000m) (Interval 1mm)







**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC) J15050A**

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drp. Ref.</b>		
<b>Made by</b> MP	<b>Date</b> 08-Feb-2016	<b>Checked</b>

**Problem Type**

Problem Type : Tunneling and Embedded Wall Excavations

**Displacement Data**

Type	Name	Direction of extrusion	Point/Line/Line for extrusion	No. of intervals across extrusion/line	Extrusion depth	No. of intervals along extrusion	Calculate	Surface type for tunnels
			First point	Second point				
			X [m]	Y [m]	Z (level) [m]	X [m]	Y [m]	Z (level) [m]
Grid	Grid 1		Global X	-30.00000	-0.00000	17.00000	70.00000	17.00000
Line	Line 1	-		-1.00000	-1.00000	17.00000	47.00000	17.00000
Line	Line 2	-		0.00000	-1.00000	17.00000	0.00000	12.00000
Line	Line 3	-		-0.00000	12.00000	17.00000	47.00000	17.00000
Line	Line 4	-		48.00000	12.00000	17.00000	48.00000	1.00000
Line	Line 5	-		48.00000	1.00000	17.00000	41.00000	17.00000
Line	Line 6	-		52.00000	1.00000	17.00000	52.00000	-0.00000
Line	Line 7	-		52.00000	-5.00000	18.00000	70.00000	-5.00000
Line	Line 8	-		70.00000	-5.00000	18.00000	70.00000	40.00000
Line	Line 9	-		70.00000	40.00000	18.00000	52.00000	40.00000
Line	Line 10	-		52.00000	40.00000	17.00000	52.00000	38.00000
Line	Line 11	-		52.00000	38.00000	17.00000	6.00000	38.00000
Line	Line 12	-		48.00000	38.00000	17.00000	8.00000	40.00000
Line	Line 13	-		6.00000	40.00000	17.00000	8.00000	40.00000
Line	Line 14	-		8.00000	40.00000	17.00000	8.00000	41.00000
Line	Line 15	-		60.00000	41.00000	18.00000	80.00000	41.00000

**Vertical Ground Movement Curves**

**Curve Name:** No vertical ground movement  
**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (k)]  
[0.000,0.000,0.000][1.000,0.000,0.000][0.000,1.000,0.000][1.000,1.000,0.000]  
**Curve Fitting Method:** Polynomial  
**k Order:** 1  
**y Order:** 0  
**Polynomial:** z = 0.0x + 0.0  
**Coeff. of Determination:** -2147483648.E+2147483647

**Curve Name:** 80 % of Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))  
**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (k)]  
[0.000,0.000,0.039][0.100,0.000,0.049][0.200,0.000,0.056][0.300,0.000,0.062][0.400,0.000,0.067][0.500,0.000,0.070][0.600,0.000,0.072][0.700,0.000,0.073][0.800,0.000,0.072][0.900,0.000,0.071][1.000,0.000,0.070][1.100,0.000,0.068][1.200,0.000,0.065][1.300,0.000,0.061][1.400,0.000,0.058][1.500,0.000,0.054][1.600,0.000,0.050][1.700,0.000,0.046][1.800,0.000,0.042][1.900,0.000,0.038][2.000,0.000,0.034][2.100,0.000,0.030][2.200,0.000,0.027][2.300,0.000,0.023][2.400,0.000,0.020][2.500,0.000,0.016][2.600,0.000,0.012][2.700,0.000,0.008][2.800,0.000,0.005][2.900,0.000,0.002][3.000,0.000,0.000][3.100,0.000,0.000][3.200,0.000,0.000][3.300,0.000,0.000][3.400,0.000,0.000][3.500,0.000,0.000]  
**Curve Fitting Method:** Polynomial  
**k Order:** 4  
**y Order:** 0  
**Polynomial:** z = -2.6455E-3x<sup>4</sup> + 2.8495E-2x<sup>3</sup> - 1.0051E-1x<sup>2</sup> + 1.0569E-1x + 3.8990E-2  
**Coeff. of Determination:** 9.9991E-1

**Curve Name:** 93 % of Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(b))  
**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Settlement / wall depth or max. excavation depth (z) (k)]  
[0.000,0.000,0.036][0.100,0.000,0.046][0.200,0.000,0.052][0.300,0.000,0.058][0.400,0.000,0.062][0.500,0.000,0.065][0.600,0.000,0.067][0.700,0.000,0.068][0.800,0.000,0.068][0.900,0.000,0.067][1.000,0.000,0.065][1.100,0.000,0.063][1.200,0.000,0.060][1.300,0.000,0.057][1.400,0.000,0.054][1.500,0.000,0.050][1.600,0.000,0.046][1.700,0.000,0.042][1.800,0.000,0.038][1.900,0.000,0.034][2.000,0.000,0.031][2.100,0.000,0.028][2.200,0.000,0.025][2.300,0.000,0.021][2.400,0.000,0.019][2.500,0.000,0.016][2.600,0.000,0.013][2.700,0.000,0.011][2.800,0.000,0.009][2.900,0.000,0.007][3.000,0.000,0.005][3.100,0.000,0.003][3.200,0.000,0.002][3.300,0.000,0.001][3.400,0.000,0.000][3.500,0.000,0.000]  
**Curve Fitting Method:** Polynomial  
**k Order:** 4  
**y Order:** 0  
**Polynomial:** z = -2.4603E-3x<sup>4</sup> + 2.6500E-2x<sup>3</sup> - 9.3470E-2x<sup>2</sup> + 9.8293E-2x + 3.6261E-2  
**Coeff. of Determination:** 9.9991E-1

**Horizontal Ground Movement Curves**

**Curve Name:** No horizontal ground movement  
**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (k)]  
[0.000,0.000,0.000][1.000,0.000,0.000][0.000,1.000,0.000][1.000,1.000,0.000]  
**Curve Fitting Method:** Polynomial  
**k Order:** 0  
**y Order:** 0  
**Polynomial:** z = 0.0  
**Coeff. of Determination:** -2147483648.E+2147483647

**Curve Name:** 80 % of Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))  
**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (k)]  
[0.000,0.000,5.120][4.000,0.000,0.000]  
**Curve Fitting Method:** Polynomial  
**k Order:** 1  
**y Order:** 0  
**Polynomial:** z = -3.00E-2x + 1.20E-1  
**Coeff. of Determination:** 1.00

**Curve Name:** 93 % of Excavation in front of high stiffness wall in stiff clay (CIRIA 580 Fig. 2.11(a))  
**Coordinates:** [Distance from wall / wall depth or max. excavation depth (x), Depth / wall depth or max. excavation depth (y), Horizontal movement / wall depth or max. excavation depth (z) (k)]  
[0.000,0.000,5.140][4.000,0.000,0.000]  
**Curve Fitting Method:** Polynomial  
**k Order:** 1  
**y Order:** 0  
**Polynomial:** z = -3.50E-2x + 1.40E-1



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC) J15050A**

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drp. Ref.</b>		
<b>Made by</b> MP	<b>Date</b> 08-Feb-2016	<b>Checked</b>

Type	Name	Direction of extrusion	Point/Line/Line For extrusion	No. of intervals across extrusion/line	Extrusion depth	No. of intervals along extrusion	Calculate	Surface type for tunnels
Coef. of Determination:							1.00	

**Polygonal Excavations**

**Excavation Name:** East Terrace - Double Level Basement  
**Surface Level [m]:** 11.000  
**Contribution:** Positive  
**Surface movement curves which are selected are applied between surface and [m]:** 13.450

Corner	x [m]	y [m]	Level [m]	Base Stiffened	Previous Side d [m]	Next Side d [m]	Vertical	Horizontal
1	0.0	0.0	13.450	Yes	0.0	67.000	25.000	0.0
2	48.000	0.0	13.450	Yes	0.0	67.000	25.000	0.0
3	48.000	12.000	13.450	Yes	0.0	67.000	25.000	0.0
4	0.0	12.000	13.450	Yes	0.0	67.000	25.000	0.0

**Excavation Name:** Library & Treasurers House - Single Level Basement  
**Surface Level [m]:** 21.000  
**Contribution:** Positive  
**Surface movement curves which are selected are applied between surface and [m]:** 16.340

Corner	x [m]	y [m]	Level [m]	Base Stiffened	Previous Side d [m]	Next Side d [m]	Vertical	Horizontal
1	0.0	0.0	16.340	Yes	0.0	67.000	25.000	0.0
2	82.000	0.0	16.340	Yes	0.0	67.000	25.000	0.0
3	82.000	40.000	16.340	Yes	0.0	67.000	25.000	0.0
4	0.0	40.000	16.340	Yes	0.0	67.000	25.000	0.0

**Damage Category Strains**

Name	0 (Negligible)	1 (Very Slight)	2 (Slight)	3 (Moderate)	4 (Severe)
Burland Strain Limits	0.0	500.00E-6	750.00E-6	0.0015000	

**Specific Structures - Geometry**

Structure Name	Sub-Structure Name	Displacement Line	Start Distance Along Line [m]	End Distance Along Line [m]	Vertical Offsets from Line [m]	Vertical Displacement Limit [mm]	Damage Category	Strains	Poisson's Ratio	E/G
East Terrace	Sub 1	Line 1	0.00000	17.85000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
East Terrace	Sub 2	Line 2	0.00000	13.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
East Terrace	Sub 3	Line 3	0.00000	47.85000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library (East Terrace)	Sub 4	Line 4	0.00000	13.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library (Eastern Elevation)	Sub 5	Line 5	0.00000	3.85000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library (Eastern Elevation)	Sub 6	Line 6	0.00000	6.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library (Eastern Elevation)	Sub 7	Line 7	0.00000	18.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library (Northern Elevation)	Sub 8	Line 8	0.00000	45.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library (Western Elevation)	Sub 9	Line 9	0.00000	18.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Library / Great Hall (Western Elevation)	Sub 10	Line 10	0.00000	2.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Great Hall (Western Elevation)	Sub 11	Line 11	0.00000	46.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Great Hall (Western Elevation)	Sub 12	Line 12	0.00000	2.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Great Hall (Western Elevation)	Sub 13	Line 13	0.00000	14.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Great Hall (Southern Elevation)	Sub 14	Line 14	0.00000	41.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	
Boundary Wall (adjacent to single level basement)	Sub 15	Line 15	0.00000	30.00000	0.0	0.10000	Burland Strain Limits	0.20000	2.6000	

**Specific Structures - Bending Parameters**

Structure Name	Sub-Structure Name	Height	Default Properties	Hogging	Sagging
			2nd Moment of Area (per unit strain)	Distance of Centroid from Edge (per unit strain)	2nd Moment of Area of Bending of N.A. (per unit strain)



GEA LIMITED  
(GEOTECHNICAL & ENV ASSOC)

Job No.	Sheet No.	Rev.
J15050A		
Drg. Ref.		
Made by	Date	Checked
MP	08-Feb-2016	

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Type/No.	Name	Dist.	Coordinates			Displacements			Angle of Line to x Axis
			x	y	z	x	y	z	
	62.42424	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	63.93939	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	65.45455	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	66.96970	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	68.48485	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	70.00000	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	71.51515	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	73.03030	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	74.54545	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	76.06061	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	77.57576	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	79.09091	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	80.60606	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	82.12122	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	83.63636	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	85.15152	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	86.66667	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	88.18182	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	89.69697	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	91.21212	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	92.72727	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	94.24242	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	95.75758	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	97.27273	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	98.78788	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	100.30303	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	101.81818	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	103.33333	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	104.84848	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	106.36364	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	107.87879	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	109.39394	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	110.90909	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	112.42424	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	113.93939	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	115.45455	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	116.96970	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	118.48485	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	120.00000	-30.00000	17.00000	0.0	0.0	0.0	-	-	-
	-30.00000	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-28.48485	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-26.98970	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-25.48455	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-23.98939	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-22.42424	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-20.93999	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-19.39394	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-17.87879	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-16.36364	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-14.84848	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-13.33333	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-11.81818	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-10.30303	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-8.78788	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-7.27273	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-5.75758	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-4.24242	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	-2.72727	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	0.30303	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	1.81818	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	3.33333	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	4.84848	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	6.36364	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	7.87879	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	9.39394	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	10.90909	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	12.42424	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	13.93939	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	15.45455	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	16.96970	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	18.48485	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	19.99990	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	21.51515	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	23.03030	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	24.54545	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	26.06061	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	27.57576	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	29.09091	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	30.60606	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	32.12122	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	33.63636	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	35.15152	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	36.66667	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	38.18182	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	39.69697	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	41.21212	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	42.72727	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	44.24242	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	45.75758	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	47.27273	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	48.78788	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	50.30303	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	51.81818	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	53.33333	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	54.84848	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	56.36364	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	57.87879	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	59.39394	-28.98990	17.00000	0.0	0.0	0.0	-	-	-
	60.90909	-28.98990	17.00000	0.0	0.0	0.0	-	-	-

**Building Segment Combinations**

Structure Name	Sub-Structure Name	Vertical Offset from Line for Vertical Movement Calculations	Segment Start	Length	Curvature	Combined Segment
No structures have segments combined.						

**Warnings**  
1 Multiple excavations have been specified. The displacements resulting from these excavations are calculated by summing the displacements resulting from each individual excavation. No account has been taken of the interactions between excavations (e.g. overlapping zones of influence or "shielding" of one excavation by another).

**Displacement and Strain Results**

Type/No.	Name	Dist.	Coordinates			Displacements			Angle of Line to x Axis
			x	y	z	x	y	z	
	Grid 1		[m]	[m]	[m]	[mm]	[mm]	[mm]	[°]
			[m]	[m]	[m]	[mm]	[mm]	[mm]	[°]
			-30.00000	-30.00000	17.00000	0.0	0.0	0.0	-
			-28.48485	-30.00000	17.00000	0.0	0.0	0.0	-
			-26.98970	-30.00000	17.00000	0.0	0.0	0.0	-
			-25.48455	-30.00000	17.00000	0.0	0.0	0.0	-
			-23.98939	-30.00000	17.00000	0.0	0.0	0.0	-
			-22.42424	-30.00000	17.00000	0.0	0.0	0.0	-
			-20.93999	-30.00000	17.00000	0.0	0.0	0.0	-
			-19.39394	-30.00000	17.00000	0.0	0.0	0.0	-
			-17.87879	-30.00000	17.00000	0.0	0.0	0.0	-
			-16.36364	-30.00000	17.00000	0.0	0.0	0.0	-
			-14.84848	-30.00000	17.00000	0.0	0.0	0.0	-
			-13.33333	-30.00000	17.00000	0.0	0.0	0.0	-
			-11.81818	-30.00000	17.00000	0.0	0.0	0.0	-
			-10.30303	-30.00000	17.00000	0.0	0.0	0.0	-
			-8.78788	-30.00000	17.00000	0.0	0.0	0.0	-
			-7.27273	-30.00000	17.00000	0.0	0.0	0.0	-
			-5.75758	-30.00000	17.00000	0.0	0.0	0.0	-
			-4.24242	-30.00000	17.00000	0.0	0.0	0.0	-
			-2.72727	-30.00000	17.00000	0.0	0.0	0.0	-
			0.30303	-30.00000	17.00000	0.0	0.0	0.0	-
			1.81818	-30.00000	17.00000	0.0	0.0	0.0	-
			3.33333	-30.00000	17.00000	0.0	0.0	0.0	-
			4.84848	-30.00000	17.00000	0.0	0.0	0.0	-
			6.36364	-30.00000	17.00000	0.0	0.0	0.0	-
			7.87879	-30.00000	17.00000	0.0	0.0	0.0	-
			9.39394	-30.00000	17.00000	0.0	0.0	0.0	-
			10.90909	-30.00000	17.00000	0.0	0.0	0.0	-
			12.42424	-30.00000	17.00000	0.0	0.0	0.0	-
			13.93939	-30.00000	17.00000	0.0	0.0	0.0	-
			15.45455	-30.00000	17.00000	0.0	0.0	0.0	-
			16.96970	-30.00000	17.00000	0.0	0.0	0.0	-
			18.48485	-30.00000	17.00000	0.0	0.0		



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.		Coordinates			Displacements			Angle of Lime		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
		-26.96970	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-25.45455	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-23.93939	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-22.42424	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-20.90909	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-19.39394	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-17.87879	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-16.36364	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-14.84848	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-13.33333	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-11.81818	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-10.30303	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-8.78788	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-7.27273	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-5.75758	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-4.24242	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-2.72727	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		1.81818	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		3.33333	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		4.84848	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		6.36364	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		7.87879	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		9.39394	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		10.90909	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		12.42424	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		13.93939	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		15.45455	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		16.96970	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		18.48485	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		20.00000	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		21.51515	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		23.03030	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		24.54545	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		26.06061	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		27.57576	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		29.09091	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		30.60606	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		32.12121	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		33.63636	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		35.15152	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		36.66667	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		38.18182	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		39.69697	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		41.21212	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		42.72727	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		44.24242	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		45.75758	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		47.27273	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		48.78788	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		50.30303	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		51.81818	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		53.33333	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		54.84848	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		56.36364	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		57.87879	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		59.39394	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		60.90909	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		62.42424	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		63.93939	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		65.45455	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		66.96970	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		68.48485	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		70.00000	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		71.51515	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		73.03030	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		74.54545	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		76.06061	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		77.57576	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		79.09091	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		80.60606	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		82.12121	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		83.63636	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		85.15152	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		86.66667	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		88.18182	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		89.69697	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		91.21212	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		92.72727	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		94.24242	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		95.75758	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		97.27273	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		98.78788	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		100.30303	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		101.81818	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		103.33333	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		104.84848	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		106.36364	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		107.87879	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		109.39394	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		110.90909	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		112.42424	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		113.93939	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		115.45455	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		116.96970	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		118.48485	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		120.00000	-27.97980	17.00000	0.0	0.0	0.0	-	-	-
		-28.48485	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-26.96970	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-25.45455	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-23.93939	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-22.42424	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-20.90909	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-19.39394	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-17.87879	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-16.36364	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-14.84848	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-13.33333	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-11.81818	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-10.30303	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-8.78788	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-7.27273	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-5.75758	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-4.24242	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		-2.72727	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		1.81818	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		3.33333	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		4.84848	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		6.36364	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		7.87879	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		9.39394	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		10.90909	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		12.42424	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		13.93939	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		15.45455	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		16.96970	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		18.48485	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		20.00000	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		21.51515	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		23.03030	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		24.54545	-26.96970	17.00000	0.0	0.0	0.0	-	-	-
		26.06061	-26.96							



GEA LIMITED  
(GEOTECHNICAL & ENV ASSOC)

