North	0.9x	0.77	1 × [	0.36	] x [	24.19	Т×Г	0.63	×	0.7	T≃É	5.32	(74)
North	0.9x	0.77	×	0.8	1 x [	24.19	ī x [	0.63	×	0.7	i - F	11.83	(74)
North	0.9x	0.77	×	0.64	i x i	24.19	1 x [	0.63	i x F	0.7	<b>≒</b> - F	9.46	(74)
North	0.9x	0.77	×	14.11	T x	24.19	x	0.63	x	0.7	i e i	104.31	(74)
North	0.9x	0.77	x	1.61	×	13.12	×	0.63	×	0.7	<b>∃</b>	6.45	(74)
North	0.9x	0.77	ī x Ī	0.36	ī * [	13.12	ī × Ē	0.63	7 x [	0.7	i ₌ i	2.89	(74)
North	0.9x	0.77	x	0.8	T x [	13.12	x	0.63	x	0.7	=	6.41	(74)
North	0.9x	0.77	×	0.64	T x	13.12	×	0.63	x	0.7		5.13	(74)
North	0.9x	0.77	х	14.11	x	13.12	×	0.63	x	0.7	T = [	56.57	(74)
North	0.9x	0.77	] x [	1.61	] x	8.86	] x [	0.63	x	0.7	] = [	4.36	(74)
North	0.9x	0.77	x	0.36	x	8.86	×	0.63	×	0.7	= [	1.95	(74)
North	0.9x	0.77	х	0.8	x	8.86	×	0.63	x	0.7	] = [	4.33	(74)
North	0.9x	0.77	x [	0.64	x	8.86	x	0.63	x	0.7	] = [	3.47	(74)
North	0.9x	0.77	x [	14,11	×	8.86	x [	0.63	x	0.7	] = [	38.23	(74)
South	0.9x	0.77	×	1.61	x	46.75	x [	0.63	x	0.7	] = [	23	(78)
South	0.9x	0.77	х	8.72	х	46.75	x	0.63	x	0.7	= [	124.59	(78)
South	0.9x	0.77	х	30.79	х	46.75	x	0.63	x	0.7	] = [	439.93	(78)
South	0.9x	0.77	X	3.97	*	46.75	x	0.63	X	0.7	=	56.72	(78)
South	0.9x	0.77	x	2,66	х	46.75	x	0.63	X	0.7	1=	38.01	(78)
South	0.9x	0.77	х	6.08	x	46.75	x	0.63	х	0.7	] = [	86.87	(78)
South	0.9x	0.77	×	8.39	х	46.75	x	0.63	X	0.7		119.88	(78)
South	0.9x	0.77	x	0.25	x	46.75	x	0.63	Х	0.7	] = [	3.57	(78)
South	0.9x	0.77	x	0.64	x	46.75	x	0.63	х	0.7	= [	18.29	(78)
South	0.9x	0.77	х	0.72	x	46.75	×	0.63	X	0.7	=	10.29	(78)
South	0.9x	0.77	×	1.61	×	76.57	x	0.63	X	0.7	= [	37.67	(78)
South	0.9x	0.77	Х	8.72	х	76.57	X	0.63	X	0.7	/=/	204.05	(78)
South	0.9x	0.77	х.	30.79	x	76.57	X	0.63	Х	0.7		720.49	(78)
South	0.9x	0.77	х	3.97	х	76.57	×	0.63	х	0.7	-	92.9	(78)
South	0.9x	0.77	Х	2.66	X	76.57	Х	0.63	Х	0.7	=	62.24	(78)
South	0.9x	0.77	Х	6.08	X	76.57	Х	0,63	X	0.7	= _	142.27	(78)
South	0.9x	0.77	х	8.39	х	76.57	х	0.63	х	0.7	=	196.33	(78)
South	0.9x	0.77	×	0.25	×	76.57	×	0.63	X	0.7	=	5.85	(78)
South	0.9x	0.77	х	0.64	х	76.57	×	0.63	X	0.7	_ = _	29.95	(78)
South	0.9x	0.77	x	0.72	x	76.57	×	0.63	x	0.7	=	16.85	(78)
South	0.9x	0.77	х	1.61	х	97.53	х	0.63	х	0.7	= _	47.99	(78)
South	0.9x	0.77	×	8.72	×	97.53	×	0.63	×	0.7	= 1	259.92	(78)
South	0.9x	0.77	х	30.79	x	97.53	_ x _	0.63	х	0.7	_ * _	917.78	(78)
South	0.9x	0.77	х	3.97	_ x [	97.53	×	0.63	x	0.7	= _	118.34	(78)
South	0.9x	0.77	х	2.66	x	97.53	x	0.63	x	0.7		79.29	(78)
South	0.9x	0.77	×	6.08	_	97.53	_ x	0.63	×	0.7	=	181.23	(78)
South	0.9x	0.77	X.	8.39	Х	97.53	X	0.63	X	0.7	=	250.09	(78)

South	0.9x	0.77	1 × [	0.25	1 × [	97.53	] × [	0.63	x	0.7	7 - [	7.45	(78)
South	0.9x	0.77	x	0.64	x	97.53	×	0.63	х	0.7	<b>7</b> = [	38.15	(78)
South	0.9x	0.77	×	0.72	ī x Ī	97.53	x	0.63	x	0.7	ī = Ē	21.46	(78)
South	0.9x	0.77	×	1.61	×	110.23	x	0.63	×	0.7	ī - [	54.24	(78)
South	0.9x	0.77	] x [	8.72	] × [	110.23	×	0.63	х	0.7	] = [	293.77	(78)
South	0.9x	0.77	х [	30.79	] x [	110.23	×	0.63	x	0.7	=	1037.29	(78)
South	0.9x	0.77	х	3.97	x [	110.23	x	0.63	x	0.7	=	133.75	(78)
South	0.9x	0.77	×	2.66	] x [	110.23	x	0.63	×	0.7	=	89.61	(78)
South	0.9x	0.77	_ x [	6.08	x	110.23	x	0.63	х	0.7	= [	204.83	(78)
South	0.9x	0.77	x	8.39	_ x [	110.23	x	0.63	x	0.7	=	282.65	(78)
South	0.9x	0.77	х	0.25	х	110.23	x	0.63	х	0.7	=	8.42	(78)
South	0.9x	0.77	х	0.64	х	110.23	X	0.63	х	0.7	=	43.12	(78)
South	0.9x	0.77	х	0.72	x	110.23	x	0.63	х	0.7	=	24.26	(78)
South	0.9x	0.77	х	1.61	X	114.87	x	0.63	X	0.7	( = )	56.52	(78)
South	0.9x	0.77	_ x	8.72	x	114.87	x	0.63	х	0.7	-	306.13	(78)
South	0.9x	0.77	х	30.79	* [	114.87	×	0.63	х	0.7	5	1080.92	(78)
South	0.9x	0.77	x	3.97	×	114.87	×	0.63	x	0.7	= [	139.37	(78)
South	0.9x	0.77	х	2.66	x	114.87	x	0.63	х	0.7	=	93.38	(78)
South	0.9x	0.77	х	6.08	x	114.87	x	0,63	х	0.7	=	213.45	(78)
South	0.9x	0.77	×	8.39	×	114.87	_ x [	0.63	x	0.7	] = [	294.54	(78)
South	0.9x	0.77	X	0.25	×	114.87	х	0.63	х	0.7	=	8.78	(78)
South	0.9x	0.77	х	0.64	x [	114.87	х	0.63	х	0.7	= [	44.94	(78)
South	0.9x	0.77	×	0.72	x	114.87	х	0.63	х	0.7	=	25.28	(78)
South	0.9x	0.77	х	1.61	×	110.55	×	0.63	х	0.7	=	54.39	(78)
South	0.9x	0.77	x	8.72	х	110.55	х	0.63	Х	0.7	=	294.6	(78)
South	0.9x	0.77	х	30.79	x	110.55	X	0.63	х	0.7	=	1040.24	(78)
South	0.9x	0.77	Х	3.97	x	110.55	х	0.63	х	0.7	=	134.13	(78)
South	0.9x	0.77	х	2.66	×	110.55	×	0.63	х	0.7	=	89.87	(78)
South	0.9x	0.77	Х	6.08	x	110.55	X	0.63	x	0.7	=	205.41	(78)
South	0.9x	0.77	×	8,39	×	110.55	×	0.63	Х	0.7	(5)	283.45	(78)
South	0.9x	0.77	x	0.25	x	110.55	×	0.63	х	0.7	_ = _	8.45	(78)
South	0.9x	0.77	×	0.64	х	110.55	×	0.63	х	0.7	=	43.24	(78)
South	0.9x	0.77	х	0.72	x	110.55	x	0.63	х	0.7	<u> </u>	24.33	(78)
South	0.9x	0.77	×	1.61	x	108.01	x	0.63	Х	0.7	= _	53.15	(78)
South	0.9x	0.77	×	8.72	х	108.01	×	0,63	х	0.7	_ = _	287.85	(78)
South	0.9x	0.77	Х	30.79	×	108.01	X	0.63	х	0.7		1016.37	(78)
South	0.9x	0.77	×	3.97	] × [	108.01	x	0.63	x	0.7	<u> </u>	131.05	(78)
South	0.9x	0.77	Х	2.66	×	108.01	x	0.63	×	0.7	_ = _	87.81	(78)
South	0.9x	0.77	×	6.08	×	108.01	_ × _	0.63	х	0.7	_ =	200.7	(78)
South	0.9x	0.77	×	8.39	×	108.01	×	0.63	×	0.7		276.95	(78)
South	0.9x	0.77	×	0.25	×	108.01	X	0.63	×	0.7	=	8.25	(78)

