

# 16 Procter Street Planning Compliance Report

15-1597 16 Procter Street, London, WC1

22/09/2015





# CONTENTS

1.0	INTRODUCTION
2.0	ENVIRONMENTAL NOISE SURVEY AND EQUIPMENT
2.1	Procedure
2.2	Equipment
3.0	RESULTS
4.0	NOISE CRITERIA
5.0	DISCUSSION
5.1	Objective overview
5.2	BS8233 Assessment
5.3	Proposed Mitigation Measures for Plant6
6.0	CONCLUSION

# **List of Attachments**

12841.SP1	Indicative Site Plan Showing Noise Monitoring Position
12841.TH1	Environmental Noise Time History
Appendix A	Glossary of Acoustic Terminology
Appendix B	Acoustic Calculations
Appendix C	Anti-Vibration Mounting Specification Reference Document

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# 1.0 INTRODUCTION

Syntegra Group, Syntegra House, 63 Milford Road, Reading, RG1 8LG has been commissioned by Capital Eagle Limited, to undertake an environmental noise survey at 16 Procter Street, London, WC1V 6NX. The background noise levels measured will be used to determine daytime and night-time noise emission criteria for plant unit installation in agreement with the planning requirements of the London Borough of Camden.

This report presents the overall methodology and results from the environmental survey followed by calculations to demonstrate the feasibility of the plant installation to satisfy the emissions criterion at the closest noise-sensitive receiver and outline mitigation measures as appropriate.

# 2.0 ENVIRONMENTAL NOISE SURVEY AND EQUIPMENT

#### 2.1 Procedure

Automated noise monitoring was undertaken at the site as shown in Site Plan 12841.SP1. The choice of this position was based both on accessibility and on collecting representative noise data in relation to the nearest noise sensitive receiver relative to the proposed plant unit installation. The duration of the survey was between 11:00 on 07/07/2014 and 11:00 on 08/07/2014.

Initial inspection of the site revealed that the background noise profile at the monitoring location was dominated by plant noise from a neighbouring plant installation, as well as road traffic noise from the surrounding roads.

The weather during the course of the survey was generally dry with wind speeds within acceptable tolerances and therefore suitable for the measurement of environmental noise. The measurement procedure complied with ISO 1996-2:2007 Acoustics *"Description, measurement and assessment of environmental noise - Part 2: Determination of environmental noise levels"*.

# 2.2 Equipment

The equipment calibration was verified before and after the survey and no calibration irregularities were observed.

The equipment used was as follows.

- 1 No. Svantek Type 957 Class 1 Sound Level Meter
- B&K Type 4231 Class 1 Calibrator

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# 3.0 RESULTS

The results from the continuous noise monitoring are shown as a time history of  $L_{Aeq}$ ,  $L_{Amax}$ ,  $L_{A10}$  and  $L_{A90}$  averaged over 5 minute sample periods in Figure 12841.TH1.

Minimum background noise levels are shown in Table 3.1.

	Minimum background noise level LA90: 5min dB(A)
Daytime (07:00-23:00)	54
Night-time (23:00-07:00)	51

Table 3.1: Minimum measured background noise levels

# 4.0 NOISE CRITERIA

The criterion of the London Borough of Camden for noise emissions of new plant in this instance is as follows:

"The proposed plant and machinery shall be operated so as to ensure that any noise generated is "not audible" outside the nearest residential premises. To demonstrate inaudibility, you will need to provide calculations that show that the plant noise level is 10dBA below the lowest background level (LA90 (15minutes)) 1m from the nearest residential window, over the proposed operating hours. Tonality must also be taken into consideration."

As the proposed units could be used at any time, we would recommend the night-time criterion to ensure the amenity of the closest residential receiver will be protected.

	Day-time (07:00 to 23:00)	Night-time (23:00 to 07:00)
Noise criterion at nearest receiver	44 dB(A)	41dB(A)

#### Table 4.1: Proposed Noise Emissions Criteria

# 5.0 DISCUSSION

It is understood that the plant installation is comprised of the following unit:

- 3 No Mitsubishi Air Conditioning
- 2 No Air Cooled Chillers Hitachi RCME -70AH1

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The closest noise sensitive receiver to the plant unit location will be a residential window located approximately 7 meters away from the proposed installation at the roof level and approximately 15m away from the proposed installation at level 5.

