BASEMENT IMPACT ASSESSMENT

At

13 KYLEMORE ROAD LONDON NW6 2PT

Job No: 141040 Date: AUGUST 2015



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Design Information - Structural

Introduction

Camden Council will only permit basement and underground developments that do not:

- Cause harm to the built and natural environment and local amenity
- Result in flooding
- Lead to ground instability

The internal walls are masonry on the ground floor and stud walls on the first floor with timber suspended floors on the ground and first floor. The roof is pitched and supported on the external brickwork and internal load bearing stud walls.

The property is an existing two storey mid terraced property with an existing semibasement towards the front part of the house. At the rear of the existing house the floor to ceiling height is increased due to the property being at split level throughout.

This basement impact assessment has been prepared to justify these requirements to the local town planners so they can make an informed decision on the proposed construction works.

Proposed works

The proposed work constitutes increasing the existing height of the semi-basement at the front of the property and forming a new terraced garden area with steps down to the lower ground level. This will be constructed using mass concrete underpinning the existing external walls. The existing bay fronted window will be constructed at basement level to provide additional natural daylight at basement level.

In addition, at the same time it is proposed that alterations throughout the house and a loft conversion is to be undertaken.

The basement method of construction will be carried out as follows:

- 1. Excavate front to allow for conveyor to be inserted.
- Form front of basement with cantilevered retaining walls.
- Slowly work from the front to the rear inserting 1200 long concrete underpinning sections.
- 4. Cast ground slab.
- 5. Waterproof internal space as required with a drained cavity system.

Loading requirements (Eurocode 1-1-1)

	UDL kN/m2	Concentrated Loads kN	
Domestic Single Dwellings	1.5	2.0	·
The basement does not lie within	a 45 angle of the	highway, therefore High	ways
loading is not required to be applied			·

Number of storeys	3 becoming 4	
	Is Live Load Reduction included in design	No

Progressive collapse	(Design for consequence	s of localized failure in building	
Trogressive compac	(Design for consequences of localized failure in building from and unspecified cause)		
Is the Development	No	-,	
Multi Occupancy			
EC1-1-7	Consequence Class	Example of categorisation of	
(Progressive collapse)		building type and occupancy	
	Class 1	Houses not exceeding 4 storeys	
Progressive collapse	To NHBC guidance comp	liance is only required to other	
Change of use	floors if a material change	of use occurs to the property.	
	Initial Building Class	1	
	Proposed Building Class	1	
	If class has changed		
· ·	material change has	No	
: 	occurred		
Compliance Measures	Class 1 – No Requirements		
EC1-1-7	Provided a building has been designed and constructed in		
	accordance with the rules given in EN1990 to EN1999 for		
	satisfying stability in normal use, no specific consideration is		
	necessary with regard to accidental actions from		
	unidentified causes.		
Lateral stability	Wind action = 0.6kN/m2		
Exposure and wind			
loading conditions			
Stability Design	, , , , , , , , , , , , , , , , , , , ,		
	house are not being altered. The mass concrete		
	underpinning is designed to carry the vertical loading		
	applied from above.		
	The leteral couth accesses	overte e beginnet face and the	
	THE Tateral earth pressure	exerts a horizontal force on the	

	1	nal walls. They will be checked for resistance to any urning that this produces.
Lateral Actions	Lateral Forces applied from:	
	!	static pressure
	1 '	arge loading
	ł.	produce retaining wall thrust; this is restrained by the
	oppos	ing walls/foundations.
1 Basement Impact		
Screening	¢4! -	n 1. Culturan and Burney and a state of
Groundwater flow	Section 1.	n 1 – Subterranean flow screening chart
	a.	Is the site located directly above an aquifer?
		No. The site is underlain by London Clay.
		The tribute and an arrange by contact, and the
		The site is not near boundary of soil interfaces. It is
		not considered that the new basement will cause
		new springs to appear.
	b.	Will the proposed basement extend beneath the
		water table surface?
		Unknown.
	2.	Carry forward to scoping stage. Is the site within 100m of a watercourse, well
	2.	used/disused or potential spring line?
		No. OS maps and local walkover survey show no
·	:	wells, watercourses or potential spring lines within
		100m of the site.
	3.	Will the proposed basement development result in a
		change in the proportion of hard surfaces/paved
		areas?
		No. there are no works expected in the gardens
	4.	apart from the front light well. As part of the site drainage will more surface water
	4.	(eg. rainfall and run-off) than at present be
		discharged to the ground (eg. via Soakaways and or
		SUDS)?
		No. Existing roof Drainage will run into the existing
		drainage system. Surface water will still discharge to
		ground.
Slope Stability	Section 2 – Slope Stability screening flowchart	
	1.	Does the existing site include slopes, natural or man

