

55 GLOUCESTER AVENUE, LONDON, NW1 7BA

PROPOSED BASEMENT CONSTRUCTION UNDER PART OF THE FRONT GARDEN (IN AREA OF EXISTING VAULTS), REAR AREA UNDER EXISTING GARAGE AND REBUILD OF EXISTING RETAINING WALLS

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INTRODUCTION.

The property is a large four storey, semi detached dwelling probably constructed in the latter part of the 19th century.

The basement development proposal has three parts:

- 1. Construct a basement under part of the front garden. This will involve removing the existing vaults under the front garden. It should be noted that the rear wall of the existing vaults has collapsed and that the vaults are structurally unsound and liable to collapse. The vaults are only under the front garden so there is no current danger to the public. The new basement structure will have a slightly larger footprint than the existing vaults.
- 2. Construct a new rear lower ground floor area. This new area will be roughly below the area of the existing garage and will have a floor at the same level as the existing lower ground under the main house.
- 3. Rebuild the retaining walls to the lightwells to the existing lower ground floor. The existing lightwell retaining walls are showing signs of failure with buckling/deformation on the inner faces. There appear to have been some attempts at repair.

Details of the proposals are shown by the relative James Wyman Architects drawings.

The purpose of this report / statement is to provide details of the stage 1 and 2 BIA as requested by the 'Camden Planning Guidance Basements and Light wells', together with details of the method and sequence of construction.

STAGE 1 - SCREENING FOR BIA- Reference Camden Planning Guidance Basements and Lightwells

Figure 1. Subterranean (ground water) flow screening chart.

Q1a Is the site located directly above an aquifer?

NO. See figure 8, site above 'unproductive strata'

Q1b Will the proposed basement extend below the water table surface?

NO. Formation of new basement is at - 4.25m below ground level, site investigation has borehole was dry to -6.0m below ground level.

Q2. Is the site within 100m of a watercourse, well or potential spring line?

NO. With reference to figure 12 the site is not within 100m of any of these features.

Q3. Is the site within the catchment of the pond chains on Hampstead Heath.

NO. Refer to figure 14.

Q4. Will the proposed basement development result in a change in the proportion of hard surfaced paved areas.

NO. Basement is below footprint of existing building, and below garden. Front area replaces existing vaults.



- Q5. As part of the site drainage will more surface water than at present be discharged into the ground.
- NO. There is no increase in impermeable area.
- Q6. Is the lowest point of the proposed excavation close to or lower than the mean level in any pond or spring line.
- NO. There are no nearby ponds or spring lines.

Figure 2. Slope Stability Screening Flow Chart.

- Q1. Does the existing site include slopes natural or manmade greater than 70
- NO. Site is level.
- Q2. Will the proposed re-profiling of the landscaping at site change slopes at the boundary to more than 7°
- NO. There are no re-profiling works.
- Q3. Does the development neighbour land have slopes greater than 7°.
- **NO.** Neighbouring land is level
- Q4. Is the site within a wider hillside with general slopes greater than 7° .
- NO. Site is within a wider level area.
- Q5 Is the London Clay the shallowest strata on the site.
- **NO**. Site Investigation describes highest strata as made ground over a silty sandy clay which is believed to be the Claygate Beds. This overlays the stiff London Clay
- Q6. Will any trees be felled or are any of the works within root zones of protected trees?
- NO. No trees will be felled.
- Q7. Is there a history of seasonal shrink swell subsidence in the area? And evidence that this affects the site.
- **NO**. Site examination of buildings did not reveal evidence of subsidence due to shrink / swelling of soils.
- Q8. Is the site within 100m of a watercourse or a potential spring line?
- NO. Site is not within 100m of such features
- Q9. Is the site within an area of previously worked ground?
- **NO**. The site is presently a dwelling within its own land.
- Q10. Is the site within an aquifer?
- NO. See figure 8, site above 'unproductive strata'
- Q11. Is the site within 50m of Hampstead Heath Ponds?
- NO. Site is within South Camden
- Q12 Is the site within 5m of a highway or pedestrian Way.
- **YES**. Gloucester Avenue footpath is 0.5m away from the front of the proposed extension to the front vaults. The St Mark's Crescent footpath is approximately 3.5m away from the proposed rear extension. As described in the Design Philosophy the structural elements at subterranean level will be designed to accommodate the loading from the Public Highway.