Job No.	Sheet No.	Rev.
J15050A		
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Type/No.		Coordinates			Displacements			Angle of Lime		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
		97.27273	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		98.78788	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		100.30303	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		101.81818	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		103.33333	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		104.84848	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		106.36364	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		107.87879	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		109.39394	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		110.90909	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		112.42424	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		113.93939	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		115.45455	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		116.96970	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		118.48485	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		120.00000	-25.95960	17.00000	0.0	0.0	0.0	-	-	-
		-30.00000	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-26.48485	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-26.96970	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-23.46485	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-23.93939	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-22.42424	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-20.90909	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-19.39394	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-17.87879	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-16.36364	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-14.84848	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-13.33333	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-11.81818	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-10.30303	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-8.78788	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-7.27273	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-5.75758	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-4.24242	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-2.72727	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-1.21212	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		0.30303	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		1.81818	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		3.33333	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		4.84848	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		6.36364	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		7.87879	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		9.39394	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		10.90909	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		12.42424	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		13.93939	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		15.45455	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		16.96970	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		18.48485	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		20.00000	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		21.51515	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		23.03030	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		24.54545	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		26.06061	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		27.57576	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		29.09091	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		30.60606	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		32.12121	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		33.63636	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		35.15152	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		36.66667	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		38.18182	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		39.69697	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		41.21212	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		42.72727	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		44.24242	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		45.75758	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		47.27273	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		48.78788	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		50.30303	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		51.81818	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		53.33333	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		54.84848	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		56.36364	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		57.87879	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		59.39394	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		60.90909	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		62.42424	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		63.93939	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		65.45455	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		66.96970	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		68.48485	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		70.00000	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		71.51515	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		73.03030	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		74.54545	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		76.06061	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		77.57576	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		79.09091	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		80.60606	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		82.12121	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		83.63636	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		85.15152	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		86.66667	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		88.18182	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		89.69697	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		91.21212	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		92.72727	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		94.24242	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		95.75758	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		97.27273	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		98.78788	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		100.30303	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		101.81818	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		103.33333	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		104.84848	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		106.36364	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		107.87879	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		109.39394	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		110.90909	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		112.42424	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		113.93939	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		115.45455	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		116.96970	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		118.48485	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		120.00000	-24.94949	17.00000	0.0	0.0	0.0	-	-	-
		-30.00000	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-26.48485	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-26.96970	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-23.46485	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-23.93939	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-22.42424	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-20.90909	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-19.39394	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-17.87879	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-16.36364	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-14.84848	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-13.33333	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-11.81818	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-10.30303	-23.93939	17.00000	0.0	0.0	0.0	-	-	-
		-8.78788	-23.93939							



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC)**

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>J15050A</b>		
<b>Drng. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
<b>MP</b>	<b>08-Feb-2016</b>	

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Type/No.		Coordinates			Displacements			Angle of Line		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
70.00000	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
71.51515	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
73.03030	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
74.54545	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
76.06061	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
77.57576	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
79.09091	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80.60606	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
82.12121	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
83.63636	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
85.15152	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
86.66667	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
88.18182	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
89.69697	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
91.21212	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
92.72727	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
94.24242	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
95.75758	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
97.27273	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
98.78788	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
100.30303	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
101.81818	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
103.33333	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
104.84848	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
106.36364	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
107.87879	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
109.39394	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
110.90909	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
112.42424	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
113.93939	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
115.45455	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
116.96970	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
118.48485	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
120.00000	-22.92929	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-28.48485	-20.90909	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-26.96970	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-25.45455	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-23.93939	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-22.42424	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-20.90909	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-19.39394	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-17.87879	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-16.36364	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-14.84848	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-13.33333	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-11.81818	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-10.30303	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-8.78788	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-7.27273	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-5.75758	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-4.24242	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-2.72727	-21.91919	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.21212	-21.91919	17.00000	0.0	0.0	0.0094638	0.0	0.0	0.0	0.0	0.0
2.72727	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
4.24242	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
5.75758	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
7.27273	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
8.78788	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
10.30303	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
11.81818	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
13.33333	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
14.84848	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
16.36364	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
17.87879	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
19.39394	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
20.90909	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
22.42424	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
23.93939	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
25.45455	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
26.96970	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
28.48485	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
29.99999	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
31.51515	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
33.03030	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
34.54545	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
36.06061	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
37.57576	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
39.09091	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
40.60606	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
42.12121	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
43.63636	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
45.15152	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
46.66667	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
48.18182	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
49.69697	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
51.21212	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
52.72727	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
54.24242	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
55.75758	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
57.27273	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
58.78788	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
60.30303	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
61.81818	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
63.33333	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
64.84848	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
66.36364	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
67.87879	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
69.39394	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
70.90909	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
72.42424	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
73.93939	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
75.45455	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
76.96970	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
78.48485	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
79.99999	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
81.51515	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0	0.0	0.0	0.0
83.03030	-21.91919	17.00000	0.0	0.0	0.0	0.016162	0.0			



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Name	Dist.	x	y	z	x	y	z	Displacements	Horizontal displacement	Horizontal displacement	Angle of Lime to x Axis
42.72727	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
44.24242	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
45.75758	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
47.27273	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
48.78788	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
50.30303	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
51.81818	-19.88889	17.00000	0.0	0.0	0.42020	-	-	-	-	-	-	-
53.33333	-19.88889	17.00000	0.0	0.0	0.27974	-	-	-	-	-	-	-
54.84848	-19.88889	17.00000	0.0	0.0	0.19110	-	-	-	-	-	-	-
56.36364	-19.88889	17.00000	0.0	0.0	0.20876	-	-	-	-	-	-	-
57.87879	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
59.39394	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
60.90909	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
62.42424	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
63.93939	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
65.45455	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
66.96970	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
68.48485	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
70.00000	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
71.51515	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
73.03030	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
74.54545	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
76.06061	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
77.57576	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
79.09091	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
80.60606	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
82.12121	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
83.63636	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
85.15152	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
86.66667	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
88.18182	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
89.69697	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
91.21212	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
92.72727	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
94.24242	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
95.75758	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
97.27273	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
98.78788	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
100.30303	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
101.81818	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
103.33333	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
104.84848	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
106.36364	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
107.87879	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
109.39394	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
110.90909	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
112.42424	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
113.93939	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
115.45455	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
116.96970	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
118.48485	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
120.00000	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
121.51515	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
123.03030	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
124.54545	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
126.06061	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
127.57576	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
129.09091	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
130.60606	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
132.12121	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
133.63636	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
135.15152	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
136.66667	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
138.18182	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
139.69697	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
141.21212	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
142.72727	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
144.24242	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
145.75758	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
147.27273	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
148.78788	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
150.30303	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
151.81818	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
153.33333	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
154.84848	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
156.36364	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
157.87879	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
159.39394	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
160.90909	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
162.42424	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
163.93939	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
165.45455	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
166.96970	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
168.48485	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
170.00000	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
171.51515	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
173.03030	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
174.54545	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
176.06061	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
177.57576	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
179.09091	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
180.60606	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
182.12121	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
183.63636	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
185.15152	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
186.66667	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
188.18182	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
189.69697	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
191.21212	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
192.72727	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
194.24242	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
195.75758	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
197.27273	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
198.78788	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
200.30303	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
201.81818	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
203.33333	-19.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Name	Dist.	x	y	z	x	y	z	Displacements	Horizontal displacement	Horizontal displacement	Angle of Lime to x Axis
104.84848	-18.88889	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
106.36364	-18.88889	17.0										



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Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by, Date, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements, Angle of Lims, Horizontal displacement, Horizontal displacement to x Axis



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Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement to x Axis, Angle of Line to x Axis



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Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Name	Dist.	x	y	z	x	y	z	Displacements	Horizontal displacement	Horizontal displacement	Angle of Line to x Axis
-23.93939	3.33333	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-22.42424	3.33333	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-20.90909	3.33333	17.00000	0.0	0.0	0.21818	0.0	0.0	0.0	-	-	-	-
-19.39394	3.33333	17.00000	0.0	0.0	0.43636	0.0	0.0	0.0	-	-	-	-
-17.87879	3.33333	17.00000	0.0	0.0	0.65455	0.0	0.0	0.0	-	-	-	-
-16.36364	3.33333	17.00000	0.0	0.0	0.87273	0.0	0.0	0.0	-	-	-	-
-14.84849	3.33333	17.00000	0.0	0.0	1.09091	0.0	0.0	0.0	-	-	-	-
-13.33333	3.33333	17.00000	0.0	0.0	1.30909	0.0	0.0	0.0	-	-	-	-
-11.81818	3.33333	17.00000	0.0	0.0	1.52727	0.0	0.0	0.0	-	-	-	-
-10.30303	3.33333	17.00000	0.0	0.0	1.74545	0.0	0.0	0.0	-	-	-	-
-8.78788	3.33333	17.00000	0.0	0.0	1.96364	0.0	0.0	0.0	-	-	-	-
-7.27273	3.33333	17.00000	0.0	0.0	2.18182	0.0	0.0	0.0	-	-	-	-
-5.75758	3.33333	17.00000	0.0	0.0	2.39999	0.0	0.0	0.0	-	-	-	-
-4.24242	3.33333	17.00000	0.0	0.0	2.61818	0.0	0.0	0.0	-	-	-	-
-2.72727	3.33333	17.00000	0.0	0.0	2.83636	0.0	0.0	0.0	-	-	-	-
-1.21212	3.33333	17.00000	0.0	0.0	3.05455	0.0	0.0	0.0	-	-	-	-
0.30303	3.33333	17.00000	0.0	0.0	3.27273	0.0	0.0	0.0	-	-	-	-
1.81818	3.33333	17.00000	0.0	0.0	3.49091	0.0	0.0	0.0	-	-	-	-
3.33333	3.33333	17.00000	0.0	0.0	3.70909	0.0	0.0	0.0	-	-	-	-
4.84849	3.33333	17.00000	0.0	0.0	3.92727	0.0	0.0	0.0	-	-	-	-
6.36364	3.33333	17.00000	0.0	0.0	4.14545	0.0	0.0	0.0	-	-	-	-
7.87879	3.33333	17.00000	0.0	0.0	4.36364	0.0	0.0	0.0	-	-	-	-
9.39394	3.33333	17.00000	0.0	0.0	4.58182	0.0	0.0	0.0	-	-	-	-
10.90909	3.33333	17.00000	0.0	0.0	4.80000	0.0	0.0	0.0	-	-	-	-
12.42424	3.33333	17.00000	0.0	0.0	5.01818	0.0	0.0	0.0	-	-	-	-
13.93939	3.33333	17.00000	0.0	0.0	5.23636	0.0	0.0	0.0	-	-	-	-
15.45455	3.33333	17.00000	0.0	0.0	5.45455	0.0	0.0	0.0	-	-	-	-
16.96970	3.33333	17.00000	0.0	0.0	5.67273	0.0	0.0	0.0	-	-	-	-
18.48485	3.33333	17.00000	0.0	0.0	5.89091	0.0	0.0	0.0	-	-	-	-
20.00000	3.33333	17.00000	0.0	0.0	6.10909	0.0	0.0	0.0	-	-	-	-
21.51515	3.33333	17.00000	0.0	0.0	6.32727	0.0	0.0	0.0	-	-	-	-
23.03030	3.33333	17.00000	0.0	0.0	6.54545	0.0	0.0	0.0	-	-	-	-
24.54545	3.33333	17.00000	0.0	0.0	6.76364	0.0	0.0	0.0	-	-	-	-
26.06061	3.33333	17.00000	0.0	0.0	6.98182	0.0	0.0	0.0	-	-	-	-
27.57576	3.33333	17.00000	0.0	0.0	7.20000	0.0	0.0	0.0	-	-	-	-
29.09091	3.33333	17.00000	0.0	0.0	7.41818	0.0	0.0	0.0	-	-	-	-
30.60606	3.33333	17.00000	0.0	0.0	7.63636	0.0	0.0	0.0	-	-	-	-
32.12121	3.33333	17.00000	0.0	0.0	7.85455	0.0	0.0	0.0	-	-	-	-
33.63636	3.33333	17.00000	0.0	0.0	8.07273	0.0	0.0	0.0	-	-	-	-
35.15152	3.33333	17.00000	0.0	0.0	8.29091	0.0	0.0	0.0	-	-	-	-
36.66667	3.33333	17.00000	0.0	0.0	8.50909	0.0	0.0	0.0	-	-	-	-
48.78788	3.33333	17.00000	0.0	0.0	9.35000	0.0	0.0	0.0	-	-	-	-
50.30303	3.33333	17.00000	0.0	0.0	9.56818	0.0	0.0	0.0	-	-	-	-
51.81818	3.33333	17.00000	0.0	0.0	9.78636	0.0	0.0	0.0	-	-	-	-
53.33333	3.33333	17.00000	0.0	0.0	10.00455	0.0	0.0	0.0	-	-	-	-
54.84849	3.33333	17.00000	0.0	0.0	10.22273	0.0	0.0	0.0	-	-	-	-
56.36364	3.33333	17.00000	0.0	0.0	10.44091	0.0	0.0	0.0	-	-	-	-
57.87879	3.33333	17.00000	0.0	0.0	10.65909	0.0	0.0	0.0	-	-	-	-
59.39394	3.33333	17.00000	0.0	0.0	10.87727	0.0	0.0	0.0	-	-	-	-
60.90909	3.33333	17.00000	0.0	0.0	11.09545	0.0	0.0	0.0	-	-	-	-
62.42424	3.33333	17.00000	0.0	0.0	11.31364	0.0	0.0	0.0	-	-	-	-
63.93939	3.33333	17.00000	0.0	0.0	11.53182	0.0	0.0	0.0	-	-	-	-
65.45455	3.33333	17.00000	0.0	0.0	11.75000	0.0	0.0	0.0	-	-	-	-
66.96970	3.33333	17.00000	0.0	0.0	11.96818	0.0	0.0	0.0	-	-	-	-
68.48485	3.33333	17.00000	0.0	0.0	12.18636	0.0	0.0	0.0	-	-	-	-
69.99999	3.33333	17.00000	0.0	0.0	12.40455	0.0	0.0	0.0	-	-	-	-
71.51515	3.33333	17.00000	0.0	0.0	12.62273	0.0	0.0	0.0	-	-	-	-
73.03030	3.33333	17.00000	0.0	0.0	12.84091	0.0	0.0	0.0	-	-	-	-
74.54545	3.33333	17.00000	0.0	0.0	13.05909	0.0	0.0	0.0	-	-	-	-
76.06061	3.33333	17.00000	0.0	0.0	13.27727	0.0	0.0	0.0	-	-	-	-
77.57576	3.33333	17.00000	0.0	0.0	13.49545	0.0	0.0	0.0	-	-	-	-
79.09091	3.33333	17.00000	0.0	0.0	13.71364	0.0	0.0	0.0	-	-	-	-
80.60606	3.33333	17.00000	0.0	0.0	13.93182	0.0	0.0	0.0	-	-	-	-
82.12121	3.33333	17.00000	0.0	0.0	14.15000	0.0	0.0	0.0	-	-	-	-
83.63636	3.33333	17.00000	0.0	0.0	14.36818	0.0	0.0	0.0	-	-	-	-
85.15152	3.33333	17.00000	0.0	0.0	14.58636	0.0	0.0	0.0	-	-	-	-
86.66667	3.33333	17.00000	0.0	0.0	14.80455	0.0	0.0	0.0	-	-	-	-
88.18182	3.33333	17.00000	0.0	0.0	15.02273	0.0	0.0	0.0	-	-	-	-
89.69697	3.33333	17.00000	0.0	0.0	15.24091	0.0	0.0	0.0	-	-	-	-
91.21212	3.33333	17.00000	0.0	0.0	15.45909	0.0	0.0	0.0	-	-	-	-
92.72727	3.33333	17.00000	0.0	0.0	15.67727	0.0	0.0	0.0	-	-	-	-
94.24242	3.33333	17.00000	0.0	0.0	15.89545	0.0	0.0	0.0	-	-	-	-
95.75758	3.33333	17.00000	0.0	0.0	16.11364	0.0	0.0	0.0	-	-	-	-
97.27273	3.33333	17.00000	0.0	0.0	16.33182	0.0	0.0	0.0	-	-	-	-
98.78788	3.33333	17.00000	0.0	0.0	16.55000	0.0	0.0	0.0	-	-	-	-
100.30303	3.33333	17.00000	0.0	0.0	16.76818	0.0	0.0	0.0	-	-	-	-
101.81818	3.33333	17.00000	0.0	0.0	16.98636	0.0	0.0	0.0	-	-	-	-
103.33333	3.33333	17.00000	0.0	0.0	17.20455	0.0	0.0	0.0	-	-	-	-
104.84849	3.33333	17.00000	0.0	0.0	17.42273	0.0	0.0	0.0	-	-	-	-
106.36364	3.33333	17.00000	0.0	0.0	17.64091	0.0	0.0	0.0	-	-	-	-
107.87879	3.33333	17.00000	0.0	0.0	17.85909	0.0	0.0	0.0	-	-	-	-
109.39394	3.33333	17.00000	0.0	0.0	18.07727	0.0	0.0	0.0	-	-	-	-
110.90909	3.33333	17.00000	0.0	0.0	18.29545	0.0	0.0	0.0	-	-	-	-
112.42424	3.33333	17.00000	0.0	0.0	18.51364	0.0	0.0	0.0	-	-	-	-
113.93939	3.33333	17.00000	0.0	0.0	18.73182	0.0	0.0	0.0	-	-	-	-
115.45455	3.33333	17.00000	0.0	0.0	18.95000	0.0	0.0	0.0	-	-	-	-
116.96970	3.33333	17.00000	0.0	0.0	19.16818	0.0	0.0	0.0	-	-	-	-
118.48485	3.33333	17.00000	0.0	0.0	19.38636	0.0	0.0	0.0	-	-	-	-
119.99999	3.33333	17.00000	0.0	0.0	19.60455	0.0	0.0	0.0	-	-	-	-
121.51515	3.33333	17.00000	0.0	0.0	19.82273	0.0	0.0	0.0	-	-	-	-
123.03030	3.33333	17.00000	0.0	0.0	20.04091	0.0	0.0	0.0	-	-	-	-
124.54545	3.33333	17.00000	0.0	0.0	20.25909	0.0	0.0	0.0	-	-	-	-
126.06061	3.33333	17.00000	0.0	0.0	20.47727	0.0	0.0	0.0	-	-	-	-
127.57576	3.33333	17.00000	0.0	0.0	20.69545	0.0	0.0	0.0	-	-	-	-
129.09091	3.33333	17.00000	0.0	0.0	20.91364	0.0	0.0	0.0	-	-	-	-
130.60606	3.33333	17.00000	0.0	0.0	21.13182	0.0	0.0	0.0	-	-	-	-
132.12121	3.33333	17.00000	0.0	0.0	21.35000	0.0	0.0	0.0	-	-	-	-
133.63636	3.33333	17.00000	0.0	0.0	21.56818	0.0	0.0	0.0	-	-	-	-
135.15152	3.33333	17.00000	0.0	0.0	21.78636	0.0	0.0	0.0	-	-	-	-
136.66667	3.33333	17.00000	0.0	0.0	22.00455	0.0	0.0	0.0	-	-	-	-