South	0.9x	0.77	] × [	0.64	1 × [	108.01	x	0.63	ТхГ	0.7	] = [	42.25	(78)
South	0.9x	0.77	×	0.72	ī x [	108.01	x	0.63	x	0.7	=	23.77	(78)
South	0.9x	0.77	×	1.61	ī * [	104.89	x	0.63	x	0.7	=	51.61	(78)
South	0.9x	0.77	x	8.72	ī x Ī	104.89	х	0.63	x	0.7	=	279.54	(78)
South	0.9x	0.77	×	30.79	ī x Ē	104.89	×	0.63	x	0.7	<b>1</b> = [	987.04	(78)
South	0.9x	0.77	×	3.97	ī x Ī	104.89	×	0.63	х	0.7	<b>7</b> = [	127.27	(78)
South	0.9x	0.77	x	2.66	×	104.89	x	0.63	x	0.7	7 = [	85.27	(78)
South	0.9x	0.77	x	6.08	] x [	104.89	x	0.63	x	0.7	] = [	194.91	(78)
South	0.9x	0.77	x	8.39	] x [	104.89	x	0.63	х	0.7	=	268.96	(78)
South	0.9x	0.77	_ x [	0.25	] x [	104.89	x	0.63	х	0.7	] = [	8.01	(78)
South	0.9x	0.77	×	0.64	] × [	104.89	×	0.63	×	0.7	= [	41.03	(78)
South	0.9x	0.77	] x [	0.72	_ x [	104.89	x	0.63	х	0.7	= [	23.08	(78)
South	0.9x	0.77	×	1.61	×	101.89	х	0.63	х	0.7	=	50.13	(78)
South	0.9x	0.77	x	8.72	] x [	101.89	х	0.63	X	0.7	=	271.52	(78)
South	0.9x	0.77	x	30.79	x [	101.89	х	0.63	х	0.7	=	958.73	(78)
South	0.9x	0.77	_ x	3.97	×	101.89	х	0.63	х	0.7		123.62	(78)
South	0.9x	0.77	х	2.66	×	101.89	х	0.63	Х	0.7	=	82.83	(78)
South	0.9x	0.77	x	6.08	] x [	101.89	x	0.63	X	0.7	= [	189.32	(78)
South	0,9x	0.77	х	8.39	_ x	101.89	X	0.63	X	0.7	=	261.24	(78)
South	0.9x	0.77	_ x [	0.25	] × [	101.89	X	0.63	x	0.7	=	7.78	(78)
South	0.9x	0.77	×	0.64	×	101.89	×	0.63	х	0.7	=	39.86	(78)
South	0.9x	0.77	×	0.72	×	101.89	х	0.63	X	0.7	= [	22.42	(78)
South	0.9x	0.77	×	1.61	×	82.59	х	0.63	х	0.7	=	40.64	(78)
South	0.9x	0.77	х	8.72	×	82.59	х	0,63	х	0.7	=	220.09	(78)
South	0.9x	0.77	×	30.79	х	82.59	х	0.63	х	0.7	=	777.12	(78)
South	0.9x	0.77	х	3.97	х	82.59	х	0.63	X	0.7	=	100.2	(78)
South	0.9x	0.77	×	2.66	х	82.59	×	0.63	х	0.7	-	67.14	(78)
South	0.9x	0.77	×	6.08	×	82.59	x	0.63	X	0.7	] = [	153.45	(78)
South	0.9x	0.77	×	8.39	х	82.59	х	0.63	Х	0.7	-	211.76	(78)
South	0.9x	0.77	×	0.25	×	82.59	X	0.63	X	0.7	=	6.31	(78)
South	0.9x	0.77	X	0.64	х	82.59	X	0.63	х	0.7	=	32.31	(78)
South	0.9x	0.77	x	0.72	×	82.59	×	0.63	x	0.7	_ = _	18.17	(78)
South	0.9x	0.77	х	1.61	×	55.42	X	0.63	Х	0.7	= _	27.27	(78)
South	0.9x	0.77	X	8.72	×	55.42	×	0.63	X	0.7	=	147.68	(78)
South	0.9x	0.77	х	30,79	×	55.42	X	0.63	х	0.7	-	521.47	(78)
South	0.9x	0.77	х	3.97	] ×	55.42	x	0.63	x	0.7	=	67.24	(78)
South	0.9x	0.77	×	2.66	ı × L	55.42	×	0.63	Х	0.7		45.05	(78)
South	0.9x	0.77	×	6.08	] * [	55.42	×	0.63	x	0.7		102.97	(78)
South	0.9x	0.77	×	8.39	Ţ×Ĺ	55.42	×	0.63	х	0.7	=	142.09	(78)
South	0.9x	0.77	×	0.25	] × [	55.42	X	0.63	X	0.7	=	4.23	(78)
South	0.9x	0.77	Х	0.64	×	55.42	Х	0.63	X	0.7	=	21.68	(78)

