Type 2: After CHP

	L	Jser De	etails:						
Assessor Name: Software Name: Stroma FSAP 2012		ę	Softwa	a Num are Ver L2 2BF	sion:		Versic	on: 1.0.1.25	
Address: , NW1 1JD		porty /			Laor				
1. Overall dwelling dimensions:									
Ground floor		Area		(1a) x	<b>Av. Hei</b> 3.	<b>ght(m)</b> 15	(2a) =	<b>Volume(m<sup>3</sup>)</b> 252	) (3a)
Total floor area TFA = $(1a)+(1b)+(1c)+(1d)+(1e)+(1e)+(1e)+(1e)+(1e)+(1e)+(1e)+(1e$	+(1n)	8	30	(4)					
Dwelling volume				(3a)+(3b)	+(3c)+(3d	)+(3e)+	.(3n) =	252	(5)
2. Ventilation rate:					1-1-1				
	condary eating 0	+	0 0	] = [	total 0 0	x 2	40 = 20 = 0 =	m <sup>3</sup> per hour	(6a) (6b)
					0			0	(7a)
Number of passive vents				Ļ	0		0 =	0	(7b)
Number of flueless gas fires 0   x   40 =   0   (7c) Air changes per hour Infiltration due to chimneys, flues and fans = (6a)+(6b)+(7a)+(7c) =   0   ÷ (5) =   0   (8)									ur
If a pressurisation test has been carried out or is intended, proceed to (17), otherwise continue from (9) to (16)          Number of storeys in the dwelling (ns)       0       (9)         Additional infiltration       [(9)-1]x0.1 =       0       (10)								(9) (10) (11)	
If suspended wooden floor, enter 0.2 (unseale	d) or 0.1	(sealed	d), else	enter 0				0	(12)
If no draught lobby, enter 0.05, else enter 0								0	(13)
Percentage of windows and doors draught stri	pped	0		x (14) ÷ 1	001			0	(14)
Window infiltration Infiltration rate				x (14) ÷ 1 + (11) + (1		0	(15)		
Air permeability value, q50, expressed in cubic	- metres i			0	(16) (17)				
If based on air permeability value, then $(18) = [(17)]$	-	•	•	•		nvelope	uluu	0.15	(17)
Air permeability value applies if a pressurisation test has b					is being us	sed			
Number of sides sheltered								0	(19)
Shelter factor				0.075 x (1	9)] =			1	(20)
Infiltration rate incorporating shelter factor		(2	21) = (18)	x (20) =				0.15	(21)
Infiltration rate modified for monthly wind speed	lune	1.1	A	0.000	Ort	Nierr	Dee	1	
Jan Feb Mar Apr May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Monthly average wind speed from Table 7(22)m=5.154.94.44.3	3.8	3.8	3.7	4	4.3	4.5	4.7	1	
	5.0	5.0	3.1	4	4.5	4.0	4.1	l	
Wind Factor (22a)m = (22)m $\div$ 4	0.05	0.05 T			4.00	4.40	4.40	1	
(22a)m= 1.27 1.25 1.23 1.1 1.08	0.95	0.95	0.92	1	1.08	1.12	1.18		

Adjust	ed infiltr	ation rat	e (allowi	ing for sh	elter an	d wind s	peed) =	(21a) x	(22a)m					
	0.19	0.19	0.18	0.16	0.16	0.14	0.14	0.14	0.15	0.16	0.17	0.18		
		<i>ctive air</i> al ventila	-	rate for t	he appli	cable ca	se						0.5	(22.0)
				endix N, (2	3b) = (23a	i) x Fmv (e	equation (N	N5)), other	wise (23b	) = (23a)			0.5	(23a) (23b)