Q.13 Will the proposed basement significantly increase the differential depth of foundations to the relative properties.

NO. Increase in depth of foundations will be 700mm which in terms of foundation formations is not significant.

Q. 14. Is the site over any tunnels?

NO. No tunnels are known to exist under the site.

Figure 3. Surface Flow and Flooding Screening Flowchart.

- Q1. Is the site within the catchment of the pond chains on Hampstead Heath.
- NO. Site is in South Camden.
- Q2. As part of the proposed site drainage will surface water flows be materially changed from the existing route?
- **NO**. The existing surface water routes will not be changed by the development.
- Q. 3. Will the proposed basement development result in a change in the proportion of hard surfaced / paved external areas.
- **NO**. The development does not increase the impermeable paved areas.
- Q4. Will the basement result in changes to the profiles of the inflows of surface water being received by adjacent properties or downstream watercourses.
- **NO**. The development does not increase the impermeable paved areas.
- Q5. Will the proposed basement result in changes to the quality of surface water being received by adjacent properties or downstream watercourses.
- **NO**. The presence of the basement structure will not alter the quality of the surface water.
- Q6. Is the site in an area known to be at risk of flooding?

Yes. Areas of Gloucester Avenue were flooded during the August 1975 storm. The development will not add to the risk of or be affected by surface flooding.

STAGE 2 - SCOPING FOR BIA- Reference Camden Planning Guidance Basements and Lightwells

Figure 2.

Q12 Is the site within 5m of a highway or pedestrian Way.

YES. Gloucester Avenue footpath is within 0.5m of the extended front vaults. The St Mark's Crescent footpath is approximately 3.5m away from the proposed rear extension. As described in the Design Philosophy the structural elements at subterranean level will be designed to accommodate the loading from the Public Highway.

The structural element design and stability of the walls and base to the front vaults will be made to accommodate a surcharge load of 10KN/m² or wheel load of 100KN which ever gives the most onerous loading.

The structural elements for the rear basement area will not be subject to surcharge load from the footpath / Public Highway.

Design of final structure and temporary elements within the method of construction will be made to minimise ground movement laterally, refer to method statement for construction.

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Figure 3. Surface Flow and Flooding Scoping Flowchart.

Q6. Is the site in an area known to be at risk of flooding?

YES. Camden Planning Guidance on page 29 lists Gloucester Avenue as being flooded in August 1975. This occurred 39 years ago due to surcharge of existing drains during a storm and it is assumed that drainage improvements have been made to improve the situation. 'The Camden Flood Risk Management Strategy' describes the improvements and strategy to maintain the overall area surface water drainage system.

The basement will be protected from water / moisture by an internal cavity drainage layer (Delta membrane system or similar approved), gravity drainage will not effectively be linked to the basement therefore the external drainage system will not be able to surcharge the new basement.

It should be noted that this is not a self contained apartment.

STAGE 3 - SITE INVESTIGATION AND STUDY- Reference Camden Planning Guidance Basements and Lightwells

The site is assessed as low risk.

A geological desk top study and a site specific borehole have been completed. Both are attached at the end of this document with the borehole also included as a separate document.



STAGE 4 - IMPACT ASSESSMENT- Reference Camden Planning Guidance Basements and Lightwells

<u>Attribute</u>	Change from baseline	Comment		
Geological / land stability	Nil	Ground is flat lying, made ground over firm London Clay.		
		The underlying London Clay is effectively impermeable.		
Hydrogeological	Nil to not significant	The upper made ground is permeable howver there is currently no water in this layer and any water that is in this layer has a path around the proposed development. Furthermore the proposed construction level is not lower than the existing 19th century original lower ground level which does not have any sign of water ingress.		
		There is negligible increase in impermeable area. The front basement area replaces the area of the		
Hydrological	Nil	main vaults with a slight increase to towards the perimeter but not of significance in the context of the size of the front garden and the area already covered by hard standing.		
Hydrological (surface water)		The rear basement area replaces an area of hard standing and garage.		
		The proposed lightwell retaining walls and bases replace the existing lightwells plus a slight (approximately 200mm) width increase which is not significant within the conext of the size of the unbuilt area of the front garden.		
Structural to own	NEI	The proposed development does not undermine the foundations of the existing property.		
property	Nil	No structural work is being undertaken to the existing main house.		
Structural to		The proposed development does not undermine the foundations of the neighbouring properties either on Gloucester Avenue or St Mark's Crescent.		
neighbouring properties / highway	Nil / improve	The public footpath and highway on the Gloucster Avenue are currently partially undermined by the unsound existing front vaults. The front basement will replace the failing vaults and improve the structural stability.		

