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# CALCULATIONS FOR RETAINING WALLS FOR 102 CAMDEN MEWS LONDON NW1 9AG

12.568 October 2014

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Date 01/10/14

Eng. JC

Job No. 12.568

Sheet No.

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102 CAMDEN MEWS  
LONDON  
NW1 9AG

## RETAINING WALLS

Party wall:

$$s/w \text{ b/wk} = (5.1 \text{ kN/m}^2 \times 4.9 \text{ m}) + (7.8 \text{ kN/m}^2 \times 3.0 \text{ m})$$

$$s/w \text{ roof} = 0.75 \text{ kN/m}^2 \times 2.0 \text{ m} \times 2$$

$$V \text{ roof} = 0.75 \text{ kN/m}^2 \times 2.0 \text{ m} \times 2$$

$$s/w \text{ floor} = 0.5 \text{ kN/m}^2 \times 2.0 \text{ m} \times 2 \times 3$$

$$V \text{ floor} = 1.5 \text{ kN/m}^2 \times 2.0 \text{ m} \times 2 \times 3$$

kN/m	
Pl	V
48.4	
3.0	
	3.0
6.0	
	18.0
57.4	21.0

Front and rear wall:

$$s/w \text{ b/wk} = (5.1 \text{ kN/m}^2 \times 3.4 \text{ m}) + (7.8 \text{ kN/m}^2 \times 5.0 \text{ m})$$

$$s/w \text{ stud} = 1.0 \text{ kN/m}^2 \times 1.5 \text{ m}$$

$$s/w \text{ roof} = 0.75 \text{ kN/m}^2 \times 1.55 \text{ m}$$

$$V \text{ roof} = 0.75 \text{ kN/m}^2 \times 1.55 \text{ m}$$

$$s/w \text{ door} = 0.5 \text{ kN/m}^2 \times 1.55 \text{ m} \times 3$$

$$V \text{ floor} = 1.2 \text{ kN/m}^2 \times 1.55 \text{ m} \times 3$$

MAX LOADING

40.8	
1.5	
	1.2
1.2	
	1.2
2.4	
	7.0
45.9	8.2

$$s/w \text{ b/wk} = (5.1 \text{ kN/m}^2 \times 2.7 \text{ m}) + (7.8 \text{ kN/m}^2 \times 2.8 \text{ m})$$

MIN LOADING

worst case

35.6



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Project 102 Camden Mews, London, NW1 9AG		Job no. 12.568	
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### RETAINING WALL ANALYSIS

In accordance with EN1997-1:2004 incorporating Corrigendum dated February 2009 and the UK National Annex incorporating Corrigendum No.1

Tedds calculation version 2.4.08

#### Retaining wall details

Stem type	Cantilever		
Stem height	$h_{\text{stem}} = 2400$ mm		
Prop height	$h_{\text{prop}} = 0$ mm		
Stem thickness	$t_{\text{stem}} = 330$ mm		
Angle to rear face of stem	$\alpha = 90$ deg		
Stem density	$\gamma_{\text{stem}} = 25$ kN/m <sup>3</sup>		
Toe length	$l_{\text{toe}} = 1200$ mm		
Heel length	$l_{\text{heel}} = 100$ mm		
Base thickness	$t_{\text{base}} = 350$ mm		
Base density	$\gamma_{\text{base}} = 25$ kN/m <sup>3</sup>		
Height of retained soil	$h_{\text{ret}} = 2400$ mm	Angle of soil surface	$\beta = 0$ deg
Depth of cover	$d_{\text{cover}} = 0$ mm		
Height of water	$h_{\text{water}} = 1600$ mm		
Water density	$\gamma_w = 9.8$ kN/m <sup>3</sup>		

#### Retained soil properties

Soil type	Soft clay		
Moist density	$\gamma_{\text{mr}} = 17$ kN/m <sup>3</sup>		
Saturated density	$\gamma_{\text{sr}} = 17$ kN/m <sup>3</sup>		
Characteristic effective shear resistance angle		$\phi'_{\text{r.k}} = 18$ deg	
Characteristic wall friction angle		$\delta_{\text{r.k}} = 9$ deg	

#### Base soil properties

Soil type	Firm clay		
Moist density	$\gamma_{\text{mb}} = 18$ kN/m <sup>3</sup>		
Characteristic effective shear resistance angle		$\phi'_{\text{b.k}} = 18$ deg	
Characteristic wall friction angle		$\delta_{\text{b.k}} = 9$ deg	
Characteristic base friction angle		$\delta_{\text{bb.k}} = 12$ deg	
Presumed bearing capacity	$P_{\text{bearing}} = 100$ kN/m <sup>2</sup>		

