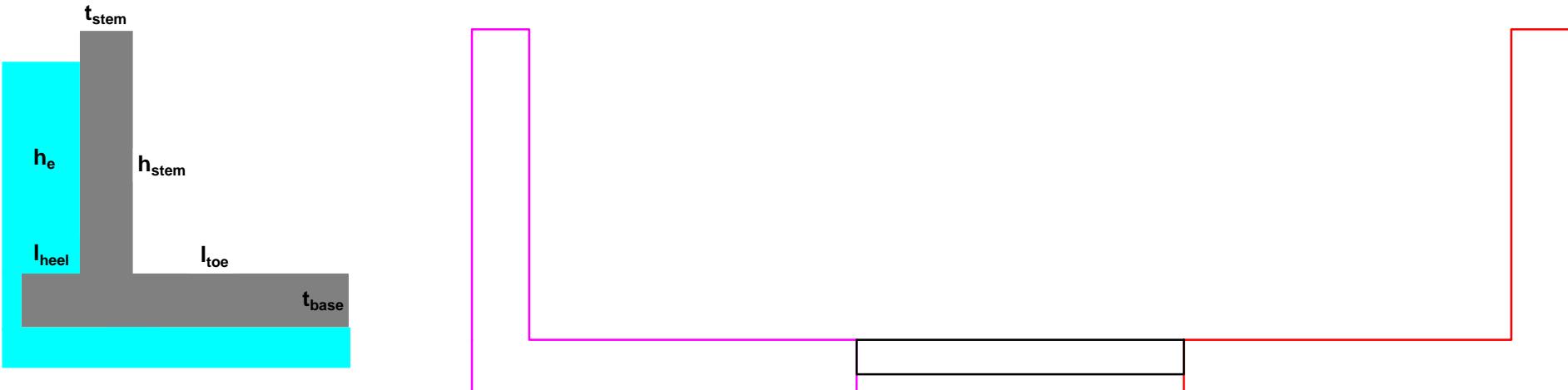


# Design of RC Basement walls for Party Wall to No. 83 and Gable wall

Page:	1
Job Ref:	MDM406



## Left hand side basement wall

### Party wall with No. 83

Position of stem :	
Total height of wall including thickness of base (h) :	3.15 m
Thickness of wall ( $t_{stem}$ ) :	0.35 m
Height of soil including thickness of base ( $h_e$ ) :	2.88 m
Angle of backfill or slope ( $\beta$ ) :	0 Degree
Internal angle of friction for retained soil ( $\phi$ ) :	20 Degree
Dead surcharge in SLS ( $W_{d_s}$ ) :	0.0 kN/m <sup>2</sup>
Live surcharge in SLS ( $W_{l_s}$ ) :	0.0 kN/m <sup>2</sup>
Height of surcharge loads from underneath of base ( $h_s$ ) :	0.00 m
Vertical dead load on stem under temporary work in SLS ( $W_{d2}$ ) :	33.6 kN/m
Vertical live load on stem under temporary work in SLS ( $W_{l2}$ ) :	5.2 kN/m
Vertical dead load on stem after construction in SLS ( $W_{d3}$ ) :	34.5 kN/m
Vertical live load on stem after construction in SLS ( $W_{l3}$ ) :	10.3 kN/m
Additional horizontal dead load to stem in SLS ( $W_{d_h}$ ) :	0.00 kN/m
Additional horizontal live load to stem in SLS ( $W_{l_h}$ ) :	0.00 kN/m
Height of horizontal load from underneath of base ( $h_h$ ) :	0.00 m
Height of ground water from underneath of base ( $h_w$ ) :	2.00 m
Depth of base ( $t_{base}$ ) :	0.45 m
Length of toe ( $l_{toe}$ ) :	1.00 m
Length of heel ( $l_{heel}$ ) :	0.00 m
Dead load by wall, screed or others on toe in SLS ( $W_{d\_toe}$ ) :	0.00 kN/m <sup>2</sup>
Live load on toe in SLS ( $W_{l\_toe}$ ) :	0.00 kN/m <sup>2</sup>

## Right hand side basement wall

### Gable wall

Position of stem :	
Total height of wall including thickness of base (h) :	3.15 m
Thickness of wall ( $t_{stem}$ ) :	0.40 m
Height of soil including thickness of base ( $h_e$ ) :	3.15 m
Angle of backfill or slope ( $\beta$ ) :	0 Degree
Internal angle of friction for retained soil ( $\phi$ ) :	20 Degree
Dead surcharge in SLS ( $W_{d_s}$ ) :	2.2 kN/m <sup>2</sup>
Live surcharge in SLS ( $W_{l_s}$ ) :	1.5 kN/m <sup>2</sup>
Height of surcharge loads from underneath of base ( $h_s$ ) :	1.90 m
Vertical dead load on stem under temporary work in SLS ( $W_{d2}$ ) :	76.2 kN/m
Vertical live load on stem under temporary work in SLS ( $W_{l2}$ ) :	2.0 kN/m
Vertical dead load on stem after construction in SLS ( $W_{d3}$ ) :	77.1 kN/m
Vertical live load on stem after construction in SLS ( $W_{l3}$ ) :	10.8 kN/m
Additional horizontal dead load to stem in SLS ( $W_{d_h}$ ) :	15.60 kN/m
Additional horizontal live load to stem in SLS ( $W_{l_h}$ ) :	2.20 kN/m
Height of horizontal load from underneath of base ( $h_h$ ) :	0.43 m
Height of ground water from underneath of base ( $h_w$ ) :	2.00 m
Depth of base ( $t_{base}$ ) :	0.45 m
Length of toe ( $l_{toe}$ ) :	1.00 m
Length of heel ( $l_{heel}$ ) :	0.00 m
Dead load by wall, screed or others on toe in SLS ( $W_{d\_toe}$ ) :	0.00 kN/m <sup>2</sup>
Live load on toe in SLS ( $W_{l\_toe}$ ) :	0.00 kN/m <sup>2</sup>

## General

Density of soil ( $W_e$ ) :	19.0 kN/m <sup>3</sup>
Required ratio of resistance against sliding :	1.5
Strength of steel ( $f_y$ ) :	500 N/mm <sup>2</sup>
Allowable bearing pressure of ground (q) :	200 kN/m <sup>2</sup>

Density of saturated soil ( $W_{sat}$ ) :	0.0 kN/m <sup>3</sup>
Required ratio of resistance against overturning :	1.5
Strength of concrete ( $f_{cu}$ ) :	40 N/mm <sup>2</sup>
Allowable bearing pressure of ground (q) :	

\*\*\* The design is based on cantilever retaining walls which considers 1m length. Each wall will be analysed for 3 cases and designed for the worst case \*\*\*

Left hand side loading in SLS			Right hand side loading in SLS		
Active pressure coefficient ( $K_a$ )	0.49		Active pressure coefficient ( $K_a$ )	0.49	
Passive pressure coefficient ( $K_p$ )	2.04		Passive pressure coefficient ( $K_p$ )	2.04	
Total height of soil behind retaining wall ( $h_{e\ wall}$ )	2.88	m	Total height of soil behind retaining wall ( $h_{e\ wall}$ )	3.15	m
Height of stem ( $h_{stem}$ )	2.70	m	Height of stem ( $h_{stem}$ )	2.70	m
Total height of soil behind stem ( $h_{e\ stem}$ )	2.70	m	Total height of soil behind stem ( $h_{e\ stem}$ )	2.70	m
Self weight of stem ( $SW_{stem}$ )	22.7	kN/m	Self weight of stem ( $SW_{stem}$ )	25.9	kN/m
Total additional horizontal load to stem ( $W_h$ )	0.0	kN/m	Total additional horizontal load to stem ( $W_h$ )	17.8	kN/m
Length of base ( $l_{base}$ )	1.35	m	Length of base ( $l_{base}$ )	1.40	m
Self weight of base ( $SW_{base}$ )	14.6	kN/m	Self weight of base ( $SW_{base}$ )	15.1	kN/m
Self weight of toe ( $SW_{toe}$ )	10.8	kN/m	Self weight of toe ( $SW_{toe}$ )	10.8	kN/m
Total dead load on toe ( $W_{d\ toe\ tot}$ )	0.0	kN/m	Total dead load on toe ( $W_{d\ toe\ tot}$ )	0.0	kN/m
Total live load on toe ( $W_{l\ toe\ tot}$ )	0.0	kN/m	Total live load on toe ( $W_{l\ toe\ tot}$ )	0.0	kN/m
Total surcharge on heel ( $W_{s\ heel}$ )	0.0	kN/m	Total surcharge on heel ( $W_{s\ heel}$ )	0.0	kN/m
Height of saturated soil above base ( $h_{sat}$ )	1.55	m	Height of saturated soil above base ( $h_{sat}$ )	1.55	m
Self weight of saturated soil on heel ( $SW_{sat}$ )	0.0	kN/m	Self weight of saturated soil on heel ( $SW_{sat}$ )	0.0	kN/m
Self weight of non saturated soil behind stem ( $SW_e$ )	0.0	kN/m	Self weight of non saturated soil behind stem ( $SW_e$ )	0.0	kN/m

#### CASE 1: ANALYSIS FOR EXISTING LOADING

Not applicable	Not applicable
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#### Case 2: UNDER TEMPORARY WORK ANALYSIS

(Consider using only the existing vertical dead loads for stability against sliding and overturning without any pressure from ground water)

Left hand side wall			Right hand side wall		
<b>Stability for sliding</b>			<b>Stability for sliding</b>		
$\mu = 0.75 * \tan\phi$	0.27		$\mu = 0.75 * \tan\phi$	0.27	
Active force from soil ( $P_{a\ e\ 2}$ )	38.6	kN/m	Active force from soil ( $P_{a\ e\ 2}$ )	46.2	kN/m
Active force from surcharge ( $P_{a\ s\ 2}$ )	0.0	kN/m	Active force from surcharge ( $P_{a\ s\ 2}$ )	3.4	kN/m
Total sliding force ( $F_2$ )	38.6	kN/m	Total sliding force ( $F_2$ )	67.5	kN/m
Resistance by friction ( $P_{f\ 2}$ )	19.3	kN/m	Resistance by friction ( $P_{f\ 2}$ )	32.0	kN/m
Resistance by passive force ( $P_{p\ 2}$ )	3.9	kN/m	Resistance by passive force ( $P_{p\ 2}$ )	3.9	kN/m
Total resistance force ( $F_{res\ 2}$ )	23.3	kN/m	Sliding resistance force ( $F_{res\ 2}$ )	35.9	kN/m
Ratio of resistance against sliding = $F_{res\ 2} / F_2$	0.6		Ratio of resistance against sliding = $F_{res\ 2} / F_2$	0.5	
0.6 < 1.5	** FAILS. Backfill of soil is required **		0.5 < 1.5	** FAILS. Backfill of soil is required **	
<b>Stability for overturning</b>			<b>Stability for overturning</b>		
Soil ( $M_{e\ 2}$ )	37.1	kNm/m	Soil ( $M_{e\ 2}$ )	48.5	kNm/m
Surcharge ( $M_{s\ 2}$ )	0.0	kNm/m	Surcharge ( $M_{s\ 2}$ )	3.3	kNm/m
Additional horizontal load ( $M_{h\ 2}$ )	0.0	kNm/m	Additional horizontal load ( $M_{h\ 2}$ )	7.7	kNm/m
Total overturning moment ( $M_2$ )	37.1	kNm/m	Total overturning moment ( $M_2$ )	59.5	kNm/m
Resistance by stem & vertical DL ( $M_{r\ stem\ 2}$ )	66.1	kNm/m	Resistance by stem & vertical DL ( $M_{r\ stem\ 2}$ )	122.5	kNm/m
Resistance by base ( $M_{r\ base\ 2}$ )	9.8	kNm/m	Resistance by base ( $M_{r\ base\ 2}$ )	10.6	kNm/m
Resistance by surcharge on heel ( $M_{r\ s\ heel\ 2}$ )	0.0	kNm/m	Resistance by surcharge on heel ( $M_{r\ s\ heel\ 2}$ )	0.0	kNm/m
Total resistance moment ( $M_{res\ 2}$ )	76.0	kNm/m	Total resistance moment ( $M_{res\ 2}$ )	133.1	kNm/m
Ratio of resistance against overturning = $M_{res\ 2} / M_2$	2.0		Ratio of resistance against overturning = $M_{res\ 2} / M_2$	2.2	
2.0 >= 1.5	OK		2.2 >= 1.5	OK	
<b>Bearing pressure in SLS</b>			<b>Bearing pressure in SLS</b>		
Total vertical load on base ( $N_{SLS\ base\ 2}$ )	70.9	kN/m	Total vertical load on base ( $N_{SLS\ base\ 2}$ )	117.2	kN/m

