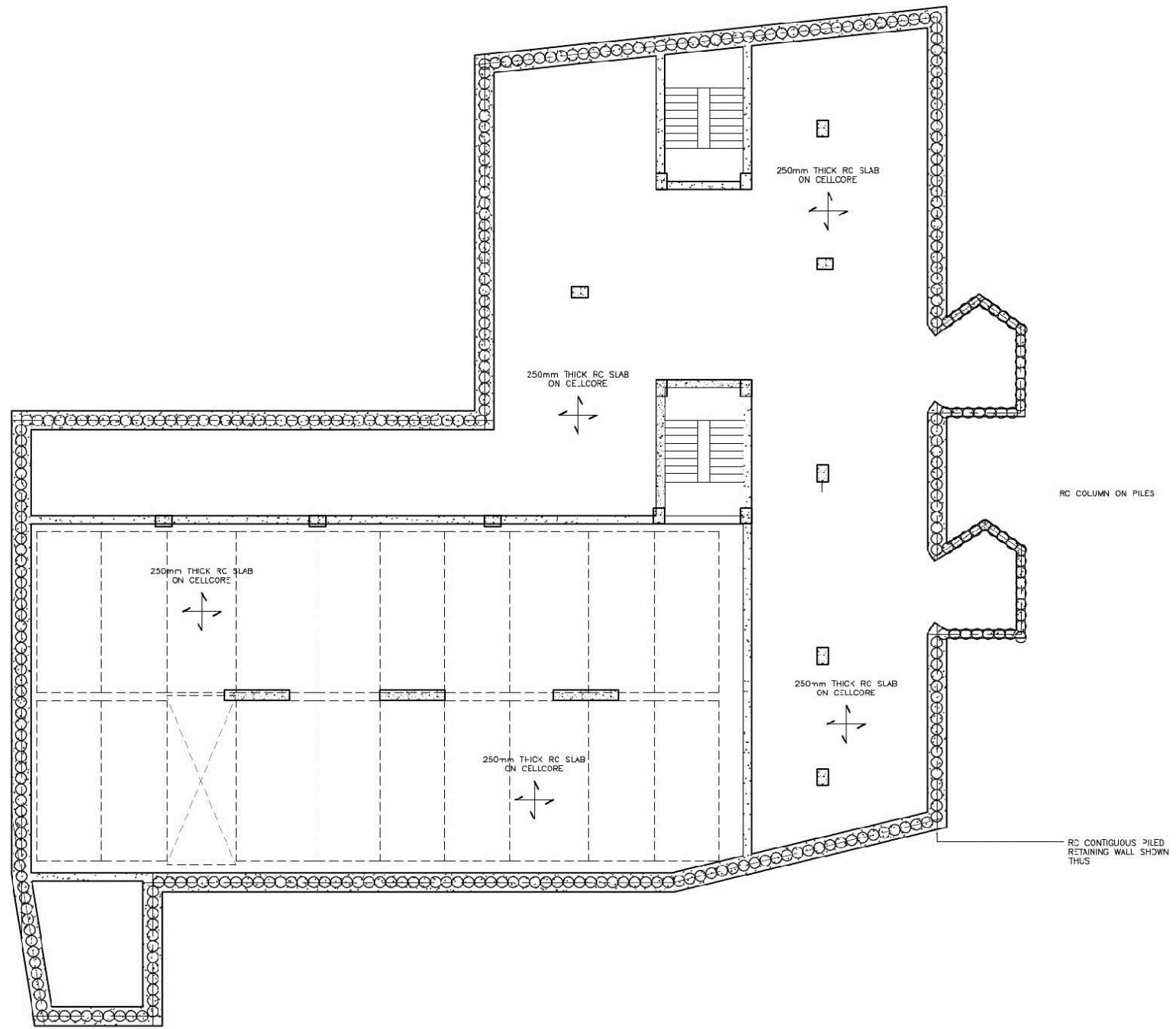


APPENDICES

APPENDIX A: Proposed Drawings and Sequence of Works



Notes

1. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH ALL RELEVANT ARCHITECTS & ENGINEERS DRAWINGS AND SPECIFICATIONS
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Rev	Date	By	Amendments
P1	08.11.14	JNS	PRELIMINARY ISSUE

