



**34 Queens Grove  
NW8 6HN**

**DESIGN PHILOSOPHY**

March 2015

**Project Ref: 12686**

**REVISION HISTORY**

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<b>Rev</b>	<b>Purpose</b>	<b>Date</b>	<b>Issued By</b>	<b>Approved</b>
Rev 0	Initial report	30.03.15	GG	BC

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## **INTRODUCTION**

Green Structural Engineering has been involved in numerous successful basement designs in a number of London Boroughs on behalf of private clients, developers and contractors.

The basement projects previously undertaken successfully have been of a similar size to that proposed in this application and quite often on a much larger scale and complexity.

Green Structural engineering also undertakes the temporary works design and sequencing for a number of contractors who operate in RBKC, LBHF and Westminster.

This experience has positioned GSE at the forefront of basement design and indeed temporary works design for basement construction. This experience has led to an in-depth understanding and appreciation of the design parameters that should be considered for all basement construction projects.

GSE holds £2million in professional indemnity insurance and is a member of the ACE.

## **SCOPE OF WORKS**

A new single story basement is to be created under the footprint of the existing property and both the front and rear gardens. The proposed basement will create a wine store, larder, media store, sports equipment store, winter and summer closet, archives and storage room, and changing room. Both front and rear lightwells will be created to provide natural light and ventilation to the basement.

## **DESCRIPTION OF 34 QUEENS GROVE AND ADJOINING PROPERTIES**

The existing property has five stories ranging from lower ground to the existing loft conversion at fifth floor level. The property is semi-detached sharing a party wall with number 35 Queens Grove.

It is of traditional construction; loadbearing masonry walls supporting timber floors to all levels and a timber rafter roof.

The adjoining properties are of similar construction and look to be in sound condition from an external non – intrusive visual examination.

## **GEOLOGY AND HYDROLOGY CONDITIONS (see also report in Appendix A)**

A site – specific borehole has been sunk to 6.0m depth below lower ground level which is below the proposed formation level. This confirms that ground conditions are generally consistent with those expected for the area. Specifically this comprises of dark brown clayey made ground to depth of 0.8m underlain by mid brown clay containing grey mottle (London Clay) to 6.0m where the borehole terminates. Please see appendix A for the full geotechnical and hydrological report.

The borehole was noted to be dry on completion and as such it is unlikely groundwater will be affected by the basement development.

The basement will be designed with the recommendations of BS8102:1990; Protection of structures against water from the ground. Clause 3.4 states that a water table should be assumed at 1.0 metre below ground level.

The design bearing pressure will be limited to 175kN/m<sup>2</sup> which, given the in-situ testing noted from the borehole, we consider conservative. Therefore at formation level, the existing geology at the depth of the proposed basement will be capable of supporting the loads generated by the new structure.

Any effect on surface water will be negligible as the rear basement will have 1.0m of soil above the basement slab allowing free drainage of surface water.

The site – specific borehole has identified a limited amount of ground water within the zone of the new structure. Ground water will be able to flow around and under the proposed basement within the permeable sand and gravel layer identified in the site investigation and so the impact on ground water flows and levels will be negligible.

## **PROPOSED WORKS**

As can be seen from the proposed drawings in appendix C, the proposed works involve the construction of a retrofit basement under the rear garden.

The underpins will be constructed using reinforced concrete (RC) as will the new basement slab and retaining walls for the light well. The ground floor support will be via steel beams positioned under the existing load bearing walls. Any new floor structure at ground level will be constructed from timber joists or beam and block as specified by the client depending on their requirements.

The proposed basement under the existing property will be formed using an underpinning method, constructed in sections each no wider than 1000mm, with no adjacent underpins constructed within a 48 hour period. This method of construction reduces the amount of potential ground movement and so minimises the effects of settlement of the adjacent structures.

## **DESIGN PRINCIPALS AND PHILOSOPHY**

### **Design Philosophy**

The design of the structural elements will be carried out in such a way to limit the impact of the structural works on the existing building construction and that of the neighbouring properties.

### **Deflection Limits**

Beams supporting existing masonry	= span/500 Total Load
Beams supporting new structure	= span/360 Live Load

### **New Basement Structure**

The existing load – bearing structure will be underpinned in a traditional ‘1 to 5’ sequence. The underpins will comprise of a vertical stem which will be immediately beneath the existing wall and will be at least the same thickness as the existing wall. In the case of a party wall, the rear face of the stem will be in line with the face of the wall above so as not to encroach into the adjacent

property's space, should they wish to construct a similar basement in the future. The reinforcement in the stems will be designed for bending about the top of the base in the permanent case.

The vertical loads applied to the underpin stems from the existing structure will be calculated according to the thickness and height of the existing structure above.

The underpins will be designed for the temporary and permanent cases, as follows: In the temporary case, the underpins will be designed for soil pressures and a surcharge. The factor of safety against overturning and sliding will be taken as 1.5.

In the permanent case, the underpins will be designed for soil pressures, a surcharge and water pressures calculated at 1 m below the retained height. The new basement slab will be structurally connected to the underpinning bases using dowel bars, therefore it will be assumed that the new basement slab will restrain the under pins against sliding.

Surcharge on the underpins will be taken as follows:

Internal live load (e.g. floors) = 10.0 kN/m<sup>2</sup>

Space underneath existing timber joists = 10.0 kN/m<sup>2</sup>

External: gardens, footpaths, driveways = 10 kN/m<sup>2</sup>

External: up to or within 1.0m of the highway = 20 kN/m<sup>2</sup>

The basement slab will be designed for uplift due to water pressure, spanning between the bases of opposite underpins. The net uplift pressure is taken as the head of water minus the dead load of the basement slab and any permanent finishes, e.g. screed.

### **Geotechnical Design**

The retaining walls will be designed using 'active' pressures (where movement of the retaining wall is likely and acceptable), as opposed to 'at rest' pressures (where movement of the retaining wall is unlikely or unacceptable). The underpinning process, where soil is excavated underneath an existing load – bearing wall and a vertical shear face of soil is exposed, allows the excavated face of soil to move, thus mobilizing the 'active' pressures. In addition, once the underpin has been constructed and is working as a retaining wall, the retaining wall is likely to deflect, thus mobilizing the 'active' pressures. These movements will be very slight and will most likely have a negligible effect on the vertical settlement of the retained soil behind the underpinning / retaining walls. These movements are considered acceptable.

Ground – bearing pressures below the underpinning bases will be calculated for the temporary condition. In the permanent condition, the new basement slab will be tied in to the retaining wall bases, hence the entire substructure will act as a raft foundation. Ground – bearing pressures will not be an issue in this condition.

### **Water Table**

The site specific borehole log shows some ground water to be present. The ground water will not be affected by the construction of the basement as the ground water will simply flow around and underneath the proposed basement.

An assumed accidental case will be used at 1.0 m below ground level for design of uplift on the slab and lateral forces on the retaining walls.

## **POTENTIAL IMPACT ON ADJOINING PROPERTIES**

The underpinning of the perimeter walls and lowering of the floor slab will be carried out using an underpinning method, with each pin constructed no wider than 1000mm, with no adjacent underpins constructed within a 48 hour period.

The proposed works, if executed correctly and in accordance with the appointed Engineer's details and procedures, will pose no significant threat to the structural stability of the property or indeed adjoining properties.

