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Ashton Court
254 – 256 Camden Road
London
NW1 9HE

Ground Movement Assessment

For

Origin Housing

Project Number:

12047

July 2015

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1.0 INTRODUCTION

1.1. Appointment and Scope

- 1.1.1. Campbell Reith Hill LLP (CampbellReith) has been appointed by the Robert Lombardelli Partnership, on behalf of Origin Housing (the client), to undertake a ground movement assessment to determine the impact of the construction of a basement at Ashton Court on Camden Mews in north London. This assessment comprises part of a basement impact assessment required by the London Borough of Camden Council for the proposed redevelopment of Ashton Court, 254 – 256 Camden Road, NW1 9HE (the site). The proposal comprises the demolition of two existing buildings and the construction of a new building with three above ground floors and a single storey basement on Camden Mews; and a two storey building on Camden Park Road.
- 1.1.2. This report only considers the magnitude and impact of vertical and horizontal ground movements on the neighbouring properties on Camden Mews, in particular 103 Camden Mews which is adjacent to the west. This report is based on a site specific investigation undertaken by Ground Engineering Limited in January 2015 and describes the ground conditions at the site and the assumptions made as to the existing and proposed structures. The approach taken to determining ground movements is described and the implications for the neighbouring properties are discussed. It is intended that this report is submitted to London Borough of Camden as part of the BIA.
- 1.1.3. Appendix A contains figures showing the site location together with the properties along Camden Mews within the zone of influence of the proposed development and the proposed development. A basement construction sequence report prepared by CampbellReith is included in Appendix B. A summary of the results of the analyses undertaken using the Oasys programme Pdisp Version 19.3, the associated calculations and plots of the horizontal and vertical movement associated with the construction of the retaining wall and subsequent excavation are presented in Appendix C.

2.0 GROUND CONDITIONS

2.1. Site Investigation

- 2.1.1. A site specific ground investigation was procured by the Robert Lombardelli Partnership and is reported separately. The BIA report prepared by CampbellReith (FDemb-12047-020715-BIA-F1) contains an assessment of the data obtained. The investigation comprised a single windowless sampler hole in the garden in the rear of the site undertaken to 10m bgl. The sequence of strata encountered was Made Ground (1.50m thick) underlain by London Clay to the base of the hole. Two foundation inspection pits were undertaken on the boundary with the neighbouring property on the west and these indicated the Made Ground extends to at least 1.70m bgl in places. The base of the London Clay is believed to be at c45m bgl overlying the Lambeth Group (which changes between clays and sands) and the Thanet Sand, which are anticipated to be present up to 70m bgl. The Lambeth Group and Thanet Sand are underlain by Chalk up to at least 120m bgl.
- 2.1.2. Groundwater was not encountered during the site works. A single monitoring visit was undertaken on 3rd February 2015 and the recorded water level was 5.23m bgl.

3.0 EXISTING AND PROPOSED STRUCTURES

3.1. Existing Building

3.1.1. The existing building dates from the early 1980s and is anticipated to be of traditional cavity wall construction (from drawings on a previous planning application for rebuilding the common room). This section on Camden Mews, which is to be demolished and rebuilt with a basement, currently has two above ground floors with partial undercroft parking at ground level. The ground level in the vicinity of the site along Camden Mews is approximately 45.60m AOD and it gently slopes down to 45.40m AOD in the garden in the rear of the building.

3.2. Proposed Building

3.2.1. It is proposed to demolish the existing building and construct a new building with three above ground floors and a single storey basement comprising flats. The basement is indicated to cover approximately the same area as the existing building on Camden Mews on the proposed plans.

4.0 ANALYSIS ASSUMPTIONS AND INPUT PARAMETERS

4.1. Ground Conditions

4.1.1. The sequence of strata is outlined above and the soils have been assumed to be incompressible below 0m AOD.

4.2. Foundation Assumptions

4.2.1. In considering ground movements associated with the proposed redevelopment, it has been assumed that demolition will result in an unloading on the founding stratum of approximately 30kN/m². The maximum excavation depth is anticipated to be c3m, and this will result in a further unloading of 60kN/m² due to the weight of soil being removed. In assessing resultant ground movements, the excavation has been modelled as a rectangle (26 x 10m) to account for the building footprint and the decking at ground level which will extend to maximum 2.50m into the garden.

4.2.2. For this initial assessment, the proposed structure is assumed to be supported on a raft and has been modelled as a rectangle (26 x 7m) to approximate the shape of the proposed basement footprint. A load take down by CampbellReith (Appendix B) indicates the bearing pressure at the underside of the basement slab (42.65m AOD) is likely to be approximately 60kN/m².

4.2.3. The foundations to the neighbouring properties have been assumed to be strip footings at a depth of 0.75m bgl (44.75m AOD). At 103 Camden Mews, these are assumed to be perpendicular to the road at intervals of 4.50m. The foundation inspection trial pits were inconclusive but suggested they might be piled. Consequently this is a conservative assumption.

4.3. Basement Construction Sequence

4.3.1. Whilst the final construction sequence is the responsibility of the Contractor, an assumed basement construction sequence is detailed in SKsk-12047-020715-CS-F1 in Appendix B. A summary is provided below.

4.3.2. Our ground movement assessment assumes that sheet piles are installed around the perimeter of the basement following demolition, followed by partial excavation to 500mm. Propping comprises perimeter head restraint beams which are bolted to the head of the sheet piles. Horizontal props, where required would also be installed across the width of the basement followed by excavation down to 50mm below the underside of the basement slab level. Propping ensures that ground movements are minimised.

4.3.3. The basement slab would then be cast on the blinding. It is assumed the basement slab, which is designed as a raft to distribute the vertical loads evenly, would be 300mm thick reinforced concrete with 450mm deep local thickenings under all concrete walls and around the perimeter.

4.3.4. The basement walls would then be constructed followed by temporary prop removal and casting of the ground floor slab. All the props would be removed. The basement tanking system would then be installed followed by the internal basement walls and then construction of the upper floors.

4.4. Pdisp Analysis

4.4.1. The purpose of the Pdisp analysis is to estimate impact of the vertical ground movements on the neighbouring properties, in particular 103 Camden Mews, to ensure that any damage resulting from the demolition and construction activities is within acceptable limits. Reference to CIRIA C580 [1] reveals that ground movements typically reduce to zero at a distance not exceeding four times the excavation depth. Pdisp relies on structural loads and soil properties being defined by reference to x, y coordinates, hence the modelling of the proposed building footprint as a rectangle and the strip footings of the neighbouring properties as grid lines. GL1 to GL6 represent the assumed locations of the strip footings of the properties within four times the depth of the excavation (c12m). The assumptions are based on observations of the form and type of nearby buildings made during a site reconnaissance visit. Vertical ground movements have been estimated at the assumed foundation locations and the programme assumes a fully flexible foundation which is likely to overestimate ground movements.

4.4.1. Modulus values have been derived empirically, with the undrained modulus (E_u) being equal 400 x undrained shear strength (C_u) in the London Clay [2]. The drained modulus (E') has been taken as 0.75 x E_u . In the Made Ground, E_u has conservatively been assumed to be 5000kN/m² which is based on our experience in similar soils and has been taken to be equal to E' . The following parameters were adopted for analysis:

TABLE 4.1: Soil Input Parameters

Stratum	Bulk Unit Weight (kN/m ³)	Undrained Shear Strength (kN/m ²)	Young's Modulus (kN/m ²)	Poisson's ratio
Made Ground	18	N/A	$E_u = E' = 5000$	$\nu = 0.5$ $\nu' = 0.2$
London Clay	20	$C_u = 70 + 6z^1$	$E_u = 28000 + 2400z$ $E' = 21000 + 1800z$	$\nu = 0.5$ $\nu' = 0.2$

Where z = depth below the top of the London Clay which was encountered at 1.50m bgl

4.4.2. Laboratory triaxial tests were undertaken as part of the ground investigation, however, these were performed on samples from a windowless sampler hole which are likely to have experienced sample disturbance, resulting in lower apparent strengths. CampbellReith's experience in working with the London Clay allowed a reasonable estimation of the undrained shear strength (C_u) to be made using both the site investigation information and data from other sites in north London. The vertical undrained modulus in the London Clay $E_u = 400C_u$ and drained modulus, $E' = 0.75E_u$.

4.5. Ground Movements due to Excavation

4.5.1. Although the sequence of works described above allows the wall support to be assessed as high stiffness, moderate support stiffness has been assumed for the purposes of this assessment. This is a conservative assumption. Based on CIRIA C580 Table 2.4, this indicates vertical and horizontal surface movements of 0.30% of the maximum excavation depth. Curves presented in Figures 2.11a and 2.11b of CIRIA C580 allow the profile of ground movements behind the wall to be estimated.

- 4.6. Assessment of Strain and Building Damage
 - 4.6.1. Initially, the ground movements on the neighbouring properties comprise heave due to the demolition of the existing building and excavation of the basement offset by settlement due to the excavation of the basement. The former are derived the Pdisp analysis and the latter from CIRIA C580. Horizontal movements will also occur which can again be assumed from CIRIA C580. The likely maximum vertical and horizontal strain can then be calculated which then enables an estimation of the building damage category.
 - 4.6.2. As described above, the ground movements have been estimated at the assumed locations of the neighbouring property footings.

5.0 ASSESSMENT OF GROUND MOVEMENTS AND BUILDING DAMAGE

5.1. Ground Movements

- 5.1.1. Ground movements have been estimated along the length of the neighbouring property footings at a level of 44.75m AOD (0.75m below the street level in front of 103 Camden Mews as given in the topographic survey provided by the client). According to CIRIA C580, ground movements associated with the construction of the basement and retaining walls are could theoretically extend to 101 and 103 Camden Mews, 88 – 90 Camden Mews and 59 Camden Park Road.
- 5.1.2. An analysis of the vertical ground movements (heave/settlement) associated with the demolition of the existing building and the construction of the new building together has been undertaken using the Oasys programme Pdisp Version 19.3.
- 5.1.3. Immediate heave due to the demolition of the existing building and excavation of the basement is in the order of 10mm beneath the party wall foundations with 103 Camden Mews. This reduces to approximately 3mm halfway along the length of the building and 1mm on the party wall between 103 and 101 Camden Mews. The maximum likely heave beneath 84 – 90 Camden Mews is estimated to be less than 3mm, and 2mm on 59 Camden Park Road.
- 5.1.4. As described in Section 4.5, based on CIRIA C580 Table 2.4, vertical and horizontal surface movements of 0.30% of the maximum excavation depth have been assumed.
- 5.1.5. Immediate settlement (vertical surface movements) due to the excavation would be in the order of 9mm at the party wall foundations with 103 Camden Mews, 6mm halfway along the length of the building and 3mm on the party wall between 103 and 101 Camden Mews. The heave from the Pdisp analysis is offset by the settlement from the CIRIA C580 therefore the maximum likely vertical ground surface movement at the wall is estimated to be 1mm, 3mm at 4.50m away from the wall and 2mm at 9m. The maximum vertical movement, Δ , between the assumed foundation locations of 103 Camden Mews is estimated to be 4mm.
- 5.1.6. The horizontal movements at the top of the sheet pile wall are also likely to be in the order of 9mm, reducing to 6mm at a distance of 4.5m and 3mm at a distance of 9m. The maximum horizontal movement, δh , between the assumed foundation locations of 103 Camden Mews is estimated to be 3mm.
- 5.1.7. Post construction, there may be some further settlement. Vertical ground movements (total settlement from the construction minus long term heave from the demolition of the existing building and basement excavation) on 103 Camden Mews are not expected to exceed 5mm. This occurs midway along the party wall. However, as Pdisp assumes a fully flexible foundation this is likely to be an overestimate. The maximum likely long term movement beneath 84 – 90 Camden Mews and 59 Camden Park Road is less than 1mm.

5.2. Assessment of Strain and Building Damage

- 5.2.1. The length of the neighbouring property (103 Camden Mews) has been assumed to be 9m with an approximate height (H) of 6m. The strain has been assessed over the full length of the property (L =9m) and between the party wall and the foundation at 4.50m beyond it (L= 4.5m).

Following the procedure given in CIRIA C580 Box 2.5, $L/H=0.75$ (i.e. at the intermediate foundation) and at 1.5 at $L=9\text{m}$ (i.e. at the far side of the property).

- 5.2.2. The maximum horizontal strain, $\epsilon_h (\delta h/L) = 0.06\%$ and the maximum deflection ratio $\Delta/L = 0.08\%$ beneath the adjoining property (103 Camden Mews). This represents a maximum damage category of 'slight' (Burland Category 2).

6.0 CONCLUSIONS

- 6.1. The maximum horizontal movement, $\delta h = 3\text{mm}$, and vertical movement, $\Delta = 4\text{mm}$ between the assumed foundation locations of 103 Camden Mews. Although there is predicted heave of up to 10mm (Pdisp analysis), this is offset by settlement of up to 9mm (as derived from CIRIA C580).
- 6.2. An assessment of the strain as a result of the demolition and basement excavation indicates that the damage to 103 Camden Mews falls within category 2, 'slight'.
- 6.3. Post construction, the maximum vertical movement beneath 103 Camden Mews is less than 5mm.
- 6.4. The movements and hence the damage on the remaining properties within the zone of influence are negligible.

TECHNICAL REFERENCES

Reference	Reference Title	Type
1	CIRIA C580 Embedded retaining walls - guidance for economic design.	CIRIA Publication
2	C J Padfield and M J Sharrock, Settlement of Structures on Clay Soils	CIRIA Publication

LIMITATIONS

1. Where any data or information supplied by the client or other external source, including that from previous studies, has been used, it has been assumed that the information is correct. No responsibility can be accepted by CampbellReith for inaccuracies within this data or information.
2. This report is limited to those aspects described in the introduction and no liability is accepted for any other aspects.
3. The generalised soil conditions described in the text are intended to convey trends in subsurface conditions. The boundaries between strata are approximate and have been developed on interpretations of the exploration locations and samples collected.
4. Water level and gas readings have been taken at times and under conditions stated on the exploration logs. It must be noted that fluctuations in the level of groundwater or gas may occur due to a variety of factors which may differ from those prevailing at the time the measurements were taken.
5. The findings and opinions expressed are relevant to those dates of the reported site work and should not be relied upon to represent conditions at substantially later dates.
6. This report is produced solely for the benefit of the client, and no liability is accepted for any reliance placed upon it by any other party unless specifically agreed in writing.

APPENDIX A: FIGURES

Figure 1: Site Location

Figure 2a and 2b: Proposed Development



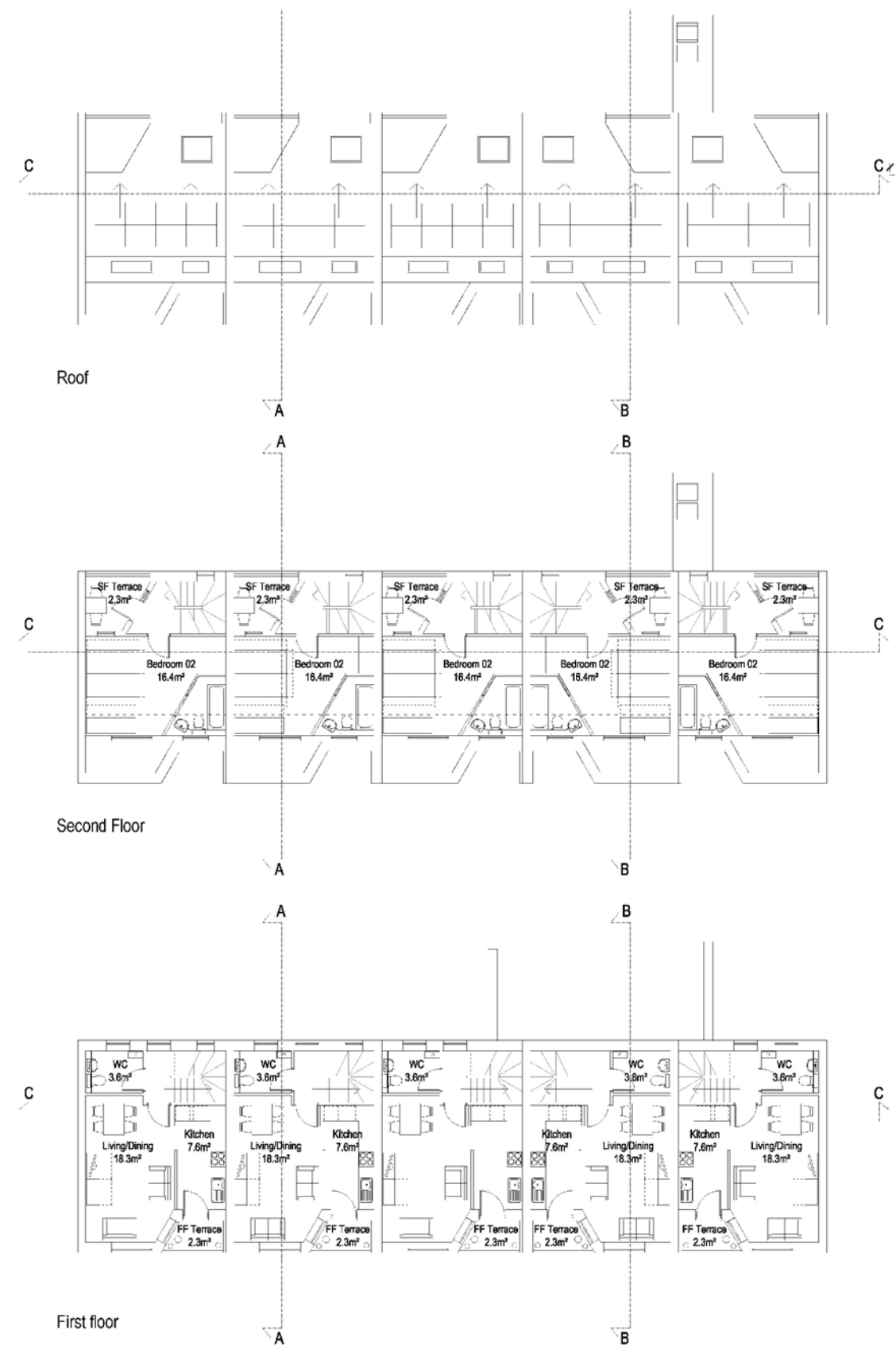
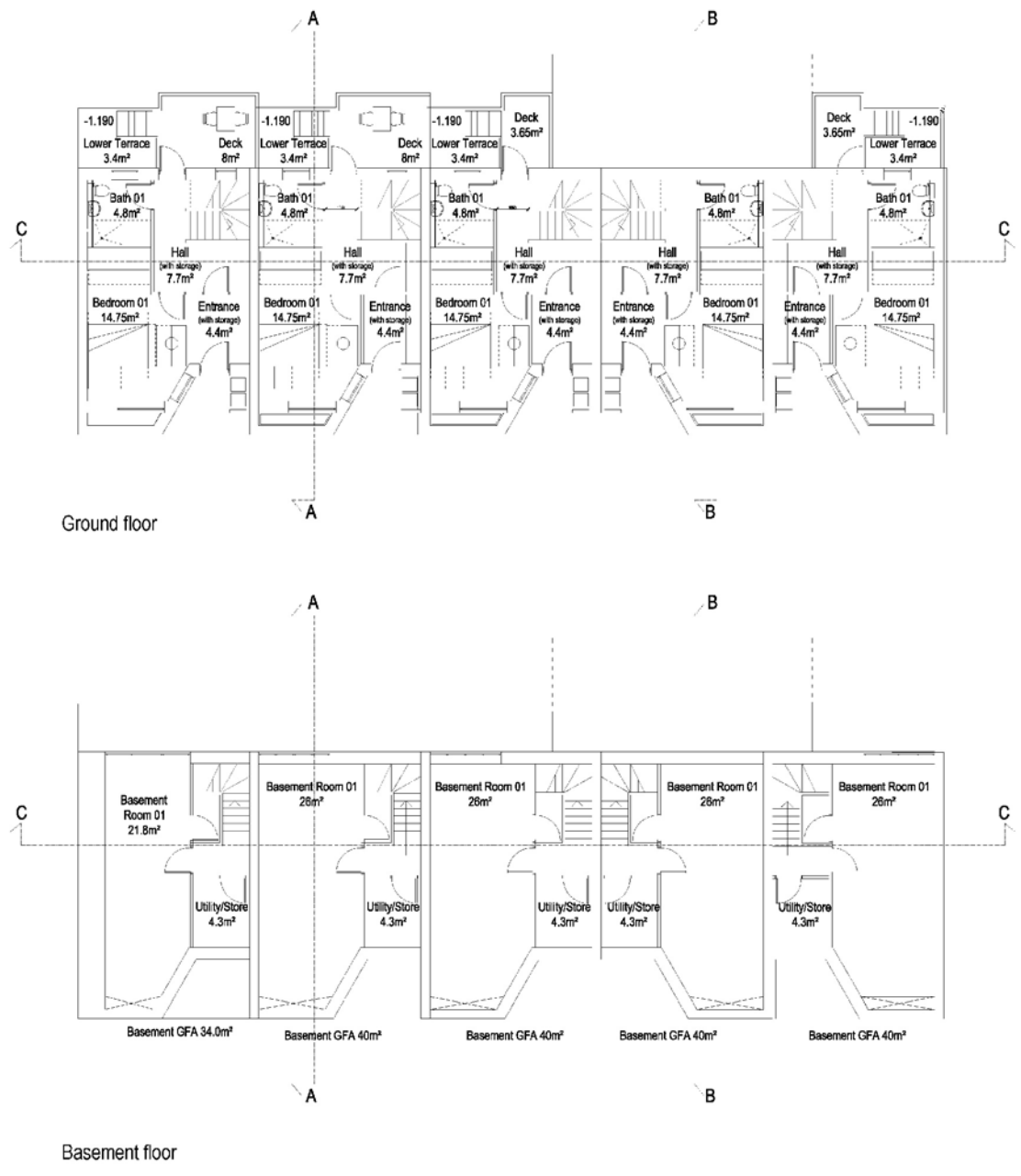
Ashton Court
 Client: Origin Housing

Figure 1:
 Site Location and Neighbouring Properties Within Zone
 of Influence of Proposed Basement

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Ashton Court
 Client: Origin Housing

Figure 2a:
 Camden Mews Proposed Development (All Floors)

NTS

Scale: NTS
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APPENDIX B: BASEMENT CONSTRUCTION SEQUENCE

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Ashton Court
254 – 256 Camden Road
NW1 9HE

Basement Construction Sequence of Works

For

Origin Housing

Project Number:

12047

July 2015

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Project Name	Ashton Court

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1.0 EXECUTIVE SUMMARY

- 1.1. The following report has been produced to show an indicative sequence of works for the construction of a new single storey basement at Ashton Court, Camden, NW1 9HE. All sketches and information provided within this report are indicative only and subject to change following further investigations and detailed design.
- 1.2. The final Construction Sequence and Method Statements remain the responsibility of the Contractor. All temporary works design and stability of existing structures remain the responsibility of the Contractor during construction.