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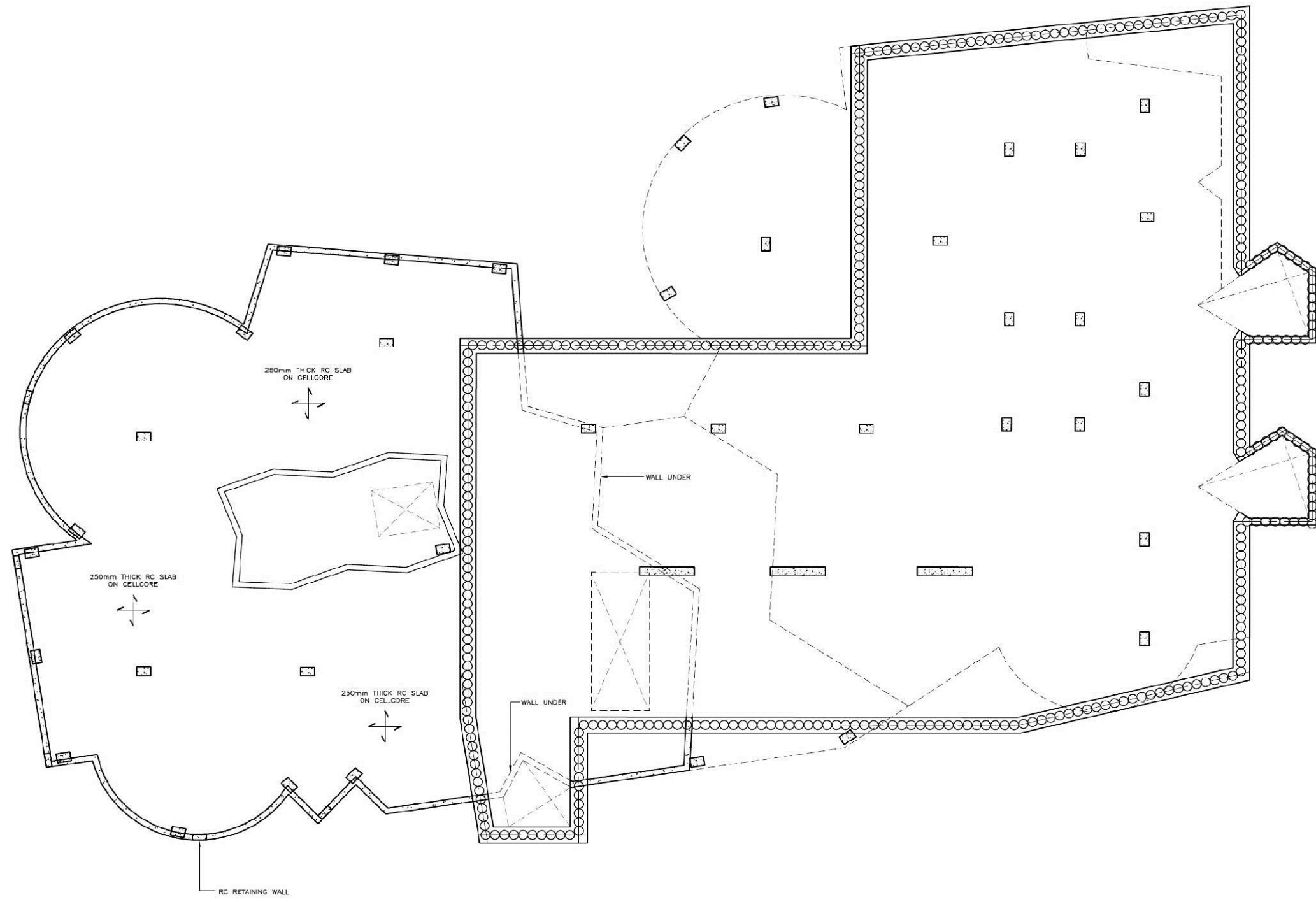
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Drawing Title
**BASEMENT FLOOR
 PLAN**