## **SLOPE STABILITY**

The site is located on ground that can be classified as flat (less than 7°) and so geological slope instability is not applicable to this site.

The proposed works will not alter the slope of the site profile to greater than 7° so geological slope instability will not become applicable to this site.

The presence of made ground to the depth of 0.8m below lower ground level does not constitute a cause for concern as this is less than a storey height and so will be removed as part of the basement construction.

## **DESIGN PRINCIPAL DRAWINGS**

See drawings GA01, D01 in the Appendices. GA01 is a general basement plan showing the proposed underpinning bays and suggested underpinning sequence while D01 shows a section taken through the proposed underpinning to each of the party walls.

## **SPECIFICATION**

Please see appendix F for the underpinning specification.

*Prepared By*

**E. Alexander**

*B. Eng*

*Approved*



**Brian Cochrane**

*BEng, CEng, MStructE.*



## **APPENDICES**

The following appendices are included with this report.

- Appendix A - Site Investigation
- Appendix B - Existing floor plans
- Appendix C - Proposed floor plans
- Appendix D - Design calculations
- Appendix E - Construction Principal Drawings GA/01, D/01
- Appendix F - Underpinning Specification

**APPENDIX A**

**SITE INVESTIGATION**



# Geotechnical Survey Report

FSI Ref: 9144  
Issue Date: December 2014

Address: 34 Queens Grove  
London  
NW8

Engineer: David Kavanagh / Dan Vickerstaff

Company: Cranbrook Basements

Director: Martin Rush MSc FGS  
Office Manager: Louise Hiscock BSc (Hons)  
Report Writer: Perry Martin AMCIHT

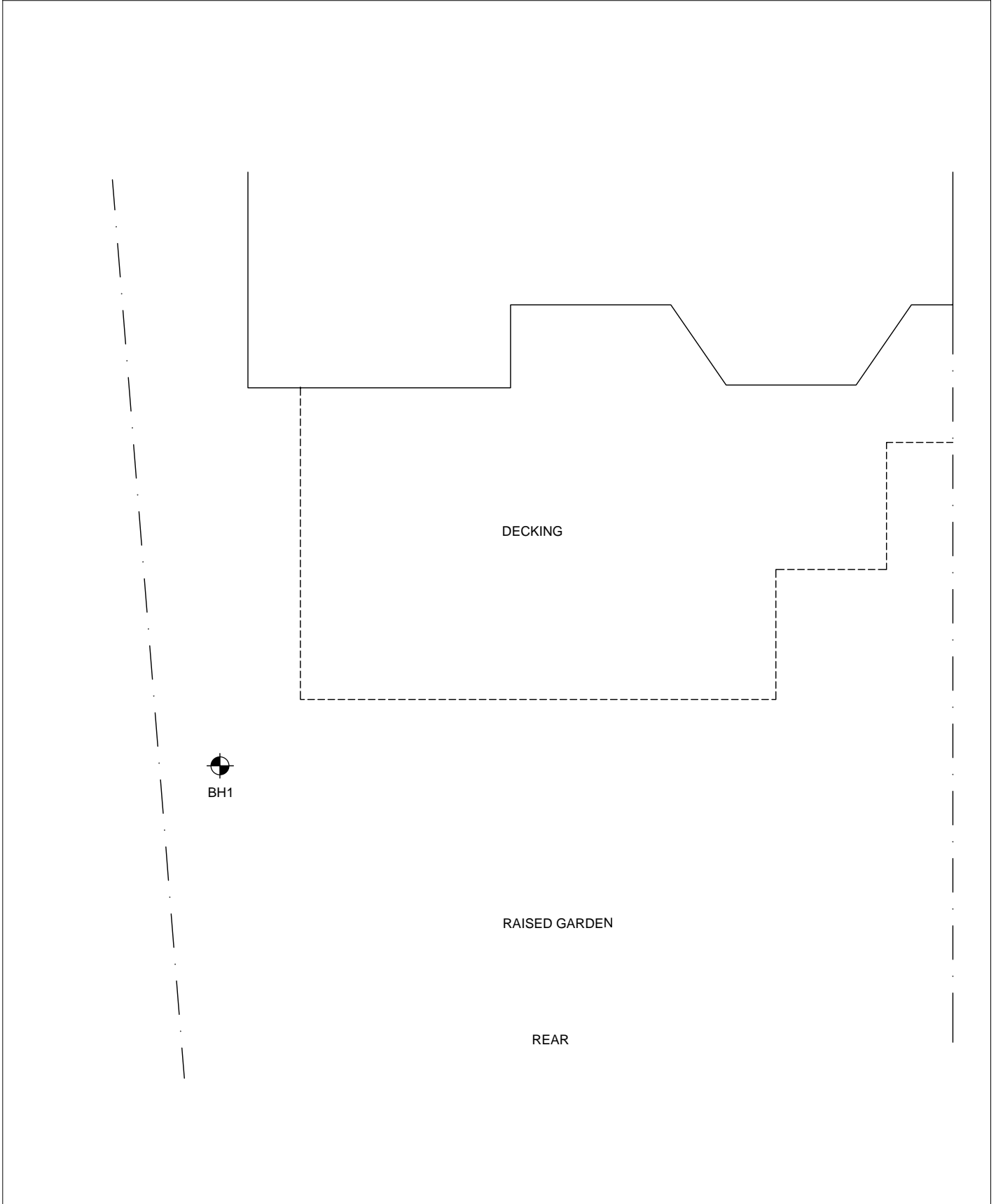
Laboratory Manager: Lara Knight







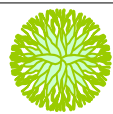



## SITE PLAN

**Property Address:** 34 Queens Grove, London, NW8

**Client Claim Ref:** 34 Queens Grove

**Survey date:** 10/12/2014


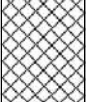
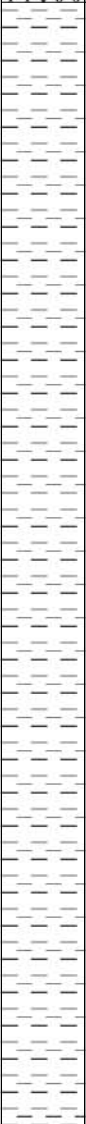
**Operative:** SE1



<b>Scale:</b>	<b>Drawn by:</b>	<b>Key:</b>							
NTS	LK	 Trial Pit	 Manholes	 Rain Water Pipe	 Surface Water Gully	 Shrub	 Tree (Conifer)	 Tree (Deciduous)	
		 Borehole	 Soil & Vent Pipe	 Foul Water Gully					

## BOREHOLE LOG

**Property Address:** 34 Queens Grove, London, NW8  
**Client Claim Ref:** 34 Queens Grove      **Survey date:** 10/12/2014      **Operative:** SE1

**Borehole ID:** BH1      **Hole Type:** FA      **Scale:** 1:35

Water Strikes	Samples		Insitu Tests		Depth (m)	Legend	Stratum Description and Observations
	Type	Depth (m)	Type	Results			
					0.30		Dark brown Topsoil
					0.80		Dark brown clayey MADE GROUND containing brick and gravel
		1.00	V	104.00 104.00			Mid brown CLAY containing grey mottle Noted to contain orange sand pockets from 0.80m to 2.20m
		2.00	V	118.00 122.00			
		3.00	V	140.00			
		4.00	V	140.00			
		5.00	V	140.00			
		6.00	V	140.00	6.00		
							End of Borehole at 6.00 m