				Page:	3	Job Ref:	MDM406
Distance to reaction ( $X_{SLS\ 2}$ )	0.55	m		Distance to reaction ( $X_{SLS\ 2}$ )	0.63	m	
Eccentricity of vertical load in SLS ( $e_{SLS\ 2}$ )	0.13	m		Eccentricity of vertical load in SLS ( $e_{SLS\ 2}$ )	0.07	m	
$I_{base} / 6 = 0.23 \geq 0.13$	Load resultant lies inside middle third			$I_{base} / 6 = 0.23 \geq 0.07$	Load resultant lies inside middle third		
Pressure under base ( $p_{SLS}$ ) :	81.9	kN/m <sup>2</sup>		Pressure under base ( $p_{SLS}$ ) :	109.4	kN/m <sup>2</sup>	
81.9 <= 200	OK			109.4 <= 200	OK		
<b>Moment for stem in ULS</b>				<b>Moment for stem in ULS</b>			
Soil ( $M_e$ ULS stem 2)	49.2	kNm/m		Soil ( $M_e$ ULS stem 2)	53.5	kNm/m	
Surcharge ( $M_s$ ULS stem 2)	0	kNm/m		Surcharge ( $M_s$ ULS stem 2)	3.7010566	kNm/m	
Additional horizontal loads ( $M_h$ ULS stem 2)	0.0	kNm/m		Additional horizontal loads ( $M_h$ ULS stem 2)	5.2	kNm/m	
Total moment for stem ( $M_{ULS\ stem\ 2}$ )	49.2	kNm/m		Total moment for stem ( $M_{ULS\ stem\ 2}$ )	62.4	kNm/m	
<b>Moment for base in ULS</b>				<b>Moment for base in ULS</b>			
Total vertical load on base ( $N_{ULS\ base\ 2}$ )	107.5	kN/m		Total vertical load on base ( $N_{ULS\ base\ 2}$ )	167.3	kN/m	
Total moment on base ( $M_{ULS\ base\ 2}$ )	51.9	kNm/m		Total moment on base ( $M_{ULS\ base\ 2}$ )	83.7	kNm/m	
Total resistance moment on base ( $M_{res\ ULS\ base\ 2}$ )	106.4	kNm/m		Total resistance moment on base ( $M_{res\ ULS\ base\ 2}$ )	186.4	kNm/m	
Distance to reaction ( $X_{ULS\ 2}$ )	0.51	m		Distance to reaction ( $X_{ULS\ 2}$ )	0.61	m	
Eccentricity of vertical load in ULS ( $e_{ULS\ 2}$ )	0.17	m		Eccentricity of vertical load in ULS ( $e_{ULS\ 2}$ )	0.09	m	
$I_{base} / 6 = 0.23 \geq 0.17$	Load resultant lies inside middle third			$I_{base} / 6 = 0.23 \geq 0.09$	Load resultant lies inside middle third		
Maximum pressure under base ( $p_{max\ ULS\ base\ 2}$ )	139.4	kN/m <sup>2</sup>		Maximum pressure under base ( $p_{max\ ULS\ base\ 2}$ )	163.8	kN/m <sup>2</sup>	
Minimum pressure under base ( $p_{min\ ULS\ base\ 2}$ )	19.9	kN/m <sup>2</sup>		Minimum pressure under base ( $p_{min\ ULS\ base\ 2}$ )	75.3	kN/m <sup>2</sup>	
Bearing length of base ( $L_p$ base 2)	1.35	m		Bearing length of base ( $L_p$ base 2)	1.40	m	
Bearing length of heel ( $L_p$ heel 2)	0.00	m		Bearing length of heel ( $L_p$ heel 2)	0.00	m	
Pressure under heel/stem interface ( $p_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>		Pressure under heel/stem interface ( $p_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>	
Pressure under toe/stem interface ( $p_{ULS\ toe\ 2}$ )	50.9	kN/m <sup>2</sup>		Pressure under toe/stem interface ( $p_{ULS\ toe\ 2}$ )	100.6	kN/m <sup>2</sup>	
Total vertical load on heel ( $N_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>		Total vertical load on heel ( $N_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>	
Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 2}$ )	0.0	kNm/m		Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 2}$ )	0.0	kNm/m	
Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 2}$ )	0.0	kNm/m		Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 2}$ )	0.0	kNm/m	
Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 2}$ )	0.0	kNm/m		Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 2}$ )	0.0	kNm/m	
Moment for toe at wall centre ( $M_{ULS\ toe\ 2}$ )	61.4	kNm/m		Moment for toe at wall centre ( $M_{ULS\ toe\ 2}$ )	87.2	kNm/m	
Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 2}$ )	61.4	kNm/m		Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 2}$ )	87.2	kNm/m	

CASE 3: AFTER CONSTRUCTION ANALYSIS					
(Consider using all loads but no check for stability against sliding is required)					
Left hand side wall		Right hand side wall			
<b>Stability for overturning</b>		<b>Stability for overturning</b>			
Surcharge ( $M_s$ 3)	0.0	kNm/m	Surcharge ( $M_s$ 3)	3.3	kNm/m
Additional horizontal load ( $M_h$ 3)	0.0	kNm/m	Additional horizontal load ( $M_h$ 3)	7.7	kNm/m
Moist backfill above water table ( $M_{mbaw}$ 3)	8.3	kNm/m	Moist backfill above water table ( $M_{mbaw}$ 3)	14.7	kNm/m
Moist backfill below water table ( $M_{mbbw}$ 3)	16.4	kNm/m	Moist backfill below water table ( $M_{mbbw}$ 3)	21.4	kNm/m
Saturated backfill ( $M_{sb}$ 3)	-6.4	kNm/m	Saturated backfill ( $M_{sb}$ 3)	-6.4	kNm/m
Water ( $M_w$ 3)	13.1	kNm/m	Water ( $M_w$ 3)	13.1	kNm/m
Total overturning moment ( $M_3$ )	31.3	kNm/m	Total overturning moment ( $M_3$ )	53.7	kNm/m
Resistance by stem & vertical loads ( $M_r$ stem 3)	79.3	kNm/m	Resistance by stem & vertical loads ( $M_r$ stem 3)	136.6	kNm/m
Resistance by base ( $M_r$ base 3)	9.8	kNm/m	Resistance by base ( $M_r$ base 3)	10.6	kNm/m
Resistance by loads on toe ( $M_r$ toe 3)	0.0	kNm/m	Resistance by loads on toe ( $M_r$ toe 3)	0.0	kNm/m
Resistance by surcharge on heel ( $M_r$ s heel 3)	0.0	kNm/m	Resistance by surcharge on heel ( $M_r$ s heel 3)	0.0	kNm/m
Resistance by moist backfill ( $M_r$ mb 3)	0.0	kNm/m	Resistance by moist backfill ( $M_r$ mb 3)	0.0	kNm/m
Resistance by saturated backfill ( $M_r$ sb 3)	0.0	kNm/m	Resistance by saturated backfill ( $M_r$ sb 3)	0.0	kNm/m
Total resistance moment ( $M_{res}$ 3)	89.1	kNm/m	Total resistance moment ( $M_{res}$ 3)	147.2	kNm/m

				Page:	4	Job Ref:	MDM406
Ratio of resistance against overturning = $M_{res\ 3} / M_3$				Ratio of resistance against overturning = $M_{res\ 3} / M_3$	2.8	2.7	
2.8	$\geq$	1.5	OK	2.7	$\geq$	1.5	OK
<b>Bearing pressure in SLS</b>				<b>Bearing pressure in SLS</b>			
Total vertical load on base ( $N_{SLS\ base\ 3}$ )		82.1	kN/m	Total vertical load on base ( $N_{SLS\ base\ 3}$ )		128.9	kN/m
Distance to reaction ( $X_{SLS\ 3}$ )		0.70	m	Distance to reaction ( $X_{SLS\ 3}$ )		0.72	m
Eccentricity of vertical load in SLS ( $e_{SLS\ 3}$ )		0.03	m	Eccentricity of vertical load in SLS ( $e_{SLS\ 3}$ )		0.02	m
$I_{base} / 6 = 0.23 \geq 0.03$	Load resultant lies inside middle third			$I_{base} / 6 = 0.23 \geq 0.02$	Load resultant lies inside middle third		
Pressure under base ( $p_{SLS}$ ) :		68.7	kN/m <sup>2</sup>	Pressure under base ( $p_{SLS}$ ) :		101.9	kN/m <sup>2</sup>
68.7	$\leq$	200	OK	101.9	$\leq$	200	OK
<b>Moment for stem in ULS</b>				<b>Moment for stem in ULS</b>			
Surcharge ( $M_s\ ULS\ stem\ 3$ )		0	kNm/m	Surcharge ( $M_s\ ULS\ stem\ 3$ )		3.7010566	kNm/m
Additional horizontal loads ( $M_h\ ULS\ stem\ 3$ )		0.0	kNm/m	Additional horizontal loads ( $M_h\ ULS\ stem\ 3$ )		5.1988	kNm/m
Moist backfill above water table ( $M_{mbaw}\ ULS\ stem\ 3$ )		17.8	kNm/m	Moist backfill above water table ( $M_{mbaw}\ ULS\ stem\ 3$ )		18.6	kNm/m
Moist backfill below water table ( $M_{mbbw}\ ULS\ stem\ 3$ )		18.0	kNm/m	Moist backfill below water table ( $M_{mbbw}\ ULS\ stem\ 3$ )		18.0	kNm/m
Saturated backfill ( $M_{sb}\ ULS\ stem\ 3$ )		-4.2	kNm/m	Saturated backfill ( $M_{sb}\ ULS\ stem\ 3$ )		-4.2	kNm/m
Water ( $M_w\ ULS\ stem\ 3$ )		8.5	kNm/m	Water ( $M_w\ ULS\ stem\ 3$ )		8.5	kNm/m
Total moment for stem ( $M_{ULS\ stem\ 3}$ )		40.2	kNm/m	Total moment for stem ( $M_{ULS\ stem\ 3}$ )		49.9	kNm/m
<b>Moment for base in ULS</b>				<b>Moment for base in ULS</b>			
Total vertical load on base ( $N_{ULS\ base\ 3}$ )		116.9	kN/m	Total vertical load on base ( $N_{ULS\ base\ 3}$ )		182.7	kN/m
Total moment on base ( $M_{ULS\ base\ 3}$ )		43.9	kNm/m	Total moment on base ( $M_{ULS\ base\ 3}$ )		75.6	kNm/m
Total resistance moment on base ( $M_{res\ ULS\ base\ 3}$ )		127.2	kNm/m	Total resistance moment on base ( $M_{res\ ULS\ base\ 3}$ )		208.6	kNm/m
Distance to reaction ( $X_{ULS\ 3}$ )		0.71	m	Distance to reaction ( $X_{ULS\ 3}$ )		0.73	m
Eccentricity of vertical load in ULS ( $e_{ULS\ 3}$ )		0.04	m	Eccentricity of vertical load in ULS ( $e_{ULS\ 3}$ )		0.03	
$I_{base} / 6 = 0.23 < 0.71$	Load resultant lies outside middle third			$I_{base} / 6 = 0.23 < 0.73$	Load resultant lies outside middle third		
Maximum pressure under base ( $p_{max\ ULS\ base\ 3}$ )		109.4	kN/m <sup>2</sup>	Maximum pressure under base ( $p_{max\ ULS\ base\ 3}$ )		167.3	kN/m <sup>2</sup>
Minimum pressure under base ( $p_{min\ ULS\ base\ 3}$ )		0.0	kN/m <sup>2</sup>	Minimum pressure under base ( $p_{min\ ULS\ base\ 3}$ )		0.0	kN/m <sup>2</sup>
Bearing length of base ( $L_p\ base\ 3$ )		1.35	m	Bearing length of base ( $L_p\ base\ 3$ )		1.40	m
Bearing length of heel ( $L_p\ heel\ 3$ )		0.00	m	Bearing length of heel ( $L_p\ heel\ 3$ )		0.00	m
Pressure under heel/stem interface ( $p_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>	Pressure under heel/stem interface ( $p_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>
Pressure under toe/stem interface ( $p_{ULS\ toe\ 3}$ )		28.4	kN/m <sup>2</sup>	Pressure under toe/stem interface ( $p_{ULS\ toe\ 3}$ )		47.8	kN/m <sup>2</sup>
Total vertical load on heel ( $N_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>	Total vertical load on heel ( $N_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>
Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 3}$ )		0.0	kNm/m	Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 3}$ )		0.0	kNm/m
Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 3}$ )		0.0	kNm/m	Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 3}$ )		0.0	kNm/m
Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 3}$ )		0.0	kNm/m	Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 3}$ )		0.0	kNm/m
Moment for toe at wall centre ( $M_{ULS\ toe\ 3}$ )		43.0	kNm/m	Moment for toe at wall centre ( $M_{ULS\ toe\ 3}$ )		74.6	kNm/m
Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 3}$ )		43.0	kNm/m	Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 3}$ )		74.6	kNm/m

### DESIGN OF STEMS

Left hand side stem		Right hand side stem				
Cover for reinforcement ( $c_w$ ) :	75	mm	Cover for reinforcement ( $c_w$ ) :	75	mm	
Diameter of tension bars ( $\phi_{t w}$ ) :	16	mm	Tension bars ( $\phi_{t w}$ ) :	3 No. Layers Mesh A393	10	mm
C/C spacing for tension reinforcement ( $S_{t\ wall}$ ) :	200	mm	C/C spacing for tension reinforcement ( $S_{t\ wall}$ ) :	200	mm	
Diameter of distribution bars ( $\phi_{d w}$ ) :	12	mm	Distribution bars ( $\phi_{d w}$ ) :	3 No. Layers Mesh A393	10	mm
C/C spacing for distribution reinforcement ( $S_{d\ wall}$ ) :	200	mm	C/C spacing for distribution reinforcement ( $S_{d\ wall}$ ) :	200	mm	
Design moment ( $M_{wall}$ ) = Max ( $M_{ULS\ stem\ 2}, M_{ULS\ stem\ 3}$ )	49.2	kNm/m	Design moment ( $M_{wall}$ ) = Max ( $M_{ULS\ stem\ 2}, M_{ULS\ stem\ 3}$ )	62.4	kNm/m	
Depth for tension reinforcement ( $d_{wall}$ )	267.0	mm	Depth for tension reinforcement ( $d_{wall}$ )	300.0	mm	

$K_{wall} = M_{wall} / (f_{cu} * 1000 * d_{wall}^2)$	0.017	
0.017 <= 0.156	then only tension reinforcement is required.	
Lever arm ( $Z_{wall}$ )	253.7	mm
Required tension reinforcement ( $A_{st \text{ req wall}}$ )	446	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min wall}}$ )	455	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ wall}}$ ) = Max ( $A_{st \text{ req wall}}, A_{st \text{ min wall}}$ )	455	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro wall}}$ )	1005	mm <sup>2</sup> /m
1005 > 455 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis wall}}$ ) = $A_{st \text{ min wall}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis wall}}$ )	565	mm <sup>2</sup> /m
565 >= 455 OK		
Total horizontal force to wall in ULS ( $F_{ULS \text{ wall}}$ )	47.5	kN/m
Applied shear stress to wall ( $v_{ULS \text{ wall}}$ )	0.18	N/mm <sup>2</sup>
0.18 <= 5.0 OK		
$A_{st \text{ pro in wall}} / (d_{wall} * 10)$	0.38	
Design concrete shear stress $v_c$ wall from Table 3.8 – BS 8110:	0.57	N/mm <sup>2</sup>
0.57 >= 0.18 No shear reinforcement required.		
Design service stress ( $f_s$ wall)	150.9	N/mm <sup>2</sup>
Modification factor for tension	2.0	
Permissible span to depth ration	14.0	
Actual span to depth ration = $h_{stem} / d_{wall}$	10.1	
14.0 >= 10.1 OK		