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC) J15050A**

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Name	Dist.	x	y	z	x	y	z	Displacements	Horizontal displacement	Horizontal displacement	Angle of Line to x Axis
100.30303	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
101.81818	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
102.33333	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
104.84848	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
106.86868	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
107.87879	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
109.39394	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
110.90909	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
112.42424	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
113.93939	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
115.45455	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
116.96970	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
118.48485	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
120.00000	5.35354	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-30.00000	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-28.48485	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-26.96970	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-25.45455	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-23.93939	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-22.42424	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-20.90909	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-19.39394	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-17.87879	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-16.36364	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-14.84848	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-13.33333	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-11.81818	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-10.30303	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-8.78788	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-7.27273	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-5.75758	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-4.24242	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-2.72727	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
-1.21212	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
0.30303	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
1.81818	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
3.33333	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
4.84848	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
6.36364	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
7.87879	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
9.39394	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
10.90909	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
12.42424	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
13.93939	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
15.45455	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
16.96970	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
18.48485	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
20.00000	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
21.51515	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
23.03030	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
24.54545	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
26.06061	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
27.57576	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
29.09091	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
30.60606	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
32.12121	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
33.63636	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
35.15152	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
36.66667	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
38.18182	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
39.69697	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
41.21212	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
42.72727	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
44.24242	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
45.75758	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
47.27273	6.36364	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	-	-	-	-
48.78788	6.36364	17.00000	-9.3502	0.0	6.7187	-	-	-	-	-	-	-
50.30303	6.36364	17.00000	-6.7187	0.0	6.9321	-	-	-	-	-	-	-
51.81818	6.36364	17.00000	-4.0860	0.0	6.9321	-	-	-	-	-	-	-
53.33333	6.36364	17.00000	-1.4593	0.0	6.9321	-	-	-	-	-	-	-
54.84848	6.36364	17.00000	-0.9426	0.0	6.9321	-	-	-	-	-	-	-
56.36364	6.36364	17.00000	-0.4259	0.01243	4.8577	-	-	-	-	-	-	-
57.87879	6.36364	17.00000	-0.9124	0.02823	3.8489	-	-	-	-	-	-	-
59.39394	6.36364	17.00000	-2.8291	0.17638	3.1650	-	-	-	-	-	-	-
60.90909	6.36364	17.00000	-2.8291	0.17638	3.1650	-	-	-	-	-	-	-
62.42424	6.36364	17.00000	-1.2227	0.42021	2.3616	-	-	-	-	-	-	-
63.93939	6.36364	17.00000	-0.44333	0.44944	1.4774	-	-	-	-	-	-	-
65.45455	6.36364	17.00000	0.14230	0.93660	2.0707	-	-	-	-	-	-	-
66.96970	6.36364	17.00000	0.32263	1.9794	1.8044	-	-	-	-	-	-	-
68.48485	6.36364	17.00000	0.15812	1.5215	1.9133	-	-	-	-	-	-	-
70.00000	6.36364	17.00000	0.0	2.7414	0.8045	-	-	-	-	-	-	-
71.51515	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
73.03030	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
74.54545	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
76.06061	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
77.57576	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
79.09091	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
80.60606	6.36364	17.00000	0.0	2.4348	2.0664	-	-	-	-	-	-	-
82.12121	6.36364	17.00000	-0.01899	1.7375	1.8023	-	-	-	-	-	-	-
83.63636	6.36364	17.00000	-0.19883	1.6344	1.7380	-	-	-	-	-	-	-
85.15152	6.36364	17.00000	-0.39112	1.4441	1.6026	-	-	-	-	-	-	-
86.66667	6.36364	17.00000	-0.31368	1.1924	1.4205	-	-	-	-	-	-	-
88.18182	6.36364	17.00000	-0.48139	0.90653	1.2059	-	-	-	-	-	-	-
89.69697	6.36364	17.00000	0.7996	0.7996	0.7996	-	-	-	-	-	-	-
91.21212	6.36364	17.00000	-0.39652	0.90087	0.73820	-	-	-	-	-	-	-
92.72727	6.36364	17.00000	-0.31368	0.4026	0.60221	-	-	-	-	-	-	-
94.24242	6.36364	17.00000	-0.20904	0.19669	0.26609	-	-	-	-	-	-	-
95.75758	6.36364	17.00000	-0.08071	0.06825	0.021820	-	-	-	-	-	-	-
97.27273	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
98.78788	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
100.30303	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
101.81818	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
102.33333	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
104.84848	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
106.86868	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
107.87879	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
109.39394	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
110.90909	6.36364	17.00000	0.0	0.0	0.0	-	-	-	-	-	-	-
112.42424												





**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC)**

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
J15050A		
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Coordinates			Displacements			Angle of Line to x Axis
	Dist.	x	y	x	y	z	
73.03030	8.38384	17.00000	0.0	3.4237	3.1460	-	-
74.04545	8.38384	17.00000	0.0	3.4237	3.1460	-	-
76.00007	8.38384	17.00000	0.0	3.4237	3.1460	-	-
77.07576	8.38384	17.00000	0.0	3.4237	3.1460	-	-
78.00000	8.38384	17.00000	0.0	3.4237	3.1460	-	-
80.06096	8.38384	17.00000	0.0	3.4237	3.1460	-	-
82.12121	8.38384	17.00000	-0.03188	0.0	0.0	-	-
83.63636	8.38384	17.00000	-0.40288	2.3676	2.6451	-	-
85.15152	8.38384	17.00000	-0.88488	2.0886	2.3384	-	-
86.66667	8.38384	17.00000	-0.84288	1.7371	2.0721	-	-
88.18182	8.38384	17.00000	-0.87489	1.3609	1.7684	-	-
89.69697	8.38384	17.00000	-0.79584	0.9380	1.4507	-	-
91.21212	8.38384	17.00000	-0.62610	0.65356	1.1369	-	-
92.72727	8.38384	17.00000	-0.47844	0.4134	0.84833	-	-
94.24242	8.38384	17.00000	-0.41932	0.32921	0.76384	-	-
95.75758	8.38384	17.00000	-0.27188	0.0	0.0	-	-
97.27273	8.38384	17.00000	-0.091886	0.057728	0.022119	-	-
98.78788	8.38384	17.00000	0.0	0.0	0.0	-	-
100.30303	8.38384	17.00000	0.0	0.0	0.0	-	-
101.81818	8.38384	17.00000	0.0	0.0	0.0	-	-
103.33333	8.38384	17.00000	0.0	0.0	0.0	-	-
104.84848	8.38384	17.00000	0.0	0.0	0.0	-	-
106.36364	8.38384	17.00000	0.0	0.0	0.0	-	-
107.87879	8.38384	17.00000	0.0	0.0	0.0	-	-
109.39394	8.38384	17.00000	0.0	0.0	0.0	-	-
110.90909	8.38384	17.00000	0.0	0.0	0.0	-	-
112.42424	8.38384	17.00000	0.0	0.0	0.0	-	-
113.93939	8.38384	17.00000	0.0	0.0	0.0	-	-
115.45455	8.38384	17.00000	0.0	0.0	0.0	-	-
116.96970	8.38384	17.00000	0.0	0.0	0.0	-	-
118.48485	8.38384	17.00000	0.0	0.0	0.0	-	-
120.00000	8.38384	17.00000	0.0	0.0	0.0	-	-
-10.00000	9.39394	17.00000	0.0	0.0	0.0	-	-
-28.48485	9.39394	17.00000	0.0	0.0	0.0	-	-
-26.96970	9.39394	17.00000	0.0	0.0	0.0	-	-
-23.45455	9.39394	17.00000	0.0	0.0	0.0	-	-
-23.93939	9.39394	17.00000	0.0	0.0	0.0	-	-
-22.42424	9.39394	17.00000	0.0	0.0	0.0	-	-
-20.90909	9.39394	17.00000	0.0	0.21818	-	-	-
-19.39394	9.39394	17.00000	0.0	0.0	0.0	-	-
-17.87879	9.39394	17.00000	0.096364	0.0	0.85074	-	-
-16.36364	9.39394	17.00000	0.57396	0.0	0.0	-	-
-14.84848	9.39394	17.00000	1.13005	0.0	1.6039	-	-
-13.33333	9.39394	17.00000	2.12334	0.0	2.7784	-	-
-11.81818	9.39394	17.00000	2.7773	0.0	2.6900	-	-
-10.30303	9.39394	17.00000	3.1460	0.0	2.4349	-	-
-8.78788	9.39394	17.00000	4.3443	0.0	4.3118	-	-
-7.27273	9.39394	17.00000	5.1800	0.0	5.2316	-	-
-5.75758	9.39394	17.00000	6.0601	0.0	6.1037	-	-
-4.24242	9.39394	17.00000	6.9922	0.0	6.9738	-	-
-2.72727	9.39394	17.00000	7.9834	0.0	7.9138	-	-
-1.21212	9.39394	17.00000	9.0412	0.0	8.9121	-	-
0.30303	9.39394	17.00000	0.0	0.0	0.0	-	-
1.81818	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
3.33333	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
4.84848	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
6.36364	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
7.87879	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
9.39394	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
10.90909	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
12.42424	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
13.93939	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
15.45455	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
16.96970	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
18.48485	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
20.00000	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
21.51515	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
23.03030	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
24.54545	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
26.06061	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
27.57576	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
29.09091	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
30.60606	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
32.12121	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
33.63636	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
35.15152	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
36.66667	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
38.18182	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
39.69697	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
41.21212	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
42.72727	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
44.24242	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
45.75758	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
47.27273	9.39394	17.00000	Point lies within an excavation.	-	-	-	-
48.78788	9.39394	17.00000	-0.3802	0.0	6.1887	-	-
50.30303	9.39394	17.00000	-0.82724	0.0	6.9321	-	-
51.81818	9.39394	17.00000	-1.2634	0.0	7.6821	-	-
53.33333	9.39394	17.00000	-1.6136	0.0	8.4388	-	-
54.84848	9.39394	17.00000	-1.9695	0.028599	9.5351	-	-
56.36364	9.39394	17.00000	-4.0389	0.072163	4.7241	-	-
57.87879	9.39394	17.00000	-3.5847	0.12883	3.9641	-	-
59.39394	9.39394	17.00000	-3.0881	0.20452	3.4688	-	-
60.90909	9.39394	17.00000	-1.8550	0.36285	2.9025	-	-
62.42424	9.39394	17.00000	0.64882	0.47698	2.3508	-	-
63.93939	9.39394	17.00000	-0.11110	0.94925	2.6231	-	-
65.45455	9.39394	17.00000	0.51885	1.3925	2.8893	-	-
66.96970	9.39394	17.00000	0.67628	1.8206	2.8106	-	-
68.48485	9.39394	17.00000	0.43533	2.4727	2.9969	-	-
70.00000	9.39394	17.00000	0.0	2.9417	3.1088	-	-
71.51515	9.39394	17.00000	0.0	3.9351	3.7474	-	-
73.03030	9.39394	17.00000	0.0	3.9351	3.7474	-	-
74.54545	9.39394	17.00000	0.0	3.9351	3.7474	-	-
76.06061	9.39394	17.00000	0.0	3.9351	3.7474	-	-
77.57576	9.39394	17.00000	0.0	3.9351	3.7474	-	-
79.09091	9.39394	17.00000	0.0	3.9351	3.7474	-	-
80.60606	9.39394	17.00000	0.0	3.9351	3.7474	-	-
82.12121	9.39394	17.00000	-0.041284	0.912	2.1241	-	-
83.63636	9.39394	17.00000	-0.52060	2.3739	2.9771	-	-
85.15152	9.39394	17.00000	-0.87862	2.3938	2.7310	-	-
86.66667	9.39394	17.00000	-1.0703	1.9738	2.4160	-	-
88.18182	9.39394	17.00000	-1.1069	1.5410	2.0624	-	-
89.69697	9.39394	17.00000	-0.9148	1.1847	1.8970	-	-
91.21212	9.39394	17.00000	-0.84896	0.79124	1.8479	-	-
92.72727	9.39394	17.00000	-0.65765	0.37621	1.0389	-	-
94.24242	9.39394	17.00000	-0.53619	0.37683	0.70855	-	-
95.75758	9.39394	17.00000	-0.37479	0.28445	0.41817	-	-
97.27273	9.39394	17.00000	-0.18119	0.10210	0.12899	-	-
98.78788	9.39394	17.00000	0.0	0.0	0.0	-	-
100.30303	9.39394	17.00000	0.0	0.0	0.0	-	-
101.81818	9.39394	17.00000	0.0	0.0	0.0	-	-
103.33333	9.39394	17.00000	0.0	0.0	0.0	-	-
104.84848	9.39394	17.00000	0.0	0.0	0.0	-	-
106.36364	9.39394	17.00000	0.0	0.0	0.0	-	-
107.87879	9.39394	17.00000	0.0	0.0	0.0	-	-
109.39394	9.39394	17.00000	0.0	0.0	0.0	-	-
110.90909	9.39394	17.00000	0.0	0.0	0.0	-	-
112.42424	9.39394	17.00000	0.0	0.0	0.0	-	-
113.93939	9.39394	17.00000	0.0	0.0	0.0	-	-
115.45455	9.39394	17.00000	0.0	0.0	0.0	-	-
116.96970	9.39394	17.00000	0.0	0.0	0.0	-	-
118.48485	9.39394	17.00000	0.0	0.0	0.0	-	-
120.00000	9.39394	17.00000	0.0	0.0	0.0	-	-
-10.00000	10.40404	17.00000	0.0	0.0	0.0	-	-
-28.48485	10.40404	17.00000	0.0	0.0	0.0	-	-
-26.96970	10.40404	17.00000	0.0	0.0	0.0	-	-
-23.45455	10.40404	17.00000	0.0	0.0	0.0	-	-
-23.93939	10.40404	17.00000	0.0	0.0	0.0	-	-
-22.42424	10.40404	17.00000	0.0	0.0	0.0	-	-
-20.90909	10.40404	17.00000	0.0	0.21818	-	-	-
-19.39394	10.40404	17.00000	0.0	0.0	0.0	-	-
-17.87879	10.40404	17.00000	0.0	0.85074	-	-	-



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC)**

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
J15050A		
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Coordinates			Displacements			Angle of Line to x Axis
	Dist.	x	y	x	y	z</	





GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., X, Y, Z, Displacements (X, Y, Z, Horizontal, Horizontal to X Axis), Angle of Line to X Axis, Displacement displacement



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., X, Y, Z, Displacements (X, Y, Z, Horizontal, Horizontal to X Axis), Angle of Line to X Axis, Displacement displacement



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC)** **J15050A**

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drg. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
<b>MP</b>	<b>08-Feb-2016</b>	

Type/No.	Coordinates			Displacements			Angle of Lime		
	Dist.	x	y	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
18.48485	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
20.00000	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
21.51515	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
23.03030	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
24.54545	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
26.06061	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
27.57576	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
29.09091	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
30.60606	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
32.12121	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
33.63636	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
35.15152	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
36.66667	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
38.18182	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
39.69697	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
41.21212	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
42.72727	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
44.24242	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
45.75758	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
47.27273	14.44444	17.00000	0.0	-8.1756	7.1399	0.0	-	-	-
48.78788	14.44444	17.00000	-1.9103	-5.9269	5.8460	0.0	-	-	-
50.30303	14.44444	17.00000	-1.9192	-3.9051	5.4088	0.0	-	-	-
51.81818	14.44444	17.00000	-1.9281	-1.8833	4.9716	0.0	-	-	-
53.33333	14.44444	17.00000	-1.9370	-0.8615	4.5344	0.0	-	-	-
54.84848	14.44444	17.00000	-1.9459	0.1603	4.0972	0.0	-	-	-
56.36364	14.44444	17.00000	-1.9548	1.1781	3.6600	0.0	-	-	-
57.87879	14.44444	17.00000	-1.9637	2.1959	3.2228	0.0	-	-	-
59.39394	14.44444	17.00000	-1.9726	3.2137	2.7856	0.0	-	-	-
60.90909	14.44444	17.00000	-1.9815	4.2315	2.3484	0.0	-	-	-
62.42424	14.44444	17.00000	-1.9904	5.2493	1.9112	0.0	-	-	-
63.93939	14.44444	17.00000	-2.0000	6.2671	1.4740	0.0	-	-	-
65.45455	14.44444	17.00000	-2.0100	7.2849	1.0368	0.0	-	-	-
66.96969	14.44444	17.00000	-2.0200	8.3027	0.5996	0.0	-	-	-
68.48485	14.44444	17.00000	-2.0300	9.3205	0.1624	0.0	-	-	-
70.00000	14.44444	17.00000	0.0	9.2988	0.1644	0.0	-	-	-
71.51515	14.44444	17.00000	0.0	9.2922	0.2852	0.0	-	-	-
73.03030	14.44444	17.00000	0.0	9.2922	0.2852	0.0	-	-	-
74.54545	14.44444	17.00000	0.0	9.2922	0.2852	0.0	-	-	-
76.06061	14.44444	17.00000	0.0	9.2922	0.2852	0.0	-	-	-
77.57576	14.44444	17.00000	0.0	9.2922	0.2852	0.0	-	-	-
79.09091	14.44444	17.00000	0.0	9.2922	0.2852	0.0	-	-	-
80.60606	14.44444	17.00000	-0.17984	5.2655	5.1363	0.0	-	-	-
82.12121	14.44444	17.00000	-0.18973	3.2511	4.7100	0.0	-	-	-
83.63636	14.44444	17.00000	-0.19962	1.2357	4.2837	0.0	-	-	-
85.15152	14.44444	17.00000	-0.20951	0.2203	3.8574	0.0	-	-	-
86.66667	14.44444	17.00000	-0.21940	0.8049	3.4311	0.0	-	-	-
88.18182	14.44444	17.00000	-0.22929	1.3895	3.0048	0.0	-	-	-
89.69697	14.44444	17.00000	-0.23918	1.9741	2.5785	0.0	-	-	-
91.21212	14.44444	17.00000	-0.24907	2.5587	2.1522	0.0	-	-	-
92.72727	14.44444	17.00000	-0.25896	3.1433	1.7259	0.0	-	-	-
94.24242	14.44444	17.00000	-0.26885	3.7279	1.3000	0.0	-	-	-
95.75758	14.44444	17.00000	-0.27874	4.3125	0.8741	0.0	-	-	-
97.27273	14.44444	17.00000	-0.28863	4.8971	0.4482	0.0	-	-	-
98.78788	14.44444	17.00000	-0.29852	5.4817	0.0223	0.0	-	-	-
100.30303	14.44444	17.00000	-0.30841	6.0663	0.0000	0.0	-	-	-
101.81818	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
103.33333	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
104.84848	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
106.36364	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
107.87879	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
109.39394	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
110.90909	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
112.42424	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
113.93939	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
115.45455	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
116.96969	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
118.48485	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
119.99999	14.44444	17.00000	0.0	0.0	0.0	0.0	-	-	-
-10.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-12.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-14.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-16.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-18.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-20.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-22.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-24.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-26.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-28.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-30.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-32.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-34.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-36.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-38.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-40.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-42.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-44.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-46.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-48.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-50.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-52.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-54.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-56.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-58.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-60.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-62.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-64.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-66.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-68.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-70.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-72.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-74.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-76.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-78.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-80.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-82.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-84.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-86.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-88.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-90.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-92.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-94.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-96.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-98.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-100.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-102.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-104.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-106.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-108.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-110.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-112.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-114.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-116.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-118.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-120.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-	-	-
-122.40000	15.45455	17.00000	0.0	0.0	0.0	0.0	-		



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No. J15050A, Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked.

Main data table with columns: Type/No., Name, Dist., X, Y, Z, Displacements (X, Y, Z), Horizontal displacement, Horizontal displacement to X Axis, Angle of Line to X Axis.



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No. J15050A, Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked.

Main data table with columns: Type/No., Name, Dist., X, Y, Z, Displacements (X, Y, Z), Horizontal displacement, Horizontal displacement to X Axis, Angle of Line to X Axis.