Job No.	Drawing No.	Revision
2014052	01	P1

Scale	1:100 AT A1	Original Size A1
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P1	02.12.14	JNS	PRELIMINARY ISSUE

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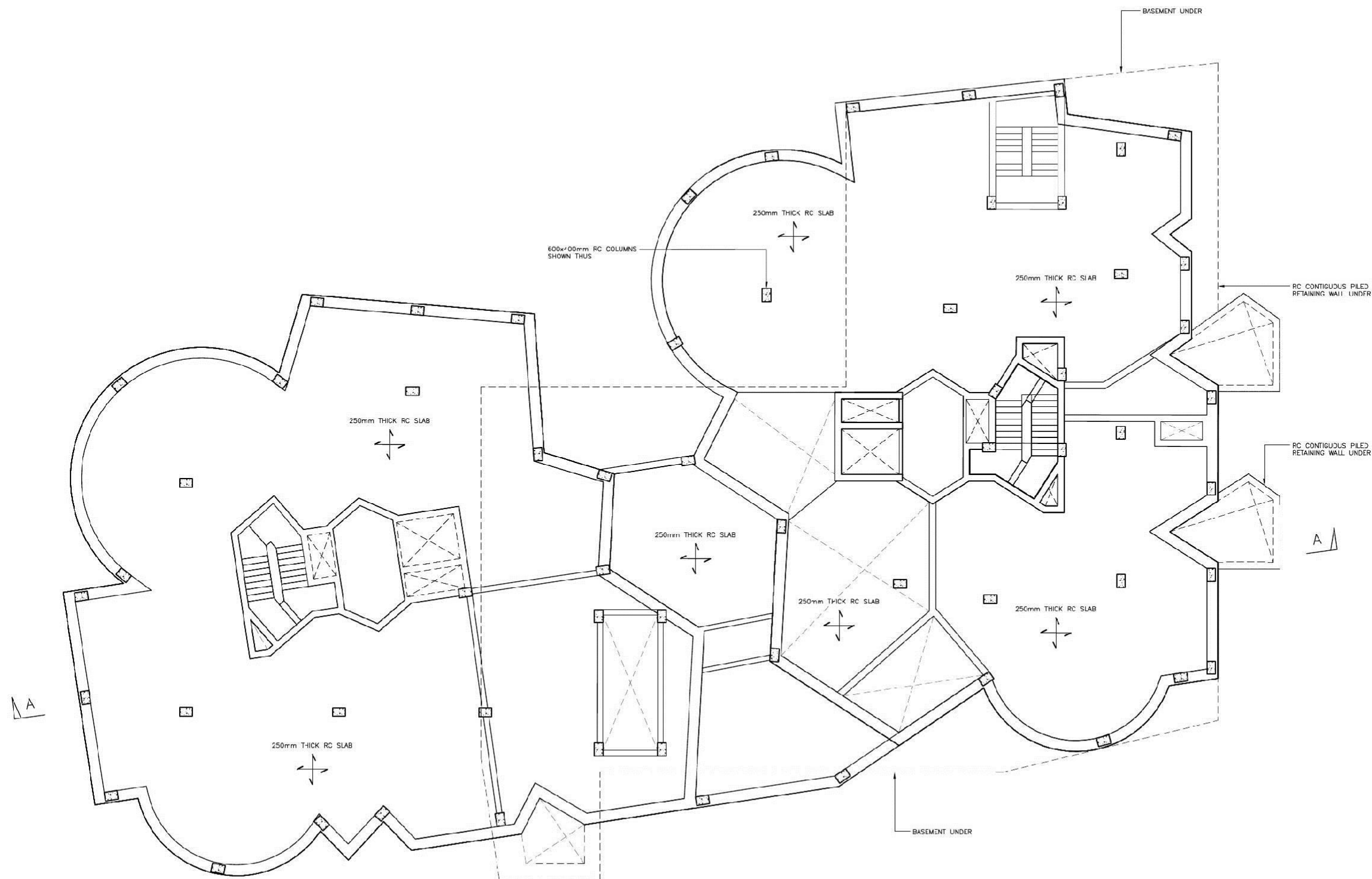
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Drawing Title:
**LOWER GROUND FLOOR
 PLAN**

