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## 285-287 GRAYS INN ROAD, LONDON

## **NOISE IMPACT ASSESSMENT**

Report 9722-NIA-01

Prepared on 25 November 2014

Issued For: CA Medical 285-287 Grays Inn Road London WC1X 8QD









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## **1.0** INTRODUCTION

Clement Acoustics has been commissioned by CA Medical to measure existing background noise levels at 285-287 Grays Inn Road, London WC1X 8QD. The measured noise levels will be used to determine noise emission criteria for the proposed plant installation in agreement with the planning requirements of the London Borough of Camden.

This report presents the results of the environmental survey followed by noise impact calculations and outlines any necessary mitigation measures.

## 2.0 SITE DESCRIPTION

Current proposals are to install an external air conditioning condenser unit for commercial use at 285-287 Grays Inn Road, London WC1X 8QD. The proposed unit will be installed on the front light well wall in the basement, as shown in attached site plan 9722-SP1.

Following an onsite inspection, residential premises were observed both opposite the property, as well as a residential property located 3 houses to the north.

## 3.0 ENVIRONMENTAL NOISE SURVEY

## 3.1 Procedure

Measurements were undertaken at one position as shown on indicative site drawing 9722-SP1. The choice of this position was based both on accessibility and on collecting representative noise data in relation to the site.

Continuous automated monitoring was undertaken for the duration of the survey between 12:00 on 24 November 2014 and 12:00 on 25 November 2014. Weather conditions were generally dry with light winds, therefore suitable for the measurement of environmental noise.

Background noise levels at the monitoring positions consisted mainly of noise pedestrians in the area.

The measurement procedure generally complied with BS7445:1991. *Description and measurement of environmental noise, Part 2- Acquisition of data pertinent to land use*.



## 3.2 Equipment

The equipment calibration was verified before and after use and no abnormalities were observed.

The equipment used was as follows.

- 1 No. Svantek Type 957 Class 1 Sound Level Meter
- Norsonic Type 1251 Class 1 Calibrator

## 4.0 **RESULTS**

The  $L_{Aeq: 5min}$ ,  $L_{Amax: 5min}$ ,  $L_{A10: 5min}$  and  $L_{A90: 5min}$  acoustic parameters were measured at the location shown in site drawing 9722-SP1.

The measured noise levels are shown as a time history in Figure 9722-TH1.

	Average ambient noise level L <sub>Aeq: Smin</sub> dB(A)	Minimum background noise level L <sub>A90: 5min</sub> dB(A)
Daytime (07:00 - 23:00)	67 dB(A)	51 dB(A)
Night-time (23:00 - 07:00)	65 dB(A)	42 dB(A)
Operational hours (07:00 – 20:00)	67 dB(A)	52 dB(A)

Table 4.1: Minimum background noise levels

## 5.0 NOISE CRITERIA

In order to provide a suitably robust assessment and protect the amenity of residential premises in the area, we propose to set noise emissions criteria as follows:

"The 'A' weighted sound pressure level from the plant, when operating at its noisiest, shall not at any time exceed a value of 10 dB below the minimum external background noise, at a point 1 metre outside any window of any residential property."

As the proposed plant units will only be operating during the opening hours of CA Medical, which is understood to be 07:00 to 20:00, we propose to set the noise criteria at 42 dB(A), the value 10 dB below the minimum calculated background noise during the operational hours.



## 6.0 DISCUSSION

#### 6.1 **Proposed Installation**

The proposed plant installation is comprised of the following:

• 1 No. Mitsubishi Condenser Unit type SCM125ZM-S.

Noise emissions for the proposed plant units, as provided by the manufacturer, are shown in Table 6.1. Loudest modes of operation have been used in order to present a robust assessment.

		Sound Power Level (dB) in each Frequency Band									
Unit	63Hz	125Hz	250Hz	500Hz	1kHz	2kHz	4kHz	8kHz			
Mitsubishi SCM125ZM-S	42	49	50	54	58	52	49	41			

Table 6.1: Manufacturer Noise Emissions Levels

The proposed plant location is in a front facade light-well, below street level, in the location shown on indicative site plan 9722-SP1.

Two receivers have been identified, as follows:

- Receiver 1: Front window of house to the north of the site,
  - o 10m from proposed condenser unit,
- Receiver 2: Block of flats across Grays Inn Road,
  - o 25m from proposed condenser unit.

#### 6.2 Noise Impact Assessment

Taking into account all necessary acoustic corrections, the resulting noise level at the identified residential windows would be as shown in Table 6.2. Detailed calculations are shown in Appendix B.