 l	
	made greater than 7° (approximately 1 in 8)? No. Difference in height between the rear garden and front is less than 1 in 8 slope (approx flat). There are no major falls within 20m which will increase the risk of land slip. Refer to Map 2.
2.	Will the proposed re profiling of landscaping at site change slopes at the property boundary to more than 7° (approximately 1 in 8)? No. Proposed landscaping does not affect the slope.
3.	Does the development neighbouring land including railway cuttings and the like with a slope greater than 7° (approximately 1 in 8)? No. There are no railway cuttings adjacent to the property.
4.	Is the site within a wider hillside setting in which the general slope is greater than 7° (approximately 1 in 8)? No. The slope of the wider hillside setting is as per the property, approximately flat.
5.	Is the London Clay the shallowest strata on site? Yes.
 6.	Will any tree/s be felled as part of the proposed development and/or are any of the works proposed within any tree protection.
7.	No. No local trees are to be felled. Is there a history of seasonal shrink-swell subsidence in the local area, and/or evidence of such effects at the site? Unknown.
8.	Is the site within 100m of a watercourse or a potential spring line? No. OS maps and local walkover survey show no wells, watercourses or potential spring lines within 100m of the site.
9.	Is the site within an area of previously worked ground? No. From historical maps, the site has been residential for a substantial period of time.
10.	Is the site within an aquifer. If so will the proposed basement extend beneath the water table such that dewatering may be required during construction.
	No. The site is underlain by London Clay.

		Site Water Table Unknown — Knowledge of groundwater table required. Trial pit will be completed prior to undertaking the work. The design of the foundation will be to the new EuroCodes which requires the water table to be considered to full height this allows for local flooding/burst water mains, etc. Carry forward to scoping stage.
	11.	Is the site within 5m of a highway or pedestrian footway? Yes. Site is within 5m of the footpath/alleyway and the road surface is further than 5m from the front bay structure. Carry forward to scoping stage.
	12.	Will the proposed basement significantly increase the differential depth of foundations relative to the neighbouring properties. No. The differential depth will only be increased by approximately 0.8m. The footing will be bearing on London Clay and no significant change will occur. Party wall will be underpinned. Existing footings are expected to be corbelled masonry approx. 600mm below ground level. Carry forward to scoping stage.
	13.	Is the site over (or within the exclusion zone) of any tunnels, eg. railway lines. No. Nearest is the Overground Rail, + 65m from site, approximately.
Surface flow and flooding		
	1.	As part of the proposed site drainage, will surface water flows (eg. volume of rainfall and peak runoff) be materially changed from the existing route. No. The rainwater run-off will still percolate into the ground.
	2.	Will the proposed basement development result in a change to the hard surfaced/pave external areas? No. The amount of hard standing will remain unchanged.
	3.	Will the proposed basement result in changes to the inflows (instantaneous and long term of surface water being received by adjacent properties or downstream watercourses)? No. The proposed development will enter the current drainage system.

	4. Will the proposed basement result in changes to the quality of surface water being received by adjacent properties or downstream watercourses?	
	No. We propose a 150mm layer of compacted type 1 should be provided to prevent damming.	
	5. Is the site in an area known to be at risk from surface water flooding? No. From LDF flood risk maps, the street is within a	
	low risk area of flooding from surface water.	
2 Basement Impact		
Scoping Groundwater flow		
	The property and adjacent railway is evident on these maps at this time, and is known to have been constructed in the middle of the 19 th Century.	
	It is unlikely therefore the land under this site had industrial uses at any time in its history.	
	A trial pit investigation has previously been undertaken which confirm the exact depth of the existing foundations as 600mm below ground level at the back of the property.	
	The basement is within 5m of the footpath. A Line at 45° from the base of the footings does not interect with the pavement. Therefore no highways loading will be allowed for. The front is a drive and it will be designed for a 5kN/m2 surcharge.	
	As the party wall is to be underpinned and will leave the party wall with a deeper footing than the neighbour's other walls, the design should look at the available bearing capacity. As part of the Party Wall agreement a precondition survey will be carried out. The design will consider the impact of the deeper footings.	
Surface flow and	This proposal is considered to be in an area of low risk of	
flooding	flooding.	
	The flow of surface water (above the basement) will need to	
	be considered. A 150mm high protrusion above ground	
	level of the wall from the lightwell will minimise the risk of	
	localized flooding through the lightwell.	
Foundation type	Mass Concrete Underpinning bases.	