$K_{wall} = M_{wall} / (f_{cu} * 1000 * d_{wall}^2)$	0.017	
0.017 <= 0.156	then only tension reinforcement is required.	
Lever arm ( $Z_{wall}$ )	285.0	mm
Required tension reinforcement ( $A_{st \text{ req wall}}$ )	503	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min wall}}$ )	520	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ wall}}$ ) = Max ( $A_{st \text{ req wall}}, A_{st \text{ min wall}}$ )	520	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro in wall}}$ )	1178	mm <sup>2</sup> /m
1178 > 520 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis wall}}$ ) = $A_{st \text{ min wall}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis wall}}$ )	1178	mm <sup>2</sup> /m
1178 >= 520 OK		
Total horizontal force to wall in ULS ( $F_{ULS \text{ wall}}$ )	75.4	kN/m
Applied shear stress to wall ( $v_{ULS \text{ wall}}$ )	0.25	N/mm <sup>2</sup>
0.25 <= 5.0 OK		
$A_{st \text{ pro in wall}} / (d_{wall} * 10)$	0.39	
Design concrete shear stress $v_c$ wall from Table 3.8 – BS 8110:	0.57	N/mm <sup>2</sup>
0.57 >= 0.25 No shear reinforcement required.		
Design service stress ( $f_s$ wall)	147.1	N/mm <sup>2</sup>
Modification factor for tension	2.0	
Permissible span to depth ration	14.0	
Actual span to depth ration = $h_{stem} / d_{wall}$	9.0	
14.0 >= 9.0 OK		

## DESIGN OF BASES

Left hand side base	Right hand side base	
Cover for reinforcement ( $c_b$ ):	75	mm
Diameter of tension bars ( $\phi_{t,b}$ ):	16	mm
C/C spacing for tension reinforcement ( $S_{t \text{ base}}$ ):	200	mm
Diameter of distribution bars ( $\phi_{d,b}$ ):	16	mm
C/C spacing for distribution reinforcement ( $S_{d \text{ base}}$ ):	200	mm
Moment for base ( $M_{ULS \text{ base net}}$ ) = Max ( $M_{ULS \text{ base net 2}}, M_{ULS \text{ base net 3}}$ )		
61.4	kNm/m	
Depth for tension reinforcement in base ( $d_{base}$ )	367.0	mm
$K_{base} = M_{ULS \text{ base net}} / (f_{cu} * 1000 * d_{base}^2)$	0.011	
0.011 <= 0.156 then only tension reinforcement is required.		
Lever arm ( $Z_{base}$ )	348.7	mm
Required tension reinforcement ( $A_{st \text{ req base}}$ )	405	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ base}}$ ) = Max( $A_{st \text{ req base}}, A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro base}}$ )	1005	mm <sup>2</sup> /m
1005 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis base}}$ ) = $A_{st \text{ min base}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis base}}$ )	1005	mm <sup>2</sup> /m
1005 >= 585 OK		
Shear for heel at face of wall ( $V_{ULS \text{ heel}}$ )	0.0	kN/m
Shear for toe at face of wall ( $V_{ULS \text{ toe}}$ )	101.8	kN/m
Applied shear stress to base ( $v_{ULS \text{ base}}$ )	0.28	N/mm <sup>2</sup>
0.28 <= 5.0 OK		
$A_{st \text{ pro base}} / (d_{base} * 10)$	0.27	
Cover for reinforcement ( $c_b$ ):	75	mm
Tension bars ( $\phi_{t,b}$ ):	4 No. Layers Mesh A393	10 mm
C/C spacing for tension reinforcement ( $S_{t \text{ base}}$ ):	200	mm
Distribution bars ( $\phi_{d,b}$ ):	4 No. Layers Mesh A393	10 mm
C/C spacing for distribution reinforcement ( $S_{d \text{ base}}$ ):	200	mm
Moment for base ( $M_{ULS \text{ base net}}$ ) = Max ( $M_{ULS \text{ base net 2}}, M_{ULS \text{ base net 3}}$ )		
87.2	kNm/m	
Depth for tension reinforcement in base ( $d_{base}$ )	340.0	mm
$K_{base} = M_{ULS \text{ base net}} / (f_{cu} * 1000 * d_{base}^2)$	0.019	
0.019 <= 0.156 then only tension reinforcement is required.		
Lever arm ( $Z_{base}$ )	323.0	mm
Required tension reinforcement ( $A_{st \text{ req base}}$ )	621	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ base}}$ ) = Max( $A_{st \text{ req base}}, A_{st \text{ min base}}$ )	621	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro base}}$ )	1571	mm <sup>2</sup> /m
1571 > 621 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis base}}$ ) = $A_{st \text{ min base}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis base}}$ )	1571	mm <sup>2</sup> /m
1571 >= 585 OK		
Shear for heel at face of wall ( $V_{ULS \text{ heel}}$ )	0.0	kN/m
Shear for toe at face of wall ( $V_{ULS \text{ toe}}$ )	167.6	kN/m
Applied shear stress to base ( $v_{ULS \text{ base}}$ )	0.60	N/mm <sup>2</sup>
0.60 <= 5.0 OK		
$A_{st \text{ pro base}} / (d_{base} * 10)$	0.46	

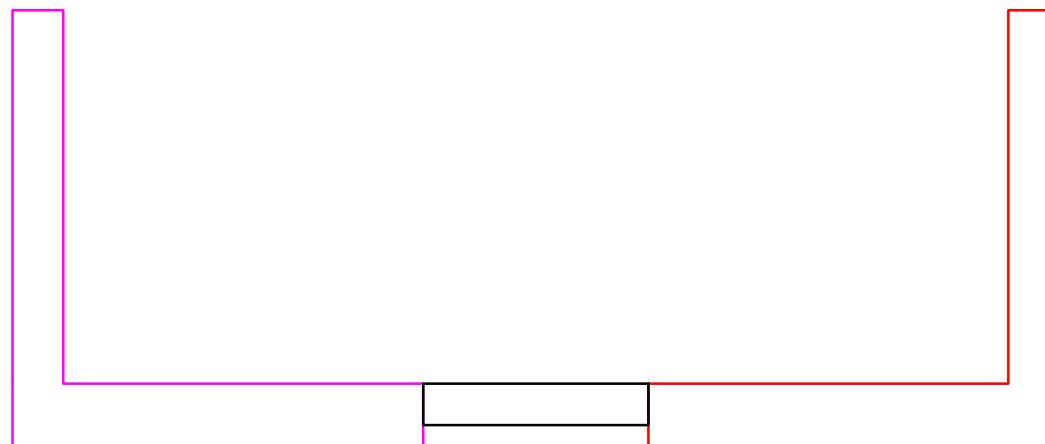
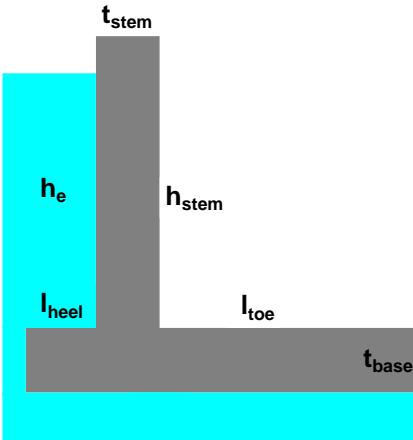
Design concrete shear stress $v_{c \text{ base}}$ from Table 3.8 – BS 8110: 0.50 $\geq$ 0.28 No shear reinforcement required	0.50 N/mm <sup>2</sup>	Design concrete shear stress $v_{c \text{ base}}$ from Table 3.8 – BS 8110: 0.61 $\geq$ 0.60 No shear reinforcement required	[Page: 6 Job Ref: MDM406]
Tension reinforcement for each face of stem:	T16 @ 200 mm	Reinforcement for each face of stem:	3 No. Layers Mesh A393
Distribution reinforcement for each face of stem:	T12 @ 200 mm	Reinforcement in top & bottom of base:	4 No. Layers Mesh A393
Tension reinforcement in top & bottom of base:	T16 @ 200 mm		
Distribution reinforcement in top & bottom of base:	T16 @ 200 mm	Provide T10 @ 200 mm U-bars for top of stem	
Provide T8 @ 200 mm U-bars for top of stem			

### DESIGN OF SLABS IN BASEMENT

Thickness of slab ( $t_{\text{slab}}$ ) :	0.30 m	Span of slab ( $l_{\text{slab}}$ ) :	4.30 m
Diameter of tension bars ( $\phi_{t \text{ slab}}$ ) :	16 mm	C/C of reinforcements ( $S_{t \text{ slab}}$ ) :	200 mm
Diameter of distribution bars ( $\phi_{d \text{ slab}}$ ) :	16 mm	Top cover for reinforcement ( $c_{\text{slab}}$ ) :	25 mm
Diameter of dowel bars ( $\phi_{\text{dowel}}$ ) :	16 mm	C/C of dowel bars ( $S_{\text{dowel}}$ ) :	200 mm
Design slab for heave as worst case loading than water pressure as a simply supported slab connected between base of retaining walls with dowels			
Pressure from heave ( $P_{\text{heave}} = (h_e * W_e) - (20\% * (h_e * W_e))$		$P_{\text{heave}} =$	43.8 kN/m <sup>2</sup>
Net uplift pressure ( $P_{\text{up}} = P_{\text{heave}} - (24 * t_{\text{slab}}) - (\text{Min}(W_{\text{d toe left}}, W_{\text{d toe right}}))$		$P_{\text{up}} =$	36.6 kN/m <sup>2</sup>
Moment by uplift ( $M_{\text{up}} = (1.5 * P_{\text{up}} * l_{\text{slab}}^2) / 8$		$M_{\text{up}} =$	110.2 kNm/m
Shear by uplift ( $V_{\text{up}} = (1.5 * P_{\text{up}} * l_{\text{slab}}) / 2$		$V_{\text{up}} =$	118.0 kN/m
Depth for tension reinforcement in base ( $d_{\text{slab}}$ )		$d_{\text{slab}} =$	267.0 mm
$K_{\text{slab}} = M_{\text{up}} / (f_{\text{cu}} * 1000 * d_{\text{slab}}^2)$		$K_{\text{slab}} =$	0.039
Lever arm ( $Z_{\text{slab}} = \text{Min}((d_{\text{slab}} * (0.5 + \sqrt{0.25 - (K_{\text{slab}} / 0.9)})), (0.95 * d_{\text{slab}}))$		$0.039 \leq 0.156$	Only tension reinforcement is required
Required tension reinforcement ( $A_{st \text{ req slab}} = M_{\text{up}} / (0.87 * f_y * Z_{\text{slab}})$		$Z_{\text{slab}} =$	253.7 mm
Minimum required tension reinforcement ( $A_{st \text{ min slab}} = 0.13 * t_{\text{slab}} * 10^4$		$A_{st \text{ req slab}} =$	999 mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ slab}} = \text{Max}(A_{st \text{ req slab}}, A_{st \text{ min slab}})$		$A_{st \text{ min slab}} =$	390 mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro slab}} = (1000 * \pi * \phi_{t \text{ slab}}^2) / (4 * S_{t \text{ slab}})$		$A_{st \text{ slab}} =$	999 mm <sup>2</sup> /m
Minimum required distribution reinforcement ( $A_{s \text{ min dis slab}} = A_{st \text{ min slab}}$		$A_{st \text{ pro slab}} =$	1005 mm <sup>2</sup> /m
Provided distribution reinforcement ( $A_{s \text{ pro dis slab}} = (1000 * \pi * \phi_{d \text{ slab}}^2) / (4 * S_{t \text{ slab}})$		$1005 > 999$	OK
Design service stress ( $f_{s \text{ slab}} = (2 * f_y * A_{st \text{ slab}}) / (3 * A_{st \text{ pro slab}})$		$A_{s \text{ min dis slab}} =$	390 mm <sup>2</sup> /m
Modification factor for tension = $0.55 + ((477 - f_{s \text{ slab}}) / (120 * (0.9 + (M_{\text{up}} / (1000 * d_{\text{slab}}^2)))))$		$A_{s \text{ pro dis slab}} =$	1005 mm <sup>2</sup> /m
Permissible span to depth ration = Basic span to effective depth ratio * Modification factor for tension * 1		$1005 \geq 390$	OK
Actual span to depth ration = $l_{\text{slab}} / d_{\text{slab}}$		$f_{s \text{ slab}} =$	331.2 N/mm <sup>2</sup>
Provided reinforcement by dowels ( $A_{s \text{ dowel}} = (1000 * \pi * \phi_{\text{dowel}}^2) / (4 * S_{\text{dowel}})$		$20.9 \geq 16.1$	OK
Shear capacity of dowels ( $V_{\text{res dowel}} = (0.6 * f_y * A_{s \text{ dowel}}) / 1000$		$A_{s \text{ dowel}} =$	1005 mm <sup>2</sup> /m
Tension reinforcement in top & bottom of slab:	T16 @ 200 mm	$V_{\text{res dowel}} =$	301.6 kN/m
Distribution reinforcement in top & bottom of slab:	T16 @ 200 mm	$301.6 > 118.0$	OK
Connect slab to the base of retaining walls with T16 dowels @ 200 mm			

# Design of RC Basement walls for Rear Extension Wall to No. 83 and Rear Extension right hand side wall

Page:	7
Job Ref:	MDM406



## Left hand side basement wall

### Rear extension wall to No. 83

Position of stem :	
Total height of wall including thickness of base (h) :	3.15 m
Thickness of wall ( $t_{stem}$ ) :	0.45 m
Height of soil including thickness of base ( $h_e$ ) :	3.15 m
Angle of backfill or slope ( $\beta$ ) :	0 Degree
Internal angle of friction for retained soil ( $\phi$ ) :	20 Degree
Dead surcharge in SLS ( $W_{ds}$ ) :	0.0 kN/m <sup>2</sup>
Live surcharge in SLS ( $W_{ls}$ ) :	1.5 kN/m <sup>2</sup>
Height of surcharge loads from underneath of base ( $h_s$ ) :	3.15 m
Vertical dead load on stem under temporary work in SLS ( $W_{d2}$ ) :	0.0 kN/m
Vertical live load on stem under temporary work in SLS ( $W_{l2}$ ) :	0.0 kN/m
Vertical dead load on stem after construction in SLS ( $W_{d3}$ ) :	14.5 kN/m
Vertical live load on stem after construction in SLS ( $W_{l3}$ ) :	5.0 kN/m
Additional horizontal dead load to stem in SLS ( $W_{dh}$ ) :	0.00 kN/m
Additional horizontal live load to stem in SLS ( $W_{lh}$ ) :	0.00 kN/m
Height of horizontal load from underneath of base ( $h_h$ ) :	0.00 m
Height of ground water from underneath of base ( $h_w$ ) :	2.00 m
Depth of base ( $t_{base}$ ) :	0.45 m
Length of toe ( $l_{toe}$ ) :	1.60 m
Length of heel ( $l_{heel}$ ) :	0.00 m
Dead load by wall, screed or others on toe in SLS ( $W_{d toe}$ ) :	0.00 kN/m <sup>2</sup>
Live load on toe in SLS ( $W_{l toe}$ ) :	0.00 kN/m <sup>2</sup>