The impact of the development is considered low and a full BIA is not considered necessary .



STRUCTURAL DESIGN PHILOSOPHY FOR CONSTRUCTION OF FRONT AND REAR BASEMENT AREAS

External Walls

Extended lower ground floor external walls below the property are designed as propped cantilevers in reinforced concrete, the lower ground floor slab acting as the prop at base level. The walls will be designed using the soil parameters noted in the site investigation report. The walls will be designed for a water table 3/4h above the base of the stem in accordance with the relevant Code Of Practice.

The surcharge load allowed on the external walls of the property will be 10KN/m^2 . The party wall bounding will have a surcharge load of 5.00KN/m^2 for adjoining floor and partition wall construction and will also take into account any loads from adjoining foundations. The vault structure within the front garden will be designed as necessary for a surcharge load of 10KN/m^2 or 100 KN wheel load, whichever gives the most onerous design case.

Basement Slab

The slab will be formed in reinforced concrete. It will be designed for uplift due to water pressure below, or as a clear span as appropriate. The basement slab will act as a prop to the base of the basement walls.

Design Criteria.

Basement walls and bases will be designed using the parameters for the retained soils and bearing soils as indicated by the Site Investigation. The design is in accordance with BS 8002:1994.

The design will accommodate active and passive earth pressures. Pressure coefficients in the design will adopt 'at rest pressures'.

The wall and base in designed for the following

- 1. Vertical loads from walls above.
- 2.Party wall will be designed for a surcharge loading of 5kN/m².
- 3. Other external will be designed with a surcharge load of 10.00KN/m².
- 4. The design adopts a water head behind the wall to $\frac{3}{4}$ the height of the wall below ground in accordance with BS 8102.
- 5. Front vault areas will be designed for a surcharge of 10KN/m² or a wheel load of 100KN, which ever is most onerous.



The Site Investigation describes the sub soils at new basement formation level as London Clay, an SBP of 150KN/m² will be used in the design to limit differential foundation movements.

Concrete will generally be grade C35 and Class 1 to BRE Digest 363. Reinforcement will be grade 500N/mm².

Existing brickwork assumes 7N bricks in a lime mortar, CP.111 gives basic compressive stress for this makeup of 0.45N/mm², and therefore allowable bearing stress will be 0.45N/mm². Any bearings into existing external or party wall masonry will take account of this allowable stress.

Mortar will be class (ii) or (iii) as required.

Relevant Codes of Practice and British Standards

B.S. 8004	Code of Practice For Foundations
B.S. 6031	Code of Practice For Earthworks
B.S. 8110	Structural Use of Concrete
B.S. 5750	Structural Use of Steelwork in Buildings

BRIEF METHOD STATEMENT FOR CONSTRUCTION.

The exact sequence of works will be agreed with Main Contractor and Structural Engineer, a Construction Method Statement for the works could be as follows.

- a) The walls to the perimeter of the new/existing rooms will be underpinned in reinforced concrete. The underpins will take the vertical loads from the walls and horizontal loads from the earth. During their construction the walls and bases will require laterally propping in the temporary condition; propping will be made against the central earth pudding.
- b) Underpinning legs will be excavated in short sections not exceeding 1200mm in width.
- c) The sequence of the underpinning will be in the 1, 3, 5, 2, 4 sequence and such that any given underpin will be completed, dry packed, and a minimum period of 48 hours lapsed before an adjacent excavation commenced to form another underpin.
- d) In the event that the existing foundations to the wall are found to be unstable, sacrificial steel jacks will be installed underneath the foundation to prop the bottom few courses of bricks. These steel jacks will be left in place and will be incorporated into the concrete stem.
- e) Whilst forming the wall and in the event that the vertical soil face is unstable, lateral propping will be provided as required to the excavation and to the sides of the working trench. The front and side faces of the excavation will be propped using a sacrificial inert board and acrow props as appropriate.
- f) Concrete will be chuted from the point of delivery into a 'holding bath' within the working areas and placed by wheelbarrow and /or bucket, or mixed on site. The exact arrangement will be finalised when works commence on site.