Vicinity of trees	Some shrubbery and general vegetation in the neighbouring garden. A mature tree is also present in the neighbouring garden.		
Special precautions	N/A		
due to trees			
Drainage effects on	Drainage Design is Non Structi		
Structure	Note any build over agreemen		
Underground			
	1	The proposed works will not	
	directly affect LUL assets.		
Basement design	Typical loadings and lateral str		
Water Table	Has a soil investigation been c	arried out No	
Water Table Level	Unknown water table level		
	Unknown water table Design	•	
	Basement Depth < 4m : Desig		
	Water table set at ¾ of basem	ent d ept h.	
	Check for uplift for all garde	n basements, bungalows and	
	basements beneath two store	y buildings.	
Undermining of	Check for		
Existing Structure	ructure 5kN/m2 if within 45° of pavement		
	Garden Surcharge 2.5kN/m2		
	1	enty $1.5kN/m2 = + 4kN/m2$ for	
	concrete ground bearing slab.		
	Adjacent properties		
		s within 45° to have additional	
	geotechnical engineers input.		
Soil above garden	.	inimum soil required above a	
structures	garden basement.	1000	
	For trees	1000mm deep	
•	For grass	400mm deep	
	Patios	200mm deep	
		in gardens. Typically stated	
	on planning, but not a building		
Drainage and damp	_	damp proofing is by others.	
	Details are not provide within our brief.		
	Our recommendation is that drained cavity systems are used		
	to habitable basements with pumped sumps. This is a		
· · · · · · · · · · · · · · · · · · ·	specialist contractor design item.		
	Concrete is not designed BS 8007. But where possible BS		
	8007 detailing is observed to help limit crack width		
	concrete.		
Design			
	l Danien avaneli stehilituka V O	K values	
Temporary Works	Design overall stability to K & Walls are designed to be temp		

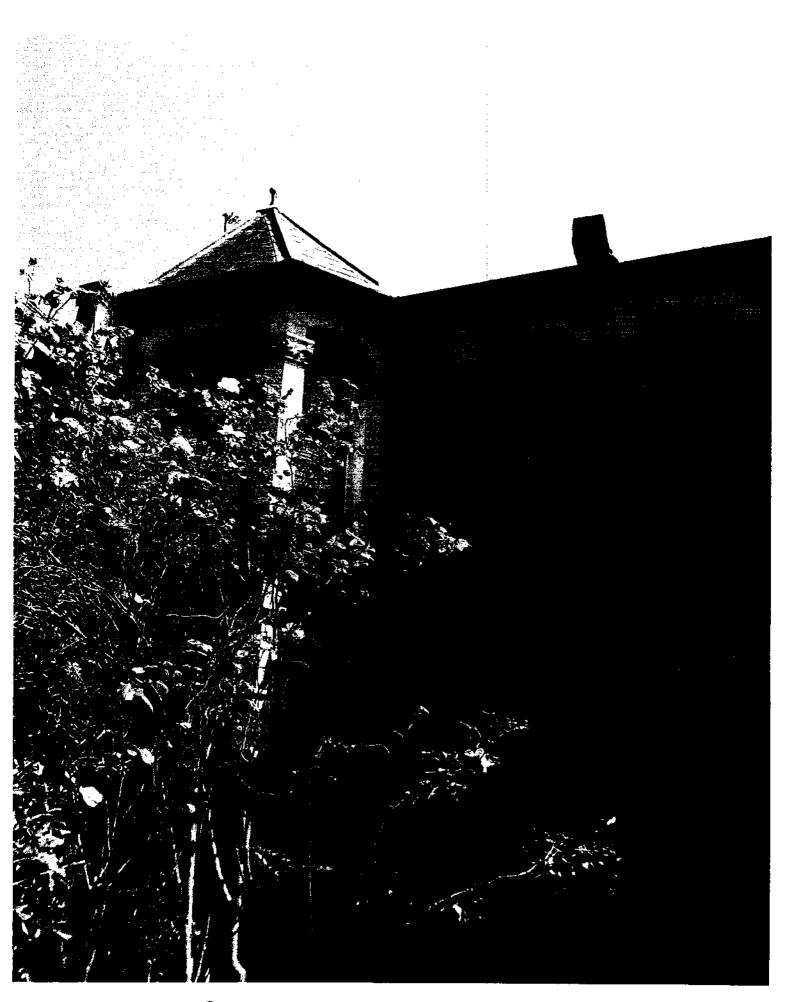
	Temporary propping details will be required for the ground and soil and this must be provided by the contractor. The details should be forwarded to M W Design & Consultin Limited.
Party Wall	Party Wall Notices will be required.
	Works are to be completed to the Party Wall consisting of installing padstones and spreader padstones together with the underpinning works.
Temporary Works	Temporary works are to be contractor's responsibility. An loads required can be provided on request.
	Walls are designed to be temporarily stable. Temporar propping details will be required for the ground and soil an this must be provided by the contractor. Their detail should be forwarded to M W Design & Consulting Limited.
Structural Design Not Supplied	
	Any structural steelwork connections to be designed by steelwork contractor. Contractor to provide/supplifabrication drawings and calculations where necessary.
	Temporarysupport structure is contractor's responsibility. Loads supplied on request.
	Setting out from Architectural information.
	Items not required by Part A of the building regulations Services searches for electrical, drainage, Thames Water Comms, gas etc. by others.
:	