Job No.	Drawing No.	Revision
2014052	02	P1
Scale	1:100 A1	Original Size A1
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Drawing Title

GROUND FLOOR
PLAN

Job No.	Drawing No.	Revision
2014052	03	P1

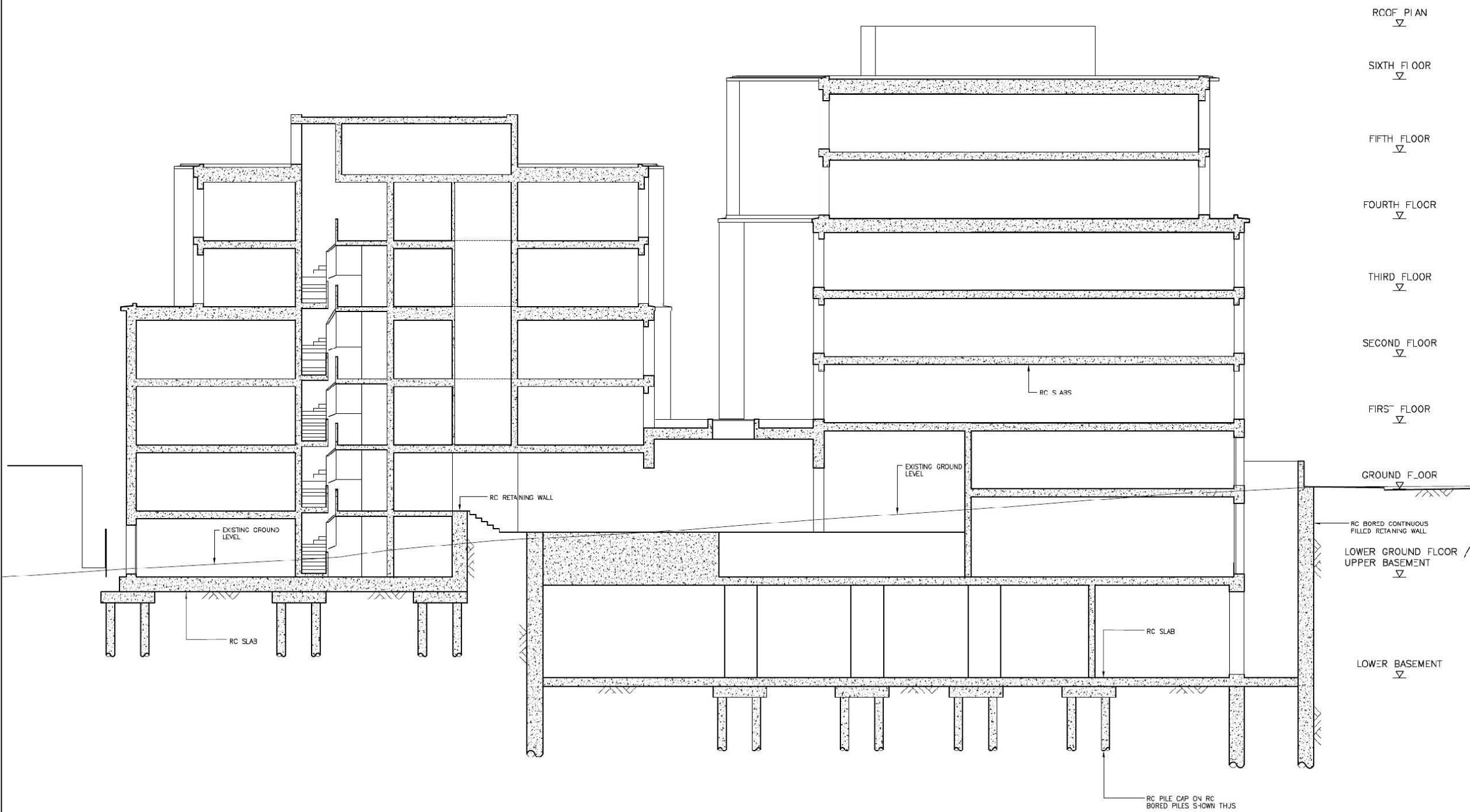
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Drawn By	SAV	Date: J.JULY 2014 Checked: AH

