

## **Bearing Pressure Report**



Site 3 Honeybourne Road

London NW6 1HH

Client Imogen Strachan

Date February 2016

Our Ref | BPR/5678A



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- Borehole Record Sheets (BH1 & BH2)
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- Laboratory Test Results
- Sketch Fieldwork Location Plans



#### **EXECUTIVE SUMMARY**

Item	Comments
Site	3 Honeybourne Road, London NW6 1HH
Ground Conditions	The current work encountered Made Ground to a maximum depth of 1.08m below existing ground level. This in turn was found to be underlain by the London Clay which was not penetrated at the maximum borehole termination depth of 8.00m.
Groundwater Roots	Groundwater was not encountered at the time of the investigation.  Roots of live and dead appearance to 2mm in diameter were noted within BH1, BH2, TP2 and TP3 down to a maximum depth of 1.90m. Hair and Fibrous roots were observed in BH1 to a maximum depth of 2.30m below ground level.
Bearing Pressure	It is assumed that the proposed extension foundations will be set at a depth between 1.00m and 2.00m below existing ground level. At this depth the extension foundations should be set within the firm to stiff London Clay Formation. Based on in-situ and laboratory testing in conjunction with empirical correlations (Bjerrum, 1972) the clay at a depth of 1.00m below existing ground level is estimated to have an undrained shear strength (cu) of around 66 kPa which rises to 83 kPa at a depth of 2.00m. Based on the estimated shear strength, the maximum bearing capacity of the London Clay at 1.00m is 340 kPa which rises to 425 kPa at 2.00m. Applying a global factor of safety of 3 it is recommended that an allowable bearing pressure not exceeding 113 kPa is applied for foundations set at a depth of 1.00m and 142 kPa at a depth of 2.00m, at which settlements are expected to be within normal acceptable tolerances.  It is assumed that the potential basement will be set at a depth of 3.50m below existing
	ground level. At this depth the basement would be set within the stiff London Clay Formation. Based on in-situ and laboratory testing in conjunction with empirical correlation (Bjerrum, 1972) the clay at a depth of 3.50m below existing ground level is estimated to have an undrained shear strength (cu) of around 90 kPa. Based on the estimated shear strength, the maximum bearing capacity of the London Clay at 3.50m is 460 kPa. Applying a global factor of safety of 3 it is recommended that an allowable bearing pressure not exceeding 153 kPa is applied for a basement set at a depth of 3.50m, at which settlements are expected to be within normal acceptable tolerances.
Buried Concrete	Chemical testing has been carried out to determine the nature of the soils in the context of the durability of buried concrete. Based on the available test data the soluble sulphate content of the soils is noted to show little variation and ranges between 0.95 and 2.01 g/l (measured as soluble SO4) but with a pH of 7.7 to 8.1. Taking the worst case data, the soils are classified as DS-3 in accordance with BRE guidance (Ref. 3) with a corresponding ACEC class of AC-3.
Swelling and Shrinking	The London Clay Formation has been confirmed to possess 'high' volume change potential in accordance with the National House Building Councils (NHBC) classification system given in Part 4 of their Standards (Ref 4).
Recommendations for Further Work	Prior to or as part of the final design stage it is recommended that a full Ground Movement Analysis for the project be undertaken in order to assess the impact of the proposed basement on the adjacent properties during both temporary and permanent works, together with recommending in detail on heave protection measures related to anticipated stress changes.
	A Basement Impact Assessment (BIA) should also be considered if the proposed basement plans are confirmed. A BIA should be used to fully understand the hydrogeological regime at the site and the impact that basement construction may have. Any planning requirements of Camden Council will need to be followed regarding basement construction.



#### 1.0 INTRODUCTION & SCOPE OF WORKS

- 1.1 This report has been prepared by Chelmer Site Investigation Laboratories Limited (CSI) to the instructions of INGealtoir Consulting Structural Engineers on behalf of the client, Imogen Strachan
- 1.2 This intrusive investigation has been commissioned to provide information on the subsoil conditions of the site which included the depth and condition of the property foundations as well as to identify the geological strata on which the building has been founded on and to provide a bearing capacities for the strata encountered.
- 1.3 The site under consideration belongs to a three storey terraced house with an extension extending into the rear garden. The site address is 3 Honeyburne Road, London NW6 1HH and is located at the approximate Ordnance Survey grid reference 525561E 185080N.
- 1.4 It is understood that this investigation will aid with the development of a single storey extension to the rear of the property and the possible extension of the existing cellar to form a new single-storey basement below the footprint of the existing dwelling.
- 1.5 A Desk Top Study was not requested by the client.
- 1.6 This report presents a summary of the site investigation work carried out and discusses the findings.



#### 2.0 SUMMARY OF FIELDWORK EXECUTED

- 2.1 All fieldwork was generally executed in accordance with applicable British Standard and accepted industry good practice (Ref 1).
- 2.2 The borehole and trial pit locations were chosen by the Structural Engineer and are indicated on the appended *Sketch Fieldwork Location Plan*.
- 2.3 Fieldwork was undertaken on the 11<sup>th</sup> and 19<sup>th</sup> August 2015 and comprised the following elements:

#### Hand Excavated Trial Pits

- 2.4 The scope of works involved the excavation of four trial pits (TP1-TP4) in order to establish the depth and condition of the current properties foundations and the geological strata on which the house was built on. The locations of the trial pits are indicated on the Sketch Fieldwork Location Plans (Sheet 1 and Sheet 2).
- 2.5 TP1 was excavated to a depth of 1275mm and found that the building brickwork was resting on a 75mm brick corbel which in turn was sitting on natural London Clay strata at a depth of 1.07m.
- 2.6 TP2 was terminated at a depth of 450mm as a result of contact with a drainage run.
- 2.7 TP3 was excavated between the kitchen bay and the main building extending into the rear garden (see TP3 section A & B). The trial pit found that the main building brickwork was constructed upon two 75mm brick corbel foundations which in turn was built upon Made Ground at a depth of 0.80m. The kitchen bay brickwork was resting on three 75mm brick corbels which in turn was resting on Made Ground at a depth of 0.875m bgl.
- 2.8 TP4 was excavated against the front elevation to a depth of 725mm and found that the brickwork was resting on a 75mm brick corbel which in turn was resting on a 300mm concrete foundation. The Concrete foundation was sitting on natural London Clay deposits at 0.56m bgl. A hand augered borehole (BH1) was sunk through the base of TP4.
- 2.5 Discrete disturbed samples were taken from the underside of the foundation footings for laboratory testing in each of the trial pits.
- 2.6 Mackintosh and Pilcon Vane Tests were undertaken on the strata encountered below the underside of the foundation footings in order to provide additional information on the consistency and strength of the material.
- 2.7 Full details of the trial pit findings are given on the appended *trial pit record sheets*