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC) J15050A**

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drng. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
<b>MP</b>	<b>08-Feb-2016</b>	

Type/No.	Coordinates			Displacements			Angle of Line		
	Name	Dist.		x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
115.45455	19.49495	17.00000	0.0	0.0	0.0	0.0			
116.98970	19.49495	17.00000	0.0	0.0	0.0	0.0			
118.48485	19.49495	17.00000	0.0	0.0	0.0	0.0			
120.00000	19.49495	17.00000	0.0	0.0	0.0	0.0			
121.66984	20.50505	17.00000	0.0	-4.0	0.0	0.0			
-28.48485	20.50505	17.00000	0.0	0.0	0.0	0.0			
-25.45455	20.50505	17.00000	0.0	0.0	0.0	0.0			
-23.93939	20.50505	17.00000	0.0	0.0	0.0	0.0			
-22.42424	20.50505	17.00000	0.0	0.0	0.0	0.0			
-19.39394	20.50505	17.00000	0.0	0.0	0.15462	0.0			
-17.87879	20.50505	17.00000	0.0	0.0	0.44027	0.0			
-16.36364	20.50505	17.00000	0.0	0.0	0.71862	0.0			
-14.84848	20.50505	17.00000	0.15790	-0.09466	1.0138	0.0			
-13.33333	20.50505	17.00000	0.43003	-0.32661	1.7004	0.0			
-11.81818	20.50505	17.00000	0.70552	-0.54372	1.9396	0.0			
-10.30303	20.50505	17.00000	1.02957	-0.74903	1.9800	0.0			
-8.78788	20.50505	17.00000	1.2098	-1.1708	2.2339	0.0			
-7.27273	20.50505	17.00000	1.2978	-1.5782	2.5796	0.0			
-5.75758	20.50505	17.00000	1.3853	-2.0464	2.9494	0.0			
-4.24242	20.50505	17.00000	1.2978	-2.5417	3.2957	0.0			
-2.72727	20.50505	17.00000	0.86376	-3.0317	3.6566	0.0			
1.21212	20.50505	17.00000	0.48127	-3.3769	3.7996	0.0			
0.30303	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
1.81818	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
3.33333	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
4.84848	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
6.36364	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
7.87879	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
9.39394	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
10.90909	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
12.42424	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
13.93939	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
15.45455	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
16.96970	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
18.48485	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
20.00000	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
21.51515	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
23.03030	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
24.54545	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
26.06061	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
27.57576	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
29.09091	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
30.60606	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
32.12122	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
33.63636	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
35.15152	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
36.66667	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
38.18182	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
39.69697	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
41.21212	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
42.72727	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
44.24242	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
45.75758	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
47.27273	20.50505	17.00000	0.0	-4.4973	4.4821	0.0			
48.78788	20.50505	17.00000	-0.33847	-4.4973	4.4821	0.0			
50.30303	20.50505	17.00000	-0.84710	-3.1283	3.6549	0.0			
51.81818	20.50505	17.00000	-1.2689	-2.1809	3.1283	0.0			
53.33333	20.50505	17.00000	-1.5696	-2.1809	3.0484	0.0			
54.84848	20.50505	17.00000	-1.7327	-1.7047	2.6994	0.0			
56.36364	20.50505	17.00000	-1.7327	-1.2316	2.3816	0.0			
57.87879	20.50505	17.00000	-1.0613	-0.93091	1.9968	0.0			
59.39394	20.50505	17.00000	-0.83889	-0.62858	1.7500	0.0			
60.90909	20.50505	17.00000	-0.52908	-0.34858	1.3810	0.0			
62.42424	20.50505	17.00000	-0.20268	-0.09498	0.9498	0.0			
63.93939	20.50505	17.00000	-0.01918	-0.010628	0.79453	0.0			
65.45455	20.50505	17.00000	0.0	0.0	0.64219	0.0			
66.96970	20.50505	17.00000	0.0	0.0	0.48219	0.0			
68.48485	20.50505	17.00000	0.0	0.0	0.0	0.0			
70.00000	20.50505	17.00000	0.0	0.0	0.0	0.0			
71.51515	20.50505	17.00000	0.0	0.0	0.0	0.0			
73.03030	20.50505	17.00000	0.0	0.0	0.0	0.0			
74.54545	20.50505	17.00000	0.0	0.0	0.0	0.0			
76.06061	20.50505	17.00000	0.0	0.0	0.0	0.0			
77.57576	20.50505	17.00000	0.0	0.0	0.0	0.0			
79.09091	20.50505	17.00000	0.0	0.0	0.0	0.0			
80.60606	20.50505	17.00000	0.0	0.0	0.0	0.0			
82.12122	20.50505	17.00000	-10.091	0.0	6.9817	0.0			
83.63636	20.50505	17.00000	-8.9150	0.0	6.0856	0.0			
85.15152	20.50505	17.00000	-7.8242	0.0	5.2449	0.0			
86.66667	20.50505	17.00000	-6.8080	0.0	4.5024	0.0			
88.18182	20.50505	17.00000	-5.8586	0.0	3.8586	0.0			
89.69697	20.50505	17.00000	-4.9559	0.0	3.3116	0.0			
91.21212	20.50505	17.00000	-4.0986	0.0	2.8696	0.0			
92.72727	20.50505	17.00000	-3.2709	0.0	2.5270	0.0			
94.24242	20.50505	17.00000	-2.4838	0.0	2.2816	0.0			
95.75758	20.50505	17.00000	-1.7088	0.0	2.1288	0.0			
97.27273	20.50505	17.00000	-1.1785	0.0	2.07625	0.0			
98.78788	20.50505	17.00000	-0.64824	0.0	2.03000	0.0			
100.30303	20.50505	17.00000	-0.11794	0.0	2.025700	0.0			
101.81818	20.50505	17.00000	0.0	0.0	0.0	0.0			
103.33333	20.50505	17.00000	0.0	0.0	0.0	0.0			
104.84848	20.50505	17.00000	0.0	0.0	0.0	0.0			
106.36364	20.50505	17.00000	0.0	0.0	0.0	0.0			
107.87879	20.50505	17.00000	0.0	0.0	0.0	0.0			
109.39394	20.50505	17.00000	0.0	0.0	0.0	0.0			
110.90909	20.50505	17.00000	0.0	0.0	0.0	0.0			
112.42424	20.50505	17.00000	0.0	0.0	0.0	0.0			
113.93939	20.50505	17.00000	0.0	0.0	0.0	0.0			
115.45455	20.50505	17.00000	0.0	0.0	0.0	0.0			
116.96970	20.50505	17.00000	0.0	0.0	0.0	0.0			
118.48485	20.50505	17.00000	0.0	0.0	0.0	0.0			
120.00000	20.50505	17.00000	0.0	0.0	0.0	0.0			
-28.48485	21.51515	17.00000	0.0	0.0	0.0	0.0			
-25.45455	21.51515	17.00000	0.0	0.0	0.0	0.0			
-23.93939	21.51515	17.00000	0.0	0.0	0.0	0.0			
-22.42424	21.51515	17.00000	0.0	0.0	0.0	0.0			
-20.90909	21.51515	17.00000	0.0	0.0	0.0	0.0			
-19.39394	21.51515	17.00000	0.0	0.0	0.07952	0.0			
-17.87879	21.51515	17.00000	0.0	0.0	0.44937	0.0			
-16.36364	21.51515	17.00000	0.0	0.0	0.81620	0.0			
-14.84848	21.51515	17.00000	0.07925	-0.04936	0.8907	0.0			
-13.33333	21.51515	17.00000	0.25738	-0.1368	1.0786	0.0			
-11.81818	21.51515	17.00000	0.55493	-0.44679	1.4444	0.0			
-10.30303	21.51515	17.00000	0.79404	-0.73311	1.7214	0.0			
-8.78788	21.51515	17.00000	0.97938	-1.0604	2.0179	0.0			
-7.27273	21.51515	17.00000	1.1268	-1.4449	2.3088	0.0			
-5.75758	21.51515	17.00000	1.1268	-1.8622	2.6417	0.0			
-4.24242	21.51515	17.00000	1.0798	-2.2812	2.9334	0.0			
-2.72727	21.51515	17.00000	0.76696	-2.6758	3.1798	0.0			
1.21212	21.51515	17.00000	0.37626	-2.9694	3.3643	0.0			
0.30303	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			
1.81818	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			
3.33333	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			
4.84848	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			
6.36364	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			
7.87879	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			
9.39394	21.51515	17.00000	0.0	-3.9569	3.8839	0.0			



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement to x Axis, Angle of Line to x Axis



GEA LIMITED

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The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement to x Axis, Angle of Line to x Axis



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with 3 columns: Job No., Sheet No., Rev.
Table with 3 columns: Drg. Ref., Date, Checked

Main data table with columns: Name, Type, Dist., x, y, z, Displacements, Angle of Line to x Axis



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with 3 columns: Job No., Sheet No., Rev.
Table with 3 columns: Drg. Ref., Date, Checked

Main data table with columns: Name, Type, Dist., x, y, z, Displacements, Angle of Line to x Axis







GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL

Wall Movements Rev 3 Piling and Excavation

Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Coordinates	Displacements	Angle of Line to x Axis						
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement
6.36364	31.61616	17.00000	0.0	0.0	0.0	0.47677			
7.87879	31.61616	17.00000	0.0	0.0	0.0	0.47677			
9.39394	31.61616	17.00000	0.0	0.0	0.0	0.47677			
10.90909	31.61616	17.00000	0.0	0.0	0.0	0.47677			
12.42424	31.61616	17.00000	0.0	0.0	0.0	0.47677			
13.93939	31.61616	17.00000	0.0	0.0	0.0	0.47677			
15.45455	31.61616	17.00000	0.0	0.0	0.0	0.47677			
16.96970	31.61616	17.00000	0.0	0.0	0.0	0.47677			
18.48485	31.61616	17.00000	0.0	0.0	0.0	0.47677			
20.00000	31.61616	17.00000	0.0	0.0	0.0	0.47677			
21.51515	31.61616	17.00000	0.0	0.0	0.0	0.47677			
23.03030	31.61616	17.00000	0.0	0.0	0.0	0.47677			
24.54545	31.61616	17.00000	0.0	0.0	0.0	0.47677			
26.06061	31.61616	17.00000	0.0	0.0	0.0	0.47677			
27.57576	31.61616	17.00000	0.0	0.0	0.0	0.47677			
29.09091	31.61616	17.00000	0.0	0.0	0.0	0.47677			
30.60606	31.61616	17.00000	0.0	0.0	0.0	0.47677			
32.12121	31.61616	17.00000	0.0	0.0	0.0	0.47677			
33.63636	31.61616	17.00000	0.0	0.0	0.0	0.47677			
35.15152	31.61616	17.00000	0.0	0.0	0.0	0.47677			
36.66667	31.61616	17.00000	0.0	0.0	0.0	0.47677			
38.18182	31.61616	17.00000	0.0	0.0	0.0	0.47677			
39.69697	31.61616	17.00000	0.0	0.0	0.0	0.47677			
41.21212	31.61616	17.00000	0.0	0.0	0.0	0.47677			
42.72727	31.61616	17.00000	0.0	0.0	0.0	0.47677			
44.24242	31.61616	17.00000	0.0	0.0	0.0	0.47677			
45.75758	31.61616	17.00000	0.0	0.0	0.0	0.47677			
47.27273	31.61616	17.00000	0.0	0.0	0.0	0.47677			
48.78788	31.61616	17.00000	0.0	0.0	0.0	0.47677			
50.30303	31.61616	17.00000	0.0	0.0	0.0	0.44982			
51.81818	31.61616	17.00000	0.0	0.0	0.0	0.40314			
53.33333	31.61616	17.00000	0.0	0.0	0.0	0.33435			
54.84848	31.61616	17.00000	0.0	0.0	0.0	0.14848			
56.36364	31.61616	17.00000	0.0	0.0	0.0	0.13055			
57.87879	31.61616	17.00000	0.0	0.0	0.0	0.0073505			
59.39394	31.61616	17.00000	0.0	0.0	0.0	0.0			
60.90909	31.61616	17.00000	0.0	0.0	0.0	0.0			
62.42424	31.61616	17.00000	0.0	0.0	0.0	0.0			
63.93939	31.61616	17.00000	0.0	0.0	0.0	0.0			
65.45455	31.61616	17.00000	0.0	0.0	0.0	0.0			
66.96970	31.61616	17.00000	0.0	0.0	0.0	0.0			
68.48485	31.61616	17.00000	0.0	0.0	0.0	0.0			
70.00000	31.61616	17.00000	0.0	0.0	0.0	0.0			
71.51515	31.61616	17.00000	0.0	0.0	0.0	0.0			
73.03030	31.61616	17.00000	0.0	0.0	0.0	0.0			
74.54545	31.61616	17.00000	0.0	0.0	0.0	0.0			
76.06061	31.61616	17.00000	0.0	0.0	0.0	0.0			
77.57576	31.61616	17.00000	0.0	0.0	0.0	0.0			
79.09091	31.61616	17.00000	0.0	0.0	0.0	0.0			
80.60606	31.61616	17.00000	0.0	0.0	0.0	0.0			
82.12121	31.61616	17.00000	-10.091	0.0	0.0	5.3817			
83.63636	31.61616	17.00000	-8.9150	0.0	0.0	6.0856			
85.15152	31.61616	17.00000	-7.8242	0.0	0.0	6.3230			
86.66667	31.61616	17.00000	-6.8080	0.0	0.0	5.7002			
88.18182	31.61616	17.00000	-5.8556	0.0	0.0	4.9924			
89.69697	31.61616	17.00000	-4.9559	0.0	0.0	4.1442			
91.21212	31.61616	17.00000	-4.2098	0.0	0.0	3.2696			
92.72727	31.61616	17.00000	-3.2709	0.0	0.0	2.4515			
94.24242	31.61616	17.00000	-2.4838	0.0	0.0	1.7423			
95.75758	31.61616	17.00000	-1.7088	0.0	0.0	1.1636			
97.27273	31.61616	17.00000	-0.9424	0.0	0.0	0.3303			
98.78788	31.61616	17.00000	-0.11794	0.0	0.0	0.0257000			
100.30303	31.61616	17.00000	0.0	0.0	0.0	0.0			
101.81818	31.61616	17.00000	0.0	0.0	0.0	0.0			
103.33333	31.61616	17.00000	0.0	0.0	0.0	0.0			
104.84848	31.61616	17.00000	0.0	0.0	0.0	0.0			
106.36364	31.61616	17.00000	0.0	0.0	0.0	0.0			
107.87879	31.61616	17.00000	0.0	0.0	0.0	0.0			
109.39394	31.61616	17.00000	0.0	0.0	0.0	0.0			
110.90909	31.61616	17.00000	0.0	0.0	0.0	0.0			
112.42424	31.61616	17.00000	0.0	0.0	0.0	0.0			
113.93939	31.61616	17.00000	0.0	0.0	0.0	0.0			
115.45455	31.61616	17.00000	0.0	0.0	0.0	0.0			
116.96970	31.61616	17.00000	0.0	0.0	0.0	0.0			
118.48485	31.61616	17.00000	0.0	0.0	0.0	0.0			
120.00000	31.61616	17.00000	0.0	0.0	0.0	0.0			
121.51515	31.61616	17.00000	0.0	0.0	0.0	0.0			
123.03030	31.61616	17.00000	0.0	0.0	0.0	0.0			
124.54545	31.61616	17.00000	0.0	0.0	0.0	0.0			
126.06061	31.61616	17.00000	0.0	0.0	0.0	0.0			
127.57576	31.61616	17.00000	0.0	0.0	0.0	0.0			
129.09091	31.61616	17.00000	0.0	0.0	0.0	0.0			
130.60606	31.61616	17.00000	0.0	0.0	0.0	0.0			
132.12121	31.61616	17.00000	0.0	0.0	0.0	0.0			
133.63636	31.61616	17.00000	0.0	0.0	0.0	0.0			
135.15152	31.61616	17.00000	0.0	0.0	0.0	0.0			
136.66667	31.61616	17.00000	0.0	0.0	0.0	0.0			
138.18182	31.61616	17.00000	0.0	0.0	0.0	0.0			
139.69697	31.61616	17.00000	0.0	0.0	0.0	0.0			
141.21212	31.61616	17.00000	0.0	0.0	0.0	0.0			
142.72727	31.61616	17.00000	0.0	0.0	0.0	0.0			
144.24242	31.61616	17.00000	0.0	0.0	0.0	0.0			
145.75758	31.61616	17.00000	0.0	0.0	0.0	0.0			
147.27273	31.61616	17.00000	0.0	0.0	0.0	0.0			
148.78788	31.61616	17.00000	0.0	0.0	0.0	0.0			
150.30303	31.61616	17.00000	0.0	0.0	0.0	0.0			
151.81818	31.61616	17.00000	0.0	0.0	0.0	0.0			
153.33333	31.61616	17.00000	0.0	0.0	0.0	0.0			
154.84848	31.61616	17.00000	0.0	0.0	0.0	0.0			
156.36364	31.61616	17.00000	0.0	0.0	0.0	0.0			
157.87879	31.61616	17.00000	0.0	0.0	0.0	0.0			
159.39394	31.61616	17.00000	0.0	0.0	0.0	0.0			
160.90909	31.61616	17.00000	0.0	0.0	0.0	0.0			
162.42424	31.61616	17.00000	0.0	0.0	0.0	0.0			
163.93939	31.61616	17.00000	0.0	0.0	0.0	0.0			
165.45455	31.61616	17.00000	0.0	0.0	0.0	0.0			
166.96970	31.61616	17.00000	0.0	0.0	0.0	0.0			
168.48485	31.61616	17.00000	0.0	0.0	0.0	0.0			
170.00000	31.61616	17.00000	0.0	0.0	0.0	0.0			
171.51515	31.61616	17.00000	0.0	0.0	0.0	0.0			
173.03030	31.61616	17.00000	0.0	0.0	0.0	0.0			
174.54545	31.61616	17.00000	0.0	0.0	0.0	0.0			
176.06061	31.61616	17.00000	0.0	0.0	0.0	0.0			
177.57576	31.61616	17.00000	0.0	0.0	0.0	0.0			
179.09091	31.61616	17.00000	0.0	0.0	0.0	0.0			
180.60606	31.61616	17.00000	0.0	0.0	0.0	0.0			
182.12121	31.61616	17.00000	-10.091	0.0	0.0	5.3817			
183.63636	31.61616	17.00000	-8.9150	0.0	0.0	6.0856			
185.15152	31.61616	17.00000	-7.8242	0.0	0.0	6.3230			
186.66667	31.61616	17.00000	-6.8080	0.0	0.0	5.7002			
188.18182	31.61616	17.00000	-5.8556	0.0	0.0	4.9924			
189.69697	31.61616	17.00000	-4.9559	0.0	0.0	4.1442			
191.21212	31.61616	17.00000	-4.2098	0.0	0.0	3.2696			
192.72727	31.61616	17.00000	-3.2709	0.0	0.0	2.4515			
194.24242	31.61616	17.00000	-2.4838	0.0	0.0	1.7423			
195.75758	31.61616	17.00000	-1.7088	0.0	0.0	1.1636			
197.27273	31.61616	17.00000	-0.9424	0.0	0.0	0.3303			
198.78788	31.61616	17.00000	-0.11794	0.0	0.0	0.0257000			
200.30303	31.61616	17.00000	0.0	0.0	0.0	0.0			
201.81818	31.61616	17.00000	0.0	0.0	0.0	0.0			
203.3									





GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement to x Axis, Angle of Line to x Axis



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The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement to x Axis, Angle of Line to x Axis