Proposed Construction Sequence for Substructure

1. Install bored cast in situ reinforced concrete contiguous piles to full perimeter of basement. Piles will be designed to cantilever above basement level in temporary condition.
2. Install internal bored cast in situ reinforced concrete piles, casting to approximately basement level.
3. Install internal bored cast in situ reinforced concrete piles sacrificial piles for temporary works, casting to ground level.
4. Cast reinforced concrete capping beam to contiguous piles to full perimeter.
5. Install temporary props at ground level, propping the perimeter capping beam onto internal temporary works piles at ground level.
6. Excavate basement down to first basement level.
7. Install temporary props at upper basement level, propping the contiguous piled wall onto internal temporary works piles at upper level of basement.
8. Excavate down to lower basement formation level.
9. Cut down internal piles and cast reinforced concrete pile caps.
10. Install below slab services.

11. Cast lower basement reinforced concrete slab, including epoxy dowelled connection to contiguous piles.
12. Cast reinforced concrete verticals from lower basement to upper basement.
13. Cast upper basement reinforced concrete slab, including epoxy dowelled connection to contiguous piles.
14. Remove temporary works at upper basement level.
15. Cast reinforced concrete verticals from upper basement to Ground floor.
16. Cast reinforced concrete ground floor slab and beams, including connection to capping beam.
17. Remove temporary works at ground floor level.
18. Break down internal sacrificial piles to basement slab level.
19. Cast reinforced concrete liner wall to inner face of contiguous piled wall.
20. Install internal cavity drain to vertical and horizontal inner faces of basement.

Construction method and sequence to be confirmed by contractor once appointed



Notes

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Drawing Title:
SECTION A - A

Job No.	Drawing No.	Revision
2014052	20	P1

Scale:	1:50 AT A1	Original Size A1
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APPENDIX B: Structural Calculations



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	Job No.	Sheet No.	Revision
	2014052	CL1	
Job Title	79 Fitzjohns Avenue, London NW3	Date	Made By
Section	Nov 14	RT	Checked By

Column Loads

Preliminary assessment of typical column loads

Typical floor load

- 75mm screed, $0.075 \text{m} \times 22 \text{kN/m}^3 = 1.7 \text{kN/m}^2$
 - Block partitions 1kN/m^2
 - Ceiling & services 0.3kN/m^2
 - Boarding 0.1kN/m^2
 - Imposed 1.5kN/m^2
 - Slab $0.25 \text{m} \times 24 \text{kN/m}^3 = 6 \text{kN/m}^2$
- $\Sigma 10.6 \text{kN/m}^2$

Typical roof

- Brown roof + PVs 1kN/m^2
- 75mm screed 1.7kN/m^2
- Ceiling & services 0.3kN/m^2
- Imposed 0.3kN/m^2
- Slab $0.25 \text{m} \times 24 \text{kN/m}^3 = 6 \text{kN/m}^2$
- Cladding 9.8kN/m^2
- 65% windows $(0.1 \text{m} \times 20 \text{kN/m}^2 + 0.1 \text{m} \times 15 \text{kN/m}^2) = 2.3 \text{kN/m}^2$