#### Hand Augered Borehole

- 2.8 A single hand augered borehole (BH1) was sunk at the site at the position indicated on the *Sketch Fieldwork Location Plan* through the base of TP4. It was originally proposed that a borehole was undertaken on the properties front driveway but the client's car was obstructing drilling on the day of the investigation, as such a hand augered borehole was undertaken. The borehole was advanced to a depth of 3.70m below ground level before it was terminated as a result of the ground becoming too dense to auger.
- 2.9 Discrete disturbed samples were taken from the borehole at regular depth intervals as the borehole was advanced.
- 2.10 Pilcon Vane Tests were undertaken throughout the borehole in order to provide additional information +on the consistency and strength of the material encountered.
- 2.11 Full details of the borehole findings are given on the appended *borehole record* sheets.

#### C.F.A Borehole

- 2.12 A single c.f.a borehole (BH2) was undertaken at the site on the 19<sup>th</sup> August 2015 and was located on the front driveway as indicated on the *Sketch Fieldwork Location Plan*. BH2 was advanced to a depth of 8.00m below existing ground level.
- 2.13 Discrete disturbed samples were taken from the borehole at regular depth intervals as the borehole was advanced.
- 2.14 Pilcon Vane Tests were undertaken throughout the borehole in order to provide additional information on the consistency and strength of the material encountered.
- 2.15 Full details of the borehole findings are given on the appended *borehole record* sheets.



#### 3.0 GEOLOGICAL SETTING

3.1 According to information published by the British Geological Survey (England and Wales, 1:50,000 Sheet E256; North London and BGS online resources) the underlying geology at this site is shown as the London Clay Formation.

#### London Clay

3.2 It is thought that the London Clay formation was deposited during a period of sea inundation in the area up to 200m in depth. The London Clay can be up to 150m thick beneath south Essex thinning across London to about 90m near Reading. The formation consists of mainly dark blue to brown grey clay containing variable amounts of fine-grained sand and silt. London Clay generally weathers to an orange-brown colour with pockets of silty fine sand. The formation is particularly susceptible to swelling and shrinking when subjected to moisture content changes. In addition, gypsum (selenite) crystals and pyrite nodules are commonly found throughout the formation.

London Clay consists mainly of dark bluish grey to brownish grey clay containing variable amounts of fine-grained sand and silt. When exposed to the weathering process its upper regions oxidise to brown in colour. It usually contains selenite crystals, often grouped in bands or layers, which are thought to have originated from the decomposition of shell fragments. London Clay contains clay minerals in the form of illite, kaolinite and smectite. The presence of smectite renders the London Clay particularly susceptible to heave caused by alternate wetting and drying near the surface. In addition, weathering and possible slight transportation of semi-frozen material "en-masse" in glacial or peri-glacial regions can occur. This action often completely destroys the structure of the material and can involve a serious loss of strength. As the materials are based on local constituents, the lithology of the deposit is often similar to that of the parent strata.



#### 4.0 SUMMARY OF GROUND CONDITIONS ENCOUNTERED

4.1 Full details of the ground conditions encountered are presented on the *borehole and trial pit records* appended to this report and can be summarised as follows:

Depth (m bgl)	Depth To (m bgl)	Description
0.00	0.05 - 0.40	TOPSOIL/BLOCK PAVING/CONCRETE
0.05 - 0.40	1.08 +	MADE GROUND: Medium dense, brown, slightly
		gravelly fine to medium sand with numerous brick,
		clinker, bitumen, concrete fragments and pieces
0.20 - 0.30	0.53 - 1.08	MADE GROUND: Medium dense, dark brown,
		gravelly sandy silty clay with numerous brick, concrete
		and clinker fragments
0.40 - 1.08	8.00	Firm to stiff, brown slightly sandy silty CLAY with
		partings of brown and orange silt and fine sand.
		Occasional disseminated selenite crystals (LONDON
		CLAY)

- 4.2 It should be noted that the Made Ground depths recorded above are those encountered within the boreholes and trial pits undertaken during the current work. Owing to the variable nature and unknown provenance of Made Ground it is possible that deeper or more extensive areas of Made Ground may exist at this site which have not been revealed by the current work.
- In-situ testing within the London Clay deposits found beneath the property in TP1 & TP4 and both boreholes indicated that the material was 'firm' becoming 'very stiff' in consistency with depth.
- 4.4 Groundwater was not encountered at the time of the investigation.
- 4.5 Roots of live and dead appearance to 3mm in diameter were noted within TP1. Roots of live and dead appearance to 2mm were noted within BH1, BH2, TP2 and TP3 down to a maximum depth of 1.90m. Hair and Fibrous roots were observed in BH1 to a maximum depth of 2.30m below ground level.



#### 5.0 LABORATORY TESTING

- 5.1 The following geotechnical laboratory testing has been carried out on samples recovered from the boreholes and trial pits undertaken at this site.
- 5.2 Unless otherwise stated, the geotechnical tests have generally been carried out in accordance with applicable British Standard (Ref. 2).
- 5.3 Atterberg Limits and Moisture Content Tests

The Atterberg Limits and moisture content have been determined for three samples from the London Clay formation from BH2.

For the samples tested, the liquid limit (LL) was found to range between 66% and 77%, the plastic limit (PL) was found to range between 23% and 25%, the plasticity index between 42% and 52% and a modified plasticity index from 40% to 49%. The moisture content of these samples was found to range from 27% to 31%.

These results indicate that the samples tested would be classified as Clay of 'high' to 'very high' plasticity (CH–CV) in accordance with the Casagrande Geotechnical classification system.

5.4 BRE Special Digest 1:2005 Concrete Classification Tests

Three samples taken from the site were selected and tested to assess the aggressive chemical environment for concrete (ACEC) within the site. Two samples were taken from the London Clay Formation in BH2 and one sample was taken from the Made Ground in TP3.

The pH value was found to range between 7.7 and 8.1 with the sulphate content, on a 2:1 water:soil extract found to range between 0.95 and 2.01 g/l.