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.		Coordinates			Displacements			Angle of Lime		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
103.33333	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
104.84848	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
110.93939	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
107.87879	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
110.93939	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
110.93939	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
112.42424	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
113.93939	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
115.44545	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
116.96970	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
118.48485	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
120.00000	36.66667	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-30.00000	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-28.48485	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-26.96970	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-25.45455	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-23.93939	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-22.42424	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-20.90909	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
13.93939	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-17.87879	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-16.36364	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-14.84848	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-13.33333	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-11.81818	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-10.30303	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-8.78788	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-7.27273	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-5.75758	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-4.24242	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-2.72727	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
0.30303	38.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
1.81818	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
3.33333	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
4.84848	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
6.36364	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
7.87879	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
9.39394	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
10.90909	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
12.42424	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
13.93939	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
15.45455	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
16.96970	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
18.48485	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
19.99999	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
21.51515	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
23.03030	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
24.54545	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
26.06061	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
27.57576	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
29.09091	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
30.60606	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
32.12121	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
33.63636	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
35.15152	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
36.66667	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
38.18182	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
39.69697	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
41.21212	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
42.72727	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
44.24242	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
45.75758	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
47.27273	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
48.78788	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
50.30303	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
51.81818	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
53.33333	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
54.84848	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
56.36364	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
57.87879	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
59.39394	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
60.90909	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
62.42424	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
63.93939	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
65.45455	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
66.96970	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
68.48485	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
70.00000	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
71.51515	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
73.03030	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
74.54545	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
76.06061	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
77.57576	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
79.09091	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
80.60606	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
82.12121	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
83.63636	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
85.15152	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
86.66667	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
88.18182	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
89.69697	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
91.21212	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
92.72727	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
94.24242	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
95.75758	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
97.27273	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
98.78788	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
100.30303	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
101.81818	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
103.33333	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
104.84848	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
106.36364	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
107.87879	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
109.39394	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
110.90909	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
112.42424	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
113.93939	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
115.45455	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
116.96970	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
120.00000	37.67677	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-30.00000	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-26.96970	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-23.93939	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-20.90909	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-19.39394	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-17.87879	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-16.36364	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-14.84848	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-13.33333	39.68687	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
-11.81818	39.68687	17.00000	0.0	0.0						



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., X, Y, Z, Displacements (X, Y, Z), Horizontal displacement, Horizontal displacement to X Axis, Angle of Line to X Axis



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(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Coordinates	Displacements		Angle of Line	
Name	Dist.	x	y	Horizontal displacement	Horizontal to x Axis
118.4845	50.80808	17.00000	0.0	0.0	0.0
120.00000	50.80808	17.00000	0.0	0.0	0.0
-10.00000	51.81818	17.00000	0.0	0.0	0.0
-28.4845	51.81818	17.00000	0.0	0.0	0.0
-26.86970	51.81818	17.00000	0.0	0.0	0.0
-25.45455	51.81818	17.00000	0.0	0.0	0.0
-23.93939	51.81818	17.00000	0.0	0.0	0.0
-22.42424	51.81818	17.00000	0.0	0.0	0.0
-20.90909	51.81818	17.00000	0.0	0.0	0.0
-19.39394	51.81818	17.00000	0.0	0.0	0.0
-17.87879	51.81818	17.00000	0.0	0.0	0.0
-16.36364	51.81818	17.00000	0.0	0.0	0.0
-14.84848	51.81818	17.00000	0.0	0.0	0.0
-13.33333	51.81818	17.00000	0.0	0.0	0.0
-11.81818	51.81818	17.00000	0.0	0.0	0.0
-10.30303	51.81818	17.00000	0.0	0.0	0.0
-8.78788	51.81818	17.00000	0.0	0.0	0.0
-7.27273	51.81818	17.00000	0.0	0.0	0.0
-5.75758	51.81818	17.00000	0.0	0.0	0.0
-4.24242	51.81818	17.00000	0.0	0.0	0.0
-2.72727	51.81818	17.00000	0.0	0.0	0.0
1.18182	51.81818	17.00000	0.0	0.0	0.0
3.10303	51.81818	17.00000	0.0	0.0	0.0
1.81818	51.81818	17.00000	0.0	0.0	0.0
3.33333	51.81818	17.00000	0.0	0.0	0.0
4.84848	51.81818	17.00000	0.0	0.0	0.0
6.36364	51.81818	17.00000	0.0	0.0	0.0
7.87879	51.81818	17.00000	0.0	0.0	0.0
9.39394	51.81818	17.00000	0.0	0.0	0.0
10.90909	51.81818	17.00000	0.0	0.0	0.0
12.42424	51.81818	17.00000	0.0	0.0	0.0
13.93939	51.81818	17.00000	0.0	0.0	0.0
15.45455	51.81818	17.00000	0.0	0.0	0.0
16.96970	51.81818	17.00000	0.0	0.0	0.0
18.4845	51.81818	17.00000	0.0	0.0	0.0
20.00000	51.81818	17.00000	0.0	0.0	0.0
21.51515	51.81818	17.00000	0.0	0.0	0.0
23.03030	51.81818	17.00000	0.0	0.0	0.0
24.54545	51.81818	17.00000	0.0	0.0	0.0
26.06061	51.81818	17.00000	0.0	0.0	0.0
27.57576	51.81818	17.00000	0.0	0.0	0.0
29.09091	51.81818	17.00000	0.0	0.0	0.0
30.60606	51.81818	17.00000	0.0	0.0	0.0
32.12122	51.81818	17.00000	0.0	0.0	0.0
33.63636	51.81818	17.00000	0.0	0.0	0.0
35.15152	51.81818	17.00000	0.0	0.0	0.0
36.66667	51.81818	17.00000	0.0	0.0	0.0
38.18182	51.81818	17.00000	0.0	0.0	0.0
39.69697	51.81818	17.00000	0.0	0.0	0.0
41.21212	51.81818	17.00000	0.0	0.0	0.0
42.72727	51.81818	17.00000	0.0	0.0	0.0
44.24242	51.81818	17.00000	0.0	0.0	0.0
45.75758	51.81818	17.00000	0.0	0.0	0.0
47.27273	51.81818	17.00000	0.0	0.0	0.0
48.78788	51.81818	17.00000	0.0	0.0	0.0
50.30303	51.81818	17.00000	0.0	0.0	0.0
51.81818	51.81818	17.00000	0.0	0.0	0.0
53.33333	51.81818	17.00000	0.0	0.0	0.0
54.84848	51.81818	17.00000	0.0	0.0	0.0
56.36364	51.81818	17.00000	0.0	0.0	0.0
57.87879	51.81818	17.00000	0.030664	-0.26575	0.009590
59.39394	51.81818	17.00000	0.090397	-0.068137	0.12731
60.90909	51.81818	17.00000	0.21788	-0.28234	0.42467
62.42424	51.81818	17.00000	0.45409	-0.42444	0.84089
63.93939	51.81818	17.00000	0.31854	-0.62115	0.83264
65.45455	51.81818	17.00000	0.16318	-0.80007	1.07313
66.96970	51.81818	17.00000	0.30552	-1.1915	1.3204
68.4845	51.81818	17.00000	0.18700	-1.6719	1.7347
70.00000	51.81818	17.00000	0.0	-2.1515	1.9801
73.03030	51.81818	17.00000	0.0	-2.4373	1.9801
74.54545	51.81818	17.00000	0.0	-2.4373	1.9801
76.06061	51.81818	17.00000	0.0	-2.4373	1.9801
77.57576	51.81818	17.00000	0.0	-2.4373	1.9801
79.09091	51.81818	17.00000	0.0	-2.4373	1.9801
80.60606	51.81818	17.00000	0.0	-2.4373	1.9801
82.12122	51.81818	17.00000	-0.107110	-1.6682	1.6686
83.63636	51.81818	17.00000	-0.21721	-1.5688	1.6686
85.15152	51.81818	17.00000	-0.36929	-1.3866	1.5615
86.66667	51.81818	17.00000	-0.45059	-1.1398	1.3660
88.18182	51.81818	17.00000	-0.46732	-0.8582	1.1584
89.69697	51.81818	17.00000	-0.42756	-0.45648	0.93385
91.21212	51.81818	17.00000	-0.33978	-0.05894	0.70344
92.72727	51.81818	17.00000	-0.29689	-0.32709	0.47221
94.24242	51.81818	17.00000	-0.19179	-0.8810	0.28858
95.75758	51.81818	17.00000	-0.064684	-0.25877	0.20394
97.27273	51.81818	17.00000	0.0	0.0	0.0
98.78788	51.81818	17.00000	0.0	0.0	0.0
100.30303	51.81818	17.00000	0.0	0.0	0.0
101.81818	51.81818	17.00000	0.0	0.0	0.0
103.33333	51.81818	17.00000	0.0	0.0	0.0
104.84848	51.81818	17.00000	0.0	0.0	0.0
106.36364	51.81818	17.00000	0.0	0.0	0.0
107.87879	51.81818	17.00000	0.0	0.0	0.0
109.39394	51.81818	17.00000	0.0	0.0	0.0
110.90909	51.81818	17.00000	0.0	0.0	0.0
112.42424	51.81818	17.00000	0.0	0.0	0.0
113.93939	51.81818	17.00000	0.0	0.0	0.0
115.45455	51.81818	17.00000	0.0	0.0	0.0
116.96970	51.81818	17.00000	0.0	0.0	0.0
118.4845	51.81818	17.00000	0.0	0.0	0.0
120.00000	51.81818	17.00000	0.0	0.0	0.0
-28.4845	52.82828	17.00000	0.0	0.0	0.0
-26.86970	52.82828	17.00000	0.0	0.0	0.0
-25.45455	52.82828	17.00000	0.0	0.0	0.0
-23.93939	52.82828	17.00000	0.0	0.0	0.0
-22.42424	52.82828	17.00000	0.0	0.0	0.0
-20.90909	52.82828	17.00000	0.0	0.0	0.0
-19.39394	52.82828	17.00000	0.0	0.0	0.0
-17.87879	52.82828	17.00000	0.0	0.0	0.0
-16.36364	52.82828	17.00000	0.0	0.0	0.0
-14.84848	52.82828	17.00000	0.0	0.0	0.0
-13.33333	52.82828	17.00000	0.0	0.0	0.0
-11.81818	52.82828	17.00000	0.0	0.0	0.0
-10.30303	52.82828	17.00000	0.0	0.0	0.0
-8.78788	52.82828	17.00000	0.0	0.0	0.0
-7.27273	52.82828	17.00000	0.0	0.0	0.0
-5.75758	52.82828	17.00000	0.0	0.0	0.0
-4.24242	52.82828	17.00000	0.0	0.0	0.0
-2.72727	52.82828	17.00000	0.0	0.0	0.0
1.18182	52.82828	17.00000	0.0	0.0	0.0
3.10303	52.82828	17.00000	0.0	0.0	0.0
1.81818	52.82828	17.00000	0.0	0.0	0.0
3.33333	52.82828	17.00000	0.0	0.0	0.0
4.84848	52.82828	17.00000	0.0	0.0	0.0
6.36364	52.82828	17.00000	0.0	0.0	0.0
7.87879	52.82828	17.00000	0.0	0.0	0.0
9.39394	52.82828	17.00000	0.0	0.0	0.0
10.90909	52.82828	17.00000	0.0	0.0	0.0
12.42424	52.82828	17.00000	0.0	0.0	0.0
13.93939	52.82828	17.00000	0.0	0.0	0.0
15.45455	52.82828	17.00000	0.0	0.0	0.0
16.96970	52.82828	17.00000	0.0	0.0	0.0
18.4845	52.82828	17.00000	0.0	0.0	0.0
20.00000	52.82828	17.00000	0.0	0.0	0.0
21.51515	52.82828	17.00000	0.0	0.0	0.0
23.03030	52.82828	17.00000	0.0	0.0	0.0
24.54545	52.82828	17.00000	0.0	0.0	0.0
26.06061	52.82828	17.00000	0.0	0.0	0.0
27.57576	52.82828	17.00000	0.0	0.0	0.0



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.	Coordinates	Displacements		Angle of Line	
Name	Dist.	x	y	Horizontal displacement	Horizontal to x Axis
29.09091	52.82828	17.00000	0.0	0.0	0.0
30.60606	52.82828	17.00000	0.0	0.0	0.0
32.12122	52.82828	17.00000	0.0	0.0	0.0
33.63636	52.82828	17.00000	0.0	0.0	0.0
35.15152	52.82828	17.00000	0.0	0.0	0.0
36.66667	52.82828	17.00000	0.0	0.0	0.0
38.18182	52.82828	17.00000	0.0	0.0	0.0
39.69697	52.82828	17.00000	0.0	0.0	0.0
41.21212	52.82828	17.00000	0.0	0.0	0.0
42.72727	52.82828	17.00000	0.0	0.0	0.0
44.24242	52.82828	17.00000	0.0	0.0	0.0
45.75758	52.82828	17.00000	0.0	0.0	0.0
47.27273	52.82828	17.00000	0.0	0.0	0.0
48.78788	52.82828	17.00000	0.0	0.0	0.0
50.30303	52.82828	17.00000	0.0	0.0	0.0
51.81818	52.82828	17.00000	0.0	0.0	0.0
53.33333	52.82828	17.00000	0.0	0.0	0.0
54.84848	52.82828	17.00000	0.0	0.0	0.0
56.36364	52.82828	17.00000	0.0	0.0	0.0
57.87879	52.82828	17.00000	0.054137	-0.05729	0.054137
59.39394	52.82828	17.00000	0.11463	-0.13864	0.11837
60.90909	52.82828	17.00000	0.17220	-0.24299	0.23244
62.42424	52.82828	17.00000	0.23881	-0.	



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The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement, Angle of Line to x Axis



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The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement, Angle of Line to x Axis





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The Great Hall, Lincoln's Inn, Newmar's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by	Date	Checked
MP	08-Feb-2016	

Type/No.		Coordinates			Displacements			Angle of Line		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
63.93939	56.86869	17.00000	0.035246	-0.098101	0.03424	-	-	-	-	-
65.45455	56.86869	17.00000	0.048317	-0.17931	0.12454	-	-	-	-	-
66.96970	56.86869	17.00000	0.045959	-0.25477	0.19959	-	-	-	-	-
68.48485	56.86869	17.00000	0.028440	-0.31463	0.25588	-	-	-	-	-
70.00000	56.86869	17.00000	0.0	-0.35603	0.28744	-	-	-	-	-
71.51515	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
73.03030	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
74.54545	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
76.06061	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
77.57576	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
79.09091	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
80.60606	56.86869	17.00000	0.0	-0.53139	0.31772	-	-	-	-	-
82.12121	56.86869	17.00000	-0.002532	-0.35551	0.28728	-	-	-	-	-
83.63636	56.86869	17.00000	-0.020552	-0.35055	0.26758	-	-	-	-	-
85.15152	56.86869	17.00000	-0.052511	-0.27914	0.21835	-	-	-	-	-
86.66667	56.86869	17.00000	-0.084531	-0.14037	0.14037	-	-	-	-	-
88.18182	56.86869	17.00000	-0.042639	-0.11635	0.034163	-	-	-	-	-
89.69697	56.86869	17.00000	-0.073251	-0.01619	0.005031	-	-	-	-	-
91.21212	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
92.72727	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
94.24242	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
95.75758	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
97.27273	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
98.78788	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
100.30303	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
101.81818	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
103.33333	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
104.84848	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
106.36364	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
107.87879	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
109.39394	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
110.90909	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
112.42424	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
113.93939	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
115.45455	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
116.96970	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
118.48485	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
120.00000	56.86869	17.00000	0.0	0.0	0.0	-	-	-	-	-
-30.00000	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-28.48485	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-26.96970	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-25.45455	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-23.93939	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-22.42424	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-20.90909	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-19.39394	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-17.87879	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-16.36364	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-14.84848	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-13.33333	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-11.81818	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-10.30303	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-8.78788	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-7.27273	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-5.75758	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-4.24242	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-2.72727	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
-1.21212	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
0.30303	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
1.81818	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
3.33333	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
4.84848	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
6.36364	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
7.87879	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
9.39394	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
10.90909	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
12.42424	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
13.93939	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
15.45455	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
16.96970	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
18.48485	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
20.00000	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
21.51515	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
23.03030	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
24.54545	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
26.06061	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
27.57576	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
29.09091	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
30.60606	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
32.12121	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
33.63636	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
35.15152	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
36.66667	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
38.18182	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
39.69697	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
41.21212	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
42.72727	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
44.24242	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
45.75758	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
47.27273	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
48.78788	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
50.30303	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
51.81818	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
53.33333	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
54.84848	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
56.36364	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
57.87879	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
59.39394	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
60.90909	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
62.42424	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
63.93939	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
65.45455	57.87879	17.00000	0.0076372	-0.038040	0.0071465	-	-	-	-	-
66.96970	57.87879	17.00000	0.0147628	-0.080677	0.016284	-	-	-	-	-
68.48485	57.87879	17.00000	0.011034	-0.13020	0.046637	-	-	-	-	-
70.00000	57.87879	17.00000	0.0	-0.15300	0.059333	-	-	-	-	-
71.51515	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
73.03030	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
74.54545	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
76.06061	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
77.57576	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
79.09091	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
80.60606	57.87879	17.00000	0.0	-0.22836	0.075123	-	-	-	-	-
82.12121	57.87879	17.00000	-0.0010350	-0.15266	0.038535	-	-	-	-	-
83.63636	57.87879	17.00000	-0.012286	-0.14653	0.039897	-	-	-	-	-
85.15152	57.87879	17.00000	-0.016222	-0.092029	0.022925	-	-	-	-	-
86.66667	57.87879	17.00000	-0.0070215	-0.052052	0.0097811	-	-	-	-	-
88.18182	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
89.69697	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
91.21212	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
92.72727	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
94.24242	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
95.75758	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
97.27273	57.87879	17.00000	0.0	0.0	0.0	-	-	-	-	-
98.78788	57.878									





GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.		Coordinates			Displacements			Angle of Lime		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
9.39394	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
10.90909	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
12.42424	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
13.93939	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
15.45455	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
16.96970	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
18.48485	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
20.00000	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
21.51515	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
23.03030	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
24.54545	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
26.06061	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
27.57576	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
29.09091	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
30.60606	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
32.12121	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
33.63636	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
35.15152	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
36.66667	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
38.18182	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
39.69697	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
41.21212	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
42.72727	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
44.24242	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
45.75758	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
47.27273	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
48.78788	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
50.30303	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
51.81818	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
53.33333	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
54.84848	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
56.36364	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
57.87879	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
59.39394	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
60.90909	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
62.42424	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
63.93939	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
65.45455	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
66.96970	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
68.48485	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
70.00000	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
71.51515	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
73.03030	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
74.54545	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
76.06061	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
77.57576	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
79.09091	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
80.60606	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
82.12121	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
83.63636	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
85.15152	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
86.66667	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
88.18182	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
89.69697	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
91.21212	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
92.72727	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
94.24242	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
95.75758	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
97.27273	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
98.78788	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
100.30303	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
101.81818	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
103.33333	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
104.84848	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
106.36364	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
107.87879	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
109.39394	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
110.90909	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
112.42424	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
113.93939	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
115.45455	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
116.96970	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
118.48485	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
120.00000	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
121.51515	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
123.03030	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
124.54545	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
126.06061	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
127.57576	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
129.09091	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
130.60606	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
132.12121	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
133.63636	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
135.15152	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
136.66667	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
138.18182	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
139.69697	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
141.21212	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
142.72727	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
144.24242	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
145.75758	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
147.27273	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
148.78788	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
150.30303	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
151.81818	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
153.33333	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
154.84848	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
156.36364	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
157.87879	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
159.39394	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
160.90909	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
162.42424	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
163.93939	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
165.45455	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
166.96970	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
168.48485	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
170.00000	62.92929	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.		Coordinates			Displacements			Angle of Lime		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	to x Axis
71.51515	63.93939	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
73.03030	63.93939	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
74.54545	63.93939	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
76.06061	63.93939	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
77.57576	63.93939	17.00000	0.0	0.0	0.0	0.0	0.0	-	-	-
79.09091	63.93939	17.00000	0.0	0.0	0					