**Key:**  Water Strike      D Disturbed Sample      V Insitu vane test (kPa)      MP Mackintosh Probe Test

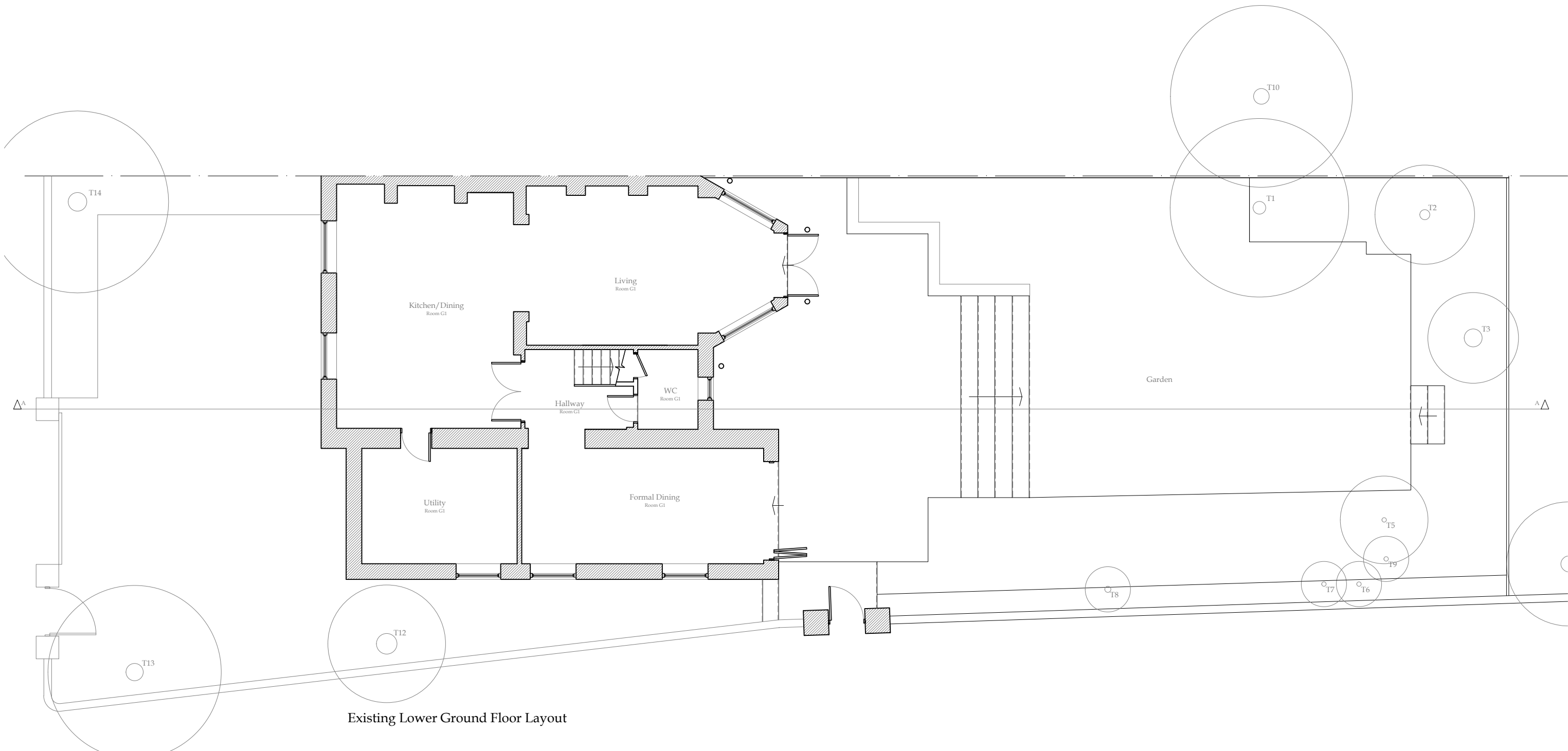
Remarks: Borehole was closed at 6.00m as requested. Borehole was noted to be dry on completion.

N.b. Unless otherwise stated small vane paddle used. To convert MP to SPT divide average blows for 75mm by 1.5

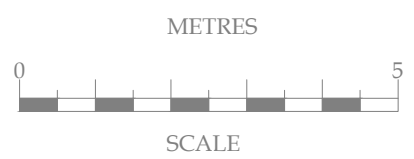


## **APPENDIX B**

## **EXISTING PLANS**

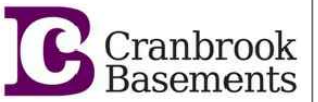


Existing Lower Ground Floor Layout



No.	Date	Amendment	Initials
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Client : Ms L Clarke  
 Project : 34 Queen's Grove  
 London  
 NW8 6HN