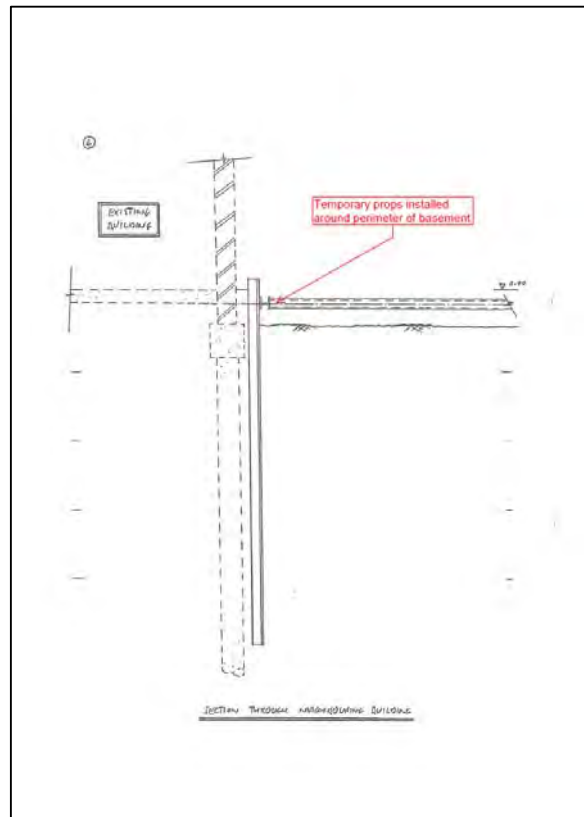
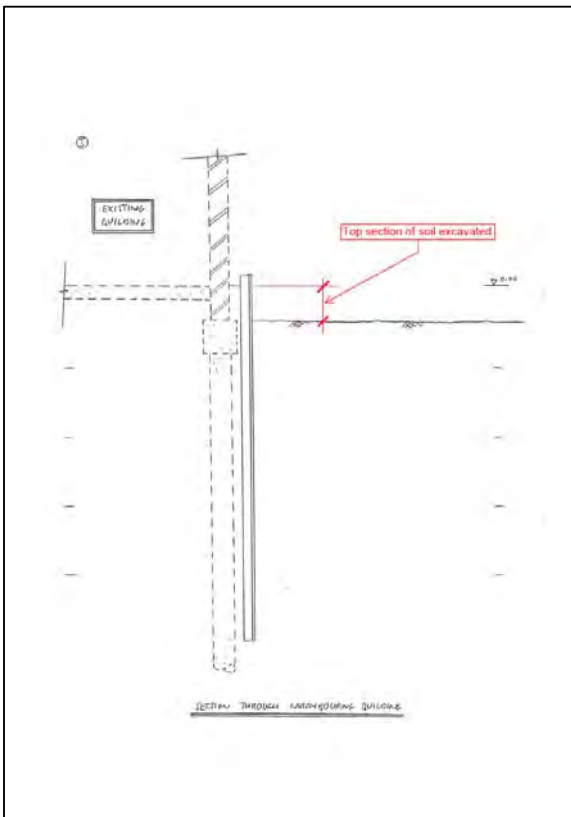
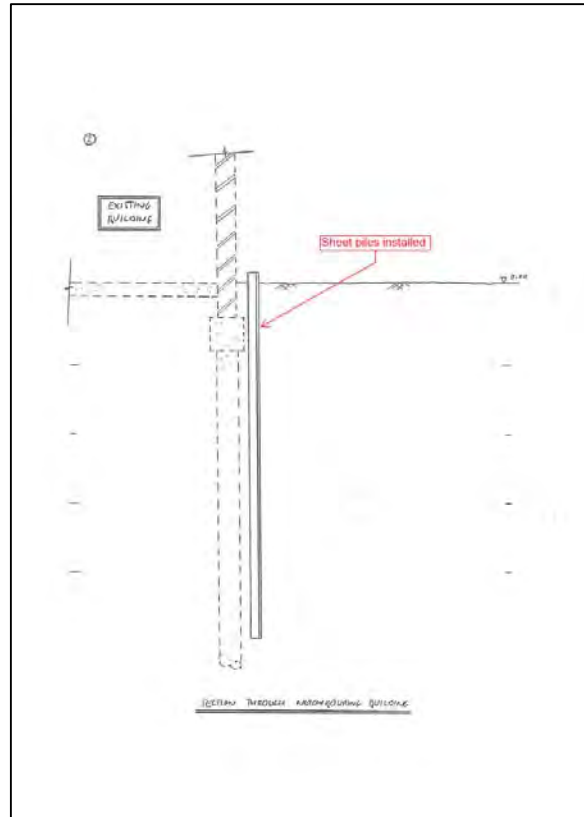
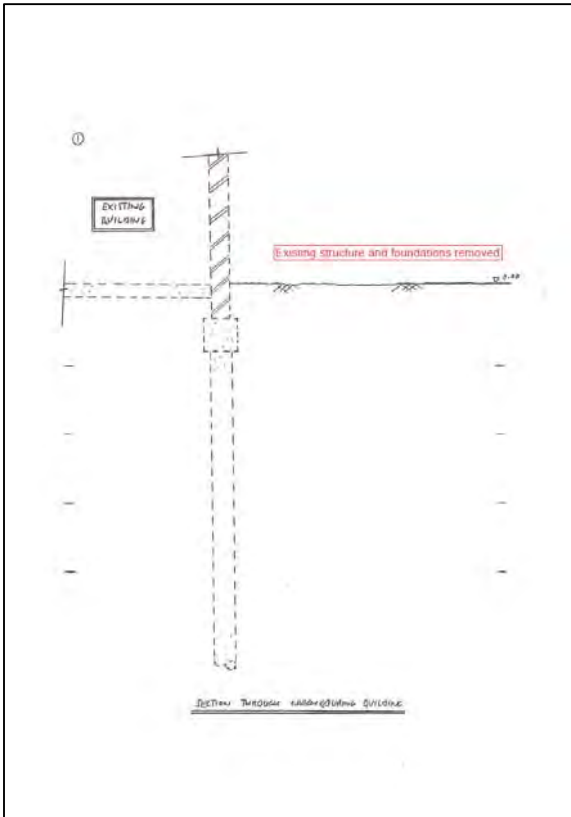
2.0 DEMOLITION

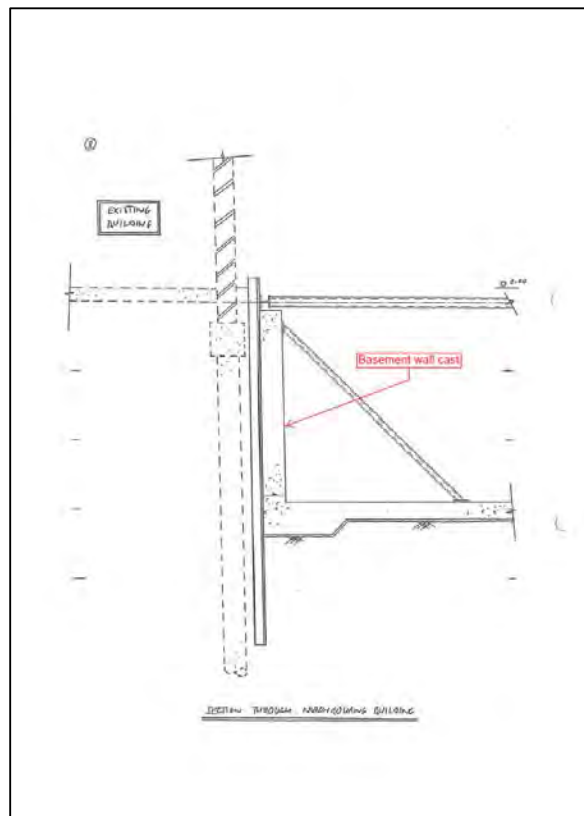
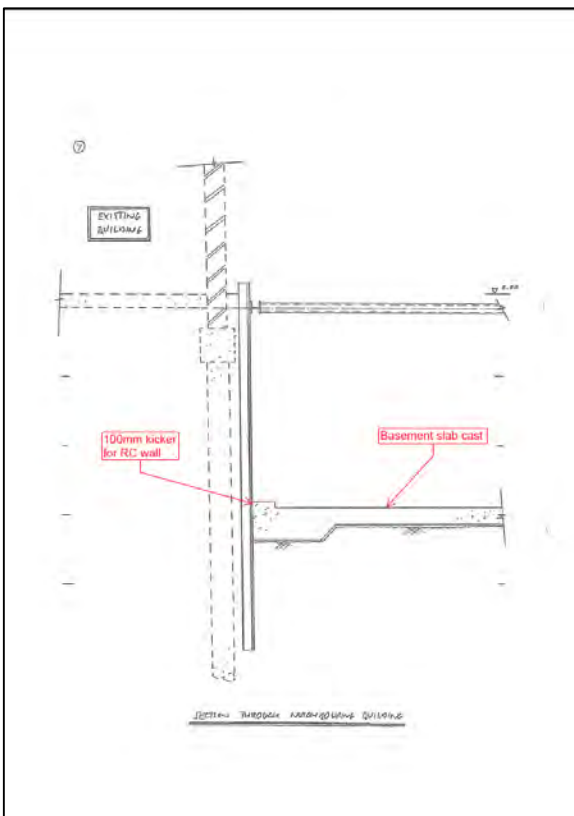
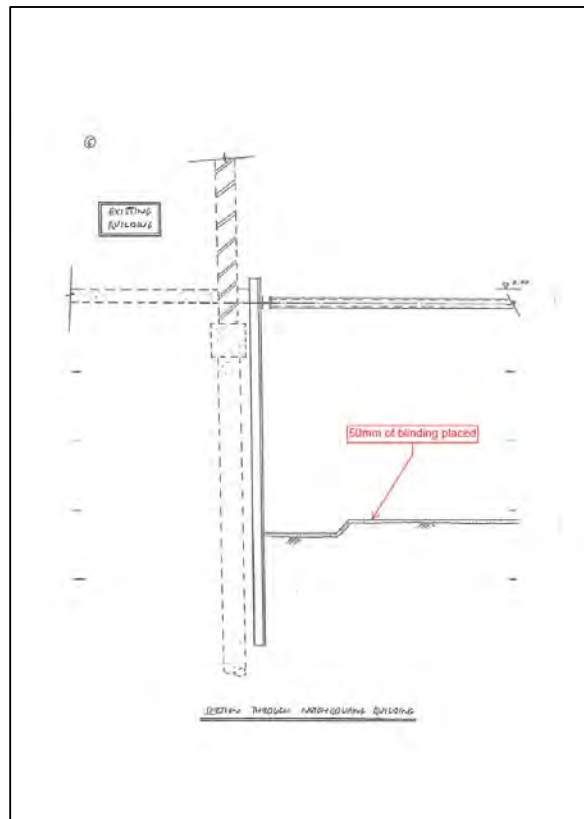
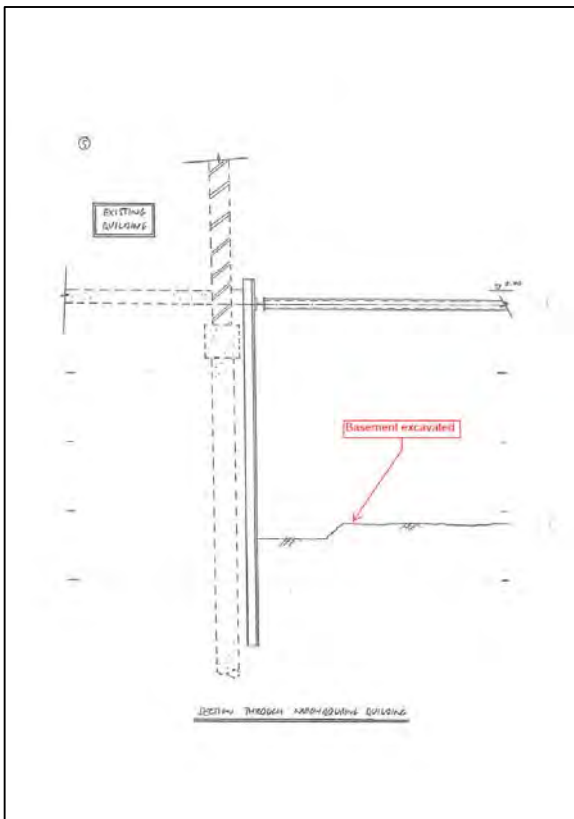
- 2.1. The existing building on Camden Mews in the southern area of the site is to be demolished in order to construct a new three storey residential building with an additional single storey basement.
- 2.2. The link building to the east of the site on Camden Park Road is also to be demolished and will not require significant temporary works during excavation of the basement. For this reason, this report concentrates on the section through the retained neighbouring property. Two inspection pits failed to confirm the nature of the foundations to the neighbouring property. TP1 revealed what could have been a ground beam and it has been assumed that the building has piled foundations. This must be confirmed prior to the final design of the basement and foundations to Ashton Court.

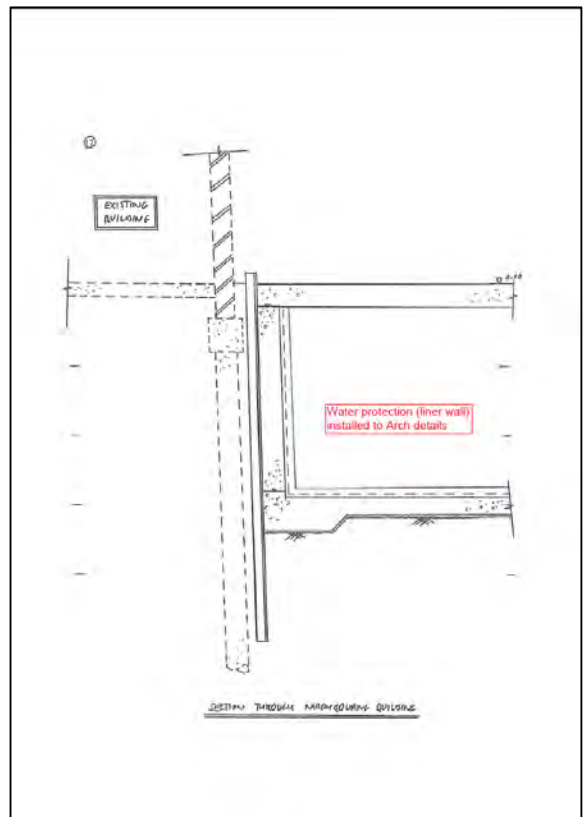
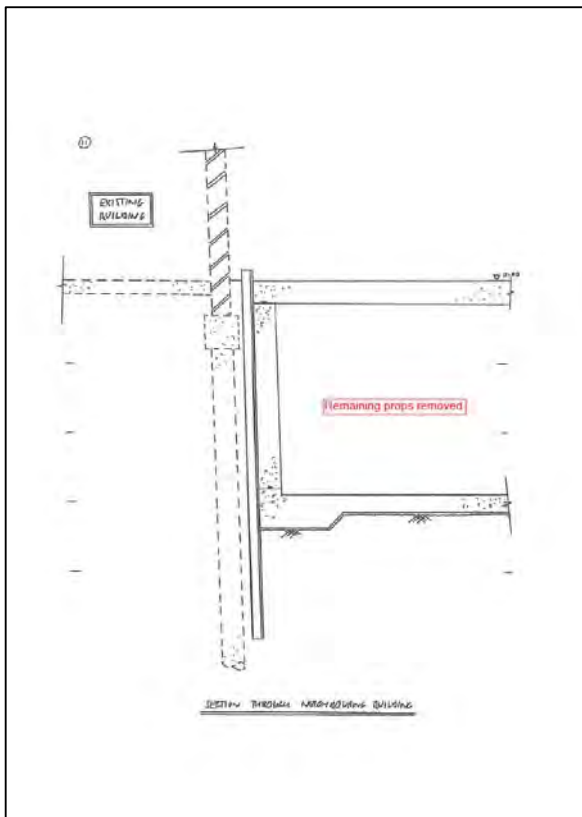
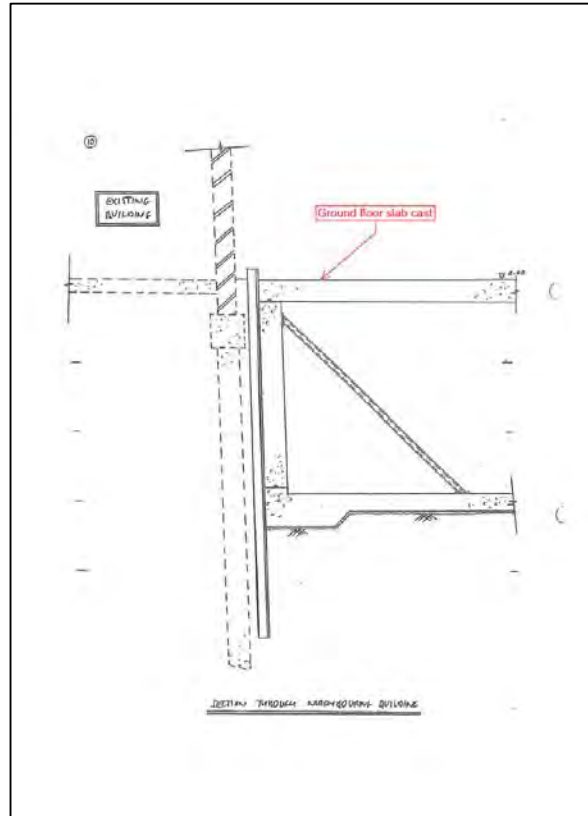
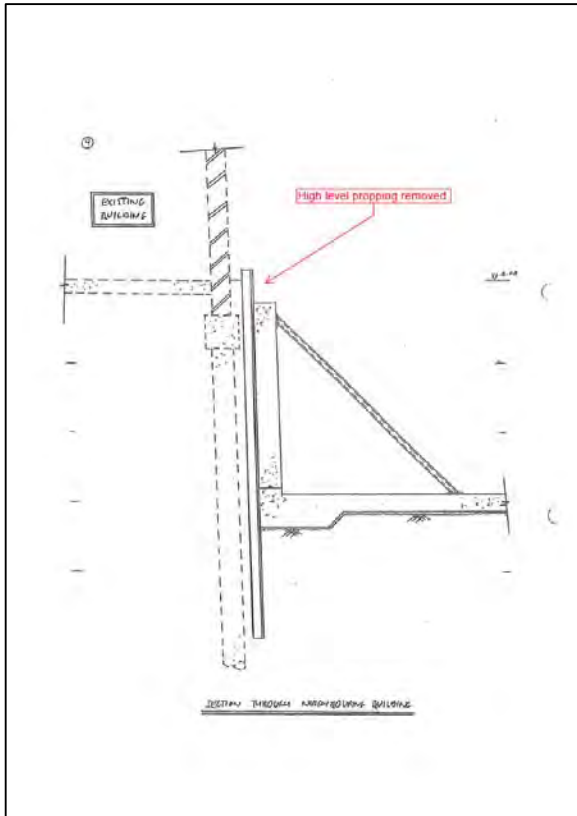
3.0 SEQUENCE OF WORKS

- 3.1. Also refer to the sequence of work sketches shown following the step-by-step description below. These sketches show the section through the west of the basement, adjacent to the neighbouring property. Sections on the other sides of the basement will be similar but without the neighbouring structure and foundations.
- 3.2. Step 1 (Demolition): The existing buildings on site are to be demolished and existing foundations grubbed out.
- 3.3. Step 2 (Sheet Piling): Sheet piles are to be installed around the perimeter of the basement. Sheet piles to be designed as propped and detailed design to be carried out by the main contractor. It is anticipated that the sheet piles will extend to a depth of approximately 1.5m below the lowest level of excavation.
- 3.4. Step 3 (Excavation Stage 1): Approximately 500mm depth of excavation is carried out over the full plan area of the basement. This is to allow room to install the temporary horizontal propping. Sheet piles to also be designed for this load case.

- 3.5. Step 4 (Propping): Perimeter head restraint beams are installed and bolted to the head of the sheet piles. Horizontal props are installed where required across the width of the basement. All temporary works are the responsibility of the Main Contractor.
- 3.6. Step 5 (Excavation Stage 2): The basement is then excavated down to 50mm below the underside of the basement slab level, removing any soft spots. 150mm of type 1 hardcore is to be laid and compacted at the base of the excavation in any soft spots encountered.
- 3.7. Step 6 (Blinding): A 50mm blinding mass concrete is cast as a base on which to fix the reinforcement for the basement slab.
- 3.8. Step 7 (Basement Slab): The basement slab is cast on the blinding. At this stage it is assumed the basement slab will be 300mm thick RC with 450mm deep local thickenings under all concrete walls and around the perimeter. This slab is to be designed as a raft slab to distribute the vertical loads evenly across the full plan area of the basement. 100mm high wall kickers are cast in preparation of the walls at the next stage.
- 3.9. Step 8 (RC Basement Wall Construction): The RC walls are cast up to the underside of the temporary props. At this stage it is assumed these will be 300mm thick RC. Hydrophilic strips are to be installed at all construction joints. Any temporary props required for the walls are then installed ready for the removal of the main high level temporary props.
- 3.10. Step 9 (Temporary Prop Removal): Once the RC walls have achieved sufficient strength to resist the lateral loads, the main sheet pile head restraint beams and lateral props are removed.
- 3.11. Step 10 (Ground Floor Slab): The ground floor slab is cast. This slab is two way spanning and supported on the RC walls. Hydrophilic strips are to be installed at all construction joints.
- 3.12. Step 11 (Removal of all Props): Any additional props are now removed.
- 3.13. Step 12 (Following Construction Stages):
 - Basement tanking system installed.
 - Internal basement non-load bearing walls constructed.
 - Upper floors and structure constructed.







4.0 WATER PROTECTION

- 4.1. All below ground water protection is to be to the Architects details. The basement forms part of a dwelling and so it is anticipated this will be classed as Grade 3 in accordance with BS 8102:2009. The tanking system will be an internal drained cavity to the Architects details.

5.0 LIMITATIONS ON MOVEMENT

- 5.1. In the area of the proposed basement, the site has a roadway to the south (Camden Mews) and east (Camden Park Road). A residential property is located to the immediate west (103 Camden Mews). Although the previously described sequence of works allows the propping and retaining wall to be assessed as a high stiffness system, which reduces the expected adjacent ground movements, we have assumed a medium stiffness. Additionally, although it is considered likely that 103 Camden Mews is piled, shallow foundations for the neighbouring property have been assumed for a ground movement assessment undertaken in line with guidance from CIRIA C580. These are both conservative assumption. Assuming a maximum excavation depth of c3m, horizontal and vertical deflections are assessed not to exceed approximately 9mm at the top of the sheet pile wall and 3mm at a distance of 9m behind the wall.
- 5.2. Any suggested surveys from CIRIA C580, such as pre-condition surveys, should be carried out prior to any construction works taking place.
- 5.3. The ground movement assessment (reported separately) confirms that ground movements can be limited to acceptable levels. This assessment should be updated once the foundations to 103 Camden Mews are known and the form of the retaining wall and the construction sequence are better known. We would suggest that movement to the existing surrounding ground should be limited as follows:

Roadways: Slight, in accordance with CIRIA C580 Table 2.5

- 5.4. Neighbouring Property: Slight, in accordance with CIRIA C580 Table 2.5. However, if 103 Camden Mews is founded on piles, then actual settlement of this structure due to the excavation of the basement is expected to be minimal.

6.0 BEARING PRESURES

- 6.1. Having carried out a scheme load take down, the bearing pressure under the raft slab at basement level will be approximately 60kN/m² (unfactored). This will be made up of 75% Dead Loads and 25% Imposed Loads. From the initial ground investigation, it is demonstrated that the founding stratum (below basement slab) has a safe net bearing capacity significantly in excess of the applied load.