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmar's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Job No.	Sheet No.	Rev.
Drg. Ref.		
Made by MP	Date 08-Feb-2016	Checked

Type/No.		Coordinates			Displacements			Angle of Line to x Axis		
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	
-17.87879	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-16.76364	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-14.48448	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-13.33333	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-11.81818	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-10.10303	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-8.78788	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-7.27273	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-5.75758	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-4.24242	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-2.72727	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-1.21212	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.30303	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.81818	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3.33333	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4.84848	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
6.36364	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7.87879	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
9.39394	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
10.90909	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12.42424	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
13.93939	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
15.45455	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
16.96970	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
18.48485	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20.00000	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
21.51515	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
23.03030	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24.54545	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
26.06061	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
27.57576	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
29.09091	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
30.60606	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
32.12121	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
33.63636	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
35.15152	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
36.66667	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
38.18182	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
39.69697	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
41.21212	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
42.72727	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
44.24242	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
45.75758	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
47.27273	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
48.78788	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
50.30303	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
51.81818	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
53.33333	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
54.84848	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
56.36364	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
57.87879	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
59.39394	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
60.90909	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
62.42424	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
63.93939	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
65.45455	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
66.96970	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
68.48485	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
69.99999	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
71.51515	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
73.03030	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
74.54545	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
76.06061	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
77.57576	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
79.09091	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80.60606	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
82.12121	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
83.63636	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
85.15152	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
86.66667	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
88.18182	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
89.69697	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
91.21212	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
92.72727	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
94.24242	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
95.75758	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
97.27273	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
98.78788	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
100.30303	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
101.81818	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
103.33333	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
104.84848	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
106.36364	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
107.87879	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
109.39394	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
110.90909	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
112.42424	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
113.93939	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
115.45455	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
116.96970	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
118.48485	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
120.00000	65.95960	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-10.00000	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-18.48485	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-26.96970	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-35.45455	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-23.93939	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-22.42424	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-20.90909	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-19.39394	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-17.87879	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-16.36364	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-14.84848	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-13.33333	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-11.81818	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-10.30303	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-8.78788	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-7.27273	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-5.75758	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
-4.24242	66.96970	17.00000	0.0	0.0	0.0	0.0	0.0			



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement, Angle of Line to x Axis



GEA LIMITED

(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Type/No., Name, Dist., x, y, z, Displacements (x, y, z), Horizontal displacement, Horizontal displacement, Angle of Line to x Axis



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC)**

The Great Hall, Lincoln's Inn, Newmans Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>J15050A</b>		
<b>Drg. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
<b>MP</b>	<b>08-Feb-2016</b>	

Type/No.	Coordinates	Displacements	Angle of Line								
Name	Dist.	x	y	z	x	y	z	Horizontal displacement	Horizontal displacement	Horizontal displacement	to x Axis
Line 4	Line 4	48.0000	12.0000	17.0000	0.0	-8.1384	5.9885	0.0	0.0	0.0	270.0
	1.0000	48.0000	11.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	2.0000	48.0000	10.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	3.0000	48.0000	9.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	4.0000	48.0000	8.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	5.0000	48.0000	7.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	6.0000	48.0000	6.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	7.0000	48.0000	5.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	8.0000	48.0000	4.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	9.0000	48.0000	3.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	10.0000	48.0000	2.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
	11.0000	48.0000	1.0000	17.0000	-9.9402	0.0	6.1741	0.0	-9.9402	0.0	270.0
Line 5	Line 5	48.0350	1.0000	17.0000	-9.9201	0.0	6.2163	-9.9201	0.0	0.0	0.0
	0.2622	48.0350	1.0000	17.0000	-9.1858	0.0	6.2163	-9.1858	0.0	0.0	0.0
	1.2520	49.9750	1.0000	17.0000	-8.4998	0.0	6.1066	-8.4998	0.0	0.0	0.0
	2.8875	50.9375	1.0000	17.0000	-7.1218	0.0	7.1312	-7.1218	0.0	0.0	0.0
	3.8500	51.9000	1.0000	17.0000	-7.2108	0.0	6.9078	-7.2108	0.0	0.0	0.0
	4.8125	52.8625	1.0000	17.0000	-7.1466	0.0	6.6785	-7.1466	0.0	0.0	0.0
	5.7750	53.8250	1.0000	17.0000	-7.0327	0.0	6.4492	-7.0327	0.0	0.0	0.0
	6.7375	54.7875	1.0000	17.0000	-6.8698	0.0	6.2199	-6.8698	0.0	0.0	0.0
	7.7000	55.7500	1.0000	17.0000	-6.6680	0.0	5.9906	-6.6680	0.0	0.0	0.0
	8.6625	56.7125	1.0000	17.0000	-6.4282	0.0	5.7613	-6.4282	0.0	0.0	0.0
	9.6250	57.6750	1.0000	17.0000	-6.1511	0.0	5.5320	-6.1511	0.0	0.0	0.0
	10.5875	58.6375	1.0000	17.0000	-5.8278	0.0	5.3027	-5.8278	0.0	0.0	0.0
	11.5500	59.6000	1.0000	17.0000	-5.4592	0.0	5.0734	-5.4592	0.0	0.0	0.0
	12.5125	60.5625	1.0000	17.0000	-5.0453	0.0	4.8441	-5.0453	0.0	0.0	0.0
	13.4750	61.5250	1.0000	17.0000	-4.5868	0.0	4.6148	-4.5868	0.0	0.0	0.0
	14.4375	62.4875	1.0000	17.0000	-4.0943	0.0	4.3855	-4.0943	0.0	0.0	0.0
	15.4000	63.4500	1.0000	17.0000	-3.5678	0.0	4.1562	-3.5678	0.0	0.0	0.0
	16.3625	64.4125	1.0000	17.0000	-3.0083	0.0	3.9269	-3.0083	0.0	0.0	0.0
	17.3250	65.3750	1.0000	17.0000	-2.4158	0.0	3.6976	-2.4158	0.0	0.0	0.0
	18.2875	66.3375	1.0000	17.0000	-1.7903	0.0	3.4683	-1.7903	0.0	0.0	0.0
	19.2500	67.3000	1.0000	17.0000	-1.1318	0.0	3.2390	-1.1318	0.0	0.0	0.0
	20.2125	68.2625	1.0000	17.0000	-0.4413	0.0	3.0097	-0.4413	0.0	0.0	0.0
	21.1750	69.2250	1.0000	17.0000	0.2602	0.0	2.7804	0.2602	0.0	0.0	0.0
	22.1375	70.1875	1.0000	17.0000	0.9607	0.0	2.5511	0.9607	0.0	0.0	0.0
	23.1000	71.1500	1.0000	17.0000	1.6412	0.0	2.3218	1.6412	0.0	0.0	0.0
	24.0625	72.1125	1.0000	17.0000	2.2917	0.0	2.0925	2.2917	0.0	0.0	0.0
	25.0250	73.0750	1.0000	17.0000	2.9022	0.0	1.8632	2.9022	0.0	0.0	0.0
	25.9875	74.0375	1.0000	17.0000	3.3727	0.0	1.6339	3.3727	0.0	0.0	0.0
	26.9500	75.0000	1.0000	17.0000	3.7032	0.0	1.4046	3.7032	0.0	0.0	0.0
	27.9125	75.9625	1.0000	17.0000	3.8937	0.0	1.1753	3.8937	0.0	0.0	0.0
	28.8750	76.9250	1.0000	17.0000	3.9442	0.0	0.9460	3.9442	0.0	0.0	0.0
	29.8375	77.8875	1.0000	17.0000	3.8547	0.0	0.7167	3.8547	0.0	0.0	0.0
	30.8000	78.8500	1.0000	17.0000	3.6254	0.0	0.4874	3.6254	0.0	0.0	0.0
	31.7625	79.8125	1.0000	17.0000	3.2559	0.0	0.2581	3.2559	0.0	0.0	0.0
	32.7250	80.7750	1.0000	17.0000	2.7564	0.0	0.0288	3.2559	0.0	0.0	0.0
	33.6875	81.7375	1.0000	17.0000	2.1369	0.0	-0.1907	3.2559	0.0	0.0	0.0
	34.6500	82.7000	1.0000	17.0000	1.4174	0.0	-0.4002	3.2559	0.0	0.0	0.0
	35.6125	83.6625	1.0000	17.0000	0.6079	0.0	-0.6097	3.2559	0.0	0.0	0.0
	36.5750	84.6250	1.0000	17.0000	-0.2018	0.0	-0.8192	3.2559	0.0	0.0	0.0
	37.5375	85.5875	1.0000	17.0000	-0.9023	0.0	-1.0287	3.2559	0.0	0.0	0.0
	38.5000	86.5500	1.0000	17.0000	-1.5028	0.0	-1.2382	3.2559	0.0	0.0	0.0
	39.4625	87.5125	1.0000	17.0000	-2.0033	0.0	-1.4477	3.2559	0.0	0.0	0.0
	40.4250	88.4750	1.0000	17.0000	-2.4038	0.0	-1.6572	3.2559	0.0	0.0	0.0
	41.3875	89.4375	1.0000	17.0000	-2.7043	0.0	-1.8667	3.2559	0.0	0.0	0.0
	42.3500	90.4000	1.0000	17.0000	-2.9048	0.0	-2.0762	3.2559	0.0	0.0	0.0
	43.3125	91.3625	1.0000	17.0000	-2.9953	0.0	-2.2857	3.2559	0.0	0.0	0.0
	44.2750	92.3250	1.0000	17.0000	-2.9758	0.0	-2.4952	3.2559	0.0	0.0	0.0
	45.2375	93.2875	1.0000	17.0000	-2.8463	0.0	-2.7047	3.2559	0.0	0.0	0.0
	46.2000	94.2500	1.0000	17.0000	-2.6068	0.0	-2.9142	3.2559	0.0	0.0	0.0
	47.1625	95.2125	1.0000	17.0000	-2.2573	0.0	-3.1237	3.2559	0.0	0.0	0.0
	48.1250	96.1750	1.0000	17.0000	-1.8078	0.0	-3.3332	3.2559	0.0	0.0	0.0
	49.0875	97.1375	1.0000	17.0000	-1.2583	0.0	-3.5427	3.2559	0.0	0.0	0.0
	50.0500	98.1000	1.0000	17.0000	-0.6088	0.0	-3.7522	3.2559	0.0	0.0	0.0
	51.0125	99.0625	1.0000	17.0000	0.1417	0.0	-3.9617	3.2559	0.0	0.0	0.0
	51.9750	100.0250	1.0000	17.0000	0.7922	0.0	-4.1712	3.2559	0.0	0.0	0.0
	52.9375	100.9875	1.0000	17.0000	1.3427	0.0	-4.3807	3.2559	0.0	0.0	0.0
	53.9000	101.9500	1.0000	17.0000	1.7932	0.0	-4.5902	3.2559	0.0	0.0	0.0
	54.8625	102.9125	1.0000	17.0000	2.1437	0.0	-4.7997	3.2559	0.0	0.0	0.0
	55.8250	103.8750	1.0000	17.0000	2.3942	0.0	-5.0092	3.2559	0.0	0.0	0.0
	56.7875	104.8375	1.0000	17.0000	2.5447	0.0	-5.2187	3.2559	0.0	0.0	0.0
	57.7500	105.8000	1.0000	17.0000	2.5952	0.0	-5.4282	3.2559	0.0	0.0	0.0
	58.7125	106.7625	1.0000	17.0000	2.5457	0.0	-5.6377	3.2559	0.0	0.0	0.0
	59.6750	107.7250	1.0000	17.0000	2.3962	0.0	-5.8472	3.2559	0.0	0.0	0.0
	60.6375	108.6875	1.0000	17.0000	2.1467	0.0	-6.0567	3.2559	0.0	0.0	0.0
	61.6000	109.6500	1.0000	17.0000	1.8072	0.0	-6.2662	3.2559	0.0	0.0	0.0
	62.5625	110.6125	1.0000	17.0000	1.3877	0.0	-6.4757	3.2559	0.0	0.0	0.0
	63.5250	111.5750	1.0000	17.0000	0.9082	0.0	-6.6852	3.2559	0.0	0.0	0.0
	64.4875	112.5375	1.0000	17.0000	0.3687	0.0	-6.8947	3.2559	0.0	0.0	0.0
	65.4500	113.5000	1.0000	17.0000	-0.1408	0.0	-7.1042	3.2559	0.0	0.0	0.0
	66.4125	114.4625	1.0000	17.0000	-0.6413	0.0	-7.3137	3.2559	0.0	0.0	0.0
	67.3750	115.4250	1.0000	17.0000	-1.1418	0.0	-7.5232	3.2559	0.0	0.0	0.0
	68.3375	116.3875	1.0000	17.0000	-1.6423	0.0	-7.7327	3.2559	0.0	0.0	0.0
	69.3000	117.3500	1.0000	17.0000	-2.1428	0.0	-7.9422	3.2559	0.0	0.0	0.0
	70.2625	118.3125	1.0000	17.0000	-2.6433	0.0	-8.1517	3.2559	0.0	0.0	0.0
	71.2250	119.2750	1.0000	17.0000	-3.1438	0.0	-8.3612	3.2559	0.0	0.0	0.0
	72.1875	120.2375	1.0000								



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC) J15050A**

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drq. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
MP	08-Feb-2016	

[m]	[m]	[m]	[m]	[mm]	[mm]	Line	to Line
0.0	0.00000	-1.00000	17.00000	0.0	7.4932	0.0	0.0 d
1.0000	0.00000	0.00000	17.00000	0.0	8.1384	0.0	0.0 d
2.0000	0.00000	1.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
3.0000	0.00000	2.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
4.0000	0.00000	3.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
5.0000	0.00000	4.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
6.0000	0.00000	5.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
7.0000	0.00000	6.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
8.0000	0.00000	7.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
9.0000	0.00000	8.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
10.0000	0.00000	9.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
11.0000	0.00000	10.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
12.0000	0.00000	11.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
13.0000	0.00000	12.00000	17.00000	8.1384	0.0	0.0	-8.1384 d

d = Displacements include imported displacements.

Structure: Great Hall (East Terrace Frontage) | Sub-structure: Sub 3

Dist.	Coordinates			Displacements			
x	y	z	x	y	z	Horizontal displacement along the perpendicular Line	Horizontal displacement along the perpendicular Line to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	0.00000	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
0.99792	1.04792	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
1.9958	2.09584	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
2.9938	3.14376	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
3.9917	4.19158	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
4.9896	5.2394	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
5.9875	6.28722	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
6.9854	7.33504	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
7.9833	8.38286	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
8.9813	9.43068	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
9.9792	10.4785	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
10.9771	11.52632	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
11.9751	12.57414	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
12.973	13.62196	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
13.971	14.66978	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
14.969	15.7176	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
15.967	16.76542	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
16.965	17.81324	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
17.963	18.86106	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
18.961	19.90888	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
19.959	20.9567	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
20.957	22.00452	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
21.955	23.05234	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
22.953	24.10016	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
23.951	25.14798	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
24.949	26.1958	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
25.947	27.24362	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
26.945	28.29144	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
27.943	29.33926	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
28.941	30.38708	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
29.939	31.4349	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
30.937	32.48272	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
31.935	33.53054	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
32.933	34.57836	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
33.931	35.62618	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
34.929	36.674	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
35.927	37.72182	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
36.925	38.76964	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
37.923	39.81746	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
38.921	40.86528	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
39.919	41.9131	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
40.917	42.96092	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
41.915	44.00874	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
42.913	45.05656	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
43.911	46.10438	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
44.909	47.1522	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
45.907	48.19998	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
46.905	49.2478	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
47.903	50.29562	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
48.901	51.34344	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
49.899	52.39126	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d
50.897	53.43908	12.00000	17.00000	0.0	-9.9402	0.0	-9.9402 d

d = Displacements include imported displacements.

Structure: Library (East Terrace Frontage) | Sub-structure: Sub 4

Dist.	Coordinates			Displacements			
x	y	z	x	y	z	Horizontal displacement along the perpendicular Line	Horizontal displacement along the perpendicular Line to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	48.00000	12.00000	17.00000	0.0	-8.1384	0.0	0.0 d
1.0000	48.00000	11.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
2.0000	48.00000	10.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
3.0000	48.00000	9.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
4.0000	48.00000	8.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
5.0000	48.00000	7.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
6.0000	48.00000	6.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
7.0000	48.00000	5.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
8.0000	48.00000	4.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
9.0000	48.00000	3.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
10.0000	48.00000	2.00000	17.00000	9.9402	0.0	0.0	-9.9402 d
11.0000	48.00000	1.00000	17.00000	9.9402	0.0	0.0	-9.9402 d

d = Displacements include imported displacements.

Structure: Library (Eastern Elevation) | Sub-structure: Sub 5

Dist.	Coordinates			Displacements			
x	y	z	x	y	z	Horizontal displacement along the perpendicular Line	Horizontal displacement along the perpendicular Line to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	48.00000	1.00000	17.00000	-9.9021	0.0	0.0	-9.9021 d
0.96250	49.01250	1.00000	17.00000	-9.1859	0.0	0.0	-9.1859 d
1.92500	49.97500	1.00000	17.00000	-8.4698	0.0	0.0	-8.4698 d
2.88750	50.93750	1.00000	17.00000	-7.7537	0.0	0.0	-7.7537 d
3.85000	51.90000	1.00000	17.00000	-7.0376	0.0	0.0	-7.0376 d

d = Displacements include imported displacements.

Structure: Library (Eastern Elevation) | Sub-structure: Sub 6

Dist.	Coordinates			Displacements			
x	y	z	x	y	z	Horizontal displacement along the perpendicular Line	Horizontal displacement along the perpendicular Line to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	52.00000	1.00000	17.00000	-7.1466	0.0	0.0	-7.1466 d
1.0000	52.00000	0.00000	17.00000	-5.7408	0.0	0.0	-5.7408 d
2.0000	52.00000	-1.00000	17.00000	-4.2871	0.0	0.0	-4.2871 d
3.0000	52.00000	-2.00000	17.00000	-4.5391	2.2686	-2.2686	-4.5391 d
4.0000	52.00000	-3.00000	17.00000	-4.7887	2.7865	-2.7865	-4.7887 d
5.0000	52.00000	-4.00000	17.00000	-4.9974	2.9974	-2.9974	-4.9974 d
6.0000	52.00000	-5.00000	17.00000	-4.9933	3.1191	-3.1191	-4.9933 d

d = Displacements include imported displacements.