South	0.9x	0.77	] × [	0.72	] × [	55.42	×	0.63	] * [	0.7	] = [	12.19	(78)
South	0.9x	0.77	×	1,61	x	40.4	x	0.63	х	0.7	= [	19.88	(78)
South	0.9x	0.77	x	8.72	T x [	40.4	×	0.63	x	0.7	Ħ₌Ĕ	107.66	(78)
South	0.9x	0.77	x	30.79	ī x Ī	40.4	x	0.63	×	0.7	<b>1</b> = [	380.14	(78)
South	0.9x	0.77	×	3.97	ī x Ī	40.4	x	0.63	x	0.7	<b>-</b> [	49.01	(78)
South	0.9x	0.77	×	2.66	×	40.4	] x [	0.63	x	0.7	ī - Ē	32.84	(78)
South	0.9x	0.77	x	6.08	] x [	40.4	×	0.63	x	0.7	] = [	75.06	(78)
South	0.9x	0.77	х	8.39	] x [	40.4	×	0.63	х	0.7	= [	103.58	(78)
South	0.9x	0.77	х	0.25	×	40.4	х	0.63	X	0.7	] = [	3.09	(78)
South	0.9x	0.77	x	0.64	] × [	40.4	_ x [	0.63	x	0.7	] = [	15.8	(78)
South	0.9x	0.77	x	0.72	] × [	40.4	×	0.63	X	0.7	= [	8.89	(78)
West	0.9x	0.77	х	8.18	_ x [	19.64	х	0.63	х	0.7	] = [	49.1	(80)
West	0.9x	0.77	х	9.63	х	19.64	×	0.63	X	0.7	=	57.8	(80)
West	0.9x	0.77	x	11.5	×	19.64	×	0.63	х	0.7	=	69.03	(80)
West	0.9x	0.77	x	5.75	х	19.64	х	0.63	X	0.7	] = [	34.51	(80)
West	0.9x	0.77	х	5.7	×	19.64	х	0.63	X	0.7	=	34.21	(80)
West	0.9x	0.77	×	2,45	х	19.64	×	0.63	x	0.7	=	14.71	(80)
West	0.9x	0.77	х	9.52	×	19.64	×	0.63	x	0.7	] = [	57.14	(80)
West	0.9x	0.77	x	10.42	x	19.64	×	0.63	×	0.7	] = [	62.54	(80)
West	0.9x	0.77	x	11.33	×	19.64	×	0.63	x	0.7	] = [	68.01	(80)
West	0.9x	0.77	х	2.8	х	19.64	Х	0.63	х	0.7	= [	16.81	(80)
West	0.9x	0.77	×	8,18	] x	38.42	×	0.63	X.	0.7	] = [	96.05	(80)
West	0.9x	0.77	х	9.63	_ x	38.42	x	0.63	х	0.7	] = [	113.07	(80)
West	0.9x	0.77	×	11.5	×	38.42	×	0.63	X	0.7	=	135.03	(80)
West	0.9x	0.77	x	5.75	х	38.42	x	0.63	X	0,7	] = [	67.52	(80)
West	0.9x	0.77	×	5.7	×	38.42	х	0.63	X	0.7	=	66.93	(80)
West	0.9x	0.77	Х	2.45	х	38.42	x	0.63	Х	0.7		28.77	(80)
West	0.9x	0.77	х	9.52	х	38.42	×	0.63	х	0.7	=	111.78	(80)
West	0.9x	0.77	х	10.42	×	38.42	×	0.63	х	0.7	F .	122.35	(80)
West	0.9x	0.77	х	11.33	х	38.42	х	0.63	х	0.7	=	133.03	(80)
West	0.9x	0.77	х	2.8	х	38.42	×	0.63	Х	0.7	_ = L	32.88	(80)
West	0.9x	0.77	х	8.18	х	63.27	х	0.63	х	0.7	_ = _	158.18	(80)
West	0.9x	0.77	x	9.63	×	63.27	×	0.63	X	0.7	_] = [_	186.22	(80)
West	0.9x	0.77	Х	11.5	×	63.27	х	0.63	х	0.7	_ = _	222.38	(80)
West	0.9x	0.77	х	5.75	×	63.27	x	0.63	X	0.7	=	111.19	(80)
West	0.9x	0.77	Х	5.7	х	63.27	×	0.63	X.	0.7		110.22	(80)
West	0.9x	0.77	х	2.45	х	63.27	х	0.63	x	0.7	=	47.38	(80)
West	0.9x	0.77	х	9.52	х	63.27	x	0.63	Х	0.7	= _	184.09	(80)
West	0.9x	0.77	х	10.42	×	63.27	х	0.63	X	0.7		201.49	(80)
West	0.9x	0.77	×	11.33	×	63.27	x	0.63	х	0.7	] = [	219.09	(80)
West	0.9x	0.77	×	2,8	×	63.27	X	0.63	x	0.7	=	54.14	(80)

West	0.9x	0.77	x	8.18	×	92.28	1 × F	0.63	TxT	0.7	7 - [	230.69	(80)
West	0.9x	0.77	×	9.63	×	92.28	x	0.63	] x	0.7	Ī = Ī	271.59	(80)
West	0.9x	0.77	ī × Ī	11.5	T x	92.28	×	0.63	×	0.7	i - i	324.32	(80)
West	0.9x	0.77	×	5.75	x	92.28	×	0.63	x	0.7	T = [	162,16	(80)
West	0.9x	0.77	×	5.7	×	92.28	×	0.63	×	0.7	= [	160.75	(80)
West	0.9x	0.77	x	2.45	×	92.28	×	0.63	T x	0.7	ī - [	69.09	(80)
West	0.9x	0.77	x	9.52	×	92.28	x	0.63	x	0.7	=	268.48	(80)
West	0.9x	0.77	×	10.42	×	92.28	x	0.63	x	0.7	ī - Ī	293.86	(80)
West	0.9x	0.77	x	11.33	x	92.28	x	0.63	x	0.7	] = [	319.53	(80)
West	0.9x	0.77	x [	2.8	×	92.28	x	0.63	x	0.7	] = [	78.97	(80)
West	0.9x	0.77	x	8.18	×	113.09	×	0.63	x	0.7	= [	282.72	(80)
West	0.9x	0.77	x	9.63	х	113.09	х	0.63	x	0.7	=	332.84	(80)
West	0.9x	0.77	x	11.5	×	113.09	х	0.63	х	0.7	=	397.47	(80)
West	0.9x	0.77	x	5.75	×	113.09	х	0.63	x	0.7	] = [	198.73	(80)
West	0.9x	0.77	] x [	5.7	x	113.09	×	0.63	x	0.7	= [	197.01	(80)
West	0.9x	0.77	x	2.45	×	113.09	×	0.63	x.	0.7	=	84.68	(80)
West	0.9x	0.77	x [	9.52	X.	113.09	x	0.63	x	0.7	] = [	329.04	(80)
West	0.9x	0.77	х	10.42	x	113.09	x	0.63	x	0.7		360.14	(80)
West	0.9x	0.77	х [	11.33	×	113.09	x	0.63	x	0.7	=	391.59	(80)
West	0.9x	0.77	х	2,8	X	113.09	x	0.63	x	0.7	= [	96.78	(80)
West	0.9x	0.77	x [	8.18	×	115.77	x	0.63	x	0.7	] = [	289.42	(80)
West	0.9x	0.77	x [	9.63	×	115.77	×	0.63	x	0.7	] = [	340.72	(80)
West	0.9x	0.77	x	11.5	х	115.77	х	0.63	x	0.7	] = [	406.88	(80)
West	0.9x	0.77	x	5.75	×	115.77	х	0.63	x	0.7	= [	203.44	(80)
West	0.9x	0.77	х [	5.7	×	115.77	x	0.63	×	0.7	] = [	201.67	(80)
West	0.9x	0.77	Х	2.45	х	115.77	х	0.63	х	0.7	= [	86.68	(80)
West	0.9x	0.77	x	9.52	:X'	115.77	×	0.63	х	0.7	=	336.83	(80)
West	0,9x	0.77	х	10.42	X	115.77	х	0.63	х	0.7	= [	368.67	(80)
West	0.9x	0.77	x	11,33	x	115.77	×	0.63	x	0.7	= [	400.87	(80)
West	0.9x	0.77	×	2.8	X	115.77	x	0.63	x	0.7		99.07	(80)
West	0.9x	0.77	х	8.18	x	110.22	х	0.63	x	0.7	= [	275.54	(80)
West	0.9x	0.77	x	9.63	×	110.22	х	0.63	x	0.7	= [	324.38	(80)
West	0.9x	0.77	х	11.5	x	110.22	x	0.63	x	0.7	= [	387.37	(80)
West	0.9x	0.77	х	5,75	х	110.22	х	0.63	x	0.7	=	193.68	(80)
West	0.9x	0.77	х	5.7	X	110.22	х	0.63	х	0.7	=	192	(80)
West	.0.9x	0.77	x [	2.45	X	110.22	×	0.63	x	0.7		82.53	(80)
West	0.9x	0.77	х	9.52	x	110.22	×	0.63	x	0.7	=	320.67	(80)
West	0.9x	0.77	×	10.42	x	110.22	x	0.63	x	0.7	=	350.99	(80)
West	0.9x	0.77	x [	11.33	X	110.22	x	0.63	x	0.7	= [	381.64	(80)
West	0.9x	0.77	x	2.8	x	110.22	x	0.63	x	0.7	=	94.32	(80)
West	0,9x	0.77	X	8.18	х	94.68	x	0.63	×	0.7	II je d	236.68	(80)