#### 6.0 DISCUSSION

#### SUMMARY OF PROPOSED DEVELOPEMNT

- As discussed in the introduction it is understood that the proposed development will comprise the construction of a single storey extension to the rear of the property and the possible extension of the existing cellar to form a new single-storey basement below the footprint of the existing dwelling.
- Full details of the proposed construction are not yet developed and it is assumed that they will be subject to the findings of this investigation. As a consequence the bearing pressure below is, by necessity, general in nature and is subject to confirmation following the results of this investigation and further design.
- 6.3 Should ground conditions during construction be found to differ significantly from those described in our report Chelmer Site Investigation Laboratories Limited should be contacted immediately and that the below noted allowable bearing pressures may need to be altered accordingly.

#### **BEARING PRESSURE**

- It is assumed that the proposed extension foundations will be set at a depth between 1.00m and 2.00m below existing ground level. At this depth the extension foundations should be set within the firm to stiff London Clay Formation. Based on in-situ and laboratory testing in conjunction with empirical correlations (Bjerrum, 1972) the clay at a depth of 1.00m below existing ground level is estimated to have an undrained shear strength (cu) of around 66 kPa which rises to 83 kPa at a depth of 2.00m. Based on the estimated shear strength, the maximum bearing capacity of the London Clay at 1.00m is 340 kPa which rises to 425 kPa at 2.00m. Applying a global factor of safety of 3 it is recommended that an allowable bearing pressure not exceeding 110 kPa is applied for foundations set at a depth of 1.00m and 140 kPa at a depth of 2.00m, at which settlements are expected to be within normal acceptable tolerances.
- lt is assumed that the potential basement will be set at a depth of 3.50m below existing ground level. At this depth the basement would be set within the stiff London Clay Formation. Based on in-situ and laboratory testing in conjunction with empirical correlation (Bjerrum, 1972) the clay at a depth of 3.50m below existing ground level is estimated to have an undrained shear strength (cu) of around 90 kPa. Based on the estimated shear strength, the maximum bearing capacity of the London Clay at 3.50m is 460 kPa. Applying a global factor of safety of 3 it is recommended that an allowable bearing pressure not exceeding 150 kPa is applied for a basement set at a depth of 3.50m, at which settlements are expected to be within normal acceptable tolerances.



#### **BURIED CONCRETE**

Chemical testing has been carried out to determine the nature of the soils in the context of the durability of buried concrete. Based on the available test data the soluble sulphate content of the soils is noted to show little variation and ranges between 0.95 and 2.01 g/l (measured as soluble SO<sub>4</sub>) but with a pH of 7.7 to 8.1. Taking the worst case data, the soils are classified as DS-3 in accordance with BRE guidance (Ref. 3) with a corresponding ACEC class of AC-2s.

#### **SWELLING AND SHRINKAGE**

6.7 The London Clay Formation has been confirmed to possess 'high' volume change potential in accordance with the National House Building Councils (NHBC) classification system given in Part 4 of their Standards (Ref 4).

#### RECOMMENDATIONS FOR FURTHER WORK

- 6.8 Prior to or as part of the final design stage it is recommended that a full Ground Movement Analysis for the project be undertaken in order to assess the impact of the proposed basement on the adjacent properties during both temporary and permanent works, together with recommending in detail on heave protection measures related to anticipated stress changes.
- A Basement Impact Assessment (BIA) should also be considered if the proposed basement plans are confirmed. A BIA should be used to fully understand the hydrogeological regime at the site and the impact that basement construction may have. Any planning requirements of Camden Council will need to be followed regarding basement construction.



**Prepared By:** 

Matthew Fisher BSc (Hons)

Engineering Geologist

Reviewed By:

Matthew Proctor BEng (Hons), FGS

**Executive Director** 

#### References

- 1. BS 5930:1999+A2:2010 (2010) Code of practice for site investigations.
- 2. BS 1377:1990 (1990) Methods of Test for Soils for Civil Engineering Purposes.
- 3. BRE (2005). Concrete in aggressive ground. Special Digest 1.
- 4. NHBC (2011) NHBC Standards, Chapter 4.2, Building Near Trees.



- a) This report has been prepared for the purpose of providing advice to the client pursuant to its appointment of Chelmer Site Investigation Laboratories Limited (CSI) to act as a consultant.
- b) Save for the client no duty is undertaken or warranty or representation made to any party in respect of the opinions, advice, recommendations or conclusions herein set out.
- c) All work carried out in preparing this report has used, and is based upon, our professional knowledge and understanding of the current relevant English and European Community standards, approved codes of practice, technology and legislation.
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- q) In addition CSI will not be liable for any loss whatsoever arising directly or indirectly from any opinion within this report.



Client:	James Strachlan	Scale:	N.T.S.	Sheet No	: 1 of 1	Wea	ther: Overcast	Date: 11	1.08.15
Site:	3 Honeybourne Road, London, NW6 1HH	<b>5678</b>	Borehole No: 1		Borir	ng method: Hand Auger			
Depth Mtrs.	Description of Strata	Thick- ness	Legend	Sample	Tes <sup>s</sup> Type F	t	Root Information	Depth to Water	Depth Mtrs
	SEE TP4 LOG	0.75		D			Roots of live and dead appearance to 2mmØ to 1.9m.		0.5
0.75			×				Hair and fibrous roots to 2.3m.		
	Firm, dark brown, slightly sandy silty CLAY with partings of brown and orange silt and		- × - · · × - · · · · × - · · · · · × - · · · ·	D		L00 L06			1.0
	fine sand and crystals.			D		118 124	No roots observed below 2.3m.		1.5
	Becoming stiff from 1.9m.	2.05		D		130+ 130+			2.0
		2.95		D		130+ 130+			2.5
			×_	D		.18 .24			3.0
2.7				D		130+ 130+			3.5
3.7	Borehole ends at 3.7m. Too dense to hand auger. Thought to be claystone.								
rawn	by: DB <b>Approved by:</b> JH				oo Dense to		Jar Sample		

**Remarks:** Borehole dry and open on completion.

D Small Disturbed Sample
B Bulk Disturbed Sample
U Undisturbed Sample (U100)
M Mackintosh Probe