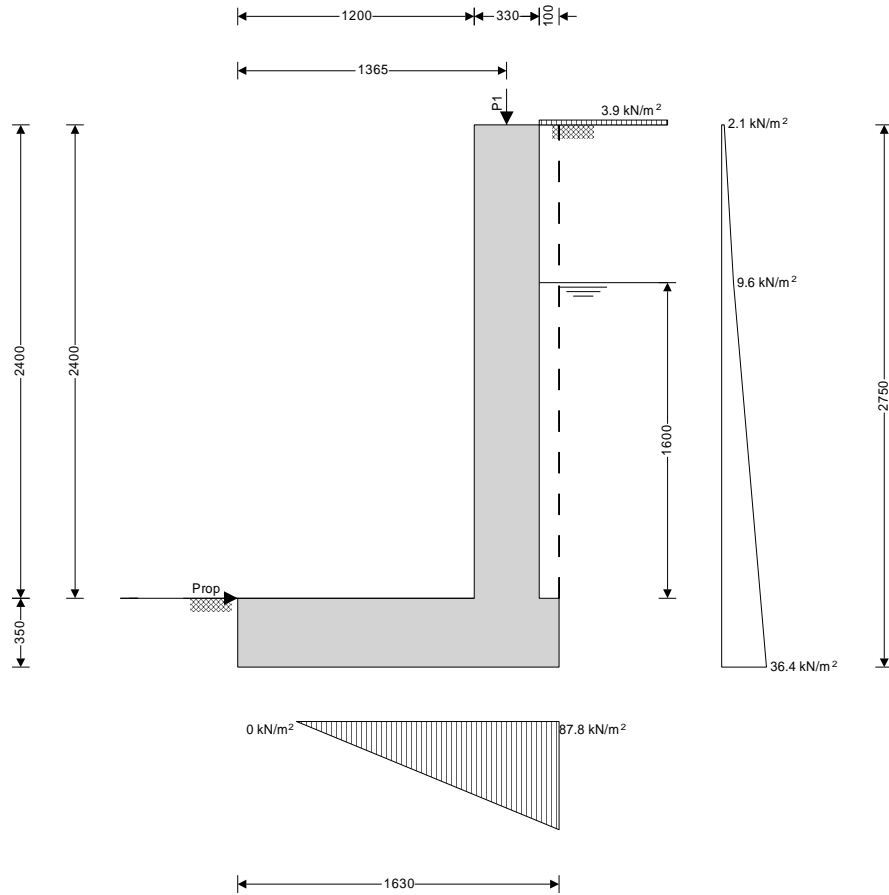
#### Loading details

Variable surcharge load	Surcharge <sub>Q</sub> = 3 kN/m <sup>2</sup>
Vertical line load at 1365 mm	$P_{G1} = 57.4$ kN/m
	$P_{Q1} = 21$ kN/m



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### Calculate retaining wall geometry

Base length	$l_{base} = 1630$ mm
Saturated soil height	$h_{sat} = 1600$ mm
Moist soil height	$h_{moist} = 800$ mm
Length of surcharge load	$l_{sur} = 100$ mm
Vertical distance	$x_{sur\_v} = 1580$ mm
Effective height of wall	$h_{eff} = 2750$ mm
Horizontal distance	$x_{sur\_h} = 1375$ mm
Area of wall stem	$A_{stem} = 0.792$ m <sup>2</sup>
Area of wall base	$A_{base} = 0.571$ m <sup>2</sup>
Area of saturated soil	$A_{sat} = 0.16$ m <sup>2</sup>
Area of water	$A_{water} = 0.16$ m <sup>2</sup>
Area of moist soil	$A_{moist} = 0.08$ m <sup>2</sup>

Vertical distance	$x_{stem} = 1365$ mm
Vertical distance	$x_{base} = 815$ mm
Vertical distance	$x_{sat\_v} = 1580$ mm
Horizontal distance	$x_{sat\_h} = 650$ mm
Vertical distance	$x_{water\_v} = 1580$ mm
Horizontal distance	$x_{water\_h} = 650$ mm
Vertical distance	$x_{moist\_v} = 1580$ mm
Horizontal distance	$x_{moist\_h} = 1186$ mm

### Using Coulomb theory

Active pressure coefficient	$K_A = 0.483$	Passive pressure coefficient	$K_P = 2.359$
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### Bearing pressure check

### Vertical forces on wall

Total  $F_{total\_v} = F_{stem} + F_{base} + F_{sat\_v} + F_{moist\_v} + F_{water\_v} + F_{sur\_v} + F_{P\_v} = 116.8$  kN/m



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### Horizontal forces on wall

Total  $F_{total\_h} = F_{sat\_h} + F_{moist\_h} + F_{water\_h} + F_{sur\_h} = 44.4$  kN/m

### Moments on wall

Total  $M_{total} = M_{stem} + M_{base} + M_{sat} + M_{moist} + M_{water} + M_{sur} + M_P = 112.7$  kNm/m

### Check bearing pressure

Propping force  $F_{prop\_base} = 44.4$  kN/m

Bearing pressure at toe  $q_{toe} = 0$  kN/m<sup>2</sup>      Bearing pressure at heel  $q_{heel} = 87.8$  kN/m<sup>2</sup>

Factor of safety  $FoS_{bp} = 1.139$

**PASS - Allowable bearing pressure exceeds maximum applied bearing pressure**

### RETAINING WALL DESIGN

In accordance with EN1992-1-1:2004 incorporating Corrigendum dated January 2008 and the UK National Annex incorporating National Amendment No.1

Tedds calculation version 2.4.08

#### Concrete details - Table 3.1 - Strength and deformation characteristics for concrete

Concrete strength class	C32/40		
Char.comp.cylinder strength	$f_{ck} = 32$ N/mm <sup>2</sup>	Mean axial tensile strength	$f_{ctm} = 3.0$ N/mm <sup>2</sup>
Secant modulus of elasticity	$E_{cm} = 33346$ N/mm <sup>2</sup>	Maximum aggregate size	$h_{agg} = 20$ mm
Design comp.concrete strength		$f_{cd} = 18.1$ N/mm <sup>2</sup>	Partial factor $\gamma_c = 1.50$

#### Reinforcement details

Characteristic yield strength	$f_{yk} = 500$ N/mm <sup>2</sup>	Modulus of elasticity	$E_s = 200000$ N/mm <sup>2</sup>
Design yield strength	$f_{yd} = 435$ N/mm <sup>2</sup>	Partial factor	$\gamma_s = 1.15$

#### Cover to reinforcement

Front face of stem	$C_{sf} = 20$ mm	Rear face of stem	$C_{sr} = 75$ mm
Top face of base	$C_{bt} = 20$ mm	Bottom face of base	$C_{bb} = 75$ mm