West	0.9x	0.77	x	9.63	] x [	94.68	x	0.63	x	0.7	Ja[	278.64	(80)
West	0.9x	0.77	×	11.5	T x [	94.68	×	0.63	x	0.7	=	332.74	(80)
West	0.9x	0.77	×	5.75	] × [	94.68	x	0.63	x	0.7	= [	166.37	(80)
West	0.9x	0.77	×	5.7	] x [	94.68	×	0.63	х	0.7	] = [	164.92	(80)
West	0.9x	0.77	x	2.45	] × [	94.68	x	0.63	×	0.7	=	70.89	(80)
West	0.9x	0.77	x	9.52	] x [	94.68	×	0.63	x	0.7	= [	275.45	(80)
West	0.9x	0.77	×	10.42	×	94.68	x	0.63	x	0.7	=	301.49	(80)
West	0.9x	0.77	×	11.33	] × [	94.68	x	0,63	×	0.7	] = [	327.82	(80)
West	0.9x	0.77	х	2.8	×	94.68	x	0.63	x	0.7	] = [	81.02	(80)
West	0.9x	0.77	×	8.18	× [	73.59	_ x [	0.63	x	0.7	= [	183.97	(80)
West	0.9x	0.77	х	9.63	_ x [	73,59	x	0.63	х	0.7	=	216.58	(80)
West	0.9x	0.77	×	11.5	× [	73,59	х	0.63	x	0.7	=	258.63	(80)
West	0.9x	0.77	×	5.75	х	73.59	_ x [	0.63	х	0.7	] = [	129.32	(80)
West	0.9x	0.77	×	5.7	] × [	73.59	×	0.63	x	0.7	=	128.19	(80)
West	0.9x	0.77	х	2.45	×	73,59	х	0.63	х	0.7	=	55.1	(80)
West	0.9x	0.77	х	9.52	×	73.59	x	0.63	х	0.7	=	214.1	(80)
West	0.9x	0.77	х	10.42	] × [	73.59	χ	0.63	х	0.7	=	234.34	(80)
West	0.9x	0.77	Х	11.33	Х	73.59	х	0.63	х	0.7	=	254.81	(80)
West	0.9x	0.77	х	2.8	x	73,59	х	0.63	х	0.7	8	62.97	(80)
West	0.9x	0.77	х	8.18	×	45.59	х	0.63	х	0.7	=	113.97	(80)
West	0.9x	0.77	х	9.63	x [	45.59	×	0.63	x	0.7	=	134.17	(80)
West	0.9x	0.77	х	11.5	×	45.59	х	0.63	х	0.7	=	160.23	(80)
West	0.9x	0.77	х	5.75	×	45,59	x	0.63	x	0.7	] = [	80.11	(80)
West	0.9x	0.77	х	5.7	×	45.59	x	0.63	x	0.7		79.42	(80)
West	0.9x	0.77	х	2.45	x [	45.59	х	0.63	х	0.7	=	34.13	(80)
West	0.9x	0.77	x	9.52	] x [	45.59	х	0.63	x	0.7	=	132.64	(80)
West	0.9x	0.77	х	10.42	×	45,59	×	0.63	x	0.7	=	145.18	(80)
West	0.9x	0.77	×	11.33	] × [	45.59	x	0.63	х	0.7	= [	157.86	(80)
West	0.9x	0.77	×	2.8	×	45.59	х	0.63	x	0.7	=	39.01	(80)
West	0.9x	0.77	x	8.18	x	24.49	х	0.63	x	0.7	] = [	61.22	(80)
West	0.9x	0.77	х	9,63	×	24.49	Х	0.63	х	0.7	=	72.07	(80)
West	0.9x	0.77	х	11.5	×	24.49	×	0.63	x	0.7	=	86.07	(80)
West	0.9x	0.77	х	5.75	×	24.49	x	0.63	х	0.7	=	43.03	(80)
West	0.9x	0.77	х	5.7	×	24,49	х	0.63	х	0.7	=	42.66	(80)
West	0.9x	0.77	х	2.45	×	24.49	X	0.63	x	0.7	=	18.34	(80)
West	0.9x	0.77	х	9.52	-x:	24.49	Х	0.63	x	0.7	=	71.25	(80)
West	0.9x	0.77	×	10.42	×	24.49	_ x [	0.63	x	0.7	=	77.99	(80)
West	0.9x	0.77	х	11.33	×	24.49	×	0.63	×	0.7	=	84.8	(80)
West	0.9x	0.77	×	2.8	_ × [	24,49	×	0.63	x	0.7	_ = [	20.96	(80)
West	0.9x	0.77	×	8.18	x [	16,15	х	0.63	×	0.7	= [	40.38	(80)
West	0.9x	0.77	×	9.63	×	16.15	х	0.63	x	0.7	=	47.53	(80)

West 0.9x	0.77	× [	11.5	] x [	16.15	×	0.63	] x [	0.7	18	56.76	(80)
West 0.9x	0.77	×	5,75	×	16.15	х	0.63	x	0.7	=	28.38	(80)
West 0.9x	0.77	×	5.7	] x [	16.15	x	0.63	x	0.7	] = [	28.14	(80)
West 0.9x	0.77	x	2.45	x	16.15	х	0.63	х	0.7	=	12.09	(80)
West 0.9x	0.77	×	9.52	×	16.15	×	0.63	x	0.7	=	46.99	(80)
West 0.9x	0.77	×	10.42	x	16.15	×	0.63	x	0.7		51.43	(80)
West 0.9x	0.77	×	11.33	x	16.15	x	0.63	x	0.7	=	55.93	(80)
West 0.9x	0.77	×	2.8	] x [	16.15	×	0.63	x	0.7	8	13.82	(80)
Rooflights 0.9x	1	×	21.7	×	26	х	0.63	x	0.8	] = [	255.92	(82)
Rooflights 0.9x	1	×	4.42	] x [	26	x	0.63	x	0.8	=	52.13	(82)
Rooflights 0.9x	1	x	2.38	x	26	х	0.63	x	0.8	=	28.07	(82)
Rooflights 0.9x	1	×	1.08	x	26	x	0.63	x	0.8	] = [	12.74	(82)
Rooflights 0.9x	1	x [	21.7	] x [	54	х	0.63	x	0.8		531.53	(82)
Rooflights 0.9x	1	x [	4.42	x	54	x	0.63	x	0.8	= [	108.27	(82)
Rooflights 0.9x	1	x	2.38	х	54	x	0.63	x	0.8	=	58.3	(82)
Rooflights 0.9x	1	×	1.08	] × [	54	x	0.63	x.	8.0	=	26.45	(82)
Rooflights 0.9x	_1_	×	21.7	] x [	96	x	0.63	x	0.8	= [	944.94	(82)
Rooflights 0.9x	1	x [	4.42	X	96	х	0.63	×	0.8	] = [	192.47	(82)
Rooflights 0.9x	1	×	2.38	] x [	96	х	0.63	x	0.8	=	103.64	(82)
Rooflights 0.9x	1	x	1.08	] x [	96	x	0.63	x	0.8	=	47.03	(82)
Rooflights 0.9x	1	x [	21.7	] × [	150	х	0.63	] × [	0.8	=	1476.47	(82)
Rooflights 0.9x	1	x [	4.42	] x [	150	x	0.63	x	0.8	] = [	300.74	(82)
Rooflights 0.9x	1	x [	2.38	] × [	150	х	0.63	×	8.0	] = [	161.94	(82)
Rooflights 0.9x	1	x [	1.08	] x [	150	×	0.63	x	0.8	= [	73.48	(82)
Rooflights 0.9x	1	x [	21.7	] x [	192	x	0.63	x	0.8	] = [	1889.88	(82)
Rooflights 0.9x	1	x	4.42	x	192	х	0.63	X.	0.8	] ≈ [	384.94	(82)
Rooflights 0.9x	1	×	2.38	] × [	192	×	0.63	x	8.0	] = [	207.28	(82)
Rooflights 0.9x	1	x [	1.08	] x [	192	x	0.63	x	0.8	] = [	94.06	(82)
Rooflights 0.9x	1	×	21.7	] × [	200	x.	0.63	x	0.8	] = [	1968.62	(82)
Rooflights 0.9x	1	×	4.42	] x [	200	х	0.63	x	8.0	=	400.98	(82)
Rooflights 0.9x	1	х	2.38	] × [	200	X-	0.63	х	0.8	=	215.91	(82)
Rooflights 0.9x	1	×	1.08	х	200	х	0.63	Х	0.8	=	97.98	(82)
Rooflights 0.9x	1	x	21.7	×	189	×	0.63	x	0.8	=	1860.35	(82)
Rooflights 0.9x	1	х	4.42	х	189	х	0.63	x	0.8	= [	378.93	(82)
Rooflights 0.9x	1	×	2.38	] x [	189	х	0.63	х	8.0	=	204.04	(82)
Rooflights 0.9x	1	x	1.08	× [	189	×	0.63	x	0.8	= [	92.59	(82)
Rooflights 0.9x	1	x	21.7	x	157	x.	0.63	×	0.8	=	1545.37	(82)
Rooflights 0.9x	1	×	4.42	х	157	x	0.63	×	0.8	=	314.77	(82)
Rooflights 0.9x	1	×	2,38	_ x	157	x	0.63	х	0.8	=	169.49	(82)
Rooflights 0.9x	1	x	1.08	×	157	x	0.63	x	0.8	=	76.91	(82)
Rooflights 0.9x	1	×	21.7	] x [	115	x	0.63	x	0.8	-	1131.96	(82)