				iency in %						) = (20u)			0.5	
			-	-	-					2h)m ⊥ ('	23P) ^ [-	1 – (23c)	64.6 ÷ 1001	(23c)
(24a)m=		0.36	0.36	0.34	0.34	0.32	0.32	0.32	0.33	0.34	0.35	0.35	÷ 100]	(24a)
				entilation								0.00		
(24b)m=					0			0	0		0	0		(24b)
	-	-	_	tilation c	-	-	-	-	Ţ	Ŭ	Ů	Ŭ		(=)
,				then (240	•	•				5 × (23b	))			
(24c)m=	, <i>,</i>	0	0	0	0	0	0	0	0	0	0	0		(24c)
d) If	natural	ı ventilatio	n or wh	ole hous	e positiv	/e input v	ı ventilatio	on from l	oft					
				m = (22k						0.5]				
(24d)m=	0	0	0	0	0	0	0	0	0	0	0	0		(24d)
Effe	ctive air	change	rate - er	nter (24a	) or (24b	o) or (240	c) or (24	d) in box	(25)					
(25)m=	0.37	0.36	0.36	0.34	0.34	0.32	0.32	0.32	0.33	0.34	0.35	0.35		(25)
3 He	at losse	s and he	at loss i	paramete	ər:									_
ELEN		Gros		Openin		Net Ar	ea	U-valu	le	AXU		k-value		A X k
		area		m		A ,r		W/m2		(W/I	K)	kJ/m <sup>2</sup> ·ł		kJ/K
Windo	ws Type	e 1				2.85	x1,	/[1/( 1.3 )+	0.04] =	3.52				(27)
Windo	ws Type	92				12.65	5 x1,	/[1/( 1.3 )+	0.04] =	15.63				(27)
Walls		67		21.2		45.8	x	0.11	] = [	5.04	F r			(29)
Total a	rea of e	lements	, m²			67								(31)
Party v	vall					19	×	0		0				(32)
Party v	vall					32	×	0		0	= 1		$\exists$	(32)
Party f						80			L		L		$\dashv$	(32a)
Party c						80					L L		$\dashv$	(32b)
	al wall **										L		$\dashv$	(32c)
			OWS USA	offective wi	ndow H-va	74	ated using	ı formula 1	/[(1/  ]_vəlu	مر) 10 (14 مر	l s aiven in	paragraph		(320)
				nternal wall			atou using	nonnula n	[[ # O Valu	0)+0.04j d	is given in	paragraph	0.2	
Fabric	heat los	s, W/K :	= S (A x	U)				(26)(30)	+ (32) =				31.24	(33)
Heat c	apacity	Cm = S(	(Axk)						((28)	.(30) + (32	2) + (32a).	(32e) =	31116	(34)
Therm	al mass	parame	ter (TM	<sup>-</sup> = Cm ÷	- TFA) ir	n kJ/m²K			Indica	tive Value	: Medium		250	(35)
	-	sments wh ad of a de		tails of the ulation.	constructi	ion are not	t known pr	ecisely the	indicative	values of	TMP in Ta	able 1f		
Therm	al bridge	es : S (L	x Y) cal	culated u	using Ap	pendix k	<						7	(36)
if details	of therma	al bridging	are not kr	nown (36) =	= 0.15 x (3	1)								
Total fa	abric he	at loss							(33) +	(36) =			38.24	(37)
Ventila	tion hea	at loss ca	alculated	d monthly	/				(38)m	= 0.33 × (	25)m x (5)		L	
	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(38)m=	30.62	30.31	30	28.44	28.13	26.57	26.57	26.26	27.19	28.13	28.75	29.38		(38)
Heat tr	ansfer o	coefficier	nt, W/K						(39)m	= (37) + (3	38)m			
(39)m=	68.86	68.55	68.24	66.68	66.36	64.81	64.81	64.49	65.43	66.36	66.99	67.61		
Stroma I	FSAP 201	2 Version	1.0.1.25	(SAP 9.92)	- http://ww	ww.stroma	.com		/	Average =	Sum(39)1	12 /12=	66.6pag	<u>ge 2 o<mark>(</mark>39)</u>