Approving Authority

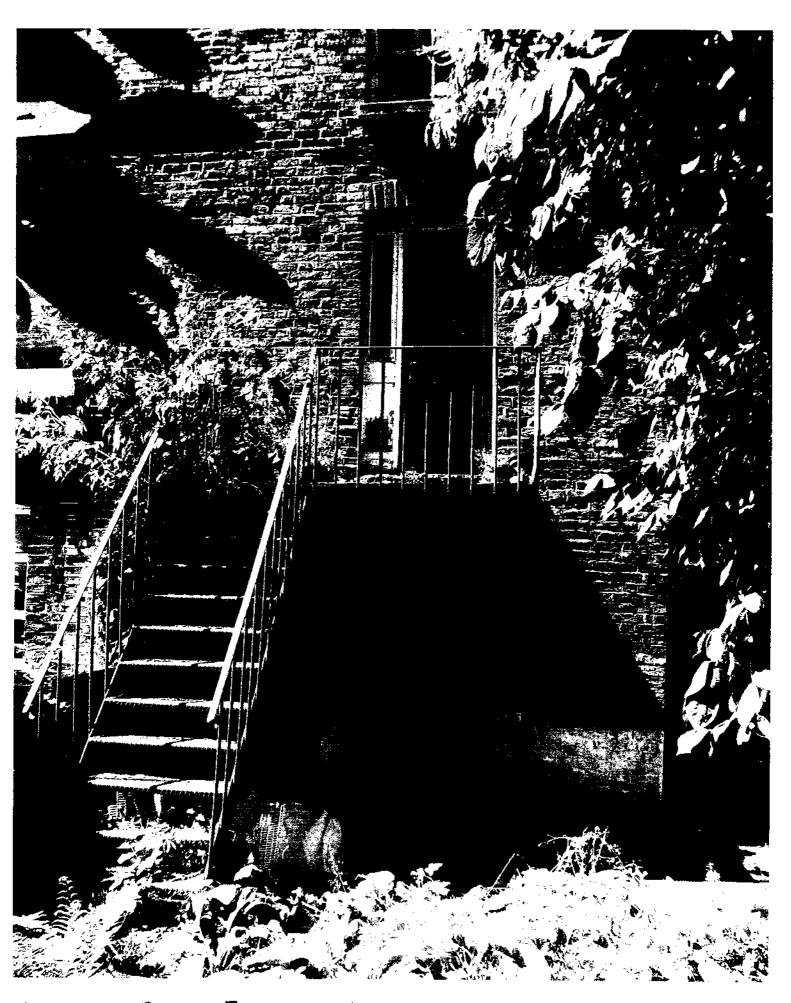
London Borough of Camden Town Hall Extension Argyle Street London WC1H 8NJ