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	Job No.	Sheet No.	Revision
	2014052	CL2	
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a) Typical internal column to Fitzjohn block

N_1 , floors

$$\left[(10.6 \text{kN/m}^2 \times 8 \text{ no} + 9.8 \text{kN/m}^2 \times 1 \text{ no}) \right]$$

$= 97.9 \text{kN/m}^2 + 1.5 \text{kN/m}^2 \text{ extra live for } \left[\begin{array}{l} \text{communal} \\ \text{extra thickness} \\ \text{transfer slab} \end{array} \right]$

$$\times \frac{12\text{m}}{2} \times \frac{12\text{m}}{2} = 3524 \text{kN}$$

N_2 , column

$$0.6\text{m} \times 0.25\text{m} \times 24 \text{kN/m}^3 \times 25\text{m} = 90 \text{kN}$$

$\Sigma 3614 \text{kN}$

b) Typical perimeter column to Fitzjohn block

N_1 , slabs

$$97.9 \text{kN/m}^2 \times \frac{6\text{m}}{2} \times \frac{12\text{m}}{2} = 1620 \text{kN}$$

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N2, cladding
 $2.3 \text{ kN/m}^2 \times \frac{11\text{m}}{2} \times 20\text{m} = 250\text{kN}$
 N3 column, as internal 90kN
 E 1960kN
 For columns at $\approx 5.5\text{m}$ centres
 load on capping beam
 $= \frac{1960\text{kN}}{5.5\text{m}} = 356 \text{ kN/m}$



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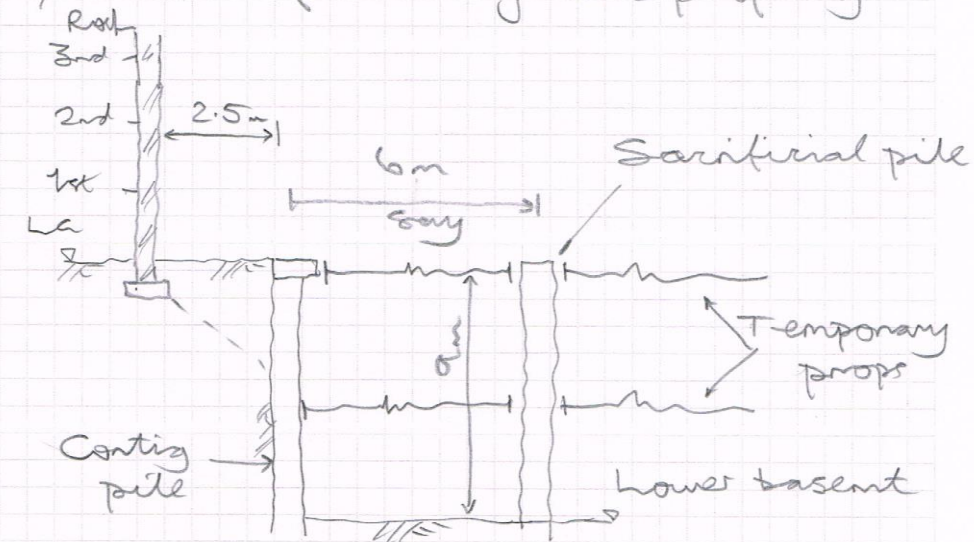
Job No.	Sheet No.	Revision
2014052	TW1	
Job Title	Date	Made By
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TEMPORARY WORKS

Preliminary assessment of temporary works load.

considers contig. piled retaining wall adjacent to North of site along Fitzjohn Avenue

a/ load from adjacent property



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i/ main house foundation load
 W1, floor 1st, 2nd, 3rd, roof
 $(0.6 + 1.5) \text{ kN/m}^2 \times \frac{5 \text{ m wide} \times 4 \text{ m}}{2} = 15 \text{ kN/m live}$
 dead live + 6 kN/m dead

