

V&R VINCENT & RYMILL VINCENT & RYMILL LAKESIDE COUNTRY CLUB FRIMLEY GREEN SURREY GU16 6PT	Project				Job Ref.	
	207 GOLDHURST TERRACE NW8				15 F02	
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LOADINGS

PITCHED ROOF

	KN/m²
Tiles	0.70
Felt & battens	0.05
Rafters	<u>0.10</u>
	<u>0.85</u>
30° on plan load D. L.	1.00 KN/m ²
30° Imposed Load	<u>0.75</u> KN/m ²
	1.75 KN/m ²

CEILING

	KN/m²
Ceiling Joists	0.10
Plasterboard	<u>0.15</u>
D. L.	0.25 KN/m ²
I. L. where applicable	<u>0.25</u> KN/m ²
	0.50 KN/m ²

FLAT ROOF

	KN/m²
Felt	0.25
Boards	0.25
Joists & firrings	0.15
Ceiling	<u>0.15</u>
D. L.	0.80 KN/m ²
I. L.	<u>0.75</u> KN/m ²
	1.55 KN/m ²

TIMBER FLOORS

	KN/m²
Boards	0.20
Joists	0.10
Ceiling	<u>0.30</u>
D. L.	0.60 KN/m ²
I. L.	<u>1.50</u> KN/m ²
	2.10 KN/m ²

200 RIBDECK

	KN/m²
Finish	1.80
CONCRETE	<u>4.20</u>
D. L.	6.00 KN/m ²
I. L.	<u>1.50</u> KN/m ²
	7.50 KN/m ²

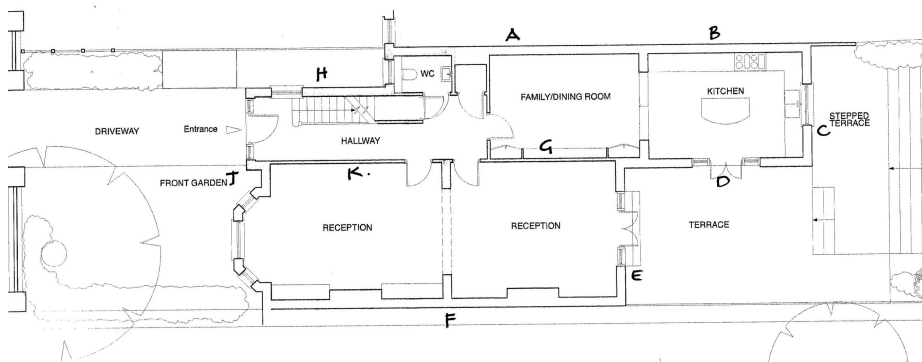
STUDWORK


	0.60KN/m ²
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MASONRY

	KN/m²
102 Brick + plaster	2.20 KN/m ²
215 BRICK + (1 x plaster)	4.60 KN/m ²
215 BRICK + (2 x plaster)	4.80 KN/m ²
330 BRICK (2 x plaster)	7.00 KN/m ²

KEY PLAN



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WALL LOADINGS

WALL A

WALL	10.5 X 4.80	=	50.40	
FLRS DL	2 X 0.6 X 1.75	=	2.10	
FLRS IL	2 X 1.5 X 1.75	=		5.25
ROOF DL	2 X 1	=	2.00	
ROOF IL	2 X 0.75	=		<u>1.50</u>
			54.50KN/m	6.75KN/m

WALL B

WALL	3.5 X 3.3	=	11.55KN/m	
ROOF DL	1.75 X 0.8	=	1.40	
ROOF IL	1.75 X 0.75	=		<u>1.30</u>
			12.95KN/m	1.30KN/m

WALL C

WALL	3.5 X 3.3 X 80%	=	9.5KN/m	
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WALL D

WALL	3.5 X 3.3 X 80%	=	9.25KN/m	
ROOF DL	1.75 X 0.8	=	1.40	
ROOF IL	1.75 X 0.75	=		<u>1.30</u>
			12.95KN/m	1.30KN/m

WALL E

WALL	7.5 X 4.6 X 70%	=	24.15	
ROOF	3 X 1	=	3.00	
ROOF	3 X 0.75	=		<u>2.25</u>
			27.15KN/m	2.25KN/m

WALL F


WALL	10.5 X 4.80	=	50.40	
FLRS DL	2 X 0.6 X 2.25	=	2.70	
FLRS IL	2 X 1.5 X 2.25	=		6.75
ROOF DL	2 X 1	=	2.00	
ROOF IL	2 X 0.75	=		<u>1.50</u>
			55.10KN/m	8.25KN/m

CHIMNEY BREASTS

MASONRY	2.4 X 1.25 X 12.5	=	37.50KN/m	
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WALL G

WALL	2.6 X 6.5	=	16.90	
STUD	0.6 X 2.5	=	1.50	
FLRS DL	4 X 0.6 X 2	=	4.80	
FLRS IL	4 X 1.5 X 2	=		<u>12.00</u>
			23.20KN/m	12.00KN/m

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WALL K

WALL	2.6 X 6.5	=	16.90	
STUD	0.6 X 2.5	=	1.50	
FLRS DL	3 X 0.6 X 2	=	3.60	
FLRS IL	3 X 1.5 X 2	=	_____	<u>9.00</u>
			22.00KN/m	9.00KN/m

WALL H

WALL	10.5 X 4.80	=	50.40	
FLRS DL	2 X 0.6 X 1	=	1.20	
FLRS IL	2 X 1.5 X 1	=		3.00
ROOF DL	2 X 1	=	2.00	
ROOF IL	2 X 0.75	=	_____	<u>1.50</u>
			53.6KN/m	4.50KN/m

WALL J

WALL	7 X 4.6 X 70%	=	22.50KN/m	
ROOF DL	3 X 1	=	3.00	
ROOF IL	3 X 0.75	=	_____	<u>2.25</u>
			25.50KN/m	2.25KN/m

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WALLS AND BASES

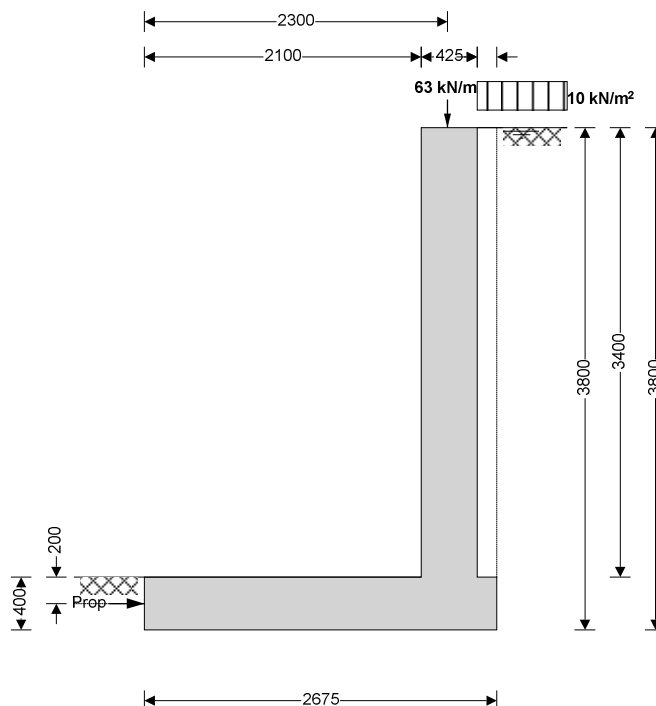
PARTY WALLS – WALLS A AND F

DL = 55.1kN/m, IL = 8.25kN/m

RETAINING WALL ANALYSIS & DESIGN (BS8002)