W Water Sample N Standard Penetration Test Blow Count



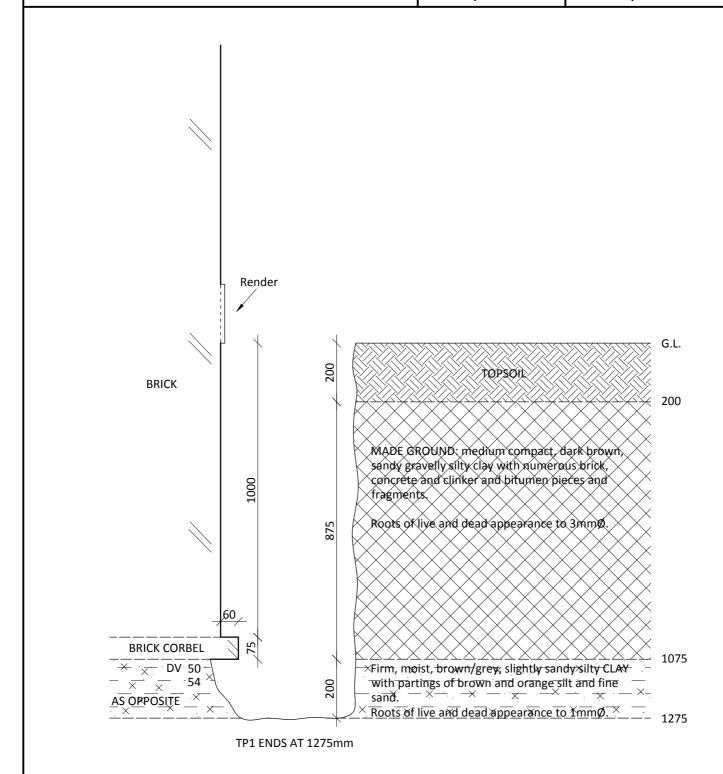
Client:	James Strachlan	Scale:	cale: N.T.S. Sheet No: 1 of 1 Weather: Overcast				ther: Overcast	Date: 19.08.1					
Site:	3 Honeybourne Road, London, NW6 1HH		Job No: 5678		No: 2	Borin	g method: CFA 100mm	Ø Secondi	man				
Depth Mtrs.	Description of Strata	Thick- ness	Legend	Sample	Tes Type	st	Root Information	Depth to Water	Depth Mtrs				
G.L.	BRICK PAVING SLABS	0.01											
0.01	SAND	0.39											
0.4	Firm, brown slightly sandy silty CLAY with partings of brown and orange silt and fine		× -	D			Roots of live and dead		0.5				
	sand.		- ×- ·-	D		62 64	appearance to 1mmØ to 0.6m.		1.0				
				D			No roots observed		1.5				
			- ×	D		70 72	below 0.6m.		2.0				
			- × -	D					2.5				
		7.6	.— ·— ·	D		78 80			3.0				
3.0	Becoming stiff from 3.0m.			D					3.5				
	G .		x-	D		84 84			4.0				
						× × ×	D					4.5	
				D		90 92			5.0				
							×	D					5.5
			- · · · · · · · · · · · · · · · · · · ·	D		102 106			6.0				
	Becoming very stiff from 7.0m.		- ××- - × ×- - × ×- - × ×-	D		120+ 120+			7.0				
8.0	8.0 Borehole ends at 8.0m			D		120+ 120+			8.0				
Drawn b	y: LS Approved by: JH	•			oo Dense t bed Sample		Jar Sample	•	•				

B Bulk Disturbed Sample V Pilcon Vane (kPa)
U Undisturbed Sample (U100) M Mackintosh Probe

W Water Sample N Standard Penetration Test Blow Count



Client: James Strachlan	Scale: N.T.S.	Sheet No: 1 of 1	Date: 11.08.15
Location: 3 Honeybourne Road, London, NW6 1HH	<b>Job No</b> : 5678	Trial Pit No: 1	Weather: Overcast
Excavation Method: Hand tools		Drawn by: DB	Checked by: JH



Remarks:

**D** Small disturbed sample

**B** Bulk disturbed sample

**U** Undisturbed sample (U100)

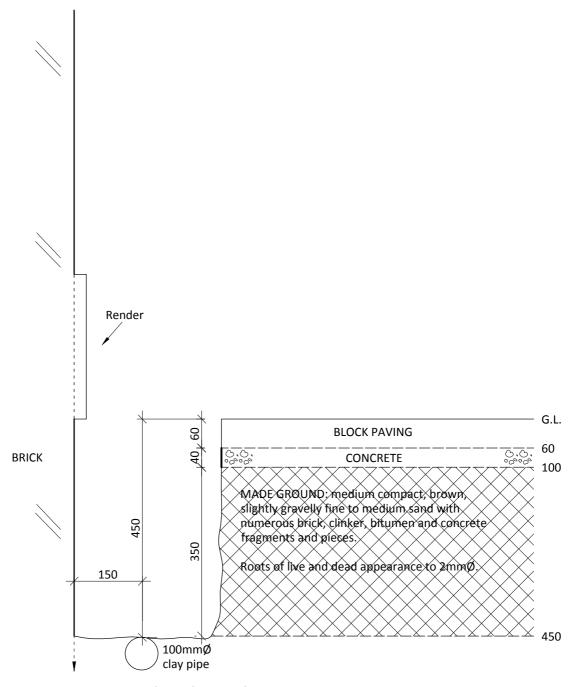
N Standard Penetration Test Blow Count

**J** Jar sample V Pilcon Vane (kPa)

M Mackintosh Probe



Client: James Strachlan	Scale:	N.T.S.	Sheet No:	1 of 1	Date:	11.08.15
Location: 3 Honeybourne Road, London, NW6 1HH	Job No:	5678	Trial Pit No:	2	Weather:	Overcast
Excavation Method: Hand tools			Drawn by:	DB	Checked by:	JH



TP2 ENDS AT 450mm due to drainage obstruction. Unable to establish underside foundation.