## Right hand side basement wall

### Rear Extension right hand side wall

Position of stem :	
Total height of wall including thickness of base (h) :	3.15 m
Thickness of wall ( $t_{stem}$ ) :	0.45 m
Height of soil including thickness of base ( $h_e$ ) :	3.15 m
Angle of backfill or slope ( $\beta$ ) :	0 Degree
Internal angle of friction for retained soil ( $\phi$ ) :	20 Degree
Dead surcharge in SLS ( $W_{ds}$ ) :	0.0 kN/m <sup>2</sup>
Live surcharge in SLS ( $W_{ls}$ ) :	1.5 kN/m <sup>2</sup>
Height of surcharge loads from underneath of base ( $h_s$ ) :	3.15 m
Vertical dead load on stem under temporary work in SLS ( $W_{d2}$ ) :	0.0 kN/m
Vertical live load on stem under temporary work in SLS ( $W_{l2}$ ) :	0.0 kN/m
Vertical dead load on stem after construction in SLS ( $W_{d3}$ ) :	13.8 kN/m
Vertical live load on stem after construction in SLS ( $W_{l3}$ ) :	3.6 kN/m
Additional horizontal dead load to stem in SLS ( $W_{dh}$ ) :	0.00 kN/m
Additional horizontal live load to stem in SLS ( $W_{lh}$ ) :	0.00 kN/m
Height of horizontal load from underneath of base ( $h_h$ ) :	0.00 m
Height of ground water from underneath of base ( $h_w$ ) :	2.00 m
Depth of base ( $t_{base}$ ) :	0.45 m
Length of toe ( $l_{toe}$ ) :	1.60 m
Length of heel ( $l_{heel}$ ) :	0.00 m
Dead load by wall, screed or others on toe in SLS ( $W_{d toe}$ ) :	0.00 kN/m <sup>2</sup>
Live load on toe in SLS ( $W_{l toe}$ ) :	0.00 kN/m <sup>2</sup>

## General

Density of soil ( $W_e$ ) :	19.0 kN/m <sup>3</sup>
Required ratio of resistance against sliding :	1.5
Strength of steel ( $f_y$ ) :	500 N/mm <sup>2</sup>
Allowable bearing pressure of ground (q) :	200 kN/m <sup>2</sup>

Density of saturated soil ( $W_{sat}$ ) :	0.0 kN/m <sup>3</sup>
Required ratio of resistance against overturning :	1.5
Strength of concrete ( $f_{cu}$ ) :	40 N/mm <sup>2</sup>
Live load on toe in SLS ( $W_{l toe}$ ) :	0.00 kN/m <sup>2</sup>

\*\*\* The design is based on cantilever retaining walls which considers 1m length. Each wall will be analysed for 3 cases and designed for the worst case \*\*\*

Left hand side loading in SLS			Right hand side loading in SLS			Page:	8	Job Ref:	MDM406
Active pressure coefficient ( $K_a$ )	0.49		Active pressure coefficient ( $K_a$ )	0.49					
Passive pressure coefficient ( $K_p$ )	2.04		Passive pressure coefficient ( $K_p$ )	2.04					
Total height of soil behind retaining wall ( $h_{e\ wall}$ )	3.15	m	Total height of soil behind retaining wall ( $h_{e\ wall}$ )	3.15	m				
Height of stem ( $h_{stem}$ )	2.70	m	Height of stem ( $h_{stem}$ )	2.70	m				
Total height of soil behind stem ( $h_{e\ stem}$ )	2.70	m	Total height of soil behind stem ( $h_{e\ stem}$ )	2.70	m				
Self weight of stem ( $SW_{stem}$ )	29.2	kN/m	Self weight of stem ( $SW_{stem}$ )	29.2	kN/m				
Total additional horizontal load to stem ( $W_h$ )	0.0	kN/m	Total additional horizontal load to stem ( $W_h$ )	0.0	kN/m				
Length of base ( $l_{base}$ )	2.05	m	Length of base ( $l_{base}$ )	2.05	m				
Self weight of base ( $SW_{base}$ )	22.1	kN/m	Self weight of base ( $SW_{base}$ )	22.1	kN/m				
Self weight of toe ( $SW_{toe}$ )	17.3	kN/m	Self weight of toe ( $SW_{toe}$ )	17.3	kN/m				
Total dead load on toe ( $W_d\ toe\ tot$ )	0.0	kN/m	Total dead load on toe ( $W_d\ toe\ tot$ )	0.0	kN/m				
Total live load on toe ( $W_l\ toe\ tot$ )	0.0	kN/m	Total live load on toe ( $W_l\ toe\ tot$ )	0.0	kN/m				
Total surcharge on heel ( $W_s\ heel$ )	0.0	kN/m	Total surcharge on heel ( $W_s\ heel$ )	0.0	kN/m				
Height of saturated soil above base ( $h_{sat}$ )	1.55	m	Height of saturated soil above base ( $h_{sat}$ )	1.55	m				
Self weight of saturated soil on heel ( $SW_{sat}$ )	0.0	kN/m	Self weight of saturated soil on heel ( $SW_{sat}$ )	0.0	kN/m				
Self weight of non saturated soil behind stem ( $SW_e$ )	0.0	kN/m	Self weight of non saturated soil behind stem ( $SW_e$ )	0.0	kN/m				

#### CASE 1: ANALYSIS FOR EXISTING LOADING

Not applicable	Not applicable
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#### Case 2: UNDER TEMPORARY WORK ANALYSIS

(Consider using only the existing vertical dead loads for stability against sliding and overturning without any pressure from ground water)

Left hand side wall			Right hand side wall		
<b>Stability for sliding</b>			<b>Stability for sliding</b>		
$\mu = 0.75 * \tan\phi$	0.27		$\mu = 0.75 * \tan\phi$	0.27	
Active force from soil ( $P_{a\ e\ 2}$ )	46.2	kN/m	Active force from soil ( $P_{a\ e\ 2}$ )	46.2	kN/m
Active force from surcharge ( $P_{a\ s\ 2}$ )	2.3	kN/m	Active force from surcharge ( $P_{a\ s\ 2}$ )	2.3	kN/m
Total sliding force ( $F_2$ )	48.5	kN/m	Total sliding force ( $F_2$ )	48.5	kN/m
Resistance by friction ( $P_f\ 2$ )	14.0	kN/m	Resistance by friction ( $P_f\ 2$ )	14.0	kN/m
Resistance by passive force ( $P_p\ 2$ )	3.9	kN/m	Resistance by passive force ( $P_p\ 2$ )	3.9	kN/m
Total resistance force ( $F_{res\ 2}$ )	17.9	kN/m	Sliding resistance force ( $F_{res\ 2}$ )	17.9	kN/m
Ratio of resistance against sliding = $F_{res\ 2} / F_2$	0.4		Ratio of resistance against sliding = $F_{res\ 2} / F_2$	0.4	
0.4 < 1.5	** FAILS. Backfill of soil is required **		0.4 < 1.5	** FAILS. Backfill of soil is required **	
<b>Stability for overturning</b>			<b>Stability for overturning</b>		
Soil ( $M_{e\ 2}$ )	48.5	kNm/m	Soil ( $M_{e\ 2}$ )	48.5	kNm/m
Surcharge ( $M_{s\ 2}$ )	3.6	kNm/m	Surcharge ( $M_{s\ 2}$ )	3.6	kNm/m
Additional horizontal load ( $M_{h\ 2}$ )	0.0	kNm/m	Additional horizontal load ( $M_{h\ 2}$ )	0.0	kNm/m
Total overturning moment ( $M_2$ )	52.2	kNm/m	Total overturning moment ( $M_2$ )	52.2	kNm/m
Resistance by stem & vertical DL ( $M_{r\ stem\ 2}$ )	53.2	kNm/m	Resistance by stem & vertical DL ( $M_{r\ stem\ 2}$ )	53.2	kNm/m
Resistance by base ( $M_{r\ base\ 2}$ )	22.7	kNm/m	Resistance by base ( $M_{r\ base\ 2}$ )	22.7	kNm/m
Resistance by surcharge on heel ( $M_{r\ s\ heel\ 2}$ )	0.0	kNm/m	Resistance by surcharge on heel ( $M_{r\ s\ heel\ 2}$ )	0.0	kNm/m
Total resistance moment ( $M_{res\ 2}$ )	75.9	kNm/m	Total resistance moment ( $M_{res\ 2}$ )	75.9	kNm/m
Ratio of resistance against overturning = $M_{res\ 2} / M_2$	1.5		Ratio of resistance against overturning = $M_{res\ 2} / M_2$	1.5	
1.5 <= 1.5	OK		1.5 <= 1.5	OK	
<b>Bearing pressure in SLS</b>			<b>Bearing pressure in SLS</b>		
Total vertical load on base ( $N_{SLS\ base\ 2}$ )	51.3	kN/m	Total vertical load on base ( $N_{SLS\ base\ 2}$ )	51.3	kN/m

				Page:	9	Job Ref:	MDM406
Distance to reaction ( $X_{SLS\ 2}$ )	0.46	m		Distance to reaction ( $X_{SLS\ 2}$ )	0.46	m	
Eccentricity of vertical load in SLS ( $e_{SLS\ 2}$ )	0.56	m		Eccentricity of vertical load in SLS ( $e_{SLS\ 2}$ )	0.56	m	
$I_{base} / 6 = 0.34 < 0.56$	Load resultant lies outside middle third			$I_{base} / 6 = 0.34 < 0.56$	Load resultant lies outside middle third		
Pressure under base ( $p_{SLS}$ ) :	73.9	kN/m <sup>2</sup>		Pressure under base ( $p_{SLS}$ ) :	73.9	kN/m <sup>2</sup>	
73.9 <= 200	OK			73.9 <= 200	OK		
<b>Moment for stem in ULS</b>				<b>Moment for stem in ULS</b>			
Soil ( $M_e$ ULS stem 2)	53.5	kNm/m		Soil ( $M_e$ ULS stem 2)	53.5	kNm/m	
Surcharge ( $M_s$ ULS stem 2)	5.0039058	kNm/m		Surcharge ( $M_s$ ULS stem 2)	5.0039058	kNm/m	
Additional horizontal loads ( $M_h$ ULS stem 2)	0.0	kNm/m		Additional horizontal loads ( $M_h$ ULS stem 2)	0.0	kNm/m	
Total moment for stem ( $M_{ULS\ stem\ 2}$ )	58.5	kNm/m		Total moment for stem ( $M_{ULS\ stem\ 2}$ )	58.5	kNm/m	
<b>Moment for base in ULS</b>				<b>Moment for base in ULS</b>			
Total vertical load on base ( $N_{ULS\ base\ 2}$ )	71.8	kN/m		Total vertical load on base ( $N_{ULS\ base\ 2}$ )	71.8	kN/m	
Total moment on base ( $M_{ULS\ base\ 2}$ )	73.8	kNm/m		Total moment on base ( $M_{ULS\ base\ 2}$ )	73.8	kNm/m	
Total resistance moment on base ( $M_{res\ ULS\ base\ 2}$ )	106.3	kNm/m		Total resistance moment on base ( $M_{res\ ULS\ base\ 2}$ )	106.3	kNm/m	
Distance to reaction ( $X_{ULS\ 2}$ )	0.45	m		Distance to reaction ( $X_{ULS\ 2}$ )	0.45	m	
Eccentricity of vertical load in ULS ( $e_{ULS\ 2}$ )	0.57	m		Eccentricity of vertical load in ULS ( $e_{ULS\ 2}$ )	0.57	m	
$I_{base} / 6 = 0.34 < 0.57$	Load resultant lies outside middle third			$I_{base} / 6 = 0.34 < 0.57$	Load resultant lies outside middle third		
Maximum pressure under base ( $p_{max\ ULS\ base\ 2}$ )	105.8	kN/m <sup>2</sup>		Maximum pressure under base ( $p_{max\ ULS\ base\ 2}$ )	105.8	kN/m <sup>2</sup>	
Minimum pressure under base ( $p_{min\ ULS\ base\ 2}$ )	0.0	kN/m <sup>2</sup>		Minimum pressure under base ( $p_{min\ ULS\ base\ 2}$ )	0.0	kN/m <sup>2</sup>	
Bearing length of base ( $L_p$ base 2)	1.36	m		Bearing length of base ( $L_p$ base 2)	1.36	m	
Bearing length of heel ( $L_p$ heel 2)	-0.69	m		Bearing length of heel ( $L_p$ heel 2)	-0.69	m	
Pressure under heel/stem interface ( $p_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>		Pressure under heel/stem interface ( $p_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>	
Pressure under toe/stem interface ( $p_{ULS\ toe\ 2}$ )	-18.9	kN/m <sup>2</sup>		Pressure under toe/stem interface ( $p_{ULS\ toe\ 2}$ )	-18.9	kN/m <sup>2</sup>	
Total vertical load on heel ( $N_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>		Total vertical load on heel ( $N_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>	
Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 2}$ )	0.0	kNm/m		Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 2}$ )	0.0	kNm/m	
Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 2}$ )	0.0	kNm/m		Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 2}$ )	0.0	kNm/m	
Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 2}$ )	0.0	kNm/m		Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 2}$ )	0.0	kNm/m	
Moment for toe at wall centre ( $M_{ULS\ toe\ 2}$ )	73.1	kNm/m		Moment for toe at wall centre ( $M_{ULS\ toe\ 2}$ )	73.1	kNm/m	
Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 2}$ )	73.1	kNm/m		Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 2}$ )	73.1	kNm/m	