RETAINING WALL ANALYSIS (BS 8002:1994)

TEDDS calculation version 1.2.01.06



Wall details

Retaining wall type

Height of wall stem

Length of toe

Overall length of base

Height of retaining wall

Depth of downstand

Position of downstand

Depth of cover in front of wall

Height of ground water

Density of wall construction

Angle of soil surface

Mobilisation factor

Moist density

Design shear strength

Design shear strength

Moist density

Cantilever

$h_{\text{stem}} = 3400$ mm

$l_{\text{toe}} = 2100$ mm

$l_{\text{base}} = 2675$ mm

$h_{\text{wall}} = 3800$ mm

$d_{\text{ds}} = 0$ mm

$l_{\text{ds}} = 1100$ mm

$d_{\text{cover}} = 0$ mm

$h_{\text{water}} = 3800$ mm

$\gamma_{\text{wall}} = 23.6$ kN/m³

$\beta = 0.0$ deg

$M = 1.5$

$\gamma_m = 18.0$ kN/m³

$\phi' = 24.2$ deg

$\phi'_b = 24.2$ deg

$\gamma_{mb} = 18.0$ kN/m³

Wall stem thickness

Length of heel

Base thickness

Thickness of downstand

Unplanned excavation depth

Density of water

Density of base construction

Effective height at back of wall

Saturated density

Angle of wall friction

Design base friction

Allowable bearing

$t_{\text{wall}} = 425$ mm

$l_{\text{heel}} = 150$ mm

$t_{\text{base}} = 400$ mm

$t_{\text{ds}} = 400$ mm

$d_{\text{exc}} = 200$ mm

$\gamma_{\text{water}} = 9.81$ kN/m³

$\gamma_{\text{base}} = 23.6$ kN/m³


$h_{\text{eff}} = 3800$ mm

$\gamma_s = 21.0$ kN/m³

$\delta = 0.0$ deg

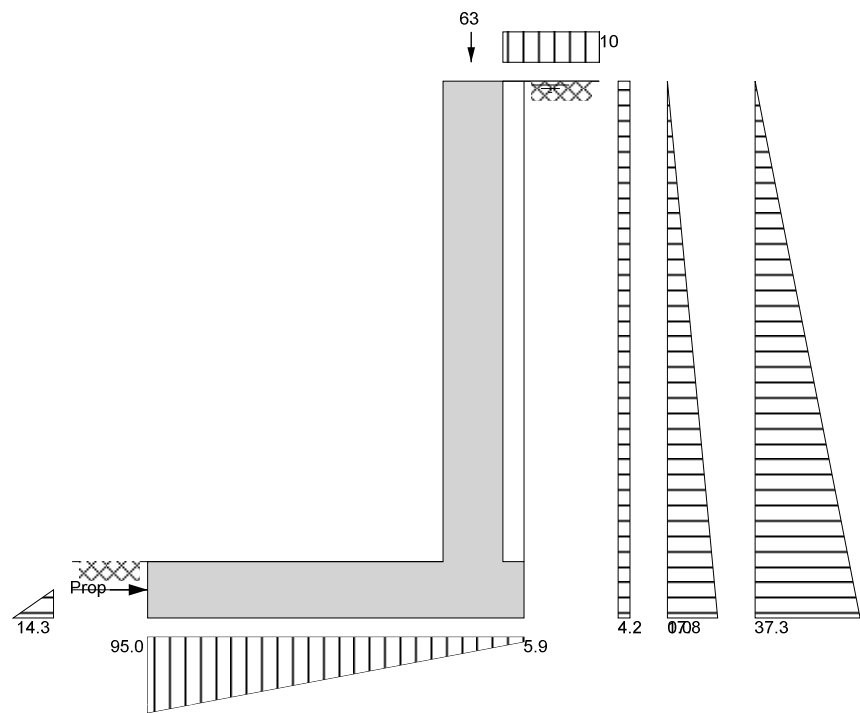
$\delta_b = 18.6$ deg

$P_{\text{bearing}} = 150$ kN/m²

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Using Coulomb theory

Active pressure	$K_a = 0.419$	Passive pressure	$K_p = 4.187$
At-rest pressure	$K_0 = 0.590$		
Loading details			
Surcharge load	Surcharge = 10.0 kN/m ²		
Vertical dead load	$W_{dead} = 55.1$ kN/m	Vertical live load	$W_{live} = 8.3$ kN/m
Horizontal dead load	$F_{dead} = 0.0$ kN/m	Horizontal live load	$F_{live} = 0.0$ kN/m
Position of vertical load	$l_{load} = 2300$ mm	Height of horizontal load	$h_{load} = 0$ mm



Loads shown in kN/m, pressures shown in kN/m²

Calculate propping force

Propping force	$F_{prop} = 77.0$ kN/m
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Check bearing pressure

Total vertical reaction	$R = 134.9$ kN/m	Distance to reaction	$x_{bar} = 944$ mm
Eccentricity of reaction	$e = 394$ mm		

Reaction acts within middle third of base

Bearing pressure at toe	$p_{toe} = 95.0$ kN/m ²	Bearing pressure at heel	$p_{heel} = 5.9$ kN/m ²
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PASS - Maximum bearing pressure is less than allowable bearing pressure

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RETAINING WALL DESIGN (BS 8002:1994)

TEDDS calculation version 1.2.01.06

Ultimate limit state load factors

Dead load factor $\gamma_{f_d} = 1.4$ Live load factor $\gamma_{f_l} = 1.6$
 Earth pressure factor $\gamma_{f_e} = 1.4$

Calculate propping force

Propping force $F_{prop} = 77.0$ kN/m

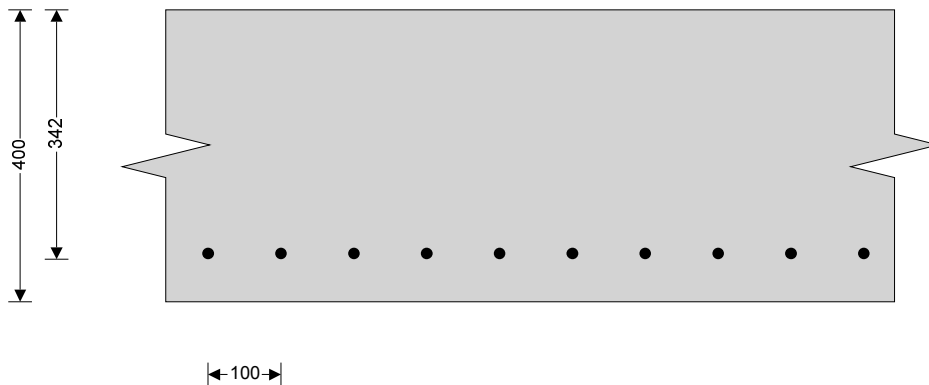
Design of reinforced concrete retaining wall toe (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40$ N/mm² Strength of reinforcement $f_y = 500$ N/mm²