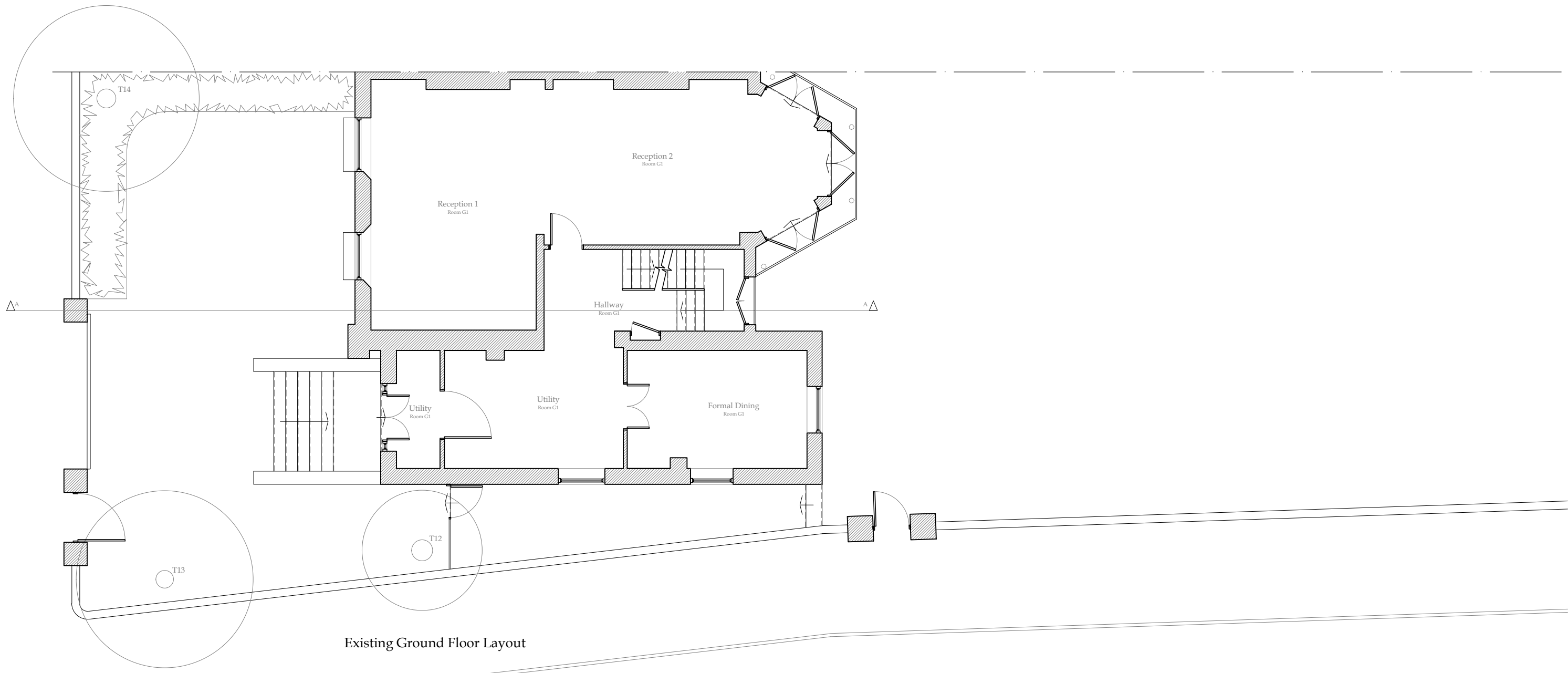


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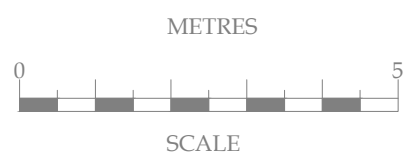
Drawing : Existing Lower Ground Floor Layout

Scale : 1:100 @ A3	Status : DESIGN	Rev :
Date : 9 Jan 15	Dwg No : 2238-100	

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Existing Ground Floor Layout



No.	Date	Amendment	Initials
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Client : Ms L Clarke  
 Project : 34 Queen's Grove  
 London  
 NW8 6HN

Drawing : Existing Ground Floor Layout

Scale : 1:100 @ A3  
 Date : 9 Jan 15

Status : DESIGN  
 Dwg No : 2238-101

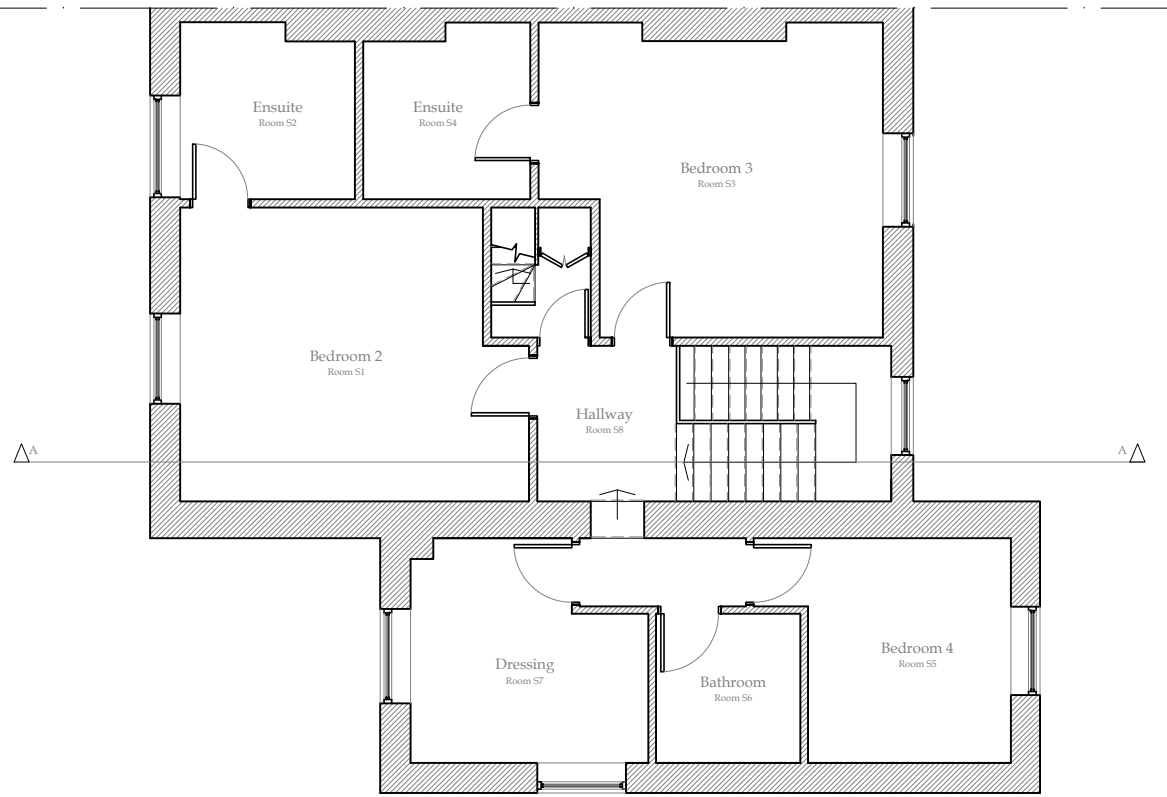


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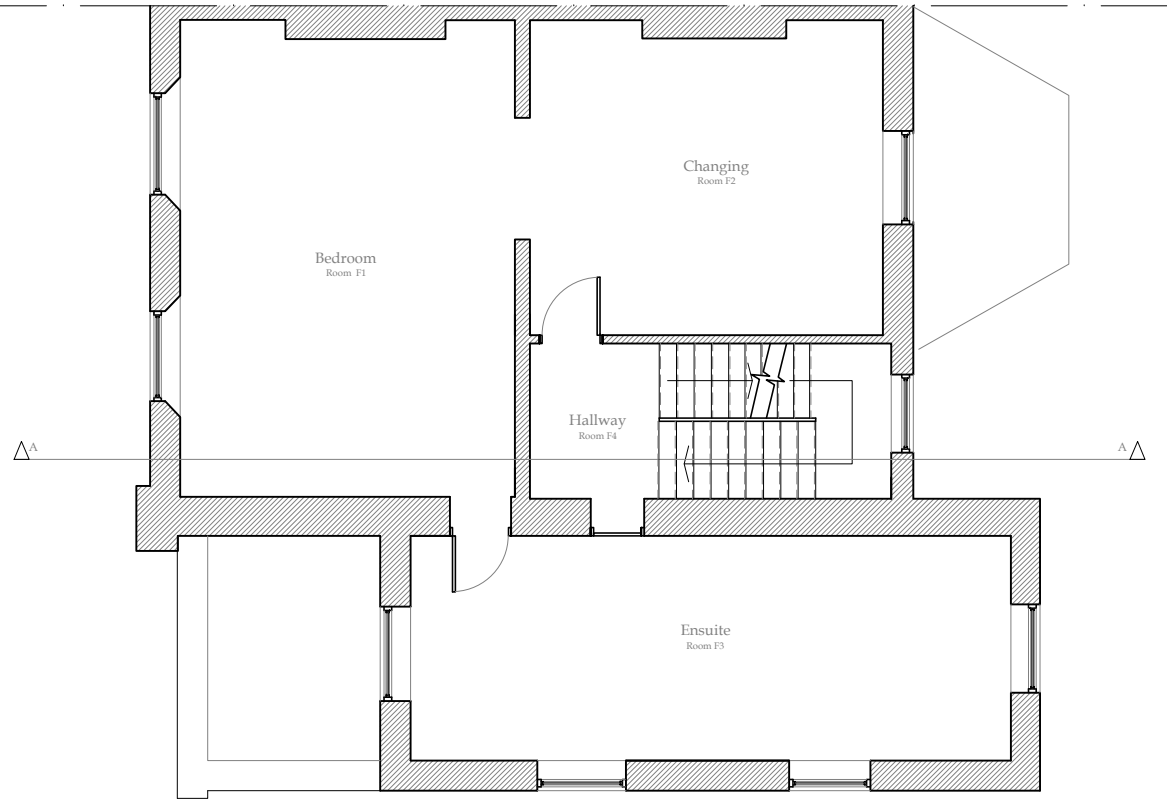