CASE 3: AFTER CONSTRUCTION ANALYSIS					
(Consider using all loads but no check for stability against sliding is required)					
Left hand side wall		Right hand side wall			
<b>Stability for overturning</b>		<b>Stability for overturning</b>			
Surcharge ( $M_{s\ 3}$ )	3.6	kNm/m	Surcharge ( $M_{s\ 3}$ )	3.6	kNm/m
Additional horizontal load ( $M_{h\ 3}$ )	0.0	kNm/m	Additional horizontal load ( $M_{h\ 3}$ )	0.0	kNm/m
Moist backfill above water table ( $M_{mbaw\ 3}$ )	14.7	kNm/m	Moist backfill above water table ( $M_{mbaw\ 3}$ )	14.7	kNm/m
Moist backfill below water table ( $M_{mbbw\ 3}$ )	21.4	kNm/m	Moist backfill below water table ( $M_{mbbw\ 3}$ )	21.4	kNm/m
Saturated backfill ( $M_{sb\ 3}$ )	-6.4	kNm/m	Saturated backfill ( $M_{sb\ 3}$ )	-6.4	kNm/m
Water ( $M_w\ 3$ )	13.1	kNm/m	Water ( $M_w\ 3$ )	13.1	kNm/m
Total overturning moment ( $M_3$ )	46.4	kNm/m	Total overturning moment ( $M_3$ )	46.4	kNm/m
Resistance by stem & vertical loads ( $M_{r\ stem\ 3}$ )	88.8	kNm/m	Resistance by stem & vertical loads ( $M_{r\ stem\ 3}$ )	85.0	kNm/m
Resistance by base ( $M_{r\ base\ 3}$ )	22.7	kNm/m	Resistance by base ( $M_{r\ base\ 3}$ )	22.7	kNm/m
Resistance by loads on toe ( $M_{r\ toe\ 3}$ )	0.0	kNm/m	Resistance by loads on toe ( $M_{r\ toe\ 3}$ )	0.0	kNm/m
Resistance by surcharge on heel ( $M_{r\ s\ heel\ 3}$ )	0.0	kNm/m	Resistance by surcharge on heel ( $M_{r\ s\ heel\ 3}$ )	0.0	kNm/m
Resistance by moist backfill ( $M_{r\ mb\ 3}$ )	0.0	kNm/m	Resistance by moist backfill ( $M_{r\ mb\ 3}$ )	0.0	kNm/m
Resistance by saturated backfill ( $M_{r\ sb\ 3}$ )	0.0	kNm/m	Resistance by saturated backfill ( $M_{r\ sb\ 3}$ )	0.0	kNm/m
Total resistance moment ( $M_{res\ 3}$ )	111.5	kNm/m	Total resistance moment ( $M_{res\ 3}$ )	107.7	kNm/m

				Page:	10	Job Ref:	MDM406
Ratio of resistance against overturning = $M_{res\ 3} / M_3$				Ratio of resistance against overturning = $M_{res\ 3} / M_3$			
2.4	$\geq$	1.5	OK	2.3	$\geq$	1.5	OK
<b>Bearing pressure in SLS</b>							
Total vertical load on base ( $N_{SLS\ base\ 3}$ )		70.8	kN/m	Total vertical load on base ( $N_{SLS\ base\ 3}$ )		68.7	kN/m
Distance to reaction ( $X_{SLS\ 3}$ )		0.92	m	Distance to reaction ( $X_{SLS\ 3}$ )		0.89	m
Eccentricity of vertical load in SLS ( $e_{SLS\ 3}$ )		0.11	m	Eccentricity of vertical load in SLS ( $e_{SLS\ 3}$ )		0.13	m
$I_{base} / 6 = 0.34 \geq 0.11$		Load resultant lies inside middle third		$I_{base} / 6 = 0.34 \geq 0.13$		Load resultant lies inside middle third	
Pressure under base ( $p_{SLS}$ ):		45.2	kN/m <sup>2</sup>	Pressure under base ( $p_{SLS}$ ):		46.6	kN/m <sup>2</sup>
45.2 $\leq$ 200	OK			46.6 $\leq$ 200	OK		
<b>Moment for stem in ULS</b>							
Surcharge ( $M_s\ ULS\ stem\ 3$ )		5.0039058	kNm/m	Surcharge ( $M_s\ ULS\ stem\ 3$ )		5.0039058	kNm/m
Additional horizontal loads ( $M_h\ ULS\ stem\ 3$ )		0.0	kNm/m	Additional horizontal loads ( $M_h\ ULS\ stem\ 3$ )		0	kNm/m
Moist backfill above water table ( $M_{mbaw}\ ULS\ stem\ 3$ )		18.6	kNm/m	Moist backfill above water table ( $M_{mbaw}\ ULS\ stem\ 3$ )		18.6	kNm/m
Moist backfill below water table ( $M_{mbbw}\ ULS\ stem\ 3$ )		18.0	kNm/m	Moist backfill below water table ( $M_{mbbw}\ ULS\ stem\ 3$ )		18.0	kNm/m
Saturated backfill ( $M_{sb}\ ULS\ stem\ 3$ )		-4.2	kNm/m	Saturated backfill ( $M_{sb}\ ULS\ stem\ 3$ )		-4.2	kNm/m
Water ( $M_w\ ULS\ stem\ 3$ )		8.5	kNm/m	Water ( $M_w\ ULS\ stem\ 3$ )		8.5	kNm/m
Total moment for stem ( $M_{ULS\ stem\ 3}$ )		46.0	kNm/m	Total moment for stem ( $M_{ULS\ stem\ 3}$ )		46.0	kNm/m
<b>Moment for base in ULS</b>							
Total vertical load on base ( $N_{ULS\ base\ 3}$ )		100.1	kN/m	Total vertical load on base ( $N_{ULS\ base\ 3}$ )		96.9	kN/m
Total moment on base ( $M_{ULS\ base\ 3}$ )		65.7	kNm/m	Total moment on base ( $M_{ULS\ base\ 3}$ )		65.7	kNm/m
Total resistance moment on base ( $M_{res\ ULS\ base\ 3}$ )		157.9	kNm/m	Total resistance moment on base ( $M_{res\ ULS\ base\ 3}$ )		152.0	kNm/m
Distance to reaction ( $X_{ULS\ 3}$ )		0.92	m	Distance to reaction ( $X_{ULS\ 3}$ )		0.89	m
Eccentricity of vertical load in ULS ( $e_{ULS\ 3}$ )		0.10	m	Eccentricity of vertical load in ULS ( $e_{ULS\ 3}$ )		0.13	
$I_{base} / 6 = 0.34 < 0.92$		Load resultant lies outside middle third		$I_{base} / 6 = 0.34 < 0.89$		Load resultant lies outside middle third	
Maximum pressure under base ( $p_{max\ ULS\ base\ 3}$ )		72.5	kN/m <sup>2</sup>	Maximum pressure under base ( $p_{max\ ULS\ base\ 3}$ )		72.5	kN/m <sup>2</sup>
Minimum pressure under base ( $p_{min\ ULS\ base\ 3}$ )		0.0	kN/m <sup>2</sup>	Minimum pressure under base ( $p_{min\ ULS\ base\ 3}$ )		0.0	kN/m <sup>2</sup>
Bearing length of base ( $L_p\ base\ 3$ )		2.05	m	Bearing length of base ( $L_p\ base\ 3$ )		2.05	m
Bearing length of heel ( $L_p\ heel\ 3$ )		0.00	m	Bearing length of heel ( $L_p\ heel\ 3$ )		0.00	m
Pressure under heel/stem interface ( $p_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>	Pressure under heel/stem interface ( $p_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>
Pressure under toe/stem interface ( $p_{ULS\ toe\ 3}$ )		15.9	kN/m <sup>2</sup>	Pressure under toe/stem interface ( $p_{ULS\ toe\ 3}$ )		15.9	kN/m <sup>2</sup>
Total vertical load on heel ( $N_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>	Total vertical load on heel ( $N_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>
Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 3}$ )		0.0	kNm/m	Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 3}$ )		0.0	kNm/m
Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 3}$ )		0.0	kNm/m	Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 3}$ )		0.0	kNm/m
Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 3}$ )		0.0	kNm/m	Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 3}$ )		0.0	kNm/m
Moment for toe at wall centre ( $M_{ULS\ toe\ 3}$ )		59.7	kNm/m	Moment for toe at wall centre ( $M_{ULS\ toe\ 3}$ )		59.8	kNm/m
Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 3}$ )		59.7	kNm/m	Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 3}$ )		59.8	kNm/m

### DESIGN OF STEMS

Left hand side stem		Right hand side stem	
Cover for reinforcement ( $c_w$ ):	75 mm	Cover for reinforcement ( $c_w$ ):	75 mm
Tension bars ( $\phi_{t w}$ ):	3 No. Layers Mesh A393	Tension bars ( $\phi_{t w}$ ):	10 mm
C/C spacing for tension reinforcement ( $S_{t\ wall}$ ):	200 mm	C/C spacing for tension reinforcement ( $S_{t\ wall}$ ):	200 mm
Distribution bars ( $\phi_{d w}$ ):	3 No. Layers Mesh A393	Distribution bars ( $\phi_{d w}$ ):	10 mm
C/C spacing for distribution reinforcement ( $S_{d\ wall}$ ):	200 mm	C/C spacing for distribution reinforcement ( $S_{d\ wall}$ ):	200 mm
Design moment ( $M_{wall}$ ) = Max ( $M_{ULS\ stem\ 2}, M_{ULS\ stem\ 3}$ )	58.5 kNm/m	Design moment ( $M_{wall}$ ) = Max ( $M_{ULS\ stem\ 2}, M_{ULS\ stem\ 3}$ )	58.5 kNm/m
Depth for tension reinforcement ( $d_{wall}$ )	350.0 mm	Depth for tension reinforcement ( $d_{wall}$ )	350.0 mm

$K_{wall} = M_{wall} / (f_{cu} * 1000 * d_{wall}^2)$	0.012	
0.012 <= 0.156	then only tension reinforcement is required.	
Lever arm ( $Z_{wall}$ )	332.5	mm
Required tension reinforcement ( $A_{st \text{ req wall}}$ )	404	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ wall}}$ ) = Max ( $A_{st \text{ req wall}}, A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro wall}}$ )	1178	mm <sup>2</sup> /m
1178 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis wall}}$ ) = $A_{st \text{ min wall}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis wall}}$ )	1178	mm <sup>2</sup> /m
1178 >= 585 OK		
Total horizontal force to wall in ULS ( $F_{ULS \text{ wall}}$ )	49.4	kN/m
Applied shear stress to wall ( $v_{ULS \text{ wall}}$ )	0.14	N/mm <sup>2</sup>
0.14 <= 5.0 OK		
$A_{st \text{ pro in wall}} / (d_{wall} * 10)$	0.34	
Design concrete shear stress $v_c$ wall from Table 3.8 – BS 8110:	0.57	N/mm <sup>2</sup>
0.57 >= 0.14 No shear reinforcement required.		
Design service stress ( $f_s$ wall)	165.5	N/mm <sup>2</sup>
Modification factor for tension	2.0	
Permissible span to depth ration	14.0	
Actual span to depth ration = $h_{stem} / d_{wall}$	7.7	
14.0 >= 7.7 OK		

$K_{wall} = M_{wall} / (f_{cu} * 1000 * d_{wall}^2)$	0.012	
0.012 <= 0.156	then only tension reinforcement is required.	
Lever arm ( $Z_{wall}$ )	332.5	mm
Required tension reinforcement ( $A_{st \text{ req wall}}$ )	404	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ wall}}$ ) = Max ( $A_{st \text{ req wall}}, A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro in wall}}$ )	1178	mm <sup>2</sup> /m
1178 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis wall}}$ ) = $A_{st \text{ min wall}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis wall}}$ )	1178	mm <sup>2</sup> /m
1178 >= 585 OK		
Total horizontal force to wall in ULS ( $F_{ULS \text{ wall}}$ )	49.4	kN/m
Applied shear stress to wall ( $v_{ULS \text{ wall}}$ )	0.14	N/mm <sup>2</sup>
0.14 <= 5.0 OK		
$A_{st \text{ pro in wall}} / (d_{wall} * 10)$	0.34	
Design concrete shear stress $v_c$ wall from Table 3.8 – BS 8110:	0.57	N/mm <sup>2</sup>
0.57 >= 0.14 No shear reinforcement required.		
Design service stress ( $f_s$ wall)	165.5	N/mm <sup>2</sup>
Modification factor for tension	2.0	
Permissible span to depth ration	14.0	
Actual span to depth ration = $h_{stem} / d_{wall}$	7.7	
14.0 >= 7.7 OK		