Signed by	
Simon Maddox	lEng, AMIStructE

APPENDIX A SITE PHOTOGRAPHS

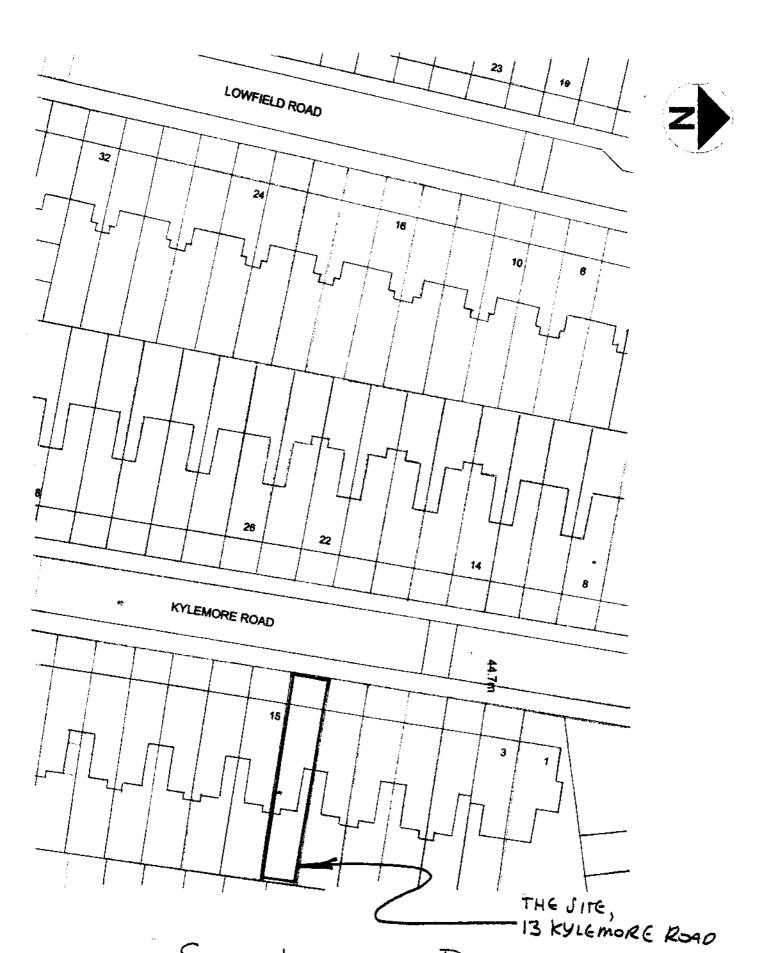


EXISTING FRONT ELEVATION

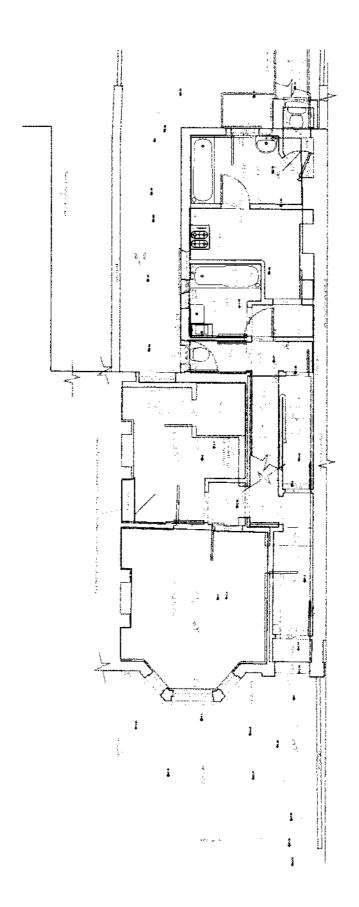