#### Check stem design at base of stem

Depth of section  $h = 330$  mm

#### Rectangular section in flexure - Section 6.1

Design bending moment	$M = 36.1$ kNm/m	$K = 0.019$	$K' = 0.207$
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**$K' > K$  - No compression reinforcement is required**

Tens.reinforcement required	$A_{sr.req} = 354$ mm <sup>2</sup> /m	Tens.reinforcement provided	$A_{sr.prov} = 1005$ mm <sup>2</sup> /m
Min.area of reinforcement	$A_{sr.min} = 388$ mm <sup>2</sup> /m	Max.area of reinforcement	$A_{sr.max} = 13200$ mm <sup>2</sup> /m

**PASS - Area of reinforcement provided is greater than area of reinforcement required**

#### Crack control - Section 7.3

Limiting crack width	$w_{max} = 0.3$ mm	Maximum crack width	$w_k = 0.165$ mm
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**PASS - Maximum crack width is less than limiting crack width**

Design shear force	$V = 45.6$ kN/m	Design shear resistance	$V_{Rd.c} = 128.1$ kN/m
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**PASS - Design shear resistance exceeds design shear force**

#### Horizontal reinforcement parallel to face of stem - Section 9.6

Min.area of reinforcement	$A_{sx.req} = 330$ mm <sup>2</sup> /m	Max.spacing of reinforcement	$s_{sx.max} = 400$ mm
Trans.reinforcement provided	10 dia.bars @ 200 c/c	Trans.reinforcement provided	$A_{sx.prov} = 393$ mm <sup>2</sup> /m

**PASS - Area of reinforcement provided is greater than area of reinforcement required**

#### Check base design at toe

Depth of section  $h = 350$  mm



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**Rectangular section in flexure - Section 6.1**

Design bending moment  $M = 42.2$  kNm/m  $K = 0.019$   $K' = 0.207$   
 *$K' > K$  - No compression reinforcement is required*

Tens.reinforcement required  $A_{bb.req} = 383$  mm<sup>2</sup>/m  
 Tens.reinforcement provided 16 dia.bars @ 200 c/c Tens.reinforcement provided  $A_{bb.prov} = 1005$  mm<sup>2</sup>/m  
 Min.area of reinforcement  $A_{bb.min} = 420$  mm<sup>2</sup>/m Max.area of reinforcement  $A_{bb.max} = 14000$  mm<sup>2</sup>/m  
**PASS - Area of reinforcement provided is greater than area of reinforcement required**

**Crack control - Section 7.3**

Limiting crack width  $w_{max} = 0.3$  mm Maximum crack width  $w_k = 0.196$  mm

**Rectangular section in shear - Section 6.2**

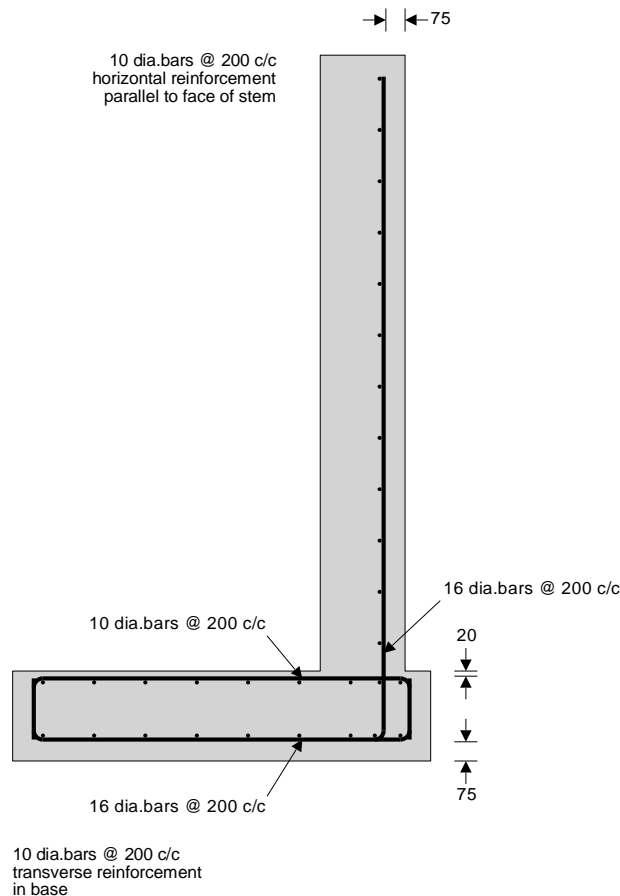
Design shear force  $V = 86.7$  kN/m Design shear resistance  $V_{Rd.c} = 137$  kN/m  
**PASS - Design shear resistance exceeds design shear force**

**Rectangular section in shear - Section 6.2**

Design shear force  $V = 7.9$  kN/m Design shear resistance  $V_{Rd.c} = 134.7$  kN/m  
**PASS - Design shear resistance exceeds design shear force**

**Secondary transverse reinforcement to base - Section 9.3**

Min.area of reinforcement  $A_{bx.req} = 201$  mm<sup>2</sup>/m Max.spacing of reinforcement  $S_{bx,max} = 450$  mm  
 Trans.reinforcement provided 10 dia.bars @ 200 c/c Trans.reinforcement provided  $A_{bx.prov} = 393$  mm<sup>2</sup>/m  
**PASS - Area of reinforcement provided is greater than area of reinforcement required**





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### RETAINING WALL ANALYSIS

In accordance with EN1997-1:2004 incorporating Corrigendum dated February 2009 and the UK National Annex incorporating Corrigendum No.1