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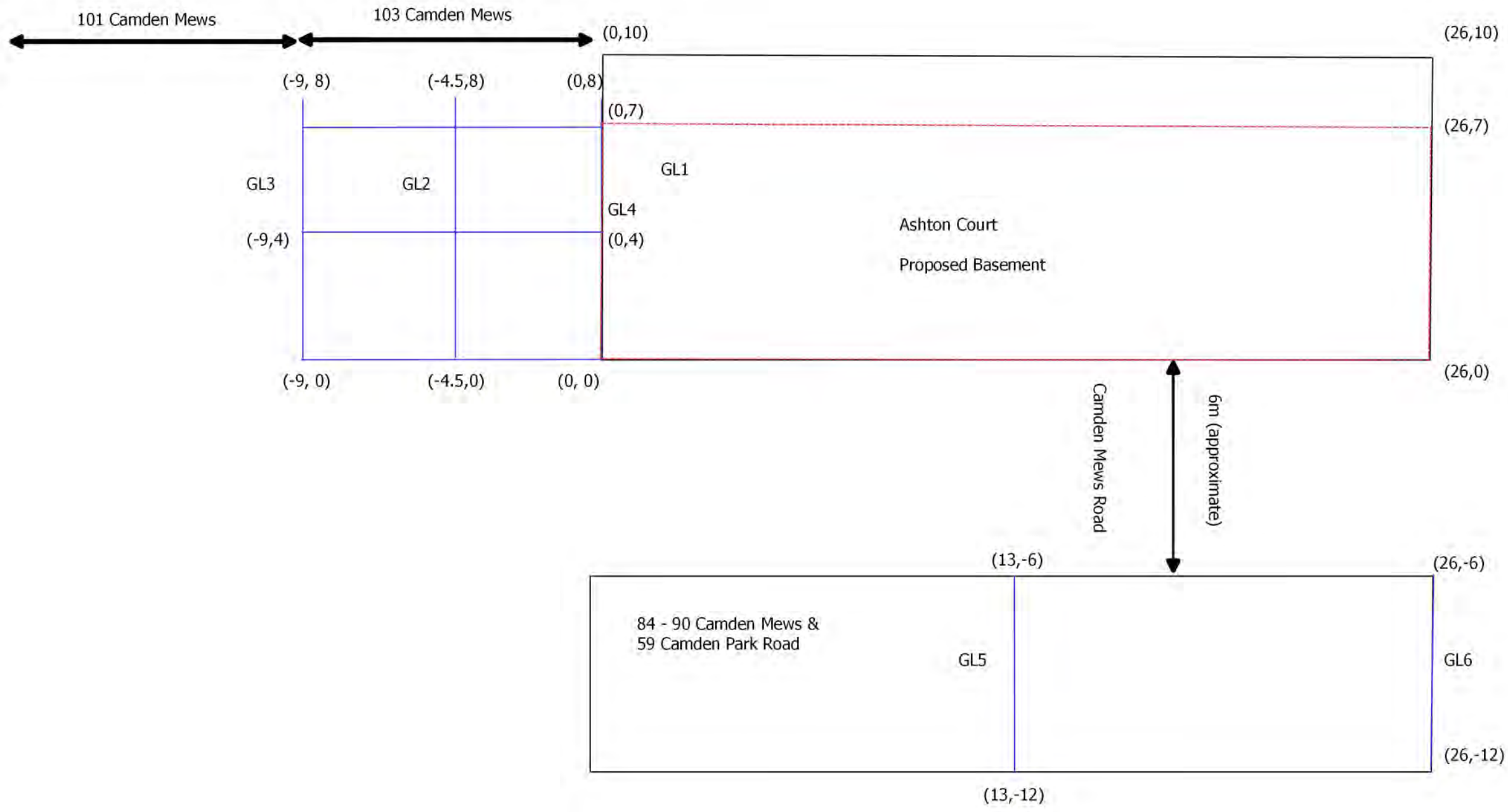
APPENDIX C: PDISP ANALYSES

Contents



Legend

- Excavation
- Construction Stage



NTS

Ashton Court
Client: Origin Housing

Coordinates (X,Y) adopted in Pdisp analysis

Scale: NTS
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Job Number: 12047
Drawn by - Checked by: LB - FD
Dwg No - Status/Revision: G15009 - B
File location: N:\12000 - 12249\12047 L - Ashton Court\Project Workspaces (pdf in Outputs)
Date (Revision History): 01/07/2015 (A, First Issue, 17/06/15, LB; B, Minor Changes, 01/07/15, LB)

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Table 1 - Ground Movement Assessment Input Data

Area	Demolition(kN/m ²)	Excavation Depth(m)	Excavation(kN/m ²)	Centre x	Centre y
Ashton Court	-30	3	-60	13	5
Proposed Building					
Loaded Area	Centre x	Centre y	Dim x (m)	Dim y (m)	P (kN/m ²)
Ashton Court	13	3.5	26	7	60
Neighbouring Properties					
	GL	X ₁	Y ₁	X ₂	Y ₂
103 Camden Mews	GL1	0	0	0	8
	GL2	-4.5	0	-4.5	8
	GL3	-9	0	-9	8
	GL4	0	4	-9	4
84-90 Camden Mews & 59 Camden Park Road	GL5	13	-6	13	-12
	GL6	26	-6	26	-12



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Ashton Court
 Demolition & Basement excavation
 Immediate heave

Notes

EU=400Cu
 CU=70+6z

Analysis Options

Analysis: Boussinesq
 Global Poisson's ratio: 0.20
 Maximum allowable ratio between values of E: 1.5
 Horizontal rigid boundary level: 0.00 [m OD]
 Displacements at area centroids calculated.

Soil Profiles/Soil Profile

Layer	Level at top [mOD]	Level at intermediate displacement levels [m]	Number of levels	Youngs Modulus [kN/m ²]	Poissons ratio	Non-linear curve
1	45.400	2	5000.0	5000.0	0.50000	None
2	43.900	43	28000.	131200.	0.50000	None

Soil Zones

Zone	Name	X coordinates min max [m]	Y coordinates min max [m]	Profile
1	SZ1	-60.000 60.000	-60.000 60.000	Soil Profile

Non-linear Curve Coordinates - Non-linear Curve 1

Point Strain Factor [%]

Load Data

Load ref.	Name	Shape	Orientation of Plane	Centre of load (Global) X Y [m]	Z (level) [m]	Load position Angle of local x from [Degrees]	Width x or Radius [m]	Length y [m]	Polygon Coordinates [m]	Rectangle of tolerance	Number of rectangles	Normal (local x) [kN/m ²]	Tangential (local x) [kN/m ²]	Tangential (local y) [kN/m ²]
1	Basement	Rectangular	Horizontal	13.000 5.0000	42.650	0.0	26.000	10.000	N/A	N/A	1	-90.000	0.0	0.0

Displacement Data

Ref.	Type	Name	Direction of Extrusion	First point X Y [m]	Z (level) [m]	Line/Line for extrusion X Y [m]	Z (level) [m]	No. of intrvl across extrusion/line	Extrusion Depth [m]	No. of intrvl along extrusion	Show Calculate Detailed results
1	Grid	BL	Global X	0.0	0.0	42.650	N/A	10	26.000	26	Yes No
2	Line	GL1	N/A	0.0	0.0	44.750	0.0	8	N/A	N/A	Yes No
3	Line	GL2	N/A	-4.5000	0.0	44.750	-4.5000	8	N/A	N/A	Yes No
4	Line	GL3	N/A	-9.0000	0.0	44.750	-9.0000	8	N/A	N/A	Yes No
5	Line	GL4	N/A	0.0	4.0000	44.750	-9.0000	9	N/A	N/A	Yes No
6	Line	GL5	N/A	13.000	-6.0000	44.750	13.000	6	N/A	N/A	Yes No
7	Line	GL6	N/A	26.000	-6.0000	44.750	26.000	6	N/A	N/A	Yes No

RESULTS FOR GRIDS

Analysis: Boussinesq
 Global Poisson's ratio: 0.20
 Horizontal rigid boundary level: 0.00 [m OD]

The maximum difference between Boussinesq method (-19.964mm) and Mindlin method (-15.515mm) occurs at point X=13.000m Y=5.0000m Level 42.650mOD and is 4.4488mm

Name	X [m]	Location Y [m]	Z [Level] [m]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
Basement	13.00000	5.00000	42.65000	-19.964	42.238	-89.978	-203.88	-0.0010354
BL	0.00000	0.00000	42.65000	-6.7342	42.238	-22.499	-52.483	-235.36E-6
	1.00000	0.00000	42.65000	-8.8092	42.238	-44.446	-92.967	-632.83E-6
	2.00000	0.00000	42.65000	-9.8331	42.238	-44.920	-99.341	-555.19E-6
	3.00000	0.00000	42.65000	-10.539	42.238	-44.975	-101.56	-523.07E-6
	4.00000	0.00000	42.65000	-11.061	42.238	-44.989	-102.64	-506.67E-6
	5.00000	0.00000	42.65000	-11.458	42.238	-44.994	-103.27	-497.06E-6
	6.00000	0.00000	42.65000	-11.766	42.238	-44.996	-103.67	-490.94E-6
	7.00000	0.00000	42.65000	-12.007	42.238	-44.997	-103.93	-486.84E-6
	8.00000	0.00000	42.65000	-12.193	42.238	-44.998	-104.11	-484.02E-6
	9.00000	0.00000	42.65000	-12.335	42.238	-44.998	-104.24	-482.05E-6
	10.00000	0.00000	42.65000	-12.440	42.238	-44.998	-104.33	-480.69E-6
	11.00000	0.00000	42.65000	-12.512	42.238	-44.998	-104.39	-479.81E-6
	12.00000	0.00000	42.65000	-12.554	42.238	-44.998	-104.42	-479.31E-6
	13.00000	0.00000	42.65000	-12.567	42.238	-44.998	-104.43	-479.15E-6
	14.00000	0.00000	42.65000	-12.554	42.238	-44.998	-104.42	-479.31E-6
	15.00000	0.00000	42.65000	-12.512	42.238	-44.998	-104.39	-479.81E-6
	16.00000	0.00000	42.65000	-12.440	42.238	-44.998	-104.33	-480.69E-6
	17.00000	0.00000	42.65000	-12.335	42.238	-44.998	-104.24	-482.05E-6
	18.00000	0.00000	42.65000	-12.193	42.238	-44.998	-104.11	-484.02E-6
	19.00000	0.00000	42.65000	-12.007	42.238	-44.997	-103.93	-486.84E-6
	20.00000	0.00000	42.65000	-11.766	42.238	-44.996	-103.67	-490.94E-6
	21.00000	0.00000	42.65000	-11.458	42.238	-44.994	-103.27	-497.06E-6
	22.00000	0.00000	42.65000	-11.061	42.238	-44.989	-102.64	-506.67E-6
	23.00000	0.00000	42.65000	-10.539	42.238	-44.975	-101.56	-523.07E-6
	24.00000	0.00000	42.65000	-9.8331	42.238	-44.920	-99.341	-555.19E-6
	25.00000	0.00000	42.65000	-8.8092	42.238	-44.446	-92.967	-632.83E-6
	26.00000	0.00000	42.65000	-6.7342	42.238	-22.499	-52.483	-235.36E-6
	0.00000	1.00000	42.65000	-8.7043	42.238	-44.446	-92.888	-634.07E-6
	1.00000	1.00000	42.65000	-11.981	42.238	-87.929	-168.60	-0.0014921
	2.00000	1.00000	42.65000	-13.320	42.238	-88.774	-178.65	-0.0012743
	3.00000	1.00000	42.65000	-14.183	42.238	-88.860	-181.72	-0.0013302
	4.00000	1.00000	42.65000	-14.794	42.238	-88.879	-183.12	-0.0013092
	5.00000	1.00000	42.65000	-15.249	42.238	-88.886	-183.89	-0.0012975
	6.00000	1.00000	42.65000	-15.595	42.238	-88.889	-184.36	-0.0012902
	7.00000	1.00000	42.65000	-15.861	42.238	-88.890	-184.66	-0.0012855
	8.00000	1.00000	42.65000	-16.066	42.238	-88.891	-184.87	-0.0012823
	9.00000	1.00000	42.65000	-16.220	42.238	-88.891	-185.01	-0.0012801
	10.00000	1.00000	42.65000	-16.334	42.238	-88.891	-185.11	-0.0012786
	11.00000	1.00000	42.65000	-16.411	42.238	-88.891	-185.17	-0.0012776
	12.00000	1.00000	42.65000	-16.456	42.238	-88.892	-185.20	-0.0012771
	13.00000	1.00000	42.65000	-16.471	42.238	-88.892	-185.22	-0.0012769
	14.00000	1.00000	42.65000	-16.456	42.238	-88.892	-185.20	-0.0012771
	15.00000	1.00000	42.65000	-16.411	42.238	-88.891	-185.17	-0.0012776
	16.00000	1.00000	42.65000	-16.334	42.238	-88.891	-185.11	-0.0012786
	17.00000	1.00000	42.65000	-16.220	42.238	-88.891	-185.01	-0.0012801
	18.00000	1.00000	42.65000	-16.066	42.238	-88.891	-184.87	-0.0012823
	19.00000	1.00000	42.65000	-15.861	42.238	-88.890	-184.66	-0.0012855
	20.00000	1.00000	42.65000	-15.595	42.238	-88.889	-184.36	-0.0012902
	21.00000	1.00000	42.65000	-15.249	42.238	-88.886	-183.89	-0.0012975
	22.00000	1.00000	42.65000	-14.794	42.238	-88.879	-183.12	-0.0013092



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Ashton Court
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FD		

Name	Location		Z [Level] [m]	Z [m]	Stresses		
	X [m]	Y [m]			Calc Level [mOD]	Vert Stress [kN/m ²]	Sum Princ [kN/m ²]
23.00000	1.00000	42.65000	-14.193	42.238	-88.860	-181.72	-0.0013302
24.00000	1.00000	42.65000	-13.320	42.238	-88.774	-178.65	-0.0013743
25.00000	1.00000	42.65000	-11.981	42.238	-87.929	-168.60	-0.0014921
26.00000	1.00000	42.65000	-8.7043	42.238	-44.446	-92.888	-634.07E-6
0.00000	2.00000	42.65000	-9.5985	42.238	-44.919	-99.143	-558.27E-6
1.00000	2.00000	42.65000	-13.302	42.238	-88.774	-178.53	-0.0013762
2.00000	2.00000	42.65000	-14.717	42.238	-89.699	-190.08	-0.0012387
3.00000	2.00000	42.65000	-15.701	42.238	-89.800	-193.70	-0.0018666
4.00000	2.00000	42.65000	-16.388	42.238	-89.824	-195.34	-0.0011620
5.00000	2.00000	42.65000	-16.891	42.238	-89.831	-196.23	-0.0011485
6.00000	2.00000	42.65000	-17.270	42.238	-89.835	-196.76	-0.0011403
7.00000	2.00000	42.65000	-17.558	42.238	-89.836	-197.10	-0.0011350
8.00000	2.00000	42.65000	-17.778	42.238	-89.837	-197.33	-0.0011314
9.00000	2.00000	42.65000	-17.944	42.238	-89.838	-197.49	-0.0011290
10.00000	2.00000	42.65000	-18.064	42.238	-89.838	-197.59	-0.0011274
11.00000	2.00000	42.65000	-18.146	42.238	-89.838	-197.66	-0.0011264
12.00000	2.00000	42.65000	-18.194	42.238	-89.838	-197.70	-0.0011258
13.00000	2.00000	42.65000	-18.210	42.238	-89.838	-197.71	-0.0011256
14.00000	2.00000	42.65000	-18.194	42.238	-89.838	-197.70	-0.0011258
15.00000	2.00000	42.65000	-18.146	42.238	-89.838	-197.66	-0.0011264
16.00000	2.00000	42.65000	-18.064	42.238	-89.838	-197.59	-0.0011274
17.00000	2.00000	42.65000	-17.944	42.238	-89.838	-197.49	-0.0011290
18.00000	2.00000	42.65000	-17.778	42.238	-89.837	-197.33	-0.0011314
19.00000	2.00000	42.65000	-17.558	42.238	-89.836	-197.10	-0.0011350
20.00000	2.00000	42.65000	-17.270	42.238	-89.835	-196.76	-0.0011403
21.00000	2.00000	42.65000	-16.891	42.238	-89.831	-196.23	-0.0011485
22.00000	2.00000	42.65000	-16.388	42.238	-89.824	-195.34	-0.0011620
23.00000	2.00000	42.65000	-15.701	42.238	-89.800	-193.70	-0.0018666
24.00000	2.00000	42.65000	-14.717	42.238	-89.699	-190.08	-0.0012387
25.00000	2.00000	42.65000	-13.302	42.238	-88.774	-178.53	-0.0013762
26.00000	3.00000	42.65000	-9.5985	42.238	-44.919	-99.143	-558.27E-6
0.00000	3.00000	42.65000	-10.112	42.238	-44.974	-101.18	-528.87E-6
1.00000	3.00000	42.65000	-13.842	42.238	-88.859	-181.40	-0.0013352
2.00000	3.00000	42.65000	-15.498	42.238	-89.800	-193.50	-0.0011897
3.00000	3.00000	42.65000	-16.562	42.238	-89.906	-197.42	-0.0011333
4.00000	3.00000	42.65000	-17.302	42.238	-89.931	-199.23	-0.0010916
5.00000	3.00000	42.65000	-17.842	42.238	-89.940	-200.18	-0.0010916
6.00000	3.00000	42.65000	-18.245	42.238	-89.944	-200.76	-0.0010827
7.00000	3.00000	42.65000	-18.551	42.238	-89.945	-201.13	-0.0010770
8.00000	3.00000	42.65000	-18.782	42.238	-89.946	-201.37	-0.0010732
9.00000	3.00000	42.65000	-18.956	42.238	-89.947	-201.54	-0.0010689
10.00000	3.00000	42.65000	-19.082	42.238	-89.947	-201.65	-0.0010689
11.00000	3.00000	42.65000	-19.168	42.238	-89.947	-201.72	-0.0010678
12.00000	3.00000	42.65000	-19.218	42.238	-89.947	-201.76	-0.0010672
13.00000	3.00000	42.65000	-19.234	42.238	-89.947	-201.77	-0.0010670
14.00000	3.00000	42.65000	-19.218	42.238	-89.947	-201.76	-0.0010672
15.00000	3.00000	42.65000	-19.168	42.238	-89.947	-201.72	-0.0010678
16.00000	3.00000	42.65000	-19.082	42.238	-89.947	-201.65	-0.0010689
17.00000	3.00000	42.65000	-18.956	42.238	-89.947	-201.54	-0.0010706
18.00000	3.00000	42.65000	-18.782	42.238	-89.946	-201.37	-0.0010732
19.00000	3.00000	42.65000	-18.551	42.238	-89.945	-201.13	-0.0010770
20.00000	3.00000	42.65000	-18.245	42.238	-89.944	-200.76	-0.0010827
21.00000	3.00000	42.65000	-17.842	42.238	-89.940	-200.18	-0.0010916
22.00000	3.00000	42.65000	-17.302	42.238	-89.931	-199.23	-0.0011064
23.00000	3.00000	42.65000	-16.562	42.238	-89.906	-197.42	-0.0011333
24.00000	3.00000	42.65000	-15.498	42.238	-89.808	-193.50	-0.0011897
25.00000	3.00000	42.65000	-13.842	42.238	-88.859	-181.40	-0.0013352
26.00000	3.00000	42.65000	-10.112	42.238	-44.974	-101.18	-528.87E-6
0.00000	4.00000	42.65000	-10.395	42.238	-44.987	-102.01	-516.50E-6
1.00000	4.00000	42.65000	-14.194	42.238	-88.877	-182.50	-0.0013188
2.00000	4.00000	42.65000	-15.908	42.238	-89.821	-194.81	-0.0011702
3.00000	4.00000	42.65000	-17.016	42.238	-89.930	-198.87	-0.0011117
4.00000	4.00000	42.65000	-17.788	42.238	-89.956	-200.74	-0.0010836
5.00000	4.00000	42.65000	-18.350	42.238	-89.965	-201.76	-0.0010681
6.00000	4.00000	42.65000	-18.769	42.238	-89.969	-202.37	-0.0010587
7.00000	4.00000	42.65000	-19.085	42.238	-89.971	-202.75	-0.0010528
8.00000	4.00000	42.65000	-19.324	42.238	-89.972	-203.01	-0.0010488
9.00000	4.00000	42.65000	-19.502	42.238	-89.972	-203.18	-0.0010461
10.00000	4.00000	42.65000	-19.632	42.238	-89.972	-203.29	-0.0010443
11.00000	4.00000	42.65000	-19.720	42.238	-89.973	-203.37	-0.0010432
12.00000	4.00000	42.65000	-19.771	42.238	-89.973	-203.41	-0.0010426
13.00000	4.00000	42.65000	-19.788	42.238	-89.973	-203.42	-0.0010424
14.00000	4.00000	42.65000	-19.771	42.238	-89.973	-203.41	-0.0010426
15.00000	4.00000	42.65000	-19.720	42.238	-89.973	-203.37	-0.0010432
16.00000	4.00000	42.65000	-19.632	42.238	-89.972	-203.29	-0.0010443
17.00000	4.00000	42.65000	-19.502	42.238	-89.972	-203.18	-0.0010461
18.00000	4.00000	42.65000	-19.324	42.238	-89.972	-203.01	-0.0010488
19.00000	4.00000	42.65000	-19.085	42.238	-89.971	-202.75	-0.0010528
20.00000	4.00000	42.65000	-18.769	42.238	-89.969	-202.37	-0.0010587
21.00000	4.00000	42.65000	-18.350	42.238	-89.965	-201.76	-0.0010681
22.00000	4.00000	42.65000	-17.788	42.238	-89.956	-200.74	-0.0010836
23.00000	4.00000	42.65000	-17.016	42.238	-89.930	-198.87	-0.0011117
24.00000	4.00000	42.65000	-15.908	42.238	-89.821	-194.81	-0.0011702
25.00000	4.00000	42.65000	-14.194	42.238	-88.877	-182.50	-0.0013188
26.00000	4.00000	42.65000	-10.395	42.238	-44.987	-102.01	-516.50E-6
0.00000	5.00000	42.65000	-10.486	42.238	-44.989	-102.23	-512.98E-6
1.00000	5.00000	42.65000	-14.305	42.238	-88.881	-182.80	-0.0013142
2.00000	5.00000	42.65000	-16.037	42.238	-89.826	-195.17	-0.0011648
3.00000	5.00000	42.65000	-17.158	42.238	-89.935	-199.27	-0.0011057
4.00000	5.00000	42.65000	-17.941	42.238	-89.962	-201.16	-0.0010772
5.00000	5.00000	42.65000	-18.510	42.238	-89.971	-202.21	-0.0010617
6.00000	5.00000	42.65000	-18.934	42.238	-89.974	-202.81	-0.0010520
7.00000	5.00000	42.65000	-19.254	42.238	-89.976	-203.21	-0.0010459
8.00000	5.00000	42.65000	-19.495	42.238	-89.977	-203.46	-0.0010419
9.00000	5.00000	42.65000	-19.676	42.238	-89.978	-203.64	-0.0010392
10.00000	5.00000	42.65000	-19.807	42.238	-89.978	-203.75	-0.0010374
11.00000	5.00000	42.65000	-19.896	42.238	-89.978	-203.83	-0.0010362
12.00000	5.00000	42.65000	-19.947	42.238	-89.978	-203.87	-0.0010356
13.00000	5.00000	42.65000	-19.964	42.238	-89.978	-203.88	-0.0010354
14.00000	5.00000	42.65000	-19.947	42.238	-89.978	-203.87	-0.0010356
15.00000	5.00000	42.65000	-19.896	42.238	-89.978	-203.83	-0.0010362
16.00000	5.00000	42.65000	-19.807	42.238	-89.978	-203.75	-0.0010374
17.00000	5.00000	42.65000	-19.676	42.238	-89.978	-203.64	-0.0010392
18.00000	5.00000	42.65000	-19.495	42.238	-89.977	-203.46	-0.0010419
19.00000	5.00000	42.65000	-19.254	42.238	-89.976	-203.21	-0.0010459
20.00000	5.00000	42.65000	-18.934	42.238	-89.974	-202.81	-0.0010520
21.00000	5.00000	42.65000	-18.510	42.238	-89.971	-202.20	-0.0010614
22.00000	5.00000	42.65000	-17.941	42.238	-89.962	-201.16	-0.0010772
23.00000	5.00000	42.65000	-17.158	42.238	-89.935	-199.27	-0.0011057
24.00000	5.00000	42.65000	-16.037	42.238	-89.826	-195.17	-0.0011648
25.00000	5.00000	42.65000	-14.305	42.238	-88.881	-182.80	-0.0013142
26.00000	5.00000	42.65000	-10.486	42.238	-44.989	-102.23	-512.98E-6
0.00000	6.00000	42.65000	-10.395	42.238	-44.987	-102.01	-516.50E-6
1.00000	6.00000	42.65000	-14.194	42.238	-88.877	-182.50	-0.0013188
2.00000	6.00000	42.65000	-15.908	42.238	-89.821	-194.81	-0.0011702
3.00000	6.00000	42.65000	-17.016	42.238	-89.930	-198.87	-0.0011117
4.00000	6.00000	42.65000	-17.788	42.238	-89.956	-200.74	-0.0010836
5.00000	6.00000	42.65000	-18.350	42.238	-89.965	-201.76	-0.0010681