	_											-	
ooflights o	.9x 1	×	4.4	12	x	115	x	0.63	x	0.8	= 1	230.56	(82
ooflights 0	.9x 1	x	2.3	38	x [	115	x	0.63	x	0.8		124.15	(82
ooflights 0	.9x 1	x	1.0	08	x T	115	x	0.63	<b>=</b> x <b>=</b>	8.0	-	56.34	(82
ooflights 0	.9x 1	x	21	.7	x F	66	x	0.63	x	0.8	ž.	649.65	(82
ooflights 0	.9x 1	×	4.4	12	×	66	×	0.63	x	0.8	-	132.32	(82
ooflights o	.9x 1	x	2.3	38	x F	66	×	0.63	×	0.8	= =	71.25	(82
ooflights o	,9x 1	x	1.0	08	x [	66	x	0.63	×	0.8		32.33	(82
ooflights o	.9x 1	×	21	.7	x T	33	i x F	0.63	x	0,8	=	324.82	(82
ooflights o	.9x 1	×	4.4	12	x T	33	x	0.63	х	0.8	-	66.16	(82
ooflights o	.9x 1	×	2.3	38	x T	33	x	0.63	x	0.8		35.63	(82
ooflights o	.9x 1	×	1,0	08	×	33	x	0.63	х	0.8	=	16.17	(82
ooflights o	.9x 1	×	21	.7	x [	21	×	0.63	х	0.8	-	206.71	(82
ooflights o	.9x 1	×	4.4	12	x [	21	×	0.63	x	0.8		42.1	(82
ooflights o	.9x 1	×	2.3	38	×	21	×	0.63	х	0.8		22.67	(82
ooflights o	.9x 1	x	1.0	08	x T	21	i x F	0.63	x	0.8	=	10.29	(82
							the same						
olar gain:	s in watts, c	calculated	for eac	h month			(83)m =	Sum(74)m .	(82)m				
3)m= 185	4.69 3374.08	5095.02	6964.21	8285.82	8410	0.25 8033.81	7038.9	1 5751.07	3867	2262.86	1559,25		(83
	s – internal		(84)m =	= (73)m	+ (83	)m , watts							
4)m= 331	6.91 4827.25	6491.53	8271.03	9496.61	9538	9115.89	8134.9	7 6900.85	5106.74	3602.62	2978.72		(84
7 Meani	nternal tem	perature	(healing	season	i)i								
Tempera	ture during	heating p	eriods ir	n the livi	ng ar	ea from Ta	ble 9, T	'h1 (°C)				21	(85
Hilipotion													
Julipation	n factor for g	gains for I	iving are	ea, h1,m	(see	Table 9a)							
	an Feb	gains for I Mar	iving are Apr	ea, h1,m May	Ju	1	Aug	Sep	Oct	Nov	Dec	]	
J					Τ .	ın Jul	Aug 0.44	Sep 0.71	Oct 0.95	Nov 1	Dec 1		(86
6)m=	an Feb 1 0.99	Mar 0.97	Apr 0.87	May 0.7	Jt 0.5	un Jul 2 0.38	0.44	0.71					(86
Ji 6)m=	an Feb	Mar 0.97	Apr 0.87	May 0.7	Jt 0.5	un Jul 2 0.38 steps 3 to	0.44	0.71					
6)m=  Mean inte 7)m= 19	an Feb 1 0.99 ernal tempe .47 19.77	Mar 0.97 rature in 20.19	Apr 0.87 living are 20.64	0.7 ea T1 (fo	0.5 ollow 20.5	un Jul 2 0.38 steps 3 to 98 21	0.44 7 in Tak 20.99	0.71 ble 9c) 20.92	0.95	1	1		
Mean inte 7)m= 19	an Feb 1 0.99 ernal tempe 1.47 19.77 ture during	Mar 0.97 rature in 20.19 heating p	Apr 0.87 living are 20.64 eriods in	0.7 ea T1 (for 20.89	Juliow 20.5	un Jul 2 0.38 steps 3 to 98 21 ling from Ta	0.44 7 in Tak 20.99 able 9,	0.71 ble 9c) 20.92 Th2 (°C)	0.95	19.87	19.42		(87
6)m=  Mean inte 7)m= 19  Temperat 8)m= 19	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81	Mar 0.97 rature in 20.19 heating p	Apr 0.87 living ard 20.64 eriods in 19.82	0.7 ea T1 (for 20.89 n rest of 19.82	Julion 20.5 dwell 19.4	un Jul 2 0.38 steps 3 to 98 21 ling from T 83 19.83	0.44 7 in Tak 20.99 able 9,	0.71 ble 9c) 20.92	0.95	1	1		(87
6)m=  Mean inte 7)m= 19  Temperat 8)m= 19	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81	Mar 0.97 rature in 20.19 heating p 19.81 gains for	Apr 0.87 living are 20.64 eriods in 19.82	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling,	Ju 0.5 ollow 20.5 dwel 19.5 h2, m	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 33 19.83 (see Table	0.44 7 in Tak 20.99 able 9, 19.83	0.71  ble 9c) 20.92  Th2 (°C) 19.83	0.95 20.49 19.82	19.87	19.42		(88
Mean inte 7)m= 19 Temperal 8)m= 19 Utilisation 9)m=	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81 n factor for (	Mar 0.97 rature in 20.19 heating p 19.81 gains for 1 0.95	Apr 0.87 living are 20.64 eriods in 19.82 rest of d	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64	Ju 0.5 ollow 20.5 dwel 19.6 h2,m 0.4	un Jul 2 0.38 steps 3 to 98 21 ling from Ti 83 19.83 (see Table 3 0.28	0.44 7 in Tab 20.99 able 9, 19.83 9a) 0.33	0.71  ble 9c) 20.92  Th2 (°C) 19.83	0.95 20.49 19.82	19.87	19.42		(88
Mean inte 7)m= 19 Temperat 8)m= 19 Utilisation 9)m=	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81 n factor for ( 1 0.99 ernal tempe	Mar 0.97 reature in 20.19 heating p 19.81 gains for r 0.95	Apr 0.87 living ard 20.64 periods in 19.82 rest of do 0.84	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64 of dwell	July 0.5 ollow 20.4 dwel 19.4 h2,m 0.4 ling T	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 83 19.83 (see Table 3 0.28 2 (follow steps	0.44 7 in Tat 20.99 able 9, 19.83 99a) 0.33 eps 3 to	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Table	0.95 20.49 19.82 0.93 e 9c)	1 19.87 19.82	19.42		(88 (89
Mean inte  Mean inte  7)m= 19  Temperal  8)m= 19  Utilisation  9)m=  Mean inte	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81 n factor for (	Mar 0.97 rature in 20.19 heating p 19.81 gains for 1 0.95	Apr 0.87 living are 20.64 eriods in 19.82 rest of d	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64	Ju 0.5 ollow 20.5 dwel 19.6 h2,m 0.4	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 83 19.83 (see Table 3 0.28 2 (follow steps	0.44 7 in Tab 20.99 able 9, 19.83 9a) 0.33	0.71 ble 9c) 20.92 Th2 (°C) 19.83  0.62 7 in Table 19.77	0.95 20.49 19.82 0.93 e 9c) 19.25	19.87 19.82 0.99	19.42		(88
Mean inte  Mean inte  7)m= 19  Temperal  8)m= 19  Utilisation  9)m=  Mean inte	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81 n factor for ( 1 0.99 ernal tempe	Mar 0.97 reature in 20.19 heating p 19.81 gains for r 0.95	Apr 0.87 living ard 20.64 periods in 19.82 rest of do 0.84	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64 of dwell	July 0.5 ollow 20.4 dwel 19.4 h2,m 0.4 ling T	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 83 19.83 (see Table 3 0.28 2 (follow steps	0.44 7 in Tat 20.99 able 9, 19.83 99a) 0.33 eps 3 to	0.71 ble 9c) 20.92 Th2 (°C) 19.83  0.62 7 in Table 19.77	0.95 20.49 19.82 0.93 e 9c) 19.25	1 19.87 19.82	19.42	0.1	(86 (87 (88 (89 (90
Mean interest in the second se	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81 n factor for ( 1 0.99 ernal tempe	Mar 0.97 rature in 20.19 heating p 19.81 gains for i 0.95 rature in 18.83	Apr 0.87 living ard 20.64 eriods in 19.82 rest of d 0.84 the rest 19.43	May 0.7 ea T1 (fd 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73	July 0.50 ollow 20.00 dwel 19.00 ollow 19.	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 83 19.83 (see Table 3 0.28 2 (follow st 82 19.83	0.44 7 in Tab 20.99 able 9, 19.83 9 9a) 0.33 eps 3 to 19.83	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Tabl 19.77	0.95 20.49 19.82 0.93 e 9c) 19.25	19.87 19.82 0.99	19.42	0.1	(88 (89 (90