Tedds calculation version 2.4.08

#### Retaining wall details

Stem type	Cantilever		
Stem height	$h_{\text{stem}} = 2400$ mm		
Prop height	$h_{\text{prop}} = 0$ mm		
Stem thickness	$t_{\text{stem}} = 330$ mm		
Angle to rear face of stem	$\alpha = 90$ deg		
Stem density	$\gamma_{\text{stem}} = 25$ kN/m <sup>3</sup>		
Toe length	$l_{\text{toe}} = 1200$ mm		
Heel length	$l_{\text{heel}} = 100$ mm		
Base thickness	$t_{\text{base}} = 350$ mm		
Base density	$\gamma_{\text{base}} = 25$ kN/m <sup>3</sup>		
Height of retained soil	$h_{\text{ret}} = 2400$ mm	Angle of soil surface	$\beta = 0$ deg
Depth of cover	$d_{\text{cover}} = 0$ mm		
Height of water	$h_{\text{water}} = 1600$ mm		
Water density	$\gamma_w = 9.8$ kN/m <sup>3</sup>		

#### Retained soil properties

Soil type	Soft clay		
Moist density	$\gamma_{\text{mr}} = 17$ kN/m <sup>3</sup>		
Saturated density	$\gamma_{\text{sr}} = 17$ kN/m <sup>3</sup>		
Characteristic effective shear resistance angle		$\phi'_{r,k} = 18$ deg	
Characteristic wall friction angle		$\delta_{r,k} = 9$ deg	

#### Base soil properties

Soil type	Firm clay		
Moist density	$\gamma_{\text{mb}} = 18$ kN/m <sup>3</sup>		
Characteristic effective shear resistance angle		$\phi'_{b,k} = 18$ deg	
Characteristic wall friction angle		$\delta_{b,k} = 9$ deg	
Characteristic base friction angle		$\delta_{bb,k} = 12$ deg	
Presumed bearing capacity	$P_{\text{bearing}} = 100$ kN/m <sup>2</sup>		

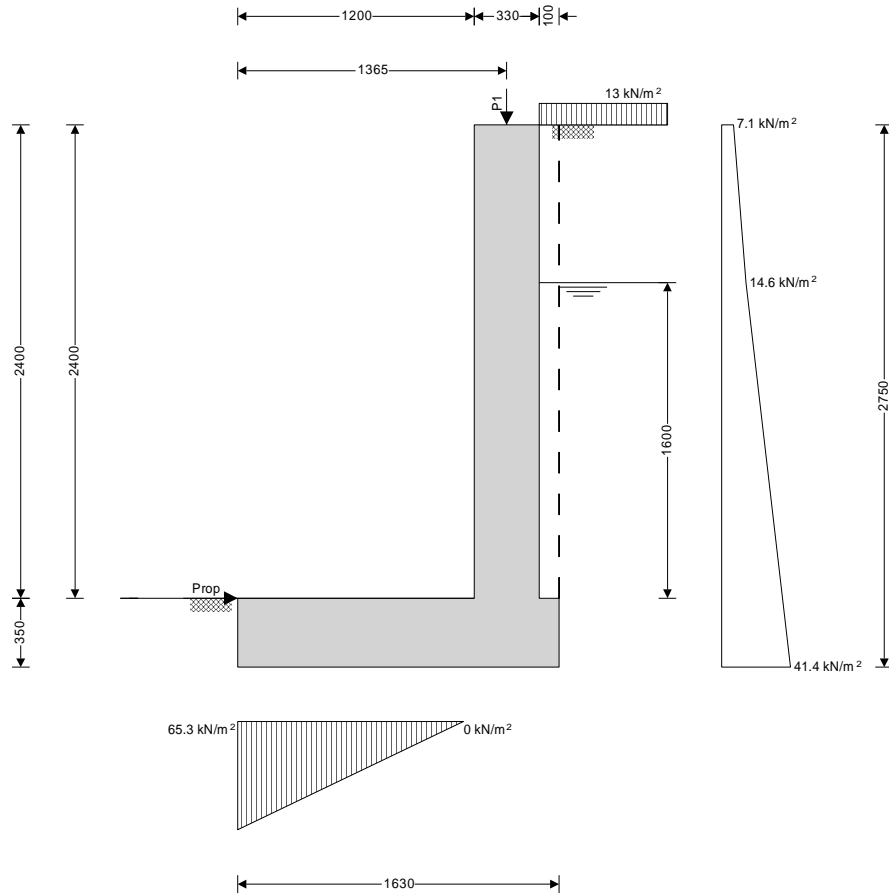
#### Loading details

Variable surcharge load	Surcharge <sub>Q</sub> = 10 kN/m <sup>2</sup>
Vertical line load at 1365 mm	$P_{G1} = 35.6$ kN/m



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### Calculate retaining wall geometry

Base length	$l_{base} = 1630$ mm
Saturated soil height	$h_{sat} = 1600$ mm
Moist soil height	$h_{moist} = 800$ mm
Length of surcharge load	$l_{sur} = 100$ mm
Vertical distance	$x_{sur\_v} = 1580$ mm
Effective height of wall	$h_{eff} = 2750$ mm
Horizontal distance	$x_{sur\_h} = 1375$ mm
Area of wall stem	$A_{stem} = 0.792$ m <sup>2</sup>
Area of wall base	$A_{base} = 0.571$ m <sup>2</sup>
Area of saturated soil	$A_{sat} = 0.16$ m <sup>2</sup>
Area of water	$A_{water} = 0.16$ m <sup>2</sup>
Area of moist soil	$A_{moist} = 0.08$ m <sup>2</sup>