CAMPBELLREITH - LONDON

Ashton Court
Demolition & Basement excavation
Immediate heave

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [Level] [m]	Z [m]	Stresses			
	X [m]	Y [m]			Calc Level [mOD]	Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
	18.00000	6.00000	42.65000	-19.324	42.238	-89.972	-203.01	-0.0010488
	19.00000	6.00000	42.65000	-19.085	42.238	-89.971	-202.75	-0.0010528
	20.00000	6.00000	42.65000	-18.769	42.238	-89.969	-202.37	-0.0010587
	21.00000	6.00000	42.65000	-18.350	42.238	-89.965	-201.76	-0.0010681
	22.00000	6.00000	42.65000	-17.789	42.238	-89.956	-200.74	-0.0010836
	23.00000	6.00000	42.65000	-17.016	42.238	-89.930	-198.87	-0.0011117
	24.00000	6.00000	42.65000	-15.908	42.238	-89.821	-194.81	-0.0011702
	25.00000	6.00000	42.65000	-14.194	42.238	-88.877	-182.50	-0.0013188
	26.00000	6.00000	42.65000	-10.395	42.238	-44.987	-102.01	-516.50E-6
	0.00000	7.00000	42.65000	-10.112	42.238	-44.974	-101.18	-528.87E-6
	1.00000	7.00000	42.65000	-13.842	42.238	-88.959	-181.40	-0.0013352
	2.00000	7.00000	42.65000	-15.498	42.238	-89.800	-193.50	-0.0011897
	3.00000	7.00000	42.65000	-16.562	42.238	-89.906	-197.42	-0.0011333
	4.00000	7.00000	42.65000	-17.302	42.238	-89.931	-199.21	-0.0011064
	5.00000	7.00000	42.65000	-17.842	42.238	-89.940	-200.18	-0.0010916
	6.00000	7.00000	42.65000	-18.245	42.238	-89.944	-200.76	-0.0010827
	7.00000	7.00000	42.65000	-18.551	42.238	-89.945	-201.13	-0.0010770
	8.00000	7.00000	42.65000	-18.782	42.238	-89.946	-201.37	-0.0010732
	9.00000	7.00000	42.65000	-18.956	42.238	-89.947	-201.54	-0.0010706
	10.00000	7.00000	42.65000	-19.082	42.238	-89.947	-201.65	-0.0010689
	11.00000	7.00000	42.65000	-19.168	42.238	-89.947	-201.72	-0.0010676
	12.00000	7.00000	42.65000	-19.218	42.238	-89.947	-201.76	-0.0010672
	13.00000	7.00000	42.65000	-19.234	42.238	-89.947	-201.77	-0.0010670
	14.00000	7.00000	42.65000	-19.218	42.238	-89.947	-201.76	-0.0010672
	15.00000	7.00000	42.65000	-19.168	42.238	-89.947	-201.72	-0.0010678
	16.00000	7.00000	42.65000	-19.082	42.238	-89.947	-201.65	-0.0010690
	17.00000	7.00000	42.65000	-18.956	42.238	-89.947	-201.54	-0.0010706
	18.00000	7.00000	42.65000	-18.782	42.238	-89.946	-201.37	-0.0010732
	19.00000	7.00000	42.65000	-18.551	42.238	-89.945	-201.13	-0.0010770
	20.00000	7.00000	42.65000	-18.245	42.238	-89.944	-200.76	-0.0010827
	21.00000	7.00000	42.65000	-17.842	42.238	-89.940	-200.18	-0.0010916
	22.00000	7.00000	42.65000	-17.302	42.238	-89.931	-199.21	-0.0011064
	23.00000	7.00000	42.65000	-16.562	42.238	-89.906	-197.42	-0.0011333
	24.00000	7.00000	42.65000	-15.498	42.238	-89.800	-193.50	-0.0011897
	25.00000	7.00000	42.65000	-13.842	42.238	-88.959	-181.40	-0.0013352
	26.00000	7.00000	42.65000	-10.395	42.238	-44.974	-101.18	-528.87E-6
	0.00000	8.00000	42.65000	-9.5885	42.238	-44.919	-99.143	-558.27E-6
	1.00000	8.00000	42.65000	-13.175	42.238	-88.774	-178.53	-0.0013762
	2.00000	8.00000	42.65000	-14.717	42.238	-89.699	-190.08	-0.0012387
	3.00000	8.00000	42.65000	-15.701	42.238	-89.800	-193.70	-0.0011866
	4.00000	8.00000	42.65000	-16.388	42.238	-89.824	-195.34	-0.0011620
	5.00000	8.00000	42.65000	-16.891	42.238	-89.831	-196.23	-0.0011485
	6.00000	8.00000	42.65000	-17.270	42.238	-89.835	-196.76	-0.0011403
	7.00000	8.00000	42.65000	-17.558	42.238	-89.836	-197.10	-0.0011350
	8.00000	8.00000	42.65000	-17.778	42.238	-89.837	-197.33	-0.0011314
	9.00000	8.00000	42.65000	-17.944	42.238	-89.838	-197.49	-0.0011290
	10.00000	8.00000	42.65000	-18.064	42.238	-89.838	-197.59	-0.0011274
	11.00000	8.00000	42.65000	-18.146	42.238	-89.838	-197.66	-0.0011264
	12.00000	8.00000	42.65000	-18.194	42.238	-89.838	-197.70	-0.0011258
	13.00000	8.00000	42.65000	-18.210	42.238	-89.838	-197.71	-0.0011256
	14.00000	8.00000	42.65000	-18.194	42.238	-89.838	-197.70	-0.0011258
	15.00000	8.00000	42.65000	-18.146	42.238	-89.838	-197.66	-0.0011264
	16.00000	8.00000	42.65000	-18.064	42.238	-89.838	-197.59	-0.0011274
	17.00000	8.00000	42.65000	-17.944	42.238	-89.838	-197.49	-0.0011290
	18.00000	8.00000	42.65000	-17.778	42.238	-89.837	-197.33	-0.0011314
	19.00000	8.00000	42.65000	-17.558	42.238	-89.836	-197.10	-0.0011350
	20.00000	8.00000	42.65000	-17.270	42.238	-89.835	-196.76	-0.0011403
	21.00000	8.00000	42.65000	-16.891	42.238	-89.831	-196.23	-0.0011485
	22.00000	8.00000	42.65000	-16.388	42.238	-89.824	-195.34	-0.0011620
	23.00000	8.00000	42.65000	-15.701	42.238	-89.800	-193.70	-0.0011866
	24.00000	8.00000	42.65000	-14.717	42.238	-89.699	-190.08	-0.0012387
	25.00000	8.00000	42.65000	-13.175	42.238	-88.774	-178.53	-0.0013762
	26.00000	8.00000	42.65000	-9.5885	42.238	-44.919	-99.143	-558.27E-6
	0.00000	9.00000	42.65000	-8.7043	42.238	-44.446	-92.888	-634.07E-6
	1.00000	9.00000	42.65000	-11.981	42.238	-87.929	-168.60	-0.0014921
	2.00000	9.00000	42.65000	-13.320	42.238	-88.774	-178.65	-0.0013743
	3.00000	9.00000	42.65000	-14.183	42.238	-88.860	-181.72	-0.0013302
	4.00000	9.00000	42.65000	-14.794	42.238	-88.879	-183.12	-0.0013092
	5.00000	9.00000	42.65000	-15.249	42.238	-88.886	-183.89	-0.0012975
	6.00000	9.00000	42.65000	-15.595	42.238	-88.889	-184.36	-0.0012902
	7.00000	9.00000	42.65000	-15.861	42.238	-88.890	-184.66	-0.0012855
	8.00000	9.00000	42.65000	-16.066	42.238	-88.891	-184.87	-0.0012823
	9.00000	9.00000	42.65000	-16.220	42.238	-88.891	-185.01	-0.0012801
	10.00000	9.00000	42.65000	-16.334	42.238	-88.891	-185.11	-0.0012786
	11.00000	9.00000	42.65000	-16.411	42.238	-88.891	-185.17	-0.0012776
	12.00000	9.00000	42.65000	-16.456	42.238	-88.892	-185.20	-0.0012771
	13.00000	9.00000	42.65000	-16.471	42.238	-88.892	-185.22	-0.0012769
	14.00000	9.00000	42.65000	-16.456	42.238	-88.892	-185.20	-0.0012771
	15.00000	9.00000	42.65000	-16.411	42.238	-88.891	-185.17	-0.0012776
	16.00000	9.00000	42.65000	-16.334	42.238	-88.891	-185.11	-0.0012786
	17.00000	9.00000	42.65000	-16.220	42.238	-88.891	-185.01	-0.0012801
	18.00000	9.00000	42.65000	-16.066	42.238	-88.891	-184.87	-0.0012823
	19.00000	9.00000	42.65000	-15.861	42.238	-88.890	-184.66	-0.0012855
	20.00000	9.00000	42.65000	-15.595	42.238	-88.889	-184.36	-0.0012902
	21.00000	9.00000	42.65000	-15.249	42.238	-88.886	-183.89	-0.0012975
	22.00000	9.00000	42.65000	-14.794	42.238	-88.879	-183.12	-0.0013092
	23.00000	9.00000	42.65000	-14.183	42.238	-88.860	-181.72	-0.0013302
	24.00000	9.00000	42.65000	-13.320	42.238	-88.774	-178.65	-0.0013743
	25.00000	9.00000	42.65000	-11.981	42.238	-87.929	-168.60	-0.0014921
	26.00000	9.00000	42.65000	-8.7043	42.238	-44.446	-92.888	-634.07E-6
	0.00000	10.00000	42.65000	-6.7342	42.238	-22.499	-52.483	-235.36E-6
	1.00000	10.00000	42.65000	-8.8092	42.238	-44.446	-92.967	-632.83E-6
	2.00000	10.00000	42.65000	-9.8331	42.238	-44.920	-99.341	-555.19E-6
	3.00000	10.00000	42.65000	-10.539	42.238	-44.975	-101.56	-523.07E-6
	4.00000	10.00000	42.65000	-11.061	42.238	-44.989	-102.64	-506.67E-6
	5.00000	10.00000	42.65000	-11.458	42.238	-44.994	-103.27	-497.06E-6
	6.00000	10.00000	42.65000	-11.766	42.238	-44.996	-103.67	-490.94E-6
	7.00000	10.00000	42.65000	-12.007	42.238	-44.997	-103.93	-486.84E-6
	8.00000	10.00000	42.65000	-12.193	42.238	-44.998	-104.11	-484.02E-6
	9.00000	10.00000	42.65000	-12.335	42.238	-44.998	-104.24	-482.05E-6
	10.00000	10.00000	42.65000	-12.440	42.238	-44.998	-104.33	-480.69E-6
	11.00000	10.00000	42.65000	-12.512	42.238	-44.998	-104.39	-479.81E-6
	12.00000	10.00000	42.65000	-12.554	42.238	-44.998	-104.42	-479.31E-6
	13.00000	10.00000	42.65000	-12.567	42.238	-44.998	-104.43	-479.15E-6
	14.00000	10.00000	42.65000	-12.554	42.238	-44.998	-104.42	-479.31E-6
	15.00000	10.00000	42.65000	-12.512	42.238	-44.998	-104.39	-479.81E-6
	16.00000	10.00000	42.65000	-12.440	42.238	-44.998	-104.33	-480.69E-6
	17.00000	10.00000	42.65000	-12.335	42.238	-44.998	-104.24	-482.05E-6
	18.00000	10.00000	42.65000	-12.193	42.238	-44.998	-104.11	-484.02E-6
	19.00000	10.00000	42.65000	-12.007	42.238	-44.997	-103.93	-486.84E-6
	20.00000	10.00000	42.65000	-11.766	42.238	-44.996	-103.67	-490.94E-6
	21.00000	10.00000	42.65000	-11.458	42.238	-44.994	-103.27	-497.06E-6
	22.00000	10.00000	42.65000	-11.061	42.238	-44.989	-102.64	-506.67E-6
	23.00000	10.0000						



**CAMPBELLREITH -
LONDON**

Ashton Court
Demolition & Basement excavation
Immediate heave

Job No. Sheet No. Rev.

12047

Drg. Ref.

Made by
FD

Date

Checked

Name	X [m]	Location		Z [Level] [mOD]	Z [mm]	Stresses		
		Y [m]	Z [Level] [mOD]			Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
	-4.50000	4.00000	44.75000	-2.6602	44.537	0.0	0.0	0.0
	-4.50000	5.00000	44.75000	-2.6835	44.537	0.0	0.0	0.0
	-4.50000	6.00000	44.75000	-2.6602	44.537	0.0	0.0	0.0
	-4.50000	7.00000	44.75000	-2.5912	44.537	0.0	0.0	0.0
	-4.50000	8.00000	44.75000	-2.4799	44.537	0.0	0.0	0.0
GL3	-9.00000	0.00000	44.75000	-0.96001	44.537	0.0	0.0	0.0
	-9.00000	1.00000	44.75000	-1.0091	44.537	0.0	0.0	0.0
	-9.00000	2.00000	44.75000	-1.0497	44.537	0.0	0.0	0.0
	-9.00000	3.00000	44.75000	-1.0800	44.537	0.0	0.0	0.0
	-9.00000	4.00000	44.75000	-1.0988	44.537	0.0	0.0	0.0
	-9.00000	5.00000	44.75000	-1.1052	44.537	0.0	0.0	0.0
	-9.00000	6.00000	44.75000	-1.0988	44.537	0.0	0.0	0.0
	-9.00000	7.00000	44.75000	-1.0800	44.537	0.0	0.0	0.0
	-9.00000	8.00000	44.75000	-1.0497	44.537	0.0	0.0	0.0
GL4	0.00000	4.00000	44.75000	-10.315	44.537	0.0	0.0	0.0
	-1.00000	4.00000	44.75000	-6.6205	44.537	0.0	0.0	0.0
	-2.00000	4.00000	44.75000	-4.8830	44.537	0.0	0.0	0.0
	-3.00000	4.00000	44.75000	-3.7610	44.537	0.0	0.0	0.0
	-4.00000	4.00000	44.75000	-2.9720	44.537	0.0	0.0	0.0
	-5.00000	4.00000	44.75000	-2.3898	44.537	0.0	0.0	0.0
	-6.00000	4.00000	44.75000	-1.9458	44.537	0.0	0.0	0.0
	-7.00000	4.00000	44.75000	-1.5988	44.537	0.0	0.0	0.0
	-8.00000	4.00000	44.75000	-1.3224	44.537	0.0	0.0	0.0
	-9.00000	4.00000	44.75000	-1.0988	44.537	0.0	0.0	0.0
GL5	13.00000	-6.00000	44.75000	-3.0813	44.537	0.0	0.0	0.0
	13.00000	-7.00000	44.75000	-2.5959	44.537	0.0	0.0	0.0
	13.00000	-8.00000	44.75000	-2.1968	44.537	0.0	0.0	0.0
	13.00000	-9.00000	44.75000	-1.8652	44.537	0.0	0.0	0.0
	13.00000	-10.00000	44.75000	-1.5872	44.537	0.0	0.0	0.0
	13.00000	-11.00000	44.75000	-1.3525	44.537	0.0	0.0	0.0
	13.00000	-12.00000	44.75000	-1.1532	44.537	0.0	0.0	0.0
GL6	26.00000	-6.00000	44.75000	-1.8423	44.537	0.0	0.0	0.0
	26.00000	-7.00000	44.75000	-1.5732	44.537	0.0	0.0	0.0
	26.00000	-8.00000	44.75000	-1.3479	44.537	0.0	0.0	0.0
	26.00000	-9.00000	44.75000	-1.1572	44.537	0.0	0.0	0.0
	26.00000	-10.00000	44.75000	-0.99448	44.537	0.0	0.0	0.0
	26.00000	-11.00000	44.75000	-0.85467	44.537	0.0	0.0	0.0
	26.00000	-12.00000	44.75000	-0.73392	44.537	0.0	0.0	0.0



CAMPBELLREITH - LONDON

Job No. Sheet No. Rev.

12047

Ashton Court
Demolition & Basement excavation
Total heave

Drg. Ref.

Made by
FD

Date

Checked

Notes

E = 0.75Eu
Eu = 400Cu
Cu = 70+6z

Analysis Options

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Maximum allowable ratio between values of E: 1.5
Horizontal rigid boundary level: 0.00 [m OD]
Displacements at area centroids calculated.

Soil Profiles/Soil Profile

Layer	Level at top	Number of intermediate displacement levels	Youngs Modulus		Poissons ratio	Non-linear curve
			Top	Btm		
	[mOD]		[kN/m ²]	[kN/m ²]		
1	45.400	2	5000.0	5000.0	0.20000	None
2	43.900	43	21000.	98400.	0.20000	None

Soil Zones

Zone	Name	X coordinates min	X coordinates max	Y coordinates min	Y coordinates max	Profile
		[m]	[m]	[m]	[m]	
1	SZ1	-60.000	60.000	-60.000	60.000	Soil Profile

Non-linear Curve Coordinates - Non-linear Curve 1

Point Strain Factor
[%]

Load Data

Load ref.	Name	Shape	Orientation of Plane	Centre of load (Global)			Angle of local x from	Width x or Radius	Length y	Polygon Coordinates	Number of tolerance rectangles	Load value			
				X	Y	Z (level)						Normal (local z)	Tangential (local x)	Tangential (local y)	
				[m]	[m]	[m]	[Degrees]	[m]	[m]	[m]		[kN/m ²]	[kN/m ²]	[kN/m ²]	
1	Basement	Rectangular	Horizontal	13.000	5.0000	42.650	0.0	26.000	10.000	N/A	N/A	1	-90.000	0.0	0.0

Displacement Data

Ref.	Type	Name	Direction of Extrusion	Line/Line for extrusion			No. of intrvl across extrusion/line	Extrusion Depth	No. of intrvl along extrusion	Calculate	Detailed results			
				X	Y	Z (level)								
				[m]	[m]	[m]								
1	Grid	BL	Global X	0.0	0.0	42.650	N/A	10.000	42.650	10	26.000	26	Yes	No
2	Line	GL1	N/A	0.0	0.0	44.750	0.0	8.0000	44.750	8	N/A	N/A	Yes	No
3	Line	GL2	N/A	-4.5000	0.0	44.750	-4.5000	8.0000	44.750	8	N/A	N/A	Yes	No
4	Line	GL3	N/A	-9.0000	0.0	44.750	-9.0000	8.0000	44.750	8	N/A	N/A	Yes	No
5	Line	N/A	N/A	0.0	4.0000	44.750	-9.0000	4.0000	44.750	8	N/A	N/A	Yes	No
6	Line	GL5	N/A	13.000	-6.0000	44.750	13.000	-12.000	44.750	6	N/A	N/A	Yes	No
7	Line	GL6	N/A	26.000	-6.0000	44.750	26.000	-12.000	44.750	6	N/A	N/A	Yes	No

RESULTS FOR GRIDS

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Horizontal rigid boundary level: 0.00 [m OD]

The maximum displacement difference between Boussinesq method (-16.071mm) and Mindlin method (-14.538mm) occurs at point X=0.0m Y=4.0000m Level 44.750mOD and is 1.5325mm

Name	Location		Z [Level]	Z [mm]	Stresses			Vert Strain
	X [m]	Y [m]			Calc Level [mOD]	Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	
Basement	13.00000	5.00000	42.65000	-30.753	42.238	-89.978	-203.88	-0.0028089
BL	0.00000	0.00000	42.65000	-10.874	42.238	-22.499	-52.483	-689.82E-6
	1.00000	0.00000	42.65000	-13.926	42.238	-44.446	-92.967	-0.0014522
	2.00000	0.00000	42.65000	-15.487	42.238	-44.920	-99.341	-0.0014227
	3.00000	0.00000	42.65000	-16.575	42.238	-44.975	-101.56	-0.0014070
	4.00000	0.00000	42.65000	-17.386	42.238	-44.989	-102.64	-0.0013986
	5.00000	0.00000	42.65000	-18.010	42.238	-44.994	-103.27	-0.0013936
	6.00000	0.00000	42.65000	-18.497	42.238	-44.996	-103.67	-0.0013904
	7.00000	0.00000	42.65000	-18.878	42.238	-44.997	-103.93	-0.0013882
	8.00000	0.00000	42.65000	-19.176	42.238	-44.998	-104.11	-0.0013867
	9.00000	0.00000	42.65000	-19.404	42.238	-44.998	-104.24	-0.0013857
	10.00000	0.00000	42.65000	-19.573	42.238	-44.998	-104.33	-0.0013849
	11.00000	0.00000	42.65000	-19.689	42.238	-44.998	-104.39	-0.0013845
	12.00000	0.00000	42.65000	-19.757	42.238	-44.998	-104.42	-0.0013842
	13.00000	0.00000	42.65000	-19.779	42.238	-44.998	-104.43	-0.0013841
	14.00000	0.00000	42.65000	-19.757	42.238	-44.998	-104.42	-0.0013842
	15.00000	0.00000	42.65000	-19.689	42.238	-44.998	-104.39	-0.0013845
	16.00000	0.00000	42.65000	-19.573	42.238	-44.998	-104.33	-0.0013849
	17.00000	0.00000	42.65000	-19.404	42.238	-44.998	-104.24	-0.0013857
	18.00000	0.00000	42.65000	-19.176	42.238	-44.998	-104.11	-0.0013867
	19.00000	0.00000	42.65000	-18.878	42.238	-44.997	-103.93	-0.0013882
	20.00000	0.00000	42.65000	-18.497	42.238	-44.996	-103.67	-0.0013904
	21.00000	0.00000	42.65000	-18.010	42.238	-44.994	-103.27	-0.0013936
	22.00000	0.00000	42.65000	-17.386	42.238	-44.989	-102.64	-0.0013986
	23.00000	0.00000	42.65000	-16.575	42.238	-44.975	-101.56	-0.0014070
	24.00000	0.00000	42.65000	-15.487	42.238	-44.920	-99.341	-0.0014227
	25.00000	0.00000	42.65000	-13.926	42.238	-44.446	-92.967	-0.0014522
	26.00000	0.00000	42.65000	-10.874	42.238	-22.499	-52.483	-689.82E-6
	0.00000	1.00000	42.65000	-13.753	42.238	-44.446	-92.888	-0.0014529
	1.00000	1.00000	42.65000	-18.519	42.238	-87.929	-169.60	-0.0030111
	2.00000	1.00000	42.65000	-20.552	42.238	-88.774	-178.65	-0.0029594
	3.00000	1.00000	42.65000	-21.874	42.238	-88.860	-181.72	-0.0029381
	4.00000	1.00000	42.65000	-22.821	42.238	-88.879	-183.12	-0.0029274
	5.00000	1.00000	42.65000	-23.532	42.238	-88.886	-183.89	-0.0029213
	6.00000	1.00000	42.65000	-24.077	42.238	-88.889	-184.36	-0.0029175
	7.00000	1.00000	42.65000	-24.499	42.238	-88.890	-184.66	-0.0029150
	8.00000	1.00000	42.65000	-24.824	42.238	-88.891	-184.87	-0.0029133
	9.00000	1.00000	42.65000	-25.072	42.238	-88.891	-185.01	-0.0029121
	10.00000	1.00000	42.65000	-25.254	42.238	-88.891	-185.11	-0.0029113
	11.00000	1.00000	42.65000	-25.379	42.238	-88.891	-185.17	-0.0029108
	12.00000	1.00000	42.65000	-25.452	42.238	-88.892	-185.20	-0.0029105
	13.00000	1.00000	42.65000	-25.476	42.238	-88.892	-185.22	-0.0029104
	14.00000	1.00000	42.65000	-25.452	42.238	-88.892	-185.20	-0.0029105
	15.00000	1.00000	42.65000	-25.379	42.238	-88.891	-185.17	-0.0029108
	16.00000	1.00000	42.65000	-25.254	42.238	-88.891	-185.11	-0.0029113
	17.00000	1.00000	42.65000	-25.072	42.238	-88.891	-185.01	-0.0029121
	18.00000	1.00000	42.65000	-24.824	42.238	-88.891	-184.87	-0.0029133
	19.00000	1.00000	42.65000	-24.499	42.238	-88.890	-184.66	-0.0029150
	20.00000	1.00000	42.65000	-24.077	42.238	-88.889	-184.36	-0.0029175
	21.00000	1.00000	42.65000	-23.532	42.238	-88.886	-183.89	-0.0029213