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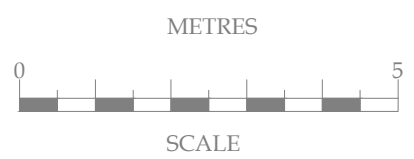




Existing Second Floor Layout

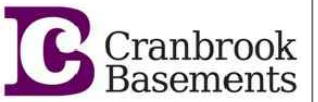


Existing First Floor Layout



No.	Date	Amendment	Initials
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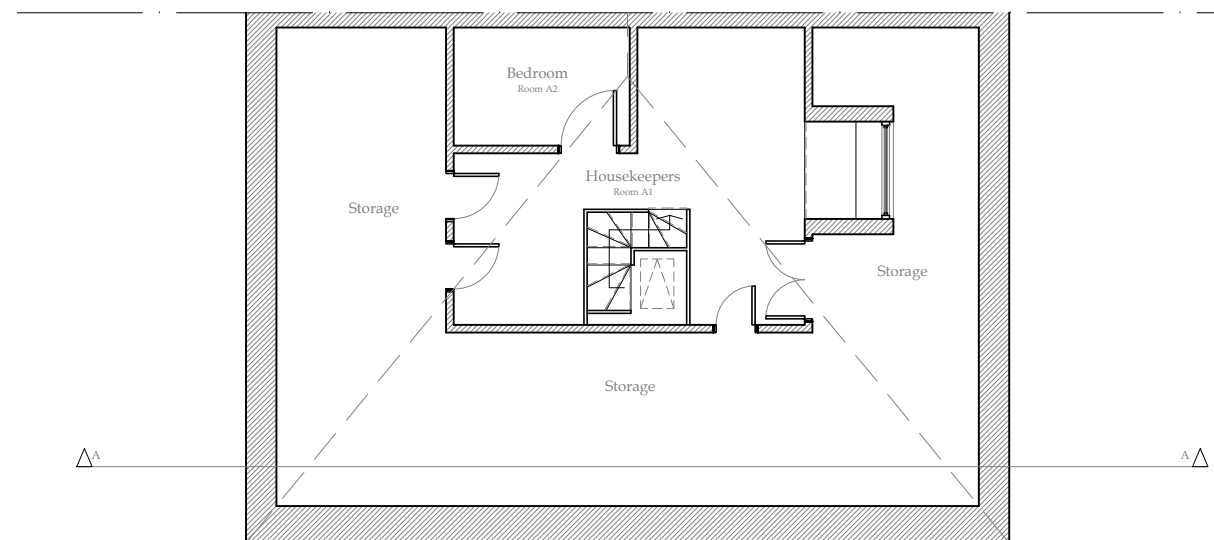


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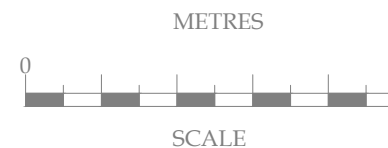
Drawing : Existing First and Second Floor Layouts

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Date : 9 Jan 15	Dwg No : 2238-102	

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Existing Attic Layout



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Drawing : Existing Attic Layout

Scale : 1:100 @ A3	Status : DESIGN	Rev :
Date : 9 Jan 15	Dwg No : 2238-103	



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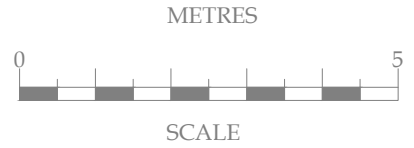
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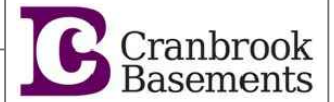
Existing Front Elevation



Existing Rear Elevation

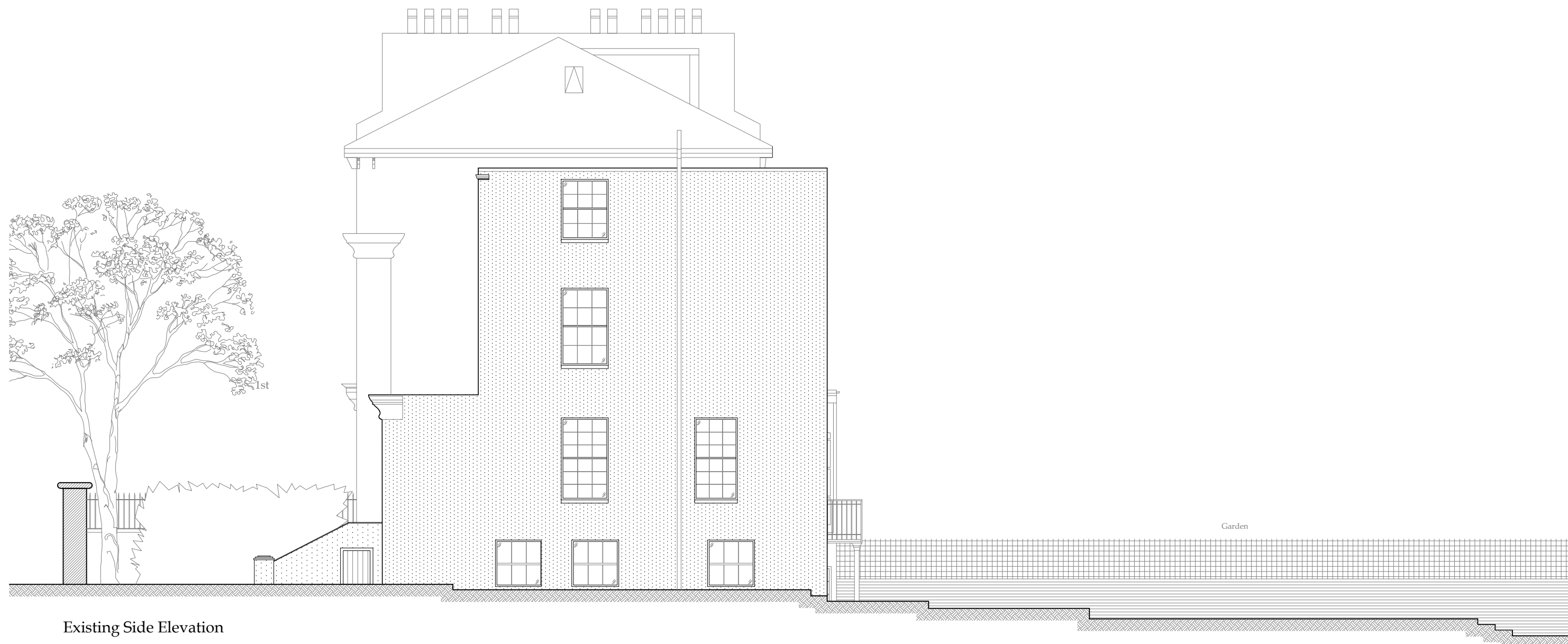


No.	Date	Amendment	Initials
<p>Client : Ms L Clarke</p> <p>Project : 34 Queen's Grove London NW8 6HN</p> <p>Drawing : Existing Front and Rear Elevations</p>			
<p>Scale : 1:100 @ A3</p>		<p>Status : DESIGN</p>	<p>Rev :</p>
<p>Date : 9 Jan 15</p>		<p>Dwg No : 2238-104</p>	
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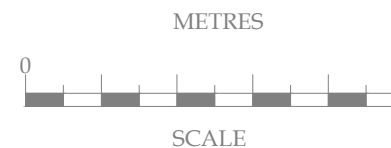