Mean inter 7)m= 19 Temperal 8)m= 19 Utilisation 9)m= 17 Mean inter	an Feb 1 0.99 ernal tempe 47 19.77 ture during 81 19.81 n factor for g 1 0.99 ernal tempe 79 18.22	Mar 0.97 rature in 20.19 heating p 19.81 gains for i 0.95 rature in 18.83	Apr 0.87 living ard 20.64 eriods in 19.82 rest of d 0.84 the rest 19.43	May 0.7 ea T1 (fd 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73	July 0.50 ollow 20.00 dwel 19.00 ollow 19.	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 83 19.83 (see Table 3 0.28 2 (follow st 82 19.83	0.44 7 in Tab 20.99 able 9, 19.83 9 9a) 0.33 eps 3 to 19.83	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Tabl 19.77	0.95 20.49 19.82 0.93 e 9c) 19.25	19.87 19.82 0.99	19.42	0.1	(88 (89 (90
Mean inter 7)m= 19 Temperat 8)m= 19 Utilisation 9)m= 17 Mean inter 0)m= 17	an Feb 1 0.99 ernal tempe 1.47 19.77 ture during 1.81 19.81 n factor for g 1 0.99 ernal tempe 1.79 18.22	Mar 0.97 rature in 20.19 heating p 19.81 gains for 0.95 rature in 18.83	Apr 0.87 living ard 20.64 eriods in 19.82 rest of di 0.84 the rest 19.43	May 0.7 ea T1 (for 20.89 in rest of 19.82 in 19.73 in 19.73 in 19.73 in 19.85	July 10.5 on 1	un Jul 2 0.38 steps 3 to 98 21 ling from Ti 83 19.83 (see Table 3 0.28 2 (follow st 82 19.83 = fLA × T1 93 19.94	0.44 7 in Tak 20.99 able 9, 19.83 99a) 0.33 eps 3 to 19.83 + (1 -	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Table 19.77  fLA) × T2 19.88	0.95  20.49  19.82  0.93  e 9c)  19.25  19.37	19.87 19.82 0.99 18.37 g area + (4	1 19.42 19.82 1 17.71	0.1	(88 (89 (90
Mean inte 7)m= 19 Temperai 8)m= 19 Utilisation 9)m=	an Feb 1 0.99 ernal tempe 47 19.77 ture during 81 19.81 n factor for g 1 0.99 ernal tempe 79 18.22 ernal tempe 95 18.38	Mar 0.97 rature in 20.19 heating p 19.81 gains for 0.95 rature in 18.83	Apr 0.87 living ard 20.64 eriods in 19.82 rest of di 0.84 the rest 19.43	May 0.7 ea T1 (for 20.89 in rest of 19.82 in 19.73 in 19.73 in 19.73 in 19.85	July 10.5 on 1	Jul   2   0.38	0.44 7 in Tak 20.99 able 9, 19.83 99a) 0.33 eps 3 to 19.83 + (1 -	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Tabl 19.77  fLA) × T2 19.88  nere approximates	0.95  20.49  19.82  0.93  e 9c)  19.25  19.37	19.87 19.82 0.99 18.37 g area + (4	1 19.42 19.82 1 17.71	0.1	(88 (89 (90 (91
Mean interpretation  Apply adj  3)m= 17	an Feb 1 0.99 ernal tempe .47 19.77 ture during .81 19.81 n factor for g 1 0.99 ernal tempe .79 18.22 ernal tempe .95 18.38 ustment to	Mar 0.97  rature in 20.19 heating p 19.81 gains for i 0.95 rature in 18.83  rature (fo 18.96 the mean	Apr 0.87 living ard 20.64 eriods in 19.82 rest of d 0.84 the rest 19.43 or the wh 19.55 interna 19.55	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73 nole dwe 19.85 temper	July 0.50 of the second of the	Jul   2   0.38	0.44 7 in Tak 20.99 able 9, 19.83 99a) 0.33 eps 3 to 19.83 + (1 - 19.94 19.94	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Tabl 19.77  fLA) × T2 19.88  nere approximates	0.95  20.49  19.82  0.93  e 9c) 19.25  FLA = Livin  19.37  opriate	19.87 19.82 0.99 18.37 g area + (4	1 19.42 19.82 1 17.71 17.88	0.1	(88 (89 (90 (91
Mean interpretation  Apply adj  3)m= 17  Space  Set Ti to to	an Feb 1 0.99 ernal tempe 47 19.77 ture during 81 19.81 n factor for g 1 0.99 ernal tempe 79 18.22 ernal tempe 95 18.38 ustment to 95 18.38 heating reg the mean in	Mar 0.97  rature in 20.19 heating p 19.81 gains for in 0.95 rature in 18.83  rature (for 18.96 the mean 18.96	Apr 0.87 living ard 20.64 eriods if 19.82 rest of d 0.84 the rest 19.43 r the wh 19.55 interna 19.55	May 0.7 ea T1 (fd 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73 nole dwe 19.85 I temper 19.85	July 0.5 ollow 20 dwel 19 old	un Jul 2 0.38 steps 3 to 98 21 ling from Ta 83 19.83 (see Table 3 0.28 2 (follow st 82 19.83 = fLA × T1 93 19.94 a from Table 93 19.94	0.44 7 in Tab 20.99 able 9, 19.83 99a) 0.33 eps 3 to 19.83 + (1 - 19.94	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Table 19.77  fLA) × T2 19.88  here approximates	0.95  20.49  19.82  0.93  e 9c)  19.25  fl.A = Livin  19.37  popriate  19.37	19.87 19.82 0.99 18.37 g area + (4	1 19.42 19.82 1 17.71 1) =		(88 (89 (90 (91
Mean interest in the utilisation of the utilisation	ernal tempe 47 19.77 ture during 81 19.81 n factor for g 1 0.99 ernal tempe 79 18.22 ernal tempe 95 18.38 ustment to 95 18.38 heating rec the mean intion factor f	Mar 0.97 reture in 20.19 heating p 19.81 gains for 0.95 reture in 18.83 reture (for 18.96) the mean 18.96	Apr 0.87 living ard 20.64 eriods if 19.82 rest of do 0.84 the rest 19.43 or the who 19.55 interna 19.55	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73 nole dwe 19.85 temper 19.85 re obtain able 9a	July 19.3 July 1	Jul   2   0.38	0.44 7 in Table 9, 19.83 9 9a) 0.33 eps 3 to 19.83 + (1 - 19.94 Table 9	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Table 19.77  fLA) × T2 19.88  nere appro 19.88	0.95  20.49  19.82  0.93  e 9c)  19.25  fLA = Livin  19.37  opriate  19.37	19.87 19.82 0.99 18.37 g area + (4 18.51 18.51	1 19.42 19.82 1 17.71 1) = 17.88 17.88		(88 (89 (90 (91
Mean inter 7)m= 19 Temperar 8)m= 19 Utilisation 9)m= 17 Mean inter 0)m= 17 Apply adj 3)m= 17 Set Ti to the utilisa	ernal tempe 47 19.77 ture during 81 19.81 n factor for g 1 0.99 ernal tempe 79 18.22 ernal tempe 95 18.38 ustment to 95 18.38 heating rep tion factor f an Feb	Mar 0.97 rature in 20.19 heating p 19.81 gains for r 0.95 rature in 18.83 rature (fo 18.96 the mean 18.96 urement	Apr 0.87 living ard 20.64 eriods in 19.82 rest of d 0.84 the rest 19.43 rr the wh 19.55 interna 19.55 mperaturusing Ta	May 0.7 ea T1 (fd 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73 nole dwe 19.85 I temper 19.85	July 0.5 ollow 20 dwel 19 old	Jul   2   0.38	0.44 7 in Tab 20.99 able 9, 19.83 99a) 0.33 eps 3 to 19.83 + (1 - 19.94	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Table 19.77  fLA) × T2 19.88  nere appro 19.88	0.95  20.49  19.82  0.93  e 9c)  19.25  fl.A = Livin  19.37  popriate  19.37	19.87 19.82 0.99 18.37 g area + (4	1 19.42 19.82 1 17.71 1) =		(88 (89 (90 (91
Mean interest interes	ernal tempe 47 19.77 ture during 81 19.81 n factor for g 1 0.99 ernal tempe 79 18.22 ernal tempe 95 18.38 ustment to 95 18.38 heating rec the mean intion factor f	Mar 0.97 rature in 20.19 heating p 19.81 gains for r 0.95 rature in 18.83 rature (fo 18.96 the mean 18.96 urement	Apr 0.87 living ard 20.64 eriods in 19.82 rest of d 0.84 the rest 19.43 rr the wh 19.55 interna 19.55 mperaturusing Ta	May 0.7 ea T1 (for 20.89 n rest of 19.82 welling, 0.64 of dwell 19.73 nole dwe 19.85 temper 19.85 re obtain able 9a	July 19.3 July 1	Jul   2   0.38	0.44 7 in Table 9, 19.83 9 9a) 0.33 eps 3 to 19.83 + (1 - 19.94 Table 9	0.71  ble 9c) 20.92  Th2 (°C) 19.83  0.62  7 in Table 19.77  fLA) × T2 19.88  nere appro 19.88	0.95  20.49  19.82  0.93  e 9c)  19.25  fLA = Livin  19.37  opriate  19.37	19.87 19.82 0.99 18.37 g area + (4 18.51 18.51	1 19.42 19.82 1 17.71 1) = 17.88 17.88		(88 (89 (90