Vertical distance	$x_{stem} = 1365$ mm
Vertical distance	$x_{base} = 815$ mm
Vertical distance	$x_{sat\_v} = 1580$ mm
Horizontal distance	$x_{sat\_h} = 650$ mm
Vertical distance	$x_{water\_v} = 1580$ mm
Horizontal distance	$x_{water\_h} = 650$ mm
Vertical distance	$x_{moist\_v} = 1580$ mm
Horizontal distance	$x_{moist\_h} = 1186$ mm

### Using Coulomb theory

Active pressure coefficient	$K_A = 0.483$	Passive pressure coefficient	$K_P = 2.359$
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### Bearing pressure check

#### Vertical forces on wall

Total  $F_{total\_v} = F_{stem} + F_{base} + F_{sat\_v} + F_{moist\_v} + F_{water\_v} + F_{sur\_v} + F_{P\_v} = 74.7$  kN/m





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### Horizontal forces on wall

Total  $F_{total\_h} = F_{sat\_h} + F_{moist\_h} + F_{water\_h} + F_{sur\_h} = 53.5$  kN/m

### Moments on wall

Total  $M_{total} = M_{stem} + M_{base} + M_{sat} + M_{moist} + M_{water} + M_{sur} + M_P = 42.8$  kNm/m

### Check bearing pressure

Propping force  $F_{prop\_base} = 53.5$  kN/m

Bearing pressure at toe  $q_{toe} = 65.3$  kN/m<sup>2</sup>      Bearing pressure at heel  $q_{heel} = 0$  kN/m<sup>2</sup>

Factor of safety  $FoS_{bp} = 1.531$

**PASS - Allowable bearing pressure exceeds maximum applied bearing pressure**

### RETAINING WALL DESIGN

In accordance with EN1992-1-1:2004 incorporating Corrigendum dated January 2008 and the UK National Annex incorporating National Amendment No.1

Tedds calculation version 2.4.08

### Concrete details - Table 3.1 - Strength and deformation characteristics for concrete

Concrete strength class	C32/40		
Char.comp.cylinder strength	$f_{ck} = 32$ N/mm <sup>2</sup>	Mean axial tensile strength	$f_{ctm} = 3.0$ N/mm <sup>2</sup>
Secant modulus of elasticity	$E_{cm} = 33346$ N/mm <sup>2</sup>	Maximum aggregate size	$h_{agg} = 20$ mm
Design comp.concrete strength		$f_{cd} = 18.1$ N/mm <sup>2</sup>	Partial factor $\gamma_c = 1.50$

### Reinforcement details

Characteristic yield strength	$f_{yk} = 500$ N/mm <sup>2</sup>	Modulus of elasticity	$E_s = 200000$ N/mm <sup>2</sup>
Design yield strength	$f_{yd} = 435$ N/mm <sup>2</sup>	Partial factor	$\gamma_s = 1.15$

### Cover to reinforcement

Front face of stem	$C_{sf} = 20$ mm	Rear face of stem	$C_{sr} = 75$ mm
Top face of base	$C_{bt} = 20$ mm	Bottom face of base	$C_{bb} = 75$ mm

### Check stem design at base of stem

Depth of section  $h = 330$  mm

### Rectangular section in flexure - Section 6.1

Design bending moment  $M = 50.6$  kNm/m       $K = 0.026$        $K' = 0.207$

**$K' > K$  - No compression reinforcement is required**

Tens.reinforcement required	$A_{sr.req} = 496$ mm <sup>2</sup> /m	Tens.reinforcement provided	$A_{sr.prov} = 1005$ mm <sup>2</sup> /m
Min.area of reinforcement	$A_{sr.min} = 388$ mm <sup>2</sup> /m	Max.area of reinforcement	$A_{sr.max} = 13200$ mm <sup>2</sup> /m

**PASS - Area of reinforcement provided is greater than area of reinforcement required**

### Crack control - Section 7.3

Limiting crack width  $w_{max} = 0.3$  mm      Maximum crack width  $w_k = 0.203$  mm

**PASS - Maximum crack width is less than limiting crack width**

Design shear force  $V = 57.6$  kN/m      Design shear resistance  $V_{Rd.c} = 128.1$  kN/m

**PASS - Design shear resistance exceeds design shear force**

### Horizontal reinforcement parallel to face of stem - Section 9.6

Min.area of reinforcement	$A_{sx.req} = 330$ mm <sup>2</sup> /m	Max.spacing of reinforcement	$s_{sx.max} = 400$ mm
Trans.reinforcement provided	10 dia.bars @ 200 c/c	Trans.reinforcement provided	$A_{sx.prov} = 393$ mm <sup>2</sup> /m

**PASS - Area of reinforcement provided is greater than area of reinforcement required**

### Check base design at toe

Depth of section  $h = 350$  mm



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**Rectangular section in flexure - Section 6.1**

Design bending moment  $M = 58.5$  kNm/m  $K = 0.026$   $K' = 0.207$   
***K' > K - No compression reinforcement is required***

Tens.reinforcement required  $A_{bb.req} = 535$  mm<sup>2</sup>/m  
Tens.reinforcement provided 20 dia.bars @ 200 c/c Tens.reinforcement provided  $A_{bb.prov} = 1571$  mm<sup>2</sup>/m  
Min.area of reinforcement  $A_{bb.min} = 417$  mm<sup>2</sup>/m Max.area of reinforcement  $A_{bb.max} = 14000$  mm<sup>2</sup>/m  
***PASS - Area of reinforcement provided is greater than area of reinforcement required***

**Crack control - Section 7.3**

Limiting crack width  $w_{max} = 0.3$  mm Maximum crack width  $w_k = 0.153$  mm

***PASS - Maximum crack width is less than limiting crack width*** Rectangular section in shear - Section 6.2

Design shear force  $V = 79.6$  kN/m Design shear resistance  $V_{Rd.c} = 158.5$  kN/m  
***PASS - Design shear resistance exceeds design shear force***