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Existing Side Elevation



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Client : Ms L Clarke

Project : 34 Queen's Grove  
London  
NW8 6HN

Drawing : Existing Side Elevation

Scale : 1:100 @ A3

Date : 9 Jan 15

Status : DESIGN

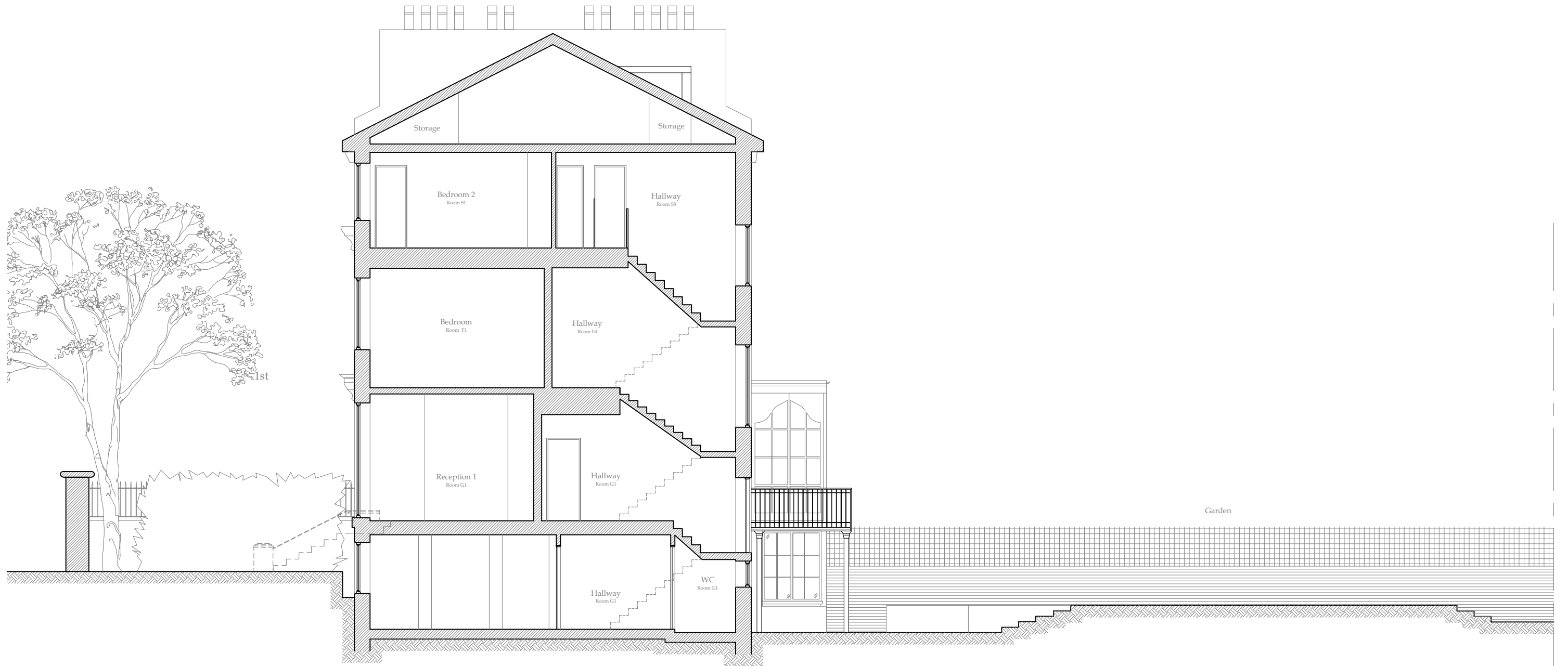
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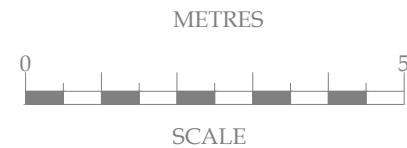
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Existing Section A-A



No.	Date	Amendment	Initials
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Client : Ms L Clarke

Project : 34 Queen's Grove  
London  
NW8 6HN

Drawing : Existing Side Elevation

Scale : 1:100 @ A3

Status : DESIGN

Rev :

Date : 9 Jan 15

Dwg No : 2238-105



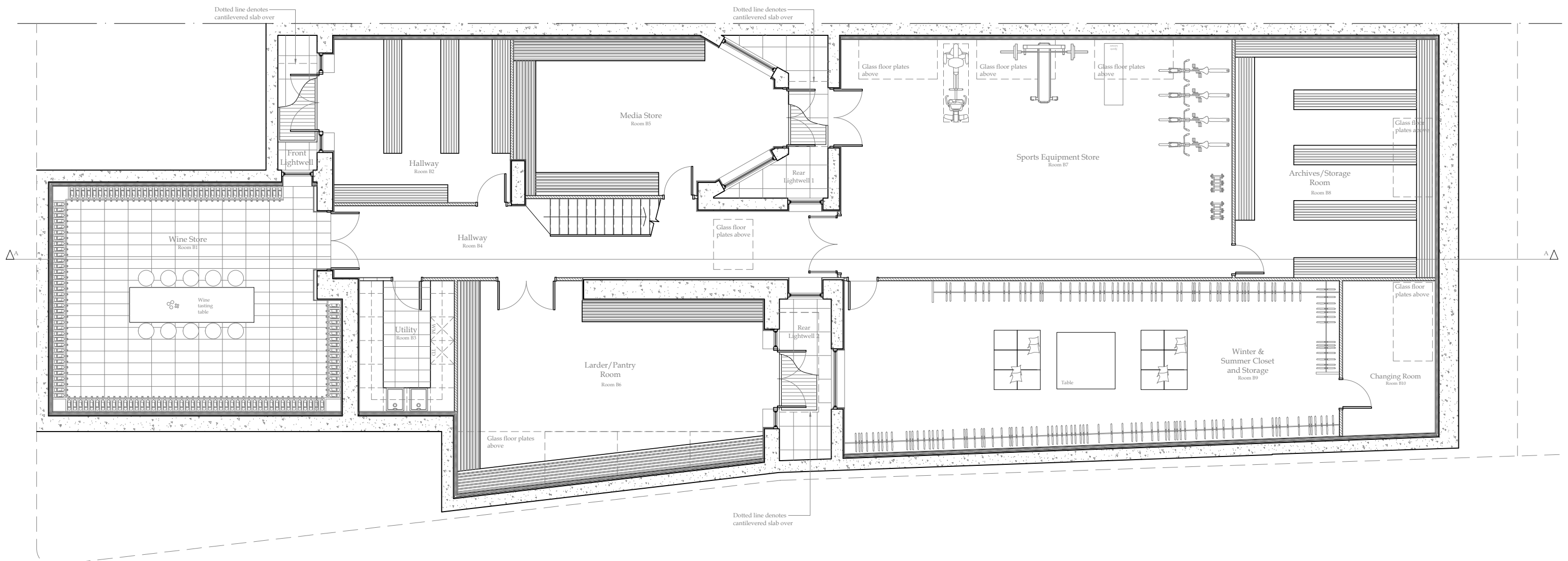
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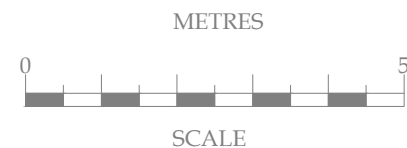
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**APPENDIX C**