EXISTING REAR ELEVATION

APPENDIX B BLOCK & SITE LOCATION PLANS

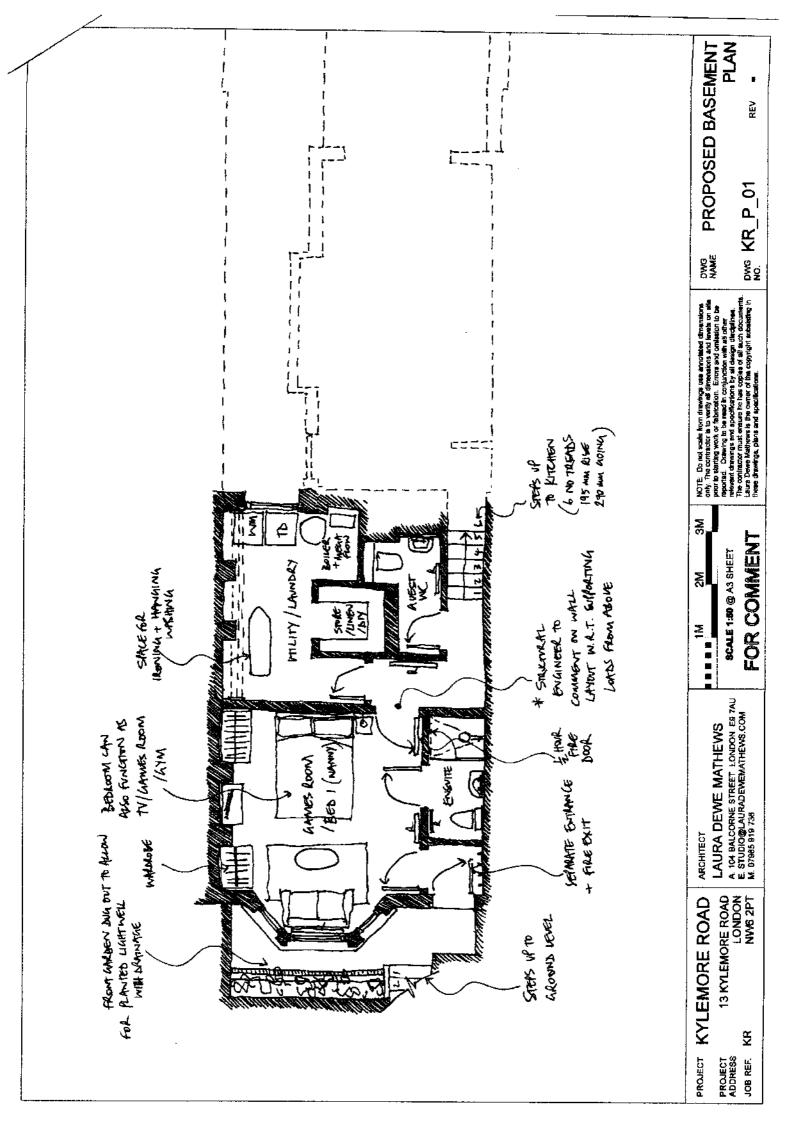


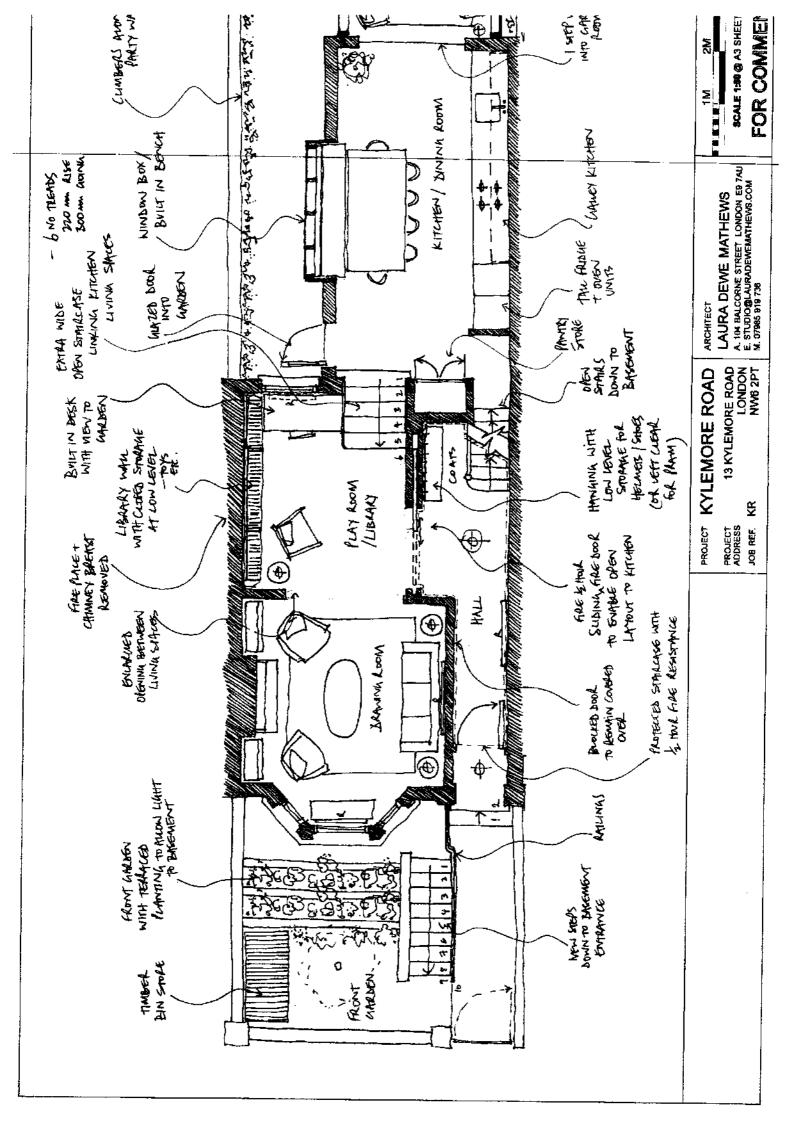
SITE LOCATION PLAN (SCALE 1:500)