**Rectangular section in flexure - Section 6.1**

Design bending moment  $M = 0.4$  kNm/m  $K = 0.000$   $K' = 0.207$   
***K' > K - No compression reinforcement is required***

Tens.reinforcement required  $A_{bt.req} = 3$  mm<sup>2</sup>/m  
Tens.reinforcement provided 12 dia.bars @ 200 c/c Tens.reinforcement provided  $A_{bt.prov} = 565$  mm<sup>2</sup>/m  
Min.area of reinforcement  $A_{bt.min} = 509$  mm<sup>2</sup>/m Max.area of reinforcement  $A_{bt.max} = 14000$  mm<sup>2</sup>/m  
***PASS - Area of reinforcement provided is greater than area of reinforcement required***

**Crack control - Section 7.3**

Limiting crack width  $w_{max} = 0.3$  mm Maximum crack width  $w_k = 0.001$  mm

***PASS - Maximum crack width is less than limiting crack width*** Rectangular section in shear - Section 6.2

Design shear force  $V = 7.7$  kN/m Design shear resistance  $V_{Rd.c} = 153.1$  kN/m  
***PASS - Design shear resistance exceeds design shear force***

**Secondary transverse reinforcement to base - Section 9.3**

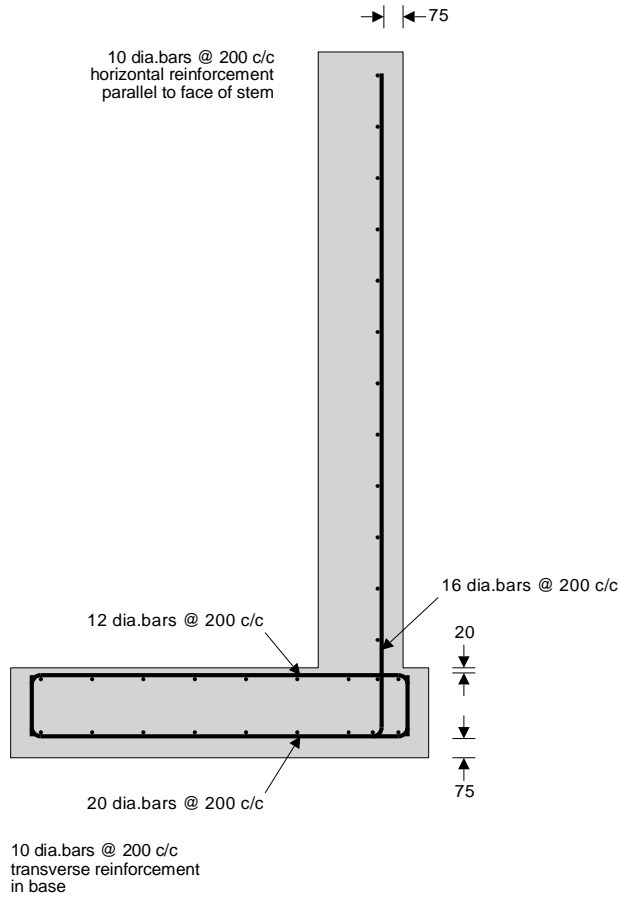
Min.area of reinforcement  $A_{bx.req} = 314$  mm<sup>2</sup>/m Max.spacing of reinforcement  $S_{bx,max} = 450$  mm  
Trans.reinforcement provided 10 dia.bars @ 200 c/c Trans.reinforcement provided  $A_{bx.prov} = 393$  mm<sup>2</sup>/m  
***PASS - Area of reinforcement provided is greater than area of reinforcement required***



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### RETAINING WALL ANALYSIS

In accordance with EN1997-1:2004 incorporating Corrigendum dated February 2009 and the UK National Annex incorporating Corrigendum No.1

Tedds calculation version 2.4.08

#### Retaining wall details

Stem type	Cantilever		
Stem height	$h_{\text{stem}} = 2400$ mm		
Prop height	$h_{\text{prop}} = 0$ mm		
Stem thickness	$t_{\text{stem}} = 330$ mm		
Angle to rear face of stem	$\alpha = 90$ deg		
Stem density	$\gamma_{\text{stem}} = 25$ kN/m <sup>3</sup>		
Toe length	$l_{\text{toe}} = 1200$ mm		
Heel length	$l_{\text{heel}} = 100$ mm		
Base thickness	$t_{\text{base}} = 350$ mm		
Base density	$\gamma_{\text{base}} = 25$ kN/m <sup>3</sup>		
Height of retained soil	$h_{\text{ret}} = 2400$ mm	Angle of soil surface	$\beta = 0$ deg
Depth of cover	$d_{\text{cover}} = 0$ mm		
Height of water	$h_{\text{water}} = 1600$ mm		
Water density	$\gamma_w = 9.8$ kN/m <sup>3</sup>		

#### Retained soil properties

Soil type	Soft clay		
Moist density	$\gamma_{\text{mr}} = 17$ kN/m <sup>3</sup>		
Saturated density	$\gamma_{\text{sr}} = 17$ kN/m <sup>3</sup>		
Characteristic effective shear resistance angle		$\phi'_{\text{r.k}} = 18$ deg	
Characteristic wall friction angle		$\delta_{\text{r.k}} = 9$ deg	

#### Base soil properties

Soil type	Firm clay		
Moist density	$\gamma_{\text{mb}} = 18$ kN/m <sup>3</sup>		
Characteristic effective shear resistance angle		$\phi'_{\text{b.k}} = 18$ deg	
Characteristic wall friction angle		$\delta_{\text{b.k}} = 9$ deg	
Characteristic base friction angle		$\delta_{\text{bb.k}} = 12$ deg	
Presumed bearing capacity	$P_{\text{bearing}} = 100$ kN/m <sup>2</sup>		