## DESIGN OF BASES

Left hand side base	Right hand side base	
Cover for reinforcement ( $c_b$ ) :	<b>75</b>	mm
Tension bars ( $\phi_{t b}$ ) :	4 No. Layers Mesh A393	<b>10</b> mm
C/C spacing for tension reinforcement ( $S_{t \text{ base}}$ ) :	<b>200</b>	mm
Distribution bars ( $\phi_{d b}$ ) :	4 No. Layers Mesh A393	<b>10</b> mm
C/C spacing for distribution reinforcement ( $S_{d \text{ base}}$ ) :	<b>200</b>	mm
Moment for base ( $M_{ULS \text{ base net}}$ ) = Max ( $M_{ULS \text{ base net 2}}, M_{ULS \text{ base net 3}}$ )	73.1	kNm/m
Depth for tension reinforcement in base ( $d_{base}$ )	340.0	mm
$K_{base} = M_{ULS \text{ base net}} / (f_{cu} * 1000 * d_{base}^2)$	0.016	
0.016 <= 0.156 then only tension reinforcement is required.		
Lever arm ( $Z_{base}$ )	323.0	mm
Required tension reinforcement ( $A_{st \text{ req base}}$ )	520	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ base}}$ ) = Max( $A_{st \text{ req base}}, A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro base}}$ )	1571	mm <sup>2</sup> /m
1571 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis base}}$ ) = $A_{st \text{ min base}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis base}}$ )	1571	mm <sup>2</sup> /m
1571 >= 585 OK		
Shear for heel at face of wall ( $V_{ULS \text{ heel}}$ )	0.0	kN/m
Shear for toe at face of wall ( $V_{ULS \text{ toe}}$ )	75.9	kN/m
Applied shear stress to base ( $v_{ULS \text{ base}}$ )	0.22	N/mm <sup>2</sup>
0.22 <= 5.0 OK		
$A_{st \text{ pro base}} / (d_{base} * 10)$	0.46	
Moment for base ( $M_{ULS \text{ base net}}$ ) = Max ( $M_{ULS \text{ base net 2}}, M_{ULS \text{ base net 3}}$ )	73.1	kNm/m
Depth for tension reinforcement in base ( $d_{base}$ )	340.0	mm
$K_{base} = M_{ULS \text{ base net}} / (f_{cu} * 1000 * d_{base}^2)$	0.016	
0.016 <= 0.156 then only tension reinforcement is required.		
Lever arm ( $Z_{base}$ )	323.0	mm
Required tension reinforcement ( $A_{st \text{ req base}}$ )	520	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ base}}$ ) = Max( $A_{st \text{ req base}}, A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro base}}$ )	1571	mm <sup>2</sup> /m
1571 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis base}}$ ) = $A_{st \text{ min base}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis base}}$ )	1571	mm <sup>2</sup> /m
1571 >= 585 OK		
Shear for heel at face of wall ( $V_{ULS \text{ heel}}$ )	0.0	kN/m
Shear for toe at face of wall ( $V_{ULS \text{ toe}}$ )	72.7	kN/m
Applied shear stress to base ( $v_{ULS \text{ base}}$ )	0.21	N/mm <sup>2</sup>
0.21 <= 5.0 OK		
$A_{st \text{ pro base}} / (d_{base} * 10)$	0.46	

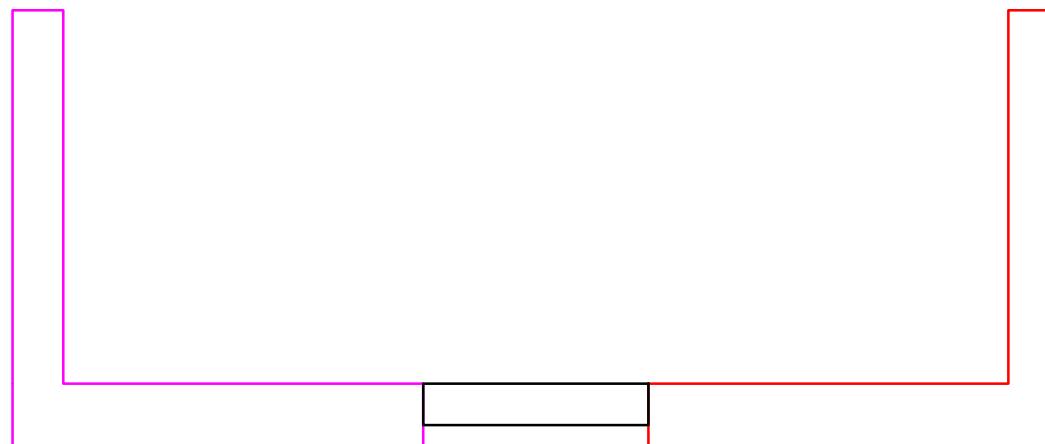
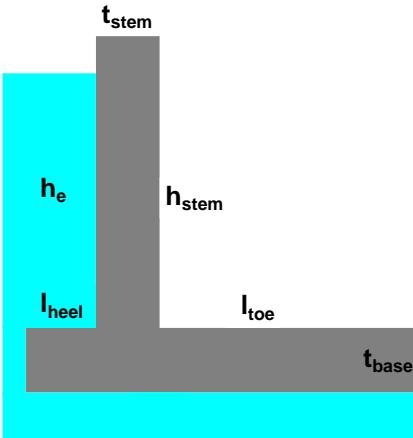
			Page:	12	Job Ref:	MDM406
Design concrete shear stress $v_{c \text{ base}}$ from Table 3.8 – BS 8110: 0.50 $\geq$ 0.22	No shear reinforcement required	0.50 N/mm <sup>2</sup>	Design concrete shear stress $v_{c \text{ base}}$ from Table 3.8 – BS 8110: 0.61 $\geq$ 0.21	No shear reinforcement required	0.61 N/mm <sup>2</sup>	
Tension reinforcement for each face of stem:	3 No. Layers Mesh A393		Reinforcement for each face of stem:	3 No. Layers Mesh A393		
Tension reinforcement in top & bottom of base:	4 No. Layers Mesh A393		Reinforcement in top & bottom of base:	4 No. Layers Mesh A393		
Provide T10 @ 200 mm U-bars for top of stem			Provide T10 @ 200 mm U-bars for top of stem			

### DESIGN OF SLABS IN BASEMENT

Thickness of slab ( $t_{\text{slab}}$ ) :	0.30 m	Span of slab ( $l_{\text{slab}}$ ) :	3.90 m		
Diameter of tension bars ( $\phi_{t \text{ slab}}$ ) :	16 mm	C/C of reinforcements ( $S_{t \text{ slab}}$ ) :	200 mm		
Diameter of distribution bars ( $\phi_{d \text{ slab}}$ ) :	16 mm	Top cover for reinforcement ( $c_{\text{slab}}$ ) :	25 mm		
Diameter of dowel bars ( $\phi_{\text{dowel}}$ ) :	16 mm	C/C of dowel bars ( $S_{\text{dowel}}$ ) :	200 mm		
Design slab for heave as worst case loading than water pressure as a simply supported slab connected between base of retaining walls with dowels					
Pressure from heave ( $P_{\text{heave}} = (h_e * W_e) - (20\% * (h_e * W_e))$		$P_{\text{heave}} =$	47.9 kN/m <sup>2</sup>		
Net uplift pressure ( $P_{\text{up}} = P_{\text{heave}} - (24 * t_{\text{slab}}) - (\text{Min} (W_{\text{d toe left}}, W_{\text{d toe right}}))$		$P_{\text{up}} =$	40.7 kN/m <sup>2</sup>		
Moment by uplift ( $M_{\text{up}} = (1.5 * P_{\text{up}} * l_{\text{slab}}^2) / 8$		$M_{\text{up}} =$	105.3 kNm/m		
Shear by uplift ( $V_{\text{up}} = (1.5 * P_{\text{up}} * l_{\text{slab}}) / 2$		$V_{\text{up}} =$	119.0 kN/m		
Depth for tension reinforcement in base ( $d_{\text{slab}}$ )		$d_{\text{slab}} =$	267.0 mm		
$K_{\text{slab}} = M_{\text{up}} / (f_{\text{cu}} * 1000 * d_{\text{slab}}^2)$		$K_{\text{slab}} =$	0.037		
Lever arm ( $Z_{\text{slab}} = \text{Min} ((d_{\text{slab}} * (0.5 + \sqrt{0.25 - (K_{\text{slab}} / 0.9)})), (0.95 * d_{\text{slab}}))$		$0.037 \leq 0.156$	Only tension reinforcement is required		
Required tension reinforcement ( $A_{\text{st req slab}} = M_{\text{up}} / (0.87 * f_y * Z_{\text{slab}})$		$Z_{\text{slab}} =$	253.7 mm		
Minimum required tension reinforcement ( $A_{\text{st min slab}} = 0.13 * t_{\text{slab}} * 10^4$		$A_{\text{st req slab}} =$	954 mm <sup>2</sup> /m		
Tension reinforcement ( $A_{\text{st slab}} = \text{Max}(A_{\text{st req slab}}, A_{\text{st min slab}})$		$A_{\text{st min slab}} =$	390 mm <sup>2</sup> /m		
Provided tension reinforcement ( $A_{\text{st pro slab}} = (1000 * \pi * \phi_{t \text{ slab}}^2) / (4 * S_{t \text{ slab}})$		$A_{\text{st slab}} =$	954 mm <sup>2</sup> /m		
Minimum required distribution reinforcement ( $A_{\text{s min dis slab}} = A_{\text{st min slab}}$		$A_{\text{st pro slab}} =$	1005 mm <sup>2</sup> /m		
Provided distribution reinforcement ( $A_{\text{s pro dis slab}} = (1000 * \pi * \phi_{d \text{ slab}}^2) / (4 * S_{t \text{ slab}})$		$1005 > 954$	OK		
Design service stress ( $f_{\text{s slab}} = (2 * f_y * A_{\text{st slab}}) / (3 * A_{\text{st pro slab}})$		$f_{\text{s slab}} =$	316.4 N/mm <sup>2</sup>		
Modification factor for tension = $0.55 + ((477 - f_{\text{s slab}}) / (120 * (0.9 + (M_{\text{up}} / (1000 * d_{\text{slab}}^2)))))$			1.1		
Permissible span to depth ration = Basic span to effective depth ratio * Modification factor for tension * 1			22.3		
Actual span to depth ration = $l_{\text{slab}} / d_{\text{slab}}$			14.6		
Provided reinforcement by dowels ( $A_{\text{s dowel}} = (1000 * \pi * \phi_{\text{dowel}}^2) / (4 * S_{\text{dowel}})$		$22.3 \geq 14.6$	OK		
Shear capacity of dowels ( $V_{\text{res dowel}} = (0.6 * f_y * A_{\text{s dowel}}) / 1000$		$A_{\text{s dowel}} =$	1005 mm <sup>2</sup> /m		
		$V_{\text{res dowel}} =$	301.6 kN/m		
		$301.6 > 119.0$	OK		
Tension reinforcement in top & bottom of slab:	T16 @ 200 mm				
Distribution reinforcement in top & bottom of slab:	T16 @ 200 mm				
Connect slab to the base of retaining walls with T16 dowels @ 200 mm					

# Design of RC Basement walls for Rear Extension Wall to No. 83 and Rear Extension right hand side wall

Page:	13
Job Ref:	MDM406



## Left hand side basement wall

### Rear extension wall to No. 83

Position of stem :	
Total height of wall including thickness of base (h) :	3.15 m
Thickness of wall ( $t_{stem}$ ) :	0.45 m
Height of soil including thickness of base ( $h_e$ ) :	3.15 m
Angle of backfill or slope ( $\beta$ ) :	0 Degree
Internal angle of friction for retained soil ( $\phi$ ) :	20 Degree
Dead surcharge in SLS ( $W_{ds}$ ) :	0.0 kN/m <sup>2</sup>
Live surcharge in SLS ( $W_{ls}$ ) :	1.5 kN/m <sup>2</sup>
Height of surcharge loads from underneath of base ( $h_s$ ) :	3.15 m
Vertical dead load on stem under temporary work in SLS ( $W_{d2}$ ) :	0.0 kN/m
Vertical live load on stem under temporary work in SLS ( $W_{l2}$ ) :	0.0 kN/m
Vertical dead load on stem after construction in SLS ( $W_{d3}$ ) :	14.5 kN/m
Vertical live load on stem after construction in SLS ( $W_{l3}$ ) :	5.0 kN/m
Additional horizontal dead load to stem in SLS ( $W_{dh}$ ) :	0.00 kN/m
Additional horizontal live load to stem in SLS ( $W_{lh}$ ) :	0.00 kN/m
Height of horizontal load from underneath of base ( $h_h$ ) :	0.00 m
Height of ground water from underneath of base ( $h_w$ ) :	2.00 m
Depth of base ( $t_{base}$ ) :	0.45 m
Length of toe ( $l_{toe}$ ) :	1.60 m
Length of heel ( $l_{heel}$ ) :	0.00 m
Dead load by wall, screed or others on toe in SLS ( $W_{d toe}$ ) :	0.00 kN/m <sup>2</sup>
Live load on toe in SLS ( $W_{l toe}$ ) :	0.00 kN/m <sup>2</sup>

## Right hand side basement wall

### Rear Extension right hand side wall

Position of stem :	
Total height of wall including thickness of base (h) :	3.15 m
Thickness of wall ( $t_{stem}$ ) :	0.45 m
Height of soil including thickness of base ( $h_e$ ) :	3.15 m
Angle of backfill or slope ( $\beta$ ) :	0 Degree
Internal angle of friction for retained soil ( $\phi$ ) :	20 Degree
Dead surcharge in SLS ( $W_{ds}$ ) :	0.0 kN/m <sup>2</sup>
Live surcharge in SLS ( $W_{ls}$ ) :	1.5 kN/m <sup>2</sup>
Height of surcharge loads from underneath of base ( $h_s$ ) :	3.15 m
Vertical dead load on stem under temporary work in SLS ( $W_{d2}$ ) :	0.0 kN/m
Vertical live load on stem under temporary work in SLS ( $W_{l2}$ ) :	0.0 kN/m
Vertical dead load on stem after construction in SLS ( $W_{d3}$ ) :	13.8 kN/m
Vertical live load on stem after construction in SLS ( $W_{l3}$ ) :	3.6 kN/m
Additional horizontal dead load to stem in SLS ( $W_{dh}$ ) :	0.00 kN/m
Additional horizontal live load to stem in SLS ( $W_{lh}$ ) :	0.00 kN/m
Height of horizontal load from underneath of base ( $h_h$ ) :	0.00 m
Height of ground water from underneath of base ( $h_w$ ) :	2.00 m
Depth of base ( $t_{base}$ ) :	0.45 m
Length of toe ( $l_{toe}$ ) :	1.60 m
Length of heel ( $l_{heel}$ ) :	0.00 m
Dead load by wall, screed or others on toe in SLS ( $W_{d toe}$ ) :	0.00 kN/m <sup>2</sup>
Live load on toe in SLS ( $W_{l toe}$ ) :	0.00 kN/m <sup>2</sup>

## General

Density of soil ( $W_e$ ) :	19.0 kN/m <sup>3</sup>
Required ratio of resistance against sliding :	1.5
Strength of steel ( $f_y$ ) :	500 N/mm <sup>2</sup>
Allowable bearing pressure of ground (q) :	200 kN/m <sup>2</sup>

Density of saturated soil ( $W_{sat}$ ) :	0.0 kN/m <sup>3</sup>
Required ratio of resistance against overturning :	1.5
Strength of concrete ( $f_{cu}$ ) :	40 N/mm <sup>2</sup>
Live load on toe in SLS ( $W_{l toe}$ ) :	0.00 kN/m <sup>2</sup>