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Page 14 of 18

Usefu	al gains,	hmGm	W = (9)	4)m x (8	4)m									
(95)m=	3305.63	4752.91	6123.46	6841.79	6049.34	4149.18	2631.76	2778.09	4304.75	4694.11	3568.03	2972.17		(95)
Month	nly aver	age exte	ernal ten	nperature	e from T	able 8								
(96)m=	4.3	4.9	6.5	8.9	11.7	14.6	16.6	16.4	14.1	10.6	7.1	4.2		(96)
Heat	loss rate	for me	an interr	nal temp	erature,	Lm , W :	=[(39)m:	x [(93)m	– (96) m	]				
(97)m=	10949.77	10792.94	9966.59	8464.17	6466,05	4208.58	2638.61	2792,94	4574.12	6964.22	9082.76	10912.66		(97)
Space	e heatin	g require	ement fo	or each r	nonth, k	Wh/mon	th = 0.02	24 x [(97	)m - (95	)m] x (4	1)m			
(98)m=	5687.24	4058.9	2859.29	1168,11	310.03	0	0	0	0	1688.96	3970.61	5907.73		
								Tota	l per year	(kWh/year	r) = Sum(9	8), 5,9 12 =	25650.86	(98)
Space	e heatin	a require	ement in	kWh/m	²/vear							i	42.79	(99)
1200					A	-								
		alingre		30. 30.00	Con To	hl- 40h								
Calcu	Jan	Feb	Mar	August. Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
Heat	10.70		-	using 2										
(100)m=	0	0	0	0	0	7420.04		5992.76	0	0	0	0		(100)
	2	tor for lo				7 120.01	CONTROL	0002.70				9.		3006
(101)m=		0	0	0	0	0.93	0.96	0.94	0	0	0	0		(101)
		ml m (V	Vatts) =	(100)m>	(101)m									4.00
(102)m=		0	0	0	0	6888.77	5618.75	5632	0	0	0	0		(102)
		nains ca	lculated	for appli	icable w				10)					
(103)m=		0	0	0	0	10505.19	_	8967.71	0	0	0	0		(103)
Section 6 1		a require	ement fo	or month	whole o	dwellina.	continue	ous ( kW	(h) = 0.0	24 x [(1)	(33)m - (	102)m] x	(41)m	
				< 3 × (98						S. O. A.	,	,	( /	
(104)m=	0	0	0	0	0	2603.83	3292.46	2481.77	0	0	0	0		
						•			Total	= Sum(	104)	=	8378.05	(104)
Cooled	d fraction	1							fC=	cooled	area ÷ (4	4) =	0.67	(105)
	_	actor (Ta	able 10b	p)										
(106)m=	0	0	0	0	0	0.25	0.25	0.25	0	0	0	0		
									Total	l = Sum(	1.04)	=	0	(106)
A Company of the Comp				month =										
(107)m=	0	0	0	0	0	434.38	549.26	414.02	0	0	0	0		-
									Total	I = Sum(	107)	= [	1397.67	(107)
Space	cooling	requirer	ment in	kWh/m²/	year				(107)	) ÷ (4) =			2.33	(108)
9b En	ergy rec	uiremer	nts – Co	miniunity	healing	scheme								
This pa	art is us	ed for sp	oace hea	ating, spa	ace cool	ing or wa	ater heat	ing prov	ided by	a comm	unity sch	neme.		
Fractio	n of spa	ace heat	from se	econdary	/suppler	nentary	heating (	Table 1	1) '0' if n	one			0	(301)
Fractio	n of spa	ace heat	from co	mmunity	system	1 - (30	1) =					Ĩ	1	(302)
The con	nmunity so	heme ma	v obtain h	eat from se	everal sou	rces. The	procedure	allows for	CHP and I	up to four	other heat	sources; th	e latter	
			•	mal and w							211101321	220023411		
Fractio	n of hea	at from C	Commur	nity CHP								1	0.87	(303a)
Fractio	n of cor	nmunity	heat fro	m heat	source 2							Ì	0.13	(303b)
				m Comr						(3	02) x (303	a) = [	0.87	(304a)
							2							(304b)
riacio	וויו נטונ	ai space	neat if	m comn	idi iity me	at sould	<i>C</i> 2			(3	02) x (303	0)-	0.13	(3040)

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Factor for control and charging method (Table	1	(305)		
Distribution loss factor (Table 12c) for commun	ity heating system		1.05	(306)
Space heating			kWh/year	
Annual space heating requirement			25650.86	]
Space heat from Community CHP		$(98) \times (304a) \times (305) \times (306) =$	23432.06	(307a
Space heat from heat source 2		(98) x (304b) x (305) x (306) =	3501.34	(307b
Efficiency of secondary/supplementary heating	system in % (from Tab	ole 4a or Appendix E)	0	(308
Space heating requirement from secondary/sup	oplementary system	(98) x (301) x 100 + (308) =	0	(309)
Water heating Annual water heating requirement			2894.26	
If DHW from community scheme: Water heat from Community CHP		(64) x (303a) x (305) x (306) =	2643.91	(310a
Water heat from heat source 2		(64) x (303b) x (305) x (306) =	395.07	(310b
Electricity used for heat distribution	0.	01 × [(307a)(307e) + (310a)(310e)] =	299.72	(313)
Cooling System Energy Efficiency Ratio			4.32	(314)
Space cooling (if there is a fixed cooling system	n, if not enter 0)	= (107) + (314) =	323.53	(315)
Electricity for pumps and fans within dwelling (1 mechanical ventilation - balanced, extract or po		de	0	(330a
warm air heating system fans			0	(330b
pump for solar water heating			0	(330g
Total electricity for the above, kWh/year		=(330a) + (330b) + (330g) =	0	(331)
Energy for lighting (calculated in Appendix L)			1056.62	(332)
10b. Fuel costs - Community heating scheme				
	Fuel kWh/year	Fuel Price (Table 12)	Fuel Cost £/year	
Space heating from CHP	(307a) x	2.97 x 0.01 =	695.93	(340a
Space heating from heat source 2	(307b) x	4.24 x 0.01 =	148.46	(340b
Water heating from CHP	(310a) x	2.97 x 0.01 =	78.52	(342a
Water heating from heat source 2	(310b) x	4.24 × 0.01 =	16.75	(342b
	(315)	Fuel Price 13.19 x 0.01 =	42.67	(348)
Space cooling (community cooling system)				(349)
Space cooling (community cooling system) Pumps and fans	(331)	13.19 x 0.01 =	0	(040)
	(331) (332)	10.10		=
Pumps and fans		10.10	139.37	(350)