Remarks:

Key:

**D** Small disturbed sample

**B** Bulk disturbed sample

**U** Undisturbed sample (U100)

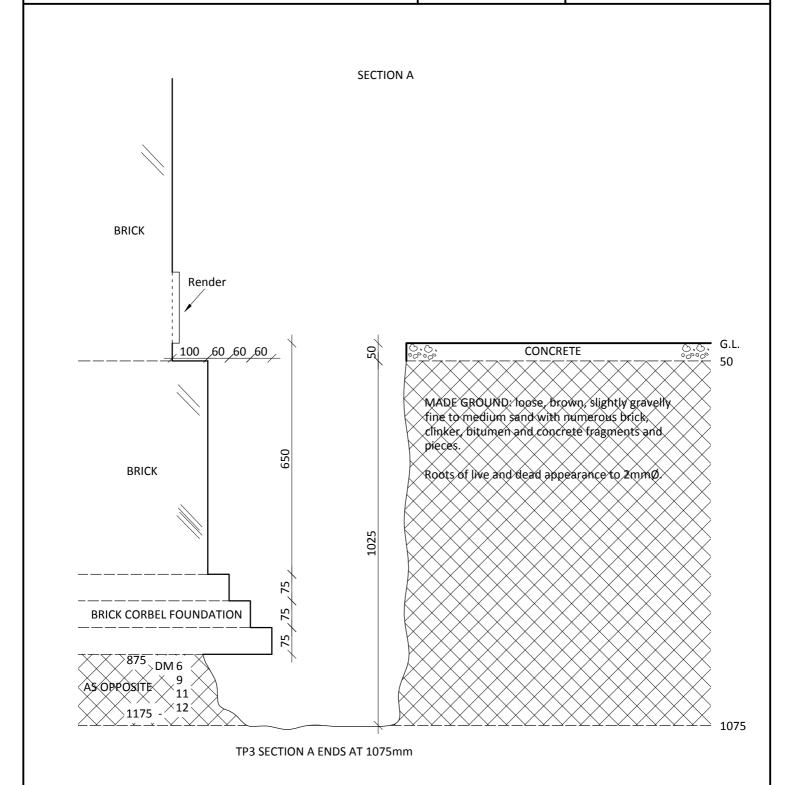
N Standard Penetration Test Blow Count

Jar samplePilcon Vane (kPa)

M Mackintosh Probe



Client: James Strachlan	Scale: N.T.S.	Sheet No: 1 of 2	Date: 11.08.15
Location: 3 Honeybourne Road, London, NW6 1HH	<b>Job No:</b> 5678	Trial Pit No: 3	Weather: Overcast
Excavation Method: Hand tools		Drawn by: DB	Checked by: JH



Remarks:

Key:

**D** Small disturbed sample

**B** Bulk disturbed sample

**U** Undisturbed sample (U100)

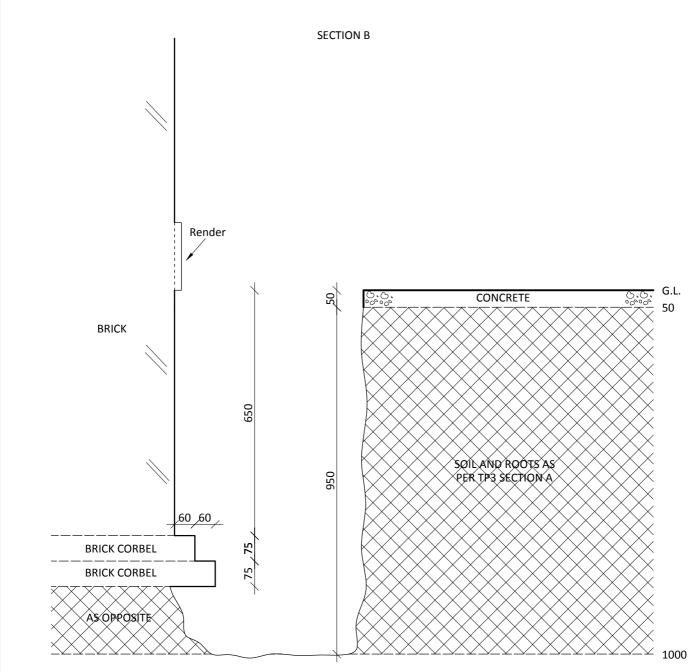
N Standard Penetration Test Blow Count

Jar samplePilcon Vane (kPa)

M Mackintosh Probe



Client: James Strachlan	Scale: N.T.S.	Sheet No: 2 of 2	Date: 11.08.15
Location: 3 Honeybourne Road, London, NW6 1HH	<b>Job No</b> : 5678	Trial Pit No: 3	Weather: Overcast
Excavation Method: Hand tools		Drawn by: DB	Checked by: JH



TP3 SECTION B ENDS AT 1000mm

Remarks:

Key:

**D** Small disturbed sample

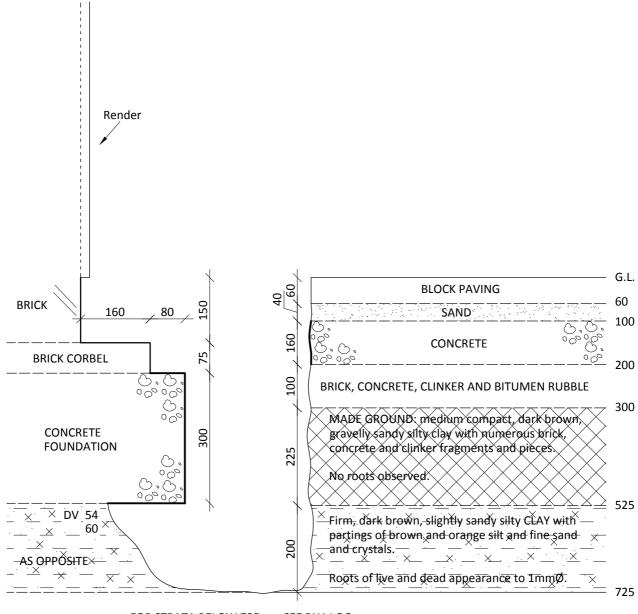
**B** Bulk disturbed sample

U Undisturbed sample (U100)N Standard Penetration Test Blow Count

J Jar sampleV Pilcon Vane (kPa)M Mackintosh ProbeW Water Sample



Client: James Strachlan	Scale: N.T.S.	Sheet No: 1 of 1	Date: 11.08.15
Location: 3 Honeybourne Road, London, NW6 1HH	<b>Job No:</b> 5678	Trial Pit No: 4	Weather: Overcast
Excavation Method: Hand tools		Drawn by: DB	Checked by: JH



FOR STRATA BELOW 725mm SEE BH1 LOG

Remarks:

(ey:

**D** Small disturbed sample

**B** Bulk disturbed sample

**U** Undisturbed sample (U100)

N Standard Penetration Test Blow Count

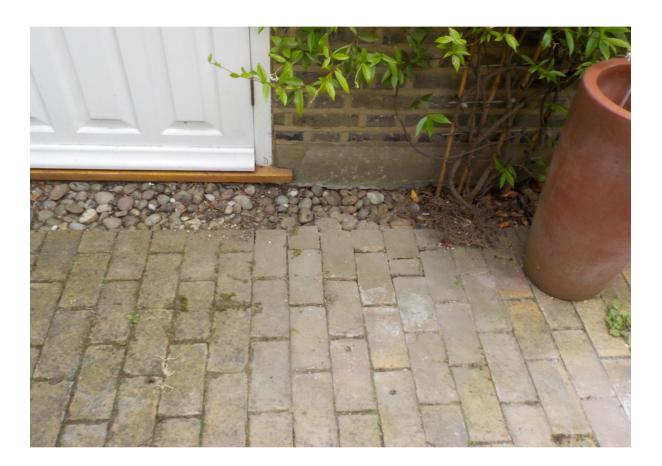
Jar samplePilcon Vane (kPa)

**M** Mackintosh Probe





# **Laboratory Report**



Site 3 Honeybourne Road, NW6

**Client James Strachlan** 

Date 11-Sep-15

Our Ref CSI5678

CGL Ref CGL5678





#### **Content Summary**

This report contains all test results as indicated on the test instruction/summary.

CGL Reference : CGL5678

Client Reference: CSI5678

For the attention of : James Strachlan

This report comprises of the following: 1 Cover Page

1 Inside Cover/Contents Page

1 Page of Results

1 Moisture/Shear Strength Chart

1 Plasticity Chart

4 Pages of BRE SD1 Results

1 Limitations of Report

#### Notes :

#### General

Please refer to report summary notes for details pertaining to methods undertaken and their subsequent accreditations

Samples were supplied by Chelmer Site Investigations

All tests performed in-house unless otherwise stated

#### **Deviant Samples**

Samples were received in suitable containers

Yes

A date and time of sampling was provided Yes

Arrived damaged and/or denatured No

#### Laboratory Testing Results



Job Number: CGL5678 Client: James Strachlan

Client Reference : CSI5678

Site Name: 3 Honeybourne Road, NW6

Date Received: 08/09/2015 Date Testing Started: 09/09/2015 Date Testing Completed: 11/09/2015

Laboratory Used: Chelmer Geotechnical, CM3 8AB

	Sample Ref	f		*Moisture Content	*Soil Faction	*Liquid Limit	*Plastic Limit	*Plasticity Index	*Liquidity Index	*Modified Plasticity	*Soil Class	Filter Paper	*Soil Sample	Insitu Shear Vane	Organic Content	*pH Value		ate Conter	nt (g/l)
BH/TP/WS	Depth (m)	UID	Sample Type	(%) [ 1 ]	> 0.425mm (%) [ 2 ]	(%) [ 3 ]	(%) [ 4 ]	(%) [ 5 ]	(%) [ 5 ]	Index (%) [ 6 ]	[7]	Contact Time (h) [ 8 ]	Suction (kPa)	Strength (kPa) [ 9 ]	(%) [ 10 ]	[11]	SO <sub>3</sub> [12]	SO <sub>4</sub> [13]	Class [ 14 ]
BH2	2.0	65783	D	27	<5	69	23	46	0.09	43	СН			71					
BH2	3.0	65784	D		<5									74					
BH2	4.0	65785	D	31	<5	66	24	42	0.16	40	СН			84					
BH2	8.0	65786	D	29	<5	77	25	52	0.07	49	CV			120					

Notes :- \*UKAS Accredited Tests

[1] BS 1377 : Part 2 : 1990, Test No 3.2

[7] BS 5930 : 1981 : Figure 31 - Plasticity Chart for the classification of fine soils

[2] Estimated if <5%, otherwise measured

[8] In-house method S9a adapted from BRE IP 4/93

[3] BS 1377 : Part 2 : 1990, Test No 4.4

[9] Values of shear strength were determined in situ by Chelmer Site Investigations using a Pilcon hand vane or Geonor vane (GV).

[4] BS 1377 : Part 2 : 1990, Test No 5.3

[5] BS 1377 : Part 2 : 1990, Test No 5.4

[6] BRE Digest 240 : 1993

[10] BS 1377 : Part 3 : 1990, Test No 4 [11] BS 1377 : Part 2 : 1990, Test No 9 [12] BS 1377 : Part 3 : 1990, Test No 5.6

[13]  $SO_4 = 1.2 \times SO_3$ 

[14] BRE Special Digest One (Concrete in Aggressive Ground) 2005

Note that if the SO<sub>4</sub> content falls into the DS-4 or DS-5 class, it would be prudent to consider the sample as falling into the DS-4m or DS-5m class respectively unless water soluble magnesium testing is undertaken to prove otherwise

- Disturbed sample
- Bulk sample
- U100 (undisturbed sample)
- Water sample

ENP - Essentially Non-Plastic

UKAS TESTING

U/S - Underside Foundation

Comments :-

Date Checked :- 11-Sep-15 Checked By :- MC Technician :- HS

Q170 Chelmer Site Investigations 2014

### Laboratory Testing Results

Moisture Content/Shear Strength Profile

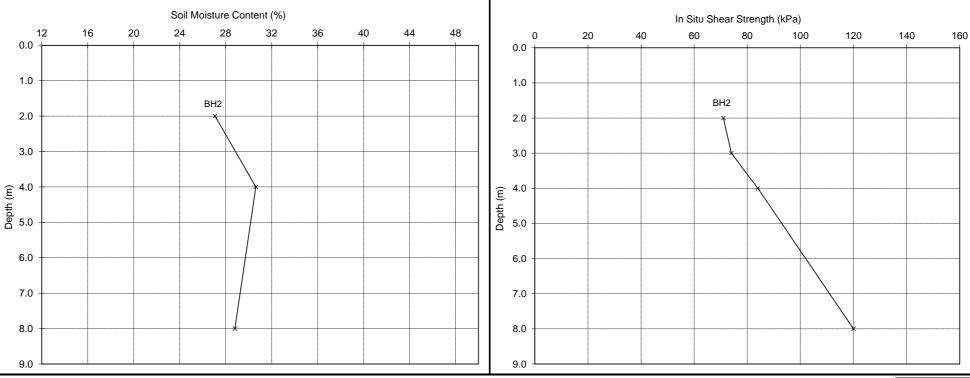


Job Number : CGL5678
Client : James Strachlan
Date Testing Started : 09/09/2015

Client Reference : CSI5678 Date Testing Completed : 11/09/2015

Site Name: 3 Honeybourne Road, NW6

Laboratory: Chelmer Geotechnical Laboratories, CM3 8AB



Notes :

2. If plotted, 0.4 LL and PL+2 (after Driscoll, 1983) should only be applied to London Clay (and similarly over consolidated clays) at shallow depths.