Heat lo	ss para	meter (H	HLP), W	/m²K					(40)m	= (39)m ÷	- (4)			
(40)m=	0.86	0.86	0.85	0.83	0.83	0.81	0.81	0.81	0.82	0.83	0.84	0.85		
								I	·	Average =	Sum(40)1	<sub>12</sub> /12=	0.83	(40)
edmuni ]		i	nth (Tab	,	Max	luna		A	Con	Oat	Nev	Dee	1	
(11)m-	Jan	Feb	Mar	Apr 20	May 21	Jun	Jul	Aug	Sep	Oct	Nov	Dec 21		(41)
(41)m=	31	28	31	30	31	30	31	31	30	31	30	31		(41)
4. Wat	ter heat	ting enei	rgy requ	irement:								kWh/ye	ear:	
if TF/	A > 13.9	upancy, l 9, N = 1 9, N = 1		: [1 - exp	(-0.0003	349 x (TF	FA -13.9	)2)] + 0.(	0013 x ( <sup>-</sup>	TFA -13		46	]	(42)
Reduce t	he annua	al average	hot water		5% if the a	welling is	designed	(25 x N) to achieve		se target c		69	]	(43)
[	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Hot wate	r usage ii	n litres per	r day for ea	ach month	Vd,m = fa	ctor from	Table 1c x	(43)	-		-		_	
(44)m=	101.96	98.25	94.55	90.84	87.13	83.42	83.42	87.13	90.84	94.55	98.25	101.96		_
Ener <mark>gy c</mark>	ontent of	hot water	used - ca	culated me	onthly $= 4$ .	190 x Vd,ı	m x nm x L	OTm / 3600			1 <mark>m(44)</mark> 112 = ables 1b, 1		1112.32	(44)
(45)m=	1 <mark>5</mark> 1.21	132.25	136.47	118.97	114.16	9 <mark>8.51</mark>	91.28	104.75	106	123.53	134.85	146.44		
lf instanta	aneous w	vater heatii	ng at point	t of use (no	o hot water	r storage),	enter 0 in	boxes (46		Total = Su	ım(45) <sub>112</sub> =	=	1458.42	(45)
(46)m=	22.68	19.84	20.47	17.85	17.12	14.78	13.69	15.71	15.9	18.53	20.23	21.97		(46)
Water s	storage	loss:						<u> </u>						
-				-				within sa	ame ves	sel		0		(47)
	•	•		ank in dw	•			• •		or (0) in (	(47)			
Water s			not wate	er (unis ir	iciudes i	nstantar	ieous co	ombi boil	ers) ente	er u in (	(47)			
	•		eclared I	oss facto	or is kno	wn (kWł	n/day):					0		(48)
			m Table			,	2,					0		(49)
				, kWh/ye	ear			(48) x (49)	) =		1	10		(50)
			-	cylinder		or is not	known:						1	
		-		rom Tabl	le 2 (kW	h/litre/da	ay)				0.	02		(51)
	•	from Ta	ee secti	on 4.3									1	(50)
			m Table	2h								03 .6		(52) (53)
				e, kWh/ye	oor			(47) x (51)	) y (52) y (	52) -			]	
0,		(54) in (5	•	, KVVII/ JV	Jai			(47) X (51)	) ^ (32) ^ (	00) -		03 03		(54) (55)
		. , .		for each	month			((56)m = (	(55) × (41)	m			I	()
(56)m=	32.01	28.92	32.01	30.98	32.01	30.98	32.01	32.01	30.98	32.01	30.98	32.01		(56)
· · /								i0), else (5					] lix H	()
(57)m=	32.01	28.92	32.01	30.98	32.01	30.98	32.01	32.01	30.98	32.01	30.98	32.01		(57)
Primar	/ circuit	loss (ar	nual) fro	om Table	e 3							0		(58)
		•	,			59)m =	(58) ÷ 36	65 × (41)	m					
(mod	ified by	factor f	rom Tab	le H5 if t	here is s	solar wa	ter heati	ng and a	a cylinde	r thermo	ostat)			