- g) Excavation for an underpin section will be excavated in a day, and the concrete to the base poured by the end of the same day.
- h) The concrete to the wall of the underpin will be poured the following day. This will be poured up to within 50 75mm of the underside of the existing wall foundations.
- i) On the following day, the gap between the concrete and the underside of the existing foundation will be dry packed with a mixture of sharp sand and cement (ratio 3 : 1).
- j) Once the dry pack has gained sufficient strength, any protrusions of the footings into the site will be carefully trimmed back using hand tools to avoid causing any damage to the foundation. The protrusions will be trimmed back to be flush in-line with the face of the wall above.
- k) A minimum of 24 hours will be allowed before adjacent sections will be excavated to form a new underpin.
- I) Once all pins are complete a temporary cross propping system will be introduced between the walls to allow bulk excavation will be carried out down to formation level.
- m) The below slab drainage for foul & ground water, sumps and pumps will then be installed. The pumps will discharge the foul / ground water into the sewer system to the front of the properties. The drainage layout will be designed in due course.
- n) The basement slab will then be constructed, once cured this will provided the designed propping to the walls and the temporary cross propping can be removed.
- o) A cavity drainage layer will be laid to the slabs and walls.

CONSTRUCTION SEQUENCE

- 1. Site set up will include a hoarding to the front garden; placement for skips will either be made within the front garden or on the public highway subject to Camden approval.
- 2. The site is accessible from Gloucester Avenue and St Mark's Crescent. Site deliveries and operations will take place from St Mark's Crescent. This entrance will be manned throughout operational hours by a banksman to ensure construction deliveries do not pose a risk to other users of St Mark's Crescent or Gloucester Avenue.
- 3. Construct site hoarding, entrance gates to provide protection to passers-by from site operations. Site accommodation including welfare facilities will be confined to the main building throughout the site works.
- 4. Terminate / protect any incoming services temporarily divert any active drainage.
- 5. Install any tree protection measures as necessary.
- 6. Install enclosed skip to front on property and install conveyor to remove excavated soil to discharge soil into skip.
- 7. Remove walls at existing lower ground floor level and fix permanent temporary steel beams to support existing ground floors that remain.
- 8. Reduce existing lower ground floor and vault levels to just above existing footing formation.
- 9. Underpins will be carried out in the usual 1, 4, 2, 5, 3 underpinning sequence, the construction sequence for forming the pin will be agreed prior to commencement of the works. To provide temporary lateral support to the wall formed it will remain propped against the internal soil 'dumpling.'



- 10. On completion of all underpinning, cross propping of the pin walls will be erected to allow bulk excavation. The propping will be designed to suit the lateral loads behind the walls but generally takes the form of a series of horizontal slimlite props adequately laced and braced set approximately 1.5m from lower ground floor level.
- 11. Bulk excavation will be carried out down to new lower ground floor formation level. Soil will continue to be removed from site via the conveyor belt.
- 12. In parallel with the above actions works will commence to rear lower ground floor extension.
- 13. The rear lower ground floor area will be formed in two drives. Initially a reinforced councrete wall section will be formed to approximately 1.0m below ground level, once the ring of the wall is formed the ground within the ring will be reduced at the same time lateral propping of the walls will be provided, either propping from a central pudding or cross propping between wall, or a combination of both. The wall section will then be underpinned in a hit a miss arrangement to form the base and lower wall section. Once complete further reduction of the internal ground levels can be made whilst adapting the lateral propping to suit the revised form.
- 14. The below slab drainage for foul & ground water, sumps and pumps will then be installed. The pumps will discharge the foul / ground water into the sewer system to the front of the properties. The drainage layout will be designed in due course.
- 15. The basement slab (ground bearing slab) will then be constructed.
- 16. After the new basement slabs have cured, the cross propping will be removed.