Base details

Minimum reinforcement $k = 0.13$ % Cover in toe $c_{toe} = 50$ mm



Design of retaining wall toe

Shear at heel $V_{toe} = 163.1$ kN/m Moment at heel $M_{toe} = 273.6$ kNm/m
Compression reinforcement is not required

Check toe in bending

Reinforcement provided **16 mm dia.bars @ 100 mm centres**
 Area required $A_{s_toe_req} = 1977.0$ mm²/m Area provided $A_{s_toe_prov} = 2011$ mm²/m
PASS - Reinforcement provided at the retaining wall toe is adequate

Check shear resistance at toe

Design shear stress $v_{toe} = 0.477$ N/mm² Allowable shear stress $v_{adm} = 5.000$ N/mm²
PASS - Design shear stress is less than maximum shear stress
 Concrete shear stress $v_{c_toe} = 0.644$ N/mm²
 $v_{toe} < v_{c_toe}$ - No shear reinforcement required


Design of reinforced concrete retaining wall heel (BS 8002:1994)

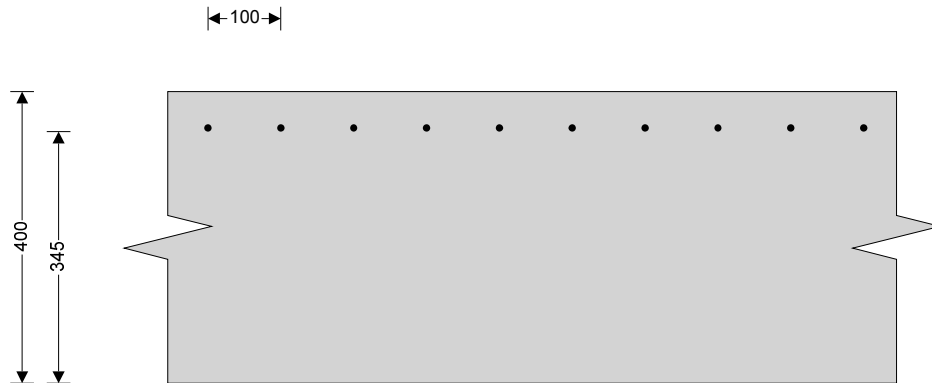
Material properties

Strength of concrete $f_{cu} = 40$ N/mm² Strength of reinforcement $f_y = 500$ N/mm²

Base details

Minimum reinforcement $k = 0.13$ % Cover in heel $c_{heel} = 50$ mm

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Design of retaining wall heel

Shear at heel

$$V_{\text{heel}} = 19.4 \text{ kN/m}$$

Moment at heel

$$M_{\text{heel}} = 5.9 \text{ kNm/m}$$

Compression reinforcement is not required

Check heel in bending

Reinforcement provided

B785 mesh

Area required

$$A_{s_{\text{heel_req}}} = 520.0 \text{ mm}^2/\text{m}$$

Area provided

$$A_{s_{\text{heel_prov}}} = 785 \text{ mm}^2/\text{m}$$

PASS - Reinforcement provided at the retaining wall heel is adequate

Check shear resistance at heel

Design shear stress

$$v_{\text{heel}} = 0.056 \text{ N/mm}^2$$

Allowable shear stress

$$v_{\text{adm}} = 5.000 \text{ N/mm}^2$$

PASS - Design shear stress is less than maximum shear stress

Concrete shear stress

$$v_{c_{\text{heel}}} = 0.468 \text{ N/mm}^2$$

$v_{\text{heel}} < v_{c_{\text{heel}}}$ - No shear reinforcement required

Design of reinforced concrete retaining wall stem (BS 8002:1994)

Material properties

Strength of concrete

$$f_{cu} = 40 \text{ N/mm}^2$$

Strength of reinforcement

$$f_y = 500 \text{ N/mm}^2$$

Wall details

Minimum reinforcement

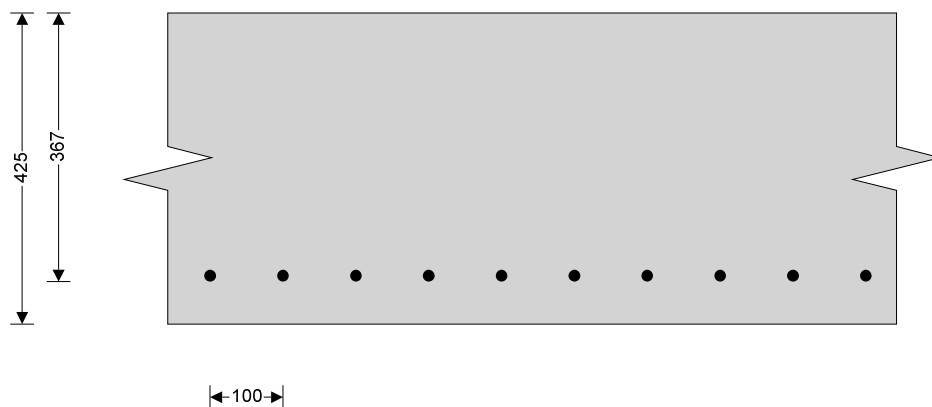
$$k = 0.13 \%$$

Cover in stem

$$c_{\text{stem}} = 50 \text{ mm}$$

Cover in wall

$$c_{\text{wall}} = 50 \text{ mm}$$



Design of retaining wall stem


Shear at base of stem

$$V_{\text{stem}} = 24.1 \text{ kN/m}$$

Moment at base of stem

$$M_{\text{stem}} = 211.5 \text{ kNm/m}$$

Compression reinforcement is not required

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Check wall stem in bending

Reinforcement provided **16 mm dia.bars @ 100 mm centres**

Area required $A_{s_stem_req} = 1394.6 \text{ mm}^2/\text{m}$ Area provided $A_{s_stem_prov} = 2011 \text{ mm}^2/\text{m}$
PASS - Reinforcement provided at the retaining wall stem is adequate


Check shear resistance at wall stem

Design shear stress $v_{stem} = 0.066 \text{ N/mm}^2$ Allowable shear stress $v_{adm} = 5.000 \text{ N/mm}^2$
PASS - Design shear stress is less than maximum shear stress