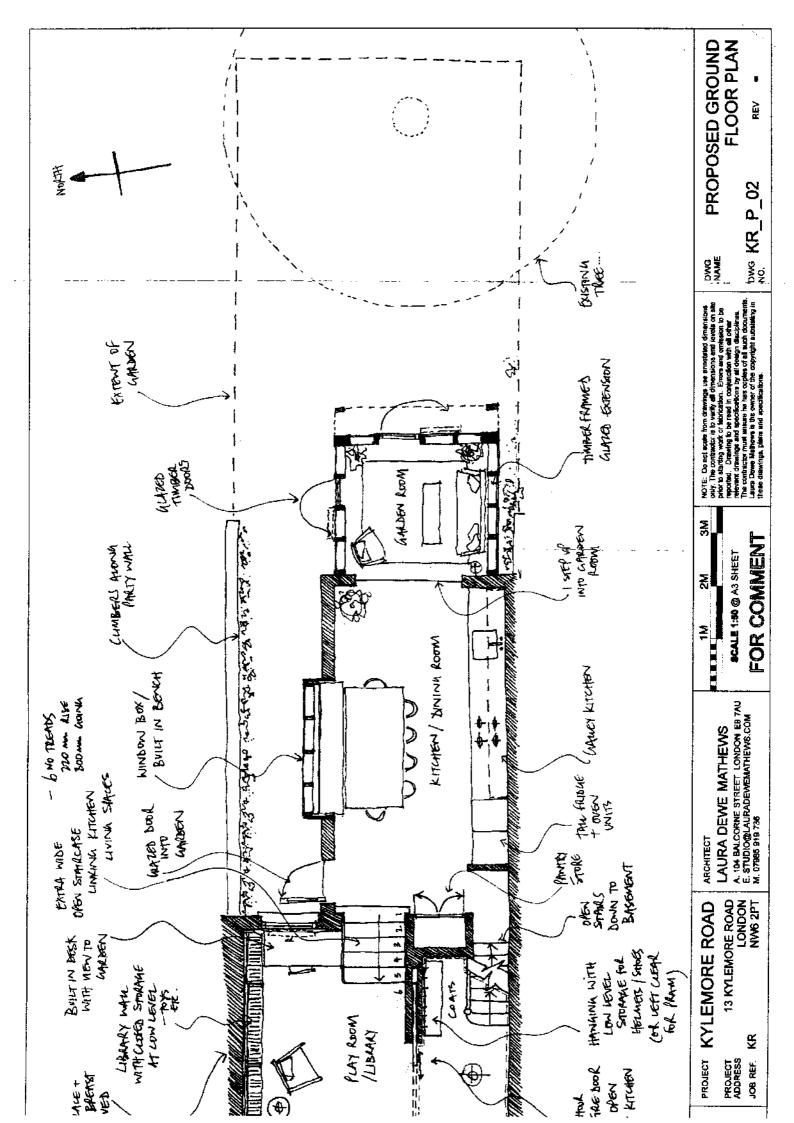


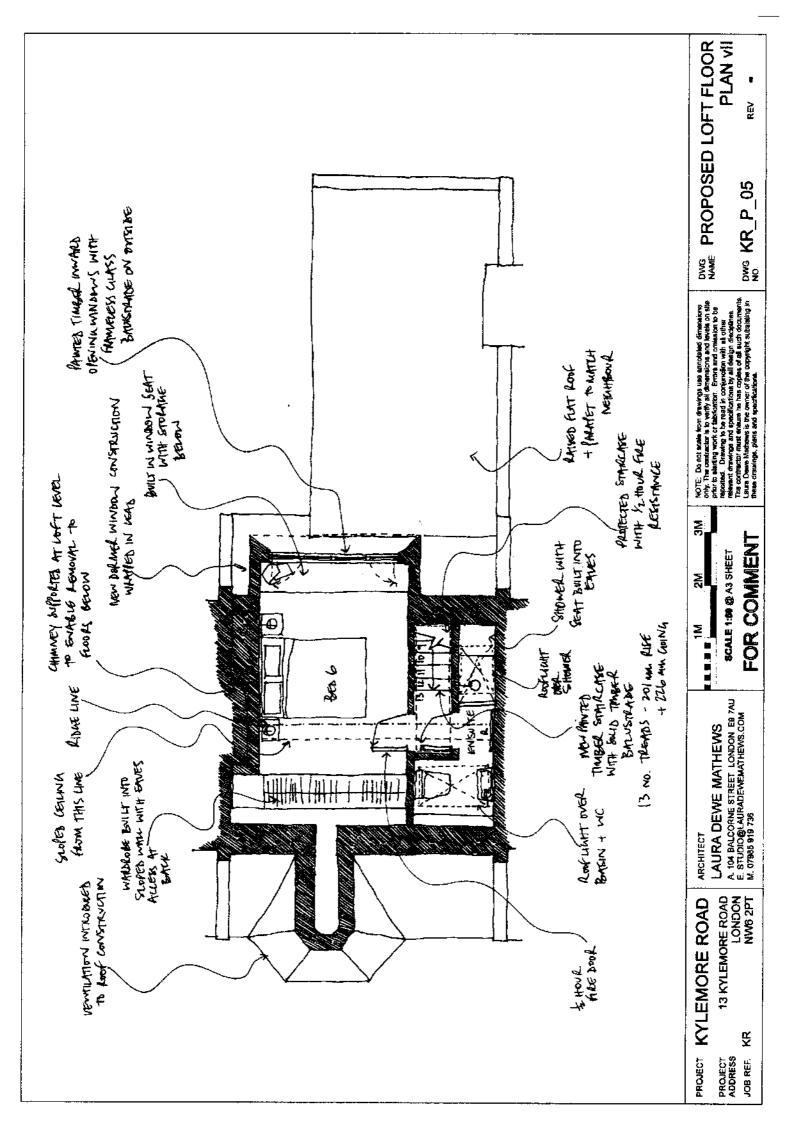
EXISTING BLOCK PLAN (SCALE 1:100)