CAMPBELLREITH - LONDON

Ashton Court
Demolition & Basement excavation
Total heave

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [Level] [m]	Z [mOD]	Calc Level [mOD]	Stresses		
	X [m]	Y [m]				Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
22.00000	1.00000	42.65000	-22.821	42.238	-88.879	-183.12	-0.0029274	
23.00000	1.00000	42.65000	-21.874	42.238	-88.860	-181.72	-0.0029381	
24.00000	1.00000	42.65000	-20.552	42.238	-88.774	-178.65	-0.0029594	
25.00000	1.00000	42.65000	-18.519	42.238	-87.929	-168.60	-0.0030011	
26.00000	1.00000	42.65000	-13.753	42.238	-44.446	-92.888	-0.0014529	
2.00000	2.00000	42.65000	-15.097	42.238	-44.919	-99.143	-0.0014243	
1.00000	2.00000	42.65000	-20.317	42.238	-88.774	-178.53	-0.0029605	
2.00000	2.00000	42.65000	-22.651	42.238	-89.699	-190.08	-0.0029103	
3.00000	2.00000	42.65000	-24.155	42.238	-89.800	-193.70	-0.0028851	
4.00000	2.00000	42.65000	-25.217	42.238	-89.824	-195.34	-0.0028726	
5.00000	2.00000	42.65000	-26.001	42.238	-89.831	-196.23	-0.0028655	
6.00000	2.00000	42.65000	-26.596	42.238	-89.835	-196.76	-0.0028612	
7.00000	2.00000	42.65000	-27.052	42.238	-89.836	-197.10	-0.0028585	
8.00000	2.00000	42.65000	-27.402	42.238	-89.837	-197.33	-0.0028566	
9.00000	2.00000	42.65000	-27.666	42.238	-89.838	-197.49	-0.0028553	
10.00000	2.00000	42.65000	-27.860	42.238	-89.838	-197.59	-0.0028545	
11.00000	2.00000	42.65000	-27.992	42.238	-89.838	-197.66	-0.0028539	
12.00000	2.00000	42.65000	-28.069	42.238	-89.838	-197.70	-0.0028536	
13.00000	2.00000	42.65000	-28.094	42.238	-89.838	-197.71	-0.0028535	
14.00000	2.00000	42.65000	-28.069	42.238	-89.838	-197.70	-0.0028536	
15.00000	2.00000	42.65000	-27.992	42.238	-89.838	-197.66	-0.0028539	
16.00000	2.00000	42.65000	-27.860	42.238	-89.838	-197.59	-0.0028545	
17.00000	2.00000	42.65000	-27.666	42.238	-89.838	-197.49	-0.0028553	
18.00000	2.00000	42.65000	-27.402	42.238	-89.837	-197.33	-0.0028566	
19.00000	2.00000	42.65000	-27.052	42.238	-89.836	-197.10	-0.0028585	
20.00000	2.00000	42.65000	-26.596	42.238	-89.835	-196.76	-0.0028612	
21.00000	2.00000	42.65000	-26.001	42.238	-89.831	-196.23	-0.0028655	
22.00000	2.00000	42.65000	-25.217	42.238	-89.824	-195.34	-0.0028726	
23.00000	2.00000	42.65000	-24.155	42.238	-89.800	-193.70	-0.0028851	
24.00000	2.00000	42.65000	-22.651	42.238	-89.699	-190.08	-0.0029103	
25.00000	2.00000	42.65000	-20.317	42.238	-88.774	-178.53	-0.0029605	
26.00000	2.00000	42.65000	-15.087	42.238	-44.919	-99.143	-0.0014243	
0.00000	3.00000	42.65000	-15.881	42.238	-44.974	-101.18	-0.0014100	
1.00000	3.00000	42.65000	-21.325	42.238	-88.859	-181.40	-0.0029407	
2.00000	3.00000	42.65000	-23.830	42.238	-89.800	-193.50	-0.0028867	
3.00000	3.00000	42.65000	-25.455	42.238	-89.906	-197.42	-0.0028413	
4.00000	3.00000	42.65000	-26.598	42.238	-89.931	-199.21	-0.0028456	
5.00000	3.00000	42.65000	-27.438	42.238	-89.940	-200.18	-0.0028379	
6.00000	3.00000	42.65000	-28.070	42.238	-89.944	-200.76	-0.0028333	
7.00000	3.00000	42.65000	-28.553	42.238	-89.945	-201.13	-0.0028303	
8.00000	3.00000	42.65000	-28.920	42.238	-89.946	-201.27	-0.0028280	
9.00000	3.00000	42.65000	-29.198	42.238	-89.947	-201.54	-0.0028269	
10.00000	3.00000	42.65000	-29.400	42.238	-89.947	-201.65	-0.0028260	
11.00000	3.00000	42.65000	-29.538	42.238	-89.947	-201.72	-0.0028254	
12.00000	3.00000	42.65000	-29.618	42.238	-89.947	-201.76	-0.0028251	
13.00000	3.00000	42.65000	-29.644	42.238	-89.947	-201.77	-0.0028250	
14.00000	3.00000	42.65000	-29.618	42.238	-89.947	-201.76	-0.0028251	
15.00000	3.00000	42.65000	-29.538	42.238	-89.947	-201.72	-0.0028254	
16.00000	3.00000	42.65000	-29.400	42.238	-89.947	-201.65	-0.0028260	
17.00000	3.00000	42.65000	-29.198	42.238	-89.947	-201.54	-0.0028269	
18.00000	3.00000	42.65000	-28.920	42.238	-89.946	-201.27	-0.0028303	
19.00000	3.00000	42.65000	-28.553	42.238	-89.945	-201.13	-0.0028333	
20.00000	3.00000	42.65000	-28.070	42.238	-89.944	-200.76	-0.0028379	
21.00000	3.00000	42.65000	-27.438	42.238	-89.940	-200.18	-0.0028413	
22.00000	3.00000	42.65000	-26.598	42.238	-89.931	-199.21	-0.0028456	
23.00000	3.00000	42.65000	-25.455	42.238	-89.906	-197.42	-0.0028513	
24.00000	3.00000	42.65000	-23.830	42.238	-89.800	-193.50	-0.0028867	
25.00000	3.00000	42.65000	-21.325	42.238	-88.859	-181.40	-0.0029407	
26.00000	3.00000	42.65000	-15.881	42.238	-44.974	-101.18	-0.0014100	
0.00000	4.00000	42.65000	-16.312	42.238	-44.987	-102.01	-0.0014037	
1.00000	4.00000	42.65000	-21.859	42.238	-88.877	-182.50	-0.0028769	
2.00000	4.00000	42.65000	-24.452	42.238	-89.821	-194.81	-0.0028769	
3.00000	4.00000	42.65000	-26.143	42.238	-89.930	-198.87	-0.0028484	
4.00000	4.00000	42.65000	-27.334	42.238	-89.956	-200.74	-0.0028341	
5.00000	4.00000	42.65000	-28.208	42.238	-89.965	-201.76	-0.0028260	
6.00000	4.00000	42.65000	-28.864	42.238	-89.969	-202.37	-0.0028211	
7.00000	4.00000	42.65000	-29.362	42.238	-89.971	-202.75	-0.0028180	
8.00000	4.00000	42.65000	-29.742	42.238	-89.972	-203.01	-0.0028159	
9.00000	4.00000	42.65000	-30.027	42.238	-89.972	-203.18	-0.0028145	
10.00000	4.00000	42.65000	-30.234	42.238	-89.972	-203.29	-0.0028135	
11.00000	4.00000	42.65000	-30.376	42.238	-89.973	-203.37	-0.0028129	
12.00000	4.00000	42.65000	-30.458	42.238	-89.973	-203.41	-0.0028126	
13.00000	4.00000	42.65000	-30.485	42.238	-89.973	-203.42	-0.0028125	
14.00000	4.00000	42.65000	-30.458	42.238	-89.973	-203.41	-0.0028126	
15.00000	4.00000	42.65000	-30.376	42.238	-89.973	-203.37	-0.0028129	
16.00000	4.00000	42.65000	-30.234	42.238	-89.972	-203.29	-0.0028135	
17.00000	4.00000	42.65000	-30.027	42.238	-89.972	-203.18	-0.0028145	
18.00000	4.00000	42.65000	-29.742	42.238	-89.972	-203.01	-0.0028159	
19.00000	4.00000	42.65000	-29.362	42.238	-89.971	-202.75	-0.0028180	
20.00000	4.00000	42.65000	-28.864	42.238	-89.969	-202.37	-0.0028211	
21.00000	4.00000	42.65000	-28.208	42.238	-89.965	-201.76	-0.0028260	
22.00000	4.00000	42.65000	-27.334	42.238	-89.956	-200.74	-0.0028341	
23.00000	4.00000	42.65000	-26.143	42.238	-89.930	-198.87	-0.0028484	
24.00000	4.00000	42.65000	-24.452	42.238	-89.821	-194.81	-0.0028769	
25.00000	4.00000	42.65000	-21.859	42.238	-88.877	-182.50	-0.0029324	
26.00000	4.00000	42.65000	-16.312	42.238	-44.987	-102.01	-0.0014037	
0.00000	5.00000	42.65000	-16.450	42.238	-44.989	-102.24	-0.0014019	
1.00000	5.00000	42.65000	-22.028	42.238	-88.881	-182.80	-0.0029301	
2.00000	5.00000	42.65000	-24.647	42.238	-89.826	-195.17	-0.0028741	
3.00000	5.00000	42.65000	-26.360	42.238	-89.935	-199.27	-0.0028453	
4.00000	5.00000	42.65000	-27.567	42.238	-89.962	-201.16	-0.0028308	
5.00000	5.00000	42.65000	-28.452	42.238	-89.971	-202.20	-0.0028226	
6.00000	5.00000	42.65000	-29.116	42.238	-89.974	-202.81	-0.0028176	
7.00000	5.00000	42.65000	-29.620	42.238	-89.976	-203.21	-0.0028145	
8.00000	5.00000	42.65000	-30.003	42.238	-89.977	-203.46	-0.0028123	
9.00000	5.00000	42.65000	-30.291	42.238	-89.978	-203.64	-0.0028109	
10.00000	5.00000	42.65000	-30.500	42.238	-89.978	-203.75	-0.0028100	
11.00000	5.00000	42.65000	-30.643	42.238	-89.978	-203.83	-0.0028093	
12.00000	5.00000	42.65000	-30.726	42.238	-89.978	-203.87	-0.0028090	
13.00000	5.00000	42.65000	-30.753	42.238	-89.978	-203.88	-0.0028089	
14.00000	5.00000	42.65000	-30.726	42.238	-89.978	-203.89	-0.0028090	
15.00000	5.00000	42.65000	-30.643	42.238	-89.978	-203.83	-0.0028093	
16.00000	5.00000	42.65000	-30.500	42.238	-89.978	-203.75	-0.0028100	
17.00000	5.00000	42.65000	-30.291	42.238	-89.978	-203.64	-0.0028109	
18.00000	5.00000	42.65000	-30.003	42.238	-89.977	-203.46	-0.0028123	
19.00000	5.00000	42.65000	-29.620	42.238	-89.976	-203.21	-0.0028145	
20.00000	5.00000	42.65000	-29.116	42.238	-89.974	-202.81	-0.0028176	
21.00000	5.00000	42.65000	-28.452	42.238	-89.971	-202.20	-0.0028226	
22.00000	5.00000	42.65000	-27.567	42.238	-89.962	-201.16	-0.0028308	
23.00000	5.00000	42.65000	-26.360	42.238	-89.935	-199.27	-0.0028453	
24.00000	5.00000	42.65000	-24.647	42.238	-89.826	-195.17	-0.0028741	
25.00000	5.00000	42.65000	-22.028	42.238	-88.881	-182.80	-0.0029301	
26.00000	5.00000	42.65000	-16.450	42.238	-44.989	-102.24	-0.0014019	
0.00000	6.00000	42.65000	-16.312	42.238	-44.987	-102.01	-0.0014037	
1.00000	6.00000	42.65000	-21.859	42.238	-88.877	-182.50	-0.0029324	
2.00000	6.00000	42.65000	-24.452	42.238	-89.821	-194.81	-0.0028769	
3.00000	6.00000	42.65000	-26.143	42.238	-89.930	-198.87	-0.0028484	
4.00000	6.00000	42.65000	-27.334	42.238	-89.956	-200.74	-0.0028341	



**CAMPBELLREITH -
LONDON**

Ashton Court
Demolition & Basement excavation
Total heave

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [Level] [m]	Z [mOD]	Calc Level [mOD]	Stresses		
	X [m]	Y [m]				Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
17.00000	6.00000	42.65000	-30.027	42.238	-89.972	-203.18	-0.0028145	
18.00000	6.00000	42.65000	-29.742	42.238	-89.972	-203.01	-0.0028159	
19.00000	6.00000	42.65000	-29.362	42.238	-89.971	-202.75	-0.0028180	
20.00000	6.00000	42.65000	-28.864	42.238	-89.969	-202.37	-0.0028211	
21.00000	6.00000	42.65000	-28.208	42.238	-89.965	-201.76	-0.0028260	
22.00000	6.00000	42.65000	-27.334	42.238	-89.956	-200.74	-0.0028341	
23.00000	6.00000	42.65000	-26.143	42.238	-89.930	-198.87	-0.0028484	
24.00000	6.00000	42.65000	-24.452	42.238	-89.821	-194.81	-0.0028769	
25.00000	6.00000	42.65000	-21.859	42.238	-88.877	-182.50	-0.0029324	
26.00000	6.00000	42.65000	-16.312	42.238	-44.987	-102.01	-0.0014037	
1.00000	7.00000	42.65000	-15.881	42.238	-44.974	-101.18	-0.0014100	
2.00000	7.00000	42.65000	-21.325	42.238	-88.859	-181.40	-0.0029407	
3.00000	7.00000	42.65000	-23.830	42.238	-89.800	-193.50	-0.0028867	
4.00000	7.00000	42.65000	-25.455	42.238	-89.906	-197.42	-0.0028593	
5.00000	7.00000	42.65000	-26.598	42.238	-89.931	-199.21	-0.0028456	
6.00000	7.00000	42.65000	-27.438	42.238	-89.940	-200.18	-0.0028379	
7.00000	7.00000	42.65000	-28.070	42.238	-89.944	-200.76	-0.0028333	
8.00000	7.00000	42.65000	-28.553	42.238	-89.945	-201.13	-0.0028303	
9.00000	7.00000	42.65000	-28.920	42.238	-89.946	-201.37	-0.0028283	
10.00000	7.00000	42.65000	-29.198	42.238	-89.947	-201.54	-0.0028269	
11.00000	7.00000	42.65000	-29.400	42.238	-89.947	-201.65	-0.0028260	
12.00000	7.00000	42.65000	-29.538	42.238	-89.947	-201.72	-0.0028254	
13.00000	7.00000	42.65000	-29.618	42.238	-89.947	-201.76	-0.0028251	
14.00000	7.00000	42.65000	-29.644	42.238	-89.947	-201.77	-0.0028250	
15.00000	7.00000	42.65000	-29.618	42.238	-89.947	-201.76	-0.0028251	
16.00000	7.00000	42.65000	-29.538	42.238	-89.947	-201.72	-0.0028254	
17.00000	7.00000	42.65000	-29.400	42.238	-89.947	-201.65	-0.0028260	
18.00000	7.00000	42.65000	-29.198	42.238	-89.947	-201.54	-0.0028269	
19.00000	7.00000	42.65000	-28.920	42.238	-89.946	-201.37	-0.0028283	
20.00000	7.00000	42.65000	-28.553	42.238	-89.945	-201.13	-0.0028303	
21.00000	7.00000	42.65000	-28.070	42.238	-89.944	-200.76	-0.0028333	
22.00000	7.00000	42.65000	-27.438	42.238	-89.940	-200.18	-0.0028379	
23.00000	7.00000	42.65000	-26.598	42.238	-89.931	-199.21	-0.0028456	
24.00000	7.00000	42.65000	-25.455	42.238	-89.906	-197.42	-0.0028593	
25.00000	7.00000	42.65000	-23.830	42.238	-89.800	-193.50	-0.0028867	
26.00000	7.00000	42.65000	-21.325	42.238	-88.859	-181.40	-0.0029407	
0.00000	8.00000	42.65000	-15.881	42.238	-44.974	-101.18	-0.0014100	
1.00000	8.00000	42.65000	-15.087	42.238	-44.919	-99.143	-0.0014243	
2.00000	8.00000	42.65000	-20.317	42.238	-88.774	-178.53	-0.0029605	
3.00000	8.00000	42.65000	-22.651	42.238	-89.699	-190.08	-0.0029103	
4.00000	8.00000	42.65000	-24.155	42.238	-89.800	-193.70	-0.0028951	
5.00000	8.00000	42.65000	-25.217	42.238	-89.824	-195.34	-0.0028726	
6.00000	8.00000	42.65000	-26.001	42.238	-89.831	-196.23	-0.0028655	
7.00000	8.00000	42.65000	-26.596	42.238	-89.835	-196.76	-0.0028612	
8.00000	8.00000	42.65000	-27.052	42.238	-89.836	-197.10	-0.0028585	
9.00000	8.00000	42.65000	-27.402	42.238	-89.837	-197.13	-0.0028565	
10.00000	8.00000	42.65000	-27.666	42.238	-89.838	-197.49	-0.0028553	
11.00000	8.00000	42.65000	-27.860	42.238	-89.838	-197.59	-0.0028545	
12.00000	8.00000	42.65000	-27.992	42.238	-89.838	-197.66	-0.0028539	
13.00000	8.00000	42.65000	-28.069	42.238	-89.838	-197.70	-0.0028536	
14.00000	8.00000	42.65000	-28.094	42.238	-89.838	-197.71	-0.0028536	
15.00000	8.00000	42.65000	-28.069	42.238	-89.838	-197.70	-0.0028536	
16.00000	8.00000	42.65000	-27.992	42.238	-89.838	-197.66	-0.0028539	
17.00000	8.00000	42.65000	-27.860	42.238	-89.838	-197.59	-0.0028545	
18.00000	8.00000	42.65000	-27.666	42.238	-89.838	-197.49	-0.0028553	
19.00000	8.00000	42.65000	-27.402	42.238	-89.837	-197.13	-0.0028565	
20.00000	8.00000	42.65000	-27.052	42.238	-89.836	-197.10	-0.0028585	
21.00000	8.00000	42.65000	-26.596	42.238	-89.835	-196.76	-0.0028612	
22.00000	8.00000	42.65000	-26.001	42.238	-89.831	-196.23	-0.0028655	
23.00000	8.00000	42.65000	-25.217	42.238	-89.824	-195.34	-0.0028726	
24.00000	8.00000	42.65000	-24.155	42.238	-89.800	-193.70	-0.0028951	
25.00000	8.00000	42.65000	-22.651	42.238	-89.699	-190.08	-0.0029103	
26.00000	8.00000	42.65000	-20.317	42.238	-88.774	-178.53	-0.0029605	
0.00000	9.00000	42.65000	-13.753	42.238	-44.446	-92.888	-0.0014529	
1.00000	9.00000	42.65000	-13.519	42.238	-44.429	-92.811	-0.0014541	
2.00000	9.00000	42.65000	-20.552	42.238	-88.774	-178.65	-0.0029594	
3.00000	9.00000	42.65000	-21.874	42.238	-88.860	-181.72	-0.0029381	
4.00000	9.00000	42.65000	-22.821	42.238	-88.879	-183.12	-0.0029274	
5.00000	9.00000	42.65000	-23.532	42.238	-88.886	-183.89	-0.0029213	
6.00000	9.00000	42.65000	-24.077	42.238	-88.889	-184.36	-0.0029175	
7.00000	9.00000	42.65000	-24.499	42.238	-88.890	-184.66	-0.0029150	
8.00000	9.00000	42.65000	-24.824	42.238	-88.891	-184.87	-0.0029133	
9.00000	9.00000	42.65000	-25.072	42.238	-88.891	-185.01	-0.0029121	
10.00000	9.00000	42.65000	-25.254	42.238	-88.891	-185.11	-0.0029113	
11.00000	9.00000	42.65000	-25.379	42.238	-88.891	-185.19	-0.0029105	
12.00000	9.00000	42.65000	-25.452	42.238	-88.892	-185.20	-0.0029105	
13.00000	9.00000	42.65000	-25.476	42.238	-88.892	-185.22	-0.0029104	
14.00000	9.00000	42.65000	-25.452	42.238	-88.892	-185.20	-0.0029105	
15.00000	9.00000	42.65000	-25.379	42.238	-88.891	-185.17	-0.0029108	
16.00000	9.00000	42.65000	-25.254	42.238	-88.891	-185.11	-0.0029113	
17.00000	9.00000	42.65000	-25.072	42.238	-88.891	-185.01	-0.0029121	
18.00000	9.00000	42.65000	-24.824	42.238	-88.891	-184.87	-0.0029133	
19.00000	9.00000	42.65000	-24.499	42.238	-88.890	-184.66	-0.0029150	
20.00000	9.00000	42.65000	-24.077	42.238	-88.889	-184.36	-0.0029175	
21.00000	9.00000	42.65000	-23.532	42.238	-88.886	-183.89	-0.0029213	
22.00000	9.00000	42.65000	-22.821	42.238	-88.879	-183.12	-0.0029274	
23.00000	9.00000	42.65000	-21.874	42.238	-88.860	-181.72	-0.0029381	
24.00000	9.00000	42.65000	-20.552	42.238	-88.774	-178.65	-0.0029594	
25.00000	9.00000	42.65000	-18.519	42.238	-87.929	-168.60	-0.0030011	
26.00000	9.00000	42.65000	-13.753	42.238	-44.446	-92.888	-0.0014529	
0.00000	10.00000	42.65000	-10.874	42.238	-22.499	-52.483	-689.82E-6	
1.00000	10.00000	42.65000	-13.926	42.238	-44.446	-92.967	-0.0014522	
2.00000	10.00000	42.65000	-15.487	42.238	-44.920	-99.341	-0.0014227	
3.00000	10.00000	42.65000	-16.575	42.238	-44.975	-101.56	-0.0014070	
4.00000	10.00000	42.65000	-17.386	42.238	-44.989	-102.64	-0.0013986	
5.00000	10.00000	42.65000	-18.010	42.238	-44.994	-103.27	-0.0013936	
6.00000	10.00000	42.65000	-18.497	42.238	-44.996	-103.67	-0.0013904	
7.00000	10.00000	42.65000	-18.878	42.238	-44.997	-103.93	-0.0013882	
8.00000	10.00000	42.65000	-19.176	42.238	-44.998	-104.11	-0.0013867	
9.00000	10.00000	42.65000	-19.404	42.238	-44.998	-104.24	-0.0013857	
10.00000	10.00000	42.65000	-19.573	42.238	-44.998	-104.33	-0.0013849	
11.00000	10.00000	42.65000	-19.689	42.238	-44.998	-104.39	-0.0013845	
12.00000	10.00000	42.65000	-19.757	42.238	-44.998	-104.42	-0.0013842	
13.00000	10.00000	42.65000	-19.779	42.238	-44.998	-104.43	-0.0013841	
14.00000	10.00000	42.65000	-19.757	42.238	-44.998	-104.43	-0.0013841	
15.00000	10.00000	42.65000	-19.689	42.238	-44.998	-104.39	-0.0013845	
16.00000	10.00000	42.65000	-19.573	42.238	-44.998	-104.33	-0.0013849	
17.00000	10.00000	42.65000	-19.404	42.238	-44.998	-104.24	-0.0013857	
18.00000	10.00000	42.65000	-19.176	42.238	-44.998	-104.11	-0.0013867	
19.00000	10.00000	42.65000	-18.878	42.238	-44.997	-103.93	-0.0013882	
20.00000	10.00000	42.65000	-18.497	42.238	-44.996	-103.67	-0.0013904	
21.00000	10.00000	42.65000	-18.010	42.238	-44.994	-103.27	-0.0013936	
22.00000	10.00000	42.65000	-17.386	42.238	-44.989	-102.64	-0.0013986	
23.00000	10.00000	42.65000	-16.575	42.238	-44.975	-101.56	-0.0014070	
24.00000	10.00000	42.65000	-15.487	42.238	-44.920	-99.341	-0.0014227	
25.00000	10.00000	42.65000	-13.926	42.238	-44.446	-92.967	-0.0014522	
26.00000	10.00000	42.65000	-10.874	42.238	-22.499	-52.483	-689.82E-6	
GL1	0.00000	0						