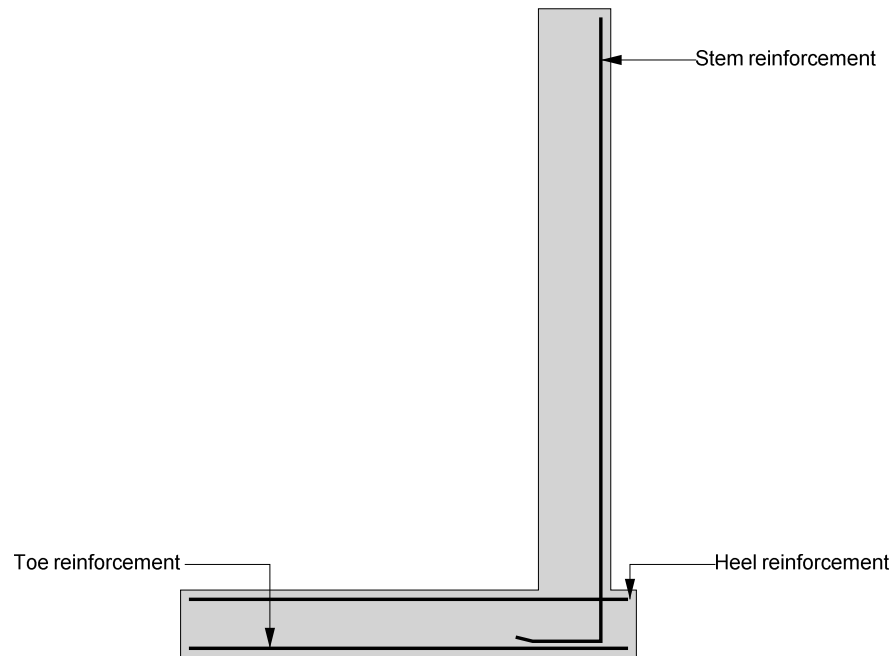
Concrete shear stress $v_{c_stem} = 0.618 \text{ N/mm}^2$
 $v_{stem} < v_{c_stem}$ - No shear reinforcement required

Check retaining wall deflection

Max span/depth ratio $ratio_{max} = 9.65$ Actual span/depth ratio $ratio_{act} = 9.26$
PASS - Span to depth ratio is acceptable

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Indicative retaining wall reinforcement diagram



Toe bars - 16 mm dia.@ 100 mm centres - (2011 mm²/m)

Heel mesh - B785 - (785 mm²/m)

Stem bars - 16 mm dia.@ 100 mm centres - (2011 mm²/m)

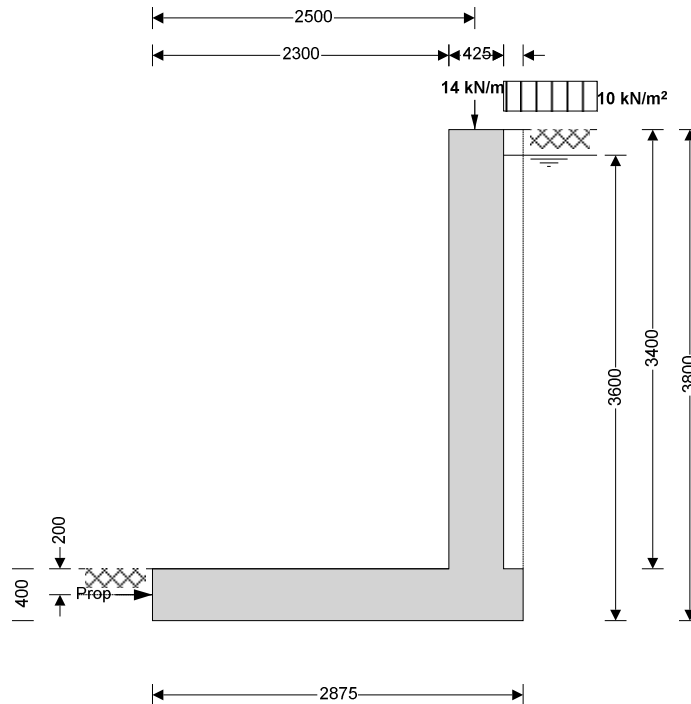
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WALLS B

RETAINING WALL ANALYSIS & DESIGN (BS8002)

RETAINING WALL ANALYSIS (BS 8002:1994)