Structure: Library (Eastern Elevation) | Sub-structure: Sub 7

Dist.	Coordinates			Displacements			
x	y	z	x	y	z	Horizontal displacement along the perpendicular Line	Horizontal displacement along the perpendicular Line to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	48.00000	1.00000	17.00000	-9.9021	0.0	0.0	-9.9021 d
0.96250	49.01250	1.00000	17.00000	-9.1859	0.0	0.0	-9.1859 d
1.92500	49.97500	1.00000	17.00000	-8.4698	0.0	0.0	-8.4698 d
2.88750	50.93750	1.00000	17.00000	-7.7537	0.0	0.0	-7.7537 d
3.85000	51.90000	1.00000	17.00000	-7.0376	0.0	0.0	-7.0376 d

d = Displacements include imported displacements.



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC) J15050A**

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drq. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
MP	08-Feb-2016	

x	y	z	x	y	z	Horizontal displacement along the perpendicular Line	Horizontal displacement along the perpendicular Line to Line
[m]	[m]	[m]	[m]	[mm]	[mm]	[mm]	[mm]
0.0	52.00000	-5.00000	18.00000	-2.4953	3.1191	-2.4953	3.1191 d
1.0000	53.00000	-5.00000	18.00000	-2.5633	2.5633	-2.5633	2.5633 d
2.0000	54.00000	-5.00000	18.00000	-2.9377	2.1688	-2.9377	2.1688 d
3.0000	55.00000	-5.00000	18.00000	-2.5289	1.8064	-2.5289	1.8064 d
4.0000	56.00000	-5.00000	18.00000	-2.3862	1.4848	-2.3862	1.4848 d
5.0000	57.00000	-5.00000	18.00000	-2.1914	1.2174	-2.1914	1.2174 d
6.0000	58.00000	-5.00000	18.00000	-1.9600	0.9900	-1.9600	0.9900 d
7.0000	59.00000	-5					



**GEA LIMITED**  
**(GEOTECHNICAL & ENV ASSOC)**

<b>Job No.</b>	<b>Sheet No.</b>	<b>Rev.</b>
<b>Drp. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
<b>MP</b>	<b>08-Feb-2016</b>	

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
3.0000	49.00000	38.00000	17.00000	0.0	0.0	0.0
4.0000	48.00000	38.00000	17.00000	0.0	0.0	0.0
5.0000	47.00000	38.00000	17.00000	0.0	0.0	0.0
6.0000	46.00000	38.00000	17.00000	0.0	0.0	0.0
7.0000	45.00000	38.00000	17.00000	0.0	0.0	0.0
8.0000	44.00000	38.00000	17.00000	0.0	0.0	0.0
9.0000	43.00000	38.00000	17.00000	0.0	0.0	0.0
10.0000	42.00000	38.00000	17.00000	0.0	0.0	0.0
11.0000	41.00000	38.00000	17.00000	0.0	0.0	0.0
12.0000	40.00000	38.00000	17.00000	0.0	0.0	0.0
13.0000	39.00000	38.00000	17.00000	0.0	0.0	0.0
14.0000	38.00000	38.00000	17.00000	0.0	0.0	0.0
15.0000	37.00000	38.00000	17.00000	0.0	0.0	0.0
16.0000	36.00000	38.00000	17.00000	0.0	0.0	0.0
17.0000	35.00000	38.00000	17.00000	0.0	0.0	0.0
18.0000	34.00000	38.00000	17.00000	0.0	0.0	0.0
19.0000	33.00000	38.00000	17.00000	0.0	0.0	0.0
20.0000	32.00000	38.00000	17.00000	0.0	0.0	0.0
21.0000	31.00000	38.00000	17.00000	0.0	0.0	0.0
22.0000	30.00000	38.00000	17.00000	0.0	0.0	0.0
23.0000	29.00000	38.00000	17.00000	0.0	0.0	0.0
24.0000	28.00000	38.00000	17.00000	0.0	0.0	0.0
25.0000	27.00000	38.00000	17.00000	0.0	0.0	0.0
26.0000	26.00000	38.00000	17.00000	0.0	0.0	0.0
27.0000	25.00000	38.00000	17.00000	0.0	0.0	0.0
28.0000	24.00000	38.00000	17.00000	0.0	0.0	0.0
29.0000	23.00000	38.00000	17.00000	0.0	0.0	0.0
30.0000	22.00000	38.00000	17.00000	0.0	0.0	0.0
31.0000	21.00000	38.00000	17.00000	0.0	0.0	0.0
32.0000	20.00000	38.00000	17.00000	0.0	0.0	0.0
33.0000	19.00000	38.00000	17.00000	0.0	0.0	0.0
34.0000	18.00000	38.00000	17.00000	0.0	0.0	0.0
35.0000	17.00000	38.00000	17.00000	0.0	0.0	0.0
36.0000	16.00000	38.00000	17.00000	0.0	0.0	0.0
37.0000	15.00000	38.00000	17.00000	0.0	0.0	0.0
38.0000	14.00000	38.00000	17.00000	0.0	0.0	0.0
39.0000	13.00000	38.00000	17.00000	0.0	0.0	0.0
40.0000	12.00000	38.00000	17.00000	0.0	0.0	0.0
41.0000	11.00000	38.00000	17.00000	0.0	0.0	0.0
42.0000	10.00000	38.00000	17.00000	0.0	0.0	0.0
43.0000	9.00000	38.00000	17.00000	0.0	0.0	0.0
44.0000	8.00000	38.00000	17.00000	0.0	0.0	0.0
45.0000	7.00000	38.00000	17.00000	0.0	0.0	0.0
46.0000	6.00000	38.00000	17.00000	0.0	0.0	0.0

Structure: Great Hall (Western Elevation) | Sub-structure: Sub 12

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	6.00000	38.00000	17.00000	0.0	0.0	0.0
1.0000	6.00000	39.00000	17.00000	0.0	0.0	0.0
2.0000	6.00000	40.00000	17.00000	0.0	0.0	0.0

Structure: Great Hall (Western Elevation) | Sub-structure: Sub 13

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	6.00000	40.00000	17.00000	0.0	0.0	0.0
1.0000	5.00000	40.00000	17.00000	0.0	0.0	0.0
2.0000	4.00000	40.00000	17.00000	0.0	0.0	0.0
3.0000	3.00000	40.00000	17.00000	0.0	0.0	0.0
4.0000	2.00000	40.00000	17.00000	0.0	0.0	0.0
5.0000	1.00000	40.00000	17.00000	0.0	0.0	0.0
6.0000	0.00000	40.00000	17.00000	0.0	0.0	0.0
7.0000	-1.00000	40.00000	17.00000	0.0	0.0	0.0
8.0000	-2.00000	40.00000	17.00000	0.0	0.0	0.0
9.0000	-3.00000	40.00000	17.00000	0.0	0.0	0.0
10.0000	-4.00000	40.00000	17.00000	0.0	0.0	0.0
11.0000	-5.00000	40.00000	17.00000	0.0	0.0	0.0
12.0000	-6.00000	40.00000	17.00000	0.0	0.0	0.0
13.0000	-7.00000	40.00000	17.00000	0.0	0.0	0.0
14.0000	-8.00000	40.00000	17.00000	0.0	0.0	0.0

Structure: Great Hall (Southern Elevation) | Sub-structure: Sub 14

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	-8.00000	40.00000	17.00000	0.0	0.0	0.0
1.0000	-8.00000	39.00000	17.00000	0.0	0.0	0.0
2.0000	-8.00000	38.00000	17.00000	0.0	0.0	0.0
3.0000	-8.00000	37.00000	17.00000	0.0	0.0	0.0
4.0000	-8.00000	36.00000	17.00000	0.0	0.0	0.0
5.0000	-8.00000	35.00000	17.00000	0.0	0.0	0.0
6.0000	-8.00000	34.00000	17.00000	0.0	0.0	0.0
7.0000	-8.00000	33.00000	17.00000	0.0	0.0	0.0
8.0000	-8.00000	32.00000	17.00000	0.0	0.0	0.0
9.0000	-8.00000	31.00000	17.00000	0.0	0.0	0.0
10.0000	-8.00000	30.00000	17.00000	0.0	0.0	0.0
11.0000	-8.00000	29.00000	17.00000	0.0	0.0	0.0
12.0000	-8.00000	28.00000	17.00000	0.02803	-0.04766	0.02363
13.0000	-8.00000	27.00000	17.00000	0.09838	-0.17914	0.03959
14.0000	-8.00000	26.00000	17.00000	0.20638	-0.36116	0.02638
15.0000	-8.00000	25.00000	17.00000	0.34994	-0.50100	0.01899
16.0000	-8.00000	24.00000	17.00000	0.52473	-0.62029	0.01733
17.0000	-8.00000	23.00000	17.00000	0.72939	-0.71374	0.01593
18.0000	-8.00000	22.00000	17.00000	0.94833	-0.7857	0.01533
19.0000	-8.00000	21.00000	17.00000	1.17319	-0.8398	0.01538
20.0000	-8.00000	20.00000	17.00000	1.4124	-0.8724	0.01542
21.0000	-8.00000	19.00000	17.00000	1.6548	-0.8862	0.01542
22.0000	-8.00000	18.00000	17.00000	1.9019	-0.8912	0.01542
23.0000	-8.00000	17.00000	17.00000	2.1544	-0.8874	0.01542
24.0000	-8.00000	16.00000	17.00000	2.4127	-0.8759	0.01542
25.0000	-8.00000	15.00000	17.00000	2.6764	-0.8570	0.01542
26.0000	-8.00000	14.00000	17.00000	2.9450	-0.8317	0.01542
27.0000	-8.00000	13.00000	17.00000	3.2187	-0.7997	0.01542
28.0000	-8.00000	12.00000	17.00000	3.4978	-0.7613	0.01542
29.0000	-8.00000	11.00000	17.00000	3.7727	-0.7177	0.01542
30.0000	-8.00000	10.00000	17.00000	4.0438	-0.6701	0.01542
31.0000	-8.00000	9.00000	17.00000	4.3114	-0.6197	0.01542
32.0000	-8.00000	8.00000	17.00000	4.5759	-0.5677	0.01542
33.0000	-8.00000	7.00000	17.00000	4.8377	-0.5144	0.01542
34.0000	-8.00000	6.00000	17.00000	5.0971	-0.4601	0.01542
35.0000	-8.00000	5.00000	17.00000	5.3544	-0.4051	0.01542
36.0000	-8.00000	4.00000	17.00000	5.6099	-0.3506	0.01542
37.0000	-8.00000	3.00000	17.00000	5.8737	-0.2969	0.01542
38.0000	-8.00000	2.00000	17.00000	6.1452	-0.2452	0.01542
39.0000	-8.00000	1.00000	17.00000	6.4247	-0.1967	0.01542
40.0000	-8.00000	0.00000	17.00000	6.7124	-0.1526	0.01542
41.0000	-8.00000	-1.00000	17.00000	7.0087	-0.1141	0.01542
42.0000	-8.00000	-2.00000	17.00000	7.3239	-0.0814	0.01542
43.0000	-8.00000	-3.00000	17.00000	7.6584	-0.0548	0.01542



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The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Dist.	Coordinates			Displacements		
	x	y	z	x	y	z
0.0	60.00000	41.00000	18.00000	0.12119	-0.01219	0.13581
1.0000	61.00000	41.00000	18.00000	0.13581	-0.01545	0.13581
2.0000	62.00000	41.00000	18.00000	0.20661	-0.02826	0.20661
3.0000	63.00000	41.00000	18.00000	0.26500	-0.03828	0.26500
4.0000	64.00000	41.00000	18.00000	0.33209	-0.05848	0.33209
5.0000	65.00000	41.00000	18.00000	0.40797	-0.08435	0.40797
6.0000	66.00000	41.00000	18.00000	0.46475	-0.16119	0.46475
7.0000	67.00000	41.00000	18.00000	0.51743	-0.20081	0.51743
8.0000	68.00000	41.00000	18.00000	0.57097	-0.28547	0.57097
9.0000	69.00000	41.00000	18.00000	1.9929	-1.9929	1.9929
10.0000	70.00000	41.00000	18.00000	0.0	0.0	-8.5161
11.0000	71.00000	41.00000	18.00000			





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<b>Made by</b>	<b>Date</b>	<b>Checked</b>
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The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
44.906 44.95620	12.00000	17.00000	6.1741 d		
44.904 44.95411	12.00000	17.00000	6.1741 d		
44.902 44.95202	12.00000	17.00000	6.1741 d		
47.900 47.95000	12.00000	17.00000	6.1741 d		

d = Displacements include imported displacements.

Structure: Library (East Terrace Frontage) | Sub-structure: Sub 4

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	48.00000	12.00000	17.00000	5.5886 d	
1.0000	48.00000	12.00000	17.00000	5.5886 d	
2.0000	48.00000	10.00000	17.00000	6.1741 d	
3.0000	48.00000	9.00000	17.00000	6.1741 d	
4.0000	48.00000	8.00000	17.00000	6.1741 d	
5.0000	48.00000	7.00000	17.00000	6.1741 d	
6.0000	48.00000	6.00000	17.00000	6.1741 d	
7.0000	48.00000	5.00000	17.00000	6.1741 d	
8.0000	48.00000	4.00000	17.00000	6.1741 d	
9.0000	48.00000	3.00000	17.00000	6.1741 d	
10.0000	48.00000	2.00000	17.00000	6.1741 d	
11.0000	48.00000	1.00000	17.00000	6.1741 d	

d = Displacements include imported displacements.

Structure: Library (Eastern Elevation) | Sub-structure: Sub 5

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	48.00000	1.00000	17.00000	6.2163 d	
0.86230	49.02120	1.00000	17.00000	6.2262 d	
1.8230	49.97500	1.00000	17.00000	7.1086 d	
2.8875	50.93750	1.00000	17.00000	7.1112 d	
3.8500	51.90000	1.00000	17.00000	8.9078 d	

d = Displacements include imported displacements.

Structure: Library (Eastern Elevation) | Sub-structure: Sub 6

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	52.00000	1.00000	17.00000	4.8765 d	
1.0000	52.00000	0.00000	17.00000	5.7952 d	
2.0000	52.00000	-1.00000	17.00000	5.5889 d	
3.0000	52.00000	-2.00000	17.00000	5.3274 d	
4.0000	52.00000	-3.00000	17.00000	5.0263 d	
5.0000	52.00000	-4.00000	17.00000	4.7128 d	
6.0000	52.00000	-5.00000	17.00000	4.4955 d	

d = Displacements include imported displacements.

Structure: Library (Eastern Elevation) | Sub-structure: Sub 7

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	52.00000	-5.00000	18.00000	4.4855 d	
1.0000	53.00000	-5.00000	18.00000	4.1694 d	
2.0000	54.00000	-5.00000	18.00000	3.8228 d	
3.0000	55.00000	-5.00000	18.00000	3.4538 d	
4.0000	56.00000	-5.00000	18.00000	3.0564 d	
5.0000	57.00000	-5.00000	18.00000	2.6608 d	
6.0000	58.00000	-5.00000	18.00000	2.2348 d	
7.0000	59.00000	-5.00000	18.00000	2.1238 d	
8.0000	60.00000	-5.00000	18.00000	2.0346 d	
9.0000	61.00000	-5.00000	18.00000	1.9703 d	
10.0000	62.00000	-5.00000	18.00000	1.9294 d	
11.0000	63.00000	-5.00000	18.00000	1.9074 d	
12.0000	64.00000	-5.00000	18.00000	1.9048 d	
13.0000	65.00000	-5.00000	18.00000	0.8765 d	
14.0000	66.00000	-5.00000	18.00000	0.8436 d	
15.0000	67.00000	-5.00000	18.00000	0.7682 d	
16.0000	68.00000	-5.00000	18.00000	0.7268 d	
17.0000	69.00000	-5.00000	18.00000	0.6829 d	
18.0000	70.00000	-5.00000	18.00000	0.6 d	

d = Displacements include imported displacements.

Structure: Library (Northern Elevation) | Sub-structure: Sub 8

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	70.00000	3.00000	18.00000	0.0 d	
1.0000	70.00000	4.00000	18.00000	0.0 d	
2.0000	70.00000	3.00000	18.00000	0.0 d	
3.0000	70.00000	2.00000	18.00000	0.0 d	
4.0000	70.00000	1.00000	18.00000	0.0 d	
5.0000	70.00000	0.00000	18.00000	0.0304 d	
6.0000	70.00000	1.00000	18.00000	0.2800 d	
7.0000	70.00000	2.00000	18.00000	0.4832 d	
8.0000	70.00000	3.00000	18.00000	0.7046 d	
9.0000	70.00000	4.00000	18.00000	1.0038 d	
10.0000	70.00000	5.00000	18.00000	1.3545 d	
11.0000	70.00000	6.00000	18.00000	1.6661 d	
12.0000	70.00000	7.00000	18.00000	2.0390 d	
13.0000	70.00000	8.00000	18.00000	2.4881 d	
14.0000	70.00000	9.00000	18.00000	2.9456 d	
15.0000	70.00000	10.00000	18.00000	3.4180 d	
16.0000	70.00000	11.00000	18.00000	3.8886 d	
17.0000	70.00000	12.00000	18.00000	4.3864 d	
18.0000	70.00000	13.00000	18.00000	4.7348 d	
19.0000	70.00000	14.00000	18.00000	5.0557 d	
20.0000	70.00000	15.00000	18.00000	5.2644 d	
21.0000	70.00000	16.00000	18.00000	5.3221 d	
22.0000	70.00000	17.00000	18.00000	5.1896 d	
23.0000	70.00000	18.00000	18.00000	4.8774 d	
24.0000	70.00000	19.00000	18.00000	0.0 d	
25.0000	70.00000	20.00000	18.00000	0.0 d	
26.0000	70.00000	21.00000	18.00000	0.0 d	
27.0000	70.00000	22.00000	18.00000	0.0 d	
28.0000	70.00000	23.00000	18.00000	0.0 d	
29.0000	70.00000	24.00000	18.00000	0.0 d	
30.0000	70.00000	25.00000	18.00000	0.0 d	
31.0000	70.00000	26.00000	18.00000	0.0 d	
32.0000	70.00000	27.00000	18.00000	0.0 d	
33.0000	70.00000	28.00000	18.00000	0.0 d	
34.0000	70.00000	29.00000	18.00000	0.0 d	
35.0000	70.00000	30.00000	18.00000	0.0 d	
36.0000	70.00000	31.00000	18.00000	0.0 d	
37.0000	70.00000	32.00000	18.00000	0.0 d	
38.0000	70.00000	33.00000	18.00000	0.0 d	
39.0000	70.00000	34.00000	18.00000	0.0 d	
40.0000	70.00000	35.00000	18.00000	0.0 d	
41.0000	70.00000	36.00000	18.00000	0.0 d	
42.0000	70.00000	37.00000	18.00000	0.0 d	



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Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
43.0000	70.00000	18.00000	18.00000	0.0 d	
44.0000	70.00000	19.00000	18.00000	0.0 d	
45.0000	70.00000	20.00000	18.00000	0.0 d	

d = Displacements include imported displacements.