**CAMPBELLREITH -
LONDON**

Ashton Court
Demolition & Basement excavation
Total heave

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [Level] [mOD]	Z [mm]	Calc Level [mOD]	Stresses		Vert Strain [-]
	X [m]	Y [m]				Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	
	-4.50000	3.00000	44.75000	-4.6350	44.537	0.0	0.0	0.0
	-4.50000	4.00000	44.75000	-4.7430	44.537	0.0	0.0	0.0
	-4.50000	5.00000	44.75000	-4.7796	44.537	0.0	0.0	0.0
	-4.50000	6.00000	44.75000	-4.7430	44.537	0.0	0.0	0.0
	-4.50000	7.00000	44.75000	-4.6350	44.537	0.0	0.0	0.0
	-4.50000	8.00000	44.75000	-4.4607	44.537	0.0	0.0	0.0
GL3	-9.00000	0.00000	44.75000	-2.0191	44.537	0.0	0.0	0.0
	-9.00000	1.00000	44.75000	-2.0999	44.537	0.0	0.0	0.0
	-9.00000	2.00000	44.75000	-2.1666	44.537	0.0	0.0	0.0
	-9.00000	3.00000	44.75000	-2.2163	44.537	0.0	0.0	0.0
	-9.00000	4.00000	44.75000	-2.2470	44.537	0.0	0.0	0.0
	-9.00000	5.00000	44.75000	-2.2573	44.537	0.0	0.0	0.0
	-9.00000	6.00000	44.75000	-2.2470	44.537	0.0	0.0	0.0
	-9.00000	7.00000	44.75000	-2.2163	44.537	0.0	0.0	0.0
	-9.00000	8.00000	44.75000	-2.1666	44.537	0.0	0.0	0.0
GL4	0.00000	4.00000	44.75000	-16.071	44.537	0.0	0.0	0.0
	-1.00000	4.00000	44.75000	-10.778	44.537	0.0	0.0	0.0
	-2.00000	4.00000	44.75000	-8.1621	44.537	0.0	0.0	0.0
	-3.00000	4.00000	44.75000	-6.4491	44.537	0.0	0.0	0.0
	-4.00000	4.00000	44.75000	-5.2294	44.537	0.0	0.0	0.0
	-5.00000	4.00000	44.75000	-4.3188	44.537	0.0	0.0	0.0
	-6.00000	4.00000	44.75000	-3.6163	44.537	0.0	0.0	0.0
	-7.00000	4.00000	44.75000	-3.0609	44.537	0.0	0.0	0.0
	-8.00000	4.00000	44.75000	-2.6133	44.537	0.0	0.0	0.0
	-9.00000	4.00000	44.75000	-2.2470	44.537	0.0	0.0	0.0
GL5	13.00000	-6.00000	44.75000	-5.5134	44.537	0.0	0.0	0.0
	13.00000	-7.00000	44.75000	-4.7437	44.537	0.0	0.0	0.0
	13.00000	-8.00000	44.75000	-4.1052	44.537	0.0	0.0	0.0
	13.00000	-9.00000	44.75000	-3.5697	44.537	0.0	0.0	0.0
	13.00000	-10.00000	44.75000	-3.1166	44.537	0.0	0.0	0.0
	13.00000	-11.00000	44.75000	-2.7303	44.537	0.0	0.0	0.0
	13.00000	-12.00000	44.75000	-2.3991	44.537	0.0	0.0	0.0
GL6	26.00000	-6.00000	44.75000	-3.4849	44.537	0.0	0.0	0.0
	26.00000	-7.00000	44.75000	-3.0537	44.537	0.0	0.0	0.0
	26.00000	-8.00000	44.75000	-2.6889	44.537	0.0	0.0	0.0
	26.00000	-9.00000	44.75000	-2.3769	44.537	0.0	0.0	0.0
	26.00000	-10.00000	44.75000	-2.1077	44.537	0.0	0.0	0.0
	26.00000	-11.00000	44.75000	-1.8738	44.537	0.0	0.0	0.0
	26.00000	-12.00000	44.75000	-1.6694	44.537	0.0	0.0	0.0



Ashton Court
Construction of new building
Immediate settlement

Notes

Eu=400Cu
Cu=70+6z

Analysis Options

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Maximum allowable ratio between values of E: 1.5
Horizontal rigid boundary level: 0.00 [m OD]
Displacements at area centroids calculated.

Soil Profiles Soil Profile

Layer	Level at top [mOD]	Number of intermediate displacement levels	Youngs Modulus [kN/m ²]	Poissons ratio	Non-linear curve
1	45.400	2	5000.0	0.50000	None
2	43.900	43	28000.0	0.50000	None

Soil Zones

Zone	Name	X coordinates min max [m]	Y coordinates min max [m]	Profile
1	SZ1	-60.000 60.000	-60.000 60.000	Soil Profile

Non-linear Curve Coordinates - Non-linear Curve 1

Point Strain Factor [%]

Load Data

Load ref.	Name	Shape	Orientation of Plane	Centre of load (Global) X Y Z [level]	Load position local x or Radius	Width x [m]	Length y [m]	Polygon Coordinates [m]	Rectangle of tolerance	Number of rectangles	Normal (local x) [kN/m ²]	Load value Tangential (local x) [kN/m ²]	Load value (local x) [kN/m ²]
1	Basement	Rectangular	Horizontal	13.000 3.5000 42.650	0.0	26.000	7.0000	N/A	N/A	1	60.000	0.0	0.0

Displacement Data

Ref.	Type	Name	Direction of Extrusion	First point X Y Z [level]	Line/Line for extrusion X Y Z [level]	Second point X Y Z [level]	No. of intrvl across extrusion/line	Extrusion Depth [m]	No. of intrvl along extrusion	Show Calculate Detailed results
1	Grid	BL	Global X	0.0 0.0 42.650	N/A	7.0000 42.650	7	26.000	26	Yes No
2	Line	GL1	N/A	0.0 0.0 44.750	0.0 8.0000 44.750	8.0000 44.750	8	N/A	N/A	Yes No
3	Line	GL2	N/A	-4.5000 0.0 44.750	-4.5000 8.0000 44.750	8.0000 44.750	8	N/A	N/A	Yes No
4	Line	GL3	N/A	-9.0000 0.0 44.750	-9.0000 8.0000 44.750	8.0000 44.750	8	N/A	N/A	Yes No
5	Line	GL4	N/A	0.0 4.0000 44.750	-9.0000 4.0000 44.750	4.0000 44.750	9	N/A	N/A	Yes No
6	Line	GL5	N/A	13.000 -6.0000 44.750	13.000 -12.0000 44.750	44.750	6	N/A	N/A	Yes No
7	Line	GL6	N/A	26.000 -6.0000 44.750	26.000 -12.0000 44.750	44.750	6	N/A	N/A	Yes No

RESULTS FOR GRIDS

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Horizontal rigid boundary level: 0.00 [m OD]

The maximum displacement difference between Boussinesq method (11.382mm) and Mindlin method (8.9146mm) occurs at point X=13.000m Y=3.5000m Level 42.650mOD and is 2.4673mm

Name	X [m]	Location Y [m]	Z [Level] [mOD]	Z [mm]	Calc Level [mOD]	Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
Basement	13.00000	3.50000	42.65000	11.382	42.238	59.959	132.87	736.81E-6
BL	0.00000	0.00000	42.65000	3.9964	42.238	14.999	34.604	162.89E-6
	1.00000	0.00000	42.65000	5.3307	42.238	29.630	61.547	428.60E-6
	2.00000	0.00000	42.65000	5.9662	42.238	29.945	65.751	377.54E-6
	3.00000	0.00000	42.65000	6.3928	42.238	29.982	67.187	356.76E-6
	4.00000	0.00000	42.65000	6.7000	42.238	29.991	67.876	346.39E-6
	5.00000	0.00000	42.65000	6.9290	42.238	29.994	68.264	340.46E-6
	6.00000	0.00000	42.65000	7.1032	42.238	29.996	68.503	336.77E-6
	7.00000	0.00000	42.65000	7.2367	42.238	29.996	68.659	334.36E-6
	8.00000	0.00000	42.65000	7.3388	42.238	29.997	68.764	332.73E-6
	9.00000	0.00000	42.65000	7.4159	42.238	29.997	68.835	331.62E-6
	10.00000	0.00000	42.65000	7.4722	42.238	29.997	68.884	330.86E-6
	11.00000	0.00000	42.65000	7.5106	42.238	29.997	68.915	330.37E-6
	12.00000	0.00000	42.65000	7.5329	42.238	29.997	68.933	330.10E-6
	13.00000	0.00000	42.65000	7.5402	42.238	29.997	68.939	330.01E-6
	14.00000	0.00000	42.65000	7.5329	42.238	29.997	68.933	330.10E-6
	15.00000	0.00000	42.65000	7.5106	42.238	29.997	68.915	330.37E-6
	16.00000	0.00000	42.65000	7.4722	42.238	29.997	68.884	330.86E-6
	17.00000	0.00000	42.65000	7.4159	42.238	29.997	68.835	331.62E-6
	18.00000	0.00000	42.65000	7.3388	42.238	29.997	68.764	332.73E-6
	19.00000	0.00000	42.65000	7.2367	42.238	29.996	68.659	334.36E-6
	20.00000	0.00000	42.65000	7.1032	42.238	29.996	68.503	336.77E-6
	21.00000	0.00000	42.65000	6.9290	42.238	29.994	68.264	340.46E-6
	22.00000	0.00000	42.65000	6.7000	42.238	29.991	67.876	346.39E-6
	23.00000	0.00000	42.65000	6.3928	42.238	29.982	67.187	356.76E-6
	24.00000	0.00000	42.65000	5.9662	42.238	29.945	65.751	377.54E-6
	25.00000	0.00000	42.65000	5.3307	42.238	29.630	61.547	428.60E-6
	26.00000	0.00000	42.65000	3.9964	42.238	14.999	34.604	162.89E-6
	0.00000	1.00000	42.65000	5.2209	42.238	29.622	61.422	430.53E-6
	1.00000	1.00000	42.65000	7.3426	42.238	58.618	111.83	0.0010036
	2.00000	1.00000	42.65000	8.1757	42.238	59.181	118.46	926.11E-6
	3.00000	1.00000	42.65000	8.6951	42.238	59.238	120.45	897.65E-6
	4.00000	1.00000	42.65000	9.0529	42.238	59.251	121.33	884.44E-6
	5.00000	1.00000	42.65000	9.3121	42.238	59.255	121.80	877.26E-6
	6.00000	1.00000	42.65000	9.5052	42.238	59.256	122.08	872.95E-6
	7.00000	1.00000	42.65000	9.6510	42.238	59.257	122.26	870.20E-6
	8.00000	1.00000	42.65000	9.7613	42.238	59.258	122.37	868.38E-6
	9.00000	1.00000	42.65000	9.8440	42.238	59.258	122.45	867.15E-6
	10.00000	1.00000	42.65000	9.9039	42.238	59.258	122.51	866.33E-6
	11.00000	1.00000	42.65000	9.9447	42.238	59.258	122.54	865.80E-6
	12.00000	1.00000	42.65000	9.9683	42.238	59.258	122.56	865.50E-6
	13.00000	1.00000	42.65000	9.9761	42.238	59.258	122.57	865.41E-6
	14.00000	1.00000	42.65000	9.9683	42.238	59.258	122.56	865.50E-6
	15.00000	1.00000	42.65000	9.9447	42.238	59.258	122.54	865.80E-6
	16.00000	1.00000	42.65000	9.9039	42.238	59.258	122.51	866.33E-6
	17.00000	1.00000	42.65000	9.8440	42.238	59.258	122.45	867.15E-6
	18.00000	1.00000	42.65000	9.7613	42.238	59.258	122.37	868.38E-6
	19.00000	1.00000	42.65000	9.6510	42.238	59.257	122.26	870.20E-6
	20.00000	1.00000	42.65000	9.5052	42.238	59.256	122.08	872.95E-6
	21.00000	1.00000	42.65000	9.3121	42.238	59.255	121.80	877.26E-6
	22.00000	1.00000	42.65000	9.0529	42.238	59.251	121.33	884.44E-6



**CAMPBELLREITH -
LONDON**

Ashton Court
Construction of new building
Immediate settlement

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [Level] [m]	Z [m]	Calc Level [mOD]	Stresses		
	X [m]	Y [m]				Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
23.00000	1.00000		42.65000	8.6951	42.238	59.238	120.45	897.65E-6
24.00000	1.00000		42.65000	8.1757	42.238	59.181	118.46	926.11E-6
25.00000	1.00000		42.65000	7.3426	42.238	58.618	111.83	0.0010036
26.00000	1.00000		42.65000	5.2209	42.238	29.629	61.422	430.53E-6
0.00000	2.00000		42.65000	5.6995	42.238	29.943	65.410	382.80E-6
1.00000	2.00000		42.65000	8.0091	42.238	59.179	118.22	929.81E-6
2.00000	2.00000		42.65000	8.9594	42.238	59.796	125.82	839.68E-6
3.00000	2.00000		42.65000	9.5443	42.238	59.863	128.15	806.31E-6
4.00000	2.00000		42.65000	9.9397	42.238	59.878	129.17	791.05E-6
5.00000	2.00000		42.65000	10.222	42.238	59.883	129.70	782.92E-6
6.00000	2.00000		42.65000	10.429	42.238	59.885	130.01	778.14E-6
7.00000	2.00000		42.65000	10.584	42.238	59.886	130.21	775.15E-6
8.00000	2.00000		42.65000	10.700	42.238	59.886	130.33	773.18E-6
9.00000	2.00000		42.65000	10.787	42.238	59.886	130.42	771.87E-6
10.00000	2.00000		42.65000	10.849	42.238	59.887	130.47	771.00E-6
11.00000	2.00000		42.65000	10.892	42.238	59.887	130.51	770.44E-6
12.00000	2.00000		42.65000	10.916	42.238	59.887	130.53	770.13E-6
13.00000	2.00000		42.65000	10.924	42.238	59.887	130.54	770.03E-6
14.00000	2.00000		42.65000	10.916	42.238	59.887	130.53	770.13E-6
15.00000	2.00000		42.65000	10.892	42.238	59.887	130.51	770.44E-6
16.00000	2.00000		42.65000	10.849	42.238	59.887	130.47	771.00E-6
17.00000	2.00000		42.65000	10.787	42.238	59.886	130.42	771.87E-6
18.00000	2.00000		42.65000	10.700	42.238	59.886	130.33	773.18E-6
19.00000	2.00000		42.65000	10.584	42.238	59.886	130.21	775.15E-6
20.00000	2.00000		42.65000	10.429	42.238	59.885	130.01	778.14E-6
21.00000	2.00000		42.65000	10.222	42.238	59.883	129.70	782.92E-6
22.00000	2.00000		42.65000	9.9397	42.238	59.878	129.17	791.05E-6
23.00000	2.00000		42.65000	9.5443	42.238	59.863	128.15	806.31E-6
24.00000	2.00000		42.65000	8.9594	42.238	59.796	125.82	839.68E-6
25.00000	2.00000		42.65000	8.0091	42.238	59.179	118.22	929.81E-6
26.00000	2.00000		42.65000	5.6995	42.238	29.943	65.410	382.80E-6
0.00000	3.00000		42.65000	5.9062	42.238	29.977	66.470	367.75E-6
1.00000	3.00000		42.65000	8.2832	42.238	59.232	119.76	908.20E-6
2.00000	3.00000		42.65000	9.2840	42.238	59.858	127.65	813.86E-6
3.00000	3.00000		42.65000	9.9011	42.238	59.928	130.13	778.34E-6
4.00000	3.00000		42.65000	10.316	42.238	59.944	131.22	762.07E-6
5.00000	3.00000		42.65000	10.610	42.238	59.950	131.78	753.44E-6
6.00000	3.00000		42.65000	10.825	42.238	59.952	132.11	748.41E-6
7.00000	3.00000		42.65000	10.984	42.238	59.953	132.31	745.28E-6
8.00000	3.00000		42.65000	11.104	42.238	59.953	132.44	743.24E-6
9.00000	3.00000		42.65000	11.193	42.238	59.953	132.53	741.88E-6
10.00000	3.00000		42.65000	11.257	42.238	59.954	132.59	740.98E-6
11.00000	3.00000		42.65000	11.300	42.238	59.954	132.63	740.41E-6
12.00000	3.00000		42.65000	11.325	42.238	59.954	132.65	740.09E-6
13.00000	3.00000		42.65000	11.333	42.238	59.954	132.65	739.99E-6
14.00000	3.00000		42.65000	11.325	42.238	59.954	132.65	740.09E-6
15.00000	3.00000		42.65000	11.300	42.238	59.954	132.63	740.41E-6
16.00000	3.00000		42.65000	11.257	42.238	59.954	132.59	740.98E-6
17.00000	3.00000		42.65000	11.193	42.238	59.953	132.53	741.88E-6
18.00000	3.00000		42.65000	11.104	42.238	59.953	132.44	743.24E-6
19.00000	3.00000		42.65000	10.984	42.238	59.953	132.31	745.28E-6
20.00000	3.00000		42.65000	10.825	42.238	59.952	132.11	748.41E-6
21.00000	3.00000		42.65000	10.610	42.238	59.950	131.78	753.44E-6
22.00000	3.00000		42.65000	10.316	42.238	59.944	131.22	762.07E-6
23.00000	3.00000		42.65000	9.9011	42.238	59.928	130.13	778.34E-6
24.00000	3.00000		42.65000	9.2840	42.238	59.858	127.65	813.86E-6
25.00000	3.00000		42.65000	8.2832	42.238	59.232	119.76	908.20E-6
26.00000	3.00000		42.65000	5.9062	42.238	29.977	66.470	367.75E-6
0.00000	4.00000		42.65000	5.9062	42.238	29.977	66.470	367.75E-6
1.00000	4.00000		42.65000	8.2832	42.238	59.232	119.76	908.20E-6
2.00000	4.00000		42.65000	9.2840	42.238	59.858	127.65	813.86E-6
3.00000	4.00000		42.65000	9.9011	42.238	59.928	130.13	778.34E-6
4.00000	4.00000		42.65000	10.316	42.238	59.944	131.22	762.07E-6
5.00000	4.00000		42.65000	10.610	42.238	59.950	131.78	753.44E-6
6.00000	4.00000		42.65000	10.825	42.238	59.952	132.11	748.41E-6
7.00000	4.00000		42.65000	10.984	42.238	59.953	132.31	745.28E-6
8.00000	4.00000		42.65000	11.104	42.238	59.953	132.44	743.24E-6
9.00000	4.00000		42.65000	11.193	42.238	59.953	132.53	741.88E-6
10.00000	4.00000		42.65000	11.257	42.238	59.954	132.59	740.98E-6
11.00000	4.00000		42.65000	11.300	42.238	59.954	132.63	740.41E-6
12.00000	4.00000		42.65000	11.325	42.238	59.954	132.65	740.09E-6
13.00000	4.00000		42.65000	11.333	42.238	59.954	132.65	739.99E-6
14.00000	4.00000		42.65000	11.325	42.238	59.954	132.65	740.09E-6
15.00000	4.00000		42.65000	11.300	42.238	59.954	132.63	740.41E-6
16.00000	4.00000		42.65000	11.257	42.238	59.954	132.59	740.98E-6
17.00000	4.00000		42.65000	11.193	42.238	59.953	132.53	741.88E-6
18.00000	4.00000		42.65000	11.104	42.238	59.953	132.44	743.24E-6
19.00000	4.00000		42.65000	10.984	42.238	59.953	132.31	745.28E-6
20.00000	4.00000		42.65000	10.825	42.238	59.952	132.11	748.41E-6
21.00000	4.00000		42.65000	10.610	42.238	59.950	131.78	753.44E-6
22.00000	4.00000		42.65000	10.316	42.238	59.944	131.22	762.07E-6
23.00000	4.00000		42.65000	9.9011	42.238	59.928	130.13	778.34E-6
24.00000	4.00000		42.65000	9.2840	42.238	59.858	127.65	813.86E-6
25.00000	4.00000		42.65000	8.2832	42.238	59.232	119.76	908.20E-6
26.00000	4.00000		42.65000	5.9062	42.238	29.977	66.470	367.75E-6
0.00000	5.00000		42.65000	5.6995	42.238	29.943	65.410	382.80E-6
1.00000	5.00000		42.65000	8.0091	42.238	59.179	118.22	929.81E-6
2.00000	5.00000		42.65000	8.9594	42.238	59.796	125.82	839.68E-6
3.00000	5.00000		42.65000	9.5443	42.238	59.863	128.15	806.31E-6
4.00000	5.00000		42.65000	9.9397	42.238	59.878	129.17	791.05E-6
5.00000	5.00000		42.65000	10.222	42.238	59.883	129.70	782.92E-6
6.00000	5.00000		42.65000	10.429	42.238	59.885	130.01	778.14E-6
7.00000	5.00000		42.65000	10.584	42.238	59.886	130.21	775.15E-6
8.00000	5.00000		42.65000	10.700	42.238	59.886	130.33	773.18E-6
9.00000	5.00000		42.65000	10.787	42.238	59.886	130.42	771.87E-6
10.00000	5.00000		42.65000	10.849	42.238	59.887	130.47	771.00E-6
11.00000	5.00000		42.65000	10.892	42.238	59.887	130.51	770.44E-6
12.00000	5.00000		42.65000	10.916	42.238	59.887	130.53	770.13E-6
13.00000	5.00000		42.65000	10.924	42.238	59.887	130.54	770.03E-6
14.00000	5.00000		42.65000	10.916	42.238	59.887	130.53	770.13E-6
15.00000	5.00000		42.65000	10.892	42.238	59.887	130.51	770.44E-6
16.00000	5.00000		42.65000	10.849	42.238	59.887	130.47	771.00E-6
17.00000	5.00000		42.65000	10.787	42.238	59.886	130.42	771.87E-6
18.00000	5.00000		42.65000	10.700	42.238	59.886	130.33	773.18E-6
19.00000	5.00000		42.65000	10.584	42.238	59.886	130.21	775.15E-6
20.00000	5.00000		42.65000	10.429	42.238	59.885	130.01	778.14E-6
21.00000	5.00000		42.65000	10.222	42.238	59.883	129.70	782.92E-6
22.00000	5.00000		42.65000	9.9397	42.238	59.878	129.17	791.05E-6
23.00000	5.00000		42.65000	9.5443	42.238	59.863	128.15	806.31E-6
24.00000	5.00000		42.65000	8.9594	42.238	59.796	125.82	839.68E-6
25.00000	5.00000		42.65000	8.0091	42.238	59.179	118.22	929.81E-6
26.00000	5.00000		42.65000	5.6995	42.238	29.943	65.410	382.80E-6
0.00000	6.00000		42.65000	5.2209	42.238	29.629	61.422	430.53E-6