TEDDS calculation version 1.2.01.06



Wall details

Retaining wall type

Height of wall stem

Length of toe

Overall length of base

Height of retaining wall

Depth of downstand

Position of downstand

Depth of cover in front of wall

Height of ground water

Density of wall construction

Angle of soil surface

Mobilisation factor

Moist density

Design shear strength

Design shear strength

Moist density

Using Coulomb theory

Active pressure

At-rest pressure

Cantilever

$h_{\text{stem}} = 3400$ mm

$l_{\text{toe}} = 2300$ mm

$l_{\text{base}} = 2875$ mm

$h_{\text{wall}} = 3800$ mm

$d_{\text{ds}} = 0$ mm

$l_{\text{ds}} = 1900$ mm

$d_{\text{cover}} = 0$ mm

$h_{\text{water}} = 3600$ mm

$\gamma_{\text{wall}} = 23.6$ kN/m³

$\beta = 0.0$ deg

$M = 1.5$

$\gamma_m = 18.0$ kN/m³

$\phi' = 24.2$ deg

$\phi'_b = 24.2$ deg

$\gamma_{mb} = 18.0$ kN/m³

$K_a = 0.419$

$K_0 = 0.590$

Wall stem thickness

Length of heel

Base thickness

Thickness of downstand

Unplanned excavation depth

Density of water

Density of base construction

Effective height at back of wall

Saturated density

Angle of wall friction

Design base friction

Allowable bearing

Passive pressure

$t_{\text{wall}} = 425$ mm

$l_{\text{heel}} = 150$ mm

$t_{\text{base}} = 400$ mm

$t_{\text{ds}} = 400$ mm

$d_{\text{exc}} = 200$ mm

$\gamma_{\text{water}} = 9.81$ kN/m³

$\gamma_{\text{base}} = 23.6$ kN/m³

$h_{\text{eff}} = 3800$ mm

$\gamma_s = 21.0$ kN/m³

$\delta = 0.0$ deg

$\delta_b = 18.6$ deg

$P_{\text{bearing}} = 150$ kN/m²

$K_p = 4.187$

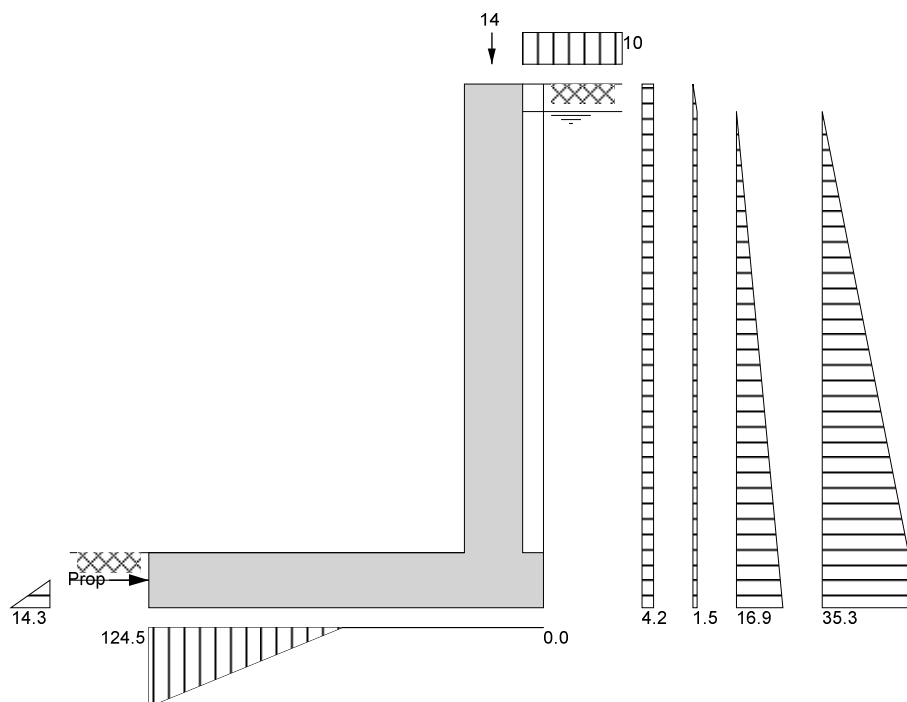


VINCENT & RYMILL
LAKESIDE COUNTRY CLUB
FRIMLEY GREEN
SURREY GU16 6PT

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Loading details

Surcharge load	Surcharge = 10.0 kN/m²		
Vertical dead load	$W_{\text{dead}} = \mathbf{13.0 \text{ kN/m}}$	Vertical live load	$W_{\text{live}} = \mathbf{1.3 \text{ kN/m}}$
Horizontal dead load	$F_{\text{dead}} = \mathbf{0.0 \text{ kN/m}}$	Horizontal live load	$F_{\text{live}} = \mathbf{0.0 \text{ kN/m}}$
Position of vertical load	$l_{\text{load}} = \mathbf{2500 \text{ mm}}$	Height of horizontal load	$h_{\text{load}} = \mathbf{0 \text{ mm}}$



Loads shown in kN/m, pressures shown in kN/m²

Calculate propping force

Propping force $F_{\text{prop}} = \mathbf{85.4 \text{ kN/m}}$


Check bearing pressure

Total vertical reaction $R = \mathbf{87.7 \text{ kN/m}}$ Distance to reaction $x_{\text{bar}} = \mathbf{469 \text{ mm}}$
Eccentricity of reaction $e = \mathbf{968 \text{ mm}}$

Bearing pressure at toe $p_{\text{toe}} = \mathbf{124.5 \text{ kN/m}^2}$ Bearing pressure at heel $p_{\text{heel}} = \mathbf{0.0 \text{ kN/m}^2}$

Reaction acts outside middle third of base

PASS - Maximum bearing pressure is less than allowable bearing pressure

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RETAINING WALL DESIGN (BS 8002:1994)

TEDDS calculation version 1.2.01.06

Ultimate limit state load factors

Dead load factor $\gamma_{f_d} = 1.4$ Live load factor $\gamma_{f_l} = 1.6$
 Earth pressure factor $\gamma_{f_e} = 1.4$

Calculate propping force

Propping force $F_{prop} = 85.4$ kN/m

Design of reinforced concrete retaining wall toe (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40$ N/mm² Strength of reinforcement $f_y = 500$ N/mm²

Base details

Minimum reinforcement $k = 0.13$ % Cover in toe $c_{toe} = 50$ mm

Design of retaining wall toe

Shear at heel $V_{toe} = 92.9$ kN/m Moment at heel $M_{toe} = 261.6$ kNm/m
Compression reinforcement is not required

Check toe in bending

Reinforcement provided **16 mm dia.bars @ 100 mm centres**
 Area required $A_{s_toe_req} = 1884.0$ mm²/m Area provided $A_{s_toe_prov} = 2011$ mm²/m
PASS - Reinforcement provided at the retaining wall toe is adequate

Check shear resistance at toe

Design shear stress $v_{toe} = 0.272$ N/mm² Allowable shear stress $v_{adm} = 5.000$ N/mm²
PASS - Design shear stress is less than maximum shear stress
 Concrete shear stress $v_{c_toe} = 0.644$ N/mm²
 $v_{toe} < v_{c_toe}$ - No shear reinforcement required

Design of reinforced concrete retaining wall heel (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40$ N/mm² Strength of reinforcement $f_y = 500$ N/mm²

Base details

Minimum reinforcement $k = 0.13$ % Cover in heel $c_{heel} = 50$ mm

Design of retaining wall heel


Shear at heel $V_{heel} = 19.3$ kN/m Moment at heel $M_{heel} = 5.8$ kNm/m
Compression reinforcement is not required

Check heel in bending

Reinforcement provided **B785 mesh**
 Area required $A_{s_heel_req} = 520.0$ mm²/m Area provided $A_{s_heel_prov} = 785$ mm²/m
PASS - Reinforcement provided at the retaining wall heel is adequate

Check shear resistance at heel

Design shear stress $v_{heel} = 0.056$ N/mm² Allowable shear stress $v_{adm} = 5.000$ N/mm²
PASS - Design shear stress is less than maximum shear stress
 Concrete shear stress $v_{c_heel} = 0.468$ N/mm²
 $v_{heel} < v_{c_heel}$ - No shear reinforcement required

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Design of reinforced concrete retaining wall stem (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40 \text{ N/mm}^2$ Strength of reinforcement $f_y = 500 \text{ N/mm}^2$

Wall details

Minimum reinforcement $k = 0.13 \%$

Cover in stem $c_{stem} = 50 \text{ mm}$ Cover in wall $c_{wall} = 50 \text{ mm}$

Design of retaining wall stem

Shear at base of stem $V_{stem} = 5.8 \text{ kN/m}$ Moment at base of stem $M_{stem} = 202.7 \text{ kNm/m}$

Compression reinforcement is not required

Check wall stem in bending

Reinforcement provided **16 mm dia.bars @ 100 mm centres**

Area required $A_{s_stem_req} = 1336.8 \text{ mm}^2/\text{m}$ Area provided $A_{s_stem_prov} = 2011 \text{ mm}^2/\text{m}$

PASS - Reinforcement provided at the retaining wall stem is adequate

Check shear resistance at wall stem

Design shear stress $v_{stem} = 0.016 \text{ N/mm}^2$ Allowable shear stress $v_{adm} = 5.000 \text{ N/mm}^2$