(59)m=	23.26	21.01	23.26	22.51	23.26	22.51	23.26	23.26	22.51	23.26	22.51	23.26		(59)

Combi	loss ca	alculated	for each	n month	(61)m =	(60) ÷ 3	865 × (41	)m						
(61)m=	0	0	0	0	0	0	0	0	0	0	0	0		(61)
Total h	eat req	uired for	water h	eating ca	alculated	for ea	ch month	(62)m =	= 0.85 × (	(45)m +	(46)m +	(57)m +	(59)m + (61)m	
(62)m=	206.48	182.17	191.74	172.47	169.44	152	146.56	160.03	159.5	178.81	188.34	201.71		(62)
Solar DH	HW input	calculated	using App	oendix G o	r Appendix	H (nega	tive quantity	/) (enter 'C	)' if no sola	r contribut	ion to wate	er heating)		
(add a	dditiona	al lines if	FGHRS	and/or \	WWHRS	applie	s, see Ap	pendix (	G)	_		-		
(63)m=	0	0	0	0	0	0	0	0	0	0	0	0		(63)
Output	from w	ater hea	ter											
(64)m=	206.48	182.17	191.74	172.47	169.44	152	146.56	160.03	159.5	178.81	188.34	201.71		
				-				Out	put from w	ater heate	r (annual)₁	12	2109.26	(64)
Heat g	ains fro	m water	heating	, kWh/m	onth 0.2	5 ´ [0.8	5 × (45)m	ı + (61)n	n] + 0.8 >	k [(46)m	+ (57)m	+ (59)m	]	
(65)m=	94.5	83.91	89.6	82.35	82.18	75.55	74.57	79.05	78.04	85.3	87.63	92.91		(65)
inclu	de (57)	m in calo	culation	of (65)m	only if c	ylinder	is in the o	dwelling	or hot w	ater is fi	rom com	munity h	leating	
5. Int	ernal a	ains (see	e Table (	5 and 5a	):	-		-				•	-	
		ns (Table			/									
metab	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
(66)m=	123.14	123.14	123.14	123.14	123.14	123.14		123.14	123.14	12 <mark>3.14</mark>	123.14	123.14		(66)
	d dains	(calcula	ted in A			ion 190	 or L9a), a							
(67)m=	19.56	17.38	14.13	10.7	8	6.75	7.3	9.48	12.73	16.16	18.86	20.11		(67)
				<u> </u>			13 or L1			L				
(68)m=	219.44		215.98	203.76	188.34	173.85		161.89	167.63	179.84	195.27	209.76		(68)
							-				199.21	209.70		(00)
		1			· · ·		5 or L15a)	· · · · · · · · · · · · · · · · · · ·			25.24	25.24		(69)
(69)m=	35.31	35.31	35.31	35.31	35.31	35.31	35.31	35.31	35.31	3 <mark>5.31</mark>	35.31	35.31		(09)
-		ins gains	·	<u> </u>									I	( <b>70</b> )
(70)m=	0	0	0	0	0	0	0	0	0	0	0	0		(70)
		vaporatic	<u> </u>	T	, `	· ·								
(71)m=	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51	-98.51		(71)
Water		gains (T	able 5)	i			-							
(72)m=	127.01	124.87	120.43	114.38	110.46	104.93	100.23	106.25	108.39	114.65	121.71	124.88		(72)
Total i	nterna	l gains =				(60	6)m + (67)m	n + (68)m ·	+ (69)m +	(70)m + (7	'1)m + (72)	m		
(73)m=	425.96	423.91	410.48	388.79	366.74	345.47	331.64	337.57	348.69	370.59	395.78	414.69		(73)
6. So	lar gain	s:												
			0	ar flux from	Table 6a a		ciated equa	itions to co	onvert to th	ne applicat		ion.		