**PROPOSED PLANS**



Proposed Basement Layout



No.	Date	Amendment	Initials
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Client : Ms L Clarke  
 Project : 34 Queen's Grove  
 London  
 NW8 6HN

Drawing : Proposed Basement Layout

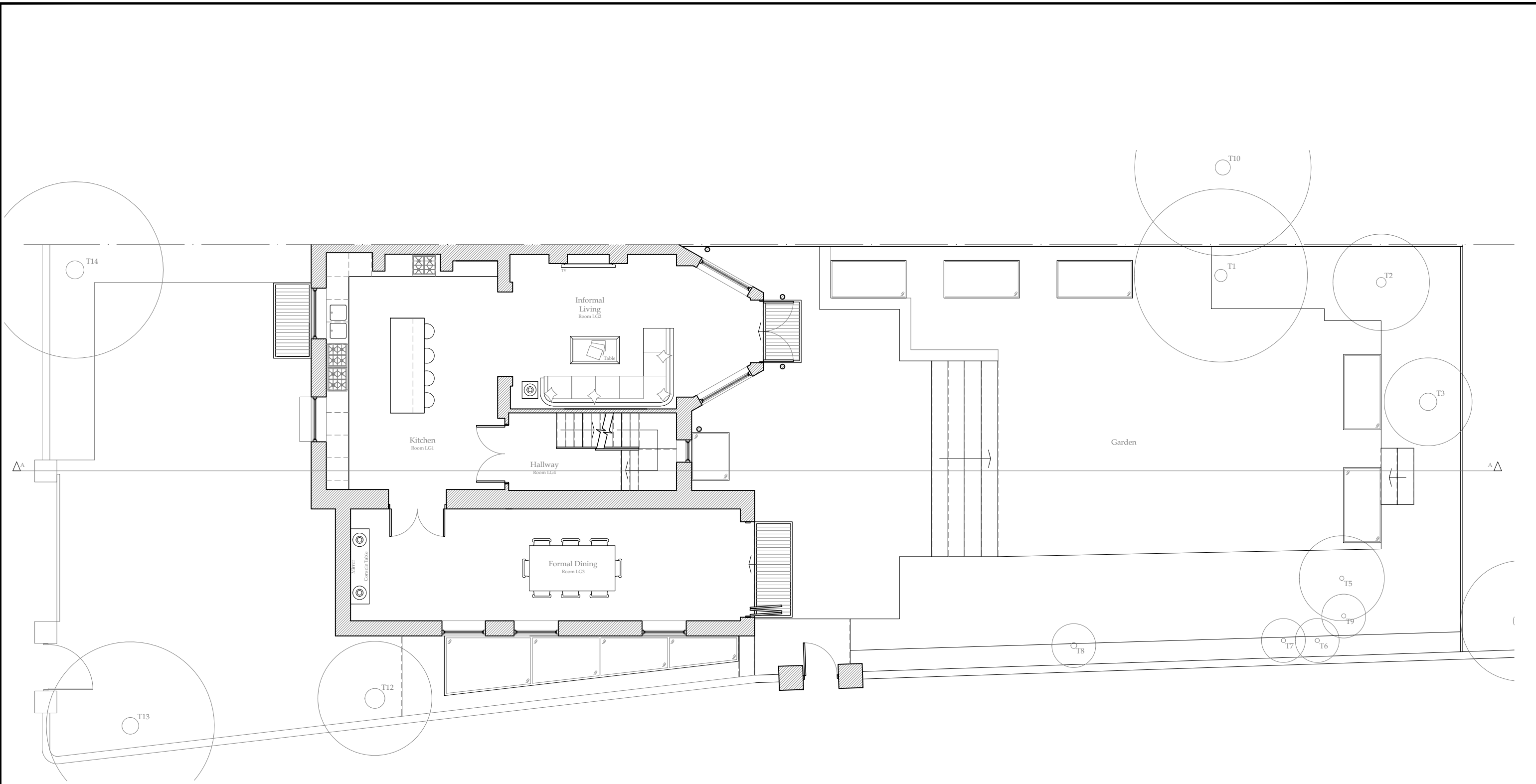
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 Dwg No : 2238-200



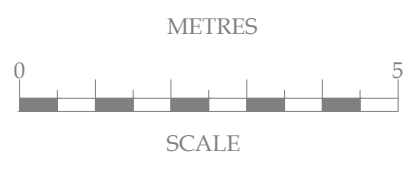
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Proposed Lower Ground Floor Layout



No.	Date	Amendment	Initials
<p>Client : Ms L Clarke</p> <p>Project : 34 Queen's Grove London NW8 6HN</p> <p>Drawing : Proposed Lower Ground Floor Layout</p>			
Scale :	1:100 @ A3	Status : DESIGN	Rev :
Date :	07 Jan 15	Dwg No : 2238-201	

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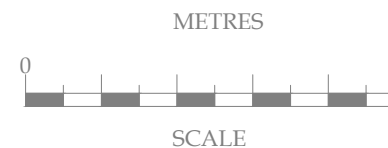




Existing Front Elevation  
(As proposed)



Existing Rear Elevation  
(As Proposed)