PASS - Design shear stress is less than maximum shear stress


Concrete shear stress $v_{c_stem} = 0.618 \text{ N/mm}^2$

$v_{stem} < v_{c_stem}$ - No shear reinforcement required

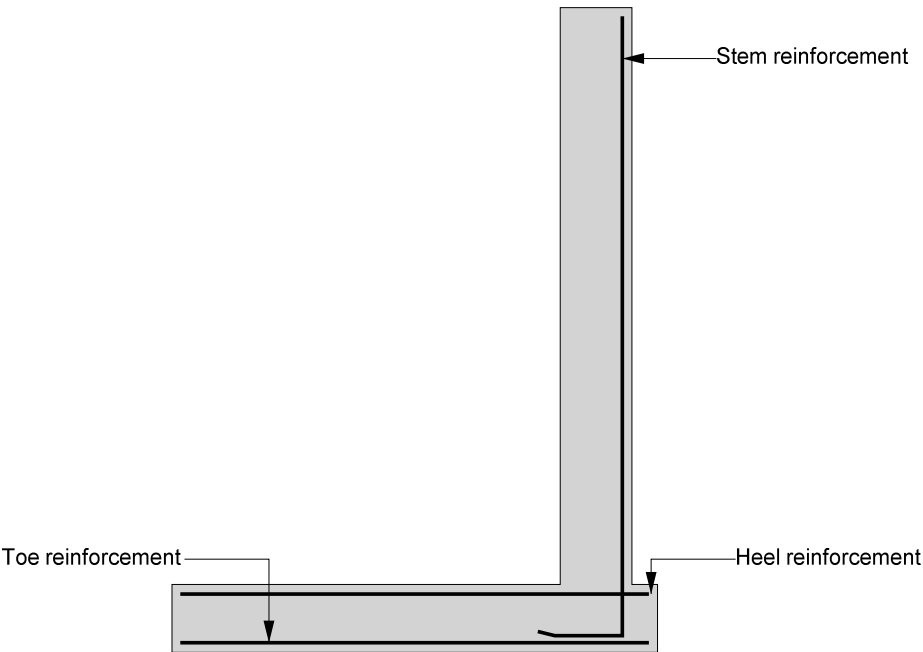
Check retaining wall deflection

Max span/depth ratio $ratio_{max} = 10.04$ Actual span/depth ratio $ratio_{act} = 9.26$

PASS - Span to depth ratio is acceptable

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Indicative retaining wall reinforcement diagram



Toe bars - 16 mm dia.@ 100 mm centres - (2011 mm²/m)
 Heel mesh - B785 - (785 mm²/m)
 Stem bars - 16 mm dia.@ 100 mm centres - (2011 mm²/m)

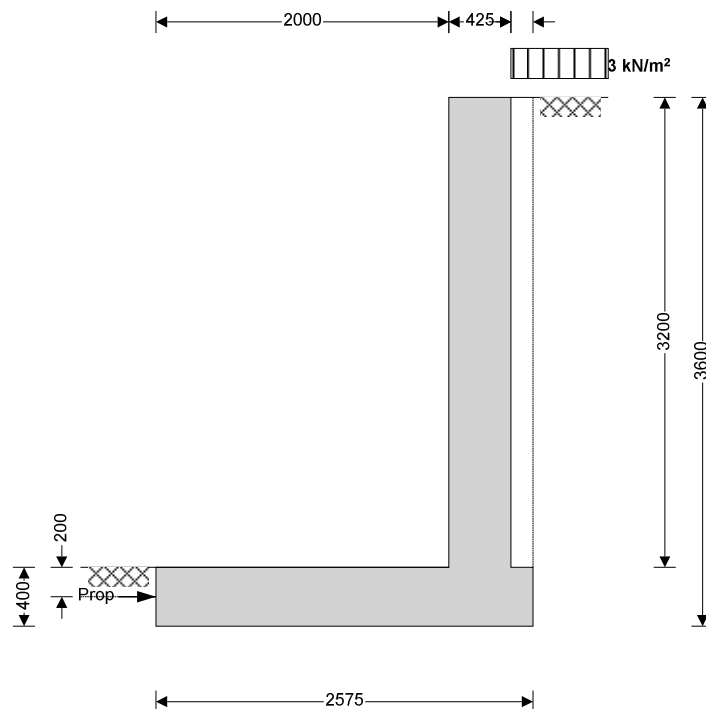
V&R VINCENT & RYMILL VINCENT & RYMILL LAKESIDE COUNTRY CLUB FRIMLEY GREEN SURREY GU16 6PT	Project		207 GOLDHURST TERRACE NW8		Job Ref.		15 F02
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TYPICAL LIGHT WELL WALL

RETAINING WALL ANALYSIS & DESIGN (BS8002)

RETAINING WALL ANALYSIS (BS 8002:1994)

TEDDS calculation version 1.2.01.06



Wall details

Retaining wall type

Height of wall stem

Length of toe

Overall length of base

Height of retaining wall

Depth of downstand

Position of downstand

Depth of cover in front of wall

Height of ground water

Density of wall construction

Angle of soil surface

Mobilisation factor

Moist density

Design shear strength

Design shear strength

Moist density

Cantilever

$h_{\text{stem}} = 3200$ mm

$l_{\text{toe}} = 2000$ mm

$l_{\text{base}} = 2575$ mm

$h_{\text{wall}} = 3600$ mm

$d_{\text{ds}} = 0$ mm

$l_{\text{ds}} = 1900$ mm

$d_{\text{cover}} = 0$ mm

$h_{\text{water}} = 0$ mm

$\gamma_{\text{wall}} = 23.6$ kN/m³

$\beta = 0.0$ deg

$M = 1.5$

$\gamma_m = 18.0$ kN/m³

$\phi' = 24.2$ deg

$\phi'_b = 24.2$ deg

$\gamma_{\text{mb}} = 18.0$ kN/m³

Wall stem thickness

Length of heel

Base thickness

Thickness of downstand

Unplanned excavation depth

Density of water

Density of base construction

Effective height at back of wall

Saturated density

Angle of wall friction

Design base friction

Allowable bearing

$t_{\text{wall}} = 425$ mm

$l_{\text{heel}} = 150$ mm

$t_{\text{base}} = 400$ mm

$t_{\text{ds}} = 400$ mm

$d_{\text{exc}} = 200$ mm

$\gamma_{\text{water}} = 9.81$ kN/m³

$\gamma_{\text{base}} = 23.6$ kN/m³

$h_{\text{eff}} = 3600$ mm

$\gamma_s = 21.0$ kN/m³

$\delta = 0.0$ deg

$\delta_b = 18.6$ deg

$P_{\text{bearing}} = 150$ kN/m²

Using Coulomb theory

Active pressure


At-rest pressure

$K_a = 0.419$

$K_0 = 0.590$

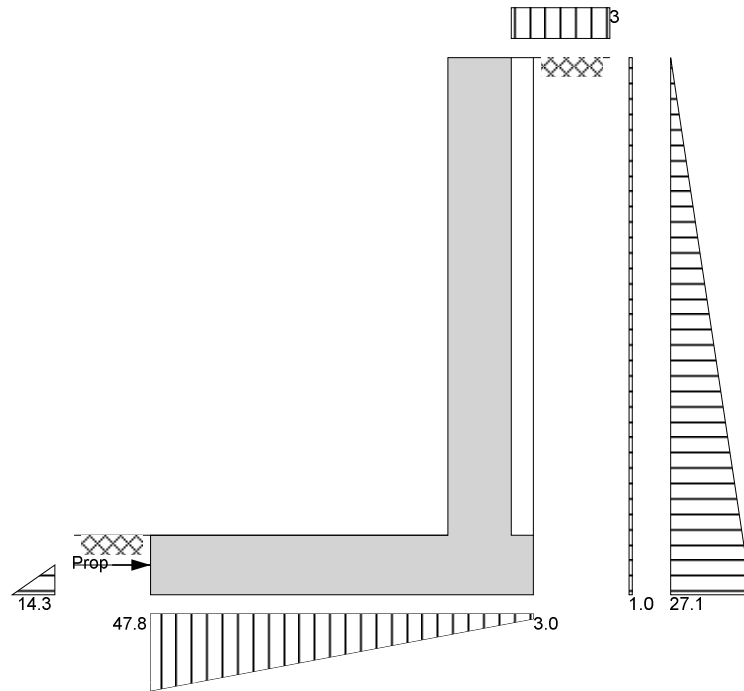
Passive pressure

$K_p = 4.187$

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Loading details

Surcharge load	Surcharge = 2.5 kN/m²			
Vertical dead load	$W_{\text{dead}} = \mathbf{0.0 \text{ kN/m}}$	Vertical live load	$W_{\text{live}} = \mathbf{0.0 \text{ kN/m}}$	
Horizontal dead load	$F_{\text{dead}} = \mathbf{0.0 \text{ kN/m}}$	Horizontal live load	$F_{\text{live}} = \mathbf{0.0 \text{ kN/m}}$	
Position of vertical load	$l_{\text{load}} = \mathbf{0 \text{ mm}}$	Height of horizontal load	$h_{\text{load}} = \mathbf{0 \text{ mm}}$	