\*\*\* The design is based on cantilever retaining walls which considers 1m length. Each wall will be analysed for 3 cases and designed for the worst case \*\*\*

Left hand side loading in SLS			Right hand side loading in SLS			Page:	14	Job Ref:	MDM406
Active pressure coefficient ( $K_a$ )	0.49		Active pressure coefficient ( $K_a$ )	0.49					
Passive pressure coefficient ( $K_p$ )	2.04		Passive pressure coefficient ( $K_p$ )	2.04					
Total height of soil behind retaining wall ( $h_{e\ wall}$ )	3.15	m	Total height of soil behind retaining wall ( $h_{e\ wall}$ )	3.15	m				
Height of stem ( $h_{stem}$ )	2.70	m	Height of stem ( $h_{stem}$ )	2.70	m				
Total height of soil behind stem ( $h_{e\ stem}$ )	2.70	m	Total height of soil behind stem ( $h_{e\ stem}$ )	2.70	m				
Self weight of stem ( $SW_{stem}$ )	29.2	kN/m	Self weight of stem ( $SW_{stem}$ )	29.2	kN/m				
Total additional horizontal load to stem ( $W_h$ )	0.0	kN/m	Total additional horizontal load to stem ( $W_h$ )	0.0	kN/m				
Length of base ( $l_{base}$ )	2.05	m	Length of base ( $l_{base}$ )	2.05	m				
Self weight of base ( $SW_{base}$ )	22.1	kN/m	Self weight of base ( $SW_{base}$ )	22.1	kN/m				
Self weight of toe ( $SW_{toe}$ )	17.3	kN/m	Self weight of toe ( $SW_{toe}$ )	17.3	kN/m				
Total dead load on toe ( $W_d\ toe\ tot$ )	0.0	kN/m	Total dead load on toe ( $W_d\ toe\ tot$ )	0.0	kN/m				
Total live load on toe ( $W_l\ toe\ tot$ )	0.0	kN/m	Total live load on toe ( $W_l\ toe\ tot$ )	0.0	kN/m				
Total surcharge on heel ( $W_s\ heel$ )	0.0	kN/m	Total surcharge on heel ( $W_s\ heel$ )	0.0	kN/m				
Height of saturated soil above base ( $h_{sat}$ )	1.55	m	Height of saturated soil above base ( $h_{sat}$ )	1.55	m				
Self weight of saturated soil on heel ( $SW_{sat}$ )	0.0	kN/m	Self weight of saturated soil on heel ( $SW_{sat}$ )	0.0	kN/m				
Self weight of non saturated soil behind stem ( $SW_e$ )	0.0	kN/m	Self weight of non saturated soil behind stem ( $SW_e$ )	0.0	kN/m				

#### CASE 1: ANALYSIS FOR EXISTING LOADING

Not applicable	Not applicable
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#### Case 2: UNDER TEMPORARY WORK ANALYSIS

(Consider using only the existing vertical dead loads for stability against sliding and overturning without any pressure from ground water)

Left hand side wall			Right hand side wall		
<b>Stability for sliding</b>			<b>Stability for sliding</b>		
$\mu = 0.75 * \tan\phi$	0.27		$\mu = 0.75 * \tan\phi$	0.27	
Active force from soil ( $P_{a\ e\ 2}$ )	46.2	kN/m	Active force from soil ( $P_{a\ e\ 2}$ )	46.2	kN/m
Active force from surcharge ( $P_{a\ s\ 2}$ )	2.3	kN/m	Active force from surcharge ( $P_{a\ s\ 2}$ )	2.3	kN/m
Total sliding force ( $F_2$ )	48.5	kN/m	Total sliding force ( $F_2$ )	48.5	kN/m
Resistance by friction ( $P_f\ 2$ )	14.0	kN/m	Resistance by friction ( $P_f\ 2$ )	14.0	kN/m
Resistance by passive force ( $P_p\ 2$ )	3.9	kN/m	Resistance by passive force ( $P_p\ 2$ )	3.9	kN/m
Total resistance force ( $F_{res\ 2}$ )	17.9	kN/m	Sliding resistance force ( $F_{res\ 2}$ )	17.9	kN/m
Ratio of resistance against sliding = $F_{res\ 2} / F_2$	0.4		Ratio of resistance against sliding = $F_{res\ 2} / F_2$	0.4	
0.4 < 1.5	** FAILS. Backfill of soil is required **		0.4 < 1.5	** FAILS. Backfill of soil is required **	
<b>Stability for overturning</b>			<b>Stability for overturning</b>		
Soil ( $M_{e\ 2}$ )	48.5	kNm/m	Soil ( $M_{e\ 2}$ )	48.5	kNm/m
Surcharge ( $M_{s\ 2}$ )	3.6	kNm/m	Surcharge ( $M_{s\ 2}$ )	3.6	kNm/m
Additional horizontal load ( $M_{h\ 2}$ )	0.0	kNm/m	Additional horizontal load ( $M_{h\ 2}$ )	0.0	kNm/m
Total overturning moment ( $M_2$ )	52.2	kNm/m	Total overturning moment ( $M_2$ )	52.2	kNm/m
Resistance by stem & vertical DL ( $M_{r\ stem\ 2}$ )	53.2	kNm/m	Resistance by stem & vertical DL ( $M_{r\ stem\ 2}$ )	53.2	kNm/m
Resistance by base ( $M_{r\ base\ 2}$ )	22.7	kNm/m	Resistance by base ( $M_{r\ base\ 2}$ )	22.7	kNm/m
Resistance by surcharge on heel ( $M_{r\ s\ heel\ 2}$ )	0.0	kNm/m	Resistance by surcharge on heel ( $M_{r\ s\ heel\ 2}$ )	0.0	kNm/m
Total resistance moment ( $M_{res\ 2}$ )	75.9	kNm/m	Total resistance moment ( $M_{res\ 2}$ )	75.9	kNm/m
Ratio of resistance against overturning = $M_{res\ 2} / M_2$	1.5		Ratio of resistance against overturning = $M_{res\ 2} / M_2$	1.5	
1.5 <= 1.5	OK		1.5 <= 1.5	OK	
<b>Bearing pressure in SLS</b>			<b>Bearing pressure in SLS</b>		
Total vertical load on base ( $N_{SLS\ base\ 2}$ )	51.3	kN/m	Total vertical load on base ( $N_{SLS\ base\ 2}$ )	51.3	kN/m

				Page:	15	Job Ref:	MDM406
Distance to reaction ( $X_{SLS\ 2}$ )	0.46	m		Distance to reaction ( $X_{SLS\ 2}$ )	0.46	m	
Eccentricity of vertical load in SLS ( $e_{SLS\ 2}$ )	0.56	m		Eccentricity of vertical load in SLS ( $e_{SLS\ 2}$ )	0.56	m	
$I_{base} / 6 = 0.34 < 0.56$	Load resultant lies outside middle third			$I_{base} / 6 = 0.34 < 0.56$	Load resultant lies outside middle third		
Pressure under base ( $p_{SLS}$ ) :	73.9	kN/m <sup>2</sup>		Pressure under base ( $p_{SLS}$ ) :	73.9	kN/m <sup>2</sup>	
73.9 <= 200	OK			73.9 <= 200	OK		
<b>Moment for stem in ULS</b>				<b>Moment for stem in ULS</b>			
Soil ( $M_e$ ULS stem 2)	53.5	kNm/m		Soil ( $M_e$ ULS stem 2)	53.5	kNm/m	
Surcharge ( $M_s$ ULS stem 2)	5.0039058	kNm/m		Surcharge ( $M_s$ ULS stem 2)	5.0039058	kNm/m	
Additional horizontal loads ( $M_h$ ULS stem 2)	0.0	kNm/m		Additional horizontal loads ( $M_h$ ULS stem 2)	0.0	kNm/m	
Total moment for stem ( $M_{ULS\ stem\ 2}$ )	58.5	kNm/m		Total moment for stem ( $M_{ULS\ stem\ 2}$ )	58.5	kNm/m	
<b>Moment for base in ULS</b>				<b>Moment for base in ULS</b>			
Total vertical load on base ( $N_{ULS\ base\ 2}$ )	71.8	kN/m		Total vertical load on base ( $N_{ULS\ base\ 2}$ )	71.8	kN/m	
Total moment on base ( $M_{ULS\ base\ 2}$ )	73.8	kNm/m		Total moment on base ( $M_{ULS\ base\ 2}$ )	73.8	kNm/m	
Total resistance moment on base ( $M_{res\ ULS\ base\ 2}$ )	106.3	kNm/m		Total resistance moment on base ( $M_{res\ ULS\ base\ 2}$ )	106.3	kNm/m	
Distance to reaction ( $X_{ULS\ 2}$ )	0.45	m		Distance to reaction ( $X_{ULS\ 2}$ )	0.45	m	
Eccentricity of vertical load in ULS ( $e_{ULS\ 2}$ )	0.57	m		Eccentricity of vertical load in ULS ( $e_{ULS\ 2}$ )	0.57	m	
$I_{base} / 6 = 0.34 < 0.57$	Load resultant lies outside middle third			$I_{base} / 6 = 0.34 < 0.57$	Load resultant lies outside middle third		
Maximum pressure under base ( $p_{max\ ULS\ base\ 2}$ )	105.8	kN/m <sup>2</sup>		Maximum pressure under base ( $p_{max\ ULS\ base\ 2}$ )	105.8	kN/m <sup>2</sup>	
Minimum pressure under base ( $p_{min\ ULS\ base\ 2}$ )	0.0	kN/m <sup>2</sup>		Minimum pressure under base ( $p_{min\ ULS\ base\ 2}$ )	0.0	kN/m <sup>2</sup>	
Bearing length of base ( $L_p$ base 2)	1.36	m		Bearing length of base ( $L_p$ base 2)	1.36	m	
Bearing length of heel ( $L_p$ heel 2)	-0.69	m		Bearing length of heel ( $L_p$ heel 2)	-0.69	m	
Pressure under heel/stem interface ( $p_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>		Pressure under heel/stem interface ( $p_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>	
Pressure under toe/stem interface ( $p_{ULS\ toe\ 2}$ )	-18.9	kN/m <sup>2</sup>		Pressure under toe/stem interface ( $p_{ULS\ toe\ 2}$ )	-18.9	kN/m <sup>2</sup>	
Total vertical load on heel ( $N_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>		Total vertical load on heel ( $N_{ULS\ heel\ 2}$ )	0.0	kN/m <sup>2</sup>	
Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 2}$ )	0.0	kNm/m		Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 2}$ )	0.0	kNm/m	
Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 2}$ )	0.0	kNm/m		Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 2}$ )	0.0	kNm/m	
Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 2}$ )	0.0	kNm/m		Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 2}$ )	0.0	kNm/m	
Moment for toe at wall centre ( $M_{ULS\ toe\ 2}$ )	73.1	kNm/m		Moment for toe at wall centre ( $M_{ULS\ toe\ 2}$ )	73.1	kNm/m	
Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 2}$ )	73.1	kNm/m		Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 2}$ )	73.1	kNm/m	

CASE 3: AFTER CONSTRUCTION ANALYSIS					
(Consider using all loads but no check for stability against sliding is required)					
Left hand side wall		Right hand side wall			
<b>Stability for overturning</b>		<b>Stability for overturning</b>			
Surcharge ( $M_{s\ 3}$ )	3.6	kNm/m	Surcharge ( $M_{s\ 3}$ )	3.6	kNm/m
Additional horizontal load ( $M_{h\ 3}$ )	0.0	kNm/m	Additional horizontal load ( $M_{h\ 3}$ )	0.0	kNm/m
Moist backfill above water table ( $M_{mbaw\ 3}$ )	14.7	kNm/m	Moist backfill above water table ( $M_{mbaw\ 3}$ )	14.7	kNm/m
Moist backfill below water table ( $M_{mbbw\ 3}$ )	21.4	kNm/m	Moist backfill below water table ( $M_{mbbw\ 3}$ )	21.4	kNm/m
Saturated backfill ( $M_{sb\ 3}$ )	-6.4	kNm/m	Saturated backfill ( $M_{sb\ 3}$ )	-6.4	kNm/m
Water ( $M_w\ 3$ )	13.1	kNm/m	Water ( $M_w\ 3$ )	13.1	kNm/m
Total overturning moment ( $M_3$ )	46.4	kNm/m	Total overturning moment ( $M_3$ )	46.4	kNm/m
Resistance by stem & vertical loads ( $M_{r\ stem\ 3}$ )	88.8	kNm/m	Resistance by stem & vertical loads ( $M_{r\ stem\ 3}$ )	85.0	kNm/m
Resistance by base ( $M_{r\ base\ 3}$ )	22.7	kNm/m	Resistance by base ( $M_{r\ base\ 3}$ )	22.7	kNm/m
Resistance by loads on toe ( $M_{r\ toe\ 3}$ )	0.0	kNm/m	Resistance by loads on toe ( $M_{r\ toe\ 3}$ )	0.0	kNm/m
Resistance by surcharge on heel ( $M_{r\ s\ heel\ 3}$ )	0.0	kNm/m	Resistance by surcharge on heel ( $M_{r\ s\ heel\ 3}$ )	0.0	kNm/m
Resistance by moist backfill ( $M_{r\ mb\ 3}$ )	0.0	kNm/m	Resistance by moist backfill ( $M_{r\ mb\ 3}$ )	0.0	kNm/m
Resistance by saturated backfill ( $M_{r\ sb\ 3}$ )	0.0	kNm/m	Resistance by saturated backfill ( $M_{r\ sb\ 3}$ )	0.0	kNm/m
Total resistance moment ( $M_{res\ 3}$ )	111.5	kNm/m	Total resistance moment ( $M_{res\ 3}$ )	107.7	kNm/m