17. A drained – cavity layer will be laid to the slabs and walls.

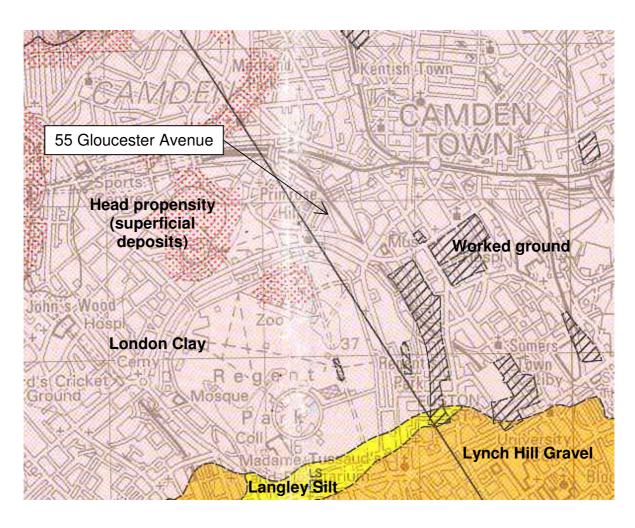
T. J. Vincent BSc C.Eng M.I.Struct E. 15 July 2014

T.J Vincont

55 GLOUCESTER AVENUE, LONDON. NW1 7BA. BASEMENT IMPACT ASSESSMENT JULY 2014.



GEOLOGICAL DESK TOP STUDY





SITE INVESTIGATION

endeavour drilling									WS1	
GEO ENVIRONMENTAL DRILLING SPECIALISTS								Sheet 1 of 1		
Project Name: Project No.						Co ordo:	Hole Type			
55 Gloucester Avenue J2384						Co-ords: -	WS			
Location: London NW1 7BA						Level: _	Scale 1:50			
Client: Basement Force								Dates: 02/07/2014	Logged By OW	
/ell	Water Strikes	Sampl Depth (m)		Situ Testing Results	Depth (m)	Level (m AOD)	Legend	Stratum Description		
	E	0.30	ES		0.20		*****	Light grey CONCRETE MADE GROUND - Dark greyish brown slightly cla	avev sitty very	
		0.70-0.80	ES		0.60			gravelly fine to medium sand with occasional coa glass and metal fragments. Gravel is angular to s to coarse brick flint and concrete.	rse gravel size	
	1	1.00-1.20 1.20	D SPT	N=11 (3,3,2,2,3,4)	1.00			MADE GROUND - Firm light brown slightly grave dessicated clay with rare rootlets. Gravel is sub a rounded fine to coarse flint and brick.	lly silty sandy ngular to sub	
		1.60-1.80	ES	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				MADE GROUND - Firm locally soft dark brown m orangish brown slightly sandy sitty gravelly clay. sub angular to sub rouded fine to coarse flint bric	Gravel is	
	_2	2.00	SPT	N=15 (4,4,3,4,4,4)				sub angular to sub rouded line to coarse film brid	Kandasii.	
		0.50.0.70							-	
		2.50-2.70	D						Ė	
	-3	3.00	SPT	N=8 (1,2,2,1,2,3)				locally soft from 3.00mbgl.	-	
		3.50-3.70	D		3.70			Soft light brown mottled orangish brown and light	grav elightly	
	-4	3.80-4.00 4.00	SPT	N=7 (1,1,2,2,1,2)				sandy silty CLAY.	grey siignuy	
		4.50-4.70	D		4.40			Firm dark greyish brown mottled bluish grey sligh CLAY.	tly sandy silty	
	5	5.00	SPT	N=16 (3,2,4,5,4,3)					Ė	
	6	5.80-6.00	D		6.00			End of Borehole at 6.00 m		
	- - -7									
									ŀ	
	-8									
	-						-			
	9									
	-									
em	arks:	 Bread No g 	king ou	it to 0.20mbgl.	Hand	dug ins	pection	oit excavated from 0.20m to 1.20mbg	I prior to sampling.	