Loads shown in kN/m, pressures shown in kN/m²

Calculate propping force

Propping force $F_{\text{prop}} = \mathbf{29.3 \text{ kN/m}}$

Check bearing pressure

Total vertical reaction $R = \mathbf{65.4 \text{ kN/m}}$

Distance to reaction $x_{\text{bar}} = \mathbf{909 \text{ mm}}$


Eccentricity of reaction $e = \mathbf{378 \text{ mm}}$

Reaction acts within middle third of base

Bearing pressure at toe $p_{\text{toe}} = \mathbf{47.8 \text{ kN/m}^2}$

Bearing pressure at heel $p_{\text{heel}} = \mathbf{3.0 \text{ kN/m}^2}$

PASS - Maximum bearing pressure is less than allowable bearing pressure

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RETAINING WALL DESIGN (BS 8002:1994)

TEDDS calculation version 1.2.01.06

Ultimate limit state load factors

Dead load factor $\gamma_{f_d} = 1.4$ Live load factor $\gamma_{f_l} = 1.6$
 Earth pressure factor $\gamma_{f_e} = 1.4$

Calculate propping force

Propping force $F_{prop} = 29.3$ kN/m

Design of reinforced concrete retaining wall toe (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40$ N/mm² Strength of reinforcement $f_y = 500$ N/mm²

Base details

Minimum reinforcement $k = 0.13$ % Cover in toe $c_{toe} = 50$ mm

Design of retaining wall toe

Shear at heel $V_{toe} = 65.2$ kN/m Moment at heel $M_{toe} = 126.4$ kNm/m
Compression reinforcement is not required

Check toe in bending

Reinforcement provided **16 mm dia.bars @ 100 mm centres**
 Area required $A_{s_toe_req} = 894.4$ mm²/m Area provided $A_{s_toe_prov} = 2011$ mm²/m
PASS - Reinforcement provided at the retaining wall toe is adequate

Check shear resistance at toe

Design shear stress $v_{toe} = 0.191$ N/mm² Allowable shear stress $v_{adm} = 5.000$ N/mm²
PASS - Design shear stress is less than maximum shear stress
 Concrete shear stress $v_{c_toe} = 0.644$ N/mm²
 $v_{toe} < v_{c_toe}$ - No shear reinforcement required

Design of reinforced concrete retaining wall heel (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40$ N/mm² Strength of reinforcement $f_y = 500$ N/mm²

Base details

Minimum reinforcement $k = 0.13$ % Cover in heel $c_{heel} = 50$ mm

Design of retaining wall heel


Shear at heel $V_{heel} = 14.7$ kN/m Moment at heel $M_{heel} = 4.5$ kNm/m
Compression reinforcement is not required

Check heel in bending

Reinforcement provided **12 mm dia.bars @ 150 mm centres**
 Area required $A_{s_heel_req} = 520.0$ mm²/m Area provided $A_{s_heel_prov} = 754$ mm²/m
PASS - Reinforcement provided at the retaining wall heel is adequate

Check shear resistance at heel

Design shear stress $v_{heel} = 0.043$ N/mm² Allowable shear stress $v_{adm} = 5.000$ N/mm²
PASS - Design shear stress is less than maximum shear stress
 Concrete shear stress $v_{c_heel} = 0.463$ N/mm²
 $v_{heel} < v_{c_heel}$ - No shear reinforcement required

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Design of reinforced concrete retaining wall stem (BS 8002:1994)

Material properties

Strength of concrete $f_{cu} = 40 \text{ N/mm}^2$ Strength of reinforcement $f_y = 500 \text{ N/mm}^2$

Wall details

Minimum reinforcement $k = 0.13 \%$

Cover in stem $c_{stem} = 50 \text{ mm}$ Cover in wall $c_{wall} = 50 \text{ mm}$

Design of retaining wall stem

Shear at base of stem $V_{stem} = 11.5 \text{ kN/m}$ Moment at base of stem $M_{stem} = 110.0 \text{ kNm/m}$

Compression reinforcement is not required

Check wall stem in bending

Reinforcement provided **16 mm dia.bars @ 100 mm centres**

Area required $A_{s_stem_req} = 725.5 \text{ mm}^2/\text{m}$ Area provided $A_{s_stem_prov} = 2011 \text{ mm}^2/\text{m}$

PASS - Reinforcement provided at the retaining wall stem is adequate

Check shear resistance at wall stem

Design shear stress $V_{stem} = 0.031 \text{ N/mm}^2$ Allowable shear stress $V_{adm} = 5.000 \text{ N/mm}^2$

PASS - Design shear stress is less than maximum shear stress


Concrete shear stress $V_{c_stem} = 0.618 \text{ N/mm}^2$

$V_{stem} < V_{c_stem}$ - No shear reinforcement required

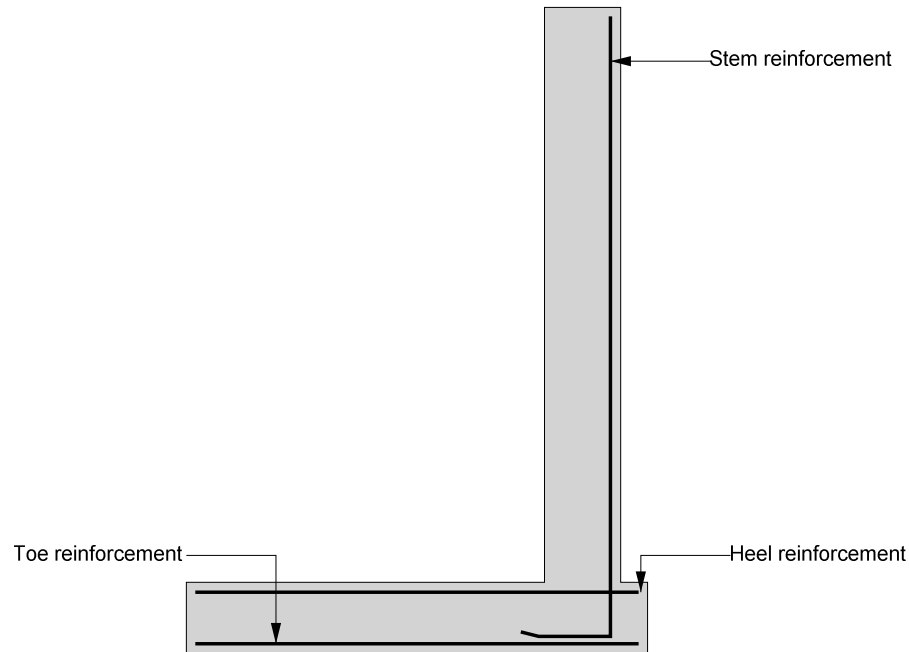
Check retaining wall deflection

Max span/depth ratio $ratio_{max} = 14.00$ Actual span/depth ratio $ratio_{act} = 8.72$