Orienta		Access F		Area			ux	т	g_	-	FF		Gains	
		Table 6d		m²		1 č	able 6a	, <u> </u>	able 6b		able 6c		(W)	-
Northea		0.77	x	2.8	35	x	11.28	x	0.7	x	1.11	=	52	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.8	35	x	22.97	x	0.7	×	1.11	=	105.84	(75)
Northea	ast <mark>0.9</mark> x	0.77	x	2.8	35	x	41.38	x	0.7	x	1.11	=	190.69	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.8	35	x	67.96	x 🗌	0.7	x	1.11	=	313.17	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.8	35	x	91.35	x	0.7	x	1.11	=	420.96	(75)

NI //														
Northea	ast <mark>0.9x</mark>	0.77	x	2.85	x	9	7.38	x	0.7	x	1.11	=	448.79	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.85	x	Ę.	91.1	x	0.7	x	1.11	=	419.84	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.85	x	× 72.63		x	0.7	x	1.11	=	334.7	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.85	×	5	0.42	x	0.7	x	1.11	=	232.36	(75)
Northea	ast <mark>0.9x</mark>	0.77	x	2.85	×	2	8.07	x	0.7	×	1.11	=	129.35	(75)
Northea	ast <mark>0.9x</mark>	0.77	×	2.85	×		14.2	x	0.7	×	1.11	=	65.43	(75)
Northea	ast <mark>0.9x</mark>	0.77	×	2.85	×		9.21	x	0.7	×	1.11	= =	42.46	(75)
Southe	ast <mark>0.9x</mark>	0.54	×	12.65	×	3	6.79	x	0.7	×	1.11	=	175.94	(77)
Southe	ast 0.9x	0.54	×	12.65	×	6	2.67	x	0.7	×	1.11	=	299.69	(77)
Southe	ast 0.9x	0.54	×	12.65	×	8	5.75	x	0.7	×	1.11	=	410.04	(77)
Southe	ast 0.9x	0.54	×	12.65	×	10	06.25	x	0.7	×	1.11	= =	508.06	(77)
Southe	ast 0.9x	0.54	×	12.65	×	1	19.01	x	0.7	×	1.11	=	569.07	(77)
Southe	ast <mark>0.9x</mark>	0.54	×	12.65	×	1	18.15	x	0.7	×	1.11	= =	564.96	(77)
Southe	ast 0.9x	0.54	×	12.65	×	1	13.91	x	0.7	×	1.11	=	544.68	(77)
Southe	ast <mark>0.9x</mark>	0.54	×	12.65	×	1(	04.39	x	0.7	×	1.11	=	499.16	(77)
Southe	ast <mark>0.9x</mark>	0.54	×	12.65	×	9	2.85	x	0.7	×	1.11	= =	443.99	(77)
Southe	ast <mark>0.9x</mark>	0.54	×	12.65	×	6	9.27	x	0.7	×	1.11	=	331.22	(77)
Sout <mark>he</mark>	ast 0.9x	0.54	×	12.65	×	4	4.07	х	0.7	x	1.11	=	210.73	(77)
Sout <mark>he</mark>	ast 0.9x	0.54	×	12.65	T x	3	1.49	x	0.7	x	1.11	=	150.57	(77)
										-				
Solar	nains in v	watts cal	culated	for each me	onth			(83)m	= Sum(74)m	(82)m				
(83)m=	227.93		600.74			013.75	964.51	833.		460.5	6 276.16	193.03		(83)
Total g	gains – ir	nternal an	d solar	(84)m = (73	3)m +	(83)m	, watts					I		
(84)m=	653.89	829.44	1011.21	1210.02 135	Total gains – internal and solar $(84)m = (73)m + (83)m$ , watts (84)m = 653.89 829.44 1011.21 1210.02 1356.78 1359.22 1296.15 1171.43 1025.04 831.16 671.94 607.72 (84)									
									.43 1025.04	831.1		(84)		
7. Mean internal temperature (heating season) Temperature during heating periods in the living area from Table 9, Th1 (°C) 21 (85)										831.1	6 671.94	607.72		(84)
			rature (	heating sea	ason)					831.1	671.94	607.72	21	
Temp	perature	during he	erature ( ating po	heating sea	ason) e living	area f	rom Tab			831.1	671.94	607.72	21	(84)