Receiver	Operating Hours Criterion	Noise Level at Receiver (due to proposed plant)
Receiver 1		31 dB(A)
Receiver 2	42 dB(A) Receiver 2	20 dB(A)

 Table 6.2: Noise levels and criteria at noise sensitive receivers



As shown in Table 6.3 and Appendix B, the proposed plant installation would be expected to meet the requirements of the set criteria, without the need for particular mitigation measures.

### 6.3 British Standard Requirements

Further calculations have been undertaken to assess whether the noise emissions from the proposed plant unit would be expected to meet recognised British Standard recommendations, in order to further ensure the amenity of nearby noise sensitive receivers.

British Standard 8233:1999 'Sound insulation and noise reduction for buildings – Code of Practice' gives recommendations for acceptable internal noise levels in residential properties. Assuming worst case conditions, of the closest window being for a bedroom, BS8233:1999 recommends 30dB(A) as being 'good' internal resting/sleeping conditions.

With loudest external levels of 31 dB(A), 'good' to 'reasonable' internal conditions would be met without taking the attenuation of the window itself into consideration. According to BS8233:1999, even a partially open window offers 10-15 dB attenuation.

It can therefore be predicted that, in addition to meeting the requirements of the set criteria, the emissions from the proposed plant would be expected to meet the most stringent recommendations of the relevant British Standard, with neighbouring windows partially open. Predicted levels are shown in Table 6.3.

Receiver	'Good' Conditions Design Range – For resting/sleeping conditions in a bedroom, in BS8233:1999	Noise Level at Receiver (due to plant installation)
Inside Residential Window	30 dB(A)	21 dB(A)

 Table 6.3: Noise levels and criteria inside nearest residential space



## 7.0 CONCLUSION

An environmental noise survey has been undertaken at 285-287 Grays Inn Road, London WC1X 8QD. The results of the survey have enabled criteria to be set for noise emissions from the proposed plant units in accordance with the requirements of the London Borough of Camden.

A noise impact assessment has then been undertaken using manufacturer noise data to predict the noise levels due to the current proposal at the nearby noise sensitive receivers.

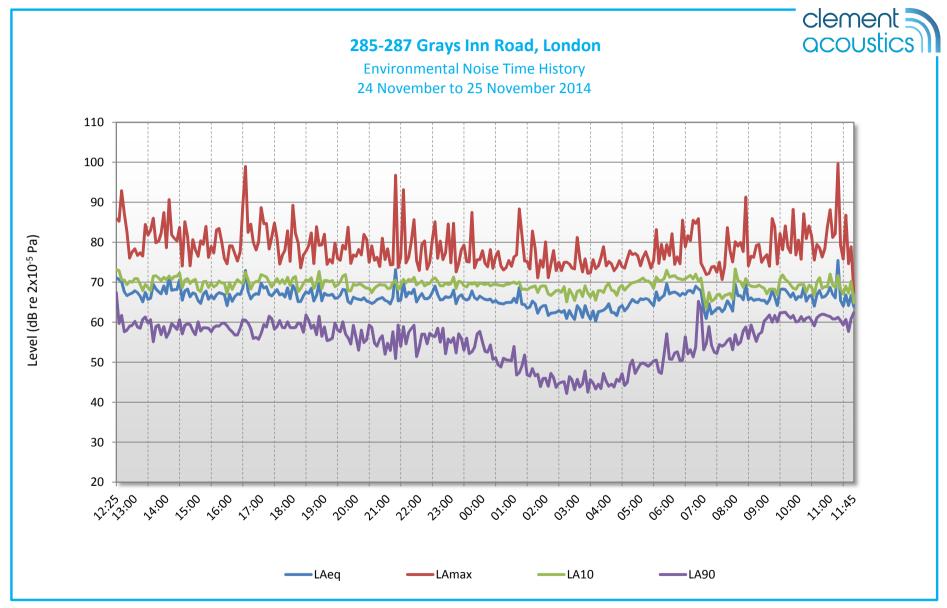
Calculations show that noise emissions from the proposed plant units would meet the requirements of the London Borough of Camden without the need for particular mitigation measures.

Report by Andrew Thomas Checked by Duncan Martin MIOA



**9722-SP1** Indicative site plan showing noise monitoring position and nearest noise sensitive receiver

Date: 26 November 2014



9722-TH1

# **APPENDIX A**

## **GLOSSARY OF ACOUSTIC TERMINOLOGY**



## dB(A)

The human ear is less sensitive to low (below 125Hz) and high (above 16kHz) frequency sounds. A sound level meter duplicates the ear's variable sensitivity to sound of different frequencies. This is achieved by building a filter into the instrument with a similar frequency response to that of the ear. This is called an A-weighting filter. Measurements of sound made with this filter are called A-weighted sound level measurements and the unit is dB(A).