PASS - Span to depth ratio is acceptable

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Indicative retaining wall reinforcement diagram



Toe bars - 16 mm dia.@ 100 mm centres - (2011 mm²/m)

Heel bars - 12 mm dia.@ 150 mm centres - (754 mm²/m)

Stem bars - 16 mm dia.@ 100 mm centres - (2011 mm²/m)

BASE SLAB

CHECK UPLIFT FROM WATER PRESSURE

NETT PRESSURE AT ULS = $1.4(10 \times 3.75) - (6.8) = 43 \text{ kN/m}^2$

B.M. MAX = $43 \times 2.5^2 / 8 = 33.5 \text{ kN.m}$

RC SLAB DESIGN (BS8110)

RC SLAB DESIGN (BS8110:PART1:1997)

TEDDS calculation version 1.0.04

CONCRETE SLAB DESIGN (CL 3.5.3 & 4)

SIMPLE ONE WAY SPANNING SLAB DEFINITION


Overall depth of slab $h = 200 \text{ mm}$

Cover to tension reinforcement resisting sagging $c_b = 35 \text{ mm}$

Trial bar diameter $D_{tryx} = 10 \text{ mm}$

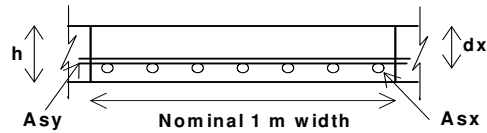
Depth to tension steel (resisting sagging)

$d_x = h - c_b - D_{tryx} / 2 = 160 \text{ mm}$

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Characteristic strength of reinforcement $f_y = 500 \text{ N/mm}^2$

Characteristic strength of concrete $f_{cu} = 35 \text{ N/mm}^2$



One-way spanning slab
(simple)

ONE WAY SPANNING SLAB (CL 3.5.4)

MAXIMUM DESIGN MOMENTS IN SPAN

Design sagging moment (per m width of slab) $m_{sx} = 33.0 \text{ kNm/m}$

CONCRETE SLAB DESIGN – SAGGING – OUTER LAYER OF STEEL (CL 3.5.4)

Design sagging moment (per m width of slab) $m_{sx} = 33.0 \text{ kNm/m}$

Moment Redistribution Factor $\beta_{bx} = 1.0$

Area of reinforcement required

$$K_x = \text{abs}(m_{sx}) / (d_x^2 \times f_{cu}) = 0.037$$

$$K'_x = \min(0.156, (0.402 \times (\beta_{bx} - 0.4)) - (0.18 \times (\beta_{bx} - 0.4)^2)) = 0.156$$

Outer compression steel not required to resist sagging

One-way Spanning Slab requiring tension steel only (sagging) - mesh

$$z_x = \min((0.95 \times d_x), (d_x \times (0.5 + \sqrt{(0.25 - K_x/0.9)}))) = 152 \text{ mm}$$

$$\text{Neutral axis depth } x_x = (d_x - z_x) / 0.45 = 18 \text{ mm}$$

Area of tension steel required

$$A_{sx_req} = \text{abs}(m_{sx}) / (1/\gamma_{ms} \times f_y \times z_x) = 499 \text{ mm}^2/\text{m}$$

Tension steel

Use B785 Mesh

$$A_{sx_prov} = A_{sl} = 785 \text{ mm}^2/\text{m} \quad A_{sy_prov} = A_{st} = 252 \text{ mm}^2/\text{m}$$

$$D_x = d_{sl} = 10 \text{ mm} \quad D_y = d_{st} = 8 \text{ mm}$$

Area of tension steel provided sufficient to resist sagging

Check min and max areas of steel resisting sagging

Total area of concrete $A_c = h = 200000 \text{ mm}^2/\text{m}$

Minimum % reinforcement $k = 0.13 \%$

$$A_{st_min} = k \times A_c = 260 \text{ mm}^2/\text{m}$$

$$A_{st_max} = 4 \% \times A_c = 8000 \text{ mm}^2/\text{m}$$


Steel defined:

$$\text{Outer steel resisting sagging } A_{sx_prov} = 785 \text{ mm}^2/\text{m}$$

Area of outer steel provided (sagging) OK

$$\text{Inner steel resisting sagging } A_{sy_prov} = 252 \text{ mm}^2/\text{m}$$

Less than min area of inner steel (sagging) FAIL

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CONCRETE SLAB DEFLECTION CHECK (CL 3.5.7)

Slab span length $l_x = 2.500$ m

Design ultimate moment in shorter span per m width $m_{sx} = 33$ kNm/m

Depth to outer tension steel $d_x = 160$ mm

Tension steel

Area of outer tension reinforcement provided $A_{sx_prov} = 785$ mm²/m

Area of tension reinforcement required $A_{sx_req} = 499$ mm²/m

Moment Redistribution Factor $\beta_{bx} = 1.00$

Modification Factors

Basic span / effective depth ratio (Table 3.9) $ratio_{span_depth} = 20$

The modification factor for spans in excess of 10m (ref. cl 3.4.6.4) has not been included.

$f_s = 2 \times f_y \times A_{sx_req} / (3 \times A_{sx_prov} \times \beta_{bx}) = 212.0$ N/mm²

$factor_{tens} = \min (2 , 0.55 + (477 \text{ N/mm}^2 - f_s) / (120 \times (0.9 \text{ N/mm}^2 + m_{sx} / d_x^2))) = 1.559$

Calculate Maximum Span

This is a simplified approach and further attention should be given where special circumstances exist. Refer to clauses 3.4.6.4 and 3.4.6.7.

Maximum span $l_{max} = ratio_{span_depth} \times factor_{tens} \times d_x = 4.99$ m

Check the actual beam span

Actual span/depth ratio $l_x / d_x = 15.63$

Span depth limit $ratio_{span_depth} \times factor_{tens} = 31.17$

Span/Depth ratio check satisfied

CHECK OF NOMINAL COVER (SAGGING) – (BS8110:PT 1, TABLE 3.4)

Slab thickness $h = 200$ mm

Effective depth to bottom outer tension reinforcement $d_x = 160.0$ mm

Diameter of tension reinforcement $D_x = 10$ mm

Diameter of links $L_{diat} = 0$ mm

Cover to outer tension reinforcement

$c_{tenx} = h - d_x - D_x / 2 = 35.0$ mm

Nominal cover to links steel

$c_{nomx} = c_{tenx} - L_{diat} = 35.0$ mm

Permissible minimum nominal cover to all reinforcement (Table 3.4)

$c_{min} = 35$ mm

Cover over steel resisting sagging OK

2 LAYERS A393 TOP 1 LAYER BOTTOM