Temp	perature	during he	erature ( ating po	heating sea eriods in the ving area, h	ason) e living n1,m (s	area f	rom Tab	ole 9,	Th1 (°C)	831.1		607.72	21	
Temp	perature ation fac	during he tor for gai	erature ( ating po ns for li	heating sea eriods in the ving area, h Apr N	ason) e living	area f see Ta	rom Tab ble 9a)		Th1 (°C) ıg Sep				21	
Temp Utilisa (86)m=	erature ation fac Jan 0.99	during he tor for gai Feb 0.95	erature ( ating po ns for li Mar 0.86	heating sea eriods in the ving area, h Apr M 0.65 0.	ason) e living n1,m (s 1ay	area f see Ta Jun 0.31	from Tab ble 9a) Jul 0.22	ole 9, Au 0.2	Th1 (°C) Ig Sep 5 0.44	Oct	Nov	Dec	21	(85)
Temp Utilisa (86)m=	erature ation fac Jan 0.99	during he tor for gai Feb 0.95	erature ( ating po ns for li Mar 0.86 ture in l	heating sea eriods in the ving area, f Apr N 0.65 0. iving area T	ason) e living 11,m (s 1ay 45	area f see Ta Jun 0.31 ow ste	from Tab ble 9a) Jul 0.22	ole 9, Au 0.2	Th1 (°C) Ig Sep 5 0.44 able 9c)	Oct 0.78	Nov 0.96	Dec 0.99	21	(85)
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Apply adjustment to the mean internal temperature from Table 4e, where appropriate

		(00)						
(93)m=         19.78         20.08         20.36         20.51         20.53         20.55         20.5           8. Space heating requirement	5 20.55 20.54 20.48 20.13 19.74	(93)						
Set Ti to the mean internal temperature obtained at step 11	of Table 9b, so that Tim=(76)m and re-calculate							
the utilisation factor for gains using Table 9a								
Jan Feb Mar Apr May Jun Ju	Aug Sep Oct Nov Dec							
Utilisation factor for gains, hm:								
(94)m= 0.98 0.94 0.83 0.63 0.43 0.28 0.2	0.23 0.41 0.75 0.95 0.99	(94)						
Useful gains, hmGm , W = (94)m x (84)m								
(95)m= 642.39 780.97 844.01 758.68 584.97 385.32 255.	7 267.56 420.8 620.87 639.37 600.2	(95)						
Monthly average external temperature from Table 8 (96)m= 4.3 4.9 6.5 8.9 11.7 14.6 16.6	6 16.4 14.1 10.6 7.1 4.2	(96)						
		(90)						
Heat loss rate for mean internal temperature, Lm , W =[(39) (97)m= 1065.91 1040.38 945.58 774.13 586.3 385.38 255.3		(97)						
Space heating requirement for each month, kWh/month = $0$		(01)						
(98)m= 315.11 174.33 75.57 11.13 0.99 0 0	0 0 25.93 168.13 335.05							
	Total per year (kWh/year) = Sum(98) <sub>15,912</sub> = 1106	5.23 (98)						
Space heating requirement in kWh/m²/year								
,	13.	55 (55)						
9b. Energy requirements – Community heating scheme								
This part is used for space heating, space cooling or water h Fraction of space heat from secondary/supplementary heating		(301)						
Fraction of space heat from community system 1 – (301) =								
The community scheme may obtain heat from several sources. The procedure allows for CHP and up to four other heat sources; the latter								
includes boilers, heat pumps, geothermal and waste heat from power station	ns. See Appendix C.							