The sound pressure level as provided by the manufacturer for the unit are shown in Table 5.1.

Unit	Sound Pressure Level dB(A)
Mitsubishi Air Conditioning - Model Unknown	64
Air Cooled Chillers Hitachi RCME -70AH1	81

Table 5.1 Manufacturer's Sound Pressure Level

Please note that the spectral sound pressure level figures are not provided by the manufacturer.

# 5.1 Objective overview

Taking all acoustic corrections into consideration, including distance corrections, the noise level expected at the closest residential window would be as shown in Table 5.2. Detailed calculations are shown in Appendix B.

<b>Receiver</b> - Nearest Noise Sensitive Window	Criterion	Noise Level at Receiver (Residential Window)
Operating hours of plant	41 dB(A)	40 dB(A)

# Table 5.2 Predicted noise level and criterion at nearest noise sensitive location

As shown in Appendix B and Table 5.2, transmission of noise to the nearest sensitive window due to the effects of the plants installation fully satisfies the emissions criteria set based on the requirements of the London Borough of Camden. However, this is providing that the mitigation measures indicated in Section 5.3 are implemented.

# 5.2 BS8233 Assessment

Furthermore, the value of 40 dB(A) is to be considered outside of the building. Windows may be closed or partially closed leading to further attenuation, as follows.

Further calculations have been undertaken to assess whether the noise emissions from the plant unit installation would be expected to meet the recognised British Standard recommendations, in order to further ensure the amenity of nearby noise sensitive receivers.

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British Standard 8233:2014 'Sound insulation and noise reduction for buildings – Code of Practice' gives recommendations for acceptable internal noise levels in residential properties. Assuming worst case conditions, of the closest window being for a bedroom, BS8233:2014 recommends 30 dB(A) as being the value for internal resting/sleeping conditions in night time.

With a calculated external level of 40 dB(A), the residential window itself would need to provide no additional attenuation in order for the conditions to be achieved. According to BS8233:2014, even a partially open window offers 10-15dB attenuation, thus leading to a further reduced interior noise level.

Receiver	Condition Design Range – For resting/sleeping conditions in a bedroom, in BS8233:2014	Noise Level at Receiver (due to plant installation)				
Inside Nearest Residential Space	30dB(A)	30 dB(A)				

Table 5.3 Noise levels and criteria inside nearest residential space

Predicted levels are shown in Table 5.3, with detailed calculations shown in Appendix B. It can therefore be stated that, as well as complying with the requirements of London Borough of Camden, the noise emissions from the plant unit installation would be expected to comfortably meet the most stringent recommendations of the relevant British Standard.

#### 5.3 Proposed Mitigation Measures for Plant

#### Air Cooled Chillers Hitachi RCME -70AH1

In order to reduce noise emissions from the proposed kitchen extract system to within the criteria specified in Section 4.0, an acoustic enclosure should be installed with acoustic louvres. The acoustic louvres should follow the attenuation characteristics shown in Table 5.3.

	Attenuation Levels (dB) in each Frequency Band (at 1m)									
Unit	63Hz	63Hz 125Hz 250Hz 500Hz 1kHz 2kHz 4kHz 8kHz								
Typical 300mm louvres	-6	-7	-10	-13	-17	-19	-13	-11		

#### Table 5.3: Required Attenuation Levels of proposed enclosure

The enclosure would need to incorporate the following elements:

#### **Acoustic Panel Work**

- Outer casing 1.2mm pre-galvanised sheet steel
- Infill 25mm, 45kg/m<sup>3</sup> mineral wool
- Inner skin minimum 0.7mm pre-galvanised expanded metal

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#### **Acoustic Louvres**

- Outer casing 1.2mm pre-galvanised sheet steel
- Infill 45kg/m<sup>3</sup> mineral wool
- Underside of louvre blades minimum 0.7mm pre-galvanised expanded metal (containing the mineral wool infill)

The above can be provided by a manufacturer for noise control products such as Noico, or any similar provider.

# 6.0 CONCLUSION

An environmental noise survey has been undertaken at Eagle House, 16 Procter Street, London, WC1V 6NX, by Syntegra Consulting Ltd between 07/07/2014 and 08/07/2014. The results of the survey have enabled criteria to be set for noise emissions.