Comments :-

Unless otherwise stated, values of Shear Strength were determined in situ by Chelmer Site Investigations using a Pilcon Hand Vane the calibration of which is limited to a maximum reading of 140 kPa. (Not UKAS accredited)



8284

Checked By :- MC

Date Checked :- 11-Sep-15

If the Soil Fraction > 0.425mm exceeds 5% the Equivalent Moisture Content of the remainder ( calculated in accordance with BS 1377: Part 2: 1990, cl.3.2.4 note 1) is also plotted and the alternative profile additionally shown as an appropriately coloured broken line.

### **Laboratory Testing Results**

Plasticity Chart for the classification of fine soils and the finer part of coarse soils In Compliance with BS5930: 1999



Job Number: CGL5678 Client: James Strachlan

Client Reference : CSI5678

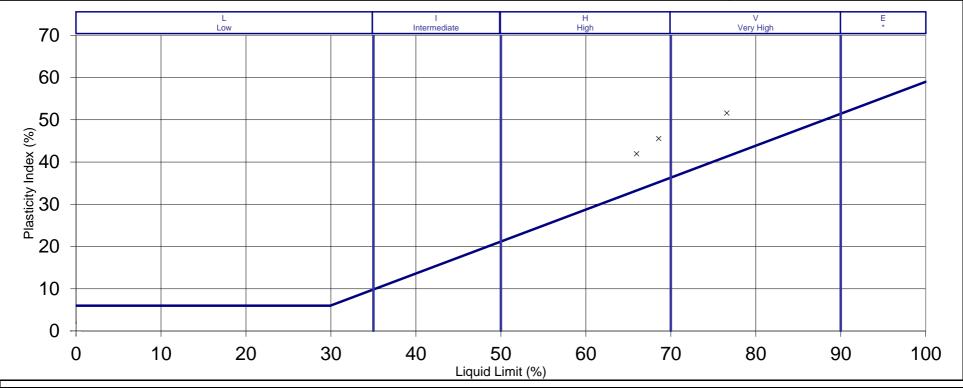
Site Name: 3 Honeybourne Road, NW6

Date Received: 08/09/2015 Date Testing Started: 09/09/2015

Date Testing Completed: 11/09/2015

Key:- BH2

Laboratory: Chelmer Geotechnical Laboratories, CM3 8AB



Notes :-

SILT (M-SOIL), M, plots below A-Line

CLAY, C, plots above A-Line }M and C may be combined as FINE SOIL, F.

Checked By :- MC

Comments :-

Date Checked :- 11-Sep-15





Mark Collyer
Chelmer Site Investigation Laboratories Ltd
Unit 15
East Hanningfield Industrial Estate
Old Church Road
East Hanningfield
Essex
CM3 8AB

#### **QTS Environmental Ltd**

Unit 1
Rose Lane Industrial Estate
Rose Lane
Lenham Heath
Kent
ME17 2JN

**t:** 01622 850410

russell.jarvis@qtsenvironmental.com

## **QTS Environmental Report No: 15-35332**

**Site Reference:** 3 Honeybourne Road, NW6

Project / Job Ref: CGL5678

**Order No:** 5089

**Sample Receipt Date:** 10/09/2015

**Sample Scheduled Date:** 10/09/2015

**Report Issue Number:** 1

**Reporting Date:** 16/09/2015

**Authorised by:** 

Russell Jarvis Director

On behalf of QTS Environmental Ltd

**Authorised by:** 

Kevin Old Director

On behalf of QTS Environmental Ltd



# QTS Environmental Ltd Unit 1, Rose Lane Industrial Estate Rose Lane Lenham Heath Maidstone Kent ME17 2JN Tel: 01622 850410



Soil Analysis Certificate								
QTS Environmental Report No: 15-35332	Date Sampled	11/08/15	11/08/15	11/08/15				
Chelmer Site Investigation Laboratories Ltd	Time Sampled	None Supplied	None Supplied	None Supplied				
Site Reference: 3 Honeybourne Road, NW6	TP / BH No	65784	65785	65787				
Project / Job Ref: CGL5678	Additional Refs	2	2	TP3				
Order No: 5089	Depth (m)	3.00	4.00	0.90				
Reporting Date: 16/09/2015	QTSE Sample No	166335	166336	166337				

Determinand	Unit	RL	Accreditation				
рН	pH Units	N/a	MCERTS	7.7	7.7	8.1	
Total Sulphate as SO <sub>4</sub>	mg/kg	< 200	NONE	4973	6550	3172	
Total Sulphate as SO <sub>4</sub>	%	< 0.02	NONE	0.50	0.66	0.32	
W/S Sulphate as SO <sub>4</sub> (2:1)	mg/l	< 10	MCERTS	950	2010	1440	
W/S Sulphate as SO <sub>4</sub> (2:1)	g/l	< 0.01	MCERTS	0.95	2.01	1.43	
Total Sulphur	%	< 0.02	NONE	0.17	0.22	0.12	
Ammonium as NH <sub>4</sub>	mg/kg	< 0.5	NONE	6.8	11.3	3.6	
Ammonium as NH <sub>4</sub>	mg/l	< 0.05	NONE	0.68	1.13	0.36	
W/S Chloride (2:1)	mg/kg	< 1	MCERTS	35	23	22	
W/S Chloride (2:1)	mg/l	< 0.5	MCERTS	17.7	11.7	11.1	
Water Soluble Nitrate (2:1) as NO <sub>3</sub>	mg/kg	< 3	MCERTS	< 3	< 3	< 3	
Water Soluble Nitrate (2:1) as NO <sub>3</sub>	mg/l	< 1.5	MCERTS	< 1.5	< 1.5	< 1.5	
W/S Magnesium	mg/l	< 0.1	NONE	16	86	86	

Analytical results are expressed on a dry weight basis where samples are dried at less than 30°C

Analysis carried out on the dried sample is corrected for the stone content

Subcontracted analysis (S)



Reporting Date: 16/09/2015

# QTS Environmental Ltd Unit 1, Rose Lane Industrial Estate Rose Lane Lenham Heath Maidstone Kent ME17 2JN Tel: 01622 850410