Fraction of heat from Community CHP	0.	6 (303a)						
Fraction of community heat from heat source 2	0.	4 (303b)						
Fraction of total space heat from Community CHP	(302) x (303a) = 0.	6 (304a)						
Fraction of total space heat from community heat source 2	(302) x (303b) = 0.	4 (304b)						
Factor for control and charging method (Table 4c(3)) for com	munity heating system 1	(305)						
Distribution loss factor (Table 12c) for community heating sys	stem 1.	4 (306)						
Space heating	kW	h/year						
Annual space heating requirement	1106	5.23						
Space heat from Community CHP	(98) x (304a) x (305) x (306) = 929	.24 (307a)						
Space heat from heat source 2	(98) x (304b) x (305) x (306) = 619	.49 (307b)						
Efficiency of secondary/supplementary heating system in %	from Table 4a or Appendix E)	(308						
Space heating requirement from secondary/supplementary s	ystem (98) x (301) x 100 ÷ (308) =	(309)						
Water heating								
Annual water heating requirement	2109	).26						
If DHW from community scheme: Water heat from Community CHP	(64) x (303a) x (305) x (306) = 177'	I.78 (310a)						
Water heat from heat source 2	$(64) \times (303b) \times (305) \times (306) =$ 118'							
Electricity used for heat distribution	0.01 × [(307a)(307e) + (310a)(310e)] = 45.	02 (313)						

Cooling System Energy Efficiency Ratio		0	(314)
Space cooling (if there is a fixed cooling system, if not enter 0)	= (107) ÷ (314) =	0	(315)
Electricity for pumps and fans within dwelling (Table 4f):		<b></b>	
mechanical ventilation - balanced, extract or positive input from o	Dutside	305.6	(330a)
warm air heating system fans		0	(330b)
pump for solar water heating		0	(330g)
Total electricity for the above, kWh/year	=(330a) + (330b) + (330g) =	305.6	(331)
Energy for lighting (calculated in Appendix L)		345.49	(332)
12b. CO2 Emissions – Community heating scheme			
Electrical efficiency of CHP unit		35	(361)
Heat efficiency of CHP unit		40	(362)
	Energy Emission factor kWh/year kg CO2/kWh	or Emissions kg CO2/year	
Space heating from CHP) $(307a) \times 100 \div (362) =$	2323.09 × 0.22	501.79	(363)
less credit emissions for electricity $-(307a) \times (361) \div (362) =$	813.08 × 0.52	-421.99	(364)
Water heated by CHP (310a) × 100 ÷ (362) =	4429.45 × 0.22	956.76	(365)
less credit emissions for electricity -(310a) × (361) ÷ (362) =	1550.31 × 0.52	-804.61	(366)
Efficiency of heat source 2 (%) If there is CHP using	two fuels repeat (363) to (366) for the second	fuel 85	(367b)
CO2 associated with heat source 2 [(307b)+(	310b)] x 100 ÷ (367b) x 0.22	= 457.58	(368)
Electrical energy for heat distribution	(313) x 0.52	= 23.36	(372)
Total CO2 associated with community systems	363)(366) + (368)(372)	= 712.9	(373)
CO2 associated with space heating (secondary)	309) x 0	= 0	(374)
CO2 associated with water from immersion heater or instantaneous	ous heater (312) x 0.22	= 0	(375)
Total CO2 associated with space and water heating	373) + (374) + (375) =	712.9	(376)
CO2 associated with electricity for pumps and fans within dwellin	ng (331)) x 0.52	= 158.6	(378)
CO2 associated with electricity for lighting	332))) x 0.52	= 179.31	(379)
Total CO2, kg/year sum of (376)(382) =		1050.81	(383)
Dwelling CO2 Emission Rate (383) ÷ (4) =		13.14	(384)
El rating (section 14)		88.74	(385)