## $L_{eq}$

The sound from noise sources often fluctuates widely during a given period of time. An average value can be measured, the equivalent sound pressure level  $L_{eq}$ . The  $L_{eq}$  is the equivalent sound level which would deliver the same sound energy as the actual fluctuating sound measured in the same time period.

## $L_{10}$

This is the level exceeded for not more than 10% of the time. This parameter is often used as a "not to exceed" criterion for noise

## L<sub>90</sub>

This is the level exceeded for not more than 90% of the time. This parameter is often used as a descriptor of "background noise" for environmental impact studies.

## **L**<sub>max</sub>

This is the maximum sound pressure level that has been measured over a period.

## **Octave Bands**

In order to completely determine the composition of a sound it is necessary to determine the sound level at each frequency individually. Usually, values are stated in octave bands. The audible frequency region is divided into 10 such octave bands whose centre frequencies are defined in accordance with international standards.

## Addition of noise from several sources

Noise from different sound sources combines to produce a sound level higher than that from any individual source. Two equally intense sound sources operating together produce a sound level which is 3dB higher than one alone and 10 sources produce a 10dB higher sound level.

## Attenuation by distance

Sound which propagates from a point source in free air attenuates by 6dB for each doubling of distance from the noise source. Sound energy from line sources (e.g. stream of cars) drops off by 3dB for each doubling of distance.

## Subjective impression of noise

Sound intensity is not perceived directly at the ear; rather it is transferred by the complex hearing mechanism to the brain where acoustic sensations can be interpreted as loudness. This makes hearing perception highly individualised. Sensitivity to noise also depends on frequency content, time of occurrence, duration of sound and psychological factors such as emotion and expectations. The following table is a reasonable guide to help explain increases or decreases in sound levels for many acoustic scenarios.

Change in sound level (dB)	Change in perceived loudness
1	Imperceptible
3	Just barely perceptible
6	Clearly noticeable
10	About twice as loud
20	About 4 times as loud

### **Barriers**

Outdoor barriers can be used to reduce environmental noises, such as traffic noise. The effectiveness of barriers is dependent on factors such as its distance from the noise source and the receiver, its height and its construction.

## **Reverberation control**

When sound falls on the surfaces of a room, part of its energy is absorbed and part is reflected back into the room. The amount of reflected sound defines the reverberation of a room, a characteristic that is critical for spaces of different uses as it can affect the quality of audio signals such as speech or music. Excess reverberation in a room can be controlled by the effective use of sound-absorbing treatment on the surfaces, such as fibrous ceiling boards, curtains and carpets.



## **APPENDIX B**

9722

## 285-287 Grays Inn Road, London **EXTERNAL PLANT NOISE EMISSIONS CALCULATION**

Receiver 1: House on same side of road									
Source: Proposed Plant Installation	Frequency, Hz								
	<u>63</u>	125	250	500	1k	2k	4k	8k	dB(A)
Manufacturer provided sound pressure level at 1 metre, dB									
Mitsubishi SCM125ZM-S	42	49	50	54	58	52	49	41	60
Correction for reflections, dB	6	6	6	6	6	6	6	6	
Attenuation due to light well wall dD	-4	-8	-11	-13	-15	-18	-21	-21	
Attenuation due to light-well wall, dB	-4	-0	-11	-15	-15	-10	-21	-21	
Distance correction to Receiver 1, dB (10m)	-20	-20	-20	-20	-20	-20	-20	-20	
·····									
Cumulative sound pressure level at Receiver 1 due to proposed plant	24	27	25	27	29	20	14	6	31

Design Criterion 42

## Receiver 2: Block of flats on opposite side of road Source: Proposed Plant Installation

Source: Proposed Plant Installation				Frequen	cy, Hz				
	63	125	250	500	1k	2k	4k	8k	dB(A)
Manufacturer provided sound pressure level at 1 metre, dB Mitsubishi SCM125ZM-S	42	49	50	54	58	52	49	41	60
Correction for reflections, dB	6	6	6	6	6	6	6	6	
Attenuation due to light-well wall, dB	-4	-8	-12	-15	-18	-21	-21	-21	
Distance correction to Receiver 2, dB (25m)	-28	-28	-28	-28	-28	-28	-28	-28	
Cumulative sound pressure level at Receiver 2 due to proposed plant	16	19	16	17	18	9	6	-2	20

Design Criterion 42