Using manufacturer noise data, noise levels are predicted at the nearby noise sensitive receivers for compliance with current requirements.

Calculations show that noise emissions from the proposed unit installation would meet the requirements of the London Borough of Camden, providing that the mitigation measures stipulated in Section 5.3 are implemented.

Checked by Daniela Catalano

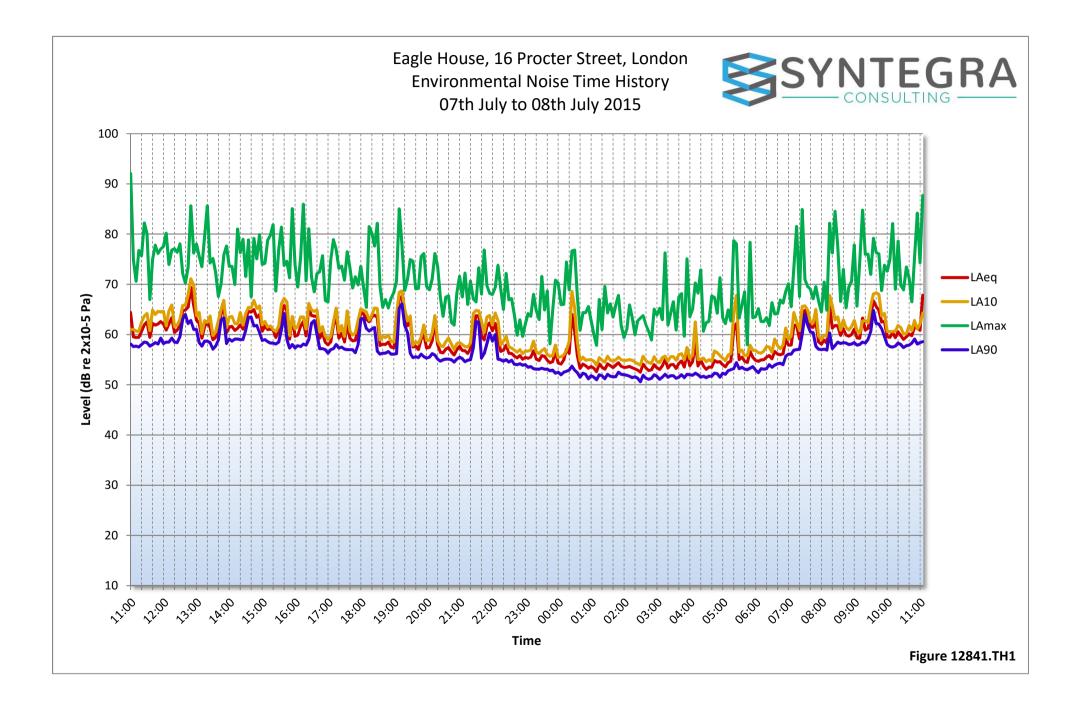
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# APPENDIX A GENERAL ACOUSTIC TERMINOLOGY Decibel scale - dB

In practice, when sound intensity or sound pressure is measured, a logarithmic scale is used in which the unit is the 'decibel', dB. This is derived from the human auditory system, where the dynamic range of human hearing is so large, in the order of 10<sup>13</sup> units, that only a logarithmic scale is the sensible solution for displaying such a range.

# Decibel scale, 'A' weighted - dB(A)

The human ear is less sensitive at frequency extremes, below 125Hz and above 16Khz. A sound level meter models the ears variable sensitivity to sound at different frequencies. This is achieved by building a filter into the Sound Level Meter with a similar frequency response to that of the ear, an A-weighted filter where the unit is dB(A).

# $L_{eq}$

The sound from noise sources often fluctuates widely during a given period of time. An average value can be measured, the equivalent sound pressure level  $L_{eq}$ . The  $L_{eq}$  is the equivalent sound level which would deliver the same sound energy as the actual fluctuating sound measured in the same time period.

# $L_{10}$

This is the level exceeded for no more than 10% of the time. This parameter is often used as a "not to exceed" criterion for noise.

# L<sub>90</sub>

This is the level exceeded for no more than 90% of the time. This parameter is often used as a descriptor of "background noise" for environmental impact studies.