**CAMPBELLREITH -
LONDON**

Ashton Court
Construction of new building
Immediate settlement

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [level] [mm]	Z [mm]	Stresses			Vert Strain [-]
	X [m]	Y [m]			Calc Level [mOD]	Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	
18.00000	6.00000		42.65000	9.7613	42.238	59.259	122.37	868.38E-6
19.00000	6.00000		42.65000	9.6510	42.238	59.257	122.26	870.20E-6
20.00000	6.00000		42.65000	9.5052	42.238	59.256	122.08	872.95E-6
21.00000	6.00000		42.65000	9.3121	42.238	59.255	121.80	877.26E-6
22.00000	6.00000		42.65000	9.0529	42.238	59.251	121.33	884.44E-6
23.00000	6.00000		42.65000	8.6951	42.238	59.238	120.45	897.65E-6
24.00000	6.00000		42.65000	8.1757	42.238	59.181	118.46	926.11E-6
25.00000	6.00000		42.65000	7.3426	42.238	58.618	111.83	0.0010036
26.00000	6.00000		42.65000	5.2209	42.238	29.629	61.422	430.53E-6
0.00000	7.00000		42.65000	3.9964	42.238	14.999	34.604	162.89E-6
1.00000	7.00000		42.65000	5.3307	42.238	29.630	61.547	428.60E-6
2.00000	7.00000		42.65000	5.9662	42.238	29.945	65.751	377.54E-6
3.00000	7.00000		42.65000	6.3928	42.238	29.982	67.187	356.76E-6
4.00000	7.00000		42.65000	6.7000	42.238	29.991	67.876	346.39E-6
5.00000	7.00000		42.65000	6.9290	42.238	29.994	68.264	340.46E-6
6.00000	7.00000		42.65000	7.1032	42.238	29.996	68.503	336.77E-6
7.00000	7.00000		42.65000	7.2367	42.238	29.996	68.659	334.36E-6
8.00000	7.00000		42.65000	7.3388	42.238	29.997	68.764	332.73E-6
9.00000	7.00000		42.65000	7.4159	42.238	29.997	68.835	331.62E-6
10.00000	7.00000		42.65000	7.4722	42.238	29.997	68.884	330.86E-6
11.00000	7.00000		42.65000	7.5106	42.238	29.997	68.915	330.37E-6
12.00000	7.00000		42.65000	7.5329	42.238	29.997	68.933	330.10E-6
13.00000	7.00000		42.65000	7.5402	42.238	29.997	68.939	330.01E-6
14.00000	7.00000		42.65000	7.5329	42.238	29.997	68.933	330.10E-6
15.00000	7.00000		42.65000	7.5106	42.238	29.997	68.915	330.37E-6
16.00000	7.00000		42.65000	7.4722	42.238	29.997	68.884	330.86E-6
17.00000	7.00000		42.65000	7.4159	42.238	29.997	68.835	331.62E-6
18.00000	7.00000		42.65000	7.3388	42.238	29.997	68.764	332.73E-6
19.00000	7.00000		42.65000	7.2367	42.238	29.996	68.659	334.36E-6
20.00000	7.00000		42.65000	7.1032	42.238	29.996	68.503	336.77E-6
21.00000	7.00000		42.65000	6.9290	42.238	29.994	68.264	340.46E-6
22.00000	7.00000		42.65000	6.7000	42.238	29.991	67.876	346.39E-6
23.00000	7.00000		42.65000	6.3928	42.238	29.982	67.187	356.76E-6
24.00000	7.00000		42.65000	5.9662	42.238	29.945	65.751	377.54E-6
25.00000	7.00000		42.65000	5.3307	42.238	29.630	61.547	428.60E-6
26.00000	7.00000		42.65000	3.9964	42.238	14.999	34.604	162.89E-6
GL1	0.00000	0.00000	44.75000	3.9703	44.537	0.0	0.0	0.0
	0.00000	1.00000	44.75000	5.1594	44.537	0.0	0.0	0.0
	0.00000	2.00000	44.75000	5.6438	44.537	0.0	0.0	0.0
	0.00000	3.00000	44.75000	5.8516	44.537	0.0	0.0	0.0
	0.00000	4.00000	44.75000	5.8516	44.537	0.0	0.0	0.0
	0.00000	5.00000	44.75000	5.6438	44.537	0.0	0.0	0.0
	0.00000	6.00000	44.75000	5.1594	44.537	0.0	0.0	0.0
	0.00000	7.00000	44.75000	3.9703	44.537	0.0	0.0	0.0
	0.00000	8.00000	44.75000	2.7450	44.537	0.0	0.0	0.0
GL2	-4.50000	0.00000	44.75000	1.1519	44.537	0.0	0.0	0.0
	-4.50000	1.00000	44.75000	1.2307	44.537	0.0	0.0	0.0
	-4.50000	2.00000	44.75000	1.2882	44.537	0.0	0.0	0.0
	-4.50000	3.00000	44.75000	1.3185	44.537	0.0	0.0	0.0
	-4.50000	4.00000	44.75000	1.3185	44.537	0.0	0.0	0.0
	-4.50000	5.00000	44.75000	1.2882	44.537	0.0	0.0	0.0
	-4.50000	6.00000	44.75000	1.2307	44.537	0.0	0.0	0.0
	-4.50000	7.00000	44.75000	1.1519	44.537	0.0	0.0	0.0
	-4.50000	8.00000	44.75000	1.0594	44.537	0.0	0.0	0.0
GL3	-9.00000	0.00000	44.75000	0.49090	44.537	0.0	0.0	0.0
	-9.00000	1.00000	44.75000	0.50976	44.537	0.0	0.0	0.0
	-9.00000	2.00000	44.75000	0.52296	44.537	0.0	0.0	0.0
	-9.00000	3.00000	44.75000	0.52976	44.537	0.0	0.0	0.0
	-9.00000	4.00000	44.75000	0.52976	44.537	0.0	0.0	0.0
	-9.00000	5.00000	44.75000	0.52296	44.537	0.0	0.0	0.0
	-9.00000	6.00000	44.75000	0.50976	44.537	0.0	0.0	0.0
	-9.00000	7.00000	44.75000	0.49090	44.537	0.0	0.0	0.0
	-9.00000	8.00000	44.75000	0.46738	44.537	0.0	0.0	0.0
GL4	0.00000	4.00000	44.75000	5.8516	44.537	0.0	0.0	0.0
	-1.00000	4.00000	44.75000	3.5446	44.537	0.0	0.0	0.0
	-2.00000	4.00000	44.75000	2.5295	44.537	0.0	0.0	0.0
	-3.00000	4.00000	44.75000	1.9051	44.537	0.0	0.0	0.0
	-4.00000	4.00000	44.75000	1.4820	44.537	0.0	0.0	0.0
	-5.00000	4.00000	44.75000	1.1784	44.537	0.0	0.0	0.0
	-6.00000	4.00000	44.75000	0.93164	44.537	0.0	0.0	0.0
	-7.00000	4.00000	44.75000	0.77717	44.537	0.0	0.0	0.0
	-8.00000	4.00000	44.75000	0.63983	44.537	0.0	0.0	0.0
	-9.00000	4.00000	44.75000	0.52976	44.537	0.0	0.0	0.0
GL5	13.00000	-6.00000	44.75000	1.7420	44.537	0.0	0.0	0.0
	13.00000	-7.00000	44.75000	1.4638	44.537	0.0	0.0	0.0
	13.00000	-8.00000	44.75000	1.2366	44.537	0.0	0.0	0.0
	13.00000	-9.00000	44.75000	1.0487	44.537	0.0	0.0	0.0
	13.00000	-10.00000	44.75000	0.89196	44.537	0.0	0.0	0.0
	13.00000	-11.00000	44.75000	0.76015	44.537	0.0	0.0	0.0
	13.00000	-12.00000	44.75000	0.64861	44.537	0.0	0.0	0.0
GL6	26.00000	-6.00000	44.75000	1.0306	44.537	0.0	0.0	0.0
	26.00000	-7.00000	44.75000	0.87860	44.537	0.0	0.0	0.0
	26.00000	-8.00000	44.75000	0.75218	44.537	0.0	0.0	0.0
	26.00000	-9.00000	44.75000	0.64578	44.537	0.0	0.0	0.0
	26.00000	-10.00000	44.75000	0.55537	44.537	0.0	0.0	0.0
	26.00000	-11.00000	44.75000	0.47798	44.537	0.0	0.0	0.0
	26.00000	-12.00000	44.75000	0.41135	44.537	0.0	0.0	0.0



Ashton Court
Construction of new building
Total settlement

Notes

E= 0.75Eu
Eu=400Cu
Cu=70+6z

Analysis Options

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Maximum allowable ratio between values of E: 1.5
Horizontal rigid boundary level: 0.00 [m OD]
Displacements at area centroids calculated.

Soil Profiles/Soil Profile

Table with columns: Layer, Level at top, Number of intermediate displacement levels, Youngs Modulus, Poissons ratio, Non-linear curve. Includes data for layers 1 and 2.

Soil Zones

Table with columns: Zone, Name, X coordinates, Y coordinates, Profile. Includes data for zone 1 (SZ1).

Non-linear Curve Coordinates - Non-linear Curve 1

Table with columns: Point, Strain, Factor. Includes data for point 1.

Load Data

Table with columns: Load ref., Name, Shape, Orientation of Plane, Centre of load (Global), Angle of local x from, Width x or Radius, Length y, Polygon Coordinates, Rectangle tolerance, Number of rectangles, Normal (local z), Tangential (local x), Tangential (local y). Includes data for load 1 (Basement).

Displacement Data

Table with columns: Ref., Type, Name, Direction of Extrusion, Line/Line for extrusion, First point, Second point, No. of intrvl across, Extrusion, No. of intrvl along, Calculate, Detailed results. Includes data for grid and line displacements.

RESULTS FOR GRIDS

Analysis: Boussinesq
Global Poisson's ratio: 0.20
Horizontal rigid boundary level: 0.00 [m OD]

The maximum displacement difference between Boussinesq method (8.9971mm) and Mindlin method (7.9041mm) occurs at point X=0.0m Y=3.0000m Level 44.750mOD and is 1.0929mm

Table with columns: Name, Location (X, Y, Z), Calc Level, Vert Stress, Sum Princ, Vert Strain. Includes data for basement and various grid points.



CAMPBELLREITH - LONDON

Ashton Court
Construction of new building
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Job No. Sheet No. Rev.

12047

Drg. Ref.

Made by Date Checked
FD

Name	Location		Z [Level] [m]	Z [m]	Calc Level [mOD]	Stresses		
	X [m]	Y [m]				Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
22.00000	1.00000	42.65000	13.812	42.238	59.251	121.33	0.0019577	
23.00000	1.00000	42.65000	13.261	42.238	59.238	120.45	0.0019645	
24.00000	1.00000	42.65000	12.468	42.238	59.181	118.46	0.0019782	
25.00000	1.00000	42.65000	11.209	42.238	58.618	111.83	0.0020054	
26.00000	1.00000	42.65000	8.1310	42.238	29.629	61.422	972.73E-6	
0.00000	2.00000	42.65000	8.8483	42.238	29.943	65.410	955.15E-6	
1.00000	2.00000	42.65000	12.206	42.238	59.179	118.22	0.0019801	
2.00000	2.00000	42.65000	13.639	42.238	59.796	125.82	0.0019475	
3.00000	2.00000	42.65000	14.530	42.238	59.863	128.15	0.0019314	
4.00000	2.00000	42.65000	15.138	42.238	59.878	129.17	0.0019237	
5.00000	2.00000	42.65000	15.575	42.238	59.883	129.70	0.0019194	
6.00000	2.00000	42.65000	15.900	42.238	59.885	130.01	0.0019169	
7.00000	2.00000	42.65000	16.144	42.238	59.886	130.21	0.0019154	
8.00000	2.00000	42.65000	16.328	42.238	59.886	130.33	0.0019143	
9.00000	2.00000	42.65000	16.466	42.238	59.886	130.42	0.0019136	
10.00000	2.00000	42.65000	16.566	42.238	59.887	130.47	0.0019129	
11.00000	2.00000	42.65000	16.634	42.238	59.887	130.51	0.0019129	
12.00000	2.00000	42.65000	16.674	42.238	59.887	130.53	0.0019127	
13.00000	2.00000	42.65000	16.687	42.238	59.887	130.54	0.0019127	
14.00000	2.00000	42.65000	16.674	42.238	59.887	130.53	0.0019127	
15.00000	2.00000	42.65000	16.634	42.238	59.887	130.51	0.0019129	
16.00000	2.00000	42.65000	16.566	42.238	59.887	130.47	0.0019132	
17.00000	2.00000	42.65000	16.466	42.238	59.886	130.42	0.0019136	
18.00000	2.00000	42.65000	16.328	42.238	59.886	130.33	0.0019143	
19.00000	2.00000	42.65000	16.144	42.238	59.886	130.21	0.0019154	
20.00000	2.00000	42.65000	15.900	42.238	59.885	130.01	0.0019169	
21.00000	2.00000	42.65000	15.575	42.238	59.883	129.70	0.0019194	
22.00000	2.00000	42.65000	15.138	42.238	59.878	129.17	0.0019237	
23.00000	2.00000	42.65000	14.530	42.238	59.863	128.15	0.0019314	
24.00000	2.00000	42.65000	13.639	42.238	59.796	125.82	0.0019475	
25.00000	2.00000	42.65000	12.206	42.238	59.179	118.22	0.0019801	
26.00000	2.00000	42.65000	8.8483	42.238	29.943	65.410	955.15E-6	
0.00000	3.00000	42.65000	9.1589	42.238	29.977	66.470	947.97E-6	
1.00000	3.00000	42.65000	12.616	42.238	59.232	119.76	0.0019699	
2.00000	3.00000	42.65000	14.125	42.238	59.858	127.65	0.0019353	
3.00000	3.00000	42.65000	15.064	42.238	59.928	130.13	0.0019181	
4.00000	3.00000	42.65000	15.702	42.238	59.944	131.22	0.0019099	
5.00000	3.00000	42.65000	16.157	42.238	59.950	131.78	0.0019054	
6.00000	3.00000	42.65000	16.493	42.238	59.952	132.11	0.0019028	
7.00000	3.00000	42.65000	16.744	42.238	59.953	132.31	0.0019011	
8.00000	3.00000	42.65000	16.934	42.238	59.953	132.44	0.0019000	
9.00000	3.00000	42.65000	17.075	42.238	59.953	132.53	0.0018993	
10.00000	3.00000	42.65000	17.177	42.238	59.954	132.59	0.0018989	
11.00000	3.00000	42.65000	17.246	42.238	59.954	132.63	0.0018985	
12.00000	3.00000	42.65000	17.287	42.238	59.954	132.65	0.0018984	
13.00000	3.00000	42.65000	17.300	42.238	59.954	132.65	0.0018983	
14.00000	3.00000	42.65000	17.287	42.238	59.954	132.65	0.0018984	
15.00000	3.00000	42.65000	17.246	42.238	59.954	132.63	0.0018985	
16.00000	3.00000	42.65000	17.177	42.238	59.954	132.59	0.0018989	
17.00000	3.00000	42.65000	17.075	42.238	59.953	132.53	0.0018993	
18.00000	3.00000	42.65000	16.934	42.238	59.953	132.44	0.0019000	
19.00000	3.00000	42.65000	16.744	42.238	59.953	132.31	0.0019011	
20.00000	3.00000	42.65000	16.493	42.238	59.952	132.11	0.0019028	
21.00000	3.00000	42.65000	16.157	42.238	59.950	131.78	0.0019054	
22.00000	3.00000	42.65000	15.702	42.238	59.944	131.22	0.0019099	
23.00000	3.00000	42.65000	15.064	42.238	59.928	130.13	0.0019181	
24.00000	3.00000	42.65000	14.125	42.238	59.858	127.65	0.0019353	
25.00000	3.00000	42.65000	12.616	42.238	59.232	119.76	0.0019699	
26.00000	3.00000	42.65000	9.1589	42.238	29.977	66.470	947.97E-6	
0.00000	4.00000	42.65000	9.1589	42.238	29.977	66.470	947.97E-6	
1.00000	4.00000	42.65000	12.616	42.238	59.232	119.76	0.0019699	
2.00000	4.00000	42.65000	14.125	42.238	59.858	127.65	0.0019353	
3.00000	4.00000	42.65000	15.064	42.238	59.928	130.13	0.0019181	
4.00000	4.00000	42.65000	15.702	42.238	59.944	131.22	0.0019099	
5.00000	4.00000	42.65000	16.157	42.238	59.950	131.78	0.0019054	
6.00000	4.00000	42.65000	16.493	42.238	59.952	132.11	0.0019028	
7.00000	4.00000	42.65000	16.744	42.238	59.953	132.31	0.0019011	
8.00000	4.00000	42.65000	16.934	42.238	59.953	132.44	0.0019000	
9.00000	4.00000	42.65000	17.075	42.238	59.953	132.53	0.0018993	
10.00000	4.00000	42.65000	17.177	42.238	59.954	132.59	0.0018989	
11.00000	4.00000	42.65000	17.246	42.238	59.954	132.63	0.0018985	
12.00000	4.00000	42.65000	17.287	42.238	59.954	132.65	0.0018984	
13.00000	4.00000	42.65000	17.300	42.238	59.954	132.65	0.0018983	
14.00000	4.00000	42.65000	17.287	42.238	59.954	132.65	0.0018984	
15.00000	4.00000	42.65000	17.246	42.238	59.954	132.63	0.0018985	
16.00000	4.00000	42.65000	17.177	42.238	59.954	132.59	0.0018989	
17.00000	4.00000	42.65000	17.075	42.238	59.953	132.53	0.0018993	
18.00000	4.00000	42.65000	16.934	42.238	59.953	132.44	0.0019000	
19.00000	4.00000	42.65000	16.744	42.238	59.953	132.31	0.0019011	
20.00000	4.00000	42.65000	16.493	42.238	59.952	132.11	0.0019028	
21.00000	4.00000	42.65000	16.157	42.238	59.950	131.78	0.0019054	
22.00000	4.00000	42.65000	15.702	42.238	59.944	131.22	0.0019099	
23.00000	4.00000	42.65000	15.064	42.238	59.928	130.13	0.0019181	
24.00000	4.00000	42.65000	14.125	42.238	59.858	127.65	0.0019353	
25.00000	4.00000	42.65000	12.616	42.238	59.232	119.76	0.0019699	
26.00000	4.00000	42.65000	9.1589	42.238	29.977	66.470	947.97E-6	
0.00000	5.00000	42.65000	8.8483	42.238	29.943	65.410	955.15E-6	
1.00000	5.00000	42.65000	12.206	42.238	59.179	118.22	0.0019801	
2.00000	5.00000	42.65000	13.639	42.238	59.796	125.82	0.0019475	
3.00000	5.00000	42.65000	14.530	42.238	59.863	128.15	0.0019314	
4.00000	5.00000	42.65000	15.138	42.238	59.878	129.17	0.0019237	
5.00000	5.00000	42.65000	15.575	42.238	59.883	129.70	0.0019194	
6.00000	5.00000	42.65000	15.900	42.238	59.885	130.01	0.0019169	
7.00000	5.00000	42.65000	16.144	42.238	59.886	130.21	0.0019154	
8.00000	5.00000	42.65000	16.328	42.238	59.886	130.33	0.0019143	
9.00000	5.00000	42.65000	16.466	42.238	59.886	130.42	0.0019136	
10.00000	5.00000	42.65000	16.566	42.238	59.887	130.47	0.0019132	
11.00000	5.00000	42.65000	16.634	42.238	59.887	130.51	0.0019129	
12.00000	5.00000	42.65000	16.674	42.238	59.887	130.53	0.0019127	
13.00000	5.00000	42.65000	16.687	42.238	59.887	130.54	0.0019127	
14.00000	5.00000	42.65000	16.674	42.238	59.887	130.53	0.0019127	
15.00000	5.00000	42.65000	16.634	42.238	59.887	130.51	0.0019129	
16.00000	5.00000	42.65000	16.566	42.238	59.887	130.47	0.0019132	
17.00000	5.00000	42.65000	16.466	42.238	59.886	130.42	0.0019136	
18.00000	5.00000	42.65000	16.328	42.238	59.886	130.33	0.0019143	
19.00000	5.00000	42.65000	16.144	42.238	59.886	130.21	0.0019154	
20.00000	5.00000	42.65000	15.900	42.238	59.885	130.01	0.0019169	
21.00000	5.00000	42.65000	15.575	42.238	59.883	129.70	0.0019194	
22.00000	5.00000	42.65000	15.138	42.238	59.878	129.17	0.0019237	
23.00000	5.00000	42.65000	14.530	42.238	59.863	128.15	0.0019314	
24.00000	5.00000	42.65000	13.639	42.238	59.796	125.82	0.0019475	
25.00000	5.00000	42.65000	12.206	42.238	59.179	118.22	0.0019801	
26.00000	5.00000	42.65000	8.8483	42.238	29.943	65.410	955.15E-6	
0.00000	6.00000	42.65000	8.1310	42.238	29.629	61.422	972.73E-6	
1.00000	6.00000	42.65000	11.209	42.238	58.618	111.83	0.0020054	
2.00000	6.00000	42.65000	12.468	42.238	59.181	118.46	0.0019782	
3.00000	6.00000	42.65000	13.261	42.238	59.238	120.45	0.0019645	
4.00000	6.00000	42.65000	13.812	42.238	59.251	121.33	0.0019577	
5.00000	6.00000							