No.	Date	Amendment	Initials
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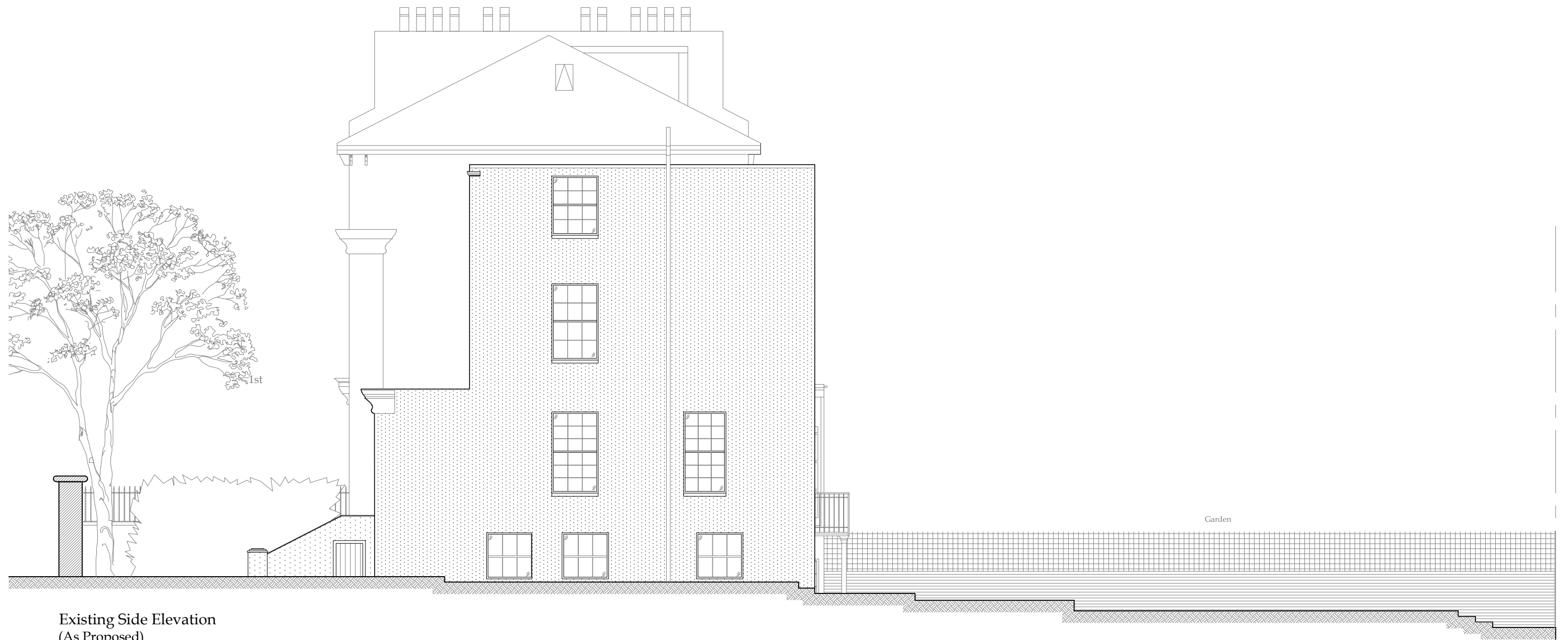
Client : Ms L Clarke  
 Project : 34 Queen's Grove  
 London  
 NW8 6HN



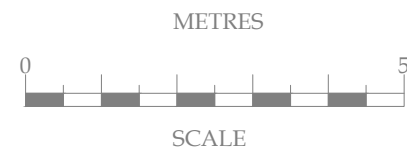
Drawing : Proposed Front & Rear Elevations  
 Scale : 1:100 @ A3  
 Date : 29 Jan 15

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Existing Side Elevation  
(As Proposed)



No.	Date	Amendment	Initials
<p>Client : Ms L Clarke</p> <p>Project : 34 Queen's Grove London NW8 6HN</p> <p>Drawing : Proposed Side Elevation</p>			
<p>Scale : 1:100 @ A3</p>		<p>Status : DESIGN</p>	<p>Rev :</p>
<p>Date : 29 Jan 15</p>		<p>Dwg No : 2238-203</p>	 <p>Cranbrook Basements 26-28 Hammersmith Grove, Hammersmith, London, W7 7BA T +44 (0)208 551 5555 F +44 (0)208 551 1580 admin@cranbrook.co.uk www.cranbrook.co.uk</p> 
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No.	Date	Amendment	Initials
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Client : Ms L Clarke  
 Project : 34 Queen's Grove  
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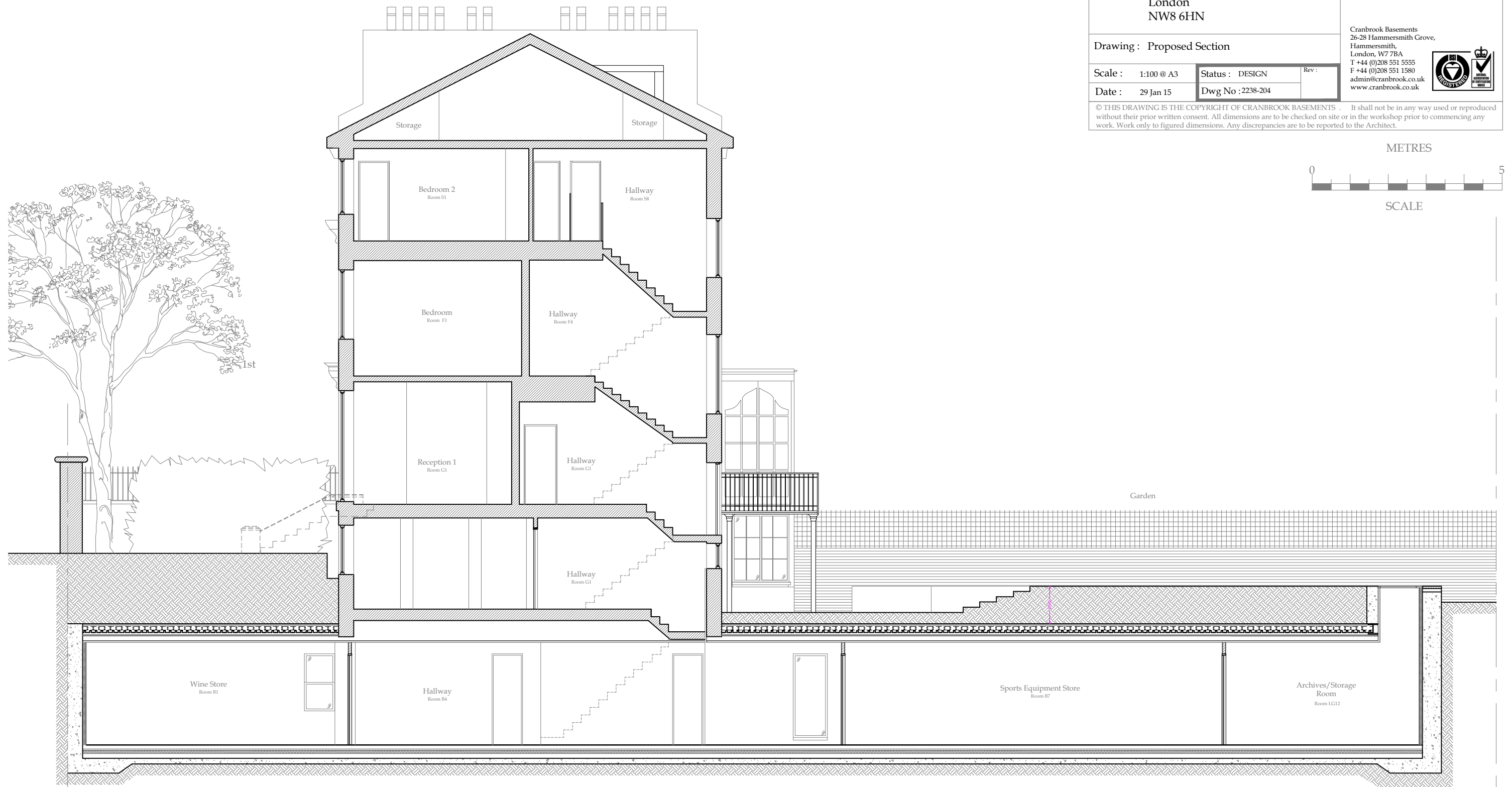
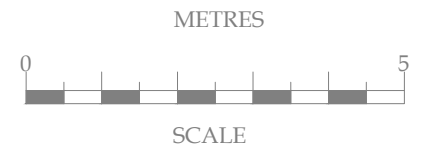
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Drawing : Proposed Section

Scale : 1:100 @ A3    Status : DESIGN    Rev :  
 Date : 29 Jan 15    Dwg No : 2238-204

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Proposed Section A-A