# Lmax

This is the maximum sound pressure level that has been measured over a period.

# **Octave Bands**

In order to completely determine the composition of a sound it is necessary to determine the sound level at each frequency individually. Usually, values are stated in octave bands. The audible frequency region is divided into 11 such octave bands whose centre frequencies are defined in accordance with international standards. These centre frequencies are: 16, 31.5, 63, 125, 250, 500, 1000, 2000, 4000, 8000 and 16000 Hertz.

Environmental noise terms are defined in BS7445, *Description and Measurement of Environmental Noise*.

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# APPENDIX A APPLIED ACOUSTIC TERMINOLOGY Addition of noise from several sources

Noise from different sound sources combines to produce a sound level higher than that from any individual source. Two equally intense sound sources operating together produce a sound level which is 3dB higher than a single source and 4 sources produce a 6dB higher sound level.

# Attenuation by distance

Sound which propagates from a point source in free air attenuates by 6dB for each doubling of distance from the noise source. Sound energy from line sources (e.g. stream of cars) drops off by 3dB for each doubling of distance.

# Subjective impression of noise

Hearing perception is highly individualised. Sensitivity to noise also depends on frequency content, time of occurrence, duration of sound and psychological factors such as emotion and expectations. The following table is a guide to explain increases or decreases in sound levels for many scenarios.

Change in sound level (dB)	Change in perceived loudness
1	Imperceptible
3	Just barely perceptible
6	Clearly noticeable
10	About twice as loud

# Transmission path(s)

The transmission path is the path the sound takes from the source to the receiver. Where multiple paths exist in parallel, the reduction in each path should be calculated and summed at the receiving point. Outdoor barriers can block transmission paths, for example traffic noise. The effectiveness of barriers is dependent on factors such as its distance from the noise source and the receiver, its height and construction.

# **Ground-borne vibration**

In addition to airborne noise levels caused by transportation, construction, and industrial sources there is also the generation of ground-borne vibration to consider. This can lead to structure-borne noise, perceptible vibration, or in rare cases, building damage.

# Sound insulation - Absorption within porous materials

Upon encountering a porous material, sound energy is absorbed. Porous materials which are intended to absorb sound are known as absorbents, and usually absorb 50 to 90% of the energy and are frequency dependent. Some are designed to absorb low frequencies, some for high frequencies and more exotic designs being able to absorb very wide ranges of frequencies. The energy is converted into both mechanical movement and heat within the material; both the stiffness and mass of panels affect the sound insulation performance.

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# APPENDIX B

# Eagle House, 16 Procter Strett, London

# PROPOSED PLANT UNIT EMISSIONS CALCULATIONS

Source: Proposed Plant Unit Installation			F	requen	cy, Hz				
Receiver: Nearest Noise Sensitive Window	63	125	250	500	1k	2k	4k	8k	dB(A)
Manufacturers Sound Pressure Level									
3 No.Mitsubishi Air Conditioning - Model Unknown									
Mitsubishi Air Conditioning (Sound Pressure Level)									64
Correction for number of units 3 No.)			No sp	ectral le	evels a	vailabl	е		5
Correction due to reflections									3
Attenuation provided by distance (min. 13m)									-22
Correction for directivity									-3
Attenuation Provided by building's envelope									-20
Total Sound Pressure Levels from 3 No. Mitsubishi Air Condicioning at									
closest noise sensitive receiver									27
2 No. Air Cooled Chillers Hitachi RCME -70AH1 (Sound Pressure Level)									81
Correction for number of units 2 No.)			No sp	ectral le	evels a	vailabl	e		3
Correction due to reflections			-						3
Attenuation provided by distance (min. 6m)									-16
Correction for directivity									-4
Attenuation Provided by building's envelope									-15
Attenuation provided by acoustic enclosure with louvres									-12
Total Sound Pressure Levels from Air Cooled Chillers Hitachi RCME -									
70AH1 at closest noise sensitive receiver									40
Sound pressure level 1m from closest noise sensitive receiver									40

Design Criterion 41

#### **Receiver: Inside Nearest Residential Window**

		Frequency, Hz							
Source: Proposed plant installation		125	250	500	1k	2k	4k	8k	dB(A)
Sound pressure level outside window									40
Minimum attenuation from partially open window, dB									-10
Sound pressure level inside nearest residential window									30