Structure: Library (Western Elevation) | Sub-structure: Sub 9

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	70.00000	40.00000	18.00000	0.0 d	
1.0000	69.00000	40.00000	18.00000	0.0 d	
2.0000	68.00000	40.00000	18.00000	0.0 d	
3.0000	67.00000	40.00000	18.00000	0.0 d	
4.0000	66.00000	40.00000	18.00000	0.0 d	
5.0000	65.00000	40.00000	18.00000	0.0 d	
6.0000	64.00000	40.00000	18.00000	0.0 d	
7.0000	63.00000	40.00000	18.00000	0.0 d	
8.0000	62.00000	40.00000	18.00000	0.0 d	
9.0000	61.00000	40.00000	18.00000	0.0 d	
10.0000	60.00000	40.00000	18.00000	0.0 d	
11.0000	59.00000	40.00000	18.00000	0.0 d	
12.0000	58.00000	40.00000	18.00000	0.0 d	
13.0000	57.00000	40.00000	18.00000	0.0 d	
14.0000	56.00000	40.00000	18.00000	0.0 d	
15.0000	55.00000	40.00000	18.00000	0.0 d	
16.0000	54.00000	40.00000	18.00000	0.0 d	
17.0000	53.00000	40.00000	18.00000	0.0 d	
18.0000	52.00000	40.00000	18.00000	0.0 d	

d = Displacements include imported displacements.

Structure: Library / Great Hall (Western Elevation) | Sub-structure: Sub 10

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	52.00000	40.00000	17.00000	0.0 d	
1.0000	52.00000	39.00000	17.00000	0.0 d	
2.0000	52.00000	38.00000	17.00000	0.0 d	

d = Displacements include imported displacements.

Structure: Great Hall (Western Elevation) | Sub-structure: Sub 11

Dist.	Coordinates				Displacements
	X [m]	Y [m]	Z [m]	Z [mm]	
<b>Vertical Offset 1</b>					
0.0	52.00000	18.00000	17.00000	0.0 d	
1.0000	51.00000	18.00000	17.00000	0.0 d	
2.0000	50.00000	18.00000	17.00000	0.0 d	
3.0000	49.00000	18.00000	17.00000	0.0 d	
4.0000	48.00000	18.00000	17.00000	0.0 d	
5.0000	47.00000	18.00000	17.00000	0.0 d	
6.0000	46.00000	18.00000	17.00000	0.0 d	
7.0000	45.00000	18.00000	17.00000	0.0 d	
8.0000	44.00000	18.00000	17.00000	0.0 d	
9.0000	43.00000	18.00000	17.00000	0.0 d	
10.0000	42.00000	18.00000	17.00000	0.0 d	
11.0000	41.00000	18.00000	17.00000	0.0 d	
12.0000	40.00000	18.00000	17.00000	0.0 d	
13.0000	39.00000	18.00000	17.00000	0.0 d	
14.0000	38.00				



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Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Dist.	Coordinates			Displacements		
[m]	X [m]	Y [m]	Z [m]	X [mm]	Y [mm]	Z [mm]
d - Displacements include imported displacements.						
Structure: Great Hall (Southern Elevation)   Sub-structure: Sub 14						
Dist.	Coordinates			Displacements		
[m]	X [m]	Y [m]	Z [m]	X [mm]	Y [mm]	Z [mm]
<b>Vertical Offset 1</b>						
0.0	-8.00000	40.00000	17.00000	0.0	0	0
1.0000	-8.00000	39.00000	17.00000	0.0	0	0
2.0000	-8.00000	38.00000	17.00000	0.0	0	0
3.0000	-8.00000	37.00000	17.00000	0.0	0	0
4.0000	-8.00000	36.00000	17.00000	0.0	0	0
5.0000	-8.00000	35.00000	17.00000	0.0	0	0
6.0000	-8.00000	34.00000	17.00000	0.0	0	0
7.0000	-8.00000	33.00000	17.00000	0.0	0	0
8.0000	-8.00000	32.00000	17.00000	0.091868	0	0
9.0000	-8.00000	31.00000	17.00000	0.27689	0	0
10.000	-8.00000	30.00000	17.00000	0.46246	0	0
11.000	-8.00000	29.00000	17.00000	0.64234	0	0
12.000	-8.00000	28.00000	17.00000	0.81703	0	0
13.000	-8.00000	27.00000	17.00000	1.0391	0	0
14.000	-8.00000	26.00000	17.00000	1.2322	0	0
15.000	-8.00000	25.00000	17.00000	1.4270	0	0
16.000	-8.00000	24.00000	17.00000	1.6237	0	0
17.000	-8.00000	23.00000	17.00000	1.8433	0	0
18.000	-8.00000	22.00000	17.00000	2.0879	0	0
19.000	-8.00000	21.00000	17.00000	2.2899	0	0
20.000	-8.00000	20.00000	17.00000	2.5133	0	0
21.000	-8.00000	19.00000	17.00000	2.7861	0	0
22.000	-8.00000	18.00000	17.00000	3.0419	0	0
23.000	-8.00000	17.00000	17.00000	3.2934	0	0
24.000	-8.00000	16.00000	17.00000	3.5267	0	0
25.000	-8.00000	15.00000	17.00000	3.7383	0	0
26.000	-8.00000	14.00000	17.00000	3.9138	0	0
27.000	-8.00000	13.00000	17.00000	4.0503	0	0
28.000	-8.00000	12.00000	17.00000	4.1327	0	0
29.000	-8.00000	11.00000	17.00000	4.1793	0	0
30.000	-8.00000	10.00000	17.00000	4.7891	0	0
31.000	-8.00000	9.00000	17.00000	4.7891	0	0
32.000	-8.00000	8.00000	17.00000	4.7891	0	0
33.000	-8.00000	7.00000	17.00000	4.7891	0	0
34.000	-8.00000	6.00000	17.00000	4.7891	0	0
35.000	-8.00000	5.00000	17.00000	4.7891	0	0
36.000	-8.00000	4.00000	17.00000	4.7891	0	0
37.000	-8.00000	3.00000	17.00000	4.7891	0	0
38.000	-8.00000	2.00000	17.00000	4.7891	0	0
39.000	-8.00000	1.00000	17.00000	4.7891	0	0
40.000	-8.00000	0.00000	17.00000	4.1327	0	0
41.000	-8.00000	-1.00000	17.00000	4.0503	0	0
d - Displacements include imported displacements.						

Dist.	Coordinates			Displacements		
[m]	X [m]	Y [m]	Z [m]	X [mm]	Y [mm]	Z [mm]
Structure: Boundary Wall (adjacent to single level basement)   Sub-structure: Sub 15						
Dist.	Coordinates			Displacements		
[m]	X [m]	Y [m]	Z [m]	X [mm]	Y [mm]	Z [mm]
<b>Vertical Offset 1</b>						
0.0	60.00000	41.00000	18.00000	0.14238	0	0
1.0000	61.00000	41.00000	18.00000	0.18847	0	0
2.0000	62.00000	41.00000	18.00000	0.24011	0	0
3.0000	63.00000	41.00000	18.00000	0.31002	0	0
4.0000	64.00000	41.00000	18.00000	0.40000	0	0
5.0000	65.00000	41.00000	18.00000	0.52289	0	0
6.0000	66.00000	41.00000	18.00000	0.69426	0	0
7.0000	67.00000	41.00000	18.00000	0.95517	0	0
8.0000	68.00000	41.00000	18.00000	1.4091	0	0
9.0000	69.00000	41.00000	18.00000	2.2877	0	0
10.000	70.00000	41.00000	18.00000	3.1896	0	0
11.000	71.00000	41.00000	18.00000	4.0710	0	0
12.000	72.00000	41.00000	18.00000	4.9710	0	0
13.000	73.00000	41.00000	18.00000	6.0710	0	0
14.000	74.00000	41.00000	18.00000	6.0710	0	0
15.000	75.00000	41.00000	18.00000	6.0710	0	0
16.000	76.00000	41.00000	18.00000	6.0710	0	0
17.000	77.00000	41.00000	18.00000	6.0710	0	0
18.000	78.00000	41.00000	18.00000	6.0710	0	0
19.000	79.00000	41.00000	18.00000	6.0710	0	0
20.000	80.00000	41.00000	18.00000	6.0710	0	0
21.000	81.00000	41.00000	18.00000	6.0710	0	0
22.000	82.00000	41.00000	18.00000	6.1896	0	0
23.000	83.00000	41.00000	18.00000	6.2423	0	0
24.000	84.00000	41.00000	18.00000	6.4038	0	0
25.000	85.00000	41.00000	18.00000	6.8853	0	0
26.000	86.00000	41.00000	18.00000	7.172	0	0
27.000	87.00000	41.00000	18.00000	7.4884	0	0
28.000	88.00000	41.00000	18.00000	8.0817	0	0
29.000	89.00000	41.00000	18.00000	1.6794	0	0
30.000	90.00000	41.00000	18.00000	3.2839	0	0
d - Displacements include imported displacements.						

<b>Specific Building Damage Results - All Segments</b>											
Structure: East Terrace   Sub-structure: Sub 1											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	1	0.0	5.9222	Sagging	0.0064878	0.033051	0.042512	-426.698-6	-448.048-6	6060.7	(Negligible) 0
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: East Terrace   Sub-structure: Sub 2											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain <td>Max. Tensile Strain <td>Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td></td></td></td>	Average Horizontal Strain <td>Max. Tensile Strain <td>Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td></td></td>	Max. Tensile Strain <td>Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td></td>	Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td>	Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td>	Min. Radius of Curvature <td>Damage Category</td>	Damage Category
0.0	1	0.0	1.9128	Hogging	0.023906	-0.35459	0.072219	0.0082051	-590.248-6	738.90	1 (Very Slight)
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Great Hall (East Terrace Frontage)   Sub-structure: Sub 3											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain <td>Max. Tensile Strain <td>Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td></td></td></td>	Average Horizontal Strain <td>Max. Tensile Strain <td>Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td></td></td>	Max. Tensile Strain <td>Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td></td>	Maximum Horizontal Displacement <td>Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td></td>	Maximum Vertical Displacement <td>Min. Radius of Curvature <td>Damage Category</td> </td>	Min. Radius of Curvature <td>Damage Category</td>	Damage Category
0.0	1	0.0	3.0000	Sagging	0.013010	0.0	0.0	0.0	585.448-6	1366.5	(Negligible) 0
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											



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<b>J15050A</b>		
<b>Drp. Ref.</b>		
<b>Made by</b>	<b>Date</b>	<b>Checked</b>
<b>MP</b>	<b>08-Feb-2016</b>	

The Great Hall, Lincoln's Inn, Newman's Row, London, WC2A 3TL  
Wall Movements Rev 3 Piling and Excavation  
Damage Assessment

Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
0.0	1	0.0	47.850	None	0.0	0.0	0.0	0.0	0.0	0.0	(Negligible) 0
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library (East Terrace Frontage)   Sub-structure: Sub 4											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	1	0.0	3.0000	Sagging	0.013045	-0.27128	0.054774	0.0082051	-590.248-6	1351.0	1 (Very Slight)
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library (Eastern Elevation)   Sub-structure: Sub 5											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	1	0.0	3.8500	Sagging	0.014079	0.06905	0.073220	-743.598-6	-636.288-6	2638.4	1 (Very Slight)
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library (Eastern Elevation)   Sub-structure: Sub 6											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	1	0.0	2.8306	Hogging	0.019434	-0.074509	0.018937	0.0013237	0.0010812	905.85	(Negligible) 0
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library (Eastern Elevation)   Sub-structure: Sub 7											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	1	0.0	1.8181	Hogging	0.016863	-0.005285	0.0014777	67.0818-6	326.138-6	10410.	(Negligible) 0
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library (Northern Elevation)   Sub-structure: Sub 8											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	1	6.0000	8.273	Hogging	0.0038317	0.031656	0.032689	-416.168-6	-472.228-6	18665.	(Negligible) 0
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library (Western Elevation)   Sub-structure: Sub 9											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	All settlements are less than the Settlement Trough Limit Sensitivity.										
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											
Structure: Library / Great Hall (Western Elevation)   Sub-structure: Sub 10											
Vertical Offset from Line for Vertical Movement	Segment	Start	Length	Curvature	Deflection Ratio <td>Average Horizontal Strain</td> <td>Max. Tensile Strain</td> <td>Maximum Horizontal Displacement</td> <td>Maximum Vertical Displacement</td> <td>Min. Radius of Curvature</td> <td>Damage Category</td>	Average Horizontal Strain	Max. Tensile Strain	Maximum Horizontal Displacement	Maximum Vertical Displacement	Min. Radius of Curvature	Damage Category
0.0	All settlements are less than the Settlement Trough Limit Sensitivity.										
Calculations	[m]	[m]	[m]	[m]	[%]	[%]	[%]	[mm]	[mm]	[mm]	[mm]
Tensile horizontal strains are +ve, compressive horizontal strains are -ve.											





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(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmar's Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

Main data table with columns: Structure Name, Parameter, Sub-Structure, Critical Segment, Start, End, Curvature, Maximum Slope, Maximum Settlement, Max. Tensile Strain, Min. Radius of Curvature (Hogging), Min. Radius of Curvature (Sagging), Damage Category

Specific Building Damage Results - All Combined Segments

Summary table for building damage results, including Structure: East Terrace, Great Hall, and Library (Eastern Elevation) with sub-structure details and damage categories.



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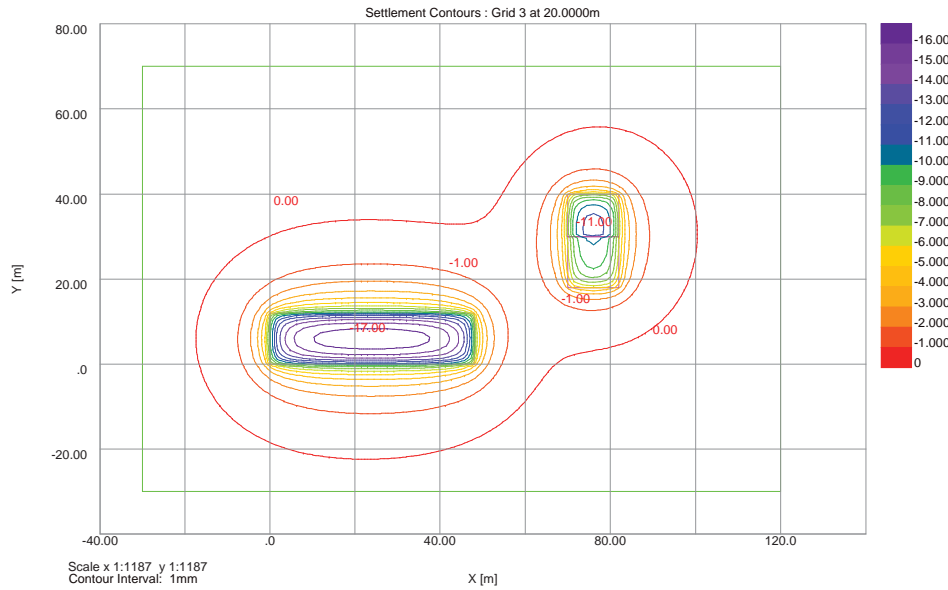
(GEOTECHNICAL & ENV ASSOC) J15050A

The Great Hall, Lincoln's Inn, Newmar's Row, London, WC2A 3TL
Wall Movements Rev 3 Piling and Excavation
Damage Assessment

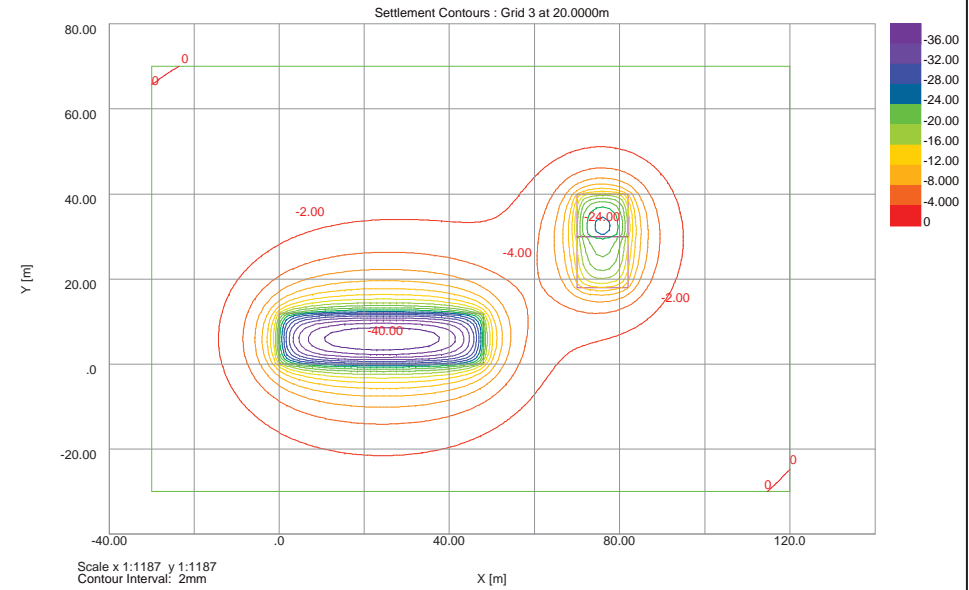
Table with Job No., Sheet No., Rev., Drg. Ref., Made by MP, Date 08-Feb-2016, Checked

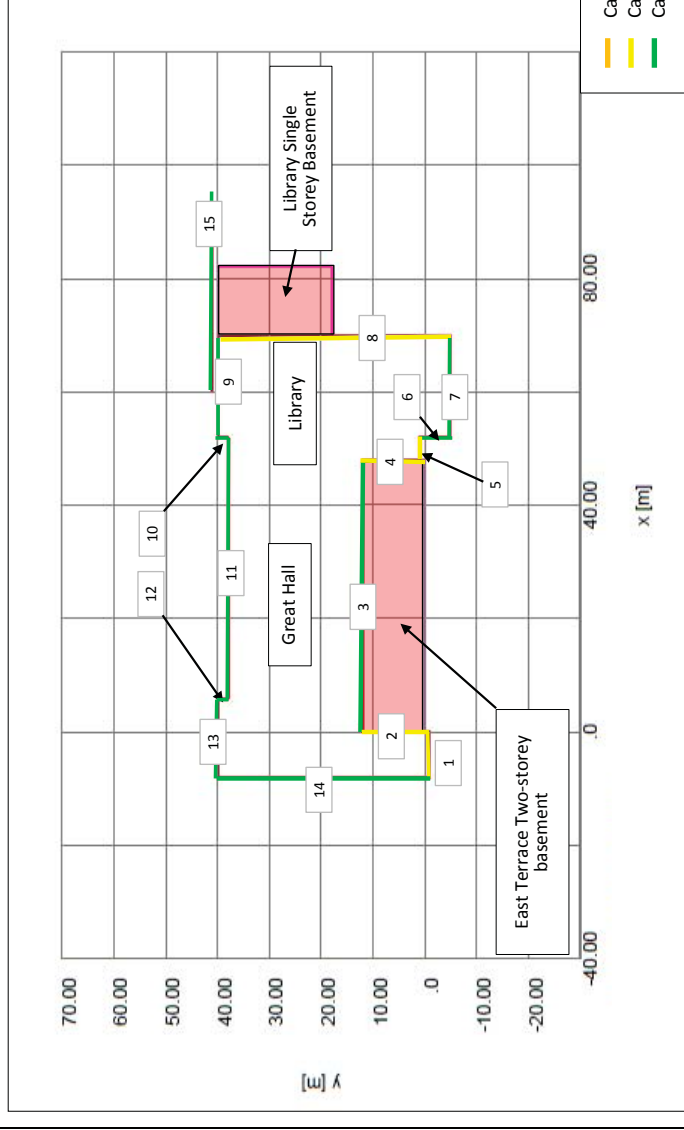
Main data table for page 88, identical in structure to page 87, covering various building segments and damage assessments.

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where information can be found on all of the services that we offer.