Assume lower end is ground bearing

W2, flank wall, solid brick
 $0.33 \text{ m thick} \times 20 \text{ kN/m}^3 \times 4 \text{ m} \text{ LA-1st}$
 $+ 0.215 \text{ m thick} \times 20 \text{ kN/m}^3 (4 \text{ m} + 4 \text{ m} + \frac{4 \text{ m}}{2}) = 70 \text{ kN/m}$

DEAD 76 kN/m
 LIVE 15 kN/m

ii/ Flank extension

W1, flank wall DEAD
 $0.215 \text{ m thick} \times 20 \text{ kN/m}^3 \times 3 \text{ m} = 13 \text{ kN/m}$
 W2, roof DEAD + LIVE
 $1.7 \text{ kN/m}^2 \times \frac{3 \text{ m}}{2} = 2.6 \text{ kN/m}$

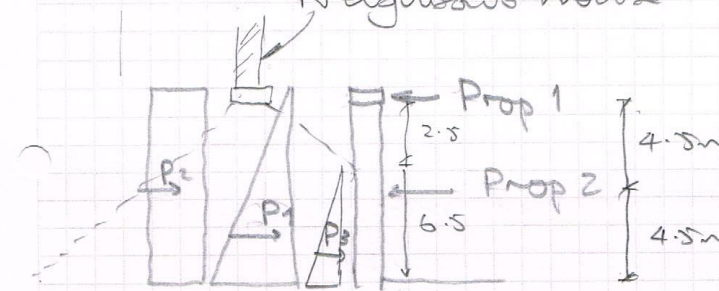


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b/ Props to retaining wall
 Neighbours house



P1, ground pressure
 $19 \text{ kN/m}^3 \times \frac{9 \text{ m}}{2} \times 0.33 \text{ kN} \times 9 \text{ m} = 254 \text{ kN}$

P2, surcharge live load in garden
 $3 \text{ kN/m}^2 \times 0.33 \text{ kN} \times 9 \text{ m} = 9 \text{ kN}$

P3, surcharge from neighbour house
 $6.5 \text{ m} \times (76 + 15 + 13 + 3) \text{ kN/m} \left[\frac{1}{(2.5 \text{ m} + 2.5 \text{ m})} + \frac{1}{(2.5 \text{ m} + 7 \text{ m})} \right]^{1/2}$
 ↑ page TW2
 $9 \text{ m} \text{ LA}$
 $\times 0.33 \text{ kN} = 35 \text{ kN}$

Consider pile as simply supported beam for loads on props.



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$$P_{prop 1} = 254 \text{ kN} \times \frac{1}{3} + \frac{9 \text{ kN}}{2} + 356 \text{ kN} \times \frac{1}{3}$$

↑
triangular P₂ →

$$= 101 \text{ kN/m}$$

$$P_{prop 2} = 254 \text{ kN} \times \frac{2}{3} + \frac{9 \text{ kN}}{2} + 356 \text{ kN} \times \frac{2}{3}$$

$$= 199.1 \text{ kN/m}$$

For props at, say, 5m c/c

Consider prop 2 as critical

$$N = 199.1 \text{ kN/m} \times 5 \text{ m c/c} \times 1.45 \text{ \gamma}_f$$

$$= 1450 \text{ kN}$$

For left = 6m

$$M_x = M_y = 1450 \text{ kN} \times 0.2 \text{ m} = 290 \text{ kNm}$$

↑
cap connection
notional eccentricity

Try 406 ϕ CHS x 10

$$\frac{F}{P_2} = \frac{1450}{4440} = 0.32$$

X-section

$$\frac{1450}{4440} + \frac{290}{513} = 0.89 < 1$$



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Buckling left = 6m

$$\frac{1450}{4110} + 0.57 \times \frac{290}{428} = 0.74 < 1$$

Adopt props 406 ϕ x 10 CHS
at 5m c/c at ground
and upper basement level.