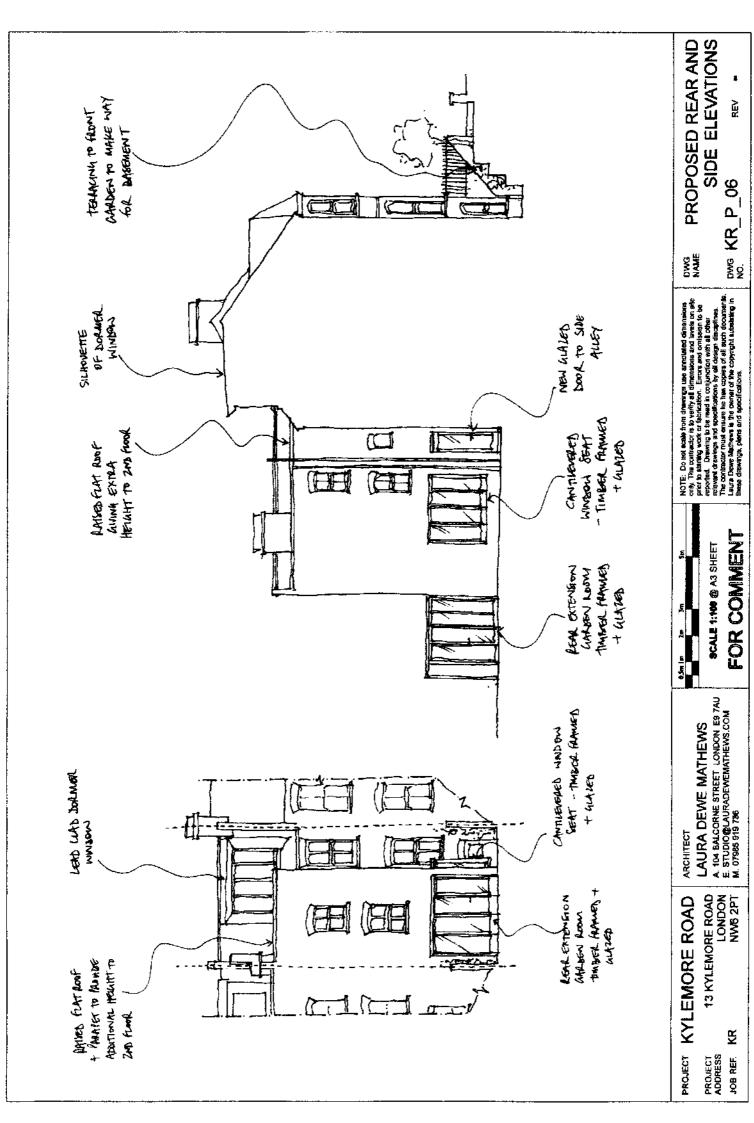
APPENDIX C ARCHITECTS SCHEME PROPOSALS

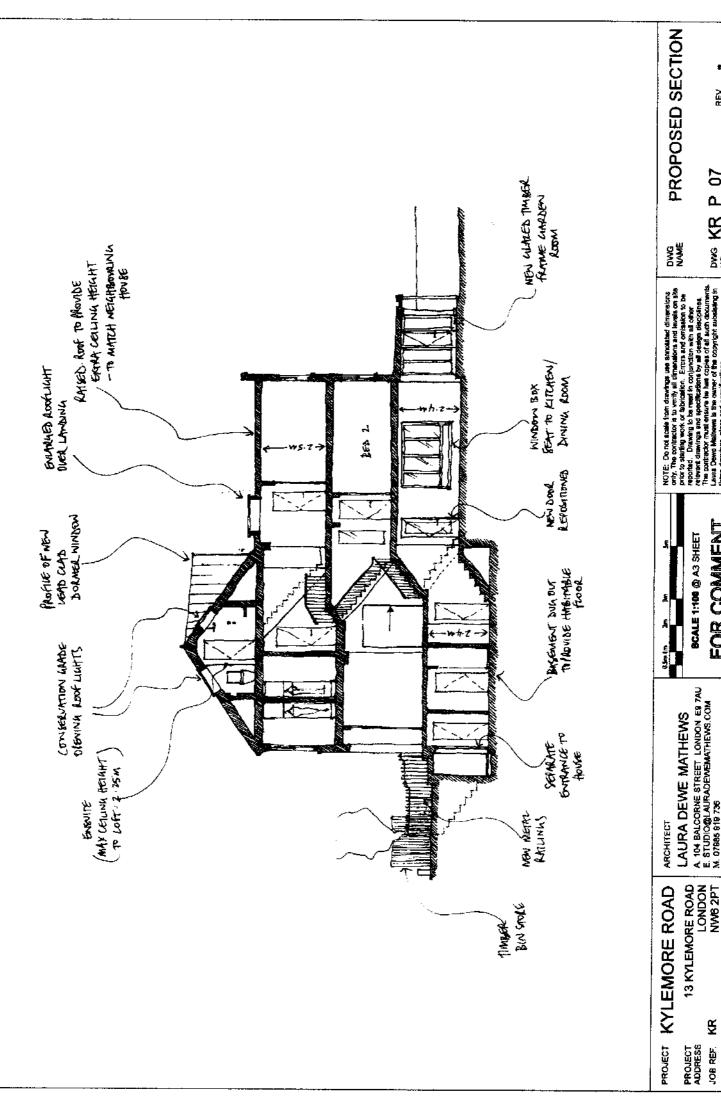












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FOR COMMENT

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JOB REF.