Soil Analysis Certificate - Sample Descriptions

QTS Environmental Report No: 15-35332

Chelmer Site Investigation Laboratories Ltd

Site Reference: 3 Honeybourne Road, NW6

Project / Job Ref: CGL5678

Order No: 5089

QTSE Sample No	TP / BH No	Additional Refs	Depth (m)	Moisture Content (%)	Sample Matrix Description
\$ 166335	65784	2	3.00	20.7	Light brown clay
\$ 166336	65785	2	4.00	20.2	Brown clay
\$ 166337	65787	TP3	0.90	15.4	Grey sandy gravel

Moisture content is part of procedure E003 & is not an accredited test Insufficient Sample  $^{\rm I/S}$  Unsuitable Sample  $^{\rm U/S}$ 

\$ samples exceeded recommended holding times



# QTS Environmental Ltd Unit 1, Rose Lane Industrial Estate Rose Lane Lenham Heath Maidstone Kent ME17 2JN Tel: 01622 850410



Soil Analysis Certificate - Methodology & Miscellaneous Information

QTS Environmental Report No: 15-35332 Chelmer Site Investigation Laboratories Ltd Site Reference: 3 Honeybourne Road, NW6

Project / Job Ref: CGL5678

Order No: 5089

Reporting Date: 16/09/2015

Matrix	Analysed On	Determinand	Brief Method Description		
Soil	D	Boron - Water Soluble	Determination of water soluble boron in soil by 2:1 hot water extract followed by ICP-OES	<b>No</b> E012	
Soil	AR		Determination of BTEX by headspace GC-MS	E001	
Soil	D		Determination of cations in soil by aqua-regia digestion followed by ICP-OES	E002	
Soil	D		Determination of chloride by extraction with water & analysed by ion chromatography	E009	
Soil	AR	Chromium - Hexavalent	Determination of hexavalent chromium in soil by extraction in water then by acidification, addition of 1,5 diphenylcarbazide followed by colorimetry	E016	
Soil	AR	Cyanide - Complex	Determination of complex cyanide by distillation followed by colorimetry	E015	
Soil	AR	Cyanide - Free	Determination of free cyanide by distillation followed by colorimetry	E015	
Soil	AR	Cyanide - Total	Determination of total cyanide by distillation followed by colorimetry	E015	
Soil	D		Gravimetrically determined through extraction with cyclohexane	E011	
Soil	AR	Diesel Range Organics (C10 - C24)	Determination of hexane/acetone extractable hydrocarbons by GC-FID	E004	
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of saturated calcium sulphate followed by electrometric measurement	E022	
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of water followed by electrometric measurement	E023	
Soil	D	Elemental Sulphur	Determination of elemental sulphur by solvent extraction followed by GC-MS	E020	
Soil	AR	EPH (C10 - C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004	
Soil	AR		Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004	
Soil	AR	EPH TEXAS (C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID for C8 to C40. C6 to C8 by headspace GC-MS	E004	
Soil	D	Fluoride - Water Soluble	Determination of Fluoride by extraction with water & analysed by ion chromatography	E009	
Soil	D	FOC (Fraction Organic Carbon)	Determination of fraction of organic carbon by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010	
Soil	D	Loss on Ignition @ 450oC	Determination of loss on ignition in soil by gravimetrically with the sample being ignited in a muffle furnace	E019	
Soil	D	Magnesium - Water Soluble	Determination of water soluble magnesium by extraction with water followed by ICP-OES	E025	
Soil	D		Determination of metals by aqua-regia digestion followed by ICP-OES	E002	
Soil	AR		Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge	E004	
Soil	AR	Moisture Content	Moisture content; determined gravimetrically	E003	
Soil	D		Determination of nitrate by extraction with water & analysed by ion chromatography	E009	
Soil	D	Organic Matter	I/ II \ CIIINNATA	E010	
Soil	AR	PAH - Speciated (EPA 16)	Determination of PAH compounds by extraction in acetone and hexane followed by GC-MS with the use of surrogate and internal standards	E005	
Soil	AR	PCB - 7 Congeners	Determination of PCB by extraction with acetone and hexane followed by GC-MS	E008	
Soil	D	Petroleum Ether Extract (PEE)	Gravimetrically determined through extraction with petroleum ether	E011	
Soil	AR	pH	Determination of pH by addition of water followed by electrometric measurement	E007	
Soil	AR	Phenols - Total (monohydric)	Determination of phenols by distillation followed by colorimetry	E021	
Soil	D	Phosphate - Water Soluble (2:1)	Determination of phosphate by extraction with water & analysed by ion chromatography	E009	
Soil	D	Sulphate (as SO4) - Total	Determination of total sulphate by extraction with 10% HCl followed by ICP-OES	E013	
Soil	D		Determination of sulphate by extraction with water & analysed by ion chromatography	E009	
Soil	D		Determination of water soluble sulphate by extraction with water followed by ICP-OES	E014	
Soil	AR		Determination of sulphide by distillation followed by colorimetry	E018	
Soil	D	Sulphur - Total	Determination of total sulphur by extraction with aqua-regia followed by ICP-OES	E024	
Soil	AR	SVOC	Determination of semi-volatile organic compounds by extraction in acetone and hexane followed by GC-MS	E006	
Soil	AR	Thiocyanate (as SCN)	Determination of thiocyanate by extraction in caustic soda followed by acidification followed by addition of ferric nitrate followed by colorimetry	E017	
Soil	D	Toluene Extractable Matter (TEM)	Gravimetrically determined through extraction with toluene	E011	
Soil	D	Total Organic Carbon (TOC)	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010	
Soil	AR		Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C35. C5 to C8 by headspace GC-MS	E004	
Soil	AR	C5-C7, C7-C8, C8-C10, C10-C12, C12- C16, C16-C21, C21-C35, C35-C44)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C44. C5 to C8 by headspace GC-MS	E004	
Soil	AR		Determination of volatile organic compounds by headspace GC-MS	E001	
Soil	AR	VPH (C6-C8 & C8-C10)	Determination of hydrocarbons C6-C8 by headspace GC-MS & C8-C10 by GC-FID	E001	

D Dried AR As Received





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Where our involvement consists exclusively of testing samples, the results and comments (if provided) relate only to the samples tested.

Any samples that are deemed to be subject to deviation will be recorded as such within the test summary.