**CAMPBELLREITH -
LONDON**

Ashton Court
Construction of new building
Total settlement

Job No.	Sheet No.	Rev.
12047		
Drg. Ref.		
Made by	Date	Checked
FD		

Name	Location		Z [level] [mm]	Z [mm]	Calc Level [mOD]	Stresses		
	X [m]	Y [m]				Vert Stress [kN/m ²]	Sum Princ [kN/m ²]	Vert Strain [-]
17.00000	6.00000	42.65000	15.055	42.238	59.258	122.45	0.0019487	
18.00000	6.00000	42.65000	14.923	42.238	59.258	122.37	0.0019493	
19.00000	6.00000	42.65000	14.748	42.238	59.257	122.26	0.0019503	
20.00000	6.00000	42.65000	14.518	42.238	59.256	122.08	0.0019518	
21.00000	6.00000	42.65000	14.215	42.238	59.255	121.80	0.0019540	
22.00000	6.00000	42.65000	13.812	42.238	59.251	121.33	0.0019577	
23.00000	6.00000	42.65000	13.261	42.238	59.238	120.45	0.0019645	
24.00000	6.00000	42.65000	12.468	42.238	59.181	118.46	0.0019782	
25.00000	6.00000	42.65000	11.209	42.238	58.618	111.83	0.0020054	
26.00000	6.00000	42.65000	8.1310	42.238	29.629	61.422	972.73E-6	
0.00000	7.00000	42.65000	6.3508	42.238	14.999	34.604	463.05E-6	
1.00000	7.00000	42.65000	8.3065	42.238	29.630	61.547	971.71E-6	
2.00000	7.00000	42.65000	9.2713	42.238	29.945	65.751	952.40E-6	
3.00000	7.00000	42.65000	9.9254	42.238	29.982	67.187	942.23E-6	
4.00000	7.00000	42.65000	10.401	42.238	29.991	67.876	936.93E-6	
5.00000	7.00000	42.65000	10.758	42.238	29.994	68.264	933.85E-6	
6.00000	7.00000	42.65000	11.032	42.238	29.996	68.503	931.92E-6	
7.00000	7.00000	42.65000	11.243	42.238	29.996	68.659	930.65E-6	
8.00000	7.00000	42.65000	11.406	42.238	29.997	68.764	929.79E-6	
9.00000	7.00000	42.65000	11.529	42.238	29.997	68.835	929.20E-6	
10.00000	7.00000	42.65000	11.619	42.238	29.997	68.884	928.80E-6	
11.00000	7.00000	42.65000	11.681	42.238	29.997	68.915	928.54E-6	
12.00000	7.00000	42.65000	11.717	42.238	29.997	68.933	928.39E-6	
13.00000	7.00000	42.65000	11.729	42.238	29.997	68.939	928.35E-6	
14.00000	7.00000	42.65000	11.717	42.238	29.997	68.933	928.39E-6	
15.00000	7.00000	42.65000	11.681	42.238	29.997	68.915	928.54E-6	
16.00000	7.00000	42.65000	11.619	42.238	29.997	68.884	928.80E-6	
17.00000	7.00000	42.65000	11.529	42.238	29.997	68.835	929.20E-6	
18.00000	7.00000	42.65000	11.406	42.238	29.997	68.764	929.79E-6	
19.00000	7.00000	42.65000	11.243	42.238	29.996	68.659	930.65E-6	
20.00000	7.00000	42.65000	11.032	42.238	29.996	68.503	931.92E-6	
21.00000	7.00000	42.65000	10.758	42.238	29.994	68.264	933.85E-6	
22.00000	7.00000	42.65000	10.401	42.238	29.991	67.876	936.93E-6	
23.00000	7.00000	42.65000	9.9254	42.238	29.982	67.187	942.23E-6	
24.00000	7.00000	42.65000	9.2713	42.238	29.945	65.751	952.40E-6	
25.00000	7.00000	42.65000	8.3065	42.238	29.630	61.547	971.71E-6	
26.00000	7.00000	42.65000	6.3508	42.238	14.999	34.604	463.05E-6	
GL1	0.00000	0.00000	44.75000	6.2706	44.537	0.0	0.0	
	0.00000	1.00000	44.75000	7.9647	44.537	0.0	0.0	
	0.00000	2.00000	44.75000	8.6859	44.537	0.0	0.0	
	0.00000	3.00000	44.75000	8.9971	44.537	0.0	0.0	
	0.00000	4.00000	44.75000	8.9971	44.537	0.0	0.0	
	0.00000	5.00000	44.75000	8.6859	44.537	0.0	0.0	
	0.00000	6.00000	44.75000	7.9647	44.537	0.0	0.0	
	0.00000	7.00000	44.75000	6.2706	44.537	0.0	0.0	
	0.00000	8.00000	44.75000	4.5204	44.537	0.0	0.0	
GL2	-4.50000	0.00000	44.75000	2.0740	44.537	0.0	0.0	
	-4.50000	1.00000	44.75000	2.1966	44.537	0.0	0.0	
	-4.50000	2.00000	44.75000	2.2859	44.537	0.0	0.0	
	-4.50000	3.00000	44.75000	2.3328	44.537	0.0	0.0	
	-4.50000	4.00000	44.75000	2.3328	44.537	0.0	0.0	
	-4.50000	5.00000	44.75000	2.2859	44.537	0.0	0.0	
	-4.50000	6.00000	44.75000	2.1966	44.537	0.0	0.0	
	-4.50000	7.00000	44.75000	2.0740	44.537	0.0	0.0	
	-4.50000	8.00000	44.75000	1.9297	44.537	0.0	0.0	
GL3	-9.00000	0.00000	44.75000	1.0129	44.537	0.0	0.0	
	-9.00000	1.00000	44.75000	1.0436	44.537	0.0	0.0	
	-9.00000	2.00000	44.75000	1.0651	44.537	0.0	0.0	
	-9.00000	3.00000	44.75000	1.0762	44.537	0.0	0.0	
	-9.00000	4.00000	44.75000	1.0762	44.537	0.0	0.0	
	-9.00000	5.00000	44.75000	1.0651	44.537	0.0	0.0	
	-9.00000	6.00000	44.75000	1.0436	44.537	0.0	0.0	
	-9.00000	7.00000	44.75000	1.0129	44.537	0.0	0.0	
	-9.00000	8.00000	44.75000	0.97444	44.537	0.0	0.0	
GL4	0.00000	4.00000	44.75000	8.9971	44.537	0.0	0.0	
	-1.00000	4.00000	44.75000	5.7098	44.537	0.0	0.0	
	-2.00000	4.00000	44.75000	4.1878	44.537	0.0	0.0	
	-3.00000	4.00000	44.75000	3.2384	44.537	0.0	0.0	
	-4.00000	4.00000	44.75000	2.5869	44.537	0.0	0.0	
	-5.00000	4.00000	44.75000	2.1138	44.537	0.0	0.0	
	-6.00000	4.00000	44.75000	1.7562	44.537	0.0	0.0	
	-7.00000	4.00000	44.75000	1.4778	44.537	0.0	0.0	
	-8.00000	4.00000	44.75000	1.2560	44.537	0.0	0.0	
	-9.00000	4.00000	44.75000	1.0762	44.537	0.0	0.0	
GL5	13.00000	-6.00000	44.75000	3.0581	44.537	0.0	0.0	
	13.00000	-7.00000	44.75000	2.6201	44.537	0.0	0.0	
	13.00000	-8.00000	44.75000	2.2592	44.537	0.0	0.0	
	13.00000	-9.00000	44.75000	1.9582	44.537	0.0	0.0	
	13.00000	-10.00000	44.75000	1.7049	44.537	0.0	0.0	
	13.00000	-11.00000	44.75000	1.4899	44.537	0.0	0.0	
	13.00000	-12.00000	44.75000	1.3063	44.537	0.0	0.0	
GL6	26.00000	-6.00000	44.75000	1.9019	44.537	0.0	0.0	
	26.00000	-7.00000	44.75000	1.6605	44.537	0.0	0.0	
	26.00000	-8.00000	44.75000	1.4577	44.537	0.0	0.0	
	26.00000	-9.00000	44.75000	1.2853	44.537	0.0	0.0	
	26.00000	-10.00000	44.75000	1.1373	44.537	0.0	0.0	
	26.00000	-11.00000	44.75000	1.0093	44.537	0.0	0.0	
	26.00000	-12.00000	44.75000	0.89782	44.537	0.0	0.0	

Table 2 - Summary of Pdssp Output

Name	Coords		Level (mOD)	Demolition & Excavation -90 kPa (heave)			Construction +60 kPa (settlement)		Total settlement - Long term heave (mm)
	X	Y		Imm(mm)	Total(mm)	Long term(mm)	Imm(mm)	Total(mm)	
GI1	0	0	44.75	-6.6955	-10.754	-4.0585	3.9703	6.2706	2.2121
	0	1	44.75	-8.6128	-13.504	-4.8912	5.1594	7.9647	3.0735
	0	2	44.75	-9.5059	-14.844	-5.3381	5.6438	8.6859	3.3478
	0	3	44.75	-10.031	-15.639	-5.608	5.8516	8.9971	3.3891
	0	4	44.75	-10.315	-16.071	-5.756	5.8516	8.9971	3.2411
	0	5	44.75	-10.406	-16.209	-5.803	5.6438	8.6859	2.8829
	0	6	44.75	-10.315	-16.071	-5.756	5.4394	7.9647	2.2087
	0	7	44.75	-10.031	-15.639	-5.608	3.9703	6.2706	0.6626
	0	8	44.75	-9.5059	-14.844	-5.3381	2.745	4.5204	-0.8177
GI2	-4.5	0	44.75	-2.1586	-3.9564	-1.7978	1.1519	2.074	0.2762
	-4.5	1	44.75	-2.3326	-4.2297	-1.8971	1.2307	2.1966	0.2995
	-4.5	2	44.75	-2.4799	-4.4607	-1.9808	1.2882	2.2859	0.3051
	-4.5	3	44.75	-2.5912	-4.635	-2.0438	1.3185	2.3328	0.289
	-4.5	4	44.75	-2.6602	-4.743	-2.0828	1.3185	2.3328	0.25
	-4.5	5	44.75	-2.6835	-4.7796	-2.0961	1.2882	2.2859	0.1898
	-4.5	6	44.75	-2.6602	-4.743	-2.0828	1.2307	2.1966	0.1138
	-4.5	7	44.75	-2.5912	-4.635	-2.0438	1.1519	2.074	0.0302
	-4.5	8	44.75	-2.4799	-4.4607	-1.9808	1.0594	1.9297	-0.0511
GI3	-9	0	44.75	-0.96001	-2.0191	-1.05909	0.4909	1.0129	-0.04619
	-9	1	44.75	-1.0091	-2.0999	-1.0908	0.50976	1.0436	-0.0472
	-9	2	44.75	-1.0497	-2.1666	-1.1169	0.52296	1.0651	-0.0518
	-9	3	44.75	-1.08	-2.2163	-1.1363	0.52976	1.0762	-0.0601
	-9	4	44.75	-1.0988	-2.247	-1.1482	0.52976	1.0762	-0.072
	-9	5	44.75	-1.1052	-2.2573	-1.1521	0.52296	1.0651	-0.087
	-9	6	44.75	-1.0988	-2.247	-1.1482	0.50976	1.0436	-0.1046
	-9	7	44.75	-1.08	-2.2163	-1.1363	0.4909	1.0129	-0.1234
	-9	8	44.75	-1.0497	-2.1666	-1.1169	0.46738	0.97444	-0.14246
GI4	0	4	44.75	-10.315	-16.071	-5.756	5.8516	8.9971	3.2411
	-1	4	44.75	-6.6205	-10.778	-4.1575	3.5446	5.7098	1.5523
	-2	4	44.75	-4.883	-8.1621	-3.2791	2.5295	4.1878	0.9087
	-3	4	44.75	-3.761	-6.4491	-2.6881	1.9051	3.2384	0.5503
	-4	4	44.75	-2.972	-5.2294	-2.2574	1.482	2.5869	0.2425
	-5	4	44.75	-2.3898	-4.3188	-1.929	1.1784	2.1138	0.1848
	-6	4	44.75	-1.9458	-3.6163	-1.6705	0.95164	1.7562	0.0857
	-7	4	44.75	-1.5988	-3.0609	-1.4621	0.77717	1.4778	0.0157
	-8	4	44.75	-1.3224	-2.6133	-1.2909	0.63983	1.256	-0.0349
	-9	4	44.75	-1.0988	-2.247	-1.1482	0.52976	1.0762	-0.072
	13	-6	44.75	-3.0813	-5.5134	-2.4321	1.742	3.0581	0.626
	13	-7	44.75	-2.5959	-4.7437	-2.1478	1.4638	2.6201	0.4723
	13	-8	44.75	-2.1968	-4.1052	-1.9084	1.2366	2.2592	0.3508
	13	-9	44.75	-1.8652	-3.5697	-1.7045	1.0487	1.9582	0.2537
	13	-10	44.75	-1.5872	-3.1166	-1.5284	0.89196	1.7049	0.1755
13	-11	44.75	-1.3575	-2.7303	-1.3778	0.76015	1.4899	0.1121	
13	-12	44.75	-1.1532	-2.3991	-1.2459	0.64861	1.3063	0.0604	
GI6	26	-6	44.75	-1.8423	-3.4849	-1.6486	1.0306	1.8019	0.2593
	26	-7	44.75	-1.5732	-3.0537	-1.4805	0.8786	1.6605	0.18
	26	-8	44.75	-1.3479	-2.6889	-1.341	0.75218	1.4577	0.1167
	26	-9	44.75	-1.1572	-2.3769	-1.2197	0.64578	1.2853	0.0656
	26	-10	44.75	-0.99448	-2.1077	-1.11327	0.55537	1.1373	0.02408
	26	-11	44.75	-0.85467	-1.8738	-1.01913	0.47798	1.0093	-0.00983
	26	-12	44.75	-0.73392	-1.6694	-0.93548	0.41135	0.89782	-0.03766

84 - 90 Camden Mews & 59 Camden Park Road

Notes

Negative values represent heave, positive values represent settlement

ASHTON COURT

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12-06-15

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GROUND MOVEMENT ASSESSMENT
(Ground movements & strain calculations).

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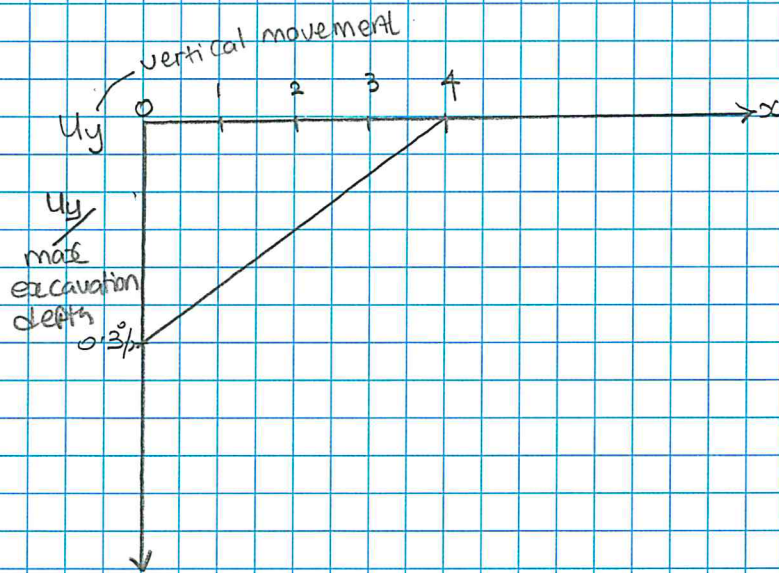
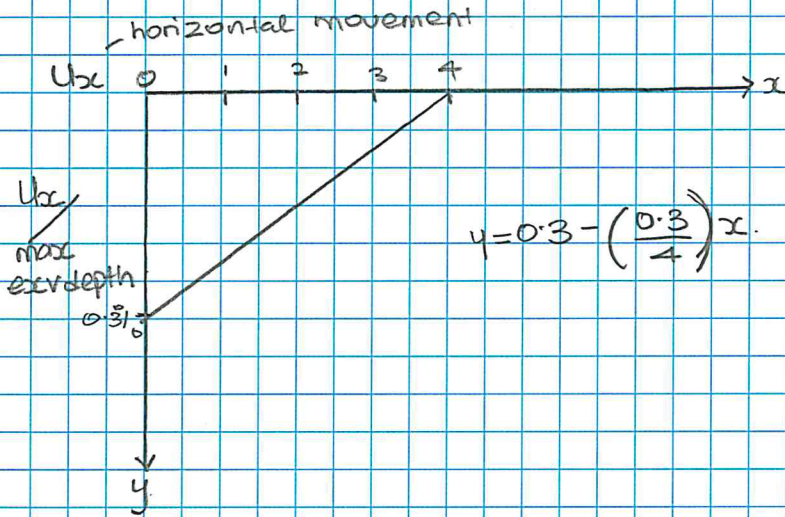
Engineer
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Checked
EMB.

L (length of 103 Camden Mews) = 9m

$H = 6m$ (two storey building)

Ground surface movement of 0.3% of max excavation depth (derived from Table 2.4 of CIRIA C580).



$\frac{L}{H}$ if considering full length of building
 $= \frac{9}{6} = 1.5$

$\frac{L}{H} = 0.75$ if considering movements at halfway along.
103 Camden Mews

SAMPLE CALC.

max exc.
depth = 3m

Movement @ 0m (i.e on the party wall)

$$y = 0.3 - \left(\frac{0.3}{4}\right) \times 0$$

$$y = 0.3\%$$

$$y = \frac{Ux}{\text{max excavation depth}}$$

$$\frac{0.3}{100} = \frac{Ux}{3}$$

$$Ux = 9\text{mm}$$

Since graphs for U_{xc} & U_{yc} are the same

$$U_{yc} = 9\text{mm @ 0m}$$

	Distance from sheet pile wall (m)		
	0	4.5	9
U_{xc}	9	6	3
U_{yc}	9	6	3

For $L = 4.5$ (halfway on 103 Camden
Mews)

$$E_h = \frac{Sh}{L} = \frac{0.003}{4.5} \times 100$$

$$= 0.06\%$$

For $L = 9$ (whole length of
building)

$$E_h = \frac{Sh}{L} = \frac{0.006}{9} \times 100$$

$$= 0.06\%$$

△ Vertical movement

@ 0m c580 - 9mm (settlement)
Pd isp - 10mm (heave)

resultant = 1mm

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@ 4.5m CS80 - 6mm
Pdisp. - 3mm
resultant 3mm

@ 9m CS80 - 3mm
Pdisp - 1mm
resultant 2mm.

$$\therefore \Delta = 3\text{mm} + 1\text{mm} = 4\text{mm}$$

$$\frac{\Delta}{L} = \frac{0.004}{4.5} \times 100 = 0.08\%$$

$$\frac{\Delta}{L} = \frac{0.002}{4.5} \times 100 = 0.04\%$$

$$\frac{E_{\text{ny}}}{E_{\text{lim}}} = \frac{0.06}{0.15} = 0.4$$

Elim values
= 0.075 -
0.15% (Table
2.5 of CIRIA
CS80)

$$\frac{\Delta/L}{E_{\text{lim}}} = \frac{0.08}{0.15} = 0.5$$

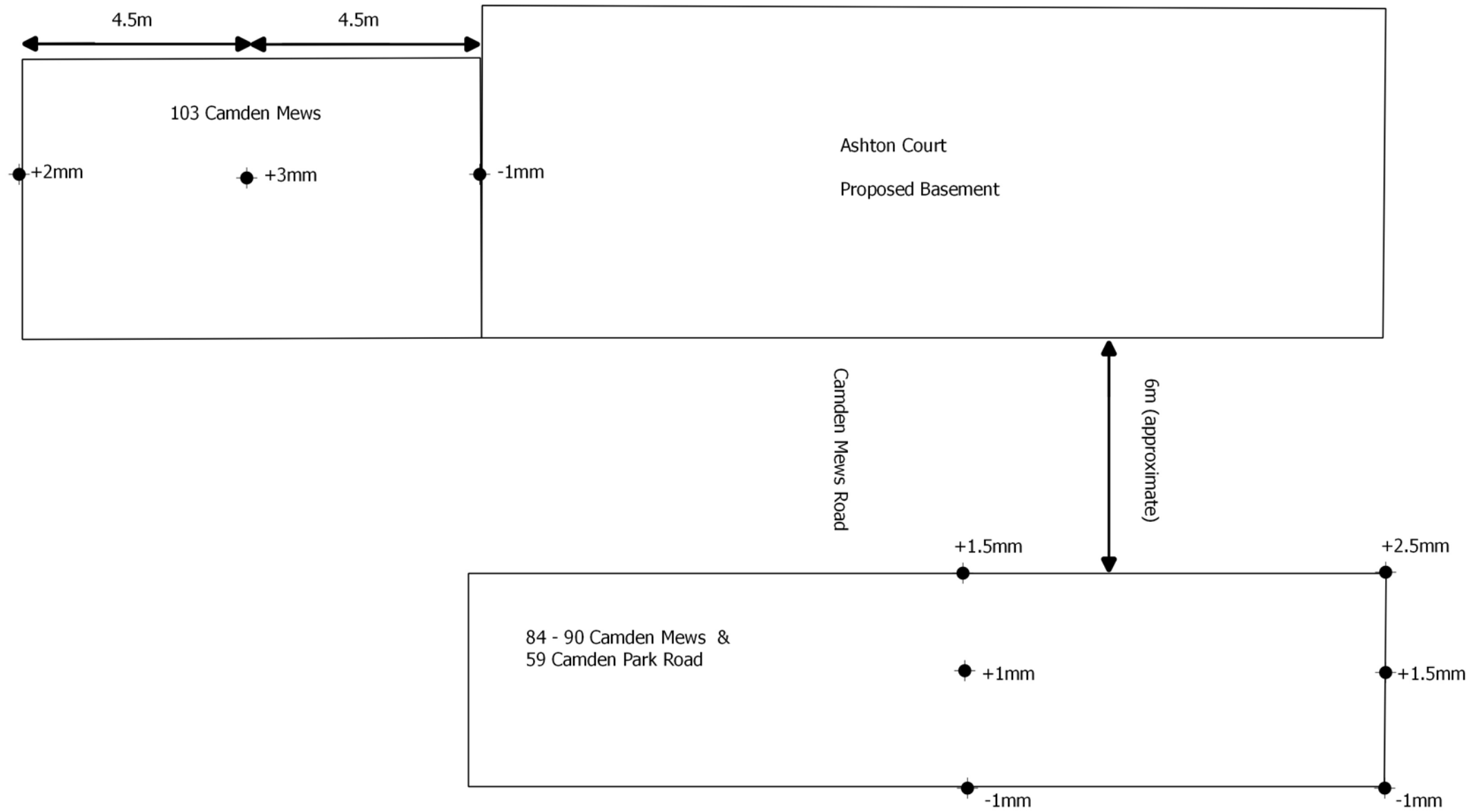
Figure 2.18b shows that for $L/H = 0.5$ and 1.5, damage to 103 Camden Mews is less than the upper bound of 'slight'

Figure 2.18c shows that the damage category is 2 for $L/H = 1$



Legend

- Heave
- + Settlement



NTS

Ashton Court
 Client: Origin Housing
 Vertical surface movements due to demolition and excavation

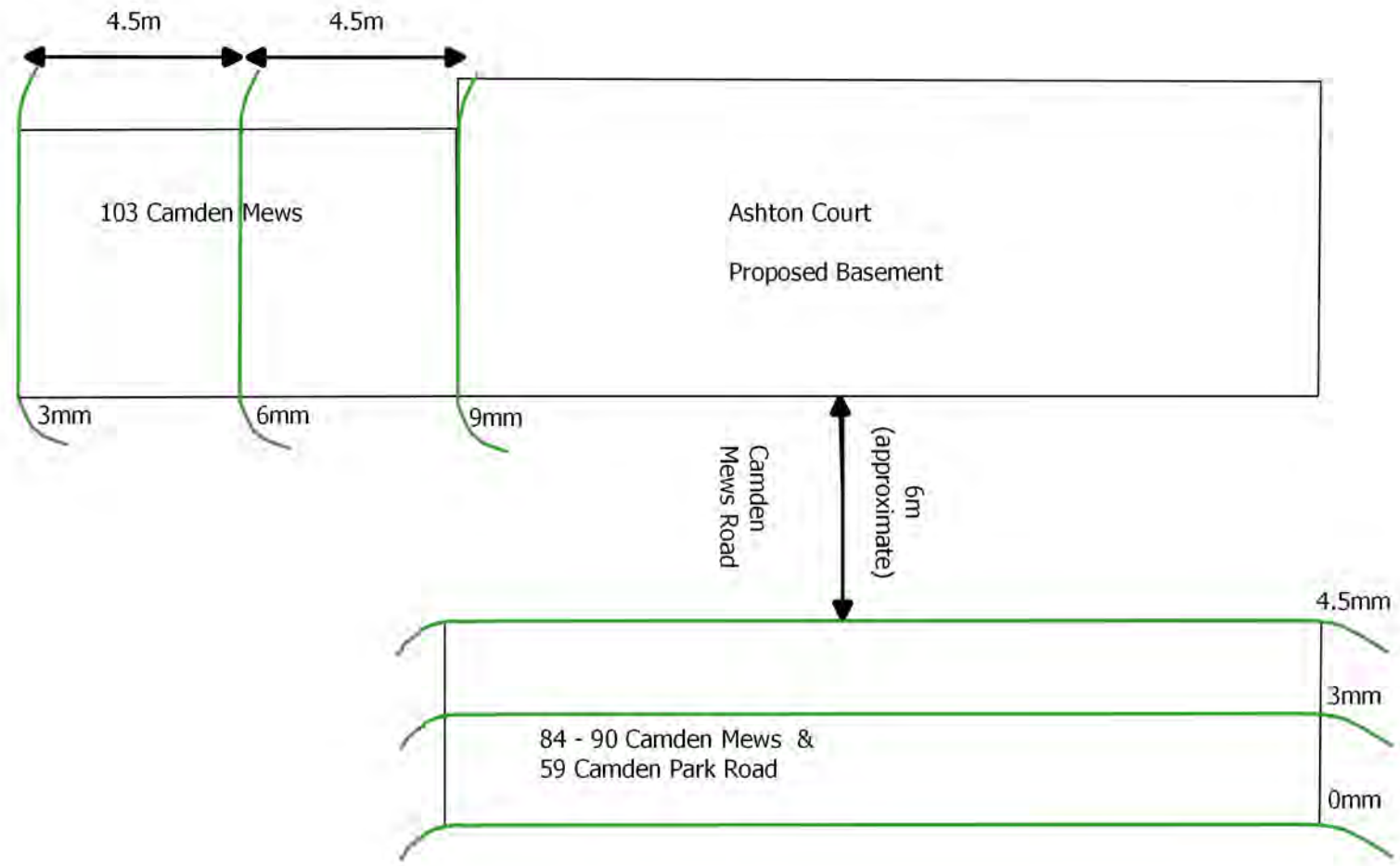
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Legend

— Horizontal Movement



NTS

Ashton Court
 Client: Origin Housing

Contour plot of horizontal surface movements around the site due to demolition and excavation

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