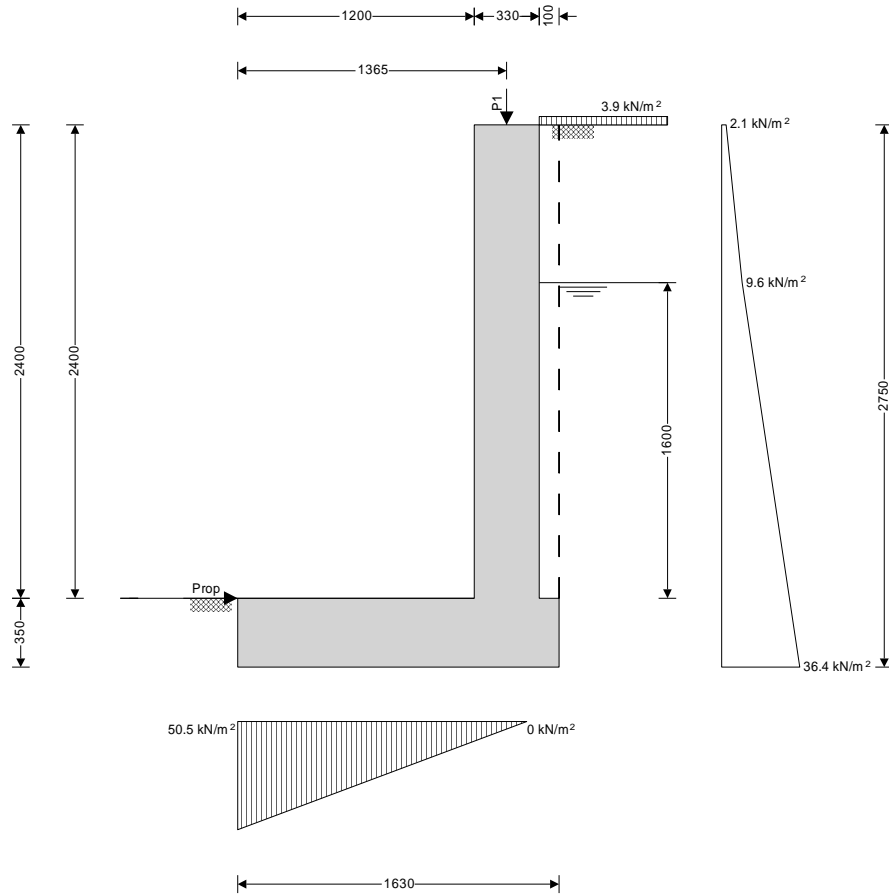
#### Loading details

Variable surcharge load	Surcharge <sub>Q</sub> = 3 kN/m <sup>2</sup>
Vertical line load at 1365 mm	$P_{G1} = 35.6$ kN/m



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### Calculate retaining wall geometry

Base length	$l_{base} = 1630$ mm	Vertical distance	$x_{stem} = 1365$ mm
Saturated soil height	$h_{sat} = 1600$ mm	Vertical distance	$x_{base} = 815$ mm
Moist soil height	$h_{moist} = 800$ mm	Vertical distance	$x_{sat\_v} = 1580$ mm
Length of surcharge load	$l_{sur} = 1000$ mm	Horizontal distance	$x_{sat\_h} = 650$ mm
Vertical distance	$x_{sur\_v} = 1580$ mm	Vertical distance	$x_{water\_v} = 1580$ mm
Effective height of wall	$h_{eff} = 2750$ mm	Horizontal distance	$x_{water\_h} = 650$ mm
Horizontal distance	$x_{sur\_h} = 1375$ mm	Vertical distance	$x_{moist\_v} = 1580$ mm
Area of wall stem	$A_{stem} = 0.792$ m <sup>2</sup>	Horizontal distance	$x_{moist\_h} = 1186$ mm
Area of wall base	$A_{base} = 0.571$ m <sup>2</sup>		
Area of saturated soil	$A_{sat} = 0.16$ m <sup>2</sup>		
Area of water	$A_{water} = 0.16$ m <sup>2</sup>		
Area of moist soil	$A_{moist} = 0.08$ m <sup>2</sup>		

### Using Coulomb theory

Active pressure coefficient	$K_A = 0.483$	Passive pressure coefficient	$K_P = 2.359$
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### Bearing pressure check

#### Vertical forces on wall

Total  $F_{total\_v} = F_{stem} + F_{base} + F_{sat\_v} + F_{moist\_v} + F_{water\_v} + F_{sur\_v} + F_{P\_v} = 74$  kN/m



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### Horizontal forces on wall

Total  $F_{total\_h} = F_{sat\_h} + F_{moist\_h} + F_{water\_h} + F_{sur\_h} = 44.4$  kN/m

### Moments on wall

Total  $M_{total} = M_{stem} + M_{base} + M_{sat} + M_{moist} + M_{water} + M_{sur} + M_P = 54.3$  kNm/m

### Check bearing pressure

Propping force  $F_{prop\_base} = 44.4$  kN/m

Bearing pressure at toe  $q_{toe} = 50.5$  kN/m<sup>2</sup>      Bearing pressure at heel  $q_{heel} = 0$  kN/m<sup>2</sup>

Factor of safety  $FoS_{bp} = 1.981$

**PASS - Allowable bearing pressure exceeds maximum applied bearing pressure**

### RETAINING WALL DESIGN

In accordance with EN1992-1-1:2004 incorporating Corrigendum dated January 2008 and the UK National Annex incorporating National Amendment No.1