Energy cost deflator (Table 12)				0.42	(356)
Energy cost factor (ECF)	[(355) x (356)] + [(4) + 45	5.0] =		0.81	(357)
SAP rating (section12)				88.71	(358)
12b CO2 Emissions - Community	heating scheme				
Electrical efficiency of CHP unit				27.2	(361)
Heat efficiency of CHP unit				66.8	(362)
		Energy kWh/year	Emission factor kg CO2/kWh	or Emissions kg CO2/year	
Space heating from CHP)	(307a) × 100 + (362) =	35077.94 X	0.22	7576.83	(363)
less credit emissions for electricity	-(307a) × (361) + (362) =	9541.2 ×	0.52	-4951.88	(364)
Water heated by CHP	(310a) × 100 + (362) =	3957.94 ×	0.22	854.92	(365)
less credit emissions for electricity	-(310a) × (361) + (362) =	1076.56 ×	0.52	-558.73	(366)
Efficiency of heat source 2 (%)	If there is CHP t	using two fuels repeat (363) t	to (366) for the second	fuel 90	(367b)
CO2 associated with heat source 2	[(307	7b)+(310b)] x 100 + (367b) x	0.22	935.14	(368)
Electrical energy for heat distribution	on	[(313) x	0.52	155.56	(372)
Total CO2 associated with commun	nity systems	(363)(366) + (368)(3	72)	= 4011.83	(373)
CO2 associated with space heating	g (secondary)	(309) x	0	0	(374)
CO2 associated with water from im	mersion heater or instant	aneous heater (312) x	0.22	= 0	(375)
Total CO2 associated with space a	nd water heating	(373) + (374) + (375) =		4011.83	(376)
CO2 associated with space cooling	J	(315) x	0.52	167.91	(377)
CO2 associated with electricity for	pumps and fans within dw	velling (331)) x	0.52	= 0	(378)
CO2 associated with electricity for	lighting	(332))) x	0,52	= 548.39	(379)
Total CO2, kg/year	sum of (376)(382) =			4728.13	(383)
<b>Dwelling CO2 Emission Rat</b>	te (383) + (4) =			7.89	(384)
El rating (section 14)				90.17	(385)
13b Primary Energy - Community	heating scheme				
Electrical efficiency of CHP unit				27.2	(361)
Heat efficiency of CHP unit				66.8	(362)
		Energy kWh/year	Primary factor	P.Energy kWh/year	
Space heating from CHP)	(307a) × 100 + (362) =	35077.94 X	1.22	42795.08	(363)
less credit emissions for electricity	-(307a) × (361) + (362) =	9541.2 X	3.07	-29291.48	(364)
Water heated by CHP	(310a) × 100 + (362) =	3957.94 ×	1.22	4828.69	(365)
less credit emissions for electricity	-(310a) × (361) + (362) =	1076.56 X	3.07	-3305.04	(366)
Efficiency of heat source 2 (%)	If there is CHP to	using two fuels repeat (363) t	to (366) for the second	fuel 90	(367b
Energy associated with heat source	e 2 [(307	7b)+(310b)] x 100 + (367b) x	1.22	5281.8	(368)
	on				(372)

Total Energy associated with community systems	(363)(366) + (368)(372)		=	21229.2	(373)
if it is negative set (373) to zero (unless specified other	wise, see C7 in Appendix C)		[	21229.2	(373)
Energy associated with space heating (secondary)	(309) x	0	] = [	0	(374)
Energy associated with water from immersion heater or in	nstantaneous heater(312) x	1.22	] = [	0	(375)
Total Energy associated with space and water heating	(373) + (374) + (375) =		[	21229.2	(376)
Energy associated with space cooling	(315) x	3.07	= [	993.25	(377)
Energy associated with electricity for pumps and fans with	nin dwelling (331)) x	3.07	] = [	0	(378)
Energy associated with electricity for lighting	(332))) x	3.07	] = [	3243.82	(379)
Total Primary Energy, kWh/year	f (376)(382) =			25466.28	(383)

#### APPENDIX (vi)

#### PEA - PREDICTED ENERGY ASSESSMENT (PRE-EPC)

### **Predicted Energy Assessment**

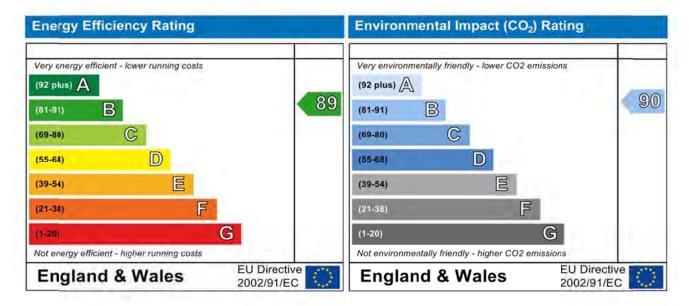


17, Branch Hill LONDON NW3 7NA Dwelling type: Date of assessment: Produced by: Total floor area:

Detached House 18 September 2014 Ondrej Gajdos 599.4 m<sup>2</sup>

This is a Predicted Energy Assessment for a property which is not yet complete. It includes a predicted energy rating which might not represent the final energy rating of the property on completion. Once the property is completed, an Energy Performance Certificate is required providing information about the energy performance of the completed property.

Energy performance has been assessed using the SAP 2012 methodology and is rated in terms of the energy use per square metre of floor area, energy efficiency based on fuel costs and environmental impact based on carbon dioxide (CO2) emissions.

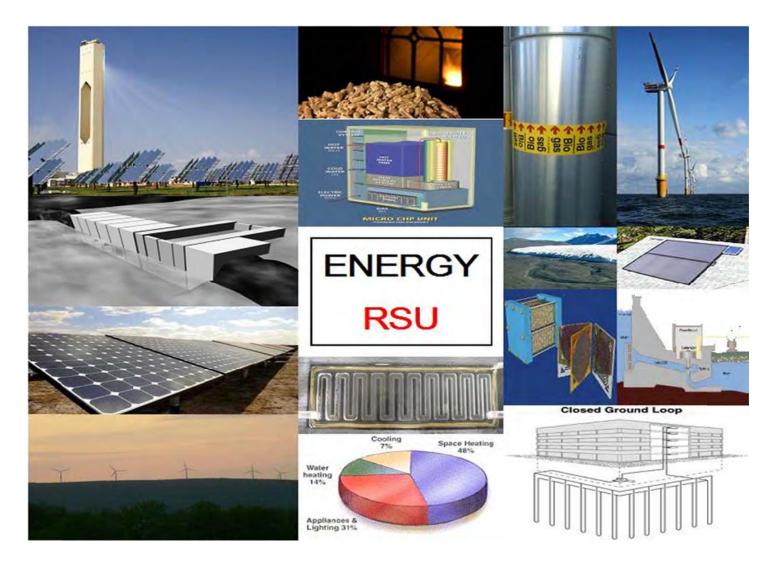


The energy efficiency rating is a measure of the overall efficiency of a home. The higher the rating the more energy efficient the home is and the lower the fuel bills are likely to be.

The environmental impact rating is a measure of a home's impact on the environment in terms of carbonn dioxide (CO2) emissions. The higher the rating the less impact it has on the environment.

#### APPENDIX (vii)

**ENERGY RSU** – RENEWABLES & SUSTAINABILITY UNIT



#### ENERGY RSU is an integrated energy sustainability unit able to provide the following:

- SAP Calculations & Certificates L1A&B New/Existing Buildings (NHER certified)
- SBEM Calculations & Certificates L2A&B New/Existing Buildings (BRE certified)
- EPC & DEC Certificates New Build (CIBSE certified)
- Rd SAP Survey EPC Certificates Existing Buildings (NHER certified)
- Commercial EPC Survey certificates Existing Buildings (BRE certified) Level 3, 4 & 5
- Energy Statements & Renewable Reports for Planning
- LEED/BREEAM assessments (USGBC/BRE certified)
- Low/Zero Carbon (LZC) and Sustainability Appraisals/designs (CIBSE Low Carbon Consultant)
- Renewable Energy Appraisals and Designs
- Carbon Rating assessments
- 2D/3D CFD and Dynamic Thermal Simulations
- EPBD Air Conditioning Inspections (Article 20) and EPBD Asset Ratings & Certificates
- Energy Usage (Running Costs)
- Utility/Bill Analysis and Recommendations
- Advice on Green and Environmental Issues Relating to M&E Building Services
- Code for Sustainable Homes New Build and Refurbishment (BRE certified)
- Solar Shading/Sun Studies













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M&E Consultants

**Energy Consultants** 



#### Section 5.0

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ME7 October 2014