				Page:	16	Job Ref:	MDM406
Ratio of resistance against overturning = $M_{res\ 3} / M_3$				Ratio of resistance against overturning = $M_{res\ 3} / M_3$			
2.4	$\geq$	1.5	OK	2.3	$\geq$	1.5	OK
<b>Bearing pressure in SLS</b>							
Total vertical load on base ( $N_{SLS\ base\ 3}$ )		70.8	kN/m	Total vertical load on base ( $N_{SLS\ base\ 3}$ )		68.7	kN/m
Distance to reaction ( $X_{SLS\ 3}$ )		0.92	m	Distance to reaction ( $X_{SLS\ 3}$ )		0.89	m
Eccentricity of vertical load in SLS ( $e_{SLS\ 3}$ )		0.11	m	Eccentricity of vertical load in SLS ( $e_{SLS\ 3}$ )		0.13	m
$I_{base} / 6 = 0.34 \geq 0.11$		Load resultant lies inside middle third		$I_{base} / 6 = 0.34 \geq 0.13$		Load resultant lies inside middle third	
Pressure under base ( $p_{SLS}$ ):		45.2	kN/m <sup>2</sup>	Pressure under base ( $p_{SLS}$ ):		46.6	kN/m <sup>2</sup>
45.2 $\leq$ 200	OK			46.6 $\leq$ 200	OK		
<b>Moment for stem in ULS</b>							
Surcharge ( $M_s\ ULS\ stem\ 3$ )		5.0039058	kNm/m	Surcharge ( $M_s\ ULS\ stem\ 3$ )		5.0039058	kNm/m
Additional horizontal loads ( $M_h\ ULS\ stem\ 3$ )		0.0	kNm/m	Additional horizontal loads ( $M_h\ ULS\ stem\ 3$ )		0	kNm/m
Moist backfill above water table ( $M_{mbaw}\ ULS\ stem\ 3$ )		18.6	kNm/m	Moist backfill above water table ( $M_{mbaw}\ ULS\ stem\ 3$ )		18.6	kNm/m
Moist backfill below water table ( $M_{mbbw}\ ULS\ stem\ 3$ )		18.0	kNm/m	Moist backfill below water table ( $M_{mbbw}\ ULS\ stem\ 3$ )		18.0	kNm/m
Saturated backfill ( $M_{sb}\ ULS\ stem\ 3$ )		-4.2	kNm/m	Saturated backfill ( $M_{sb}\ ULS\ stem\ 3$ )		-4.2	kNm/m
Water ( $M_w\ ULS\ stem\ 3$ )		8.5	kNm/m	Water ( $M_w\ ULS\ stem\ 3$ )		8.5	kNm/m
Total moment for stem ( $M_{ULS\ stem\ 3}$ )		46.0	kNm/m	Total moment for stem ( $M_{ULS\ stem\ 3}$ )		46.0	kNm/m
<b>Moment for base in ULS</b>							
Total vertical load on base ( $N_{ULS\ base\ 3}$ )		100.1	kN/m	Total vertical load on base ( $N_{ULS\ base\ 3}$ )		96.9	kN/m
Total moment on base ( $M_{ULS\ base\ 3}$ )		65.7	kNm/m	Total moment on base ( $M_{ULS\ base\ 3}$ )		65.7	kNm/m
Total resistance moment on base ( $M_{res\ ULS\ base\ 3}$ )		157.9	kNm/m	Total resistance moment on base ( $M_{res\ ULS\ base\ 3}$ )		152.0	kNm/m
Distance to reaction ( $X_{ULS\ 3}$ )		0.92	m	Distance to reaction ( $X_{ULS\ 3}$ )		0.89	m
Eccentricity of vertical load in ULS ( $e_{ULS\ 3}$ )		0.10	m	Eccentricity of vertical load in ULS ( $e_{ULS\ 3}$ )		0.13	
$I_{base} / 6 = 0.34 < 0.92$		Load resultant lies outside middle third		$I_{base} / 6 = 0.34 < 0.89$		Load resultant lies outside middle third	
Maximum pressure under base ( $p_{max\ ULS\ base\ 3}$ )		72.5	kN/m <sup>2</sup>	Maximum pressure under base ( $p_{max\ ULS\ base\ 3}$ )		72.5	kN/m <sup>2</sup>
Minimum pressure under base ( $p_{min\ ULS\ base\ 3}$ )		0.0	kN/m <sup>2</sup>	Minimum pressure under base ( $p_{min\ ULS\ base\ 3}$ )		0.0	kN/m <sup>2</sup>
Bearing length of base ( $L_p\ base\ 3$ )		2.05	m	Bearing length of base ( $L_p\ base\ 3$ )		2.05	m
Bearing length of heel ( $L_p\ heel\ 3$ )		0.00	m	Bearing length of heel ( $L_p\ heel\ 3$ )		0.00	m
Pressure under heel/stem interface ( $p_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>	Pressure under heel/stem interface ( $p_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>
Pressure under toe/stem interface ( $p_{ULS\ toe\ 3}$ )		15.9	kN/m <sup>2</sup>	Pressure under toe/stem interface ( $p_{ULS\ toe\ 3}$ )		15.9	kN/m <sup>2</sup>
Total vertical load on heel ( $N_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>	Total vertical load on heel ( $N_{ULS\ heel\ 3}$ )		0.0	kN/m <sup>2</sup>
Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 3}$ )		0.0	kNm/m	Clockwise moment for heel at wall centre ( $M_{ULS\ heel\ pos\ 3}$ )		0.0	kNm/m
Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 3}$ )		0.0	kNm/m	Anticlock moment for heel at wall centre ( $M_{ULS\ heel\ neg\ 3}$ )		0.0	kNm/m
Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 3}$ )		0.0	kNm/m	Net moment for heel at wall centre ( $M_{ULS\ heel\ net\ 3}$ )		0.0	kNm/m
Moment for toe at wall centre ( $M_{ULS\ toe\ 3}$ )		59.7	kNm/m	Moment for toe at wall centre ( $M_{ULS\ toe\ 3}$ )		59.8	kNm/m
Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 3}$ )		59.7	kNm/m	Max net moment for base at face of wall ( $M_{ULS\ base\ net\ 3}$ )		59.8	kNm/m

### DESIGN OF STEMS

Left hand side stem		Right hand side stem	
Cover for reinforcement ( $c_w$ ):	75 mm	Cover for reinforcement ( $c_w$ ):	75 mm
Tension bars ( $\phi_{t w}$ ):	3 No. Layers Mesh A393	Tension bars ( $\phi_{t w}$ ):	10 mm
C/C spacing for tension reinforcement ( $S_{t\ wall}$ ):	200 mm	C/C spacing for tension reinforcement ( $S_{t\ wall}$ ):	200 mm
Distribution bars ( $\phi_{d w}$ ):	3 No. Layers Mesh A393	Distribution bars ( $\phi_{d w}$ ):	10 mm
C/C spacing for distribution reinforcement ( $S_{d\ wall}$ ):	200 mm	C/C spacing for distribution reinforcement ( $S_{d\ wall}$ ):	200 mm
Design moment ( $M_{wall}$ ) = Max ( $M_{ULS\ stem\ 2}, M_{ULS\ stem\ 3}$ )	58.5 kNm/m	Design moment ( $M_{wall}$ ) = Max ( $M_{ULS\ stem\ 2}, M_{ULS\ stem\ 3}$ )	58.5 kNm/m
Depth for tension reinforcement ( $d_{wall}$ )	350.0 mm	Depth for tension reinforcement ( $d_{wall}$ )	350.0 mm

$K_{wall} = M_{wall} / (f_{cu} * 1000 * d_{wall}^2)$	0.012	
0.012 <= 0.156	then only tension reinforcement is required.	
Lever arm ( $Z_{wall}$ )	332.5	mm
Required tension reinforcement ( $A_{st \text{ req wall}}$ )	404	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ wall}}$ ) = Max ( $A_{st \text{ req wall}}, A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro wall}}$ )	1178	mm <sup>2</sup> /m
1178 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis wall}}$ ) = $A_{st \text{ min wall}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis wall}}$ )	1178	mm <sup>2</sup> /m
1178 >= 585 OK		
Total horizontal force to wall in ULS ( $F_{ULS \text{ wall}}$ )	49.4	kN/m
Applied shear stress to wall ( $v_{ULS \text{ wall}}$ )	0.14	N/mm <sup>2</sup>
0.14 <= 5.0 OK		
$A_{st \text{ pro in wall}} / (d_{wall} * 10)$	0.34	
Design concrete shear stress $v_c$ wall from Table 3.8 – BS 8110:	0.57	N/mm <sup>2</sup>
0.57 >= 0.14 No shear reinforcement required.		
Design service stress ( $f_s$ wall)	165.5	N/mm <sup>2</sup>
Modification factor for tension	2.0	
Permissible span to depth ration	14.0	
Actual span to depth ration = $h_{stem} / d_{wall}$	7.7	
14.0 >= 7.7 OK		

$K_{wall} = M_{wall} / (f_{cu} * 1000 * d_{wall}^2)$	0.012	
0.012 <= 0.156	then only tension reinforcement is required.	
Lever arm ( $Z_{wall}$ )	332.5	mm
Required tension reinforcement ( $A_{st \text{ req wall}}$ )	404	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ wall}}$ ) = Max ( $A_{st \text{ req wall}}, A_{st \text{ min wall}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro in wall}}$ )	1178	mm <sup>2</sup> /m
1178 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis wall}}$ ) = $A_{st \text{ min wall}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis wall}}$ )	1178	mm <sup>2</sup> /m
1178 >= 585 OK		
Total horizontal force to wall in ULS ( $F_{ULS \text{ wall}}$ )	49.4	kN/m
Applied shear stress to wall ( $v_{ULS \text{ wall}}$ )	0.14	N/mm <sup>2</sup>
0.14 <= 5.0 OK		
$A_{st \text{ pro in wall}} / (d_{wall} * 10)$	0.34	
Design concrete shear stress $v_c$ wall from Table 3.8 – BS 8110:	0.57	N/mm <sup>2</sup>
0.57 >= 0.14 No shear reinforcement required.		
Design service stress ( $f_s$ wall)	165.5	N/mm <sup>2</sup>
Modification factor for tension	2.0	
Permissible span to depth ration	14.0	
Actual span to depth ration = $h_{stem} / d_{wall}$	7.7	
14.0 >= 7.7 OK		

## DESIGN OF BASES

Left hand side base	Right hand side base	
Cover for reinforcement ( $c_b$ ) :	<b>75</b>	mm
Tension bars ( $\phi_t b$ ) :	4 No. Layers Mesh A393	<b>10</b> mm
C/C spacing for tension reinforcement ( $S_t$ base) :	<b>200</b>	mm
Distribution bars ( $\phi_d b$ ) :	4 No. Layers Mesh A393	<b>10</b> mm
C/C spacing for distribution reinforcement ( $S_d$ base) :	<b>200</b>	mm
Moment for base ( $M_{ULS \text{ base net}}$ ) = Max ( $M_{ULS \text{ base net 2}}, M_{ULS \text{ base net 3}}$ )		
73.1 kNm/m		
Depth for tension reinforcement in base ( $d_{base}$ )	340.0	mm
$K_{base} = M_{ULS \text{ base net}} / (f_{cu} * 1000 * d_{base}^2)$	0.016	
0.016 <= 0.156 then only tension reinforcement is required.		
Lever arm ( $Z_{base}$ )	323.0	mm
Required tension reinforcement ( $A_{st \text{ req base}}$ )	520	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ base}}$ ) = Max( $A_{st \text{ req base}}, A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro base}}$ )	1571	mm <sup>2</sup> /m
1571 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis base}}$ ) = $A_{st \text{ min base}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis base}}$ )	1571	mm <sup>2</sup> /m
1571 >= 585 OK		
Shear for heel at face of wall ( $V_{ULS \text{ heel}}$ )	0.0	kN/m
Shear for toe at face of wall ( $V_{ULS \text{ toe}}$ )	75.9	kN/m
Applied shear stress to base ( $v_{ULS \text{ base}}$ )	0.22	N/mm <sup>2</sup>
0.22 <= 5.0 OK		
$A_{st \text{ pro base}} / (d_{base} * 10)$	0.46	
Moment for base ( $M_{ULS \text{ base net}}$ ) = Max ( $M_{ULS \text{ base net 2}}, M_{ULS \text{ base net 3}}$ )		
73.1 kNm/m		
Depth for tension reinforcement in base ( $d_{base}$ )	340.0	mm
$K_{base} = M_{ULS \text{ base net}} / (f_{cu} * 1000 * d_{base}^2)$	0.016	
0.016 <= 0.156 then only tension reinforcement is required.		
Lever arm ( $Z_{base}$ )	323.0	mm
Required tension reinforcement ( $A_{st \text{ req base}}$ )	520	mm <sup>2</sup> /m
Minimum required tension reinforcement ( $A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Tension reinforcement ( $A_{st \text{ base}}$ ) = Max( $A_{st \text{ req base}}, A_{st \text{ min base}}$ )	585	mm <sup>2</sup> /m
Provided tension reinforcement ( $A_{st \text{ pro base}}$ )	1571	mm <sup>2</sup> /m
1571 > 585 OK		
Minimum required distribution reinforcement ( $A_{s \text{ min dis base}}$ ) = $A_{st \text{ min base}}$		
Provided distribution reinforcement ( $A_{s \text{ pro dis base}}$ )	1571	mm <sup>2</sup> /m
1571 >= 585 OK		
Shear for heel at face of wall ( $V_{ULS \text{ heel}}$ )	0.0	kN/m
Shear for toe at face of wall ( $V_{ULS \text{ toe}}$ )	72.7	kN/m
Applied shear stress to base ( $v_{ULS \text{ base}}$ )	0.21	N/mm <sup>2</sup>
0.21 <= 5.0 OK		
$A_{st \text{ pro base}} / (d_{base} * 10)$	0.46	

		Page: 18 Job Ref: MDM406
Design concrete shear stress $v_{c\ base}$ from Table 3.8 – BS 8110: 0.50 $\geq$ 0.22      No shear reinforcement required	0.50      N/mm <sup>2</sup>	Design concrete shear stress $v_{c\ base}$ from Table 3.8 – BS 8110:      0.61      N/mm <sup>2</sup> 0.61 $\geq$ 0.21      No shear reinforcement required
Tension reinforcement for each face of stem:	3 No. Layers Mesh A393	Reinforcement for each face of stem:
Tension reinforcement in top & bottom of base:	4 No. Layers Mesh A393	Reinforcement in top & bottom of base:
Provide T10 @ 200 mm U-bars for top of stem		Provide T10 @ 200 mm U-bars for top of stem