Design Criterion 30

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# **APPENDIX C**

# ANTI-VIBRATION MOUNTING SPECIFICATION REFERENCE DOCUMENT

# 1.0 General

- 1.1 All mountings shall provide the static deflection, under the equipment weight, shown in the schedules. Mounting selection should allow for any eccentric load distribution or torque reaction, so that the design deflection is achieved on all mountings under the equipment, under operating conditions.
- 1.2 It is the supplier's responsibility to ensure that all mountings offered are suitable for the loads, operating and environmental conditions which will prevail. Particular attention should be paid to mountings which will be exposed to atmospheric conditions to prevent corrosion.
- 1.3 All mountings shall be colour coded, or otherwise marked, to indicate their load capacity, to facilitate identification during installation.

Where use of resilient supports allows omission of pipe flexible connections for vibration/noise isolation, it shall be the Mechanical Service Consultant's or Contractor's responsibility to decide whether such devices are required to compensate for misalignment or thermal strain.

# 2.1 Type A Mounting (Caged Spring Type)

- 2.1.1 Each mounting shall consist of cast or fabricated telescopic top and bottom housings enclosing one or more helical steel springs as the principle isolation elements, and shall incorporate a built-in levelling device. The housing should be designed to permit visual inspection of the springs after installation, i.e. the spring must not be totally enclosed.
- 2.1.2 The springs shall have an outside diameter of not less than 75% of the operating height, and be selected to have at least 50% overload capacity before becoming coil-bound.
- 2.1.3 The bottom plate of each mounting shall have bonded to it a rubber/neoprene pad designed to attenuate any high frequency energy transmitted by the springs.
- 2.1.4 Mountings incorporating snubbers or restraining devices shall be designed so that the snubbing, damping or restraining mechanism is capable of being adjusted to have no significant effect during the normal running of the isolated machine.
- 2.1.5 All nuts, bolts or other elements used for adjustment of a mounting shall incorporate locking mechanisms to prevent the isolator going out of adjustment as a result of vibration or accidental or unauthorised tampering.

# 2.2 Type B Mounting (Open Spring Type)

- 2.2.1 Each mounting shall consist of one or more helical steel springs as the principal isolation elements, and shall incorporate a built-in levelling device.
- 2.2.2 The springs shall be fixed or otherwise securely located to cast or fabricated top and bottom plates, shall have an outside diameter of not less than 75% of the operating height, and shall be selected to have at least 50% overload capacity before becoming coil-bound.
- 2.2.3 The bottom plate shall have bonded to it a rubber/ neoprene pad designed to attenuate any high frequency energy transmitted by the springs.

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# **APPENDIX C**

# 2.3 Type C Mounting (Rubber/Neoprene Type)

Each mounting shall consist of a steel top plate and base plate completely embedded in oil resistant rubber/neoprene. Each mounting shall be capable of being fitted with a levelling device, and should have bolt holes in the base plate and a threaded metal insert in the top plate so that they can be bolted to the floor and equipment where required.

#### 3.0 Plant Bases

#### 3.1 Type A Bases (A.V. Rails)

An A.V. Rail shall comprise a steel beam with two or more height-saving brackets. The steel sections must be sufficiently rigid to prevent undue strain in the equipment and if necessary should be checked by the Structural Engineer.

#### 3.2 Type B Bases (Steel Plant Bases)

Steel plant bases shall comprise an all-welded steel framework of sufficient rigidity to provide adequate support for the equipment, and fitted with isolator height saving brackets. The frame depth shall be approximately 1/10 of the longest dimension of the equipment with a minimum of 150 mm. This form of base may be used as a composite A.V. rail system.

#### 3.3 Type C Bases (Concrete Inertia Base: for use with steel springs)

These shall consist of an all-welded steel pouring frame-work with height saving brackets, and a frame depth of approximately 1/12 of the longest dimension of the equipment, with a minimum of 100 mm. The bottom of the pouring frame should be blanked off, and concrete (2300 kg/m<sup>3</sup>) poured in over steel reinforcing rods positioned 35 mm above the bottom. The inertia base should be sufficiently large to provide support for all parts of the equipment, including any components which over-hang the equipment base, such as suction and discharge elbows on centrifugal pumps.

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