Tedds calculation version 2.4.08

### Concrete details - Table 3.1 - Strength and deformation characteristics for concrete

Concrete strength class	C32/40		
Char.comp.cylinder strength	$f_{ck} = 32$ N/mm <sup>2</sup>	Mean axial tensile strength	$f_{ctm} = 3.0$ N/mm <sup>2</sup>
Secant modulus of elasticity	$E_{cm} = 33346$ N/mm <sup>2</sup>	Maximum aggregate size	$h_{agg} = 20$ mm
Design comp.concrete strength		$f_{cd} = 18.1$ N/mm <sup>2</sup>	Partial factor $\gamma_c = 1.50$

### Reinforcement details

Characteristic yield strength	$f_{yk} = 500$ N/mm <sup>2</sup>	Modulus of elasticity	$E_s = 200000$ N/mm <sup>2</sup>
Design yield strength	$f_{yd} = 435$ N/mm <sup>2</sup>	Partial factor	$\gamma_s = 1.15$

### Cover to reinforcement

Front face of stem	$C_{sf} = 20$ mm	Rear face of stem	$C_{sr} = 75$ mm
Top face of base	$C_{bt} = 20$ mm	Bottom face of base	$C_{bb} = 75$ mm

### Check stem design at base of stem

Depth of section  $h = 330$  mm

### Rectangular section in flexure - Section 6.1

Design bending moment	$M = 36.1$ kNm/m	$K = 0.019$	$K' = 0.207$
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**$K' > K$  - No compression reinforcement is required**

Tens.reinforcement required	$A_{sr.req} = 354$ mm <sup>2</sup> /m	Tens.reinforcement provided	$A_{sr.prov} = 1005$ mm <sup>2</sup> /m
Min.area of reinforcement	$A_{sr.min} = 388$ mm <sup>2</sup> /m	Max.area of reinforcement	$A_{sr.max} = 13200$ mm <sup>2</sup> /m

**PASS - Area of reinforcement provided is greater than area of reinforcement required**

### Crack control - Section 7.3

Limiting crack width	$w_{max} = 0.3$ mm	Maximum crack width	$w_k = 0.165$ mm
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### PASS - Maximum crack width is less than limiting crack width Rectangular section in shear - Section 6.2

Design shear force	$V = 45.6$ kN/m	Design shear resistance	$V_{Rd.c} = 128.1$ kN/m
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**PASS - Design shear resistance exceeds design shear force**

### Horizontal reinforcement parallel to face of stem - Section 9.6

Min.area of reinforcement	$A_{sx.req} = 330$ mm <sup>2</sup> /m	Max.spacing of reinforcement	$s_{sx.max} = 400$ mm
Trans.reinforcement provided	10 dia.bars @ 200 c/c	Trans.reinforcement provided	$A_{sx.prov} = 393$ mm <sup>2</sup> /m

**PASS - Area of reinforcement provided is greater than area of reinforcement required**

### Check base design at toe

Depth of section  $h = 350$  mm



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**Rectangular section in flexure - Section 6.1**

Design bending moment  $M = 43.1$  kNm/m  $K = 0.019$   $K' = 0.207$   
***K' > K - No compression reinforcement is required***

Tens.reinforcement required  $A_{bb.req} = 391$  mm<sup>2</sup>/m  
Tens.reinforcement provided 16 dia.bars @ 200 c/c Tens.reinforcement provided  $A_{bb.prov} = 1005$  mm<sup>2</sup>/m  
Min.area of reinforcement  $A_{bb.min} = 420$  mm<sup>2</sup>/m Max.area of reinforcement  $A_{bb.max} = 14000$  mm<sup>2</sup>/m  
***PASS - Area of reinforcement provided is greater than area of reinforcement required***

**Crack control - Section 7.3**

Limiting crack width  $w_{max} = 0.3$  mm Maximum crack width  $w_k = 0.2$  mm

***PASS - Maximum crack width is less than limiting crack width*** Rectangular section in shear - Section 6.2

Design shear force  $V = 65.8$  kN/m Design shear resistance  $V_{Rd.c} = 137$  kN/m  
***PASS - Design shear resistance exceeds design shear force***

**Rectangular section in flexure - Section 6.1**

Design bending moment  $M = 0.2$  kNm/m  $K = 0.000$   $K' = 0.207$   
***K' > K - No compression reinforcement is required***

Tens.reinforcement required  $A_{bt.req} = 1$  mm<sup>2</sup>/m  
Tens.reinforcement provided 12 dia.bars @ 200 c/c Tens.reinforcement provided  $A_{bt.prov} = 565$  mm<sup>2</sup>/m  
Min.area of reinforcement  $A_{bt.min} = 509$  mm<sup>2</sup>/m Max.area of reinforcement  $A_{bt.max} = 14000$  mm<sup>2</sup>/m  
***PASS - Area of reinforcement provided is greater than area of reinforcement required***

**Crack control - Section 7.3**

Limiting crack width  $w_{max} = 0.3$  mm Maximum crack width  $w_k = 0$  mm

***PASS - Maximum crack width is less than limiting crack width*** Rectangular section in shear - Section 6.2

Design shear force  $V = 3.3$  kN/m Design shear resistance  $V_{Rd.c} = 153.1$  kN/m  
***PASS - Design shear resistance exceeds design shear force***

**Secondary transverse reinforcement to base - Section 9.3**

Min.area of reinforcement  $A_{bx.req} = 201$  mm<sup>2</sup>/m Max.spacing of reinforcement  $S_{bx,max} = 450$  mm  
Trans.reinforcement provided 10 dia.bars @ 200 c/c Trans.reinforcement provided  $A_{bx.prov} = 393$  mm<sup>2</sup>/m  
***PASS - Area of reinforcement provided is greater than area of reinforcement required***



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